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# Fatigue behavior of Dual-Phase and TWIP steels for lightweight automotive structures

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## **Overall** aims

- To characterize and compare mass-produced (*Dual Phase*), innovative (*TWIP*), and experimental high strength steels for car weight reduction
- To facilitate the industrialization of these new steels, with regards to both production processes and service requirements
- To study these steels fatigue crack growth behavior, which may in future be considered in the car-body design and verification, in pursuit of further weight reductions, as it now happens in aeronautic design

# Steel sheets for car bodies (I) **Desired properties**

Higher strength

Lower fuel consumption  $\rightarrow$  lower weight  $\rightarrow$  Less pollution (Euro 4 – 5 ...) Increased load (commercial vehicles) Lower cost

*Plastic energy absorption*  $\rightarrow$  *car-crash safety* 

Fatigue endurance  $\rightarrow$  ordinary car service

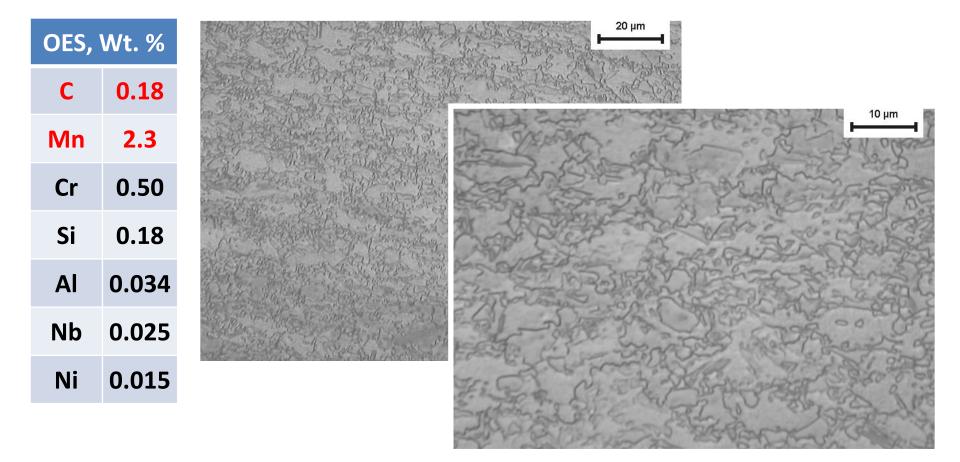
**Ductility, weldability**  $\rightarrow$  production processes

Steel sheets for car bodies (II) *Most common overall production cycle* 

- High-strength weldable steel sheets are made by:
  - continuous casting
  - hot rolling
  - cold rolling
  - continuous final heat treatment
  - protective coating (Zn)
- Sheets are cold formed to produce car body parts
- Car bodies are assembled by resistance spot welding

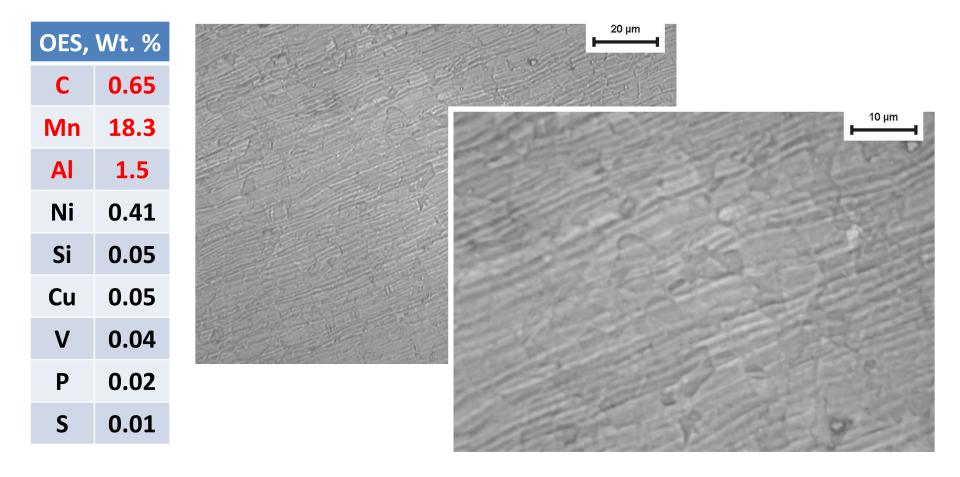
## Examined **Dual Phase** (**DP**) steel

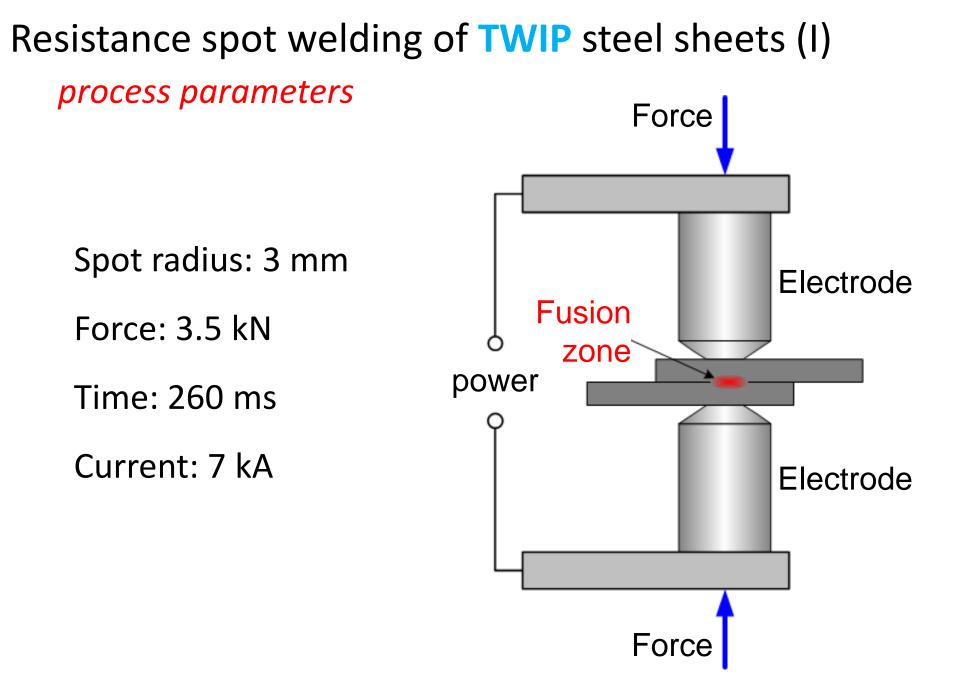
- widely used
- low alloy, ferrite and martensite microstructure
- made by intercritical annealing and quenching after cold rolling

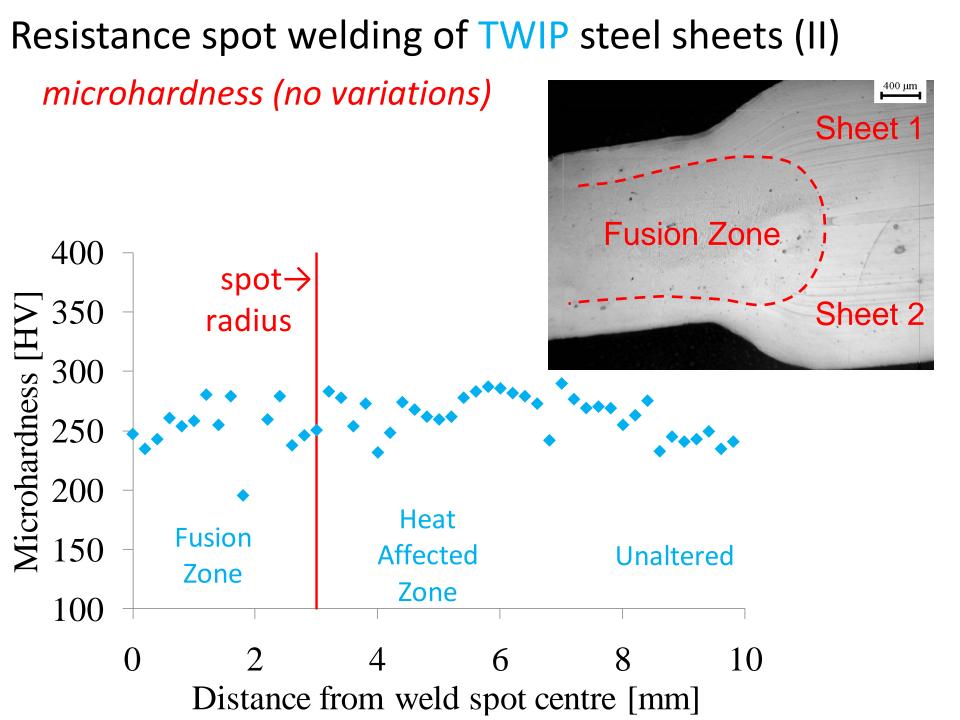


## Examined TWIP steel

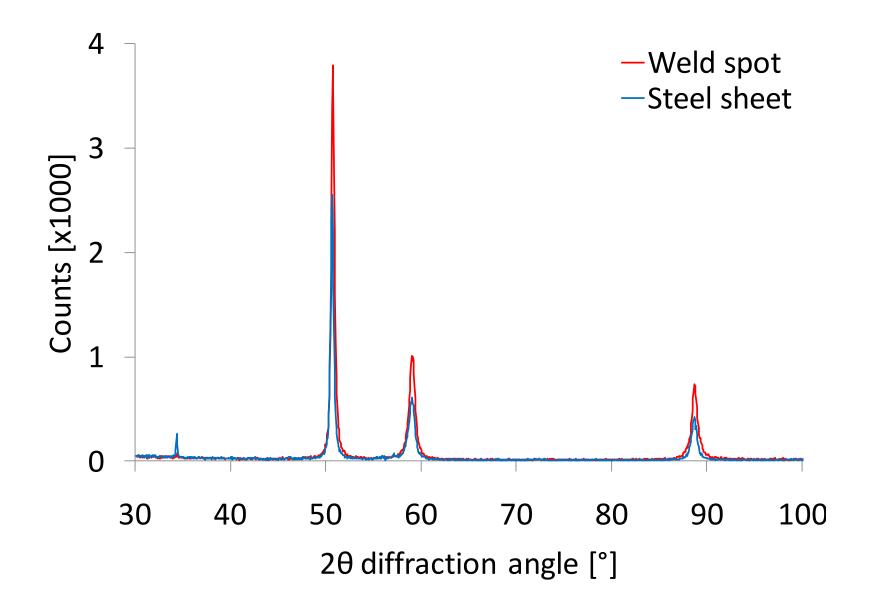
- not yet widely used
- ductile, high-Mn austenite strengthened with solute C
- TWinning Induced Plasticity (TWIP) effect



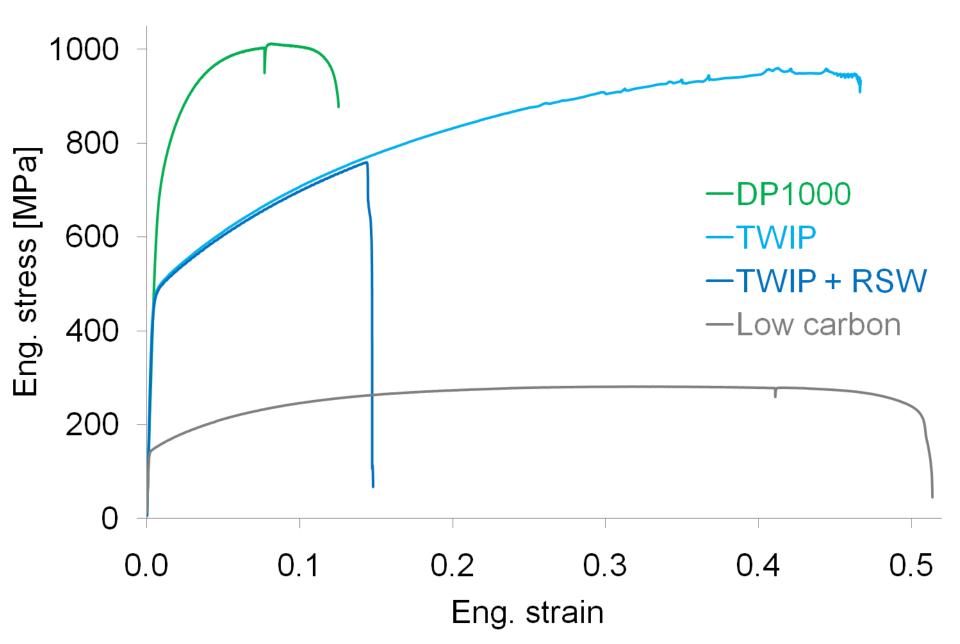




Resistance spot welding of TWIP steel sheets (III) X-ray diffraction (austenite only)



### Tensile curves



## S-N fatigue - procedures

- 20 mm wide, full thickness tensile specimens
- constant load amplitude fatigue tests
- Ioad ratio ≈ 0 (minimum load = 50 N)
- ✤ 10<sup>6</sup> cycles fatigue limit (o<sub>D</sub>), staircase method

#### As-fabricated -

#### **DP1000**

> as-fabricated (with Zn coating)

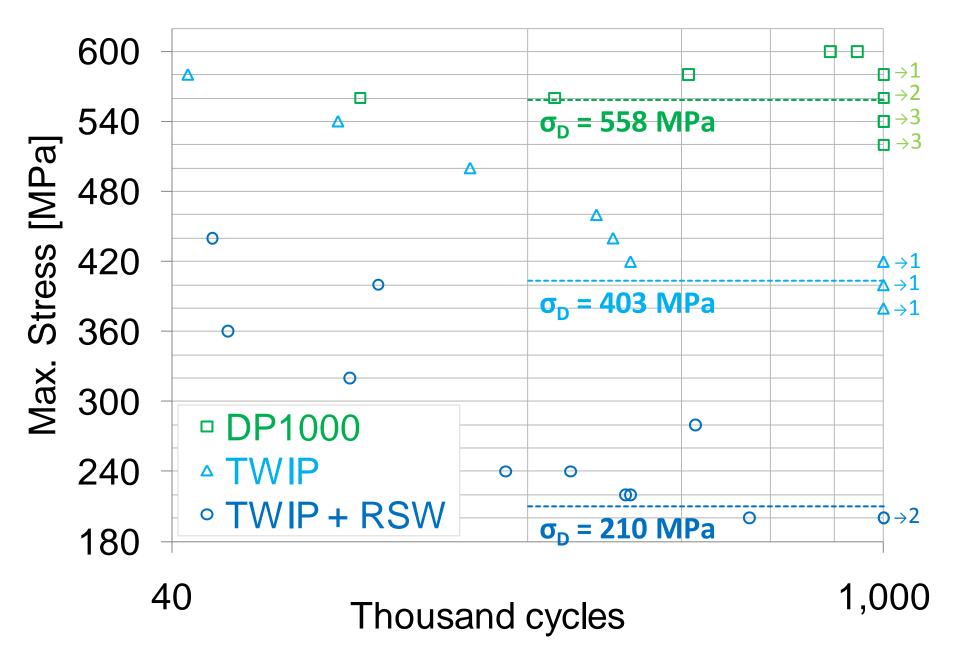
#### TWIP

- > as-fabricated (uncoated)
- with one RSW spot at mid-length (joining a 20 mm sheet square)

#### with ← RSW spot ↓



## S-N fatigue - results



## S-N fatigue – optical fractography

DP1000,  $\sigma_{max} = 600$  MPa, 888,842 cycles

Final (slant) fracture

Fatigue nucleation

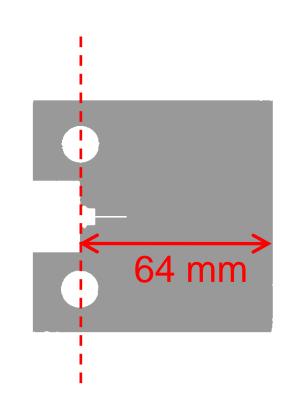
Fatigue crack propagation

## Paris fatigue - procedure

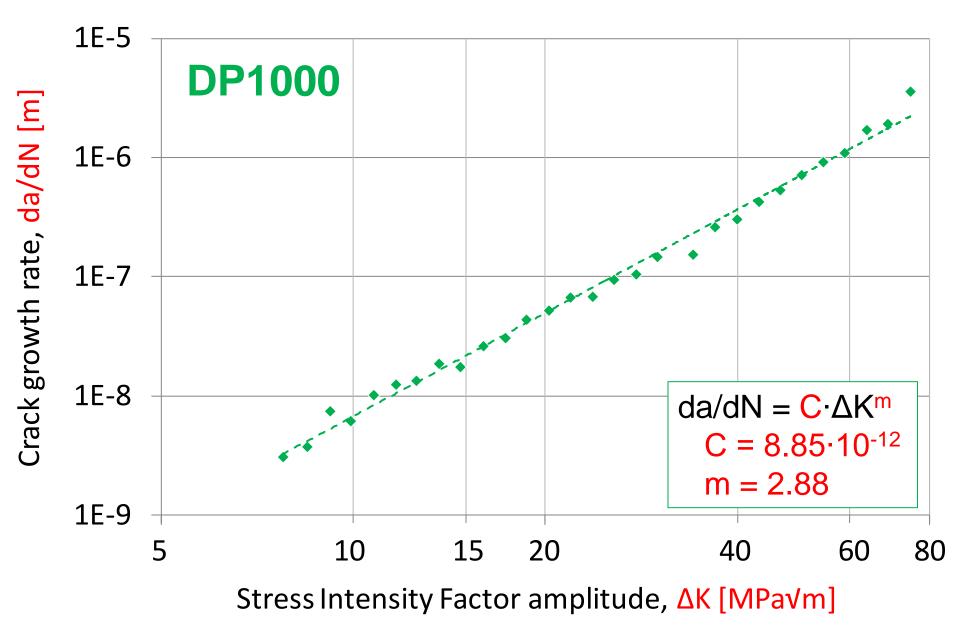
- polished Compact Tension (CT) specimens
- ♦ width W=64 mm, thickness B=1.7 mm, B/W≈ 1/38
- pre-cracking & fatigue crack growth as per ASTM E647
- ΔK-increasing procedure:
  ΔK-incr
  - Ioad-controlled fatigue steps
  - ➤ ≈ 0.3 mm crack growth per step
  - ➤ ≈ 8% ΔK increase between steps

Load ratio = 0.1

Optical crack-length measurements



Paris fatigue - results



## **Conclusions & Future Work**

- The TWIP steel (0.65% C, 18% Mn, 1.5% Al) exhibits remarkable UTS (≈ 950 MPa) and ductility (≈ 50%), but a lower fatigue limit (403 MPa at 1 million cycles) than a dual phase steel with similar strength
- RSW welding spots greatly reduce the TWIP steel strength, ductility, and fatigue resistance, even if the weld microstructure is similar to the base metal
- A Paris plot was successfully obtained for a dual phase steel sheet, notwithstanding the quite reduced thickness
- Further tests are needed for a thorough characterization and comparison of the examined steels



# Thank you for your attention!

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