

Advanced Fiber Optic-Based Sensing Technology for Unmanned Aircraft Systems



**Dr. Lance Richards, Allen R. Parker, Anthony Piazza,
Dr. William L. Ko, Dr. Patrick Chan, and John Bakalyar**

Dryden Flight Research Center, Edwards, CA

UAS Payloads Conference

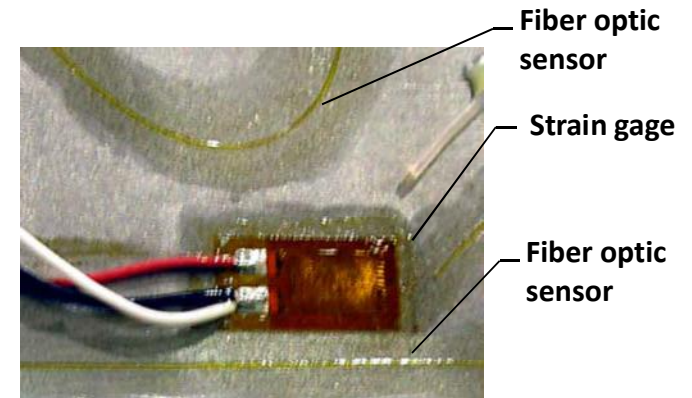
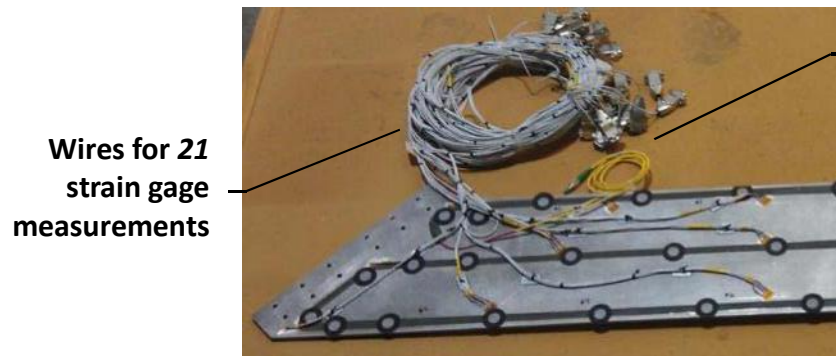
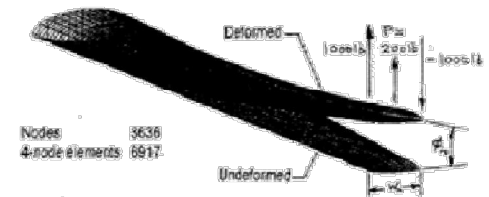
San Diego, CA

11/16/2011

Fiber Optic Sensing for UAS Applications Advantages over Conventional Measurements

- **Unrivaled density of sensors for spatially distributed measurements**
- **Measurements immune to EMI, RFI and radiation**
- **Lightweight sensors**
 - Typical installation is 0.1 - 1% the weight of conventional gage installations (based on past trade studies)
 - 1000's of sensors on a single fiber (up to 80 feet per fiber)
 - No copper wires
- **With uniquely developed algorithms, these sensors can determine out-of-plane displacement and load at points along the fiber**
- **Small fiber diameter**
 - Approximately the diameter of a human hair
 - Unobtrusive installation
 - Fibers can be bonded externally or applied as a 'Smart Layer' top ply
- **Single calibration value for an entire lot of fiber**
- **Wide temperature range (cryo – 550F)**

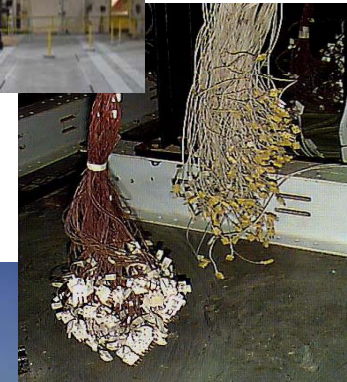
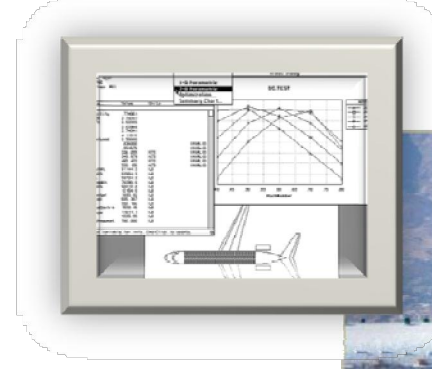
$$r_n = \frac{\Delta l^2}{6\epsilon} \left\{ (3n-1)r_n + 6 \sum_{i=1}^{n-1} (n-i)r_i + r_n \right\}$$



Fiber Optic Sensing for UAS Applications

Anticipated Impact

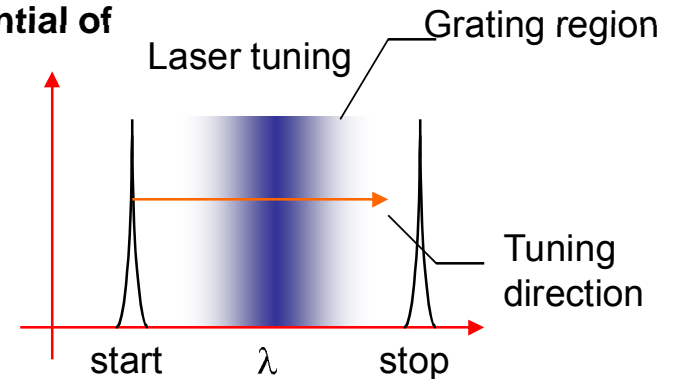
- **Potential to revolutionize UAV design and performance throughout the life-cycle**
 - *Design and development*
 - *Production*
 - *Test and Evaluation*
 - *In-flight operation*
 - *Off-nominal flight*
 - *End of life-cycle decisions*



Fiber Optic System Operation Overview

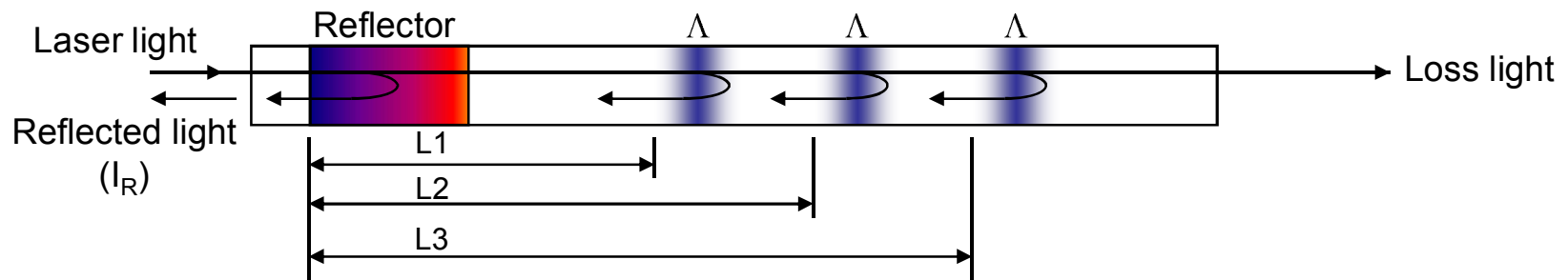
Fiber Optic Sensing with Fiber Bragg Gratings

- Immune to electromagnetic / radio-frequency interference and radiation
- Lightweight fiber-optic sensing approach having the potential of embedment into structures
- Multiplex 100s of sensors onto one optical fiber
- Fiber gratings are written at the same wavelength
- Uses a narrowband wavelength tunable laser source to interrogate sensors
- Typically easier to install than conventional strain sensors
- In addition to measuring strain and temperature these sensors can be use to determine shape



$$I_R = \sum_i R_i \cos(k2nL_i) \quad k = \frac{2\pi}{\lambda}$$

R_i – spectrum of i^{th} grating
 n – effective index
 L – path difference
 k – wavenumber

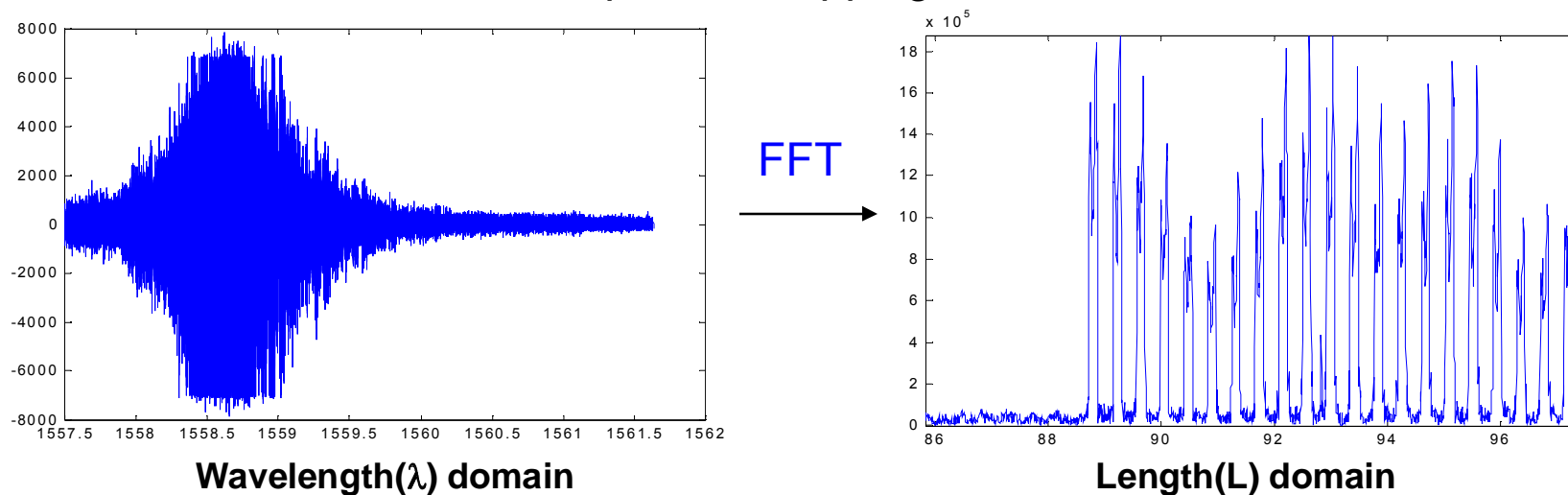


Fiber Optic System Operation Overview

- Fourier transforms (both forward and inverse) are used to discriminate between gratings
- The Fourier transform separates the I_R waveform into sinusoids of different frequency which sum to the original waveform

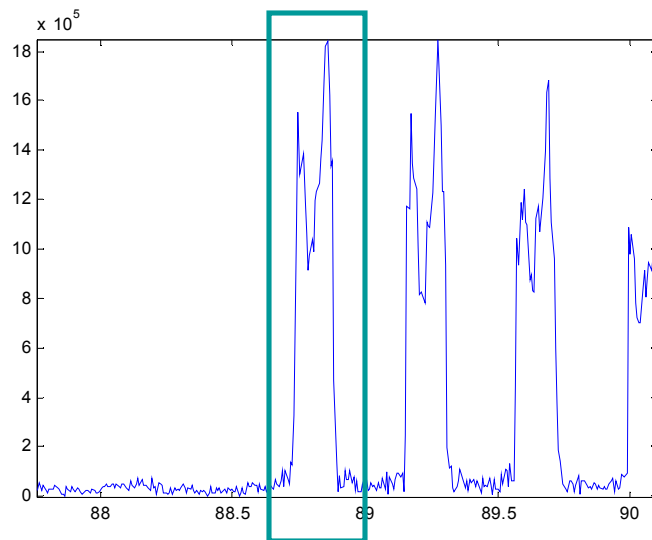
	FFT	iFFT
Traditional	Time(T) > Frequency(F)	Frequency(F) > Time(T)
Optical	Wavelength(λ) > Length(L)	Length(L) > Wavelength(λ)

Spectral Mapping



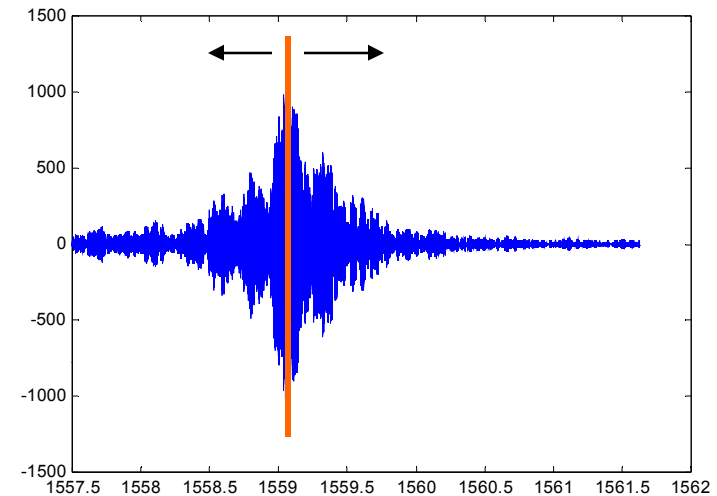
Fiber Optic System Operation Overview

- By bandpass filtering around a specific frequency (grating location) within the length domain and performing an iFFT, the spectrum of each grating can be independently measured and strain inferred (FM radio)



Length(L) domain (inches)

iFFT
→



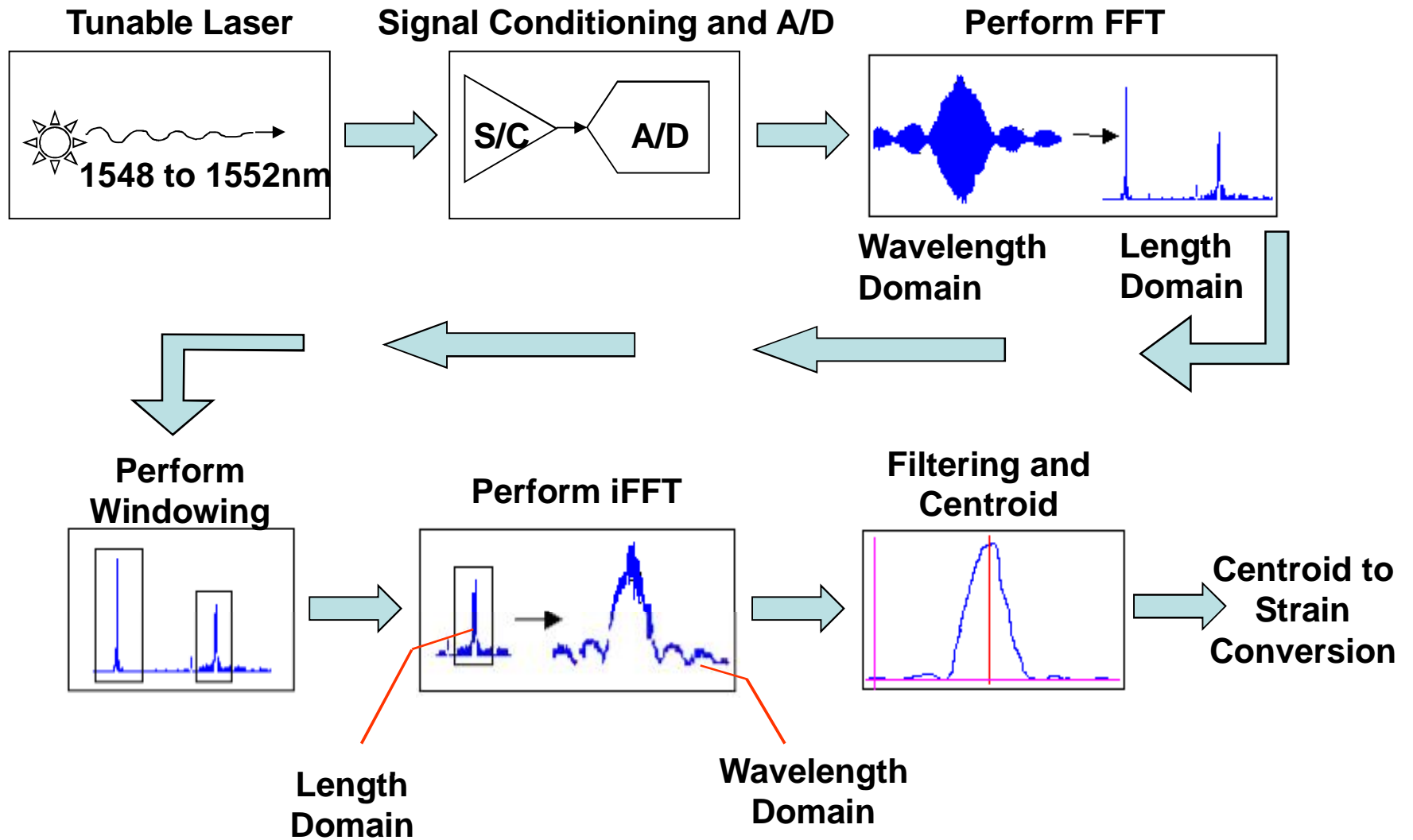
Wavelength(λ) domain

- Using a centroid function the center wavelength can be resolved
- The wavelength change is proportional to the induced strain

$$\frac{\Delta\lambda}{\lambda} = K\varepsilon$$

K – proportionality constant (0.7-0.8)

Interrogation Process



Research and Technology Development Areas

– Algorithm Development

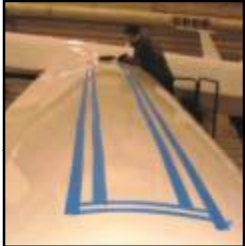
– FBG System Development

– Instrumentation

– Ground Testing / R&D

– Flight Testing

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\varepsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\varepsilon_i + \varepsilon_n \right\}$$

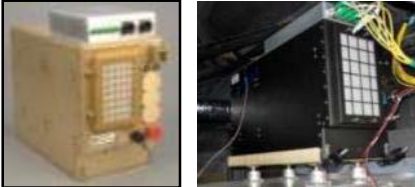
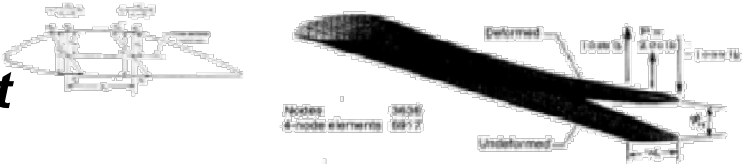


Research and Technology Development Areas

– Algorithm Development

- **Real-time wing shape measurement using fiber optics sensors**
(Ko, Richards; Patent 7,715,994)
- **Real-time applied loads on complex structures using fiber optic sensors**
(Richards, Ko; Patent 7,520,176)
- **Data processing algorithms**
(Parker, US Patent Pending)

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\epsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\epsilon_i + \epsilon_n \right\}$$



Real-time Wing Shape Measurement

Motivation – Helios UAV



Helios wing dihedral on takeoff

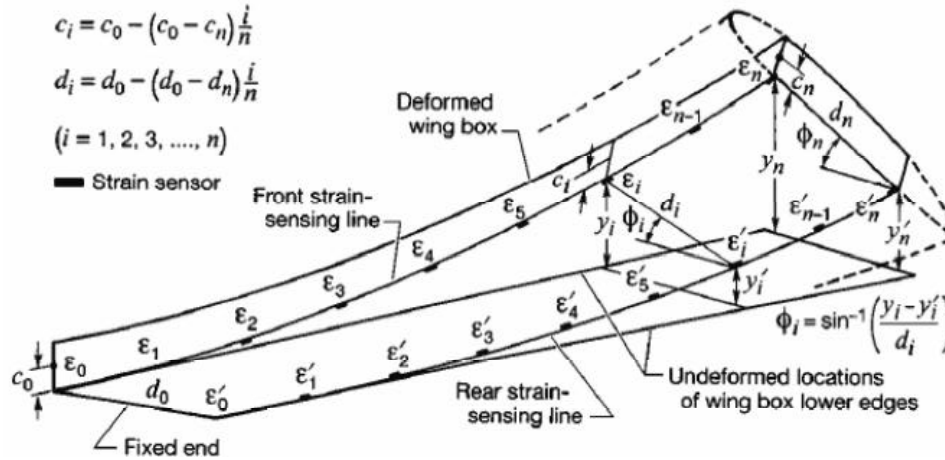


In-flight breakup

Helios Mishap Report – Lessons Learned

- Measurement of wing dihedral in real-time should be accomplished with a visual display of results available to the test crew during flight
- Procedure to control wing dihedral in flight is necessary for the Helios class of vehicle

Real-time Wing Shape Measurement Theoretical Development



Deflection of a Single Fiber:

$$y_i = \frac{(\Delta l)_i^2}{6c_{i-1}} \left[\left(3 - \frac{c_i}{c_{i-1}} \right) \varepsilon_{i-1} + \varepsilon_i \right] + y_{i-1} + (\Delta l)_i \tan \theta_{i-1}$$

Typically the first station is at the root:

$$y_0 = \tan \theta_0 = 0$$

Slope:

$$\tan \theta_i = \frac{(\Delta l)_i}{2c_{i-1}} \left[\left(2 - \frac{c_i}{c_{i-1}} \right) \varepsilon_{i-1} + \varepsilon_i \right] + \tan \theta_{i-1}$$

Real-time Wing Shape Measurement

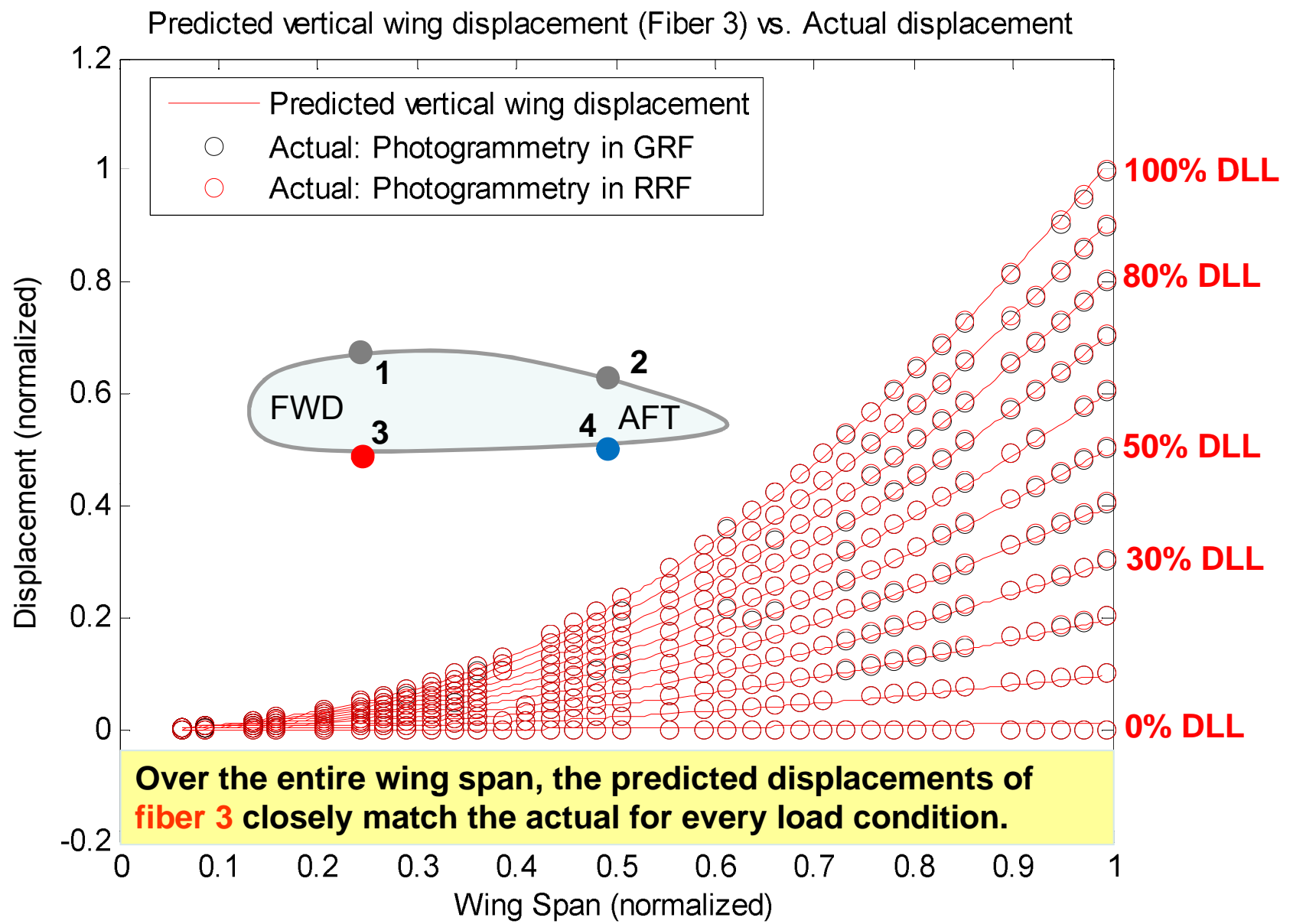
Global Observer – Algorithm Validation Testing

- **Strain gages**
 - Validate the FBGs
 - Not used for shape prediction, used for structural evaluation
- **Photogrammetry**
 - Provided validation information for wing shape prediction
 - Measures actual displacement vectors at target points
 - 10 photogrammetry images taken per load condition



Real-time Wing Shape Measurement

Global Observer – Algorithm Validation Testing



Real-Time Externally-Applied Loads Approach

- **Bending moment calculated at each analysis station**
- **Cross-sectional properties calculated by applying known load**
 - EI/c term backed out at each evaluation station
- **With properties known, strain can be directly related to bending moment**



Known moment

Measure strains

$$\frac{M}{\epsilon} = \left(\frac{EI}{c} \right)$$

Get properties at each station



Unknown moment

Measure strains

$$\left(\frac{EI}{c} \right) \cdot \epsilon = M$$

Calculate moment at each station

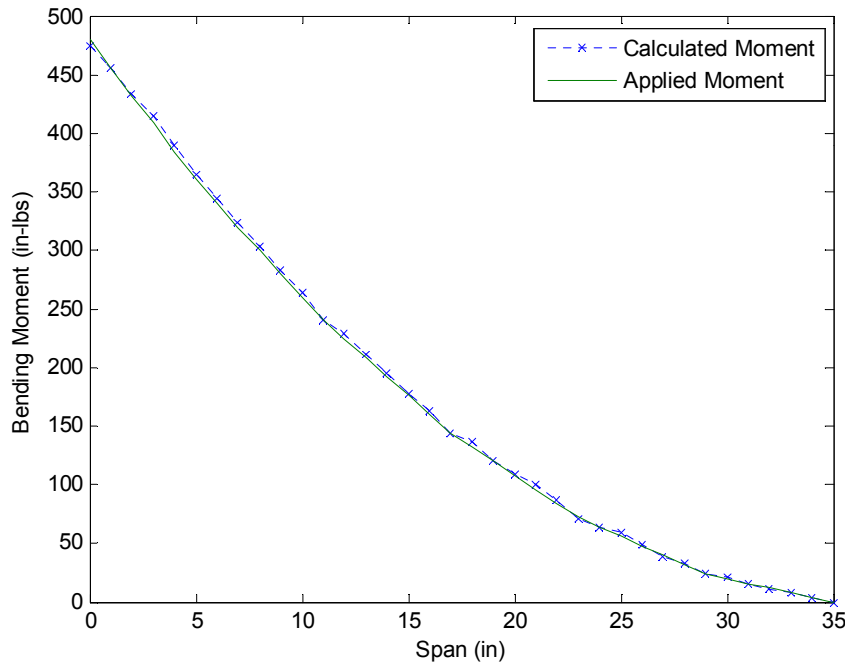
Real-Time Externally-Applied Loads

Swept Plate Loads Testing

Cross-sectional properties calculated using *Uniform* load calibration

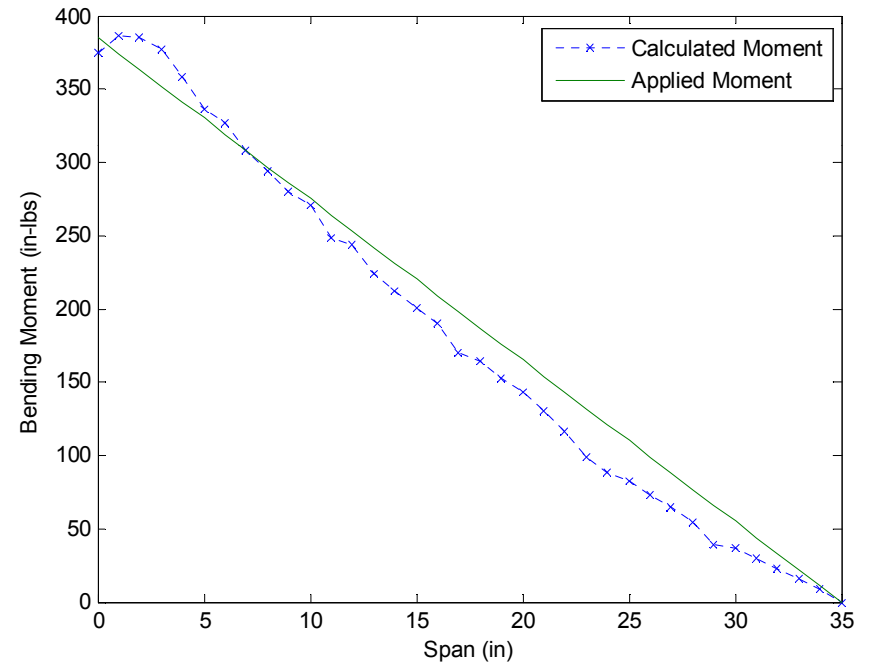
Uniform Load Case

$$M = \left(\frac{EI}{c} \right)_{UniformA} \cdot \epsilon_{UniformB}$$



Single Point Load Case

$$M = \left(\frac{EI}{c} \right)_{UniformA} \cdot \epsilon_{SinglePt}$$



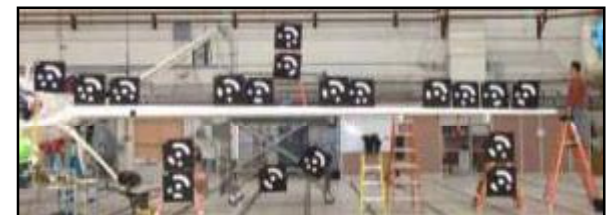
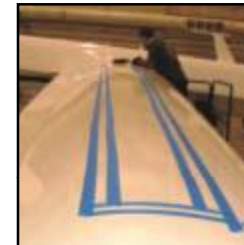
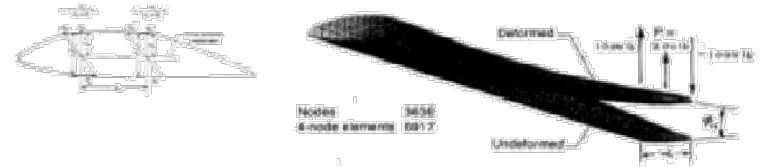
Wing Shape and Externally-Applied Loads Results

- **Deflection calculations are accurate (within ~5%)**
 - Different test articles
 - Different load cases
 - Different load magnitudes
- **Load results will be improved**
 - Least-squares method
- **Developing methods to further use FOSS measurements**
 - Angle-of-twist
 - Improved deflection and load
 - Torque

Research and Technology Development Areas

- Algorithm Development
- **FBG System Development**
- Instrumentation
- Ground Testing / R&D
- Flight Testing

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\varepsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\varepsilon_i + \varepsilon_n \right\}$$

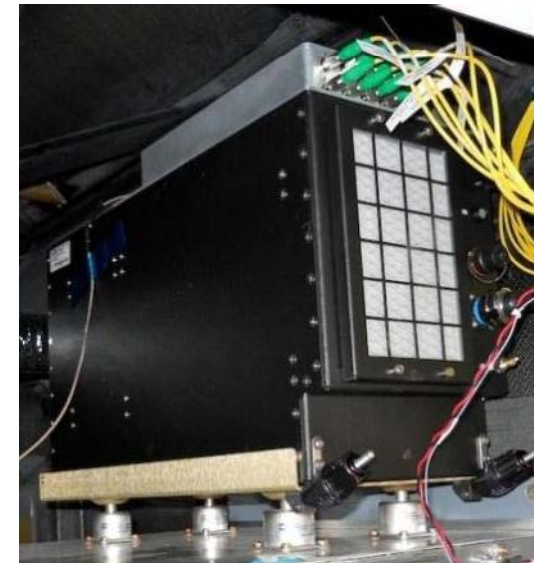


NASA Technology FOSS Systems (4DSP)

- **Technical Highlights**
 - 4DSP has licensed NASA technology to commercially develop FOSS systems
 - <http://www.4dsp.com/RTS150.php>
 - Single laser greatly reduces cost per sensor
 - High fiber count systems
 - Modular design with 8 channels per card
 - Expandable
 - Up to 32 fibers possible
 - Up to sensing 80 feet per fiber
 - 11" x 7" x 12"
 - 100 Hz max sample rate
 - Lightweight system for multitude of sensors
 - Approximately 25 lbs
- **Cost**
 - 8 fiber system approx \$100K
 - Up to 16,000 sensors
 - 32 fiber system approx \$150K
 - Up to 64,000 sensors
 - System can be flight-certified (+\$30K)
 - Low power requirements (<10 Amps at 28 Volts DC)
- **Applications**
 - Transport Aircraft, Ships, Civil Structures



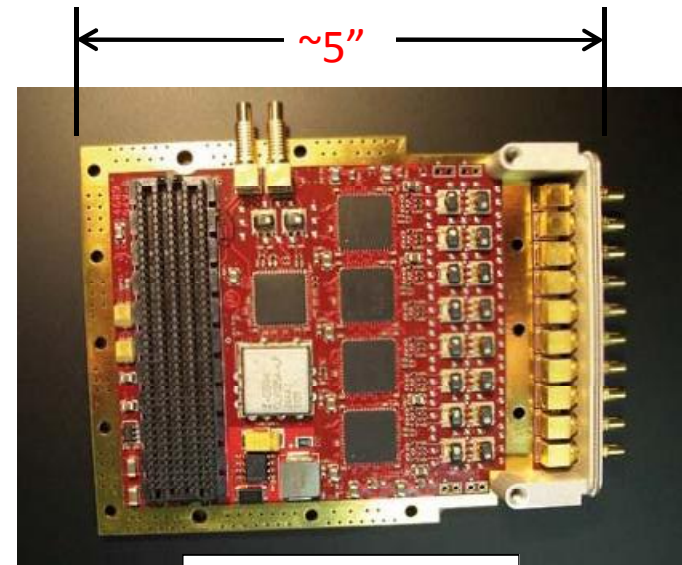
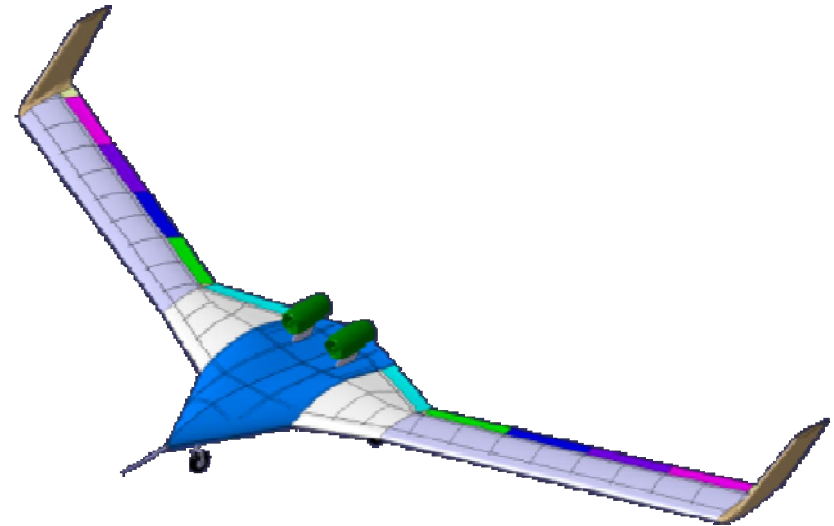
Ground system



Flight system

Compact FOSS (cFOSS) System In Development

- **Lightweight, ruggedized system**
 - Packaged within a 6" cube
- **Targeted specifications:**
 - Fiber count: 8
 - Max Fiber length: 80 ft
 - Max # sensors/system: 15,360
 - Max Sample rate: 100 Hz
 - Power: 50W @ 28Vdc
 - Weight: <10 lbs
 - Size: 5 x 6 x 6 in
 - Vibration and Shock: NASA Curve B
 - Altitude: 65kFt
- **Applications:**
 - Fighter aircraft
 - UAVs
 - Launch vehicles
 - Spacecraft
- **Target system cost: \$50K**
- **Availability: End of 2012**



8-Fiber Card

Large Scale FOSS (LsFOSS) Technology

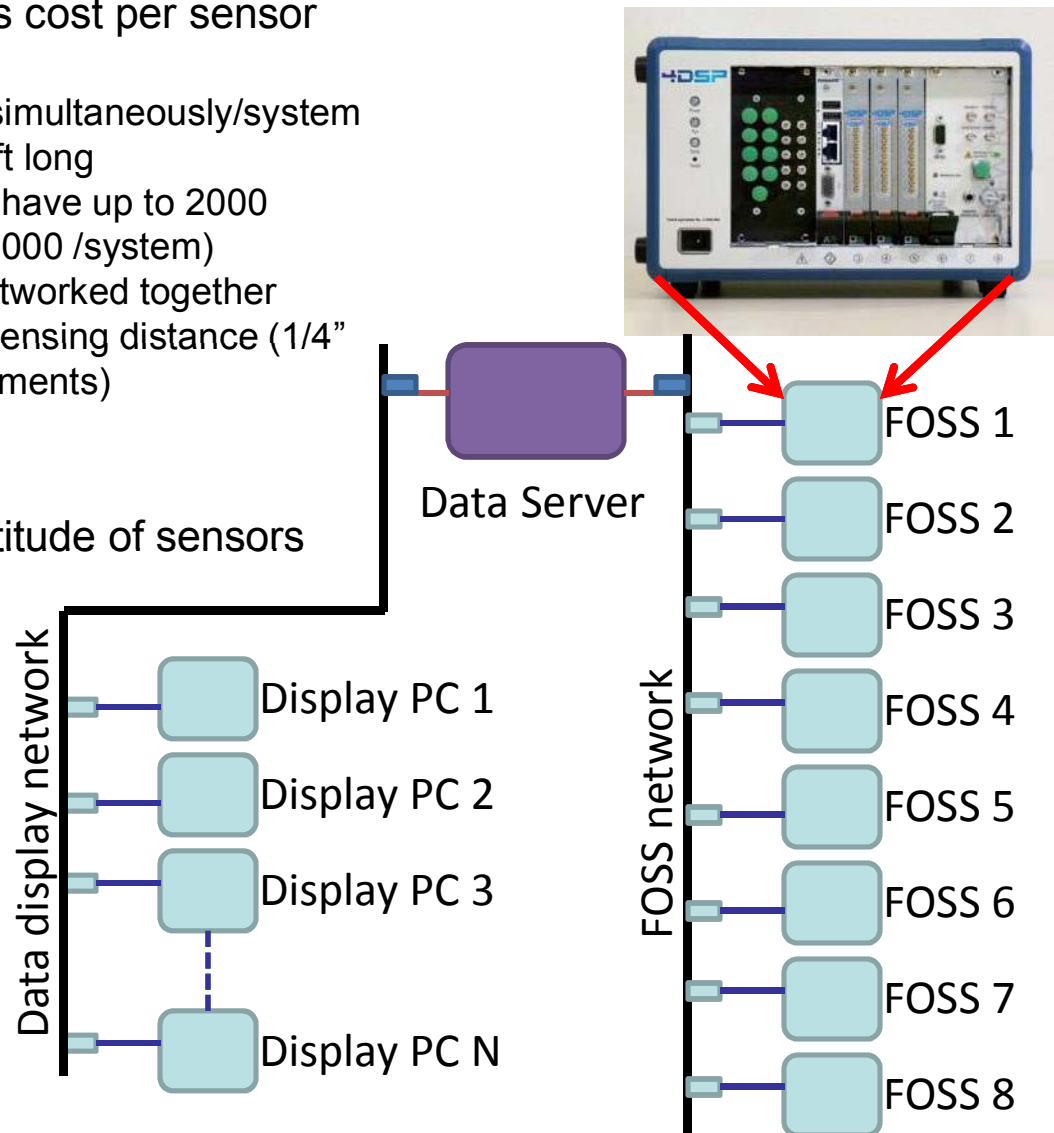
• Technical Highlights

- Single laser greatly reduces cost per sensor
- High fiber count systems
 - Up to 16 fibers monitored simultaneously/system
 - Each fiber can be up to 40ft long
 - Each fiber at 40ft long can have up to 2000 measurements (total of 32,000 /system)
 - Up to 8 systems can be networked together yielding approx. 1 mile of sensing distance (1/4" spacing, 256,000 measurements)
- 11" x 7" x 12"
- 100 Hz max sample rate
- Lightweight system for multitude of sensors
 - Approximately 25 lbs

• Applications:

- Transport Aircraft
- Ships
- Civil Structures
- Ground Testing
- Structures Laboratory

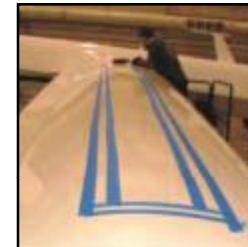
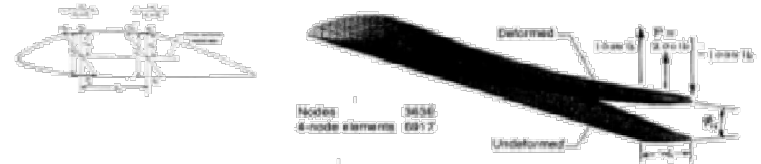
FOSS Ground System



Research and Technology Development Areas

- Algorithm Development
- FBG System Development
- Instrumentation
- Ground Testing / R&D
- Flight Testing

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\varepsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\varepsilon_i + \varepsilon_n \right\}$$



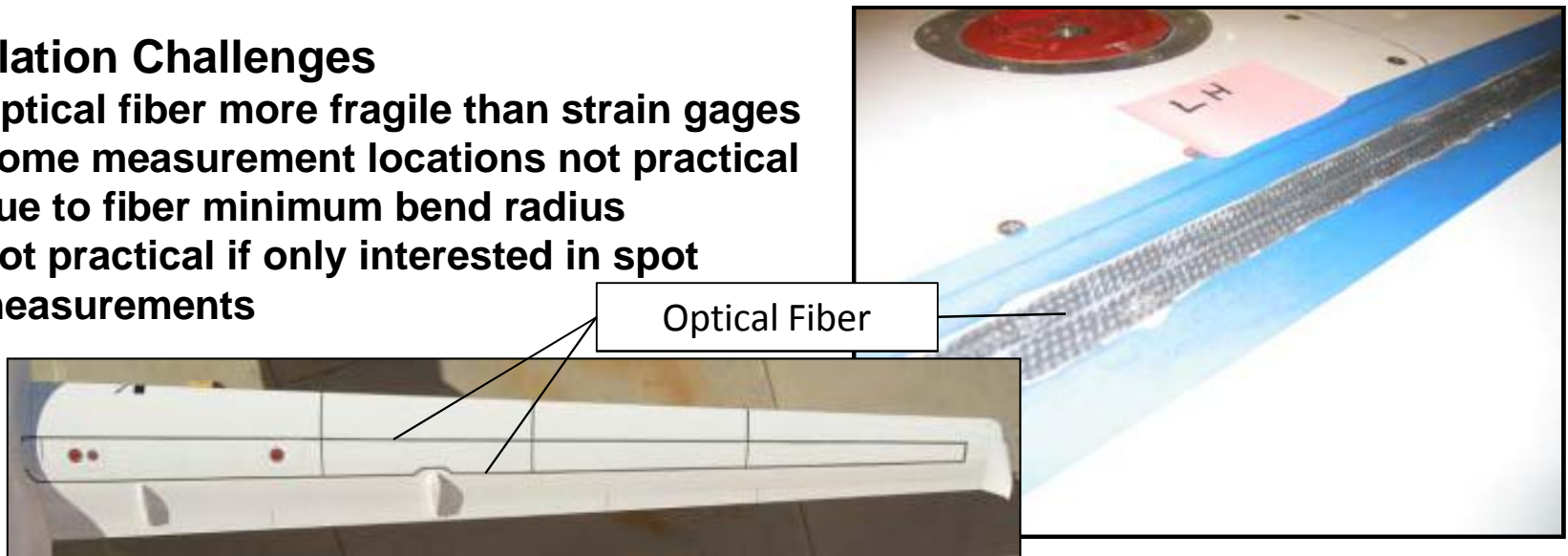
FOSS Installation Advantages and Challenges

Installation Advantages

- **Greatly reduced installation time compared to conventional strain gages**
 - 2 man-days for 40' fiber (1000 strain sensors for a continuous surface run)
 - Multiple sensors installed simultaneously
 - Same surface preparation and adhesives as conventional strain gages
 - Minimal time spent working on vehicle
 - All connectors can be added prior to installation, away from part
 - No soldering
 - No clamping pressure required
 - Circular cross-section eliminates possibility of trapping air between sensor and part (eliminates repeat installations)
- **Can be installed with little or no impact to OML**

Installation Challenges

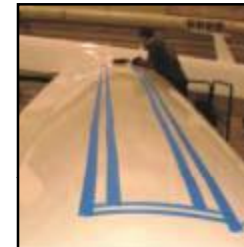
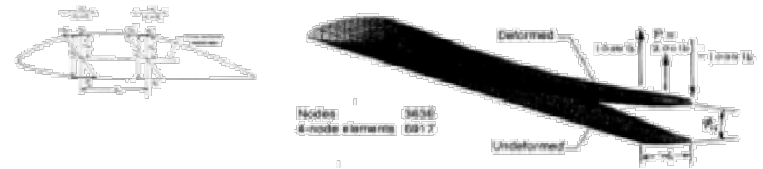
- **Optical fiber more fragile than strain gages**
- **Some measurement locations not practical due to fiber minimum bend radius**
- **Not practical if only interested in spot measurements**



Research and Technology Development Areas

- Algorithm Development
- FBG System Development
- Instrumentation
- **Ground R&D**
- Flight Testing

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\varepsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\varepsilon_i + \varepsilon_n \right\}$$



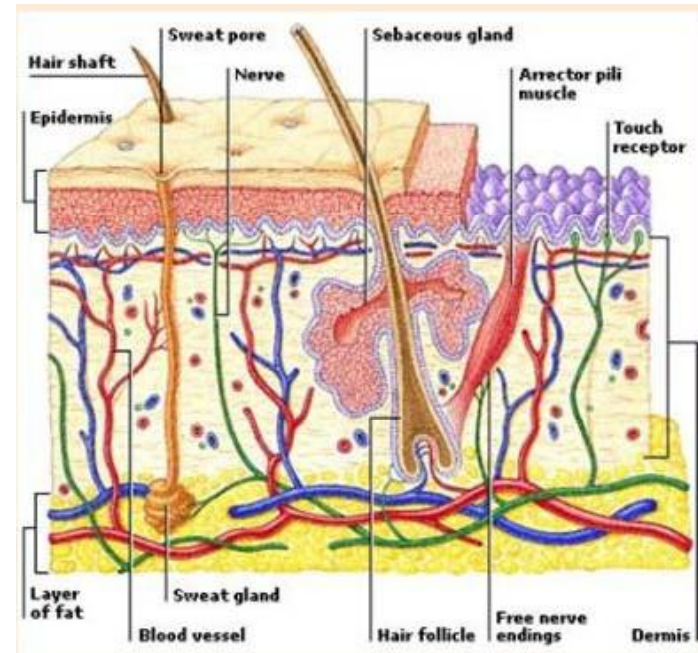
Embedment of Fiber Optic Sensors within Composites

Biological Inspiration of FOSS

Human Skin

- Four yards of nerve fibers
- 600 pain sensors
- 1300 nerve cells
- 9000 nerve endings
- 36 heat sensors
- 75 pressure sensors
- 100 sweat glands
- 3 million cells
- 3 yards of blood vessels

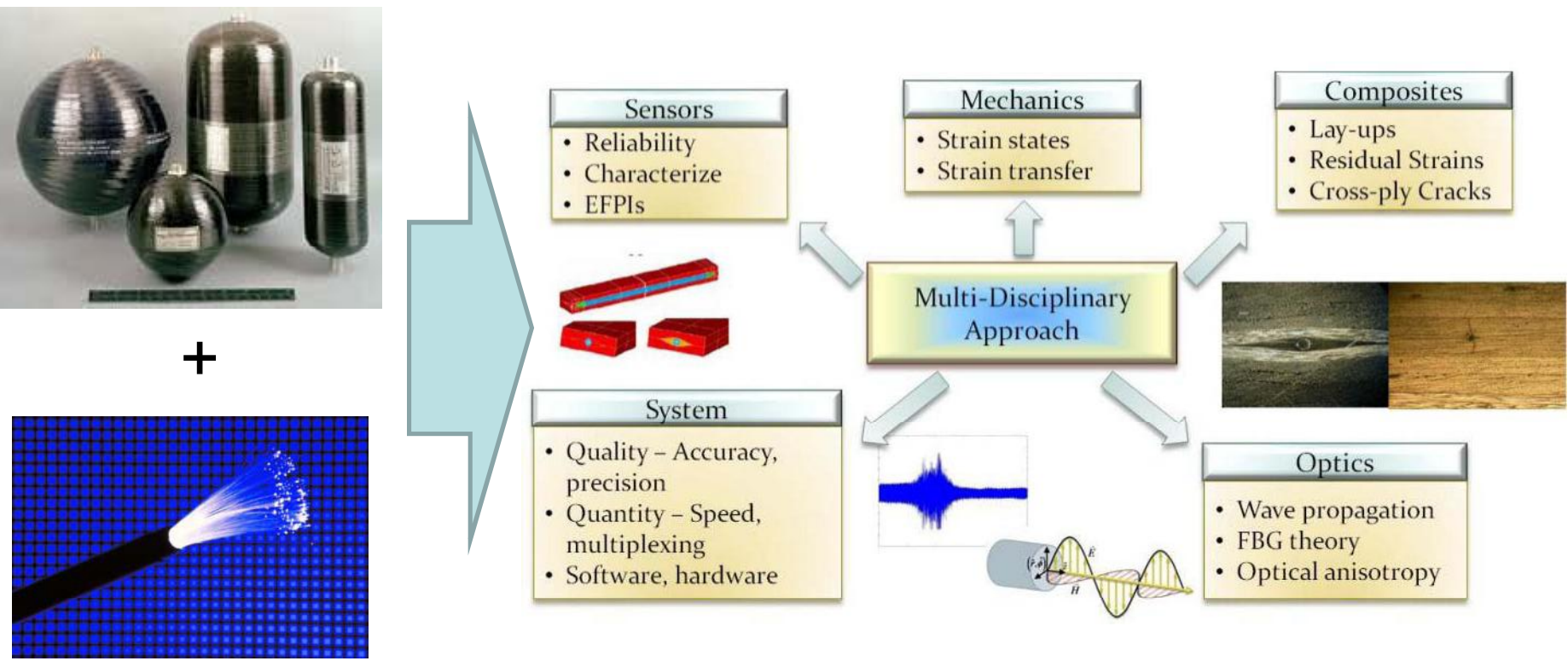
One square-inch of human skin



Source: Biswas, Aman. *Explore the Human Body*.

Embedment of Fiber Optic Sensors within Composites The Multidisciplinary Challenge

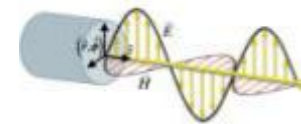
- Fiber Optic Sensors embedded within Composite Overwrapped Pressure Vessels
- Goal is to understand embedded FBG sensor response
 - Requires comprehensive, multi-disciplinary approach



Embedment of Fiber Optic Sensors within Composite Overwrapped Pressure Vessels (COPVs)

The Goal: Characterize measurement response of fiber Bragg sensors embedded in COPVs

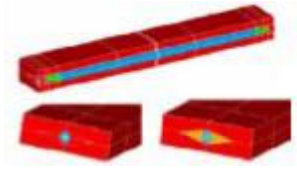
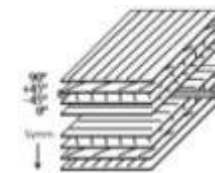
- Determine overall sensor accuracy as a function of its orientation relative to the layered materials in the structure
- Use finite element techniques to understand the thermal/mechanical loads present in the fiber optic, lenticular resin rich region, and the adjacent composite material as well as issues related to ingress/egress.
- Experimentally evaluate the accuracy and long term durability of the embedded sensor / host material system when subjected to quasi-static thermal mechanical loading



Theoretical development



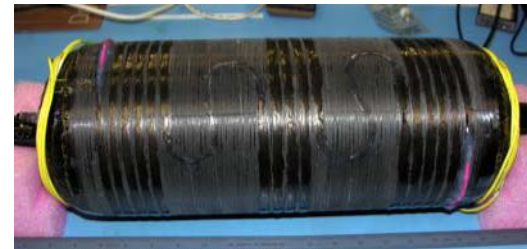
Coupon testing



Analysis and Modeling

The Approach: Evaluate accuracy and long term durability of a fiber optic sensors embedded within COPVs

- Analytical modeling of the fiber optic sensor
- Epoxy composite fabrication
- Quasi-static testing of coupons
- Long term fatigue testing
- Testing of representative aerospace



Sensor Installation



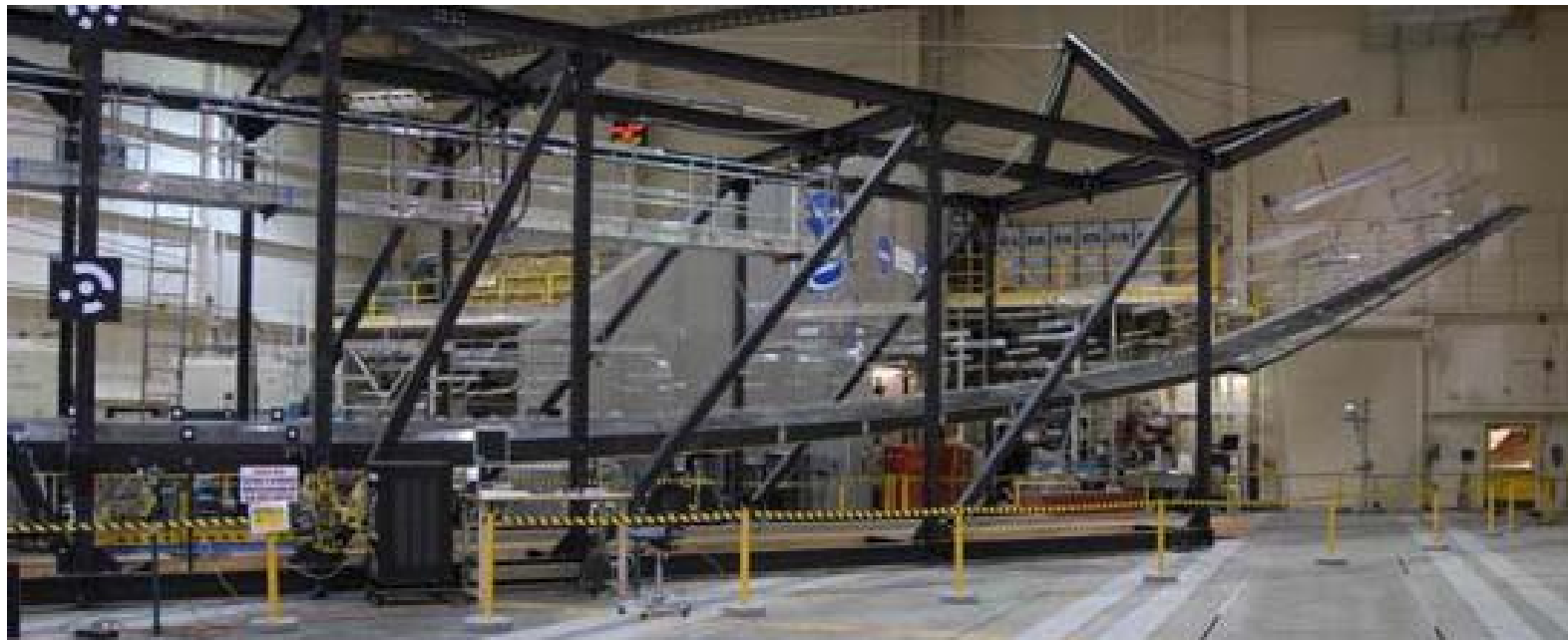
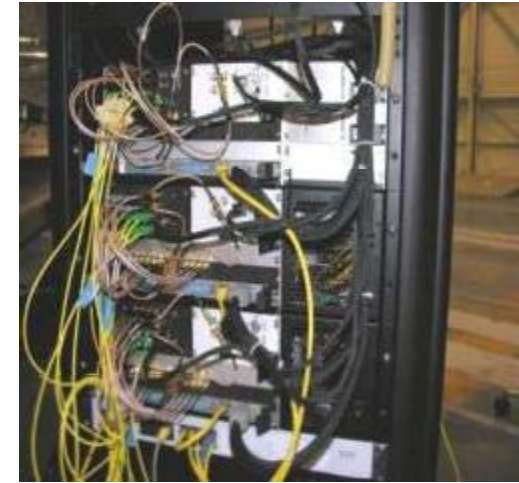
Embedding / Fabrication



Failure Testing

AeroVironment's Global Observer Wing Loads Tests at NASA Dryden

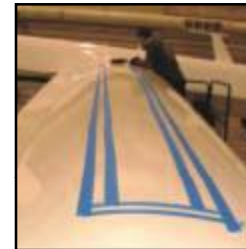
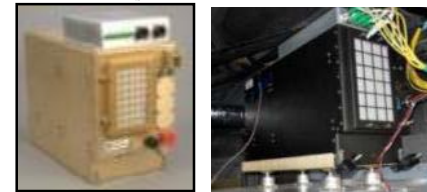
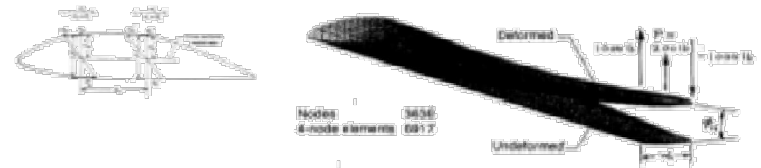
- Validate strain predictions along the wingspan
- Measured strain distribution along the centerline top and bottom as well as along the trailing edge top and bottom.
- FO Strain distribution measurements are being used to interpret shape using Dryden's single fiber shape algorithm
- A 24-fiber system was designed of which 18 fiber 40ft (~17,200 gratings) fibers were used to instrument this wing



Research and Technology Development Areas

- Algorithm Development
- FBG System Development
- Instrumentation
- Ground Testing / R&D
- Flight Testing

$$y_n = \frac{\Delta l^2}{6c} \left\{ (3n-1)\varepsilon_0 + 6 \sum_{i=1}^{n-1} (n-i)\varepsilon_i + \varepsilon_n \right\}$$



Flight Test Results

Predator-B

- **Flight validation testing**

- 18 flights tests conducted; 36 flight-hours logged
- Conducted first flight validation testing April 28, 2008
- Believed to be the first flight validation test of FBG strain and wing shape sensing
- Multiple flight maneuvers performed
- Two fiber configurations
- Fiber optic and conventional strain gages show excellent agreement
- FBG system performed well throughout entire flight – no issues



Video clip of flight data superimposed on Ikhana photograph

AeroVironment's Global Observer Flight Testing

- Validate strain predictions along the left wing using 8, 40ft fibers
- An aft fuselage surface fiber was installed to monitor fuselage and tail movement
- Strain distribution were measured along the left wing centerline top and bottom as well as along the trailing edge top and bottom.
- 8 of the 9 total fibers are attached to the system at any give time



Concluding Remarks

Fiber Optic Wing Shape Sensing toward UAS applications involves five major areas

- **Algorithm development**
 - Real-time wing shape and applied loads algorithms using fiber optics sensors were in good agreement with conventional measurements
- **FBG system development**
 - Current Flight Systems in Operation: 4 and 8 Fiber Systems
 - Flown on Ikhana and Global Observer, resp.
 - Future Systems underdevelopment:
 - 64 Fiber 'Large-Vehicle' System
 - 4 Fiber 'Compact' System
- **Instrumentation**
 - Installation Advantages
 - Greatly reduced installation time compared to conventional strain gages
 - Installation Challenges
 - Optical fiber more fragile than strain gages
- **Ground Testing / R&D**
 - A 24-fiber system was used on Global Observer; 18 fiber 40ft (~17,200 gratings) fibers were to measure strain and wing shape in real-time
- **Flight Testing**
 - Predator-B; Ikhana
 - Real time fiber Bragg strain measurements successfully acquired and validated in flight (4/28/2008)
 - Real-time fiber optic wing shape sensing successfully demonstrated in flight
 - Global Observer