crete structure. Experiments have shown that even though such a coat resides on the exterior surface, it generates a protective galvanic current that flows to the interior reinforcing steel members. By effectively transferring the corrosion process from the steel reinforcement to the exterior coating, the protective current slows or stops corrosion of the embedded steel. Specific formulations have been found to meet depolarization criteria of the National Association of Corrosion Engineers (NACE) for complete protection of steel reinforcing bars ("rebar") embedded in concrete.

A coating of this type can be applied thick enough to afford protection for ten years or longer. The coating can easily be maintained or replaced to ensure continued protection of the reinforcing steel for an indefinite time.

The costs of protecting structures by use of these coating materials are expected to be less than (or in some cases, comparable to) the costs of protection by most conventional methods:

- Typical costs of installing impressedelectric-current systems range from 10 to 30 dollars per square foot (about 110 to 330 dollars per square meter) [prices as of year 2000]. After installation, these systems incur additional costs of electrical power, inspection, and maintenance.
- The costs of installing sacrificial systems based on thermally sprayed zinc typically range between 10 and 20 dollars per square foot (about 107 to 215 dollars per square meter). Like the present developmental systems, sacrificial-zinc systems require very little maintenance once they are installed.
- Another type of sacrificial system involves the use of zinc sheet and electrically conductive glue. The costs of installing these systems typically range from 8 to 18 dollars per square foot (about 86 to 194 dollars per square meter). These systems also require very little maintenance after installa-

tion. Both this and the preceding sacrificial-zinc system have been said to offer 10-year life expectancy. However, according to NACE, pure zinc coats on concrete structures provide only partial protection because of their low driving voltages. Upon exposure, the zinc can become passivated, such that during dry weather, it does not supply protective current to steel rebar.

• The costs of protecting structures by use of the developmental coating materials have been estimated to range from 5 to 9 dollars per square foot (about 54 to 97 dollars per square meter).

This work was done by Louis G. MacDowell of Kennedy Space Center and Joseph Curran of Dynacs, Inc.

This invention is owned by NASA, and a patent application has been filed. Inquiries concerning nonexclusive or exclusive license for its commercial development should be addressed to the Technology Programs and Commercialization Office, Kennedy Space Center, (321) 867-8130. Refer to KSC-12049.

Processable Polyimides Containing APB and Reactive End Caps Properties can be tailored through choice of proportions of dianhydrides and APB.

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Imide copolymers that contain 1,3bis(3-aminophenoxy)benzene (APB) and other diamines and dianhydrides and that are terminated with appropriate amounts of reactive end caps have been invented. The reactive end caps investigated thus far include 4-phenylethynyl phthalic anhydride (PEPA), 3aminophenoxy-4'-phenylethynylbenzop henone (3-APEB), maleic anhydride (MA), and 5-norbornene-2,3-dicarboxylic anhydride [also known as nadic anhydride (NA)]. The advantage of these copolyimides terminated with reactive groups, relative to other polyimides terminated with reactive groups, is a combination of (1) higher values of desired mechanical-property parameters and (2) greater ease of processing into useful parts.

Homopolymers that contain only other diamines and dianhydrides and that are not processable under conditions reported previously can be made processable by incorporating various amounts of APB according to this invention, depending on the chemical structures of the diamines and dianhydrides used. These copolyimides exhibit high degrees of resistance to solvents, high glass-transition temperatures, and high moduli of elasticity, but are processable at low pressures [\leq 200 psi (\leq 1.38 MPa)], when the appropriate amounts of APB are utilized. In addition, when these copolymers are terminated with phenylethynyl groups, they exhibit long-term melt stability (several hours at temperatures approaching 300 °C).

The dianhydride incorporated into a polymer of this type has a rigid molecular structure that tends to degrade processability. The addition of the highly flexible APB diamine improves processability, while the imide structure provides stiffness to the polymer backbone, increases resistance to solvents, and improves mechanical properties. The resulting combination of properties is important for the use of the copolymer as a matrix in a composite material or as an adhesive or a film, coating, or molding material: If too little APB is incorporated into the polymer backbone, the resulting material is not processable under desired processing limitations. If too much APB is incorporated into the polymer backbone, the resulting material becomes highly flexible with a lower glass-transition temperature than desired.

Hence, by choosing the ratio between the amount of APB and the amount of the other diamine in the polyimide backbone, one can obtain a material that has a unique combination of solubility, glass-transition temperature, melting temperature, melt viscosity, toughness, and high-temperature mechanical properties. The exact amount of APB needed to optimize this combination of properties is not predictable and must be determined for the intended application and for the proposed method of processing the copolymer for use in the application.

This work was done by Brian J. Jensen of Langley Research Center. Further information is contained in a TSP (see page 1).

This invention has been patented by NASA (U.S. Patent No. 6,133,401). Inquiries concerning nonexclusive or exclusive license for its commercial development should be addressed to Greg Manuel, Technology Commercialization Program Office, Langley Research Center, MS 200, Hampton, VA 23861, g.s.manuel@larc.nasa.gov. Refer to LAR-15449.