

The Effect of Photon Source on Heterogeneous Photocatalytic Oxidation of Ethanol by a Silica-Titania Composite

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Abstract:

The objective of this study was to distinguish the effect of photon flux (i.e., photons per unit time reaching a surface) from that of photon energy (i.e., wavelength) of a photon source on the silica-titania composite (STC)-catalyzed degradation of ethanol in the gas phase.

Experiments were conducted in a bench-scale annular reactor packed with STC pellets and irradiated with either a UV-A fluorescent black light blue lamp ($\lambda_{\max}=365$ nm) at its maximum light intensity or a UV-C germicidal lamp ($\lambda_{\max}=254$ nm) at three levels of light intensity. The STC-catalyzed oxidation of ethanol was found to follow zero-order kinetics with respect to CO_2 production, regardless of the photon source. Increased photon flux led to increased EtOH removal, mineralization, and oxidation rate accompanied by lower intermediate concentration in the effluent. The oxidation rate was higher in the reactor irradiated by UV-C than by UV-A (38.4 vs. 31.9 nM s^{-1}) at the same photon flux, with similar trends for mineralization (53.9 vs. 43.4%) and reaction quantum efficiency (i.e., photonic efficiency, 63.3 vs. 50.1 $\text{nmol CO}_2 \mu\text{mol photons}^{-1}$). UV-C irradiation also led to decreased intermediate concentration in the effluent compared to UV-A irradiation. These results demonstrated that STC-catalyzed oxidation is enhanced by both increased photon flux and photon energy.

Keywords: Photocatalytic Oxidation, Photon Energy, Photon Source, Silica-Titania Composite (STC), Volatile Organic Compound (VOC)

1. Introduction:

Increasing awareness of health risks associated with poor air quality in closed-environment habitats (e.g., airplanes, spacecrafts, office buildings, factories, homes, etc.) as well as increasing desire for energy conservation have provoked a high demand for

more efficient and environmentally-friendly technologies for air revitalization. The current technology uses two major types of air purification units; the first category includes units based on filters to remove particulate matter or a sorbent material to collect gases and odors while the second category utilizes thermal oxidation whereby trace contaminants are broken down by heat with or without the assistance of a catalyst. While effective at the removal of volatile organic compounds (VOCs), these methods both have their own shortcomings. Sorbent materials and filters only trap the contaminants and must undergo further handling and disposal procedures to render the contaminants nonhazardous; they also require replacement or refurbishment after the material is spent [1, 2]. On the other hand, thermal methods act to break down contaminants but require significant energy input for heating: temperatures in the range of 200-250°C for processes incorporating catalysts [3] and a range of 730-850°C for those processes not incorporating catalysts [4]; furthermore, there is the potential for harmful side-product formation (e.g., NO_x and SO₂) from the thermal process which requires subsequent purification [5]. An emerging alternative method for air pollution control employs the use of semiconductors in photocatalytic oxidation (PCO) of organic contaminants to produce innocuous CO₂ and H₂O [1, 6, 7]. The primary advantages of PCO over the aforementioned technologies are the use of non-expendable materials and low energy demand because the process operates at or near room temperature.

In the photocatalytic process, light acts as an excitation source to promote an electron from the valence band to the conduction band, generating an electron-hole pair in the semiconductor catalyst. The electron and hole then participate in the reduction and oxidation of the contaminant species in a series of radical reactions [8]. The amount of

energy required to produce the electron-hole pair is known as band-gap energy; when this energy is known, the corresponding wavelength of light can be derived from the Planck-Einstein Equation, $E=hc/\lambda$. Among the photocatalysts used, titanium dioxide (TiO_2) is the most widely implemented because it is inexpensive, nonhazardous, and chemically inert. Commercially available nanoparticle TiO_2 , known as Degussa P25, is a simple mixture of anatase (70-85%), rutile, and amorphous (minor) titania [9] and has demonstrated high PCO activity in numerous studies [8, 10-14]. The anatase phase is known for its superiority in photocatalytic activity over the rutile phase [15]. The band gap energy of anatase TiO_2 is 3.2 eV; thusly, a light source with a wavelength below 388 nm has sufficient energy to activate the anatase TiO_2 . The question arises as to how the wavelength of a photon source below this critical value affects the photocatalytic activity of TiO_2 .

Previously, UV light sources of various wavelengths ranging between 250-400 nm, and with various intensities, have been used in TiO_2 -catalyzed photocatalysis [1, 11, 16-20]. Studies by Stokke et al. [11], Dijkstra et al. [16], Cen et al. [17], Alberci and Jardin [18], Kim and Hong [19], and Jacboy [20] reported that a UV-C-irradiated ($\lambda_{\text{max}} = 254$ nm) reactor resulted in greater photocatalytic oxidation of VOCs than a reactor irradiated with UV-A light ($\lambda_{\text{max}} = 365$ nm), implying that a shorter wavelength light source (i.e., higher energy photons) is more efficient. However, interpretation of the results from these studies on the effect of wavelength of TiO_2 -assisted photocatalysis is confounded with the influence of light intensity as these studies were conducted either at different light intensities or the light intensity was not well defined. It is well known that UV light intensity received at the catalyst surface dramatically affects oxidation rates [1,

13, 21], but a more clear understanding of its effects needs to be addressed. Furthermore, there are discrepancies in the literature regarding whether the use of UV-A or UV-C light sources results in the formation of more intermediates. Although Grela and Colussi [21] clearly demonstrated that the reaction quantum yield for the photocatalytic oxidation of 3-nitrophenol in aerated, aqueous colloids of crystalline or metastable TiO₂ nanoparticles was a function of photon wavelength ($254 \leq \lambda/\text{nm} \leq 366$), no similar data was available for gas-phase photocatalysis. Distinguishing the effect of UV wavelength from that of UV light intensity has profound implications in the design of an energy-efficient and low-risk PCO reactor for the following two reasons: 1) despite the higher lighting efficiency of current UV-C lamps over that of UV-A lamps, UV-C radiation is more damaging and can cause serious skin and eye injuries from both direct and reflected radiation, and 2) both traditional UV-A and UV-C lamps contain a trace amount of highly toxic and EPA-regulated mercury; light emitting diodes (LEDs) are a promising alternate light source and lighting efficiency increases with longer wavelength LED devices (~350 nm) [22]. Therefore, the objective of this study was to distinguish the effect of photon flux (i.e., light intensity) from that of photon energy (i.e., wavelength) by exploring the photocatalytic degradation of ethanol in the gas phase by an adsorption-enhanced TiO₂ photocatalyst (silica-titania composites, STCs) [12] under the illumination of UV-C and UV-A sources. Experiments were conducted in the same reactor, and the UV-C lamp was attenuated to obtain a range of photon fluxes that brackets that of the UV-A lamp.

2. Experimental:

2.1. Photocatalyst: Silica-titania composite pellets (STCs) were supplied by Sol Gel

Solutions, LLC in the form of 2x6 mm pellets. The STC was prepared by adding Degussa P25 TiO₂ to a silica sol derived from the acid hydrolysis of tetraethyl

orthosilicate (TEOS). It had a porosity of 30-40 Å and contained 4% TiO₂ (4 g Degussa P25 TiO₂ in 100 mL of TEOS silica precursor) [12]. The properties of the Degussa P25 TiO₂ were not altered during the STC synthesis process. EDX analysis was completed on a JEOL JSM-7500F Field Emission Scanning Electron Microscope using LEI detection at an 8-mm working distance and demonstrated highly incorporated titania and silica (Fig. 1).

Figure 1

2.2. Light Sources and Characterization: An 8-W UV-A (F8T5) black light blue lamp (UV-A BLB) from Philips (Amsterdam, Netherlands) with dimensions of 15.6 mm (diameter) x 304.8 mm (length) and radiant output of 1.4 W was selected as the UV-A source. An 8-W UV-C (G8T5/OF) germicidal lamp (UV-C GL) with 2.5 W of UV output from Sylvania (Danvers, MA) was selected as the UV-C source. The irradiance profiles at the surface of the catalyst bed for the selected light sources were determined in a dark room (*ex situ*) using a spectroradiometer (model OL754C, Optronics Laboratories, Orlando, FL). The light source (either the UV-A BLB or UV-C GL) was centered inside a quartz sleeve (28 mm O.D. and 25 mm I.D.) and placed directly on top of the integrating sphere of the spectroradiometer (Light attenuating discs with 12.7-mm and 6.35-mm diameters were used to avoid saturation of the detector during scanning of the UV-A and UV-C sources, respectively. The desired intensity of UV-C light was achieved by using a fine stainless-steel mesh (U.S. mesh size 16, referred to hereafter as attenuation mesh) between the quartz sleeve and lamp as a neutral density filter.

2.3. Photocatalytic Oxidation (PCO) Reactor: A custom-made annular reactor (Southern Scientific, Inc., Micanopy, FL) was used in this study and accommodated both light

sources interchangeably. As shown in Fig. 2, the reactor was comprised of an outer Pyrex housing (38.8 mm I.D., 42.0 mm O.D.) and an inner quartz sleeve (25.0 mm I.D., 28.8 mm O.D.) with Teflon caps to create an air-tight environment; the reactor length was 15.24 cm. Glass beads (3-mm dia.) were added to allow the STCs to be packed in the center of the reactor as well as to facilitate air distribution. The STC pellets (14.6 g) were then packed in the annulus space (5.0 mm) resulting in a bed height of ~65 mm. Temperature was controlled to $25 \pm 0.1^\circ\text{C}$ throughout all experiments via a water jacket and a thermostated water bath. The light source (either UV-A BLB or UV-C GL) was centered in the quartz sleeve of the reactor and the entire reactor was covered in aluminum foil to avoid penetration of room light into the reactor system and to avoid accidental UV exposure of lab personnel.

Figure 2

2.4. PCO Experiments and Process Monitoring: Tests were performed in the annular reactor packed with 14.6 g of STC pellets under continuous illumination by either the UV-A source at its maximum light intensity or the UV-C source at three varied intensity levels. All tests were carried out in a flow-through mode with an uninterrupted $2 \text{ L min}^{-1} \text{ CO}_2$ -free air ($74.7 \pm 0.8\% \text{ RH}$) containing 50 ppm_v ethanol at 25°C as the test volatile organic compound (VOC) as described previously [13]. Each test was repeated a minimum of two times. The STC pellets were regenerated in-line between each test by passing a VOC-free ($74.7 \pm 0.8\% \text{ RH}$) sweeping gas at 25°C through the reactor accompanied by UV irradiation. Both influent and effluent streams were sampled alternately every 8.45 minutes and analyzed for ethanol and its oxidation intermediates by GC/FID equipped

with an HP Plot Q column (30 m X 0.32 mm, 20 μm d.f.). The effluent stream was also directed to a CO_2 analyzer for the determination of the rate of CO_2 production.

2.5. PCO Efficiency, Kinetics, and Reaction Quantum Yield: PCO performance was quantified by EtOH removal, the measure of the removal of the test VOC regardless of it being adsorbed or oxidized at pseudo-steady state conditions, and mineralization efficiency (X_A), the measure of complete oxidation of EtOH to CO_2 . These values were calculated using equations 1 and 2, respectively, where C_0 and C_{EtOH} are the influent and effluent ethanol concentrations; ΔC_{CO_2} is the CO_2 generated by the PCO. The rate of the PCO of ethanol was determined based on the formation of CO_2 rather than the disappearance of ethanol to prevent overestimation due to the EtOH adsorption to the silica-rich photocatalyst. The reaction quantum yield (ξ), or photonic efficiency, was calculated as the ratio of the photocatalytic oxidation rate to the incident photon flux as shown in equation 3.

$$\text{EtOH Removal} = (C_0 - C_{\text{EtOH}}) / C_0 \quad \text{Eqn. 1}$$

$$X_A = \Delta C_{\text{CO}_2} / (2 * C_0) \quad \text{Eqn. 2}$$

$$\xi = \text{Rate of Reaction (nM s}^{-1}\text{)} / \text{Rate of incident photons (\mu mol s}^{-1}\text{)} \quad \text{Eqn. 3}$$

3. Results and Discussion:

3.1. Spectral Quality of the UV-A BLB and UV-C GL:

The Philips brand UV-A BLB was selected as the UV-A source because it was found to possess the highest light intensity over alternate UV-A lamps previously tested [13]. The irradiance spectrum of the UV-A lamp (Fig. 3A) had a broad primary peak (354-388 nm) centered at 365 nm and an additional peak at 405 nm that is beyond the action spectrum of anatase TiO_2 ($\lambda < 388$ nm). The UV-C GL irradiance spectrum

contained a high-intensity, narrow peak (250-255 nm) centered at 253 nm along with several low-intensity peaks at 313, 365, and 405 nm (Fig. 3B).

Figure 3

The irradiance of the primary peak for each lamp was determined through the integration of the radiation scan with defined integration limits of 1% irradiance with respect to the value at the λ_{max} . The minor peaks for both sources were also integrated in a similar fashion to determine their contribution to the total irradiance of the lamps. It was found that the 405 nm peak accounted for 0.71% of the total irradiance of the UV-A lamp; the irradiances for the 313, 365, and 405 nm peaks in the UV-C source were found to account for 0.42%, 0.89%, and 1.06% of the total irradiance, respectively. Based on these results, it is not expected that these peaks had significant contribution to the energy used in the activation of the TiO₂-assisted photocatalysis or possible photolysis of ethanol throughout this study. The irradiance at the surface of the catalyst, as well as the photon flux for both the UV-A source and UV-C source (with and without the neutral density filter), are shown in Table 1. The 8-W UV-C lamp had an irradiance 2.0 times higher than the 8-W UV-A source and was attenuated to obtain a range of intensities by the use of one or two layers of attenuation mesh.

Table 1

3.2. Effect of Photon Flux of UV-C Light on STC-Catalyzed Oxidation of Ethanol:

Figure 4

Figure 4 shows the change in carbon-normalized effluent composition over time after the introduction of contaminant flow and UV-C illumination. There were three components detected in the effluent stream: ethanol; CO₂, the complete mineralization product; and

acetaldehyde (ACD), the only quantifiable intermediate detected by the GC-FID. A carbon balance for the system further confirmed this observation. For the UV-C source under all three intensities tested, the total carbon in the effluent and adsorbed onto the STCs accounted for a minimum of 94% of carbon entering the system (data not shown), which is within the range of error associated with the system.

The photon flux at the catalyst surface had a profound effect on the rate of effluent concentration increase and effluent composition at any given time point (Fig. 4). A true steady state was not attainable under the time restrictions of the experiments; thus, the pseudo-steady state, or time at which CO₂ formation reached a steady state and the change in effluent ethanol and ACD had reached a minimum, was implemented. The pseudo-steady state was achieved approximately after the ten-hour mark in all experiments. The average concentration between 10 and 20 hours was used to calculate the ethanol removal and mineralization efficiency. The concentration of components in the effluent stream is dependent upon the balance between their production and adsorption affinity to the STC pellets. The time it took for the initial appearance of each component in the effluent as well as the time to 50% of respective concentration at pseudo-steady state are good indicators for their affinity to STC pellets. CO₂ reached its 50%-concentration mark in less than 45 minutes for all experiments after the initiation of the EtOH-contaminated air flow; this suggests minimal, if any, adsorption of CO₂ to the STC pellets. In the cases of ACD and EtOH, this mark was attained within 5 hours and 8.5 hours, respectively. These results show lower adsorption affinity for ACD than for EtOH. Because of the low affinity for CO₂, its rate of evolution was used to determine the PCO rate. The rate of ethanol oxidation by STC-assisted photocatalysis was

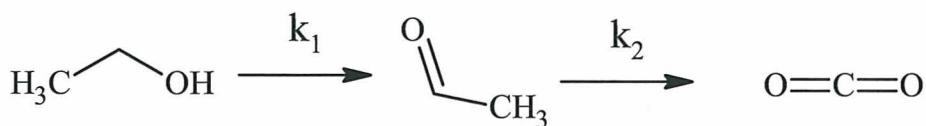
determined to be zero-order, regardless of the UV-C irradiance level implemented with respect to CO₂ evolution.

Figure 5

In general, increasing the photon flux at the catalyst surface resulted in an increase in ethanol removal (Fig. 5A), ethanol mineralization (Fig. 5B), and PCO Rate (Fig. 5C). However, the reaction quantum yield decreased with the increase of photon flux (Fig. 5D). The relationship between the photon flux (ϕ) and PCO rate (r) followed an exponential trend ($r=49.117 \phi^{0.489}$) over the range of intensities studied. Previous reports proposed that the dependence of the PCO reaction rate (r) on the photon flux (ϕ) follows a first-order kinetic trend ($r=K\phi$, where K is a constant) when ϕ is 0.008 $\mu\text{mol photons s}^{-1}$ or lower, but follows a half-order kinetic trend ($r=K\phi^{0.5}$) when ϕ exceeds this photon flux [23]. Since the photon flux employed in this study was in the range of 0.337-0.892 $\mu\text{mol photons s}^{-1}$, our results are in close agreement with the relationship proposed by Egerton and King [23]. There were several differences between our system and that used by Egerton and King [23] including 1) the use of the Degussa P25 TiO₂ opposed to the 100% rutile TiO₂ used by Egerton and King [23] where the crystal structure may have played a role in the kinetics differently; 2) the use of a UV-C light source, and thusly, higher-energy photons (only UV-A light sources were tested previously); and 3) the use of STC instead of a TiO₂ thin film: the former is not only much thicker (5 mm) than the latter, it also contains less TiO₂ for the same surface area exposed to the light (Fig. 1). Regardless of these changes, the same relationship was developed. Furthermore, our results indicate that the relationship developed between photon flux and PCO rate by Egerton and King [23] is independent of wavelength.

As a result of the decreased dependency of the PCO rate on photon flux within the range tested, the photonic efficiency decreased as the photon flux increased (Fig. 5D). This result implies that not all of the charge carriers generated in this range of photon flux were utilized in the redox process; furthermore, less reactive carriers may have accumulated and undergone recombination. In other words, energy-use efficiency decreases at a significantly large photon flux even though it leads to increased mineralization (Fig. 5B) and reduced intermediate evolution (Fig. 5E). A balance between energy-use efficiency and PCO efficiency must be scrutinized in the design of such PCO reactors.

The PCO of ethanol on a TiO_2 surface is known to follow two similar pathways that include various intermediates such as acetaldehyde, acetic acid, formaldehyde, and formic acid [24]. As previously stated, acetaldehyde was the only intermediate detected in our system. This does not mean that acetic acid, formic acid, and formaldehyde did not form during our reaction but suggests that they were oxidized at the same (or faster) rate they were formed. Therefore, a simplified schematic of the reaction, shown below, was used to better understand the decreased evolution of acetaldehyde with increased photon flux (Fig. 5E).



The fact that there was a significant amount of ACD in the effluent suggests that k_2 is slower than k_1 ; i.e., the oxidation of acetaldehyde is the rate-limiting step in the mineralization of ethanol. Furthermore, it may be assumed that the adsorption of ACD onto the STCs is not affected by photon flux since the time at which the 50% pseudo-

steady state concentration mark was reached was equivalent for the various light intensities. Although both the oxidation of ethanol to acetaldehyde (k_1) and that of acetaldehyde to CO_2 (k_2), was accelerated by increased light intensity, the ACD concentration in the effluent decreased as the photon flux increases. This implies a greater increase in k_2 than k_1 . Therefore, this result suggests that it is possible to eliminate the accumulation of ACD if sufficient light intensity and optimized reactor design are provided.

3.3. Effect of Wavelength (UV-A BLB vs. UV-C GL) at the Same Photon Flux:

The PCO of ethanol by STCs irradiated by a UV-A light source was investigated under the same conditions in the same reactor as that used in the above UV-C experiments. The key performance parameters including ethanol removal, mineralization efficiency, PCO rate, photonic efficiency, and $[\text{ACD}]_{\text{Effluent}}$ are summarized in Table 2. The corresponding performance data for a reactor illuminated with UV-C light at the equivalent photon flux of the UV-A source (i.e., $0.633 \pm 0.013 \mu\text{mol photons s}^{-1}$) was extrapolated from the relationships obtained in Figure 5 to allow for a direct comparison.

Table 2

As seen in the UV-C studies, ACD was also the only quantifiable intermediate in the UV-A studies; however, it accumulated to a higher level than seen in any of the UV-C experiments. The total carbon balance for the UV-A-irradiated system was 94.6% again confirming the claim that was no accumulation of other intermediates. The EtOH removal for the UV-A-illuminated reactor ($89.8 \pm 1.6\%$) was statistically equivalent to the projected EtOH removal (89.0%) for the UV-C-illuminated reactor at the equivalent

irradiance. However, this equivalence is not due to equivalent mineralization and PCO rate (Table 2), but is likely attributed to an accelerated k_1 and reduced k_2 , that is, an increased oxidation of ethanol to acetaldehyde and reduced oxidation of acetaldehyde to CO_2 , allowing for increased accumulation of ACD in the UV-A-irradiated reactor.

Similar to the results from the UV-C illuminated experiments, it was found that the rate of evolution of CO_2 followed a zero-order rate law when the UV-A photon source was used. The PCO rate at the equivalent photon flux was 31.9 ± 0.7 and 39.3 nM CO_2 s^{-1} for the UV-A BLB and UV-C GL, respectively. This demonstrated that photons with a shorter wavelength (or higher energy) increase the PCO rate ($r_{\text{UV-C}} > r_{\text{UV-A}}$). Moreover, the reaction quantum yield for an equivalent-photon flux UV-C-illuminated reactor was 1.25 times that of the UV-A-illuminated reactor; this is consistent with the previous findings that shorter wavelength photons render greater chemical quantum yield in crystalline TiO_2 sols or metastable TiO_2 [21], although the magnitude of the enhancement is dependent on the catalyst used. According to Grela et al. [25], chemical quantum yield increases significantly with an increase of excess photon energy over the bandgap energy according to $E^* = E_\lambda - E_{\text{bg}}$ and reaches a plateau at $E^* = \sim 0.9$ eV. In this study, the UV-A BLB gives an $E^* = 0.2$ eV while the UV-C GL gives $E^* = 1.7$ eV over the anatase TiO_2 bandgap of 3.2 eV. Our results support the theory and predict that UV-B (290 – 320 nm) give rise to the same efficiency as UV-C.

These results suggest that a shorter wavelength light source, or photons of higher energy, has an overall positive effect on the PCO of ethanol. Taking into consideration that only $\sim 10\%$ of UV-C light compared to $\sim 90\%$ of UV-A light is transmitted through a single layer of TiO_2 thin film [17], less catalyst surface was directly exposed to the UV-C

photons. The enhanced performance of the shorter wavelength source is more likely to be the result of 1) increased formation of potential active species in the photocatalytic oxidation reaction [26], 2) reduced electron-hole recombination [21], 3) increased interfacial electron transfer between TiO_2 particles, 4) increased electron transfer from ethanol to the hot carrier of TiO_2 , and/or 5) increased probability for direct photo-oxidation of ethanol. This last hypothesis was tested by packing the reactor with 3-mm glass beads instead of STC pellets and examining whether ethanol was degraded by UV light alone.

Figure 6

No significant difference in EtOH concentration between the influent and effluent was found during this experiment with the UV-A BLB (Fig. 6A). No CO_2 or ACD above the baseline level was observed in the effluent under UV-A illumination. Conversely, in the UV-C-irradiated reactor, a small quantity of ACD (average 1.36 ppm, ACD) was found in the effluent, accompanied by a small decrease in EtOH concentration between the influent to the effluent (Fig. 6B). Clearly, differential photooxidation by UV-C and UV-A plays a small role in ethanol mineralization and is not the main contributing mechanism for the 11.7% higher mineralization efficiency, 7.4% increased PCO rate, and more 1.25 times higher photonic efficiency seen in the UV-C PCO reactor over that in the UV-A reactor.

4. Conclusions:

This study demonstrated that both photon flux and photon energy have profound impacts on not only the PCO efficiency, but also on the energy-use efficiency and must be meticulously taken into consideration in the design of an efficient PCO reactor.

As the photon flux increased for the UV-C source, the quantum yield decreased. In accordance with previous studies, the mineralization efficiency for ethanol and PCO reaction rate increased with the incident photon flux within the range examined. This study also demonstrated that 254-nm photons (UV-C) are 1.25 times more efficient than 365-nm photons (UV-A) for driving the STC-catalyzed degradation of ethanol in the gas phase. This is in agreement with the findings by Grela et al. [21, 26] for the oxidation of salicylate (3.8 to 6.4 times depending on substrate concentration) and 3-nitrophenol. The extent of photooxidation of ethanol in the absence of the STCs by higher energy photons (254 nm) was slightly higher than that of lower energy photons (365 nm), but not sufficient to contribute to the increase in photonic efficiency, PCO rate, and mineralization efficiency. It is concluded that the enhanced performance by shorter wavelength photons from the UV-C light source is due to the combined result of increased active charge carriers, reduced electron-hole combination, increased interfacial electron transfer between TiO₂ particles, and also increased electron transfer from ethanol to the hot carrier of TiO₂.

5. Abbreviations and Nomenclature:

ϕ – Photon Flux
 ξ – Reaction quantum yield/Photonic efficiency
ACD – Acetaldehyde
C – Concentration
C₀ – Influent Ethanol Concentration
C_{EtOH} – Effluent Ethanol Concentration
 ΔC_{CO_2} – CO₂ generated from the PCO
EtOH – Ethanol
FL – Fluorescent Lamp
GL – Germicidal Lamp
I.D. – Internal diameter
O.D. – Outer diameter
PCO – Photocatalytic Oxidation
RH – Relative Humidity

r – PCO Rate
STC – Silica-Titania Composite
UV – Ultra-Violet
VOC – Volatile Organic Compound
 X_A – Mineralization Efficiency

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7. References:

- [1] J. Zhao, X. Yang, *Building and Environment*, 38 (2003) 645-654.
- [2] E. Uhde, in: T. Salthammer (Ed), *Organic Indoor Air Pollutants: Occurrence, Measurement, Evaluation*, Wiley-VCH. Weinheim, Germany, 1999, pp. 3-14.
- [3] *Thermal and Catalytic Oxidizers: Gas and Electric Fired Systems Specifications Sheets*, Hitemp Technology Corporation, Flemington, NJ, 9 Dec., 2010 <www.hitemptech.com>.
- [4] A.S.K. Warahena, Y.K. Chuah, *Environ. Sci. Technol.* 43 (2009) 6101-6105.
- [5] C.W. Babbitt, J.M. Stokke, D.W. Mazyck, A.S. Linder, *J. Chem. Technol. Biotechnol.* 84 (2009) 725-737.
- [6] M.R. Hoffmann, S.T. Martin, W. Choi, D.W. Bahnemann, *Chem. Rev.* 95 (1995) 69-96.
- [7] J. Mo, Y. Zhang, Q. Xu, J. J. Lamson, R. Zho, *Atmospheric Environment*, 43 (2009) 2229-2246.
- [8] O. Carp, C.L. Huisman, A. Reller, *Progress in Solid State Chemistry*. 32 (2004) 33-177.
- [9] B. Ohtani, O.O. Prieto-Mahaney, D. Li, R. Abe, *Journal of Photochemistry and Photobiology A: Chemistry*. 216 (2010) 179-182.
- [10] Y. Luo, D.F. Ollis, *J. of Catalysis*. 163 (1996) 1-11.
- [11] J.M. Stokke, D.W. Mazyck, C.Y. Wu, R. Sheahan, *Environmental Prog.* 25(4) (2006) 312-318.
- [12] J.M. Stokke, D.W. Mazyck, *Env. Sci. Technol.* 42(10) (2008) 3808-3813.
- [13] L.H. Levine, J.R. Richards, R.R. Soler, F. Maxik, J.L. Coutts, R.M. Wheeler, 40th International Conference on Environmental Systems, Barcelona, Spain, July 2010, AIAA Paper# 2010-6151
- [14] S. Kwon, M. Fanb, A.T. Cooper, H. Yang, *Critical Reviews in Environmental Science and Technology*. 38(3) (2008) 197-226.
- [15] A.G. Agrios, K.A. Gray, E. Weitz, *Langmuir*. 19 (2003) 1402-1409.
- [16] M. F. J. Dijkstra, H.J. Pannerman, J. G. M. Ninkelman, J. J. Kelly, A. A. C. M. Beenackers, *Chemical Engineering Science*. 57 (2002) 4895-4907.
- [17] J. Cen, X. Li, M. Xe, S. Zheng, M. Feng, *Chemosphere (Technical Note)*. 62 (2006) 810-816.
- [18] R. M. Alberci, N. F. Jardim, *Applied Catalysis B: Environmental*. 14 (1997) 55-68.

- [19] S. B. Kim, S. C. Hong, *Applied Catalysis B: Environmental*. 35 (2002) 305-315.
- [20] W.A. Jacoby, Destruction of trichloroethylene in air via semiconductor mediated gas-solid heterogeneous photocatalysis, PhD Dissertation, Department of Chemical Engineering, University of Colorado, USA, 1993.
- [21] M. A. Grela, A. J. Colussi, *J. Phys. Chem. B*. 103 (1999) 2614-2619.
- [22] A. Sandhu, *Nature Photonics*. 1 (2007) 38.
- [23] T. A. Egerton, C. J. King, *J. Oil Col. Chem. Assoc.* 62 (1979) 386-391.
- [24] D. S. Muggli, J. T. McCue, J. L. Falconer, *Journal of Catalysis*. 173 (1998) 470-483.
- [25] M. Grela, M. A. Brusa, A. J. Colussi, *J. Phys. Chem. B*. 101 (1997) 10986-10989.
- [26] Y. Paz, in: H. I. de Lasa, B. S. Rosales (Eds.), *Advances in Chemical Engineering: Photocatalytic Technologies*, Elsevier, Inc., Amsterdam, 2009, pp. 289-336.

Tables:

Table 1^a: Average Irradiance and Photon Flux for Selected Light Sources

Light Source	Irradiance (mW cm ⁻²)	Photon Flux (μmol photons s ⁻¹)
UV-A BLB	3.49 ± 0.07	0.633 ± 0.013
UV-C GL + 2X Mesh	2.71 ± 0.07	0.337 ± 0.009
UV-C GL + 1X Mesh	5.17 ± 0.07	0.643 ± 0.009
UV-C GL + No Mesh	7.17 ± 0.07	0.892 ± 0.009

^a: Values are the average of three scans with standard deviation. The photon flux is calculated to reflect that reaching the surface of the catalyst.

Table 2^b: Effect of Photon Energy on PCO Performance

Light Source	EtOH Removal (%)	Mineralization (%)	PCO Rate (nM CO ₂ s ⁻¹)	ξ (nmol CO ₂ μmol photons)	[ACD] _{Effluent} (ppm _v)
UV-A BLB	89.8 ± 1.6	43.4 ± 0.3	31.9 ± 0.7	50.5 ± 0.1	19.1 ± 0.2
UV-C GL ^c	89.0	55.1	39.3	63.3	13.8

^b: Where appropriate, values are given with standard deviation.

^c: Values were extrapolated from Figure 5 data for a UV-C photon flux equivalent to that of the UV-A BLB.

Figure Captions:

Figure 1: SEM (x 5,000 magnification, LEI detection, 8-mm W.D.) image of a crushed STC pellet; EDX image analysis revealed that the white areas corresponded to titania while the darker grey areas corresponded to silica.

Figure 2: Annular Photocatalytic Reactor Packed with 14.6 g STC Pellets as used in experiments.

Figure 3: Average irradiance distribution for the (A) UV-A BLB at maximum irradiance and (B) UV-C GL at maximum irradiance (solid line), attenuated irradiance using one layer of mesh (- - - line), and attenuated irradiance using two layers of mesh (· · · line). The inset in (B) shows the secondary irradiance peaks for the full-irradiance UV-C GL.

Figure 4: Time course of effluent composition (carbon-normalized) during STC-catalyzed oxidation of ethanol using the (A) full-irradiance UV-C GL, (B) UV-C GL with one layer of attenuation mesh, and (C) UV-C GL with two layers of attenuation mesh. Effluent species are designated as follows: (\blacklozenge): CO₂ carbon, (\blacktriangle): ACD carbon, and (\circ): EtOH carbon.

Figure 5: Relationships between photon flux and (A) Ethanol Removal, (B) Mineralization Efficiency, (C) PCO Rate Constant (nM CO₂ s⁻¹), and (D) Photonic Efficiency, ξ (nM CO₂ μ mol photons⁻¹). Data points designated with (\circ) were obtained using the UV-A light source and those designated with (\blacklozenge) were obtained using the UV-C light source.

Figure 6: Influent (\blacklozenge) and effluent (\diamond) EtOH composition during photolysis of ethanol by the (A) UV-A BLB and (B) UV-C light sources.

Figures:

Figure 1:

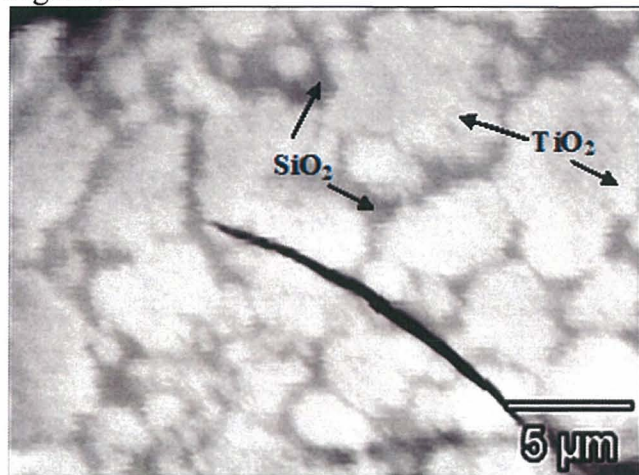


Figure 2:

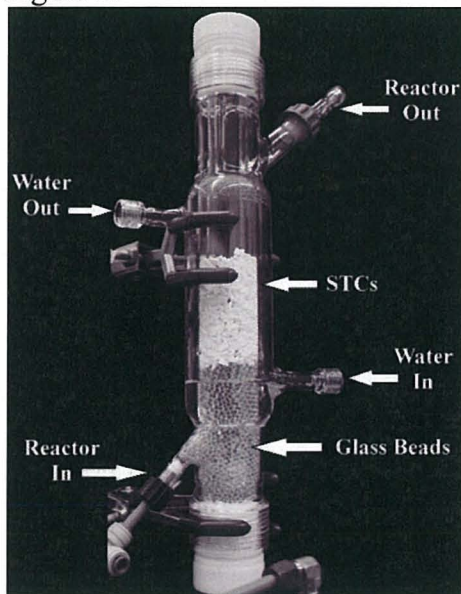


Figure 3:

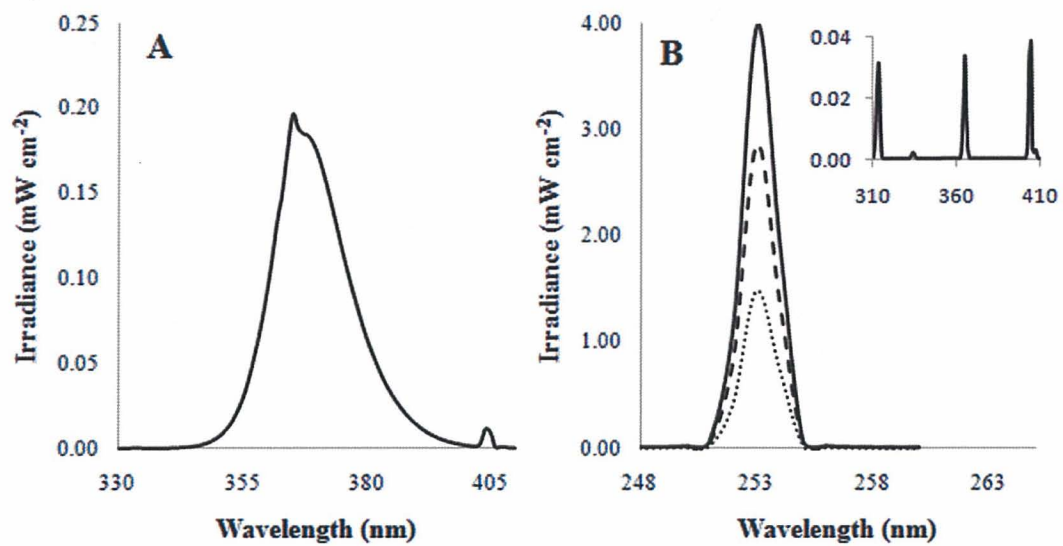


Figure 4:

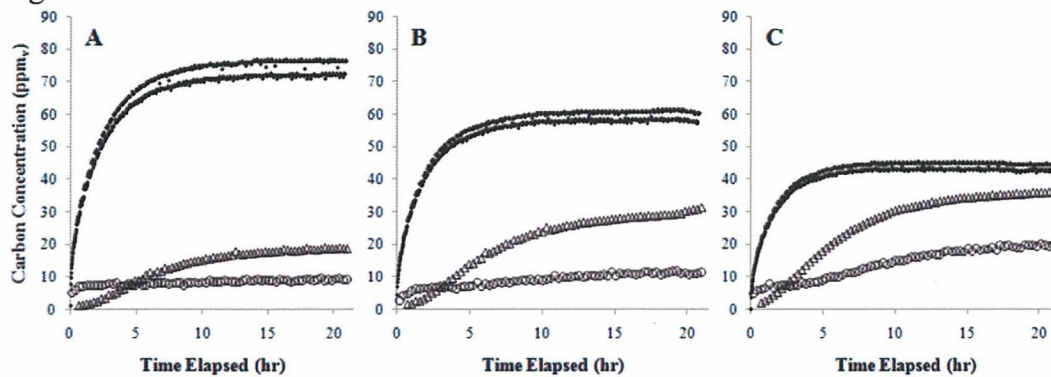


Figure 5:

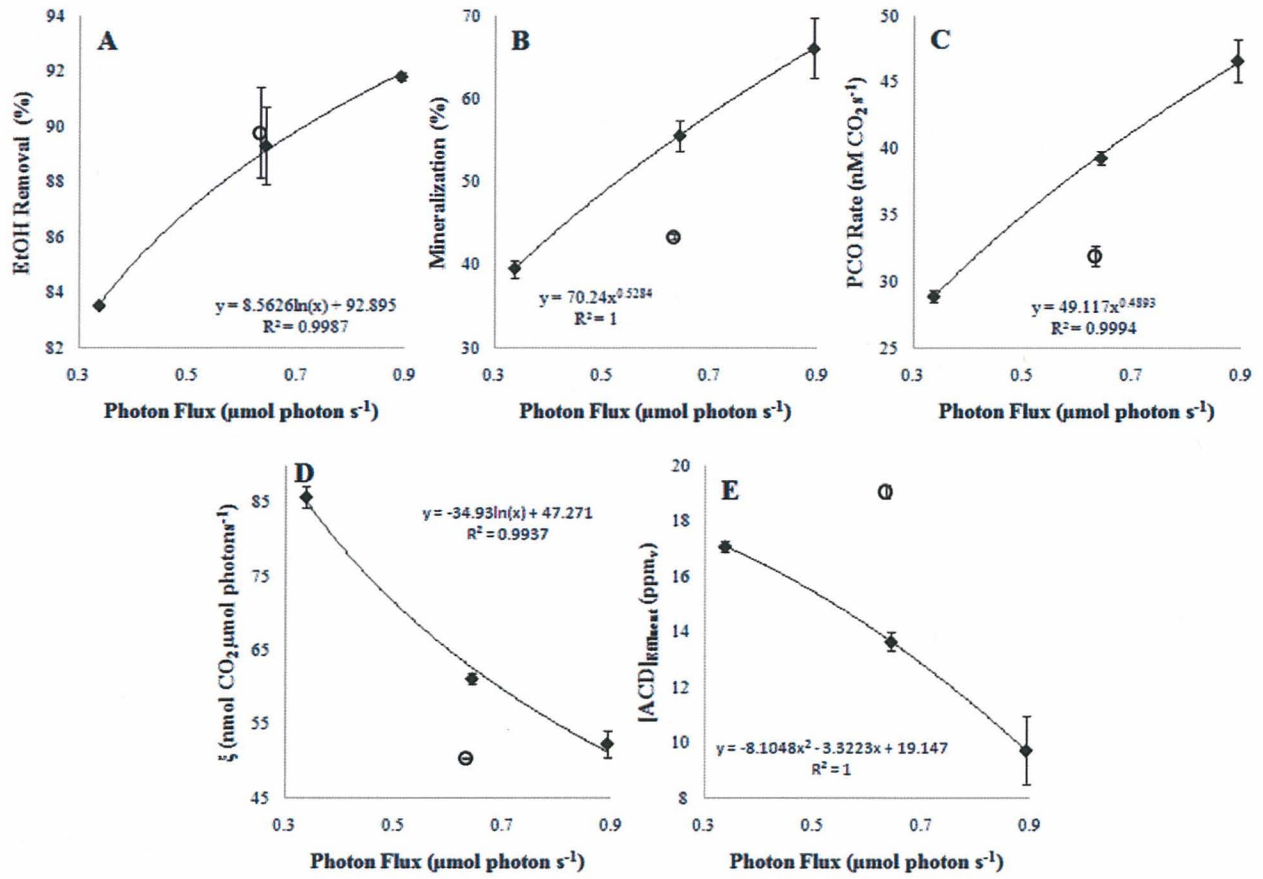


Figure 6:

