Advanced Catalysts for the Ambient Temperature Oxidation of Carbon Monoxide and Formaldehyde

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The primary applications for ambient temperature carbon monoxide (CO) oxidation catalysts include emergency breathing masks and confined volume life support systems, such as those employed on the Shuttle. While Hopcalite is typically used in emergency breathing masks for terrestrial applications, in the 1970s, NASA selected a 2% platinum (Pt) on carbon for use on the Shuttle since it is more active and also more tolerant to water vapor.

In the last 10-15 years there have been significant advances in ambient temperature CO oxidation catalysts. Langley Research Center developed a monolithic catalyst for ambient temperature CO oxidation operating under stoichiometric conditions for closed loop carbon dioxide (CO_2) laser applications which is also advertised as having the potential to oxidize formaldehyde (HCHO) at ambient temperatures. In the last decade it has been discovered that appropriate sized nano-particles of gold are highly active for CO oxidation, even at sub-ambient temperatures, and as a result there has been a wealth of data reported in the literature relating to ambient/low temperature CO oxidation.

In the shorter term missions where CO concentrations are typically controlled via ambient temperature oxidation catalysts, formaldehyde is also a contaminant of concern, and requires specially treated carbons such as Calgon Formasorb as untreated activated carbon has effectively no HCHO capacity. This paper examines the activity of some of the newer ambient temperature CO and formaldehyde (HCHO) oxidation catalysts, and measures the performance of the catalysts relative to the NASA baseline Ambient Temperature Catalytic Oxidizer (ATCO) catalyst at conditions of interest for closed loop trace contaminant control systems.

I. Background

With the advent of closed cycle CO_2 lasers, a considerable body of literature exists related to low temperature CO oxidation catalysts. The high energy plasma of the laser results in decomposition of CO_2 into stoichiometric quantities of CO and oxygen (O_2) which subsequently results in rapid power loss. To mitigate this phenomenon, low temperature CO oxidation catalysts have been developed to recombine the O_2 and CO, thereby maintaining the power output of the laser. While this application is targeting stoichiometric concentrations of CO and O_2 , more recently some of these catalysts are being evaluated for ambient temperature oxidation of CO and HCHO¹⁻².

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Much of the research related to CO_2 lasers has focused on platinum/tin-dioxide/silicon-dioxide (Pt/SnO₂/SiO₂) catalysts, however additional catalysts that have shown high activity include catalysts utilizing platinum or gold (Au) in combination with titanium dioxide (TiO2), aluminum oxide (Al₂O₃), manganese dioxide (MnO₂), and iron oxide supports (FeO and/or Fe₂O₃)³⁻⁶.

While the focus of this paper is on CO oxidation, in recent years there has been significant interest in the ambient temperature oxidation of HCHO targeting indoor air quality applications. Much of this work has identified platinum supported on tin oxide (SnO2) or titanium dioxide (TiO₂) supports as the most promising. Since most short term NASA missions requiring trace contaminant control utilize activated charcoal for the adsorption of most of the organics, and the fact that formaldehyde requires specially treated, expendable sorbents, a catalyst that can perform ambient temperature oxidation of CO and HCHO is advantageous from a design perspective.

Gold catalysts, developed by TDA Research (TDA) and 3M Corporation (3M), and platinum based catalysts developed by Hamilton Sundstrand, have been evaluated in preliminary screening tests to measure the relative activity compared to the NASA ATCO baseline ambient temperature CO oxidation catalyst which is 2% platinum on activated carbon. Additionally, limited testing for HCHO oxidation was also conducted for some of the catalysts. While the testing reported in this paper is focused on the low concentrations associated with trace contaminant control, TDA and 3M have performed additional testing of their gold catalysts at elevated CO concentrations ranging 1,000-10,000 ppm, some of which has been previously published⁷.

II. Discussion

Catalyst screening tests were conducted at approximate concentrations of interest to trace contaminant control systems consistent with the historical design requirements of the U.S. space program. Basic design requirements consider two sources of contamination – the crew and the equipment. The generation rates for numerous contaminants, compiled over the history of the U.S space program, along with the space maximum allowable concentrations (SMAC), are summarized by Perry⁸. The SMAC values for CO and HCHO are listed as 17 mg/m³ (15 ppm, ppm = mg/m³ x 22.4 liter/mole / molecular weight at 0 °C) and 0.12 mg/m³ (0.1 ppm) respectively. Nominal concentrations used in the catalyst screening tests reported in this study were approximately 10 ppm and 100 ppb, for CO and HCHO respectively.

A. CO Oxidation Tests

The test rig used for the CO oxidation studies is shown below in Fig. 1.



Figure 1.CO Oxidation Test Rig

2 American Institute of Aeronautics and Astronautics

The concentration of CO is controlled by adjusting the flow rate of a high concentration CO/nitrogen supply which is subsequently mixed with filtered laboratory air prior to feeding the CO/air mixture to the reactor. The influent is then humidified by diverting part of the process air flow through the humidifier. Table 1 identifies the characteristics of the catalysts examined.

Catalyst	Active Metal	Reactant	Support
ATCO	Pt	CO/ HCHO	Carbon
HSPT1	Pt	CO/ HCHO	TiO ₂
HSPT2	Pt	CO/ HCHO	SiO ₂
STC	Pt	CO	SnO ₂
TDA Au	Au	CO	Proprietary
3M Au	Au	CO	Proprietary

Table 1. Catalyst Characteristics

To determine an appropriate flow rate to be used in the CO screening tests, the current NASA ATCO reactor design point flow rate and catalyst volume was used for scaling, which resulted in a gas hourly space velocity (GHSV) of 2,500 hr⁻¹. However, at this space velocity the conversion of all catalysts was 100% for 5 days and therefore a relative comparison could not be made. To address this, the GHSV was increased until a conversion less than 100% was measured. A GHSV of 110,400 hr⁻¹ was determined sufficient to result in a measurable range of conversions for the various catalysts. All of the catalysts were initially tested in the "as received" form and particle size, with the exception of the TDA Au catalyst which was sieved to remove fines. The initial performance comparison utilized a volume of 15 cc for each of the catalysts tested. The results for the initial screening tests for the various catalysts in dry air at 10 ppm CO are shown in Fig. 2.



Figure 2. Relative Activity of CO Oxidation Catalysts for Trace Contaminant Control Applications at GHSV of 110,400 hrs⁻¹, 10ppm Inlet CO, in Dry Air

Figure 2 shows that most of the catalysts tested indicated higher activities for CO oxidation than the NASA baseline.

The STC Catalysts, Inc. (STC) monolith catalyst had the lowest conversion of all of the catalysts shown which is primarily assumed to be a result of lower active metal content per unit volume of catalyst, though the specific formulation was not available from the manufacturer.

As can be seen in Fig. 2, particle size has a significant effect on the activity of the platinum catalyst HSPT1, and though not measured experimentally, it is assumed that this would be true for the other catalysts tested. This is due to the high intrinsic CO oxidation reaction rate being much higher than the diffusion rate of CO within the catalyst structure. To be able to distinguish the relative activities of the 14x25 mesh catalysts, a higher space velocity ($1,850,000 \text{ hr}^{-1}$) and higher CO concentration (40 ppm) were tested and the results shown in Fig. 3.



Figure 3. Relative Activity of 14x25 mesh CO Oxidation Catalysts at GHSV of 1,850,000 hrs⁻¹, 40ppm Inlet CO, in Dry Air

The oscillations noted for the platinum catalyst are consistent with similar observations for CO oxidation reported in the literature and is attributed to a periodic "restructuring" of the active species which are adsorbed on the platinum⁹⁻¹⁰.

The effect of relative humidity was investigated in two separate tests due to the differences in conversion as a result of particle size. The larger catalyst particles, resulting in the lower conversions shown in Fig. 2, were tested at a GHSV of 110,400 hr⁻¹, whereas the smaller catalyst particles were tested at higher space velocities and a higher CO concentration to provide some resolution of the relative activity of the catalysts. The results of these tests are



shown in Fig. 4 and Fig. 5. The HSPT1 14x25 mesh platinum catalyst resulted in 100% conversion at a GHSV of 160,000 hr^{-1} but was not tested at 240,000 hr^{-1} .

Figure 4. Relative Activity of Larger Particle CO Oxidation Catalysts for Trace Contaminant Control at a GHSV of 110,400 hr⁻¹ at 50% Relative Humidity (transient performance at beginning and end of test due to humidification bypass)



Figure 5. Relative Activity of 14x25 mesh Au CO Oxidation Catalysts for Trace Contaminant Control Applications at Various GHSV, 40ppm Inlet CO, at 50% Relative Humidity

At the conditions shown for the two gold catalysts in Fig. 5, the 3M catalyst showed minimal effect due to the presence of water vapor, even with a 50% increase in GHSV, whereas the conversion of the TDA catalyst decreased approximately 38%. It is interesting to note that at higher space velocities in dry air, the TDA gold catalyst had a higher conversion compared with the 3M catalyst as noted in Fig. 3. This could be due to two factors. First, the active metal content of the 3M catalyst may be lower than TDA's and therefore at the higher space-velocity there are insufficient active sites to sustain the high reaction rate. Secondly, it is possible that due to the shorter duration of the tests conducted in the presence of water vapor, that the higher activity observed for the 3M catalyst is a result of its high initial activity (as seen in the dry testing) and if run for a longer test period, a decrease in activity would have been observed.

B. HCHO Oxidation Tests

The HCHO oxidation test set-up accommodated simultaneous testing of all candidate catalysts, using a series of 3-way valves on the outlet of each reactor to select the individual reactors for HCHO analysis of the effluent. A single, common synthetic air stream (20% O2, 80% N2) was used in all tests. Formaldehyde was generated by vaporizing paraformaldehyde. Formaldehyde generation was based on controlled diffusion of formaldehyde vapor. The formaldehyde generator consists of a vial, in which a quantity of paraformaldehyde was deposited, a diffusion tube attached to the vial, a containment vessel and a temperature controlled water bath. The vial is secured inside the containment vessel which is immersed in the water bath. Nitrogen carrier gas, preheated to the water bath operating temperature, enters the containment vessel and sweeps away formaldehyde from the end of the diffusion tube/vial before finally leaving the containment vessel. Humidity levels were controlled by passing part of the flow stream

though a bubbler followed by dilution with the balance of the flow stream and mixed prior to entering the bank of reactors. The HCHO test rig schematic is shown below in Fig. 6.



Figure 6. Detailed Schematic of HCHO Oxidation Test Rig

HCHO testing was conducted only on the "as received" larger granule size platinum catalyst. These tests were not conducted on the STC catalyst due to its low activity with respect to CO oxidation while the 3M and TDA gold catalysts were not available at the time of this study.

HCHO screening tests were conducted at GHSVs ranging from $6,000 - 120,000 \text{ hr}^{-1}$. Tests were conducted in dry air and at 30% RH, all at ambient temperature. Most of the tests were conducted at an inlet HCHO concentration of approximately 100 ppb while one test was conducted at an inlet HCHO concentration of approximately 300 ppb at a GHSV of 120,000 hr⁻¹. Since no significant deactivation was noted during the testing, the same catalyst was used for all tests. Moisture was introduced between hours 375 and 500. Results for the various tests are shown for the three catalysts in Figs. 7-9.



Figure 7. Screening Test for HCHO Oxidation on ATCO Catalyst



Figure 8. Screening Test for HCHO Oxidation on HSPT1 1/8" Cylinder Catalyst



Figure 9. Screening Test for HCHO Oxidation on HSPT2 1/8" Cylinder Catalyst

For the three catalysts tested, there were no significant differences noted in performance over the range of conditions tested. At high space velocities, the dry HSPT2 performance was slightly lower than the others, however with the introduction of moisture, the oxidation efficiency increased to levels consistent with the others. In general the effect of moisture was relatively small and not as pronounced as in the CO oxidation screening tests. Upon changing the inlet HCHO concentration to 300 ppb, at approximately 250 hours into the test, there was no significant change in conversion.

In addition to the oxidation efficiency, the outlet CO_2 concentration was also measured to allow for a mass balance to verify complete oxidation of the HCHO to CO_2 and water without the formation of intermediate species. The outlet CO_2 concentrations for the three catalysts are shown below in Fig. 10 and shows that the HCHO is completely oxidized to CO_2 within expected experimental accuracy. For complete oxidation of HCHO, the outlet CO_2 concentration should be identical to the inlet HCHO concentration. The initial lower than expected CO_2 concentration is believed to be due to an initial adsorption of the CO_2 and/or HCHO as the surface species come to equilibrium on the catalyst surface, whereas the spike noted at approximately 80 hours into the test can be traced to an approximate 5° C increase in ambient temperature, most likely resulting in desorption of adsorbed CO_2 from the catalysts.



Figure 10. Carbon Mass Balance during HCHO Oxidation – Effluent CO₂ Concentration

III. Conclusion

For all the catalysts tested for CO oxidation at the nominal Shuttle design space velocity, 100% conversion was obtained for 5 days indicating that there is most likely significant margin in the current ATCO reactor. For the catalysts tested, the platinum catalyst were more active than gold catalysts, and a significant internal mass transfer resistance is demonstrated through the testing of smaller catalyst particles, indicating that additional enhancements are possible assuming that any increased pressure drop resulting from smaller particles can be addressed using appropriate reactor design. Additionally, catalyst supports with more open structures (higher effectiveness factor) may also warrant future investigation to reduce the required amount of catalyst.

The Pt-based catalysts were more active than the Au-based catalysts at high space velocity. While the TDA Aubased catalyst was more active than the 3M catalyst in dry air, the 3M catalyst was less susceptible to moisture than the TDA catalyst. Additional testing is warranted to determine if the 3M catalyst's performance under humid conditions is sustained for longer periods of time.

All of the platinum catalysts demonstrated similar activities for HCHO oxidation, with 100% conversion at 100ppb inlet concentrations up to a GHSV of 60,000hr⁻¹, with the conversion dropping to approximately 50% at a GHSV of 120,000hr⁻¹. Minimal effect of moisture was noted at 30%RH for the HCHO oxidation on the platinum catalysts.

Based on the higher activity resulting from particle size for the platinum catalyst, a higher effectiveness catalyst would reduce bed size, though the potential impact on HCHO has not been validated.

In summary, advanced platinum and gold catalysts have demonstrated significantly higher ambient temperature oxidation efficiency for CO than the NASA baseline ATCO catalyst, and the platinum catalysts have demonstrated activity for ambient temperature oxidation of HCHO.

10 American Institute of Aeronautics and Astronautics

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