

ACCGE-17 ABSTRACT

Stability of Detached Solidification

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Abstract

Bridgman crystal growth can be conducted in the so-called “detached” solidification regime, where the growing crystal is detached from the crucible wall. A small gap between the growing crystal and the crucible wall, of the order of 100 micrometers or less, can be maintained during the process. A meniscus is formed at the bottom of the melt between the crystal and crucible wall. Under proper conditions, growth can proceed without collapsing the meniscus. The meniscus shape plays a key role in stabilizing the process. Thermal and other process parameters can also affect the geometrical steady-state stability conditions of solidification. The dynamic stability theory of the shaped crystal growth process has been developed by Tatarchenko [1]. It consists of finding a simplified autonomous set of differential equations for the radius, height, and possibly other process parameters. The problem then reduces to analyzing a system of first order linear differential equations for stability. Here we apply a modified version of this theory for a particular case of detached solidification. Approximate analytical formulas as well as accurate numerical values for the capillary stability coefficients are presented. They display an unexpected singularity as a function of pressure differential. A novel approach to study the thermal field effects on the crystal shape stability has been proposed. In essence, it rectifies the unphysical assumption of the model [1] that utilizes a perturbation of the crystal radius along the axis as being instantaneous. It consists of introducing time delay effects into the mathematical description and leads, in general, to stability over a broader parameter range. We believe that this novel treatment can be advantageously implemented in stability analyses of other crystal growth techniques such as Czochralski and float zone methods.

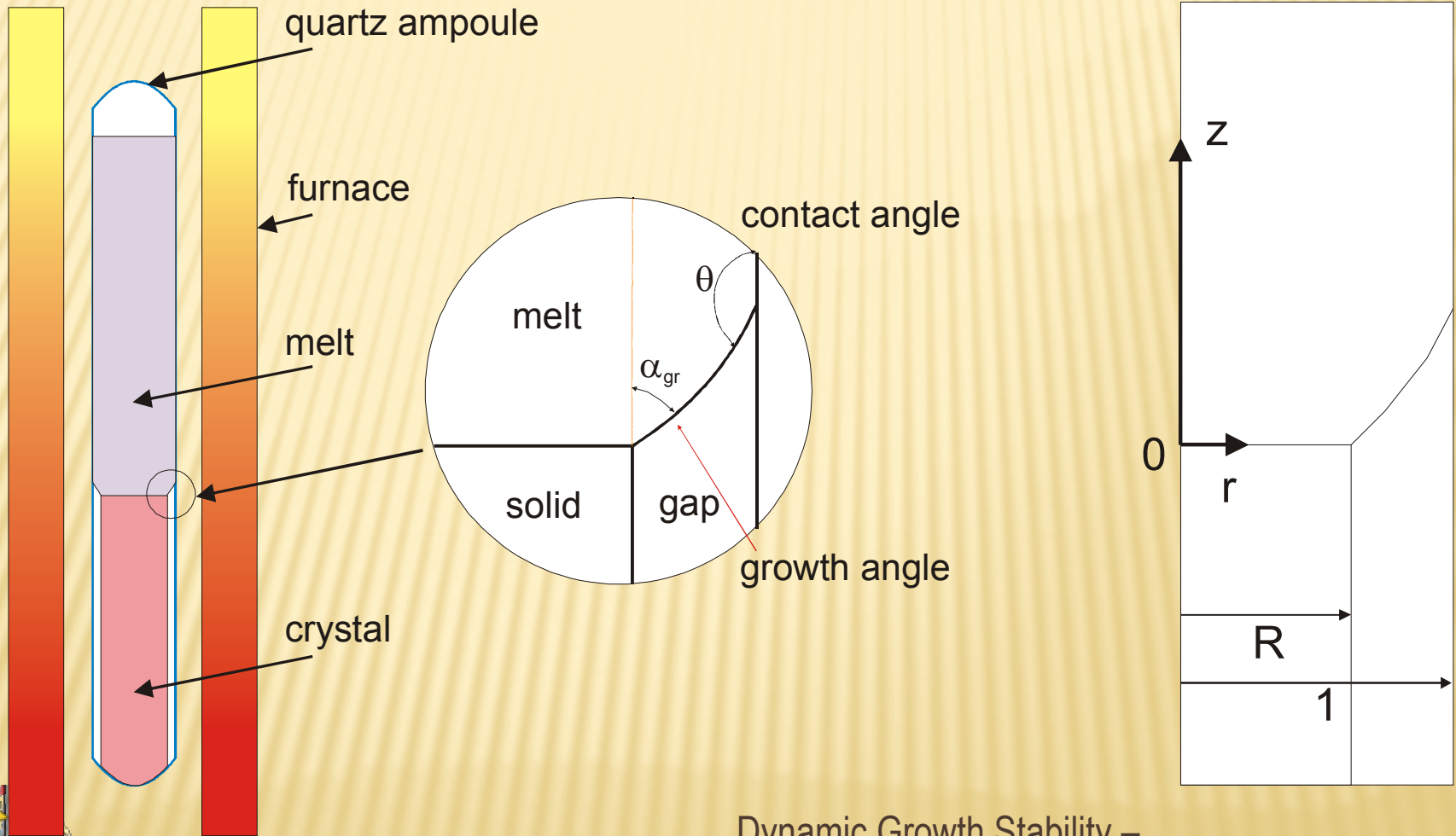
[1] V. A. Tatarchenko, *Shaped Crystal Growth*, Springer, 1993, pp. 19.

STABILITY OF DETACHED SOLIDIFICATION

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DETACHED BRIDGMAN GROWTH



Dynamic Growth Stability –
V.A.Tatarchenko – Shaped Crystal Growth



SYSTEM RESPONSE TO PERTURBATIONS

Linear response of perturbed crystal radius and height

$$\delta \dot{R} = A_{RR} \delta R + A_{Rh} \delta h$$

$$\delta \dot{h} = A_{hR} \delta R + A_{hh} \delta h$$

Stable growth if

$$A_{RR} + A_{hh} < 0$$

$$A_{RR} A_{hh} - A_{Rh} A_{hR} > 0$$



CAPILLARITY PROBLEM

Young-Laplace equation

$$\frac{z''}{(1+z'^2)^{3/2}} + \frac{z'}{r(1+z'^2)^{1/2}} = a - b z(r)$$

$$a = \frac{\Delta P_m r_C}{\gamma}$$

$$b = \frac{\rho g_0 r_C^2}{\gamma}$$

$$\Delta P_m = (P_{top} + \rho g H) - P_{bot}$$



CAPILLARY COEFFICIENTS - THEORY

$$A_{RR} = -V \frac{\partial \beta}{\partial R}$$

$$A_{Rh} = -V \frac{\partial \beta}{\partial h}$$

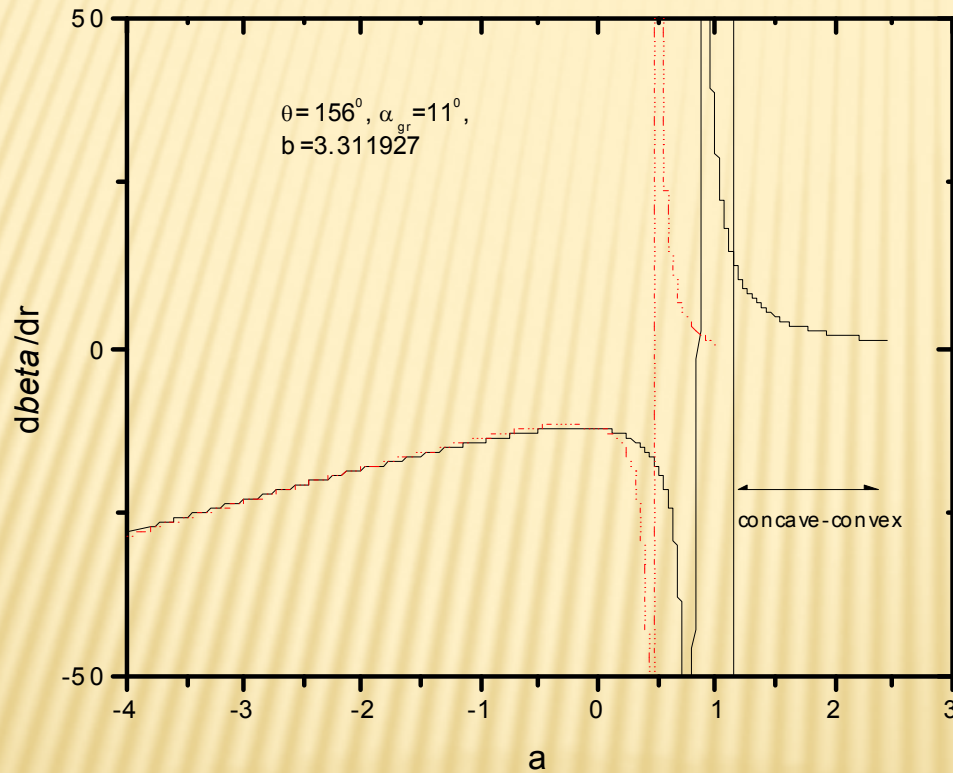
V – pulling rate

$$\frac{\partial \beta}{\partial R} = \frac{(aR - \cos \alpha_{gr}) \sin(\alpha_{gr})^2}{R_s (\alpha_{gr})^3 - b(5 - R)^2 (2.4 + R/8)}$$

$$\frac{\partial \beta}{\partial h} = -\frac{r_c^2 \rho g}{2\gamma} \frac{(1 - R^2) \sin \alpha_{gr}^2}{R_s \alpha_{gr}^3 - b(5 - R)^2 (2.4 + R/8)}$$



CAPILLARY COEFFICIENTS - NUMERICS



THERMAL RESPONSE - BASICS

Boundary condition at the interface

$$V_c L = k_s \frac{\partial T_s}{\partial z} - k_L \frac{\partial T_L}{\partial z}$$

Growth rate $V_c = V + \partial h / \partial t$

Height perturbation - Tatarchenko's model

$$\frac{\partial \delta h}{\partial t} = L^{-1} \left(k_s \frac{\partial G_s}{\partial h} - k_L \frac{\partial G_L}{\partial h} \right) \delta h + L^{-1} \left(k_s \frac{\partial G_s}{\partial R} - k_L \frac{\partial G_L}{\partial R} \right) \delta R$$

$$\delta G_s \neq \frac{\partial G_s}{\partial R} \delta R$$

questionable



ONE-DIMENSIONAL LUMP HEAT MODEL

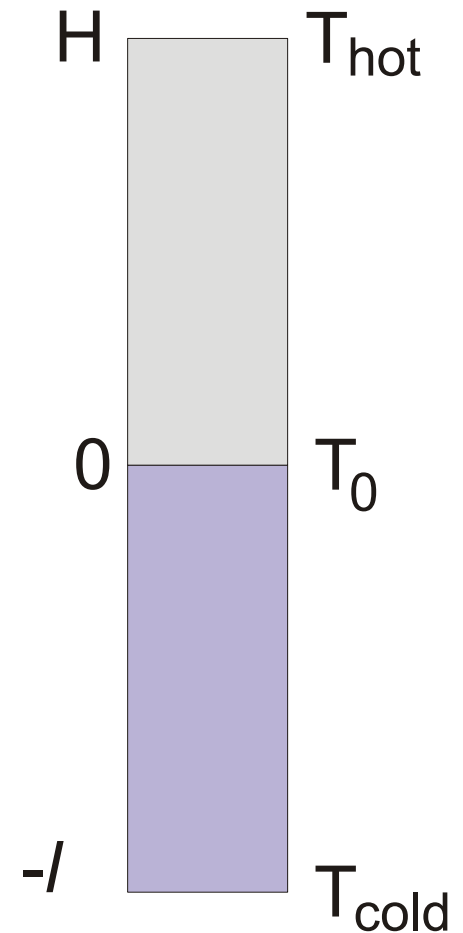
For melt
$$\frac{\partial^2 T_L}{\partial z^2} + \frac{V}{\kappa_L} \frac{\partial T_L}{\partial z} - \frac{\mu_L}{k_L} \frac{2}{r_C} (T_L - T_e) = 0$$

For crystal
$$\frac{\partial^2 T_S}{\partial z^2} + \frac{V}{\kappa_S} \frac{\partial T_S}{\partial z} - \frac{\mu_S}{k_S} \frac{2}{R + \delta(z)} (T_S - T_e) = 0$$

$$A_{hh} = -L^{-1} k_L \frac{T_{hot} - T_0}{H^2} - L^{-1} k_S \frac{T_0 - T_{cold}}{l^2}$$

Perturbation of thermal gradient at the interface due to crystal radius variation (convolution):

$$\delta G_S = -\frac{2\mu_S (T_0 - T_{cold}) V}{R^2 k_S} \int_0^t \delta R(t') e^{-V(t-t') \sqrt{\left(\frac{V}{\kappa_S}\right)^2 + \frac{8\mu_S}{k_S R}}} dt'$$



GENERALIZED RESPONSE

$$\delta \dot{h} = \int_0^t \delta R(t') G(t-t') dt' + A_{hh} \delta h$$

$$\delta \dot{R} = A_{RR} \delta R + A_{Rh} \delta h$$

Laplace transform solution

$$h(s) = \frac{G(s)\delta R(0) + s(\delta h(0) - A_{RR} \delta h(0))}{s^2 - s(A_{RR} + A_{hh}) + A_{RR}A_{hh} - A_{Rh}G(s)}$$

$$R(s) = \frac{\delta R(0)(s - A_{hh}) + A_{Rh} \delta h(0)}{s^2 - s(A_{RR} + A_{hh}) + A_{RR}A_{hh} - G(s)A_{Rh}}$$



GENERALIZED RESPONSE CONT.

Tatarchenko model gives

$$A_{hR} = -\frac{2V\mu_s(T_0 - T_e)}{LR^2s_0}$$

Our model

$$G(s) = \frac{A_{hR}s_0}{s + s_0}$$

$$s_0 = V \sqrt{\left(\frac{V}{\kappa_s}\right)^2 + \frac{8\mu_s}{k_s R}}$$

Response for the induced perturbation can be studied by analyzing the roots of the following polynomial

$$s^2 (s + s_0) - s(s + s_0)(A_{RR} + A_{hh}) + A_{RR}A_{hh}(s + s_0) - A_{Rh}A_{hR}s_0 = 0$$

MODIFIED STABILITY CRITERION

Conditions for stable growth

Our model

$$A_{RR}A_{hh} - A_{Rh}A_{hR} > 0$$

$$A_{RR} + A_{hh} < S_0$$

$$A_{RR}A_{hh} - S_0(A_{RR} + A_{hh}) > 0$$

Tatarchenko model

$$A_{RR}A_{hh} - A_{Rh}A_{hR} > 0$$

$$A_{RR} + A_{hh} < 0$$



MODEL APPROXIMATIONS

- Environmental temperature is constant
- One-dimensional lump type approximation
- Capillarity – zero order model – no meniscus motion effects, no triple point effects



CONCLUSION

- ✘ Capillarity coefficients display singularity
- ✘ Thermal response for the radius perturbation is of the convolution type – this modified model is applicable for other types of shaped crystal growth: Czochralski, Float Zone, etc.

