



Characteristics of Elastomer Seals Exposed to Space Environments

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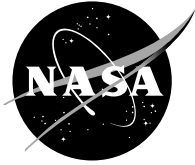
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Abstract

A universal docking and berthing system is being developed by the National Aeronautics and Space Administration (NASA) to support all future space exploration missions to low-Earth orbit (LEO), to the Moon, and to Mars. The Low Impact Docking System (LIDS) is being designed to operate using a seal-on-seal configuration in numerous space environments, each having unique exposures to temperature, solar radiation, reactive elements, debris, and mission duration. As the LIDS seal is likely to be manufactured from an elastomeric material, performance evaluation of elastomers after exposure to atomic oxygen (AO) and ultraviolet radiation (UV) was conducted, of which the work presented herein was a part. Each of the three candidate silicone elastomer compounds investigated, including Esterline ELA-SA-401, and Parker Hannifin S0383-70 and S0899-50, was characterized as a low outgassing compound, per ASTM E595, having percent total mass loss (TML) less than 1.0% and collected volatile condensable materials (CVCM) less than 0.1%. Each compound was compatible with the LIDS operating environment of -50 to 50 °C. The seal characteristics presented include compression set, elastomer-to-elastomer adhesion, and o-ring leakage rate. The ELA-SA-401 compound had the lowest variation in compression set with temperature. The S0383-70 compound exhibited the lowest compression set after exposure to AO and UV. The adhesion for all of the compounds was significantly reduced after exposure to AO and was further decreased after exposure to AO and UV. The leakage rates of o-ring specimens showed modest increases after exposure to AO. The leakage rates after exposure to AO and UV were increased by factors of up to 600 when compared to specimens in the as-received condition.

Nomenclature

AO	atomic oxygen
APAS	Androgynous Peripheral Assembly System
CBM	Common Berthing Mechanism
CEV	Crew Exploration Vehicle

CVCM	collected volatile condensable materials
ESH	equivalent sun hours
ISS	International Space Station
LEO	low-Earth orbit
LIDS	Low Impact Docking System
LVDT	linear variable displacement transformer
NASA	National Aeronautics and Space Administration
NUV	near ultraviolet radiation
RTD	resistance temperature detector
TML	total mass loss
UV	ultraviolet radiation
VUV	vacuum ultraviolet radiation

I. Introduction

The National Aeronautics and Space Administration (NASA) is developing the Low Impact Docking System (LIDS)¹ for in-space assembly of structures and rendezvous of vehicles to enable mission profiles that will ensure the success of NASA's Vision for Space Exploration. The LIDS eliminates the need for high velocity docking, provides low velocity berthing assembly, and establishes a standard interface that is reconfigurable and supports a wide range of crewed and autonomous vehicle mating and assembly operations. The LIDS is a fully androgynous mating interface designed for a wide variety of space missions, reducing the quantity of unique mechanisms, mission analyses, and training by providing the ability to structurally connect with replicate LIDS. The objective of the LIDS development effort is to provide a universal linkage attached to every in-space structure and vehicle which will join to any other in-space structure.

The mating systems currently in use, including the Common Berthing Mechanism (CBM) used to connect elements of the International Space Station (ISS) and the Androgynous Peripheral Assembly System (APAS) used to dock the Space Shuttle to the ISS, can function either as a berthing or docking mechanism, but not both. Docking refers to the mating between two free-flying structures or vehicles which are generally crewed. The joining of two structures using a robotic arm, generally unmanned autonomous modules, is referred to as berthing. Though the APAS was originally designed to be androgynous, the interface seal attached to the ISS was subsequently removed. These mating systems, in their current configurations, are composed of two non-identical halves (a male and a female), which limits their functionality to mating with structures having the opposite gender interface.

The LIDS is a fully androgynous system, such that each system half is an identical replicate of any other. Any two vehicles or modules, each having a LIDS incorporated, can mate with the other without regard for gender. At the time of mating, one LIDS is selected as the active side; the other is selected as the passive side. This type of interface provides full system redundancy which improves fault tolerance. Should a mechanism failure occur in the active LIDS, the roles are reversed such that the active is designated passive and the failure circumvented.

The androgynous nature of the LIDS creates challenges for the sealing interface between the two pressurized modules. Since each system half is an exact replicate of its mating counterpart, the gas seals must interact with a identical seal instead of a more conventional flat surface. This unconventional interaction between the gas seals adds adhesion between two similar elastomer seals as an important design consideration in addition to seal compression set and leakage flow rate, amongst others. If the adhesion forces are too great, the seals will not allow the vehicles to separate from one another without excessive force. Additionally, the possibility of dislodging one of the two systems' seals is real. Even the partial removal of one of the seals would render the attachment interface useless and must be avoided.

The operating and non-operating environments of the LIDS also create challenges for the development of the LIDS main interface seal. The non-operating environment includes the space environments to which the seal is exposed when the LIDS is not mated to another LIDS. Overcoming the synergistic effects of atomic oxygen (AO), ultraviolet and particle radiation, and debris (micrometeoroids, orbital debris, and dust) is the most problematic. The operating environment includes the temperature range to which the seal is expected to be exposed when performing docking/undocking operations. The envelope into which the LIDS seal must be designed greatly affects the performance characteristics of the seal and must be considered when developing the system. The basis for the seal design, however, is the underlying performance of the elastomers within the operating and non-operating environments.

At low altitudes, oxygen is a diatomic molecule (O₂), however, in the upper atmosphere of low-Earth orbit (LEO) photodissociation of the molecular bond between the two oxygen atoms occurs. Monatomic oxygen, or atomic oxygen, is created and is highly reactive. The exposure of unprotected materials to AO can greatly degrade performance depending upon their resistivity to oxidizing environments. The amount of AO to which the unshielded seals would be exposed will vary depending upon the mission altitude and solar activity during the mission. The average value for expected AO fluence for the years 2006-2016 is 2.0×10^{21} oxygen atoms/cm²/year (1.3×10^{22} atoms/in²/year) based upon a nominal ISS orbital trajectory.²

For organic compounds, including silicone elastomers considered herein, the exposure to ultraviolet radiation (UV) can be a strong contributor to degradation. In orbits around the Earth and Moon, as well as on the lunar surface, incident UV scissions long molecule chains. The broken bonds recombine, thereby cross-linking intertwined molecular chains. The results are shorter molecular chains than the originals and a compound with modified properties, including increased stiffness. After excessive exposure to UV, organic materials embrittle and become unusable for seal applications.

Earth and lunar surface albedo cannot be discounted for long duration missions. Though little UV is reflected from the surface (29% from the Earth³ and 7.5% from the Moon⁴), the additive effect of long time exposures can be potentially significant. Therefore, the amount of UV to which the unshielded seal is expected to be exposed is highly dependant upon the mission and careful consideration must be given to the mission duration and profile. For example, a nose nadir at noon solar inertia orbit of the Moon for 210 days would expose the LIDS seal to a UV exposure of 126 equivalent Sun hours (ESH); the exposure for a nose nadir at midnight solar inertia orbit would be 3190 ESH.

The current LIDS design does not have accommodations for a thermal management system to control the temperature of the LIDS, its tunnel, or the seal. Therefore, the temperature can be actively adjusted only by managing the heat flux generated through solar heating. The operating temperature envelope of the LIDS is -50 to 50 °C (-58 to 122°F).

Silicone elastomer compounds are typically used for seals for space flight applications where extreme heat is not a factor. Silicone elastomer compounds have a large range of operating temperatures and can function at cold temperatures better than other elastomer compound classes, due to their low embrittlement temperatures. However, only a limited number of silicone elastomers meet the low-outgas standards that NASA requires of all materials used in space. NASA specifies that all materials used for external spacecraft structures exhibit low-outgassing characteristics, as liberated products can condense onto solar cells, optical components, and thermal radiators, reducing their functionality. Materials exhibiting minimal volatility, total mass loss (TML) less than 1.0% and collected volatile condensable materials (CVCM) less than 0.1%, have a low potential for contaminating surrounding components or assemblies.

A number of investigators have studied the effects of space environments on material performance.⁵⁻¹⁸ However, only a limited number have researched seal materials.¹⁹⁻²¹ The objective of the work presented herein was to add to this body of knowledge by evaluating the characteristics of three silicone elastomers, including compression set, adhesion force between replicate samples, and the rate of leakage flow of seals. The performance of the elastomers after AO exposure and after AO and UV exposures was compared to their performance in the as-received condition in order to quantify the effects of space environments.

II. Description of the experiments

A. Specimens

Three candidate elastomer compounds of different durometer values were evaluated in this study. Specimens were molded from three types of silicone elastomer compounds produced by two manufacturers. Each compound studied (Esterline ELA-SA-401, Parker Hannifin S0899-50 and Parker Hannifin S0383-70) was classified as low-outgassing having TML less than 1.0% and CVCM less than 0.1%, per ASTM E595.²² Measured values of TML and CVCM are listed in Table 1.

TABLE 1.—RESULTS OF OUTGAS TESTING ON THREE SILICONE ELASTOMER COMPOUNDS

Compound	Durometer A	Total mass loss, (%)	Collected volatile condensable materials, (%)
ELA-SA-401	38	0.07	0.04
S0899-50	50	0.32	0.08
S0383-70	70	0.30	0.06

1. Specimens for Compression Set Tests

Specimens for compression set tests were molded from the three silicone elastomer compounds into standard AS-568A size 2-309 o-ring form. For reference, the dimensions are shown in Table 2. Specimens were prepared consistent with the standard test protocol per ASTM D395.²³

TABLE 2.—NOMINAL DIMENSIONS OF AS-568A SIZE 2-309 O-RINGS

Dimension	Units	Value
Outside diameter	cm (in.)	2.11 (0.832)
Inside diameter	cm (in.)	1.05 (0.412)
Thickness	cm (in.)	0.533 (0.210)

2. Specimens for Elastomer-to-Elastomer Adhesion Tests

Specimens for adhesion tests were fabricated from 0.53 cm (0.21 in.) thick sheet material manufactured from the three silicone elastomer compounds. Specimens were cut from the sheet using a lubricated rotating punch to form a cylindrical specimen approximately 0.89 cm (0.35 in.) in diameter and 0.53 cm (0.21 in.) thick. The specimens were not perfect cylinders due to the compliance of the elastomer sheet. The lowest durometer material specimens, ELA-SA-401, exhibited the greatest amount of taper in the cylindrical surface. For each trial, the contact areas of the specimens were measured to compensate for the variation in diameters. Prior to testing, any mold releasing agent or lubricant remaining on the specimens was removed by cleaning with isopropyl alcohol and air drying.

3. Specimens for Leakage Flow Tests

Specimens for leakage flow tests were standard AS-568A size 2-309 o-rings molded from the three silicone elastomer compounds. They were unmodified from their as-received condition beyond cleaning with isopropyl alcohol and air drying. The final design of the LIDS main interface seal has not been completed and is not likely to be a standard o-ring geometry. However, the o-rings were representative seals on which the influence of space environments was investigated.

B. Space Environments Exposures

The specimens were tested in their as-received condition, as well as after exposure to simulated space environments. Select specimens were exposed to AO and then tested. Additional tests were conducted on specimens that received both AO and subsequent UV exposure.

Specimens were cleaned prior to initial space environments exposure. After exposure to AO or UV, only compressed gas was used to remove any dust that may have settled on the specimens.

1. Atomic Oxygen (AO) Exposure

The specimens were exposed to AO in a directed beam facility located at NASA Glenn Research Center that used an electron cyclotron resonance plasma source operated on pure oxygen (Fig. 1). A brief description of the facility is presented for completeness and the details of the facility were given in the work by Stidham.²⁴ The facility generated a directed thermal energy beam of AO with less than 1% ions at energies of typically 15 to 18 eV. The source operated at microwave energy (2.45GHz, 1000 W) and used two large electromagnets for both dissociation of oxygen through electron collision and for beam focusing. The exposure was completed while the chamber was at vacuum pressure (0.03 to 0.1 Pa (0.2 to 0.8 mTorr)). In addition to producing AO, the source also produced vacuum ultraviolet (VUV) radiation at 130 nm at an intensity of approximately 150 suns. Specimens were placed onto a circular plate that was mounted in the facility for exposure such that only the surfaces nearest the source were exposed to AO.

Five polyimide Kapton H specimens were positioned to provide AO fluence measurements. Using spatial interpolation, the AO fluence of each individual elastomer specimen was determined through simultaneous exposure of the Kapton witness specimens per ASTM E2089.²⁵ These specimens have well known erosion rates when exposed to AO and serve as a quantification method for exposure to AO.²⁵ The witness specimens were placed in an 8 to 13 Pa (60 to 100 mTorr) vacuum for 48 hr prior to and subsequent to AO exposure to fully dehydrate. The difference in mass of the polyimide Kapton was used to calculate the effective fluence using Eq. 1,²⁵ where F was

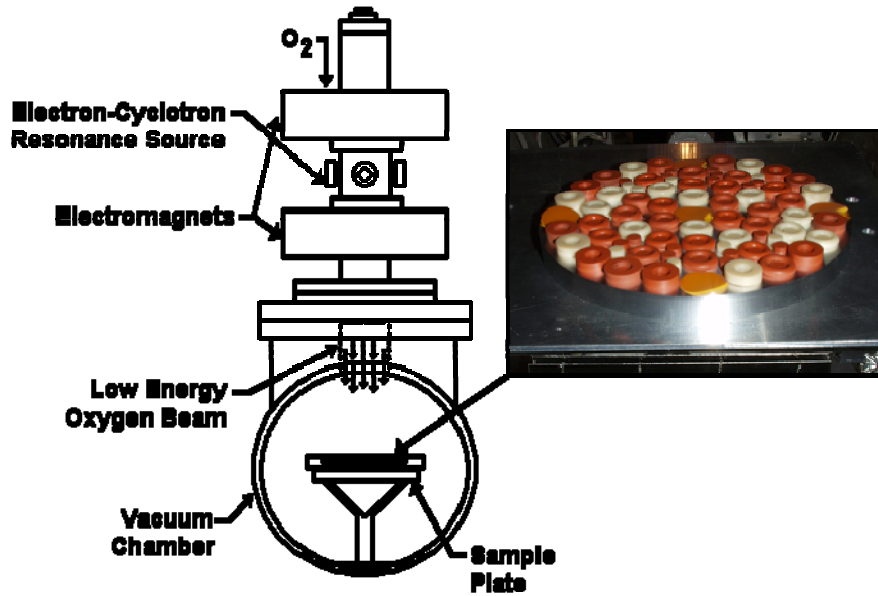


Figure 1.—AO exposure facility diagram and photograph of specimen plate.

$$F = \frac{m}{A \cdot \rho \cdot E} \quad (1)$$

the AO fluence (atoms/cm²), m was the mass loss of polyimide Kapton H (g), A was the area of the polyimide Kapton H exposed to AO (cm²), ρ was the density of polyimide Kapton H (1.42 g/cm³ (0.05 lbm/in.³)), and E was the erosion yield for polyimide Kapton H in LEO (3×10^{-24} cm³/atom (1.83×10^{-25} in.³/atom)).

2. Ultraviolet (UV) Radiation Exposure

Select specimens were exposed to UV to characterize the effects of several levels of UV on the three seal elastomers. Prior to UV exposure, the selected specimens were exposed to a level of AO fluence between 5.1×10^{21} and 7.3×10^{21} atoms/cm² (3.3×10^{22} and 4.7×10^{22} atoms/in.²). The specimens were subjected to UV exposure and then adhesion or leakage rate tested before receiving additional UV exposure and testing.

The specimens were simultaneously exposed to VUV and near ultraviolet (NUV) radiation in an exposure facility located at NASA Glenn Research Center. A brief description of the facility is presented for completeness and the details of the facility are given in the work by Dever.²⁶

The facility uses a cryogenic vacuum pumping system to expose samples under high vacuum conditions. The specimens were subjected to a pressure of approximately 7×10^{-4} Pa (5×10^{-3} mTorr) for 24 hr before beginning the UV exposure. Separate sources of VUV and NUV were oriented orthogonal to one another. The sources illuminated the specimens placed on a plate (see Fig. 2) tilted approximately 30° from vertical to receive simultaneous VUV and NUV exposure at levels similar to LEO, see Fig. 3.

The light source for VUV exposure was a 30-W deuterium lamp with a magnesium fluoride end-window, which provided a lower cut-off wavelength of 115 nm. The VUV source was calibrated to determine the exposure intensity using a cesium iodide phototube sensitive in the 115 to 200 nm wavelength band. The VUV source was installed on a vacuum port that can be isolated from the specimen chamber. Every 48 to 72 hr, exposures were briefly interrupted while the VUV source was removed from the facility, cleaned, and re-calibrated, while the specimens remained under vacuum. The VUV source produced light primarily in the 115 to 200 nm wavelength band, but the output also included near ultraviolet wavelength light (up to 400 nm). At wavelengths greater than 200 nm, however, the near ultraviolet output was a small fraction of the Sun's intensity.

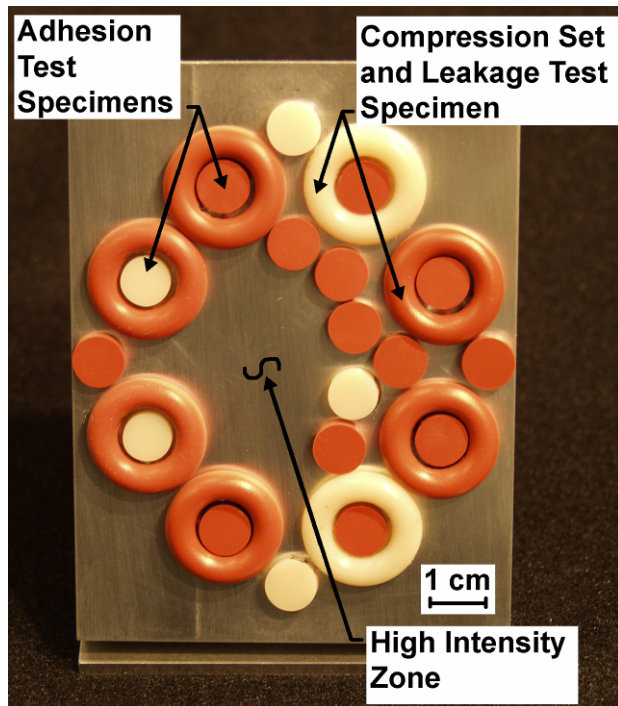


Figure 2.—Photograph of the UV exposure plate with elastomer specimens mounted.

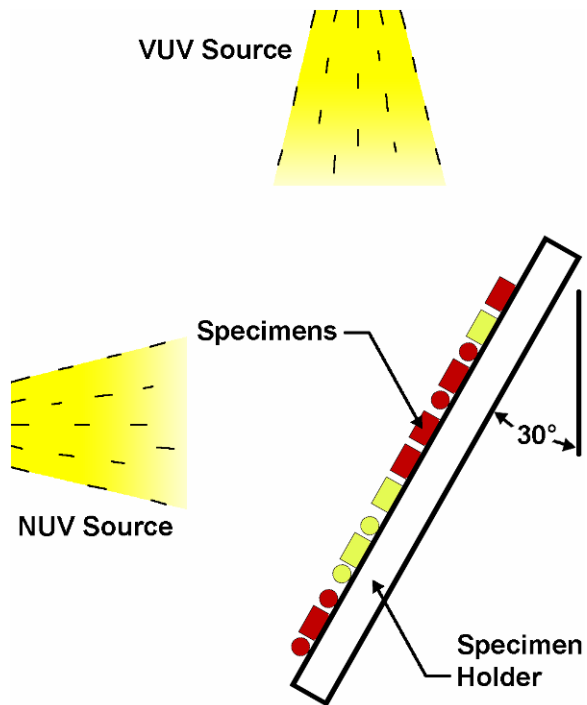


Figure 3.—Graphic depicting the orientation of the specimens in relation to the VUV and NUV light sources.

The light source for NUV exposure was a 500-W mercury (xenon) arc source which provided light in the 220 to 400 nm wavelength range. Since wavelengths above 220 nm transmit through air, the light source was located outside of the vacuum system and was transmitted through a quartz window. This NUV source was calibrated outside the facility before and after each exposure using a pyroelectric detector system and a 260 nm narrow bandpass filter. The manufacturer’s spectral output curve for the NUV source and the 260 nm data were used to calculate the integrated intensity over the 220 to 400 nm wavelength range. Intensity experienced by the specimens was corrected for the transmittance through the quartz window and for the exposure plate angle.

Across the exposure plate, differences in NUV and VUV intensity were known. Specimens were arranged as to avoid areas of highest intensity, as can be seen in Fig. 2. Five separate UV exposures were conducted. For each exposure, the levels of NUV and VUV were not equivalent. By repositioning the specimens on the exposure plate for each test, adjustments were made to the total mean value of UV (average of NUV and VUV) exposure so as to maintain similar mean values for all specimens.

C. Compression Set Tests

The compression set of each elastomer o-ring was tested in accordance with ASTM specifications D395 Method B²³ (for room and elevated temperature properties) and D1229²⁷ (for low temperature properties). A synopsis of the procedures is provided here for completeness.

A segment of the o-ring approximately 0.318 cm (0.125 in.) in length was removed from each of the 2-309 size o-ring specimens. Subsequently, the width and thickness of the specimens were measured according to ASTM D1414.²⁸ The thickness of each o-ring was determined by averaging four thickness measurements per o-ring. The specimens were compressed to a total height of 75% (± 0.03 mm (0.001 in.)) of the average thickness measurement of the o-ring. The specimens remained at a constant displacement stress level at the test temperature for 70 hr. The o-ring specimens were allowed to recover for 30 min before the thickness of each specimen was measured.

$$C_B = \frac{(t_o - t_i)}{(t_o - t_n)} * 100 \quad (2)$$

The compression set, C_B , of each of the o-rings was calculated using the following equation, where t_o was the original specimen thickness, t_i was the final specimen thickness, and t_n was the shim height.

The compression set tests were performed on the three silicone elastomers in the as-received condition at each -50, 23, 50, and 125 °C (-58, 73, 122, and 257 °F). In addition, the compression set of the elastomers was quantified in (1) the as-received condition, (2) following various levels of AO exposure, and (3) after exposure to approximately 6.0×10^{21} atoms/cm² (3.9×10^{22} atoms/in²) of AO and various quantities of UV.

The standard method for measuring compression set of o-rings mandates that the median value of the three replicate samples tested for each case be reported. This study followed those recommendations for tests involving low and elevated temperature. However, this study deviated from that practice in room temperature tests involving specimens exposed to AO and UV by reporting the compression set value for each of the samples tested. The reason for this was that the exposure level of AO and UV was varied for each sample. Therefore, no three samples (from which the median would be computed) were exposed to identical levels of AO and UV.

D. Adhesion Tests

The force required to separate two specimens of similar elastomer compound was determined by compressing two specimens together by 25% of their combined height, holding for a period of time, and then separating them. The dwell periods were 1, 2, 4, 8, 16, and 24 hr in succession using the same specimen pairs.

The elastomer specimen pairs were attached to metallic holders using cyanoacrylate adhesive and allowed to cure for 24 hr before testing. One test specimen and its holder were attached to a stationary load cell. The other specimen and holder were attached to a movable platform, see Fig. 4. A servomotor was used to (1) move the platform to compress the specimens, (2) hold during the dwell period, and (3) move the platform to decompress the specimens. A linear variable displacement transformer (LVDT) was used to measure relative positions of the two elastomers. For all adhesion tests, the rate at which the specimen pairs were compressed together followed a prescribed function of the distance between the two specimen surfaces, see Fig. 5. The compression and decompression strokes were symmetric. In the figure, the dwell period occurs when position equals zero and corresponds to 25% compression of combined specimen height.

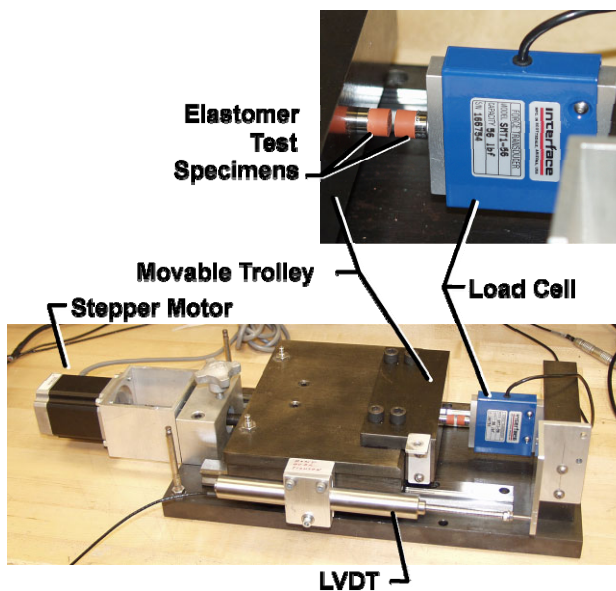


Figure 4.—Photograph of the adhesion test setup.

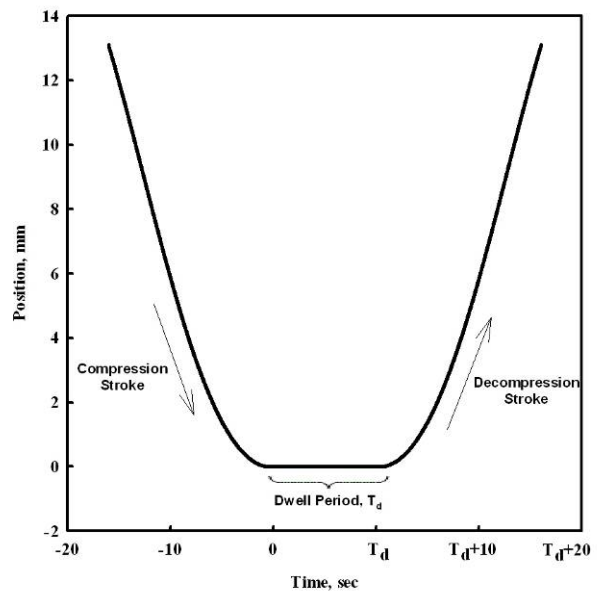


Figure 5.—Graph showing the rate of compression and decompression between two elastomer specimens during an adhesion test.

The load cell was used to quantify the force during the compression, dwell, and decompression periods of the adhesion test. The load cell was calibrated and had an accuracy of 0.01 kg (0.03 lbf). Combined with the nominal 0.89 cm (0.35 in.) diameter of the test specimens, the accuracy of reported elastomer-to-elastomer adhesion stress was approximately $\pm 0.06 \text{ N/m}^2$ (9×10^{-6} psi). The adhesion results are presented in terms of stress (force divided by area) to account for any variation in the diameters of the specimens.

The adhesion between like compound elastomers was quantified at room temperature (1) in the as-received condition, (2) following exposure to various levels of AO, and (3) after exposure to approximately 5.1×10^{21} atoms/cm² (3.3×10^{22} atoms/in.²) of AO and various quantities of UV.

E. Leakage Flow Tests

The leakage rate of the o-ring specimen was quantified using a pressure decay system. The system quantified any mass loss across the o-ring seal specimens, including the amount of dry air that passed through any leakage paths (e.g., through microcracks, between the o-ring to metal interface) and permeated through the specimens' elastomer compound.

The system consisted of a gas reservoir with known volume that was immersed in a water bath to moderate the temperature of the gas within the closed system, see Fig. 6. The temperature of the water was monitored by two resistance temperature detectors (RTDs) with a combined accuracy of $\pm 0.08 \text{ }^\circ\text{C}$ (0.14 $^\circ\text{F}$). Dry air was supplied to the gas reservoir at 101 kPa (14.7 psia). The pressure in the gas reservoir was monitored using a differential pressure transducer. The pressure transducer provided 0.05% full-scale accuracy over a range of 0 to 100 kPa (0 to 15 psid). The gas reservoir was connected to the test section containing the o-ring test specimen, see Fig. 7. External to the o-ring seal specimen, a rough vacuum pressure of approximately 20 Pa (150 mTorr) was applied and monitored by a vacuum pressure transducer with an accuracy of 1.07 Pa (8.03 mTorr).

The pressure decay system quantified the mass of gas within the system with time. To quantify the amount of gas within the system, gas pressure and temperature were monitored. Assuming an ideal gas, the mass loss or leakage rate, \dot{m} , was calculated from the following equation,

$$\dot{m} = \frac{\Delta m}{\Delta t} = \frac{V}{R \cdot \Delta t} \left(\frac{p_1}{T_1} - \frac{p_2}{T_2} \right) \quad (3)$$

where m was the mass of the gas within the leakage quantification system, t was time, V was the closed volume, p was absolute gas pressure, and T was temperature. The subscripts denote two time steps (i.e., the beginning and end of the test). To ensure that the system of the supply lines from the gas reservoir to the test section is hermetic, the system was checked with a helium leak detection system and was found to leak no greater than $10^{-8} \text{ cm}^3/\text{sec}$ ($6.10 \times 10^{-10} \text{ in.}^3/\text{sec}$). Hence, any decrease in the mass of gas within the closed system was attributable to the test specimen leakage. Any leakage of o-rings containing the vacuum pressure did not alter the leakage measurements since the mass loss was calculated based upon the measurements of the closed volume containing the gas reservoir.

An uncertainty analysis was used to produce the error bars shown on the results graphs. The uncertainty analysis of Eq. 3 resulted in Eq. 4, where u represents the uncertainty for the subscripted variable. The uncertainties for each variable within the equation, including calibration error, were estimated and combined using the root-sum-

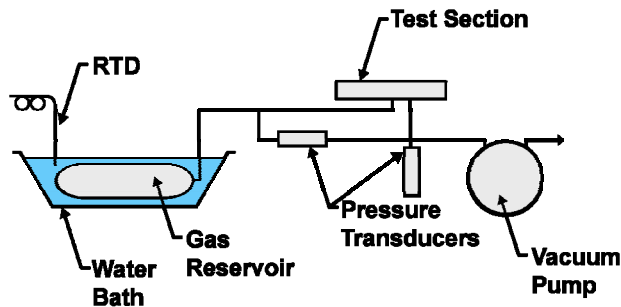


Figure 6.—Schematic of the pressure decay system.

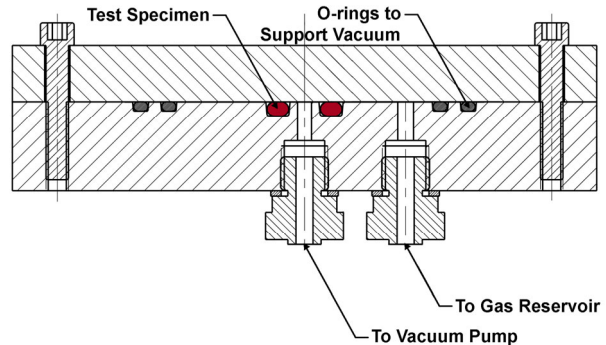


Figure 7.—Schematic of the pressure decay system test section.

square method. The leakage rate uncertainty was computed for each individual specimen trial. Due to the variation in the pressure measurements for each individual trial (and less so for temperature variability), the size of the leakage rate error bars was different for each data point plotted.

$$u_{\dot{m}} = \dot{m} \left\{ \left(\frac{u_V}{V} \right)^2 + 2 \left(\frac{u_p}{p_1 - p_2} \right)^2 + (p_1^2 + p_2^2) \left(\frac{u_T}{T(p_1 - p_2)} \right)^2 \right\}^{1/2} \quad (4)$$

The leakage rates of the silicone elastomer o-rings were quantified at room temperature (1) in the as-received condition, (2) following exposure to various levels of AO, and (3) after exposure to approximately 5.8×10^{21} atoms/cm² (3.7×10^{22} atoms/in.²) of AO and various quantities of UV. The leakage rates after exposure to simulated space environments were meant to act as a method for quantifying the change in leakage rates after periods of various mission lengths.

III. Results and Discussion

A. Compression Set

The compression set of each of the three elastomer compounds was tested in the as-received condition at -50 , 23 , 50 , and 125 °C (-58 , 73 , 122 , and 257 °F). The data for each test is tabularized in Appendix A. Per ASTM standards^{23,27}, the median compression set values of three repeated trials were recorded, see Fig. 8. All of the elastomers exhibited the least amount of compression set at room to moderate temperatures, 23 to 50 °C (73 to 122 °F), as compared with warm, 125 °C (257 °F) and refrigerated temperatures, -50 °C (-58 °F). The results showed that the ELA-SA-401 silicone elastomer compound exhibited the least amount of compression set at each of the temperatures tested and smallest variation between temperatures.

After exposure to AO, the compression set of each individual trial was measured, see Fig. 9. The erosion rates of the Kapton witness specimens varied over the exposure plate, indicating that the AO exposure varied for each specimen. Specimens received various levels of AO fluence ranging from 2.5×10^{21} to 7.6×10^{21} atoms/cm² (1.6×10^{22} to 4.9×10^{22} atoms/in.²). The three elastomer compounds had similar values of compression set. The S0383-70, S0899-50, and ELA-SA-401 compounds exhibited average compression set values of 15.1 , 13.5 , and 15.9% , respectively.

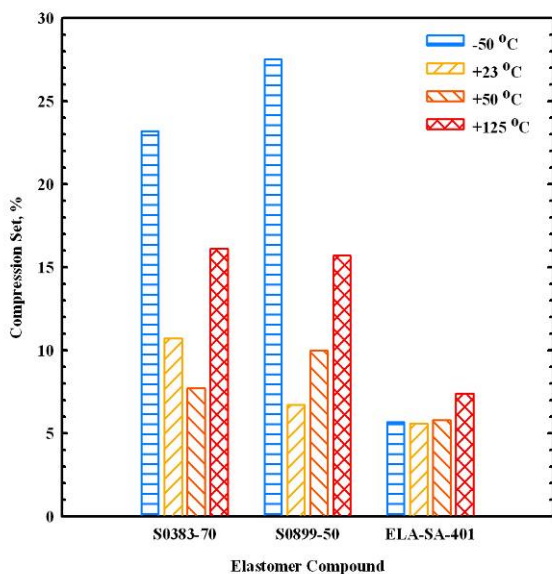


Figure 8.—Graph showing the effect of temperature on the compression set of three silicone elastomer compounds.

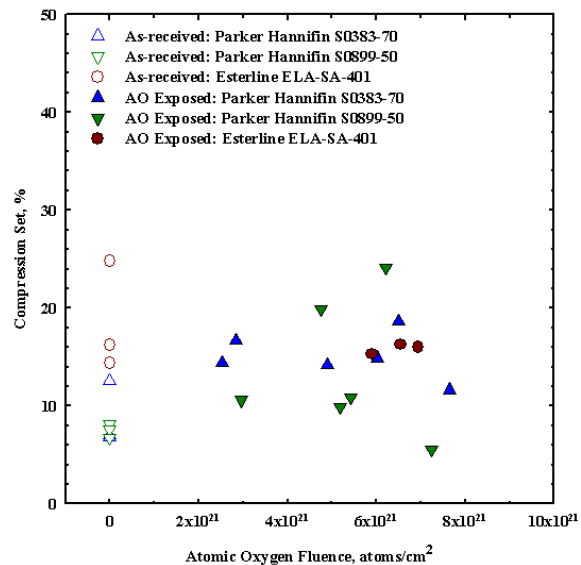


Figure 9.—Graph showing the effect of AO fluence on the compression set of three silicone elastomer compounds.

A discrepancy in results exists between the two sets of compression set data for the ELA-SA-401 material. The investigation into the effect of temperature returned a median compression set value of 5.6% at 23 °C (73 °F), whereas the AO exposure study returned a median compression set value of 16.2% for similar test conditions in the as-received state of the material. The two sets of data were produced from two different batches of material. The tests were conducted at two different locations, using different facilities and instruments. Each location followed the same ASTM standard²³, which mandates a contact type method used to measure the thickness, however, the standard does not prescribe the amount of force to be applied to the sample. As the ELA-SA-401 compound is very soft (38 durometer), small variations in this force will return different thickness measurements. To obtain identical results the measurement device and technique would have to be sensitive enough to apply an exact amount of force, which is not practical. Deviations from the standard, by using a non-contact method would greatly improve the accuracy and repeatability of the thickness measurements.

After exposure to AO and subsequently UV, the compression set for each of the compounds increased in comparison to specimens only exposed to AO, see Fig. 10. The ELA-SA-401 compound had the highest compression set. The S0899-50 and S0383-70 compounds exhibited lower compression set values. After exposure to AO and UV, the S0383-70, S0899-50, and ELA-SA-401 compounds exhibited average compression set values of 17.9, 19.6, and 27.1%, respectively.

Statistical hypothesis analyses²⁹ were performed to determine whether the individual data sets of the three materials were exposed to equivalent levels of (1) AO and (2) AO and UV. The details of the hypothesis analyses are shown in Appendix B. The mean exposure levels of the three material data sets were compared to the sample population mean value to determine if a valid comparison between data sets was permitted. The hypothesis tests confirmed, using a significance level of $\alpha = 0.05$, that the mean exposure values of (1) AO and (2) AO and UV were not statistically different for the three materials. Therefore, comparisons of average compression set values were valid even though the exposure levels were not identical for each data point across the data sets. A summary of (1) the effects of AO and (2) the combined effects of AO and UV on the compression set of 2-309 size o-ring specimens molded from the three silicone elastomer compounds was shown in Fig. 11.

Excluding the discrepancy previously noted for the ELA-SA-401 material, the compression set increased with exposure to AO over the materials in the as-received condition. The increases in average compression set for the exposed S0383-70 and S0899-50 elastomers were 71% and 79% respectively. The average compression set for the exposed ELA-SA-401 decreased 14%. This decrease can be attributed to the difficulty in measuring the compression set for very soft materials, in addition to the general experimental scatter.

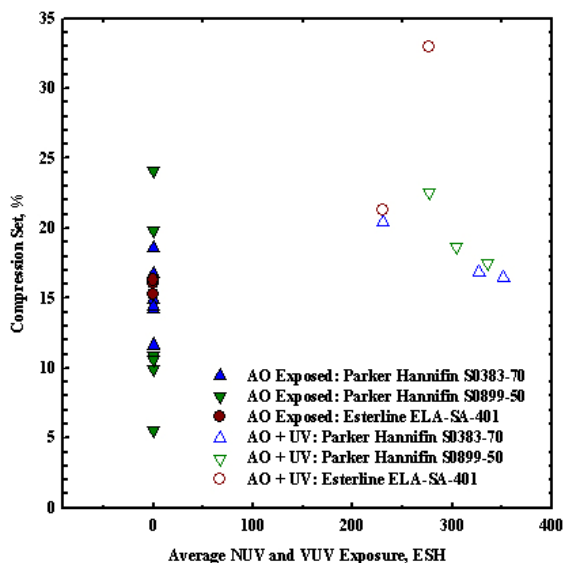


Figure 10.—Graph showing the effect of UV on the compression set of three silicone elastomer compounds previously exposed to AO.

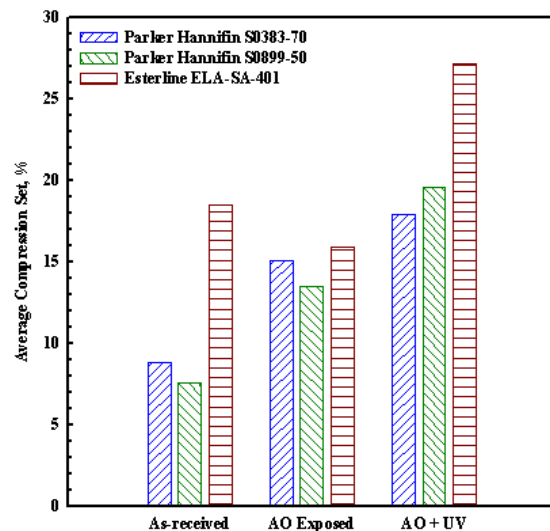


Figure 11.—Summary graph showing the effect of space environments exposures on the compression set of three silicone elastomer compounds.

The exposure to UV further increased the compression set for each of the three materials studied. The average compression set values measured for the S0383-70, S0899-50, and ELA-SA-401 elastomers increased 19%, 45%, and 71% respectively compared with the AO exposed data set. When comparing the specimens exposed to both AO and UV with those in the as-received condition, the average compression set values increased 104%, 161%, and 47% (S0383-70, S0899-50, and ELA-SA-401 respectively) after space environment exposures.

B. Elastomer-to-Elastomer Adhesion

The results of a typical elastomer-to-elastomer adhesion test are shown in Fig. 12. The data for each test is tabularized in Appendix C. The figure shows the compression stroke, dwell period, and decompression stroke for a typical S0383-70 compound test. The stiffness of the material was highest on the first compression cycle, as indicated by the steep portion of the curve during the compression stroke of the 1 hour contact period. The material subsequently softened for each of the next cycles (2, 4, 8, 16, and 24 dwell periods), and no apparent steady-state stiffness was evident. Each of the three elastomers exhibited loss of resiliency during the dwell periods of the tests. This is indicated in the figure by the vertical line of the dwell period. While being held at constant displacement, the resistive load of the elastomer pair decreased. During the decompression stroke of the test, the negative force value indicates that adhesion occurred between the specimen pair. The maximum adhesion values recorded for each of the tests are plotted in the subsequent graphs of this section.

As shown in Fig. 13, the S0899-50 compound had the highest adhesion stresses followed by S0383-70. The ELA-SA-401 exhibited the lowest adhesion stresses. After a 24 hour dwell period, the S0899-50 compound exhibited an average adhesion stress of 564 kPa (81.7 psi) while the corresponding value for the ELA-SA-401 compound was 150 kPa (21.8 psi).

Two competing factors contributed to the noted variation of adhesion with dwell period: (1) the duration of the contact, or dwell period, and (2) the number of contacts. As shown in Fig. 13, the amount of adhesion initially decreases when comparing the first and second periods of contact (1 and 2 hr dwell periods). Since the specimen pairs were repeatedly held in contact, separated, and then held in contact for a longer period, the trend indicates that the adhesion stress is lower for increasing number of contacts. After the third contact (4 hr dwell period), the adhesion values increased indicating that the adhesion stress increases with increased contact duration, as was expected.

Select elastomer-to-elastomer adhesion specimens were exposed to AO as described in section II.B.1. and subsequently evaluated as to determine the effects of the exposure. As shown in Fig. 14, modest amounts of exposure to AO greatly decreased the amount of adhesion recorded. In the case of the ELA-SA-401 material, the

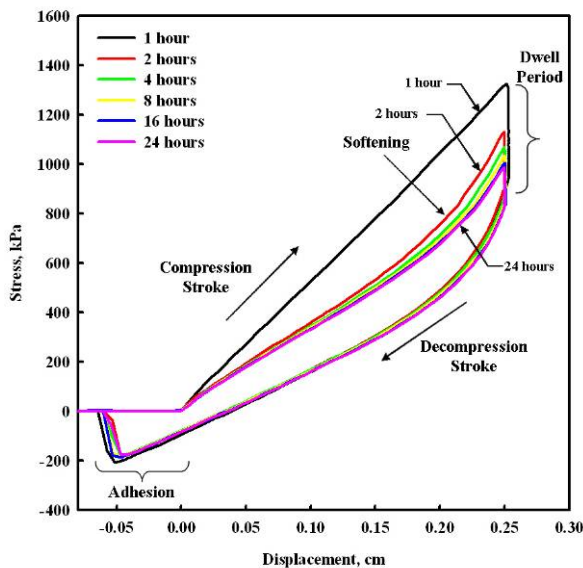


Figure 12.—Graph showing the effect of dwell period on the adhesion force for typical adhesion test.

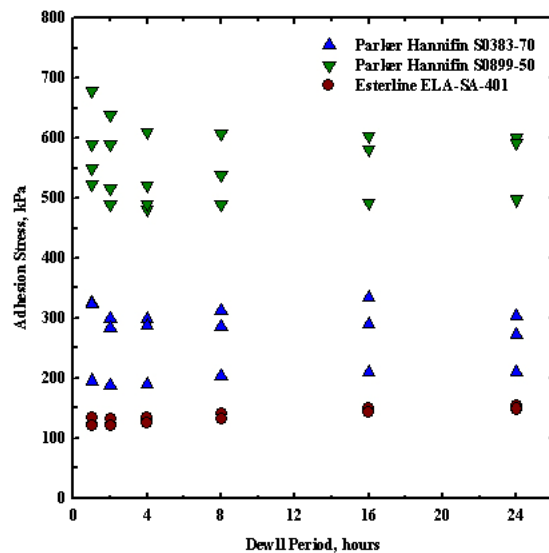


Figure 13.—Graph showing the effect of dwell period on the adhesion force of as-received three silicone elastomer compounds.

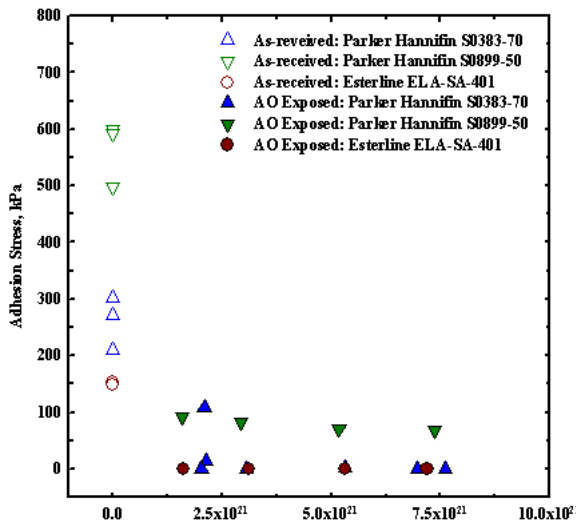


Figure 14.—Graph showing the effect of AO fluence on the elastomer-to-elastomer adhesion of three silicone elastomer compounds after 24 hr dwell period.

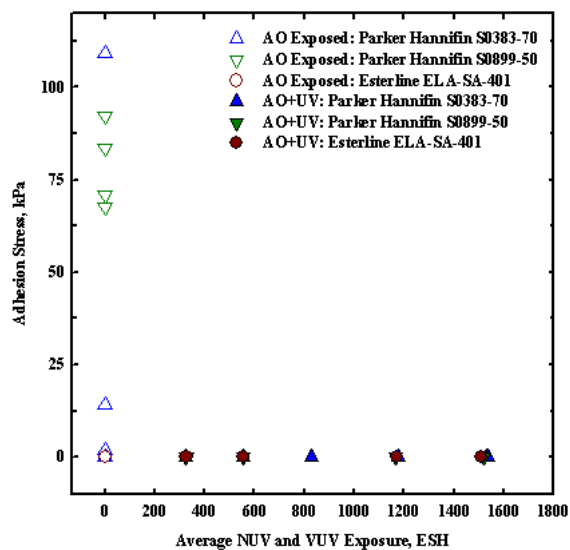


Figure 15.—Graph showing the effect of UV on the elastomer-to-elastomer adhesion after 24 hr dwell period of three silicone elastomer compounds previously exposed to AO.

low levels of adhesion observed prior to AO exposure were reduced to levels below the resolution of the test apparatus's load cell. The high levels of adhesion observed in the S0899-50 material were reduced by more than 80%.

The reduction in adhesion values after exposure to AO was expected. During exposure to AO, the oxygen replaced the methyl groups of the siloxane on the surface of the specimens. The result was a layer of SiO_x, where *x* is between 2 and 4, on the surface of the specimens. Since the SiO_x compounds are glass-like, the coated surface acts to reduce the adhesive nature of the specimens.

Select elastomer-to-elastomer adhesion specimens that were previously exposed to between 5.2×10^{21} and 6.5×10^{21} atoms/cm² (3.4×10^{22} to 4.2×10^{22} atoms/in.²) were exposed to various amount of UV. As shown in Fig. 15, after exposure to UV the elastomer-to-elastomer adhesion was reduced further. All of the elastomer-to-elastomer adhesion measurements were below the resolution of the test apparatus.

C. Leakage Flow

The leakage flow rates of the 2-309 size o-ring test specimens were measured in the as-received, post-atomic oxygen exposure, and post-atomic oxygen and UV exposure conditions. The data for each test is tabularized in Appendix D.

In the as-received condition, the average leakage rates of o-ring specimens molded from the highest durometer material, S0383-70, were the lowest (6.1×10^{-7} kg/day (1.4×10^{-6} lbm/day)), see Fig. 16. The lowest durometer material, ELA-SA-401, exhibited the highest rate of flow, 1.3×10^{-6} kg/day (3.0×10^{-6} lbm/day). These results were expected as high durometer materials have a greater stiffness than low durometer materials and produce a higher reaction force for a given amount of compression. It is the reaction force that minimizes the leakage paths between the specimens and the groove containing the seal, thereby reducing the leakage flow rate.

After exposure to various amounts of AO, the leakage flow rates were measured and plotted as a function of AO fluence, see Fig. 17. For fluence values up to 7.2×10^{21} atoms/cm² (4.6×10^{22} atoms/in.²), the exposure of the specimens to AO slightly increased the leakage flow rate. The average values of leakage flow rate of the S0383-70, S0899-50, and ELA-SA-401 compounds were 1.6×10^{-6} kg/day (3.5×10^{-6} lbm/day), 2.9×10^{-6} kg/day (6.5×10^{-6} lbm/day), and 1.9×10^{-6} kg/day (4.2×10^{-6} lbm/day) respectively.

Two specimens of each of the three compounds that had been previously exposed to AO were selected to be exposed to UV. These previously untested specimens had AO fluence levels ranging from 5.1×10^{21} to 7.3×10^{21} atoms/cm² (3.3×10^{22} to 4.7×10^{22} atoms/in.²). Specimens with similar AO exposure levels, but no exposure

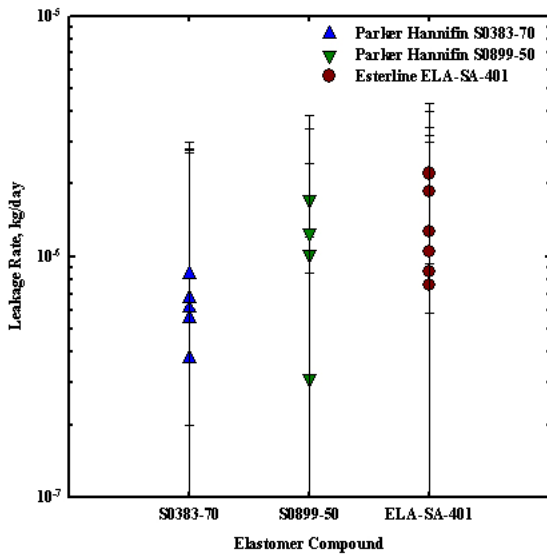


Figure 16.—Graph showing the leakage of 2-309 size o-ring specimens molded from three silicone elastomer compounds in the as-received condition.

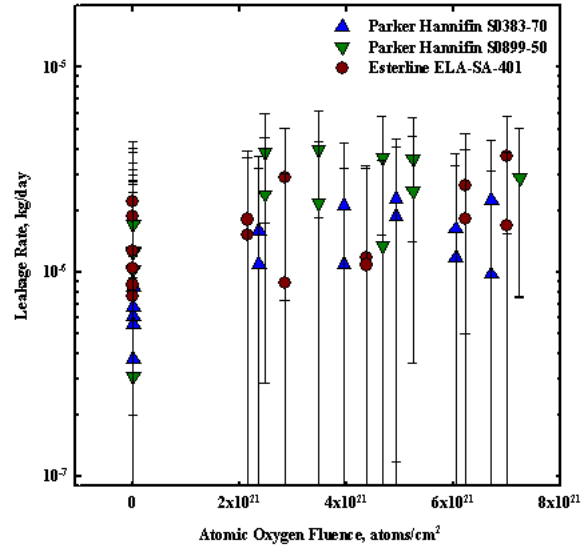


Figure 17.—Graph showing the effect of AO fluence on the leakage flow rate of 2-309 size o-ring specimens molded from three silicone elastomer compounds.

to UV, were shown at UV=0 (Fig. 18) and had leakage rates ranging from 8.9×10^{-7} to 4.0×10^{-6} kg/day (2.0×10^{-6} to 8.8×10^{-6} lbm/day). The previously untested specimens were exposed to approximately 325 ESH of UV before being leakage tested. They were then exposed and leakage tested repeatedly until the total UV exposure was approximately 1500 ESH. The range of leakage rates increased to between 2.0×10^{-5} and 9.0×10^{-4} kg/day (4.4×10^{-5} and 2.0×10^{-3} lbm/day) after approximately 1500 ESH of exposure. The leakage flow rates of each of the three compounds were shown to have increased significantly with increased UV exposure.

The variation in leakage rates between the silicone elastomer compounds was significant. The S0899-50 compound exhibited the greatest amount of degradation to UV exposure. After exposure to 1500 ESH of UV, the average leakage rate increased by a factor greater than 200 to 7.2×10^{-4} kg/day (1.6×10^{-3} lbm/day) when compared to specimens exposed to comparable levels of only AO. Comparing S0899-50 specimens exposed to approximately 1500 ESH of UV with those specimens in the as-received condition, the average leakage rates increased by a factor of greater than 600. The leakage rates for the S0383-70 and ELA-SA-401 compound increased by a factors of approximately 100 and 50, respectively, when compared to specimens exposed to only AO (to an average of 6.0×10^{-5} kg/day (1.3×10^{-4} lbm/day) and 9.8×10^{-5} kg/day (2.2×10^{-4} lbm/day), respectively).

Hypothesis analyses were calculated to ascertain the relevance of comparisons between data sets; the details of these analyses are shown in Appendix E. Using significance level of $\alpha = 0.05$, the average AO fluence levels of the three data sets were not found to be statistically different; therefore the comparison of average leakage rates was appropriate. A summary of the effects of AO on the leakage rates of 2-309 size o-rings specimens molded from the three silicone elastomer compounds is shown in Fig. 19. The exposure to AO modestly increased the leakage flow rate above the as-received averages.

Analogous hypothesis analyses were conducted to determine the similarity of space environments exposure for combined AO and UV exposed specimens. The analyses showed that the AO and UV levels of the S0899-50 and ELA-SA-401 compounds were not statistically different; however, the total amounts of AO exposure and UV exposure to which the S0383-70 specimens were subjected were not statistically equivalent to the sample population mean. The average AO and UV exposures of the S0383-70 specimens were 13% lower and 2% higher, respectively, than the combined average of the S0899-50 and ELA-SA-401 exposure levels. Nevertheless, the leakage results of the S0383-70 were presented due to the similarity of exposure levels, while acknowledging the statistical deviation.

A summary of the effects of AO and the combined effects of AO and UV on the leakage rates of 2-309 size o-rings specimens molded from the three silicone elastomer compounds is shown in Fig. 19. As previously discussed, the exposure to AO modestly increased the leakage rates whereas significant leakage increase was observed with UV exposure. Since the hypothesis test showed that the levels of AO exposure of the two data sets (AO and the combined AO and UV) were similar, the leakage increase between these two data sets can be attributed only to the exposure to UV.

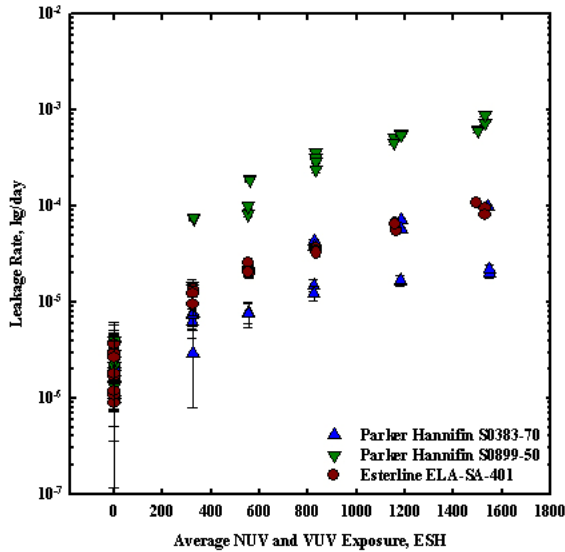


Figure 18.—Graph showing the effect of UV on flow rate of previously AO exposed 2-309 size o-ring specimens molded from three silicone elastomer compounds.

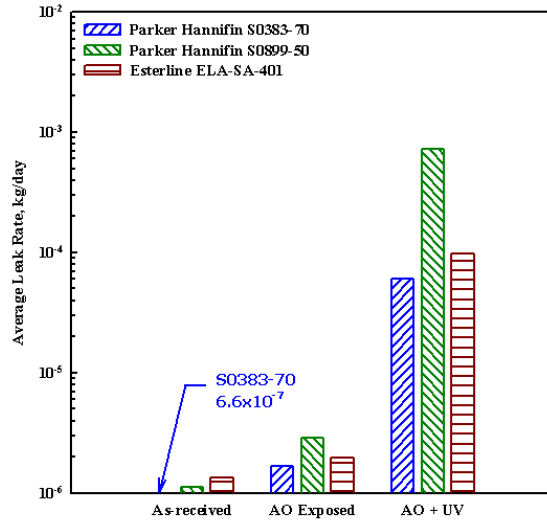


Figure 19.—Summary graph showing the effects of space environments exposures on the leakage flow rate of 2-309 size o-ring specimens molded from three silicone elastomer compounds.

IV. Conclusions

The Low Impact Docking System (LIDS) is being designed to support all future space exploration missions to low-Earth orbit (LEO), to the Moon, and to Mars. The androgynous design of the LIDS requires that the gas seals of each module mate with the other in a seal-on-seal configuration. This unusual configuration of the seals requires an in-depth understanding of the behavior and characteristics of the elastomers that comprise the seals. Since the operating envelope will be mission specific, the effects of space environments must be understood. Select effects of temperature, solar radiation, reactive elements, and mission duration were discussed in this work. The seal characteristics of compression set, elastomer-to-elastomer adhesion, and o-ring leakage rate were investigated before and after exposure to simulated AO and UV space environments.

Based on the tests performed herein, the following observations were made.

- (1) Each of the silicone elastomers compounds investigated, including Parker Hannifin compounds S0383-70 and S0899-50, and Kirkhill-TA ELA-SA-401, was characterized as low outgassing compounds meeting NASA's requirements.
- (2) Each compound exhibited acceptable compression set over the LIDS operating environment of -50 to 50 °C. The ELA-SA-401 compound exhibited the lowest compression set and variability over the operating temperature range.
- (3) Compression set increased for each of the compounds with exposure to AO only, and furthermore with combined AO and UV exposures.
- (4) In the as-received condition the ELA-SA-401 compound exhibited the lowest adhesion. The S0899-50 compound exhibited the highest adhesion. In general, adhesion increased with time held in contact under load.
- (5) Exposure to modest levels of AO lowered the rates of adhesion for all of the compounds. A further decrease was recorded after subsequent UV exposure.
- (6) Whereas the exposure to AO modestly increased the leakage flow rate, the UV exposure had a dramatic effect. Increases in leakage up to 600 times were measured after exposure to approximately 1500 ESH of UV.

These results provide guidance for the applicability of these three silicone elastomer compounds for use in sealing systems exposed to space environments.

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Appendix A Compression Set Data

1. Compression Set Data for Parker Hannifin S0383-70

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-1	S0383-70	0	0	12.54
309-2	S0383-70	0	0	6.85
309-3	S0383-70	0	0	7.00

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-34	S0383-70	6.02E+21	0	14.90
309-35	S0383-70	6.49E+21	0	18.63
309-36	S0383-70	7.64E+21	0	11.65
309-51	S0383-70	4.90E+21	0	14.21
309-100	S0383-70	2.52E+21	0	14.40
309-167	S0383-70	2.84E+21	0	16.72

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-50	S0383-70	6.55E+21	326.7	16.85
309-58	S0383-70	6.02E+21	230.4	20.45
309-59	S0383-70	5.56E+21	351.1	16.44

2. Compression Set Data for Parker Hannifin S0899-50

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-4	S0899-50	0	0	8.20
309-5	S0899-50	0	0	7.62
309-6	S0899-50	0	0	6.75

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-37	S0899-50	6.22E+21	0	24.12
309-38	S0899-50	5.41E+21	0	10.89
309-39	S0899-50	7.25E+21	0	5.56
309-61	S0899-50	5.19E+21	0	9.91
309-170	S0899-50	4.76E+21	0	19.86
309-171	S0899-50	2.96E+21	0	10.62

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-52	S0899-50	6.50E+21	304.2	18.65
309-53	S0899-50	5.42E+21	276.8	22.60
309-54	S0899-50	6.69E+21	335.4	17.53

3. Compression Set Data for Esterline XELA-SA-401

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-7	XELA-SA-401	0	0	14.42
309-8	XELA-SA-401	0	0	16.20
309-9	XELA-SA-401	0	0	24.79

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-40	XELA-SA-401	5.89E+21	0	15.30
309-41	XELA-SA-401	6.94E+21	0	16.02
309-42	XELA-SA-401	6.55E+21	0	16.30

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Compression Set [%]
309-56	XELA-SA-401	5.63E+21	230.4	21.33
309-57	XELA-SA-401	5.77E+21	276.8	32.94

4. Compression Set Data for Compound in the As-Received Condition Tested at Various Temperatures

As-received

ID	Compound	Temperature [deg C]	Compression Set [%]
551-553	S0383-70	-50	23.2
554-556	S0383-70	23	10.7
557-559	S0383-70	50	7.7
560-562	S0383-70	125	16.1
563-565	S0899-50	-50	27.5
566-568	S0899-50	23	6.7
569-571	S0899-50	50	10.0
572-574	S0899-50	125	15.7
575-577	XELA-SA-401	-50	5.7
578-580	XELA-SA-401	23	5.6
581-583	XELA-SA-401	50	5.8
584-586	XELA-SA-401	125	7.4

5. VUV and NUV Components of Average UV Values

Parker Hannifin S0383-70

ID	VUV [ESH]	NUV [ESH]
309-50	294.9	358.5
309-58	177.1	283.7
309-59	451.8	250.4

Parker Hannifin S0899-50

ID	VUV [ESH]	NUV [ESH]
309-52	294.9	358.5
309-53	269.1	284.4
309-54	404.6	266.2

Esterline ELA-SA-401

ID	VUV [ESH]	NUV [ESH]
309-56	177.1	283.7
309-57	269.1	284.4

Appendix B

Hypothesis Testing of Compression Set Data

1. Theory

The authors used hypothesis testing to analyze the compression set data. As each of the specimens were exposed to unique levels of (1) AO and (2) AO and UV, a statistical approach was used to confirm the validity of comparisons of average compression set values across the three materials for each condition. Statistical hypothesis analyses were performed to determine whether the individual data sets of the three materials were exposed to equivalent levels of AO and AO & UV.

The authors assumed that the distribution about the population mean was normally distributed such that the confidence interval could be stated according to equation (C1):

$$\bar{X} \pm t_{\alpha/2} S / \sqrt{n} \quad (C1)$$

where:

- \bar{X} the population mean
- t the student t-value at a specified value of α for t-distribution with $(n-1)$ degrees of freedom
- α the significance level
- S the standard deviation of the sample measurements
- n the sample size

The authors further assumed that the mean of the sample, μ_0 , was contained within the confidence interval. The authors tested this assumption using the hypothesis testing techniques.²⁹ If the resulting confidence interval, $t_{\alpha/2} S / \sqrt{n}$, did not contain μ_0 , then the hypothesis was rejected. If μ_0 was within the confidence interval, then the hypothesis could not be rejected. Therefore, the hypothesized value μ_0 would be rejected if

$$|T| = \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| > t_{\alpha/2} \quad (C2)$$

2. Application

The above theory was used in the analysis of results of small scale compression set results of three candidate elastomers: Parker S0383-70, Parker S08998-50, and XELA-SA-401, denoted 70, 50, and 38, respectively. Each of the materials was tested in three different conditions: (1) as-received, (2) after AO exposure, and (3) subsequent to AO and UV exposures. In conditions (2) and (3) the exposure levels to AO and/or UV were varied for each sample, thereby motivating this hypothesis analysis.

The mean exposure levels of the three material data sets were compared to the sample population mean value using a significance level of $\alpha = 0.05$. The performed calculations, along with explanation of terms are shown below.

Condition (2): AO Exposures

The population mean \bar{X} (the average of AO exposure levels for the three material data sets) was calculated to be 5.44×10^{21} atoms/cm². Using equation (C2) with μ_0 being the average level of AO exposure for each particular material, the analysis was performed as presented along with the corresponding value of t for $\alpha = 0.05$ (95% confidence):

$$\text{AO}_{70}: \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.44 \times 10^{21} - 5.07 \times 10^{21}}{2.05 \times 10^{21} / \sqrt{6}} \right| = 0.443 < t_{\alpha/2} = 3.365$$

$$AO_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.44 \times 10^{21} - 5.30 \times 10^{21}}{1.44 \times 10^{21} / \sqrt{6}} \right| = 0.237 < t_{\alpha/2} = 3.365$$

$$AO_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.44 \times 10^{21} - 6.46 \times 10^{21}}{5.30 \times 10^{20} / \sqrt{3}} \right| = 3.340 < t_{\alpha/2} = 4.303$$

The above calculations confirm that the mean exposure values of AO were not statistically different for the three materials tested in condition (2). This confirms the validity of comparisons of average compression set values for these materials, as shown in Fig. 9.

Condition (3): AO and UV Exposures

The AO population mean was calculated to be $\bar{X}=6.02 \times 10^{21}$ atoms/cm², while the UV population mean was $\bar{X}=291.5$ ESH. Similarly as in condition (2) calculations, equation (C2) was used for analysis of average AO and average UV exposures.

$$AO_{70}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{6.02 \times 10^{21} - 6.04 \times 10^{21}}{4.96 \times 10^{20} / \sqrt{3}} \right| = 0.087 < t_{\alpha/2} = 4.303$$

$$AO_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{6.02 \times 10^{21} - 6.20 \times 10^{21}}{6.85 \times 10^{20} / \sqrt{3}} \right| = 0.473 < t_{\alpha/2} = 4.303$$

$$AO_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{6.02 \times 10^{21} - 5.70 \times 10^{21}}{1.03 \times 10^{20} / \sqrt{2}} \right| = 4.345 < t_{\alpha/2} = 12.706$$

$$UV_{70}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{291.5 - 302.7}{63.8 / \sqrt{3}} \right| = 0.306 < t_{\alpha/2} = 4.303$$

$$UV_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{291.5 - 305.5}{29.3 / \sqrt{3}} \right| = 0.826 < t_{\alpha/2} = 4.303$$

$$UV_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{291.5 - 253.6}{32.8 / \sqrt{2}} \right| = 0.1.635 < t_{\alpha/2} = 12.706$$

The above calculations confirm that the mean exposure values of UV were not statistically different for the three materials tested in condition (3). Similarly, the analyses have shown that the AO levels of the three compounds were not statistically different.

Combined Conditions (2) and (3)

In order to quantify the overall effect of space environment exposure (both AO and AO with UV) on the three candidate compounds, confirmation that the individual data sets of the materials in conditions (2) and (3) were exposed to statistically equivalent levels of AO was required. The mean AO exposure levels of the three material data sets in the two conditions were compared to the sample population mean value using a significance level of $\alpha = 0.05$. The AO population mean was calculated to be $\bar{X}=5.64 \times 10^{21}$ atoms/cm². Application of equation (C2) leads to the following calculations and results:

$$AO_{70} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 5.07 \times 10^{21}}{2.05 \times 10^{21} / \sqrt{6}} \right| = 0.683 < t_{\alpha/2} = 3.365$$

$$\text{AO}_{50} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 5.30 \times 10^{21}}{1.44 \times 10^{21} / \sqrt{6}} \right| = 0.577 < t_{\alpha/2} = 3.365$$

$$\text{AO}_{38} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 6.46 \times 10^{21}}{5.30 \times 10^{20} / \sqrt{3}} \right| = 2.683 < t_{\alpha/2} = 4.303$$

$$\text{AO}_{70} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 6.04 \times 10^{21}}{4.96 \times 10^{20} / \sqrt{3}} \right| = 1.402 < t_{\alpha/2} = 4.303$$

$$\text{AO}_{50} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 6.20 \times 10^{21}}{6.85 \times 10^{20} / \sqrt{3}} \right| = 1.425 < t_{\alpha/2} = 4.303$$

$$\text{AO}_{38} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.64 \times 10^{21} - 5.70 \times 10^{21}}{1.03 \times 10^{20} / \sqrt{2}} \right| = 0.810 < t_{\alpha/2} = 12.706$$

Based on the above analysis, the mean levels of AO exposure among the specimens tested in conditions (2) and (3) were not statistically different, with a confidence level of 95%. Therefore, the change in average compression set values between conditions (2) and (3) can be solely attributed to UV exposure effects only (Figs. 10 and 11), since the average AO levels have been shown to be not statistically different.

Appendix C

Elastomer-to-Elastomer Adhesion Data

1. Elastomer-to-Elastomer Adhesion Data for Parker Hannifin S0383-70

As-Received

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		[ESH]		3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2	ID #1	ID #2						
B-16	B-17	S0383-70	0	0	0	0	28.37	27.36	27.7	29.37	30.37	30.37
B-18	B-19	S0383-70	0	0	0	0	47.32	43.29	43.29	45.3	48.66	43.96
B-20	B-21	S0383-70	0	0	0	0	46.85	41.08	40.74	41.42	42.1	39.38

AO Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		[ESH]		3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2	ID #1	ID #2						
B-64	B-85	S0383-70	6.71E+21	7.23E+21	0	0	0	0	0	0	0	0
B-68	B-87	S0383-70	7.59E+21	7.64E+21	0	0	0	0	0	0	0	0
B-84	B-187	S0383-70	5.29E+21	5.36E+21	0	0	0	0	0	0	0	0
B-130	B-131	S0383-70	1.50E+21	1.66E+21	0	0	0.33	0.67	0.67	1.33	1.99	2.99
B-181	B-184	S0383-70	3.06E+21	3.05E+21	0	0	0	0	0	0	0	0
B-124	B-125	S0383-70	1.74E+21	2.45E+21	0	0	13.77	14.81	14.46	15.15	15.5	15.84
B-126	B-127	S0383-70	2.51E+21	1.75E+21	0	0	0.34	0.34	0.34	0.67	1.01	2.03
B-123	B-129	S0383-70	1.75E+21	2.30E+21	0	0	0.69	1.03	1.03	0.34	0.34	0

AO + UV Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		[ESH]		3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2	ID #1	ID #2						
B-65	B-69	S0383-70	6.02E+21	5.56E+21	324.3	325.0	-	0	0	0	0	0
B-66	B-83	S0383-70	6.02E+21	6.04E+21	558.9	552.6	0	0	0	0	0	0
B-65	B-69	S0383-70	6.02E+21	5.56E+21	1181.7	1168.7	0	0	0	0	0	0
B-66	B-83	S0383-70	6.02E+21	6.04E+21	1532.9	1531.4	0	0	0	0	0	0
B-65	B-69	S0383-70	6.02E+21	5.56E+21	1533.7	1535.5	0	0	0	0	0	0

2. Elastomer-to-Elastomer Adhesion Data for Parker Hannifin S0899-50

As-Received

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-22	B-23	S08989-50	0	0	0	0	75.86	71.15	71.15	71.15	71.49	72.17
B-24	B-25	S08989-50	0	0	0	0	98.5	92.64	88.5	88.15	87.47	87.13
B-26	B-27	S08989-50	0	0	0	0	79.71	74.83	75.48	78.08	84.27	85.89

AO Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-88	B-91	S08989-50	7.26E+21	7.45E+21	0	0	7.36	6.40	8.64	8.96	10.24	9.6
B-90	B-93	S08989-50	5.17E+21	5.19E+21	0	0	6.70	7.02	2.56	9.58	8.94	9.89
B-144	B-145	S08989-50	1.60E+21	1.57E+21	0	0	11.94	11.62	10.97	12.59	13.23	12.91
B-197	B-198	S08989-50	2.96E+21	2.91E+21	0	0	10.52	10.52	10.84	11.16	12.12	12.12

AO + UV Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-70	B-71	S08989-50	6.22E+21	6.50E+21	325.5	325.5	-	0	0	0	0	0
B-73	B-75	S08989-50	5.41E+21	5.23E+21	558.3	553.4	0	0	0	0	0	0
B-70	B-71	S08989-50	6.22E+21	6.50E+21	1174.1	1159.6	0	0	0	0	0	0
B-70	B-71	S08989-50	6.22E+21	6.50E+21	1519.4	1519.0	0	0	0	0	0	0

3. Elastomer-to-Elastomer Adhesion Data for Esterline XELA-SA-401

As-Received

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-28	B-29	XELA-SA-401	0	0	0	0	17.95	17.95	18.73	20.29	21.46	21.46
B-30	B-30	XELA-SA-401	0	0	0	0	19.39	19.02	19.39	20.51	21.63	22.37
B-32	B-33	XELA-SA-401	0	0	0	0	17.5	17.5	18.18	19.19	20.87	21.54

AO Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-94	B-96	XELA-SA-401	7.01E+21	7.39E+21	0	0	0	0	0	0	0	0
B-153	B-159	XELA-SA-401	1.71E+21	1.51E+21	0	0	0	0	0	0	0	0
B-208	B-209	XELA-SA-401	5.26E+21	5.37E+21	0	0	0	0	0	0	0	0
B-206	B-213	XELA-SA-401	3.12E+21	3.09E+21	0	0	0	0	0.3	0.3	0.61	0.91

AO + UV Exposure

ID #1	ID #2	Compound	AO Fluence		Average UV Exposure [ESH]		Max Adhesion Stress [psi] at Time [s]					
			[atoms/cm ²]		ID #1	ID #2	3600s	7200s	14400s	28800s	57600s	86400s
			ID #1	ID #2								
B-76	B-98	XELA-SA-401	5.89E+21	5.77E+21	326.1	326.7	-	0	0	0	0	0
B-80	B-99	XELA-SA-401	6.22E+21	6.03E+21	558.3	553.4	0	0	0	0	0	0
B-76	B-98	XELA-SA-401	5.89E+21	5.77E+21	1178.3	1165.0	0	0	0	0	0	0
B-76	B-98	XELA-SA-401	5.89E+21	5.77E+21	1537.0	1481.6	0	0	0	0	0	0

4. VUV and NUV Components of Average UV Values

Parker Hannifin S0383-70

B-65			B-69		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
267.0	381.5	324.3	275.0	375.0	325.0
177.1	283.7	554.7	171.7	288.9	555.3
223.9	313.9	823.6	275.9	280.0	833.3
474.6	241.6	1181.7	404.6	266.2	1168.7
405.3	298.8	1533.7	455.0	278.6	1535.5

B-66			B-83		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
321.5	336.5	329.0	240.4	403.5	322.0
140.3	319.4	558.9	195.1	266.2	552.6
269.1	284.4	835.6	240.9	302.8	824.4
432.8	257.7	1180.9	404.6	266.2	1159.8
405.3	298.8	1532.9	471.2	271.9	1531.4

Parker Hannifin S0899-50

B-70			B-71		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
281.0	370.0	325.5	281.0	370.0	325.5
181.4	279.3	555.9	167.7	293.8	556.3
213.7	320.5	823.0	286.1	273.4	836.0
451.8	250.4	1174.1	370.8	276.5	1159.6
382.7	308.0	1519.4	430.2	288.6	1519.0

B-73			B-75		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
311.6	344.7	328.2	250.4	395.3	322.9
147.3	312.9	558.3	188.4	272.8	553.4
261.1	289.7	833.7	240.9	302.8	825.3
420.7	261.4	1174.7	488.3	236.3	1187.6
427.8	289.6	1533.4	355.6	319.0	1524.9

Esterline ELA-SA-401

B-76			B-98		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
287.0	365.1	326.1	294.9	358.5	326.7
163.7	296.7	556.3	158.3	301.9	556.8
269.1	284.4	833.0	296.3	266.7	838.3
432.8	257.7	1178.3	350.5	282.6	1154.9
427.8	289.6	1537.0	414.9	294.8	1509.7

B-80			B-99		
VUV [ESH]	NUV [ESH]	Avg. UV [ESH]	VUV [ESH]	NUV [ESH]	Avg. UV [ESH]
311.6	344.7	328.2	250.4	395.3	322.9
147.3	312.9	558.3	188.4	272.8	553.4
255.0	293.6	832.6	270.6	283.4	830.5
440.9	254.6	1180.3	453.8	249.6	1182.2
395.6	302.7	1529.5			

Appendix D Leakage Flow Data

1. Leakage Flow Data for Parker Hannifin S0383-70

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
309-10	S0383-70	0.00E+00	0.0	8.32E-07	1.23E-06	4.39E-07	3.77E-07	5.58E-07	1.99E-07
309-10	S0383-70	0.00E+00	0.0	1.34E-06	6.07E-06	1.00E-20	6.08E-07	2.75E-06	4.54E-21
309-10	S0383-70	0.00E+00	0.0	1.48E-06	6.21E-06	1.00E-20	6.72E-07	2.82E-06	4.54E-21
309-11	S0383-70	0.00E+00	0.0	1.22E-06	5.95E-06	1.00E-20	5.52E-07	2.70E-06	4.54E-21
309-11	S0383-70	0.00E+00	0.0	1.87E-06	6.58E-06	1.00E-20	8.46E-07	2.98E-06	4.54E-21

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
101	S0383-70	2.35E+21	0.0	2.42E-06	7.13E-06	1.00E-20	1.10E-06	3.23E-06	4.54E-21
101	S0383-70	2.35E+21	0.0	3.48E-06	8.17E-06	1.00E-20	1.58E-06	3.71E-06	4.54E-21
163	S0383-70	3.95E+21	0.0	2.42E-06	7.13E-06	1.00E-20	1.10E-06	3.23E-06	4.54E-21
163	S0383-70	3.95E+21	0.0	4.66E-06	9.41E-06	1.00E-20	2.12E-06	4.27E-06	4.54E-21
43	S0383-70	6.04E+21	0.0	2.58E-06	7.32E-06	1.00E-20	1.17E-06	3.32E-06	4.54E-21
43	S0383-70	6.04E+21	0.0	3.58E-06	8.31E-06	1.00E-20	1.63E-06	3.77E-06	4.54E-21
44	S0383-70	4.93E+21	0.0	4.15E-06	8.97E-06	1.00E-20	1.88E-06	4.07E-06	4.54E-21
44	S0383-70	4.93E+21	0.0	5.04E-06	9.81E-06	2.60E-07	2.28E-06	4.45E-06	1.18E-07
49	S0383-70	6.71E+21	0.0	2.15E-06	6.85E-06	1.00E-20	9.76E-07	3.11E-06	4.54E-21
49	S0383-70	6.71E+21	0.0	4.92E-06	9.65E-06	1.81E-07	2.23E-06	4.38E-06	8.21E-08

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
164	S0383-70	5.11E+21	324.3	6.53E-06	1.13E-05	1.77E-06	2.96E-06	5.13E-06	8.03E-07
164	S0383-70	5.11E+21	324.3	1.71E-05	2.18E-05	1.23E-05	7.75E-06	9.89E-06	5.58E-06
164	S0383-70	5.11E+21	554.4	1.76E-05	2.22E-05	1.30E-05	7.99E-06	1.01E-05	5.90E-06
164	S0383-70	5.11E+21	554.4	1.68E-05	2.15E-05	1.21E-05	7.61E-06	9.75E-06	5.49E-06
164	S0383-70	5.11E+21	823.3	3.29E-05	3.75E-05	2.82E-05	1.49E-05	1.70E-05	1.28E-05
164	S0383-70	5.11E+21	823.3	2.75E-05	3.22E-05	2.28E-05	1.25E-05	1.46E-05	1.03E-05
164	S0383-70	5.11E+21	1181.4	3.69E-05	4.15E-05	3.23E-05	1.67E-05	1.88E-05	1.47E-05
164	S0383-70	5.11E+21	1181.4	3.76E-05	4.23E-05	3.30E-05	1.71E-05	1.92E-05	1.50E-05
164	S0383-70	5.11E+21	1548.2	4.40E-05	4.87E-05	3.94E-05	2.00E-05	2.21E-05	1.79E-05
164	S0383-70	5.11E+21	1548.2	4.88E-05	5.34E-05	4.41E-05	2.21E-05	2.42E-05	2.00E-05
165	S0383-70	5.36E+21	322.9	1.40E-05	1.87E-05	9.24E-06	6.34E-06	8.48E-06	4.19E-06
165	S0383-70	5.36E+21	322.9	1.65E-05	2.12E-05	1.17E-05	7.47E-06	9.62E-06	5.31E-06
165	S0383-70	5.36E+21	553.0	5.57E-05	6.03E-05	5.11E-05	2.53E-05	2.74E-05	2.32E-05
165	S0383-70	5.36E+21	553.0	5.30E-05	5.78E-05	4.83E-05	2.41E-05	2.62E-05	2.19E-05
165	S0383-70	5.36E+21	824.8	9.56E-05	1.00E-04	9.09E-05	4.34E-05	4.54E-05	4.12E-05
165	S0383-70	5.36E+21	824.8	8.28E-05	8.75E-05	7.81E-05	3.76E-05	3.97E-05	3.54E-05
165	S0383-70	5.36E+21	1182.9	1.57E-04	1.64E-04	1.50E-04	7.12E-05	7.44E-05	6.80E-05
165	S0383-70	5.36E+21	1182.9	1.27E-04	1.32E-04	1.22E-04	5.75E-05	5.99E-05	5.53E-05
165	S0383-70	5.36E+21	1541.6	2.18E-04	2.27E-04	2.09E-04	9.89E-05	1.03E-04	9.48E-05
165	S0383-70	5.36E+21	1541.6	2.16E-04	2.25E-04	2.07E-04	9.80E-05	1.02E-04	9.39E-05

2. Leakage Flow Data for Parker Hannifin S899-50

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
309-12	S0899-50	0.00E+00	0.0	6.84E-07	5.39E-06	1.00E-20	3.10E-07	2.44E-06	4.54E-21
309-12	S0899-50	0.00E+00	0.0	2.26E-06	2.65E-06	1.87E-06	1.03E-06	1.20E-06	8.48E-07
309-12	S0899-50	0.00E+00	0.0	3.79E-06	8.53E-06	1.00E-20	1.72E-06	3.87E-06	4.54E-21
309-13	S0899-50	0.00E+00	0.0	2.77E-06	7.50E-06	1.00E-20	1.25E-06	3.40E-06	4.54E-21
309-13	S0899-50	0.00E+00	0.0	2.78E-06	7.50E-06	1.00E-20	1.26E-06	3.40E-06	4.54E-21

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
108	S0899-50	2.47E+21	0.0	5.29E-06	9.95E-06	6.31E-07	2.40E-06	4.51E-06	2.86E-07
108	S0899-50	2.47E+21	0.0	8.54E-06	1.32E-05	3.86E-06	3.87E-06	5.99E-06	1.75E-06
168	S0899-50	4.66E+21	0.0	2.98E-06	7.70E-06	1.00E-20	1.35E-06	3.49E-06	4.54E-21
168	S0899-50	4.66E+21	0.0	8.04E-06	1.27E-05	3.33E-06	3.64E-06	5.76E-06	1.51E-06
172	S0899-50	3.47E+21	0.0	4.84E-06	9.57E-06	1.00E-07	2.19E-06	4.34E-06	4.54E-08
172	S0899-50	3.47E+21	0.0	8.76E-06	1.35E-05	4.04E-06	3.97E-06	6.12E-06	1.83E-06
45	S0899-50	7.23E+21	0.0	6.39E-06	1.11E-05	1.65E-06	2.90E-06	5.03E-06	7.48E-07
45	S0899-50	7.23E+21	0.0	6.41E-06	1.11E-05	1.69E-06	2.91E-06	5.03E-06	7.67E-07
46	S0899-50	5.23E+21	0.0	5.49E-06	1.02E-05	7.99E-07	2.49E-06	4.63E-06	3.62E-07
46	S0899-50	5.23E+21	0.0	7.85E-06	1.26E-05	3.12E-06	3.56E-06	5.72E-06	1.42E-06

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate (kg/day)	Upper Error Limit (kg/day)	Lower Error Limit (kg/day)
60	S0899-50	7.26E+21	328.2	1.61E-04	1.68E-04	1.55E-04	7.31E-05	7.62E-05	7.03E-05
60	S0899-50	7.26E+21	328.2	1.67E-04	1.74E-04	1.60E-04	7.58E-05	7.89E-05	7.26E-05
60	S0899-50	7.26E+21	558.7	4.27E-04	4.45E-04	4.08E-04	1.94E-04	2.02E-04	1.85E-04
60	S0899-50	7.26E+21	558.7	4.06E-04	4.23E-04	3.88E-04	1.84E-04	1.92E-04	1.76E-04
60	S0899-50	7.26E+21	830.6	8.02E-04	8.37E-04	7.67E-04	3.64E-04	3.80E-04	3.48E-04
60	S0899-50	7.26E+21	830.6	7.11E-04	7.42E-04	6.80E-04	3.22E-04	3.37E-04	3.08E-04
60	S0899-50	7.26E+21	1154.2	1.12E-03	1.17E-03	1.08E-03	5.10E-04	5.31E-04	4.90E-04
60	S0899-50	7.26E+21	1154.2	1.00E-03	1.04E-03	9.58E-04	4.54E-04	4.72E-04	4.35E-04
60	S0899-50	7.26E+21	1499.6	1.41E-03	1.47E-03	1.35E-03	6.38E-04	6.67E-04	6.12E-04
60	S0899-50	7.26E+21	1499.6	1.36E-03	1.41E-03	1.30E-03	6.15E-04	6.40E-04	5.90E-04
169	S0899-50	5.49E+21	322.9	3.25E-05	3.73E-05	2.77E-05	1.47E-05	1.69E-05	1.26E-05
169	S0899-50	5.49E+21	322.9	3.07E-05	3.55E-05	2.59E-05	1.39E-05	1.61E-05	1.17E-05
169	S0899-50	5.49E+21	553.0	1.81E-04	1.89E-04	1.73E-04	8.23E-05	8.57E-05	7.85E-05
169	S0899-50	5.49E+21	553.0	2.20E-04	2.29E-04	2.10E-04	9.96E-05	1.04E-04	9.53E-05
169	S0899-50	5.49E+21	832.7	6.39E-04	6.67E-04	6.11E-04	2.90E-04	3.03E-04	2.77E-04
169	S0899-50	5.49E+21	832.7	5.22E-04	5.45E-04	4.99E-04	2.37E-04	2.47E-04	2.26E-04
169	S0899-50	5.49E+21	1183.8	1.26E-03	1.32E-03	1.21E-03	5.73E-04	5.99E-04	5.49E-04
169	S0899-50	5.49E+21	1183.8	1.23E-03	1.28E-03	1.17E-03	5.56E-04	5.81E-04	5.31E-04
169	S0899-50	5.49E+21	1529.1	1.60E-03	1.68E-03	1.53E-03	7.28E-04	7.62E-04	6.94E-04
169	S0899-50	5.49E+21	1529.1	1.99E-03	2.10E-03	1.88E-03	9.04E-04	9.53E-04	8.53E-04

3. Leakage Flow Data for Esterline ELA-SA-401

As-received

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate [kg/day]	Upper Error Limit [kg/day]	Lower Error Limit [kg/day]
309-14	ELA-SA-401	0.00E+00	0.0	1.68E-06	2.07E-06	1.29E-06	7.61E-07	9.39E-07	5.85E-07
309-14	ELA-SA-401	0.00E+00	0.0	1.91E-06	6.62E-06	1.00E-20	8.65E-07	3.00E-06	4.54E-21
309-14	ELA-SA-401	0.00E+00	0.0	4.11E-06	8.83E-06	1.00E-20	1.86E-06	4.01E-06	4.54E-21
309-14	ELA-SA-401	0.00E+00	0.0	4.88E-06	9.59E-06	1.64E-07	2.21E-06	4.35E-06	7.44E-08
309-15	ELA-SA-401	0.00E+00	0.0	2.30E-06	7.01E-06	1.00E-20	1.04E-06	3.18E-06	4.54E-21

AO Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate [kg/day]	Upper Error Limit [kg/day]	Lower Error Limit [kg/day]
115	ELA-SA-401	2.14E+21	0.0	3.33E-06	8.00E-06	1.00E-20	1.51E-06	3.63E-06	4.54E-21
115	ELA-SA-401	2.14E+21	0.0	3.98E-06	8.64E-06	1.00E-20	1.81E-06	3.92E-06	4.54E-21
173	ELA-SA-401	2.84E+21	0.0	1.96E-06	6.71E-06	1.00E-20	8.88E-07	3.04E-06	4.54E-21
173	ELA-SA-401	2.84E+21	0.0	6.36E-06	1.11E-05	1.60E-06	2.89E-06	5.03E-06	7.26E-07
174	ELA-SA-401	4.36E+21	0.0	2.39E-06	7.13E-06	1.00E-20	1.08E-06	3.23E-06	4.54E-21
174	ELA-SA-401	4.36E+21	0.0	2.61E-06	7.33E-06	1.00E-20	1.18E-06	3.32E-06	4.54E-21
47	ELA-SA-401	7.01E+21	0.0	3.71E-06	8.44E-06	1.00E-20	1.68E-06	3.83E-06	4.54E-21
47	ELA-SA-401	7.01E+21	0.0	8.12E-06	1.28E-05	3.40E-06	3.68E-06	5.81E-06	1.54E-06
48	ELA-SA-401	6.22E+21	0.0	3.99E-06	8.72E-06	1.00E-20	1.81E-06	3.96E-06	4.54E-21
48	ELA-SA-401	6.22E+21	0.0	5.81E-06	1.05E-05	1.11E-06	2.63E-06	4.76E-06	5.03E-07

AO + UV Exposure

ID	Compound	AO Fluence [atoms/cm ²]	Average UV Exposure [ESH]	Leakage Rate [lbm/day]	Upper Error Limit [lbm/day]	Lower Error Limit [lbm/day]	Leakage Rate [kg/day]	Upper Error Limit [kg/day]	Lower Error Limit [kg/day]
63	ELA-SA-401	6.03E+21	328.2	2.99E-05	3.47E-05	2.52E-05	1.36E-05	1.57E-05	1.14E-05
63	ELA-SA-401	6.03E+21	328.2	3.01E-05	3.48E-05	2.53E-05	1.36E-05	1.58E-05	1.15E-05
63	ELA-SA-401	6.03E+21	558.3	4.52E-05	4.99E-05	4.05E-05	2.05E-05	2.26E-05	1.84E-05
63	ELA-SA-401	6.03E+21	558.3	4.40E-05	4.87E-05	3.92E-05	2.00E-05	2.21E-05	1.78E-05
63	ELA-SA-401	6.03E+21	827.2	8.07E-05	8.54E-05	7.61E-05	3.66E-05	3.87E-05	3.45E-05
63	ELA-SA-401	6.03E+21	827.2	7.65E-05	8.12E-05	7.18E-05	3.47E-05	3.68E-05	3.26E-05
63	ELA-SA-401	6.03E+21	1162.6	1.25E-04	1.30E-04	1.20E-04	5.66E-05	5.90E-05	5.44E-05
63	ELA-SA-401	6.03E+21	1162.6	1.23E-04	1.28E-04	1.17E-04	5.56E-05	5.81E-05	5.31E-05
63	ELA-SA-401	6.03E+21	1529.4	2.12E-04	2.21E-04	2.03E-04	9.60E-05	1.00E-04	9.21E-05
63	ELA-SA-401	6.03E+21	1529.4	1.80E-04	1.88E-04	1.72E-04	8.16E-05	8.53E-05	7.80E-05
175	ELA-SA-401	5.37E+21	324.3	2.73E-05	3.21E-05	2.26E-05	1.24E-05	1.46E-05	1.03E-05
175	ELA-SA-401	5.37E+21	324.3	2.07E-05	2.54E-05	1.60E-05	9.38E-06	1.15E-05	7.26E-06
175	ELA-SA-401	5.37E+21	554.8	5.68E-05	6.14E-05	5.22E-05	2.58E-05	2.79E-05	2.37E-05
175	ELA-SA-401	5.37E+21	554.8	4.50E-05	4.97E-05	4.02E-05	2.04E-05	2.25E-05	1.82E-05
175	ELA-SA-401	5.37E+21	834.6	7.96E-05	8.43E-05	7.49E-05	3.61E-05	3.82E-05	3.40E-05
175	ELA-SA-401	5.37E+21	834.6	7.51E-05	7.97E-05	7.04E-05	3.40E-05	3.62E-05	3.19E-05
175	ELA-SA-401	5.37E+21	834.6	7.19E-05	7.66E-05	6.72E-05	3.26E-05	3.47E-05	3.05E-05
175	ELA-SA-401	5.37E+21	1158.2	1.46E-04	1.52E-04	1.39E-04	6.60E-05	6.89E-05	6.30E-05
175	ELA-SA-401	5.37E+21	1158.2	1.41E-04	1.47E-04	1.35E-04	6.41E-05	6.67E-05	6.12E-05
175	ELA-SA-401	5.37E+21	1495.5	2.37E-04	2.48E-04	2.27E-04	1.08E-04	1.12E-04	1.03E-04
175	ELA-SA-401	5.37E+21	1495.5	2.38E-04	2.52E-04	2.23E-04	1.08E-04	1.14E-04	1.01E-04

4. VUV and NUV Components of Average UV Values

Parker Hannifin S0383-70

ID	Exposure 1		Exposure 2		Exposure 3		Exposure 4		Exposure 5	
	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]
164	267	381.5	147.3	312.9	223.9	313.9	474.6	241.6	455	278.6
165	250.4	395.3	147.3	312.9	240.86	302.8	474.6	241.6	427.8	289.6

Parker Hannifin S0899-50

ID	Exposure 1		Exposure 2		Exposure 3		Exposure 4		Exposure 5	
	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]
60	311.6	344.7	188.36	272.8	240.86	302.8	370.8	276.5	382.7	308
169	250.4	395.3	158.3	301.9	286.1	273.36	451.8	250.4	382.7	308

Esterline ELA-SA-401

ID	Exposure 1		Exposure 2		Exposure 3		Exposure 4		Exposure 5	
	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]	VUV [ESH]	NUV [ESH]
63	311.6	344.7	158.3	301.9	223.9	313.9	404.6	266.2	455	278.6
175	267	381.5	188.36	272.8	286.1	273.36	370.8	276.5	355.6	319

Appendix E

Hypothesis Testing of Leakage Test Data

1. Theory

The method of hypothesis testing used to analyze the leakage test data was similar to that used in a previous section (Appendix B), but is repeated here for completeness. Each of the leakage specimens tested were exposed to unique levels of (1) AO and (2) AO and UV. A statistical approach was used to confirm the validity of comparisons of average leakage rate values across the three materials for each condition. Statistical hypothesis analyses were performed to determine whether the individual data sets of the three materials were exposed to equivalent levels of AO and AO & UV.

The authors assumed that the distribution about the population mean was normally distributed such that the confidence interval could be stated according to equation (D1):

$$\bar{X} \pm t_{\alpha/2} S / \sqrt{n} \quad (D1)$$

where:

- \bar{X} the population mean
- t the student t-value at a specified value of α for t-distribution with $(n-1)$ degrees of freedom
- α the significance level
- S the standard deviation of the sample measurements
- n the sample size

The authors further assumed that the mean of the sample, μ_0 , was contained within the confidence interval. The authors tested this assumption using the hypothesis testing techniques.²⁹ If the resulting confidence interval, $t_{\alpha/2} S / \sqrt{n}$, did not contain μ_0 , then the hypothesis was rejected. If μ_0 was within the confidence interval, then the hypothesis could not be rejected. Therefore, the hypothesized value μ_0 would be rejected if

$$|T| = \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| > t_{\alpha/2} \quad (D2)$$

2. Application

The above theory was used in the analysis of results of small scale leakage rate results of three candidate elastomers: Parker S0383-70, Parker S08998-50, and XELA-SA-401, denoted 70, 50, and 38, respectively. Each of the materials was tested in three different conditions: (1) as-received, (2) after AO exposure, and (3) subsequent to AO and UV exposures. In conditions (2) and (3) the exposure levels to AO and/or UV were varied for each sample, thereby motivating this hypothesis analysis.

The mean exposure levels of the three material data sets were compared to the sample population mean value using a significance level of $\alpha = 0.05$. The performed calculations, along with explanation of terms are shown below.

Condition (2): AO Exposures

The population mean \bar{X} (the average of AO exposure levels for the three material data sets) was calculated to be 5.22×10^{21} atoms/cm². Using equation (D2) with μ_0 being the average level of AO exposure for each particular material, the analysis was performed as presented along with the corresponding value of t for $\alpha = 0.05$ (95% confidence):

$$\text{AO}_{70}: \left| \frac{\bar{X} - \mu_0}{S / \sqrt{n}} \right| = \left| \frac{5.22 \times 10^{21} - 5.41 \times 10^{21}}{1.13 \times 10^{21} / \sqrt{8}} \right| = 0.463 < t_{\alpha/2} = 2.365$$

$$AO_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.22 \times 10^{21} - 5.15 \times 10^{21}}{1.45 \times 10^{21} / \sqrt{8}} \right| = 0.135 < t_{\alpha/2} = 2.365$$

$$AO_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.22 \times 10^{21} - 5.11 \times 10^{21}}{1.73 \times 10^{21} / \sqrt{8}} \right| = 0.187 < t_{\alpha/2} = 2.365$$

The above calculations confirm that the mean exposure values of AO were not statistically different for the three materials tested in condition (2). This confirms the validity of comparisons of average leakage rate values for these materials, as shown in Fig. 17.

Condition (3): AO and UV Exposures

The AO population mean was calculated to be $\bar{X}=5.77 \times 10^{21}$ atoms/cm², while the UV population mean was $\bar{X}=1523.9$ ESH. Similarly as in condition (2) calculations, equation (D2) was used for analysis of average AO and average UV exposures.

$$AO_{70}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.77 \times 10^{21} - 5.23 \times 10^{21}}{1.41 \times 10^{20} / \sqrt{4}} \right| = 7.586 > t_{\alpha/2} = 3.182$$

$$AO_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.77 \times 10^{21} - 6.38 \times 10^{21}}{1.02 \times 10^{21} / \sqrt{4}} \right| = 1.193 < t_{\alpha/2} = 3.182$$

$$AO_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.77 \times 10^{21} - 5.70 \times 10^{21}}{3.81 \times 10^{20} / \sqrt{4}} \right| = 0.378 < t_{\alpha/2} = 3.182$$

$$UV_{70}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{1523.9 - 1544.9}{3.8/\sqrt{4}} \right| = 11.064 > t_{\alpha/2} = 3.182$$

$$UV_{50}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{1523.9 - 1514.3}{17.1/\sqrt{4}} \right| = 1.117 < t_{\alpha/2} = 3.182$$

$$UV_{38}: \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{1523.9 - 1512.4}{19.5/\sqrt{4}} \right| = 1.172 < t_{\alpha/2} = 3.182$$

The above calculation confirm that the mean AO and UV exposure levels of 50 and 38 compounds were not statistically different; however, the total amounts of AO exposure and UV exposure to which the 70 specimens were subjected were not statistically equivalent to the sample population mean. The average AO and UV exposures for the 70 samples were 13% lower and 2% higher, respectively, than the combined average of the 50 and 38 exposure levels. Nevertheless, the average leakage rate results of the 70 material were presented on the same plot (Fig. 17) along with 50 and 38 due to the similarity of exposure levels, while acknowledging the statistical deviation.

Combined Conditions (2) and (3)

In order to quantify the overall effect of space environment exposure (both AO and AO with UV) on the three candidate compounds, confirmation that the individual data sets of the materials in conditions (2) and (3) were exposed to statistically equivalent levels of AO was required. The mean AO exposure levels of the three material data sets in the two conditions were compared to the sample population mean value using a significance level of $\alpha = 0.05$. The AO population mean was calculated to be $\bar{X}=5.40 \times 10^{21}$ atoms/cm². Application of equation (D2) leads to the following calculations and results:

$$\text{AO}_{70} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 5.41 \times 10^{21}}{1.13 \times 10^{21} / \sqrt{8}} \right| = 0.004 < t_{\alpha/2} = 2.365$$

$$\text{AO}_{50} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 5.15 \times 10^{21}}{1.45 \times 10^{21} / \sqrt{8}} \right| = 0.491 < t_{\alpha/2} = 2.365$$

$$\text{AO}_{38} \text{ condition (2): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 5.11 \times 10^{21}}{1.73 \times 10^{21} / \sqrt{8}} \right| = 0.485 < t_{\alpha/2} = 2.365$$

$$\text{AO}_{70} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 5.23 \times 10^{21}}{1.41 \times 10^{20} / \sqrt{4}} \right| = 2.415 < t_{\alpha/2} = 3.182$$

$$\text{AO}_{50} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 6.38 \times 10^{21}}{1.02 \times 10^{21} / \sqrt{4}} \right| = 1.910 < t_{\alpha/2} = 3.182$$

$$\text{AO}_{38} \text{ condition (3): } \left| \frac{\bar{X} - \mu_0}{S/\sqrt{n}} \right| = \left| \frac{5.40 \times 10^{21} - 5.70 \times 10^{21}}{3.81 \times 10^{20} / \sqrt{4}} \right| = 1.542 < t_{\alpha/2} = 3.182$$

Based on the above analysis, the mean levels of AO exposure among the specimens tested in conditions (2) and (3) were not statistically different, with a confidence level of 95%.

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14. ABSTRACT A universal docking and berthing system is being developed by the National Aeronautics and Space Administration (NASA) to support all future space exploration missions to low-Earth orbit (LEO), to the Moon, and to Mars. The Low Impact Docking System (LIDS) is being designed to operate using a seal-on-seal configuration in numerous space environments, each having unique exposures to temperature, solar radiation, reactive elements, debris, and mission duration. As the LIDS seal is likely to be manufactured from an elastomeric material, performance evaluation of elastomers after exposure to atomic oxygen (AO) and ultraviolet radiation (UV) was conducted, of which the work presented herein was a part. Each of the three candidate silicone elastomer compounds investigated, including Esterline ELA-SA-401, and Parker Hannifin S0383-70 and S0899-50, was characterized as a low outgassing compound, per ASTM E595, having percent total mass loss (TML) less than 1.0 percent and collected volatile condensable materials (CVCM) less than 0.1 percent. Each compound was compatible with the LIDS operating environment of -50 to 50 °C. The seal characteristics presented include compression set, elastomer-to-elastomer adhesion, and o-ring leakage rate. The ELA-SA-401 compound had the lowest variation in compression set with temperature. The S0383-70 compound exhibited the lowest compression set after exposure to AO and UV. The adhesion for all of the compounds was significantly reduced after exposure to AO and was further decreased after exposure to AO and UV. The leakage rates of o-ring specimens showed modest increases after exposure to AO. The leakage rates after exposure to AO and UV were increased by factors of up to 600 when compared to specimens in the as-received condition.					
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