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**(12) United States Patent**  
**Tang et al.****(10) Patent No.: US 6,405,594 B1**  
**(45) Date of Patent: Jun. 18, 2002****(54) SILICON BASE PLATE WITH LOW PARASITIC ELECTRICAL INTERFERENCE FOR SENSORS****(58) Field of Search** ..... 73/514.35, 504.02, 73/504.03, 504.04, 504.12, 504.14, 514.29; 257/415**(75) Inventors:** **Tony K. Tang**, Glendale; **Roman C. Gutierrez**, La Crescenta, both of CA (US)**(56) References Cited**

## U.S. PATENT DOCUMENTS

**(73) Assignee:** **California Institute of Technology**, Pasadena, CA (US)

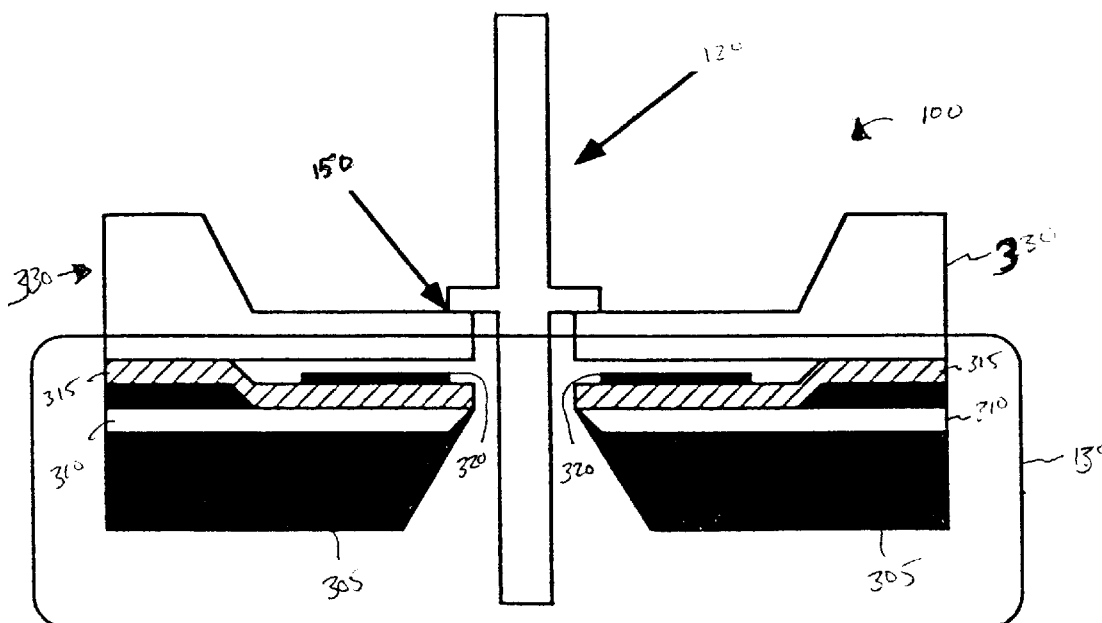
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**(\*) Notice:** Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 62 days.

\* cited by examiner

*Primary Examiner*—Richard A. Moller*(74) Attorney, Agent, or Firm*—Fish & Richardson P.C.**(21) Appl. No.:** **09/612,327****(57) ABSTRACT****(22) Filed:** **Jul. 6, 2000**

A microgyroscope has a baseplate made of the same material as the rest of the microgyroscope. The baseplate is a silicon baseplate having a heavily p-doped epilayer covered by a thick dielectric film and metal electrodes. The metal electrodes are isolated from the ground plane by the dielectric. This provides very low parasitic capacitive coupling between the electrodes. The thick dielectric reduces the capacitance between the electrodes and the ground plane.

**Related U.S. Application Data****(60)** Provisional application No. 60/143,200, filed on Jul. 9, 1999.**(51) Int. Cl.<sup>7</sup>** ..... **G01P 15/00****(52) U.S. Cl.** ..... **73/504.02; 73/514.35; 257/415****12 Claims, 2 Drawing Sheets**

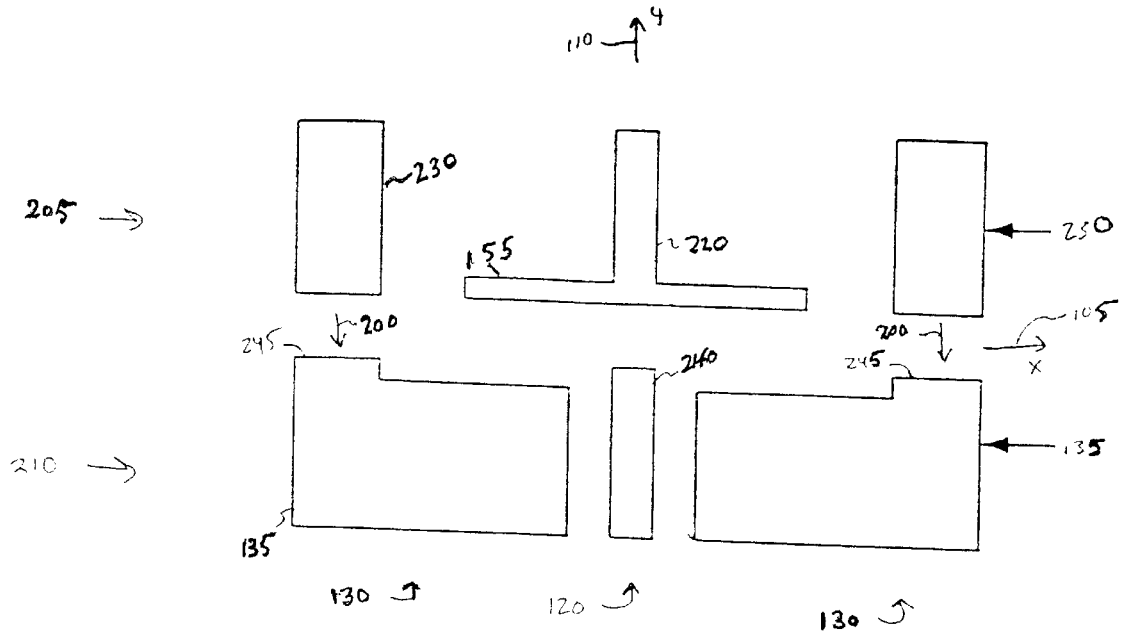


Figure 1

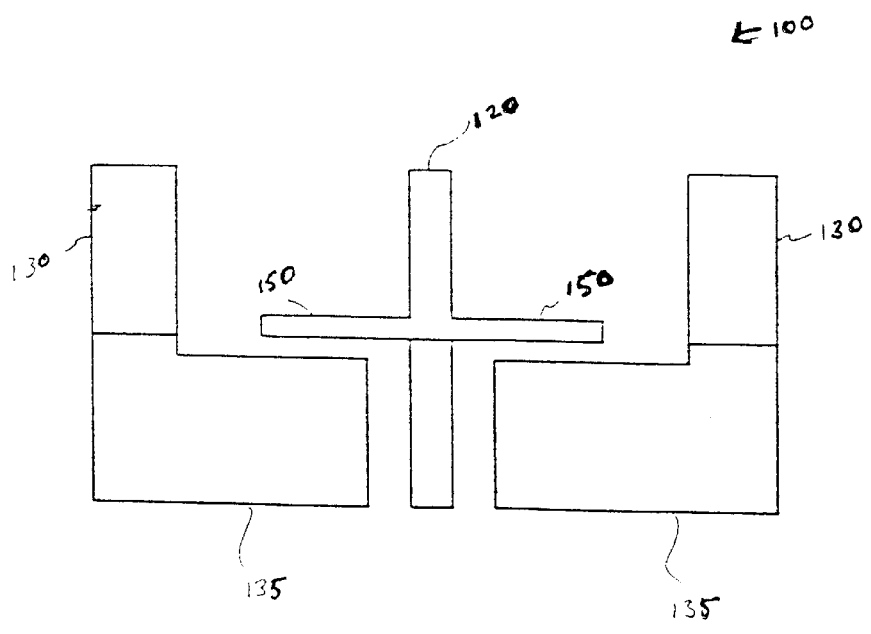


Figure 2

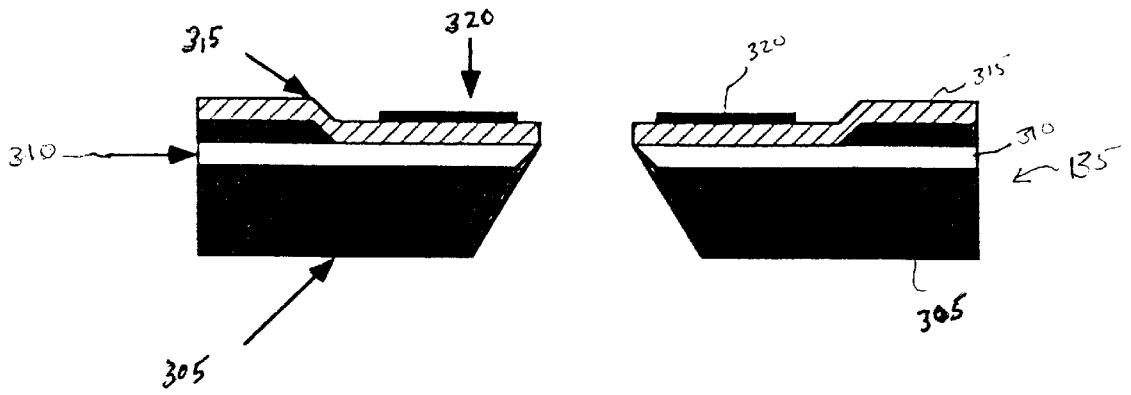


Figure 3

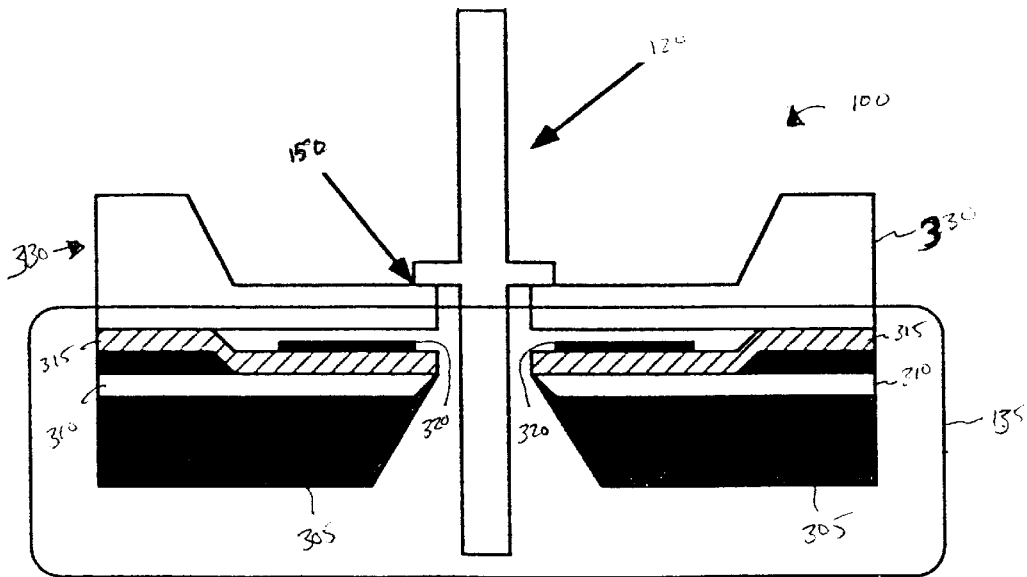


Figure 4

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## SILICON BASE PLATE WITH LOW PARASITIC ELECTRICAL INTERFERENCE FOR SENSORS

### CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims benefit of U.S. Provisional Application No. 60/143,200, filed Jul. 9, 1999.

### ORIGIN OF INVENTION

The invention described herein was made in the performance of work under a NASA contract, and is subject to the provisions of Public Law 96-517 (35 U.S.C. § 202) in which the Contractor has elected to retain title.

### TECHNICAL FIELD

This invention relates to vibratory gyroscopes, and more particularly to silicon micromachined vibratory gyroscopes.

### BACKGROUND

Multi-axis sensors are highly desirable for inertial sensing of motion in three dimensions. Previously, such sensors were constructed of relatively large and expensive electromagnetic and optical devices. More recently, micromechanical sensors have been fabricated using semiconductor processing techniques. Microelectrical mechanical or "MEMS" systems allow formation of physical features using semiconductor materials and processing techniques. These techniques enable the physical features to have relatively small sizes and be precise. Specifically, micromechanical accelerometers and gyroscopes have been formed from silicon wafers by using photolithographic and etching techniques. Such microfabricated sensors hold the promise of large scale production and therefore low cost.

The integration of three gyroscopic sensors to measure the rotation rates about the three separate axes coupled with three accelerometric sensors to measure the acceleration along the three axes on a single chip would provide a monolithic, six degree-of-freedom inertial measurement system capable of measuring all possible translations and orientations of the chip. There has been some difficulty in constructing a high-performance, or sensitive vibratory rate gyroscope to measure the rotation about the axis normal to the plane of the silicon chip, i.e., the Z-axis.

In a vibratory gyroscope, the Coriolis effect induces energy transfer from the driver input vibratory mode to another mode which is sensed or output during rotation of the gyroscope. Silicon micromachined vibratory gyroscopes are integratable with silicon electronics. These devices are capable of achieving high Q factors, can withstand high g shocks due to their small masses, are insensitive to linear vibration and consume little power. However, most of these micromachined gyroscopes have a very small rotation response, since their input and output vibration modes have different mode shapes and resonant frequencies. The use of different resonant modes also makes these devices very temperature sensitive due to the different temperature dependency of each of the modes. These devices usually have very high resonant frequencies resulting in low responsivity, since the Coriolis induced response is inversely proportional to the resonant frequency of the structure. Finally, due to the small mass of the structure, thermal noise limits the ultimate performance and use of microgyroscopes. For these reasons, micromachined vibratory gyroscopes have not been used for precision navigation and attitude control applications, but

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have been employed primarily for automotive applications in which extreme low cost is a major driving factor and performance is set at a lower premium.

Traditional baseplates for the microgyroscopes were constructed using either quartz or ceramic. Although these materials were helpful in reducing parasitic capacitance, the thermal expansion coefficient for these materials is different than the rest of the microgyroscope. Thus, under a variety of temperatures, the stress on the microgyroscope varies. What is needed is a baseplate having a similar thermal expansion coefficient as the rest of the microgyroscope while reducing the effects of parasitic capacitance.

### SUMMARY

The present invention is a microgyroscope having a baseplate made of the same material as the rest of the microgyroscope. The baseplate is a silicon baseplate having a heavily p-doped epilayer covered by a thick dielectric film and metal electrodes. The metal electrodes are isolated from the ground plane by the dielectric. This provides very low parasitic capacitive coupling between the electrodes. The thick dielectric reduces the capacitance between the electrodes and the ground plane.

### DESCRIPTION OF DRAWINGS

These and other features and advantages of the invention will become more apparent upon reading the following detailed description and upon reference to the accompanying drawings.

FIG. 1 is a side view of the components of a microgyroscope constructed according to one embodiment of the present invention.

FIG. 2 is a side view of a bonded microgyroscope according to one embodiment of the present invention.

FIG. 3 is a side view of the baseplate of the microgyroscope according to one embodiment of the present invention.

FIG. 4 is a side view of the microgyroscope including the baseplate of FIG. 3 according to one embodiment of the present invention.

### DETAILED DESCRIPTION

FIG. 1 is a side view of a microgyroscope **100** constructed according to one embodiment of the present invention. The microgyroscope **100** detects forces in the x-direction **105**, the y-direction **110**, and in the z-direction **115**. Vertical capacitors **130** surround the vertical post **120**. The vertical capacitors **130** provide electrostatic actuation of the vertical post **120** and allow for capacitive detection of the motions of the vertical post **120**.

A first section **205** of the microgyroscope **100** is made from a first silicon wafer and a second section **210** of the microgyroscope is made from a second silicon wafer. The first section **205** of the microgyroscope **100** includes a first portion **220** of the vertical post **120** and first portions **230** of the vertical capacitors **130**. The second section **210** of the microgyroscope **100** includes a second portion **240** of the vertical post **120**, second portions **245** of the vertical capacitors **130**, and a baseplate **135**. Although the invention is described with the vertical capacitors **130** being constructed of first portions **230** and second portions **245**, it can be appreciated that the first portions **230** and second portions **245** may be electrically isolated to create even more independent vertical capacitors **130**.

To construct the microgyroscope **100**, the first section **205** is positioned above the section **210**. The first section **205** is

lowered as indicated by reference numeral **200** onto the second section **210**. The first and second sections **205**, **210** are then bonded together using standard bonding techniques such as metal-to-metal bonding. The first and second sections **205**, **210** are bonded in a position so that the first portion **220** and the second portion **240** of the vertical post **120** are aligned to form one continuous vertical post **120**. The first portions **230** of the vertical capacitors **130** are aligned with the second portions **245** of the vertical capacitors **130** on the baseplate **135**. Of course, the first portions **235** and the second portions **230** may be electrically isolated. Thus, once the first section **205** is connected to the second section **210**, the vertical post **120** is positioned with the microgyroscope **100**.

FIG. 2 shows a side view of the completed microgyroscope **100** according to one embodiment of the present invention. Once constructed, the vertical post **120** is supported by a series of flanges **150**. The flanges **150** allow the vertical post **120** to rest upon the baseplate. As can be seen in FIG. 2, the flanges **150** are positioned at approximately the mid-point of the vertical post **120**. Because the vertical post **120** is connected to the baseplate **135** via the flanges **150** at approximately the mid-point, the vertical post **120** is free to move in a rocking motion in the x-direction **105** and the y-direction **110**. Under input rotation, the Coriolis force causes the vertical post **120** to move in the orthogonal direction to the drive motor. The rotation rate sensitivity is proportional to the input rotation rate, the drive amplitude, and the quality factor of the resonator.

Because each portion of the microgyroscope **100** is constructed from a silicon wafer, the performance variations from device to device is reduced. Further, the behavior of each portion of the microgyroscope **100** under varying temperature conditions is more consistent.

FIG. 3 is a side view of the baseplate **135** of the microgyroscope **100** according to one embodiment of the present invention. The baseplate **135** comprises a silicon substrate **305**, a silicon p+ epilayer **310**, a dielectric layer **315**, and metal electrodes **320**. The silicon substrate **305** is grounded and covered by the heavily p-doped epilayer **310**. The epilayer **310** is covered by the thick dielectric layer **315**. The metal electrodes **320** are formed on the dielectric layer **315**.

The dielectric layer **315** may be composed of silicon dioxide, silicon nitride, or other known dielectric materials. The dielectric layer **315** provides isolation of the metal electrodes **320** from the ground plane. The dielectric layer **315** is generally about 3 to 4 microns thick, and may be thicker than 4 microns to enhance the isolation. Because of the isolation provided by the dielectric layer, there is very little capacitive coupling between the metal electrodes **320**.

FIG. 4 is a side view of the microgyroscope **100** including the baseplate **135** of FIG. 3 according to one embodiment of

the present invention. In the fully assembled gyroscope **100**, the vertical post **120** rests on a clover-leaf structure **330**. The metal electrodes **320** provide electrostatic drive and sense control. The metal electrodes **320** are electrically isolated from each other and other electrical interference by the dielectric layer **315** and the substrate **305**.

Numerous variations and modifications of the invention will become readily apparent to those skilled in the art. Accordingly, the invention may be embodied in other specific forms without departing from its spirit or essential characteristics.

What is claimed is:

1. A method of forming a baseplate for a microgyroscope comprising:

forming a substrate layer;  
covering the substrate layer with an epilayer;  
positioning a dielectric layer on the epilayer; and  
isolating a plurality of metal electrodes from the substrate layer.

2. The method of claim 1, wherein the metal electrodes are isolated by the dielectric layer, thereby reducing parasitic capacitance.

3. The method of claim 1, wherein the dielectric layer is approximately 3 to 4 microns thick.

4. The method of claim 1, wherein the dielectric layer is greater than 4 microns thick.

5. The method of claim 1, wherein the epilayer is a heavily p-doped epilayer.

6. The method of claim 1, wherein the baseplate is formed of silicon.

7. A microgyroscope comprising:

a substrate;  
an epilayer which covers the substrate;  
a dielectric layer formed over the epilayer; and  
a plurality of metal electrodes formed on the dielectric layer, wherein the dielectric layer isolates the plurality of metal electrodes from the substrate.

8. The microgyroscope of claim 7, wherein the substrate is grounded.

9. The microgyroscope of claim 7, wherein the epilayer is p-doped.

10. The microgyroscope of claim 7, wherein the dielectric layer is approximately 3–4 microns thick.

11. The microgyroscope of claim 7, wherein the dielectric layer is thicker than 4 microns.

12. The microgyroscope of claim 7, wherein the dielectric layer reduces parasitic capacitance between the metal electrodes.

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