

Structure Detection of Nonlinear Aeroelastic Systems with Application to Aeroelastic Flight Test Data: Part I

Sunil L. Kukreja and Martin J. Brenner

NASA Dryden Flight Research Center, Structural Dynamics Group, Edwards, California, USA



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Dryden Flight Research Center

Outline

- Introduction – Objectives
- The NARMAX Structure
- NARMAX Identification Problem
 - Order, parameter estimation & *structure detection*
- Structure Detection: Current Methods
- Results
 - Application to simulated pitch-plunge model
- Conclusions



Objectives

- Investigate applicability of NARMAX structure detection to aeroelastic systems
 - Simulated model of aircraft freeplay
- Evaluate performance
 - Experimental aeroelastic flight test data



NARMAX Model Description

- Input-output relationship:

$$y(n) = F^l[y(n-1), \dots, y(n-n_y), u(n), \dots, u(n-n_u), e(n-1), \dots, e(n-n_e)] + e(n)$$

- Variety of nonlinear terms:

$$u^2(n-3) \quad u(n)u(n-1) \quad y(n-1)y(n-2) \quad u^2(n-1)y(n-2)$$

- F^l , can also be described by hard nonlinearities such as a half-wave rectifier

- Linear-in-the-parameters
 - Linear regression techniques



Full Identification Procedure

- Model order selection
 - Determine number of input, output and error lags and nonlinearity order
- Parameter estimation
 - Determine values of unknown parameters
- Structure detection
 - Select parameters to include in model



System Order

$$y(n) = F^l [y(n-1), \dots, y(n-n_y), u(n), \dots, u(n-n_u), e(n-1), \dots, e(n-n_e)] + e(n)$$

- System order represented as:

$$O = [n_u \ n_y \ n_e \ l]$$

- Output additive noise: $n_y = n_e$
 $\Uparrow \Uparrow O = [n_u \ n_y \ l]$



Parameter Estimation

- Need an estimate of θ :

$$\min_{\theta} \frac{1}{2} \|\mathbf{Z} - \Psi\theta\|_2^2$$

and statistics

- NARMAX models provide concise system representation

- noise on the output enters the model as product terms with the system input and output
- “Ordinary” least-squares \rightarrow biased; does not account for noise
- Solution extended least-squares:

$$\hat{\theta} = (\Psi^T \Psi)^{-1} \Psi^T \mathbf{Z}; \quad \text{where} \quad \Psi = [\Psi_{zu} \ \Psi_{zue} \ \Psi_{\hat{\epsilon}}].$$

- Bias addressed by modelling lagged errors
- NARMAX formulation redefined into prediction error model, ϵ replacing e and z replacing y
- Deterministic



Possible Terms

- NARMAX models described by few terms
- Maximum number of candidate terms:

$$p = \sum_{i=1}^l p_i + 1;$$
$$p_i = \frac{p_{i-1}(n_y + n_u + n_e + i)}{i}, \quad p_0 = 1$$

– Example: model of order: $O = [4\ 4\ 4\ 2] \Rightarrow p = 105$ candidate terms.



Example of Candidate Terms

- Model example:

$$y(n) = y(n-1) + u(n-1) + u^2(n-1) + e(n-1) + e(n)$$

- Described by: $O = [n_u = 1 \ n_y = 1 \ l = 2] \Rightarrow p = 15$

- Candidate terms:

$$\begin{aligned} y(n) = & \theta_0 + \theta_1 u(n) + \theta_2 u(n-1) + \theta_3 u^2(n) + \theta_4 u(n)u(n-1) + \theta_5 u^2(n-1) + \theta_6 y(n-1) \\ & + \theta_7 u(n)y(n-1) + \theta_8 u(n-1)y(n-1) + \theta_9 y^2(n-1) + \theta_{10} u(n)e(n-1) \\ & + \theta_{11} u(n-1)e(n-1) + \theta_{12} y(n-1)e(n-1) + \theta_{13} e(n-1) + \theta_{14} e^2(n-1) + e(n) \end{aligned}$$



Structure Detection

- Select a subset of candidate terms
- Best describes output



Traditional Approaches to Structure Detection

- Covariance matrix, \mathbf{P}_θ
- Stepwise Regression
- Bootstrap method



Covariance matrix, \mathbf{P}_θ

- T-test with regression analysis referred to as hypothesis testing: computing differences between means
- Suppose $E(\mathbf{Z}) = \hat{\theta}_1 + \hat{\theta}_2\psi_2 + \hat{\theta}_3\psi_3 + \dots + \hat{\theta}_p\psi_p$ was fit
 - $\hat{\theta}$'s tested against null hypothesis, $\hat{\theta}_i = 0, i = 1, 2, \dots, p$
- Confidence interval for $\hat{\theta}_i$:

$$\hat{\theta}_i \pm t(\alpha/2, N - p) \hat{P}_{ii}$$

where $\mathbf{P} = \sigma^2(\mathbf{\Psi}^T \mathbf{\Psi})^{-1}$ and \hat{P}_{ii} i th diagonal element

- t tabulated t ratio at $\alpha/2$ level of significance ($0 \leq \alpha \leq 1$) with $N - p$ d.o.f.
- Significance assessed with $(1 - \alpha)\%$ confidence that the parameter lies within this range
- Interval includes zero, indicates $\hat{\theta}_i$ is not significantly different from zero at the α level and can be removed from the model



Stepwise Regression

- Relies on the incremental change in RSS from adding or removing a parameter
- Two F distribution levels, F_{out} and F_{in} , formed to determine whether parameter(s) should be removed from the model (F_{out}) or included in the model (F_{in})
 - F-levels are based on $N - p$ d.o.f. for predetermined α th level of significance
- Statistics F_{in} and F_{out} estimated from RSS for model with p parameters as:
$$F_{\text{in}} = \frac{\text{RSS}_p - \text{RSS}_{p+1}}{\text{RSS}_{p+1}/(N - p - 1)} \quad \text{and} \quad F_{\text{out}} = \frac{\text{RSS}_{p-1} - \text{RSS}_p}{\text{RSS}_p/(N - p)}.$$
- For good model parameterisations, F_{out} must not be greater than F_{in}



Bootstrap Method

- Numerical Procedure for Estimating Parameter Statistics
- Mild Conditions on Sample Errors
 - Errors independent and identically distributed (i.i.d.)
 - Zero-mean
- Application of ℓ_2 minimisation: $\rightarrow \hat{\mathbf{Z}}, \hat{\boldsymbol{\epsilon}}$ and $\hat{\boldsymbol{\theta}}$
- Assume: $\hat{\boldsymbol{\epsilon}} = [\hat{\epsilon}_1, \hat{\epsilon}_2, \dots, \hat{\epsilon}_N]$, from Unknown Distribution, \mathcal{F}
 - Random resampling *with replacement*: $\hat{\boldsymbol{\epsilon}}^* = [\hat{\epsilon}_1^*, \hat{\epsilon}_2^*, \dots, \hat{\epsilon}_N^*]$: estimates distribution \mathcal{F} ;
 \implies Example: $N = 8$, $\hat{\boldsymbol{\epsilon}}^* = [\hat{\epsilon}_6, \hat{\epsilon}_8, \hat{\epsilon}_7, \hat{\epsilon}_3, \hat{\epsilon}_4, \hat{\epsilon}_7, \hat{\epsilon}_5, \hat{\epsilon}_1]$
- $\mathbf{Z}^* = \Psi \hat{\boldsymbol{\theta}} + \hat{\boldsymbol{\epsilon}}^*$
 - Bootstrap ℓ_2 minimisation estimate $\hat{\boldsymbol{\theta}}^*$ computed from \mathbf{Z}^*
- Repeated B Times: $\hat{\boldsymbol{\Theta}}^* = [\hat{\boldsymbol{\theta}}_1^*, \dots, \hat{\boldsymbol{\theta}}_B^*]$
- Statistics Computed from $\hat{\boldsymbol{\Theta}}^*$ at a Chosen Level of Significance, α

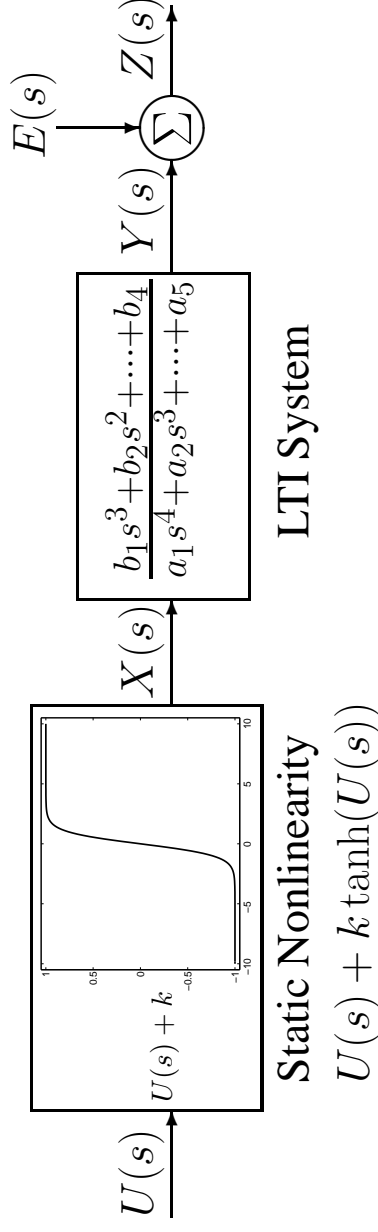


Rationale

- Structure detection provide useful process insights that can be used in subsequent development or refinement of physical models
- Investigate performance of the covariance matrix (t-test), stepwise regression and bootstrap method on a simulated NARMAX model of aeroelastic structural stiffness
- Assess performance of these techniques for applicability to experimental aircraft data.



Aeroelastic Structural Stiffness Model



- Simulated in continuous-time
- NARMAX representation aeroelastic structural stiffness model:

$$\begin{aligned}
 z(n) = & \theta_1 z(n-1) + \theta_2 z(n-2) + \theta_3 z(n-3) + \theta_4 z(n-4) + \theta_5 u(n-1) \\
 & + \theta_6 u(n-2) + \theta_7 u(n-3) + \theta_8 u(n-4) + \theta_9 \tanh(u(n-1)) \\
 & + \theta_{10} \tanh(u(n-2)) + \theta_{11} \tanh(u(n-3)) + \theta_{12} \tanh(u(n-4)) \\
 & + \theta_{13} e(n-1) + \theta_{14} e(n-2) + \theta_{15} e(n-3) + \theta_{16} e(n-4) + e(n).
 \end{aligned}$$



Continuous-Time System Coefficients

- Continuous-time values correspond to those found in experiments

CT Coefficient	Value
U	18.0 m/s
a	-0.600 m
b	0.135 m
I_α	0.065 m ² Kg
k_h	2844 N/m
k_α	2.82 Nm/rad
x_a	0.247 m
c_h	27.4 Kg/s
c_α	0.180 m ² Kg/s
ρ	1.23 kg/m ³
cl_α	3.28
cl_β	3.36
$c_{m\alpha}$	-0.628
$c_{m\beta}$	-0.635
k	2



Simulation Protocol

- One hundred Monte-Carlo simulations
- Each input/output realization unique
 - Inputs uniform, white, zero-mean, with variances of 8 rad^2
- Unique Gaussian, white, zero-mean, noise sequence added to output
 - Output additive noise amplitude increased in increments of 5 dB, from 20 to 5 dB SNR
- Identification data length: $N = [10,000 \ 80,000]$ points increased in increments of 10,000
- Bootstrap method $B = 100$ bootstrap replications generated to assess distribution of each parameter



....Simulation Protocol Cont.

- All three techniques parameters tested for significance at 95% confidence level
- Model posed for structure computation, additive nonlinear model:

$$z(n) = \sum_{v=1}^q \theta_v \psi(n) + \sum_{w=1}^r \theta_w f(\psi(n)) + e(n); \quad q + r = p.$$

- Model order: $O = [4 \ 4 \ 4 \ \text{tanh}]$
- tanh selected as basis because a wing section response limited due to structural stiffness and appears to saturate smoothly
- Full model description 27 candidate terms

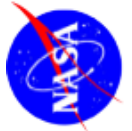
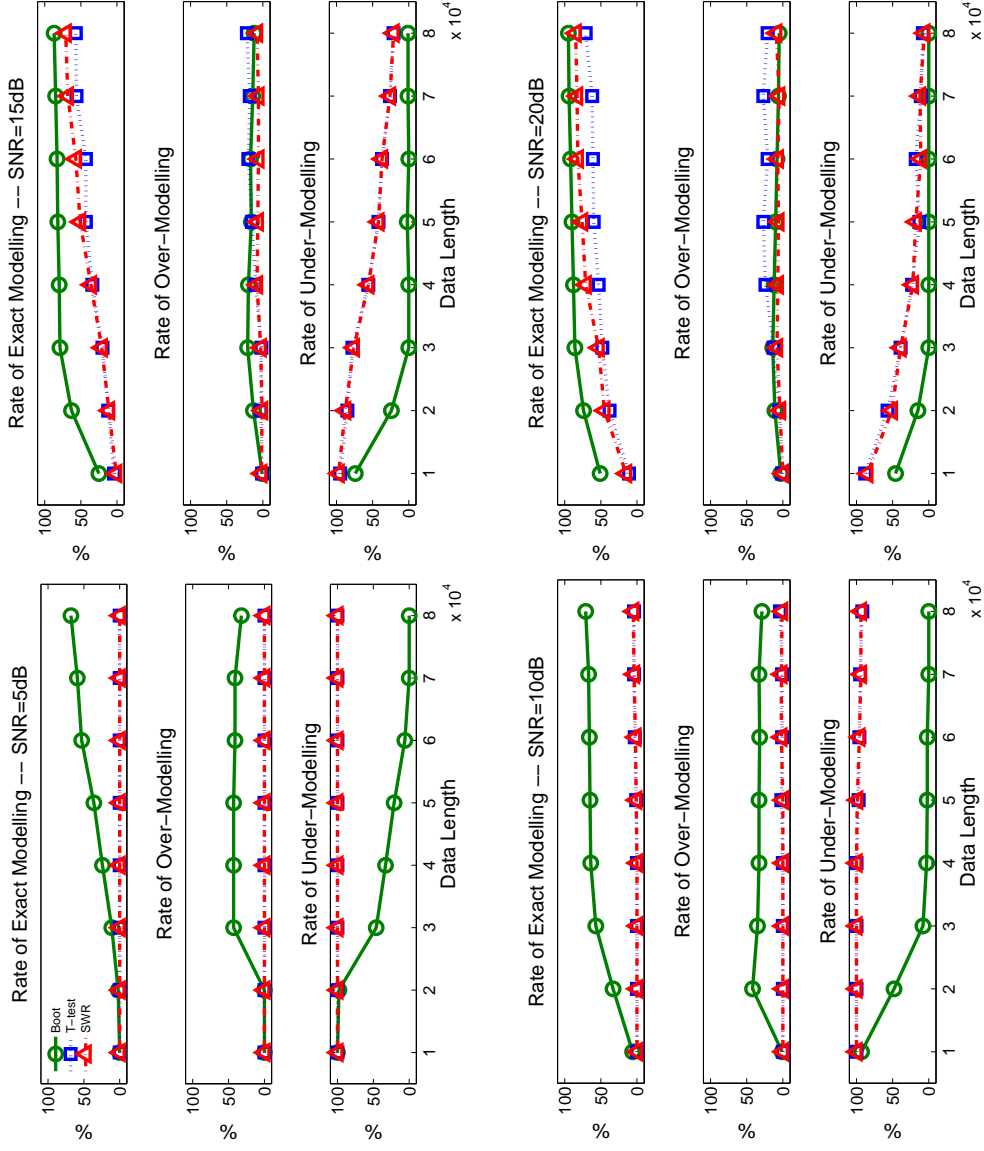


Results Classified into Three Categories

1. **Exact Model:** A model which contains only true system terms,
2. **Over-modelled:** A model with all its true system terms plus spurious parameters and
3. **Under-modelled:** A model without all its true system terms. An under-modelled model may contain spurious terms as well



Simulation Results



Summary of Simulation Findings

- For this over-parameterised model describing aeroelastic dynamics the bootstrap method clearly outperformed the t-test and stepwise regression
- For analysis of flight test data only implemented bootstrap structure detection method

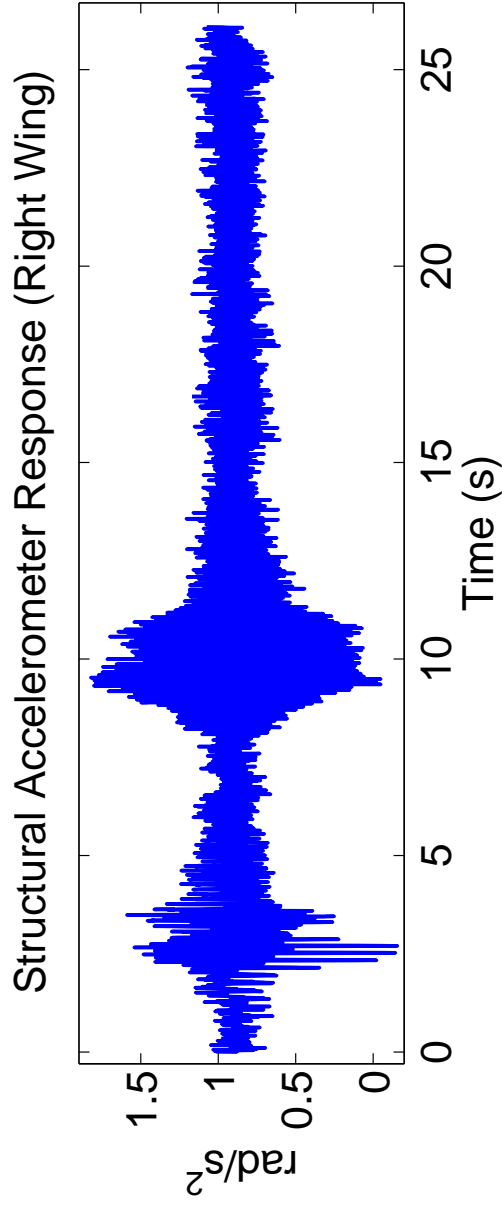
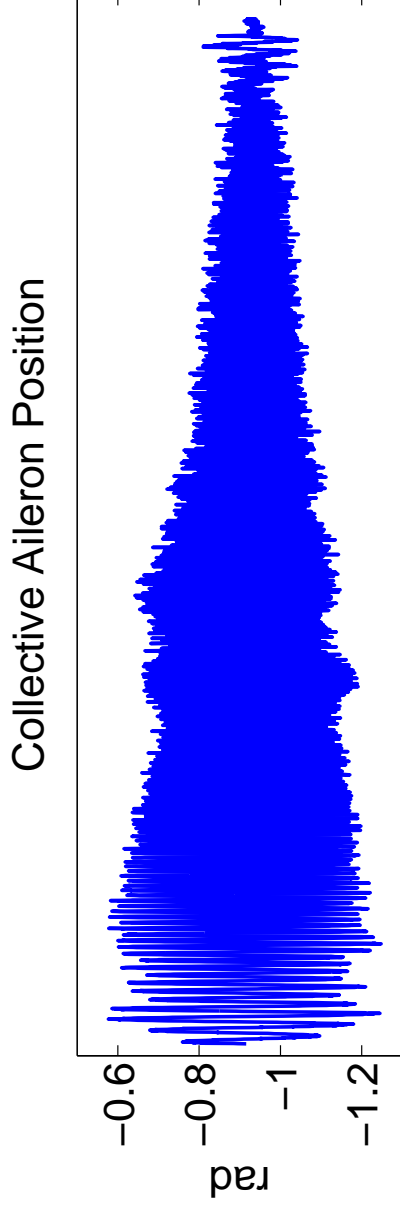


Experimental Aircraft Data

- System identified applying bootstrap approach: model form additive non-linear & $O = [4 \ 4 \ 4 \ \tanh]$
- Scaled hyperbolic tangent functions used because the input amplitude is less than ± 1
 - Scale factors used for the input, output and error signals in the range of $\nu = [0.1 \ 1.0]$ and increased in increments of 0.1
 - A scaled hyperbolic tangent is denoted as $\tanh(\cdot, \nu)$
 - Models with every possible combination of scale factors were considered (i.e. structure computation performed on 1,000 models)
 - Full model description 27 candidate terms
- Model which yielded highest cross-validation percent fit deemed the best-fit model
 - Estimation $N_e = 5, 200$: right wing & cross-validation $N_v = 5, 200$: left wing



Identification Data



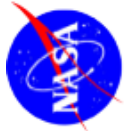
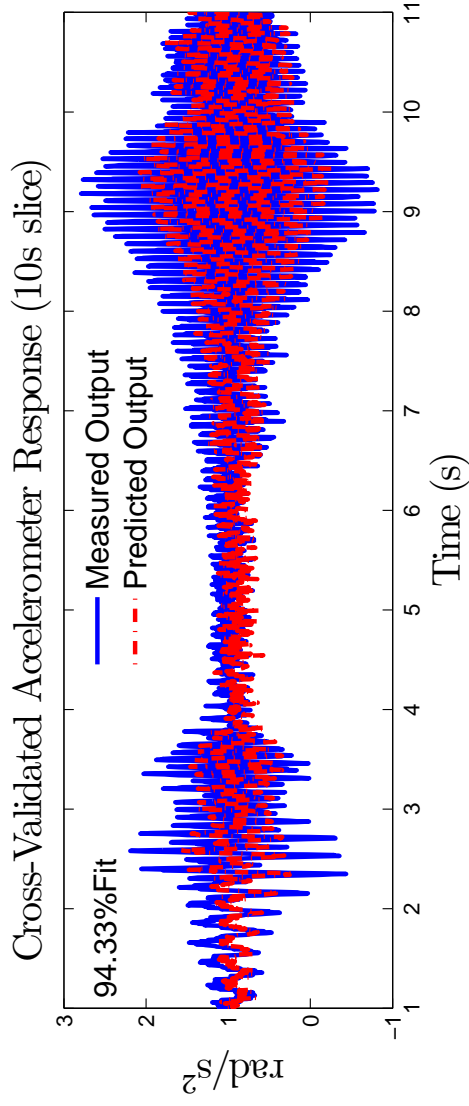
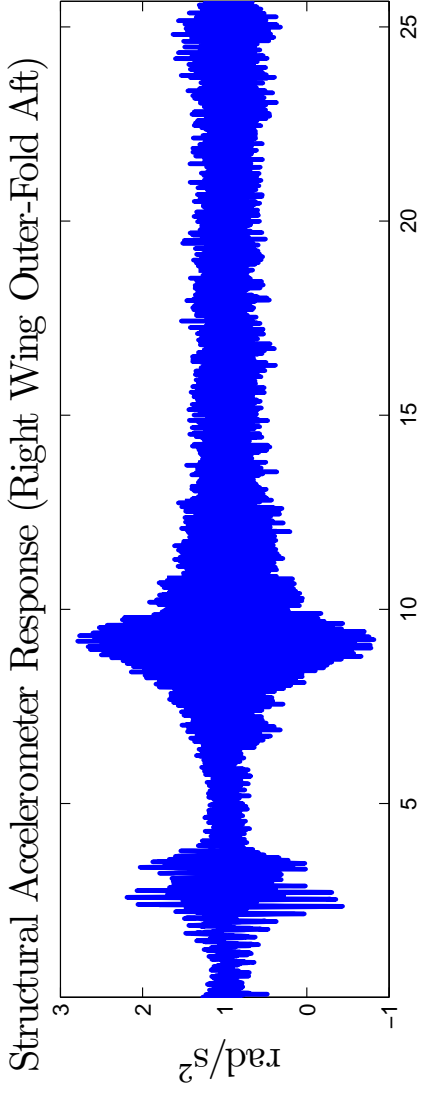
Computed Structure

- Contains 14 terms

$$\begin{aligned} z(n) = & \hat{\theta}_0 + \theta_1 z(n-1) + \hat{\theta}_2 z(n-3) + \hat{\theta}_3 z(n-4) + \hat{\theta}_4 u(n) + \hat{\theta}_5 u(n-2) \\ & + \hat{\theta}_6 u(n-4) + \hat{\theta}_7 \tanh(u(n), 0.3) + \hat{\theta}_8 \tanh(u(n-1), 0.3) \\ & + \hat{\theta}_9 \tanh(u(n-3), 0.3) + \hat{\theta}_{10} \tanh(u(n-4), 0.3) + \hat{\theta}_{11} e(n-1) \\ & + \hat{\theta}_{12} e(n-3) + \hat{\theta}_{13} e(n-4) + e(n). \end{aligned}$$



Cross-Validation Data



Summary of Findings

- Simulated model of aeroelastic structural stiffness dynamics showed:
 - Given sufficient data length ($N_e = 60,000 - 80,000$), the bootstrap method had a low rate of selecting an under-modelled model (2–0%) and a high rate of selecting the exact model (60–95%) for all SNR levels
 - Both t-test and stepwise regression had difficulty computing the correct structure, with selection range of 3–70% and 2–85% respectively, for equivalent data lengths and SNR levels
- Experimental results demonstrate:
 - Bootstrap successfully reduced number of regressors posed to aircraft aeroelastic data yielding a parsimonious model structure
 - The computed parsimonious structure capable of predicting a large portion of the cross-validation data, collected on adjacent wing with different sensor
 - Suggests identified structure and parameters explain the data well



Conclusions

- Simulation results demonstrate bootstrap approach for structure computation of aircraft structural stiffness provided a high rate of true model selection
- T-test and stepwise regression methods had difficulty providing accurate results
- Work contributes to understanding of the use of structure detection for modeling and identification of aerospace systems.
- Limitation of model complexity that can be studied with these structure computation techniques
 - Result of the large number of candidate terms, for a given model order, and the data length required to guarantee convergence
 - Another approach to structure computation problem uses a least absolute shrinkage and selection operator (LASSO)



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