Multi-scale Rule-of-Mixtures Model of Carbon Nanotube/Carbon Fiber/Epoxy Lamina

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ABSTRACT

A unidirectional carbon fiber/epoxy lamina in which the carbon fibers are coated with single-walled carbon nanotubes is modeled with a multi-scale method, the atomistically informed rule-of-mixtures. This multi-scale model is designed to include the effect of the carbon nanotubes on the constitutive properties of the lamina. It included concepts from the molecular dynamics/equivalent continuum methods, micromechanics, and the strength of materials. Within the model both the nanotube volume fraction and nanotube distribution were varied. It was found that for a lamina with 60% carbon fiber volume fraction, the Young's modulus in the fiber direction varied with changes in the nanotube distribution, from 138.8 to 140 GPa with nanotube volume fractions ranging from 0.0001 to 0.0125. The presence of nanotube near the surface of the carbon fiber is therefore expected to have a small, but positive, effect on the constitutive properties of the lamina.

INTRODUCTION

Near term applications of carbon nanotubes (CNT) in materials for aerospace vehicles are most likely to be realized with mechanical or electrical applications that require small quantities of nanotubes. To implement carbon nanotubes as structural members could be accomplished by the selective use of carbon nanotubes in critical areas of traditional composites. For example, carbon nanotubes added between the layers of a traditional carbon fiber/epoxy laminate may well improve the interface strength between carbon fiber and epoxy matrix, and thereby improve fracture toughness of these laminates.
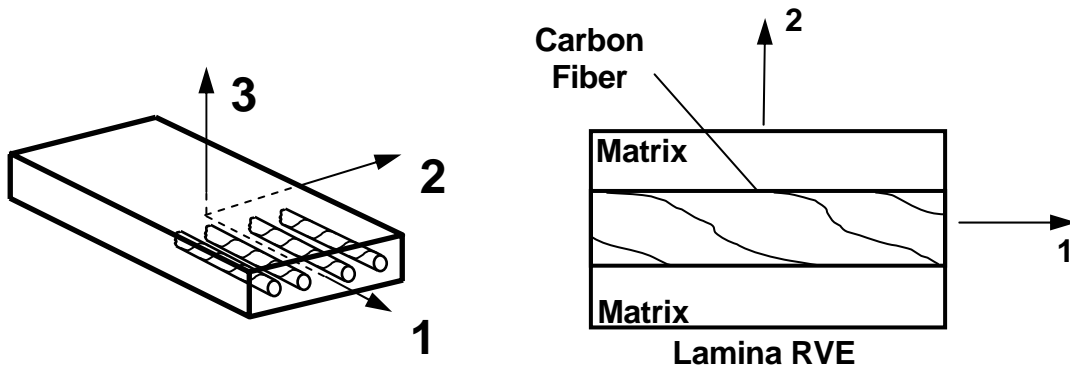
The effectiveness of adding carbon nanotubes to laminates can be analyzed with multi-scale models which are capable of incorporating atomistic details. At the atomistic-level the assumptions of 'perfect' bonding between the various contributors to the laminate can be removed in detailed atomistic simulations. With properties at this level established, the micro-scale properties can be accessed with more standard micromechanics methods such as the Mori-Tanaka method or the rule-of-mixtures analysis[1]. Multi-scale models have applied atomistic simulation and micromechanics to the constitutive properties of various functionalized nanotube materials [2-5]. There are some atomistic simulations of epoxy/nanotube composites by other researchers which address nanotube pull-out [6]. Also, a more recent study on nanotubes chemically bonded into the epoxy matrix showed a

Young's modulus of up to 160 GPa in the direction of the nanotube axis, and 4-8 GPa in the transverse direction at a nanotube volume fraction of 25 % [7].
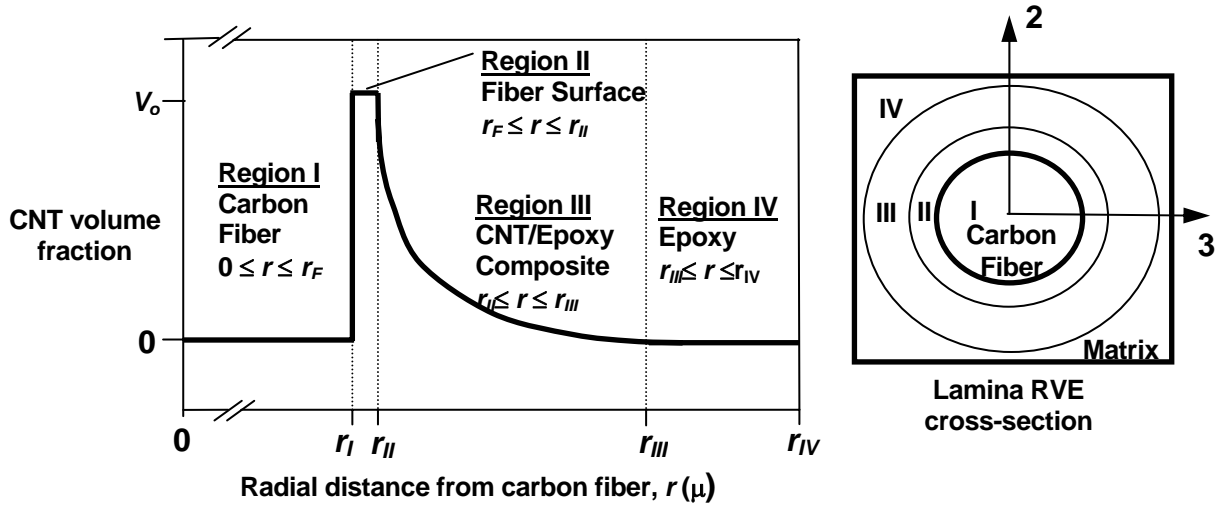
In the present work, the constitutive properties of a unidirectional carbon fiber/epoxy lamina are modeled by a multi-scale model. In the lamina, each carbon fiber is uniformly coated with carbon nanotubes. The objective is to calculate the Young's modulus in the direction of the carbon fiber of unidirectionally-reinforced carbon fiber/epoxy laminae, where the nanotube distribution around the fiber is varied. For this purpose, we develop the atomistically informed rule-of-mixtures approach.   This method requires a multi-scale approach to the analysis of several components of the nanotube-coated carbon fiber. The constitutive properties of the nanoscale components are modeled with the molecular dynamics/equivalent continuum (MD/EC) model. The CNT distribution and volume are modeled using the MD/EC model in conjunction with the Mori-Tanaka micromechanics method to calculate the Young's modulus over a defined nanotube distribution. A description of each stage of the multi-scale model is presented, and the results of applying the atomistically-informed rule-of-mixtures are given for a lamina with 60% carbon fiber volume fraction.

MATERIAL DESCRIPTION

A unidirectional carbon fiber-reinforced polymer lamina [8] (Fig. 1) is constructed such that the carbon fibers are coated with carbon nanotubes (CNT) and then cured in epoxy. The schematic in Fig. 1 defines the principal material axes with respect to the fiber direction. Herein, the 1-, 2-, and 3-axes, are referred to as longitudinal, transverse, and out-of-plane, respectively. The epoxy was comprised of bisphenol F resin reacted with epichlorohydrin and cured with triethylenetetramine (TETA). The carbon nanotubes were (10,10) single-walled carbon nanotubes of radius 0.678 nm. It is assumed in the model that there is no chemical bonding between the 3 components: carbon fiber, carbon nanotubes, and the epoxy.

Figure 1. Unidirectionally-reinforced lamina

2

3

CNT volume fraction

V_o

Region II
Fiber Surface
$r_F \leq r \leq r_{II}$

Region I
Carbon
Fiber
$0 \leq r \leq r_F$

Region III
CNT/Epoxy
Composite
$r_{II} \leq r \leq r_{III}$

Region IV
Epoxy
$r_{III} \leq r \leq r_{IV}$

0

0   r_I r_{II} r_{III} r_{IV}

Radial distance from carbon fiber, r (μ)

IV

III **II** **I**
Carbon
Fiber

Matrix

Lamina RVE
cross-section

Figure 2. Details of variations of CNT volume fraction in the representative volume element for a lamina with CNT-coated unidirectional carbon fibers

A typical representative volume element (RVE) is shown for a unidirectionally-reinforced lamina in Fig. 1. Details of the variations in the micro-structure resulting from coating the unidirectional carbon fibers with CNT are depicted in Fig. 2, along with details of the lamina RVE cross-section (1-axis, positive out-of-the-page). The carbon fiber and its surroundings are represented by four regions. The CNT volume fraction versus radial distance from the carbon fiber for each region is shown in Fig. 2. Region I is the carbon fiber itself, where r_F represents the carbon fiber radius. Region II represents the carbon fiber surface, and it has three components: the graphitic surface of the carbon fiber, carbon nanotubes and epoxy, and ranges from the carbon fiber radius at r_F to r_{II}, 0.004 microns from the carbon fiber. The CNT volume fraction in Region II is defined by the parameter V_o, shown in Fig. 2. Region III is the region surrounding the carbon fiber which is comprised of carbon nanotubes and epoxy. As depicted in Fig. 2, the CNT volume fraction in this region decays, from V_o to zero, as the radial distance from the carbon fiber increases. The width of Region III ranges from r_{II} to r_{III}, and is denoted by the parameter Δ, where $\Delta = r_{III} - r_{II}$. Region IV is the remaining epoxy matrix, and ranges from r_{III} to a maximum width denoted by parameter r_{IV}.

MULTI-SCALE MODEL

Molecular dynamics simulations

Representative volume elements (RVEs) of the molecular structure of the material system were generated via molecular dynamics (MD) simulation. In particular, three different systems with simulated with MD: the epoxy matrix (Fig. 3(a)), the epoxy matrix containing
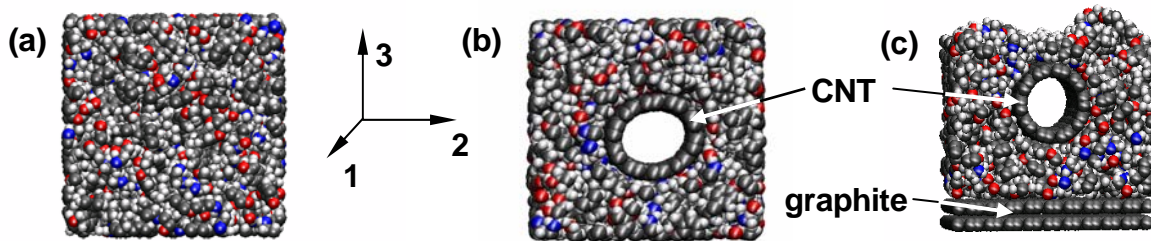
Figure 3. Molecular RVEs of (a) Epoxy, (b) epoxy nanotube composite, and (c) epoxy nanotube and graphite.

a nanotube (Fig. 3b), and the epoxy matrix containing a nanotube, but placed on a graphite surface (Fig 3(c)). The epoxy and the epoxy/nanotube were periodic in all three dimensions, and the three-component system was periodic in the 1- and 2- directions. In the 3-direction was periodic, but extended to 1 micron, and is, therefore, effectively an open boundary.

All three systems were simulated with the AMBER force field [9] using the LAMMPS [10] and DL-POLY [11] simulation codes. All the nanotube and graphite parameters were taken from the AMBER force field. Several of the force field parameters of the epoxy network were derived from *ab initio* calculations carried out with the NWChem package [12]. The partial atomic charges were derived from an RESP fit to a Hartree-Fock calculation of wavefunction. The bond lengths, angles, and dihedrals, were calculated by optimizing the geometry of parts of the epoxy network at the HF/STO-3G level. Partial charges were then fit at this geometry from a HF/6-31G* calculation. The rest of the parameters, were taken from the AMBER force field. In the simulations, electrostatic interactions were calculated with Coulomb's law, and an Ewald summation was used for the long range Coulombic interactions. Electrostatic interactions and 1-4 non-bonded dihedral interactions were scaled by the standard AMBER parameters of 0.83 and 0.50 respectively.

The molecular structure of the epoxy was a network of bisphenol F resin molecules reacted with epichlorohydrin and cross-linked via triethylenetetramine (TETA) molecules. The TETA molecule is able to cross-link with up to four resin chains, and on average 2.3 of the 4 TETA amine groups in the resultant structure were involved in cross-linking. The equilibrium structures were obtained by compressing the epoxy network until the minimum potential energy configuration at finite temperature (300 K) was reached. In the 3-component system, the epoxy was prepared with periodicity in the 1- and 2- directions, and was compressed between graphite plates. The upper graphite plate was then removed from the simulation, and the system was further equilibrated to minimize the potential energy.

Equivalent-Continuum Model

The elastic constants were then obtained for each of the molecular RVEs from equating the energies of deformation for the molecular system, which were calculated from molecular dynamics simulation, to the energies of deformation of an equivalent continuum solid under identical deformations. The material constitutive relation of stress σ and strain ε is given by Hooke's law

$$\sigma = \mathbf{C}\varepsilon. \tag{1}$$

The stiffness matrix C of an orthotropic system has 9 components:

$$\mathbf{C} = \begin{pmatrix} C_{11} & C_{12} & C_{13} & 0 & 0 & 0 \\ C_{12} & C_{22} & C_{23} & 0 & 0 & 0 \\ C_{13} & C_{23} & C_{33} & 0 & 0 & 0 \\ 0 & 0 & 0 & G_{23} & 0 & 0 \\ 0 & 0 & 0 & 0 & G_{13} & 0 \\ 0 & 0 & 0 & 0 & 0 & G_{12} \end{pmatrix} \tag{2}$$

The 9 components can be determined from the boundary conditions given in Ref. [2]. As in previous work [2], the axial stiffness C_{ii} and shear moduli G_{ij} were determined directly, and the stiffnesses C_{ij} were calculated from the plane strain bulk moduli K_{ij} and C_{ii}. For these cases, i and j are any of the 1-, 2- or 3- principal directions. The C_{ii} and K_{ij} were determined for all three systems. For the epoxy/nanotube system all nine constants were computed. The shear moduli of the remaining two systems were not needed for the model.

In the MD simulations, the displacement fields from Ref. [2] were applied to the each RVE structure in strain increments of 0.0025 every 10,000 steps at 1 fs each (10 ps per increment) up to a maximum strain of greater than 0.02. For the epoxy and epoxy/nanotube systems, application of the displacement field included displacing both the periodic boundaries and the atomic positions, then equilibrating the system with MD to its new state point. For the three-component system, the upper layer of the epoxy and the lower graphite sheet were fixed in location. The atoms in the fixed layers were displaced, but no further equilibration was performed on them.

Because of the limitation of rectilinear boxes in LAMMPS, DL-POLY was used for the shear moduli. Care was taken to translate the force field as accurately as possible between the codes, but some variation in the results is still expected.

Mori-Tanaka Micromechanics

The elastic constants determined for the molecular RVEs with the molecular dynamics/equivalent continuum method described above, are then used as input to the Mori-Tanaka micromechanics method to calculate the properties of an embedded epoxy/nanotube effective fiber in an epoxy matrix [13-15]. The stiffness tensor **C** of this nanocomposite as a function of effective fiber volume fraction v_f is

$$\mathbf{C} = \left((1-v_f)\mathbf{C}^m + v_f \mathbf{C}^f \mathbf{T}^f \right) \left((1-v_f)\mathbf{I} + v_f \mathbf{T}^f \right)^{-1} \tag{3}$$

where the dilute strain concentration tensor $\mathbf{T}^f$ is

$$\mathbf{T}^f = \left[\mathbf{I} + \mathbf{S}^f \left(\mathbf{C}^m \right)^{-1} \left(\mathbf{C}^f - \mathbf{C}^m \right) \right]^{-1} \tag{4}$$

and $\mathbf{S}^f$ is the Eshelby tensor for a prolate ellipsoid [16] with aspect ratio 1:1000. The superscripts and subscripts f and m refer to the effective fiber and matrix properties, respectively, and $\mathbf{I}$ is the identity tensor. The v_f is related to the nanotube volume fraction v_{NT} as

$$v_{NT} = v_{NT,RVE} v_f \tag{5}$$

where $v_{NT,RVE}$ is the volume fraction of nanotubes in the molecular RVE. In equation (3) the stiffness matrix C is calculated for aligned effective fibers. To randomize the orientation of the effective fibers in the nanocomposite[2,17], and therefore the nanotubes, the components of $\mathbf{C}$ are

$$\langle C_{ijmn} \rangle = \left(\kappa - \frac{2}{3}\mu \right)\left(\delta_{ij}\delta_{mn} \right) + \mu\left(\delta_{is}\delta_{jn} + \delta_{in}\delta_{jm} \right) \tag{6}$$

where $i,j,m,n = 1,2,3$, δ_{ij} is the Kronecker delta and

$$\kappa = \frac{1}{9}C_{iijj}$$

$$\mu = \frac{1}{10}\left(C_{ijij} - \frac{1}{3}C_{iijj} \right) \tag{7}$$

With the randomization of the effective fibers, $\mathbf{C}$ becomes isotropic.

Distribution of Nanotubes

The Mori-Tanaka analysis yields the modulus of the nanocomposite at different nanotube loadings, but a description of the spatial distribution of the nanotubes around the carbon fiber must also be defined. The nanotube distribution can be described by using the following exponential form:

$$v_d(r,\alpha) = V_o e^{-\alpha(r-r_{II})} - \left(\frac{r - r_{II}}{\Delta} \right)V_o e^{-\alpha\Delta}. \tag{8}$$

where, v_d is the volume fraction distribution; the parameter r measures radial distance from the center of the carbon fiber; V_o is the initial CNT-epoxy volume fraction of the molecular RVE; and Δ denotes the width of the region in which the nanotubes are distributed. In the present analysis, a value for Δ was specified, and the following constraint equation was solved for successive values of the decay parameter α using Mathematica™[18]

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$$\sum_i^N v_d(r_i,\alpha) \int_{r_i}^{r_{i+1}} 2\pi r dr = V_N \cdot A. \tag{9}$$

Here, V_N denotes the lamina volume fraction, A, the lamina RVE surface area in the 2-3 plane, shown in Fig. 2, and N, the number of subregions of Region III. The value of α that satisfies the equality of Eqn (9), for a given value of V_N, is then applied in the relation of Eqn (8) to define the distribution of CNT volume fractions Region III for width Δ.

Atomistically-Informed Rule-of-Mixtures Analysis

The contribution to the longitudinal Young's modulus of the lamina, E, from each of the four regions shown in Fig. (2) is then determined by using an atomistically-informed rule-of-mixtures analysis:

$$E = v_I E_I + v_{II} E_{II} + v_{III} E_{III} + v_{IV} E_{IV}. \tag{10}$$

where, v_i and E_i are the volume fraction and Young's modulus of each of the 4 regions. For the present analysis, v_I represents the carbon fiber volume fraction, and is fixed at 60 %. The Young's modulus of the carbon fiber, E_I, is 230 GPa. For the present analysis, the volume fraction v_{II} is fixed by setting the value of r_{II} at 0.004 microns. The Young's modulus E_{II} is calculated from the **C** tensor of the three component molecular RVE, shown in Fig 3c, resulting from the molecular dynamics/equivalent continuum method. The contributions of v_3 and E_3 are variable. In Region III the nanotube distribution varies according to Eqns (8) and (9). The variation of the modulus in Region III is taken from the properties derived by mapping the results of the Mori-Tanaka micromechanics model the CNT volume fraction distributions from Eqns (8) and (9). Finally, the Young's modulus and volume fraction for Region IV, E_{IV} and v_{IV} respectively, are calculated from the **C** tensor for the epoxy molecular RVE (Fig 3(a)) .

RESULTS AND DISCUSSION

The elastic constants of the molecular RVEs determined from the molecular dynamics simulations and the equivalent continuum model are listed in Table I. The epoxy elastic constants yield a Young's modulus of 1.44 GPa and a Poisson ratio of 0.42. These values are used for the epoxy matrix in the present analysis. Typical values for storage moduli of neat cured epoxy are 2-3 GPa at 250-300 K [19]. The volume fraction of nanotubes in the epoxy/nanotube system was 15.35%, and in the epoxy/nanotube/graphite system, 15.55 %.

Using the nanotube/epoxy composite properties presented in Table I and the properties of the epoxy matrix, the Young's modulus of the nanocomposite with randomized effective epoxy/nanotube fibers is plotted in Fig 4 as a function of nanotube volume fraction. These results are generated using the Mori-Tanaka micromechanics from eqns (3)-(7).

Table I- The Elastic Constants of the Molecular RVEs.

| Elastic Constants	Epoxy (GPa)	Epoxy/Nanotube (GPa)	Epoxy/Nanotube/Graphite (GPa)
C_{11}	4.12	99.0	267
C_{22}	5.05	9.43	182
C_{33}	3.60	6.22	9.94
K_{12}	4.78	31.9	138
K_{13}	4.73	32.4	72.2
K_{23}	4.41	12.1	49.5
G_{12}		0.33	
G_{13}		0.32	
G_{23}		0.20	
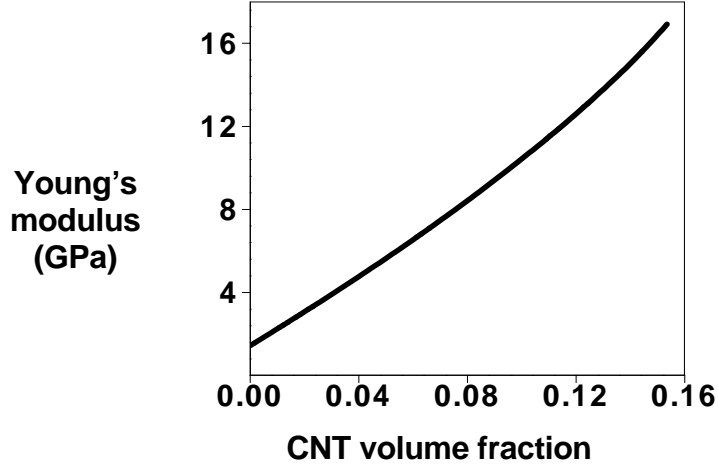
Figure 4. Young's modulus of the epoxy/CNT composite from Mori-Tanaka micromechanics

Fig 5(a) shows variations in CNT volume fraction distributions of exponential form for a lamina RVE with 60% carbon fiber volume fraction and $\Delta = 0.3$ microns. Here, volume fraction variations from Eqns (8) and (9) are depicted for lamina CNT volume fractions ranging from 0.0005 to 0.0055. The exponential form allows the CNT volume fraction distribution to vary from a nearly linear form as shown for $V_N = 0.0055$ through increasingly exponentially varying forms for decreasing values of lamina CNT volume fraction, to a nearly stepwise variation at $V_N = 0.0005$.

Fig 5(b) shows the variations in Young's modulus for Region III. Results are shown for selected nanotube distributions from Fig 5(a). Here, Mori-Tanaka micromechanics have been applied using volume fraction distributions for lamina volume fractions 0.0055, 0.0025, and 0.0005, where $\Delta = 0.3$ microns. The Young's modulus distributions of Fig 5(b) are used directly in the atomistically-informed rule-of-mixtures analysis to represent the contribution of Region III to the constitutive properties of the lamina.
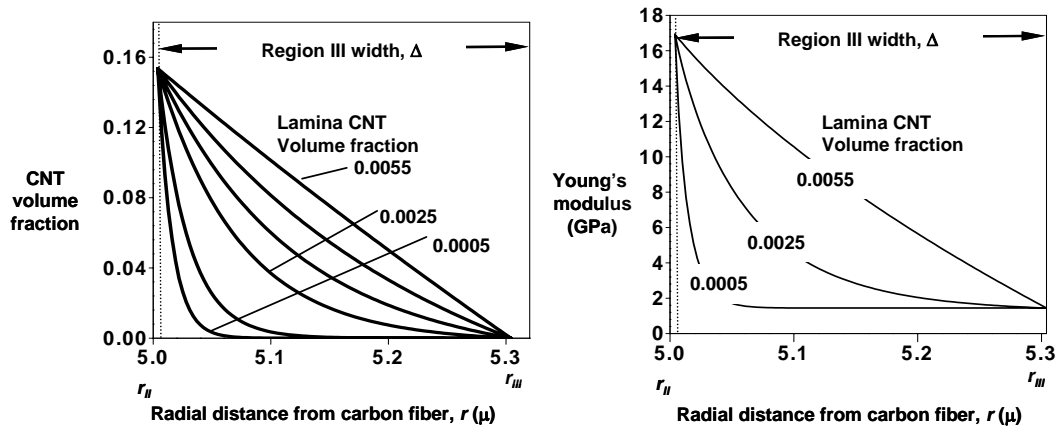
Figure 5. (a) CNT volume fraction distribution in Region III and (b) Young's modulus distribution in Region III, for $\Delta = 0.3$.

Finally, the total longitudinal Young's modulus of the unidirectionally-reinforced lamina with CNT is plotted in Fig. 6 for different sizes of Region III (Fig. 2). For nanotubes within approximately 700 nm of the carbon fiber surface the Young's modulus varies about 0.01 GPa with changes to the size of Region III. The predominant change in the Young's modulus of the coated nanotube fiber is a function of the nanotube volume fraction in the lamina. Up to nanotube loadings of 0.0125, the amount of change in the modulus is 1.2 GPa.

CONCLUSIONS

A multi-scale method, denoted the atomistically-informed rule-of-mixtures, is developed to calculate the Young's modulus of a carbon nanotube coated carbon fiber.
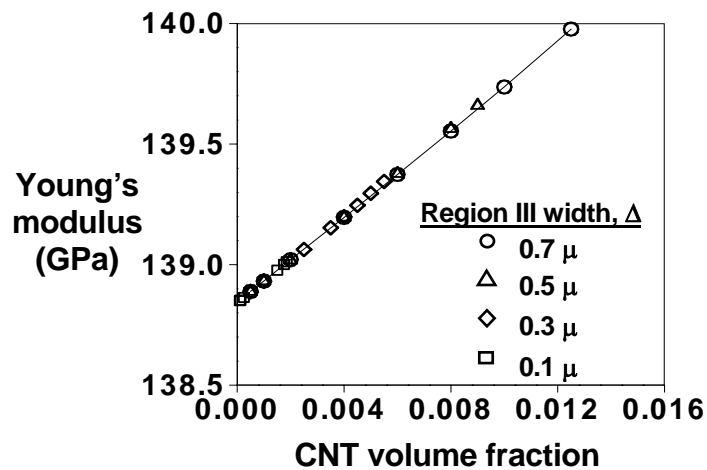
Figure 6. Atomistically informed rule-of-mixtures results for unidirectionally-reinforced lamina with CNT-coated carbon fibers.

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Within the method, the distribution of nanotubes in the vicinity of the carbon fiber surface can be varied as a function of nanotube volume fraction. For a lamina with 60% carbon fiber volume fraction, the results indicate that the Young's modulus is less dependent on the local nanotube disribution than on the nanotube volume fraction for nanotube located within 700 nm of the carbon fiber and nanotube loadings in the lamina of up to 1.25 vol %.

ACKNOWLEDGMENTS

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