Motor Control of Two Flywheels Enabling Combined Attitude Control and Bus Regulation

Barbara H. Kenny

21 April 2004

Presented at the 2004 Space Power Workshop

This presentation discussed the flywheel technology development work that is ongoing at NASA GRC with a particular emphasis on the flywheel system control. The "field orientation" motor/generator control algorithm was discussed and explained. The position-sensorless angle and speed estimation algorithm was presented. The motor current response to a step change in command at low (10 kRPM) and high (60 kRPM) was discussed. The flywheel DC bus regulation control was explained and experimental results presented. Finally, the combined attitude control and energy storage algorithm that controls two flywheels simultaneously was presented. Experimental results were shown that verified the operational capability of the algorithm.

Overall, the presentation demonstrated that GRC has an operational facility that shows high speed flywheel energy storage (60,000 RPM) and the successful implementation of an algorithm to simultaneously control both energy storage and a single axis of attitude with two flywheels.

Motor Control of Two Flywheels Enabling Combined Attitude Control and Bus Regulation

Dr. Barbara Kenny
Presented at the Space Power
Workshop
21 April 2004

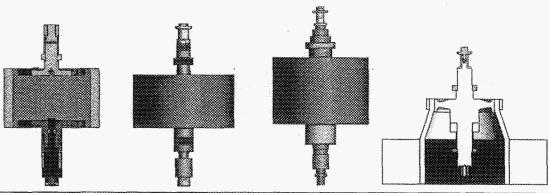


Outline of Presentation

- NASA GRC flywheel development
- NASA GRC flywheel test facility
- Control algorithms
- Motor control
- Full speed/power bus regulation
- Single axis attitude control and bus regulation
- Conclusions and future work



NASA GRC Flywheel Research



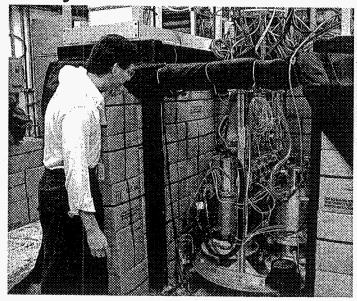
Flywheel Unit	HSS	Dev1	D1	G2	G3
Rotor	Steel Hub	Single Layer	Multilayer	Multilayer	Composite
Composition	Steel Hub	Composite	Composite	Composite	Arbor
Energy	17 wt-hr	300 wt-hr	350 wt-hr	581 wt-hr	2136 wt-hr
Specific Energy	1 W/kg	23 W/kg	20 W/kg	26 W/kg	80W/kg
Motor/Generator	PM 4 pole 165 Vrms 1-1 active cooling	PM 4 pole 165 Vrms 1-1 active cooling	PM 2 pole 80 Vrms 1-1 active cooling	PM 2 pole 80 Vrms 1-1 active cooling	PM 4 pole 60 Vrms 1-1 passive cooling
Magnetic	PM bias 4 pole	PM bias 4 pole no redundancy	PM bias 4 pole	radial	Radial+Combo PM bias 6 pole radial & axial redundancy 80lbf (356N)
Peak Tip Speed	Control XX XX State and the rest of the Control State of the Control Sta	A STANKEN OF STANKEN THE STANKEN AND STANKEN WAS AND AND STANKEN THE STANKEN THE STANKEN AND STANKEN A	750 m/s	750 m/s	1100 m/s
Operational Speed Range	0-60 krpm	20-60 krpm	20-60 krpm	20-60 krpm	25-50 krpm

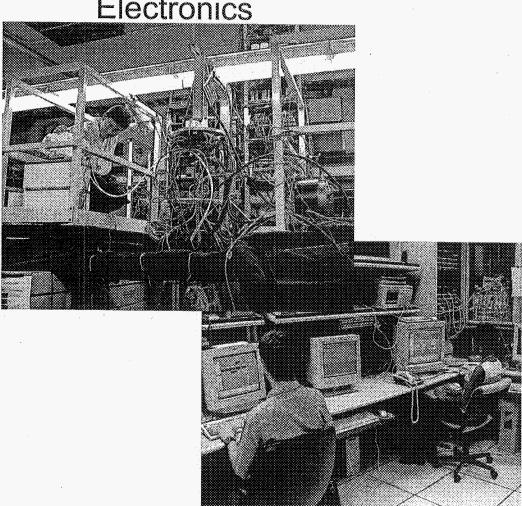


Dual Flywheel Test Facility

Electronics







Control Room

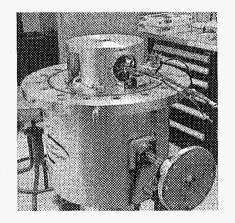
Glenn Research Center

Flywheel Modules

- D1 Flywheel Module
 - Rotor
 - 350 Whr Toray 4 ring rim
 - Monolithic steel hub
 - Motor/Generator
 - 1kW, 80V I-I, 2 pole Ashman Technology
 - Magnetic Bearings

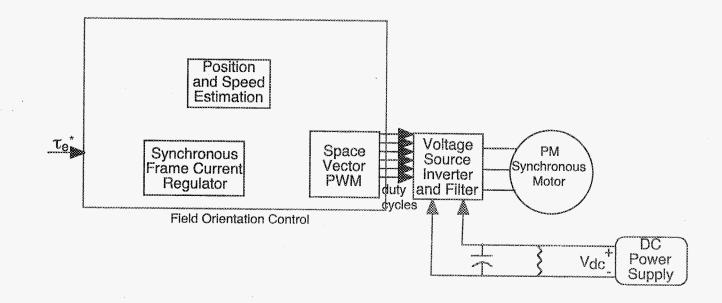
Glenn Research Center

- High Speed Shaft
 - Rotor
 - 17 Whr no rim
 - Monolithic steel hub
 - Motor/Generator
 - 3kW, 220V I-I, 4 pole Ashman Technology
 - Magnetic Bearings

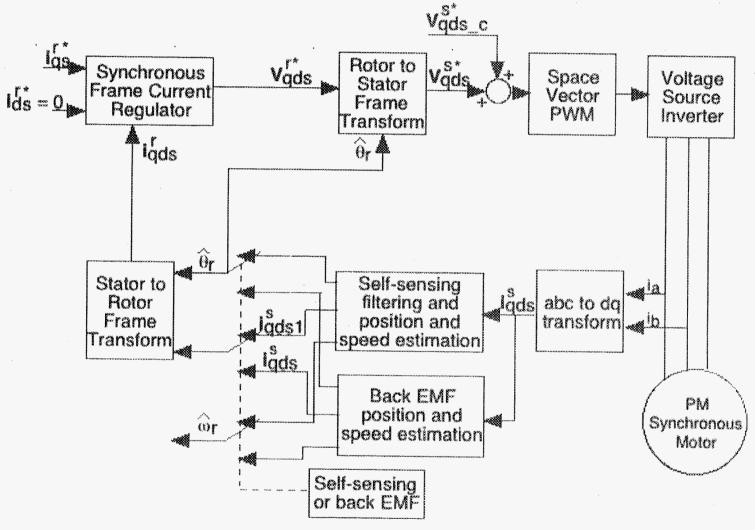




Motor and Flywheel Control Algorithms



Motor Control

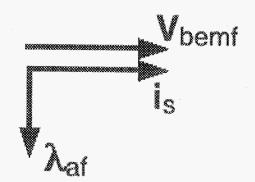




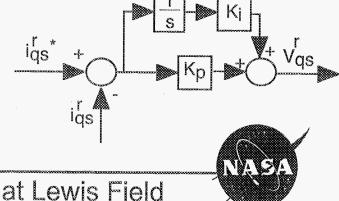
Field Orientation (Vector Control)

- Control motor current relative to rotor magnetic flux
 - Stator current vector perpendicular to rotor flux vector and in phase with back EMF voltage
- Control done in rotor reference frame
 - Control variables become dc quantities:
- Motor torque

$$\tau = \frac{3}{2} \frac{P}{2} i_{qs}^r \lambda_{af} \text{ if } i_{ds}^r = 0$$



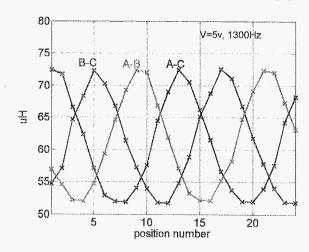
- Similar to dc motor control
- Fast torque response
- Currents regulated using PI controllers in rotor reference frame
 - Synchronous frame current regulator
 - Bandwidth ~1kHz
- Needs rotor position information Glenn Research Center

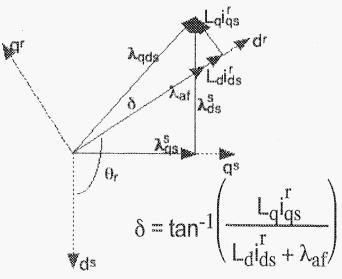


Sensorless Control

Motor Inductance

- Rotor position and speed are estimated
- Signal injection technique for starting and low speed
 - High frequency voltage added to fundamental
 - Position information contained in resulting high frequency current
 - Requires magnetic saliency on rotor
- Back EMF technique for higher (operational) speed
 - Stator flux vector determined from integrating the motor phase voltage
 - Rotor flux related to stator flux through machine inductances and phase currents

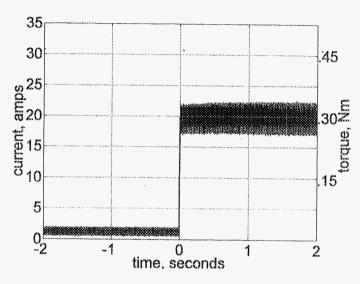




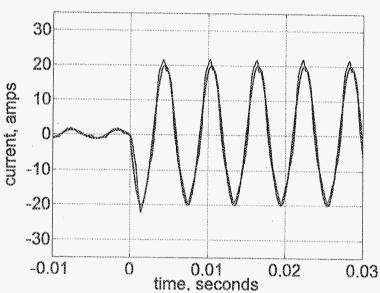


Current Regulation: 10 krpm

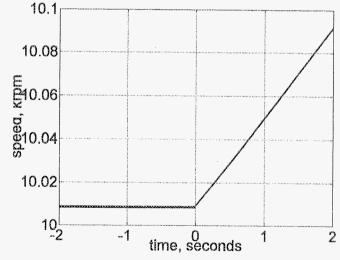
Current
Magnitude
and
Torque
Response



Motor Phase Current



Flywheel speed



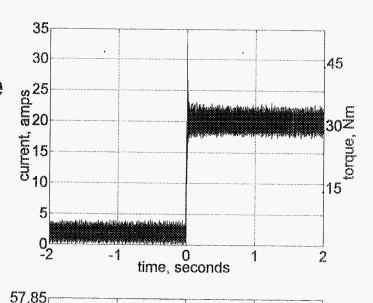
1 kHz torque response

Glenn Research Center

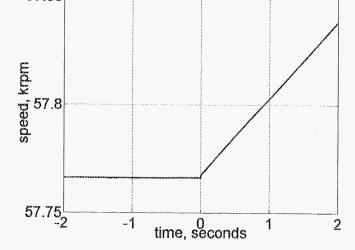


Current Regulation: 60 krpm

Current
Magnitude
and
Torque
Response

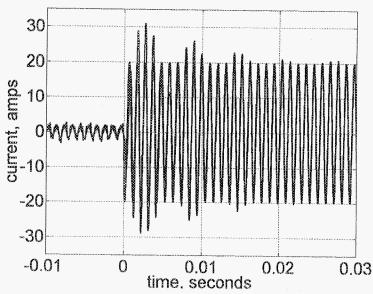






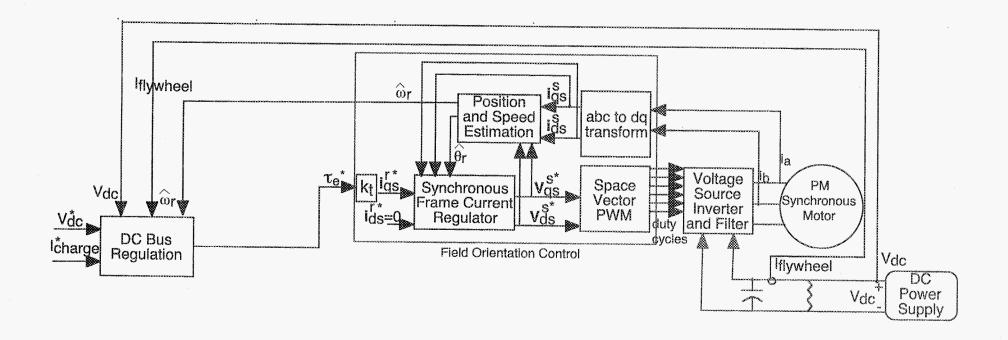
Glenn Research Center

Motor Phase Current



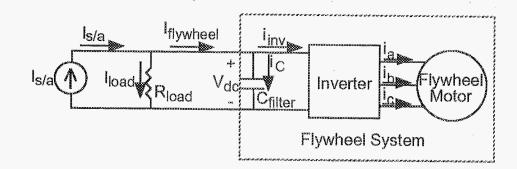
- Regulates current but oscillatory response
- Improvements
 - Back EMF decoupling
 - Include dynamics of AC filter
 - Include sampling delay

Motor and Flywheel Control Algorithms



Flywheel Bus Regulation Control

- Charge
- Charge Reduction
- Discharge

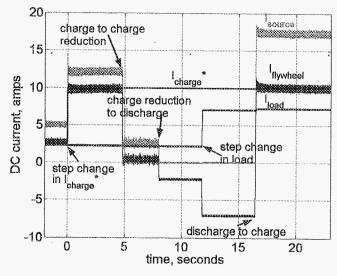


Mode	Current	DC Bus Voltage
Full Sun "Charge"	$I_{\rm S/a} = I_{ m load} + I_{ m charge}^*$ $I_{ m flywheel} = I_{ m charge}^*$	Regulated by solar array system
Partial Sun "Charge Reduction"	$I_{ m load} + I_{ m charge}^* > I_{ m S/a} > 0$ $I_{ m charge}^* > I_{ m flywheel}$	Regulated by flywheel system
Eclipse "Discharge"	$I_{ m load}$ = - $I_{ m flywheel}$ $I_{ m flywheel}$ < 0	Regulated by flywheel system

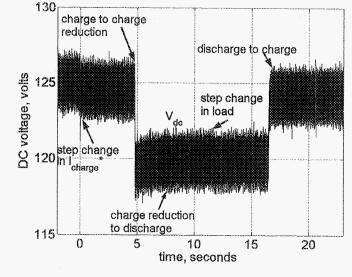


Experimental Results

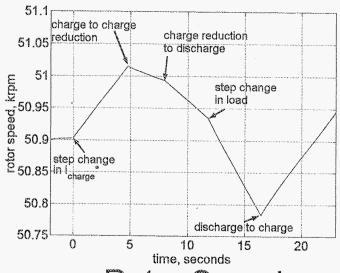




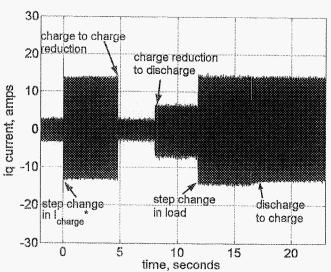
DC Bus Voltage



Glenn Research Center



Rotor Speed

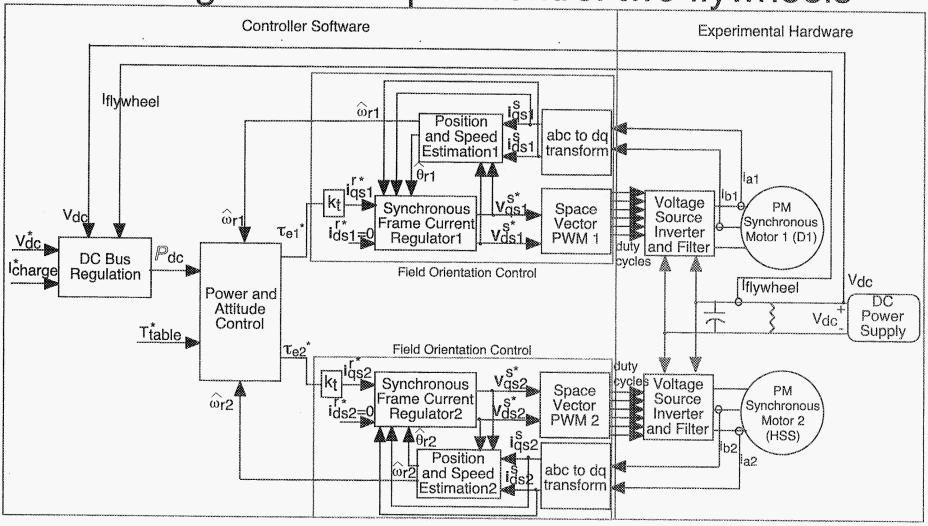


Phase Current



Attitude Control and Bus Regulation

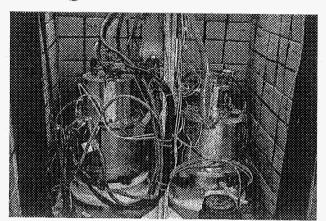
Change outer loop to control two flywheels

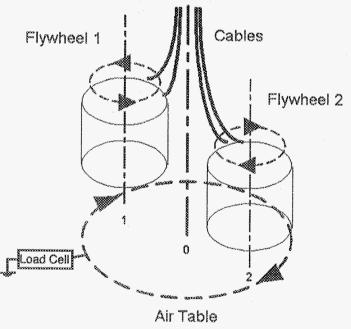




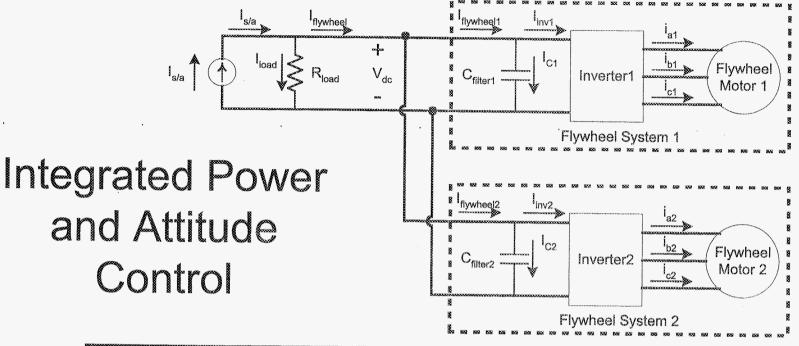
Attitude Control and Bus Regulation

- Single axis system
- Objective: control axial torque and DC power simultaneously.
 - DC power command results from DC bus regulation algorithm
- Commanded table torque and DC power translated to two motor current commands.





Glenn Research Center



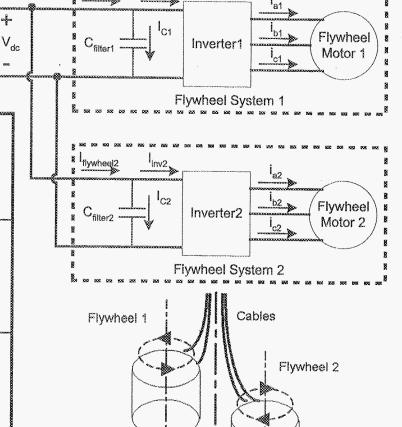
<u>Mode</u>	<u>Current</u>	DC Bus Voltage
Full Sun "Charge"	$I_{\text{S/a}} = I_{\text{load}} + I_{\text{charge}}^*$ $I_{\text{flywheel}} = I_{\text{charge}}^*$	Regulated by solar array system
Partial Sun "Charge Reduction"	$I_{\mathrm{load}} + I_{\mathrm{charge}}^* > I_{\mathrm{s/a}} > 0$ $I_{\mathrm{charge}}^* > I_{\mathrm{flywheel}}$	Regulated by flywheel system
Eclipse "Discharge"	I _{load} = - I _{flywheel} I _{flywheel} < 0	Regulated by flywheel system

Glenn Research Center

IPAC Experimental Results

Open loop torque control

B553858880555538000000000000000000000000	*	
Power Regulation Mode	Table Torque Command (N-m)	Load
Test 1: Charge → Discharge	T* = 0	300 Ω → 120 Ω
Test 2: Charge	T* = 0→-0.5 →0	300 Ω
Test 3: Discharge	T* = 0→+0.5 →0	300 Ω



Glenn Research Center



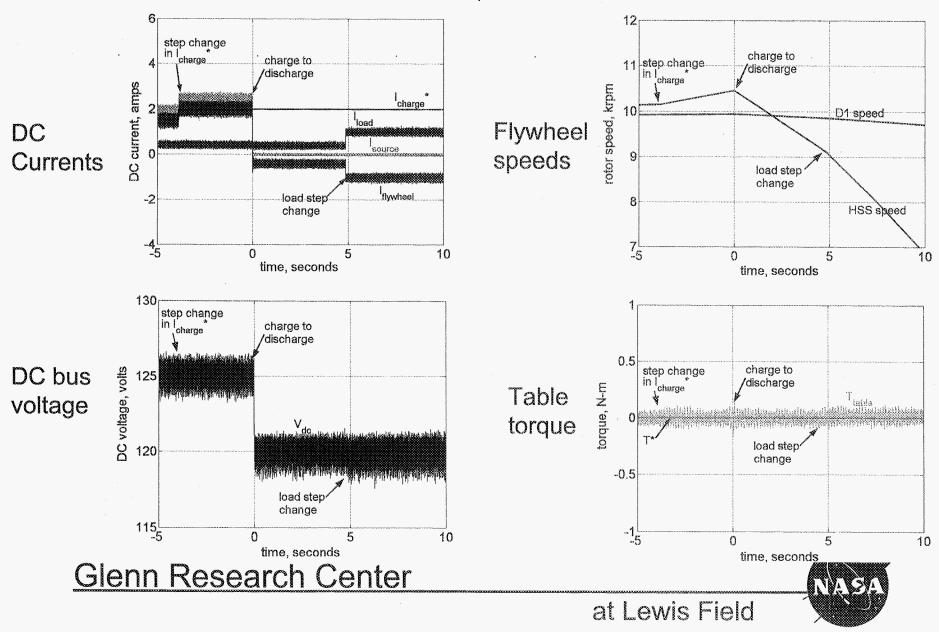
Air Table

Load Cell

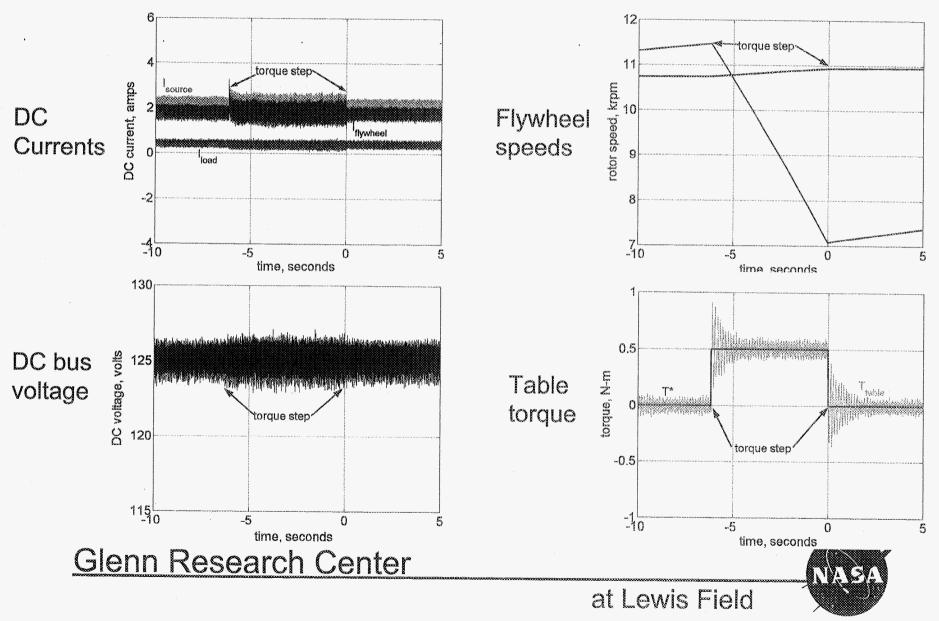
a flywheel1

flywheel

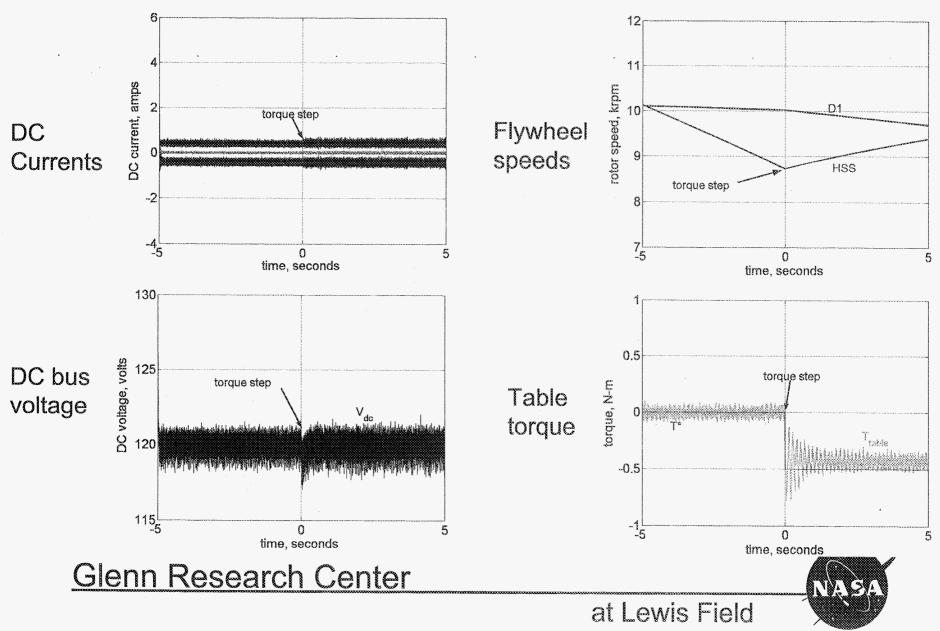
Test 1: Charge to discharge mode with a constant torque command



Test 2: Charge mode with a step change in torque command



Test 3: Discharge mode with a step change in torque command



Conclusions

- PM machine with field orientation control and sensorless position and speed estimation enables high performance flywheel outer loop control.
- NASA GRC has demonstrated single axis combined attitude control and bus regulation (IPAC) using two flywheels.
 - Single axis torque and DC power can be independently controlled and regulated.
 - DC bus voltage is accurately regulated by flywheels during discharge during load and/or torque steps.



Future Work

- NASA GRC and Lockheed Martin are building a two axis, three flywheel combined attitude control and bus regulation system (COMET).
 - Testing this summer at GRC
- NASA GRC will replace the high speed shaft with G-2 flywheel for full speed demonstration of single axis combined attitude control and bus regulation.
 - Testing this summer at GRC
- Working to move motor control and magnetic bearing algorithms to FPGAs.

