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1-D Transient Thermal Modeling of an Ablative Material (MCC-1)
Exposed to a Simulated Convective Titan IV Launch Environment

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OUTLINE

- Introduction
- Testing
- Transient Thermal Analysis
- Results
- Summary and Conclusions



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INTRODUCTION

Purpose of work is to demonstrate flat test panel substrate temperatures consistent with analysis predictions

Testing performed in aerothermal facility

MCC-1 on aluminum substrate



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Testing

- Performed in IHGF facility
- Calibration runs define aerothermal heating environment
- Three different MCC-1 thicknesses tested



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TESTING (Continued)

Bare MCC-1 Test Matrix

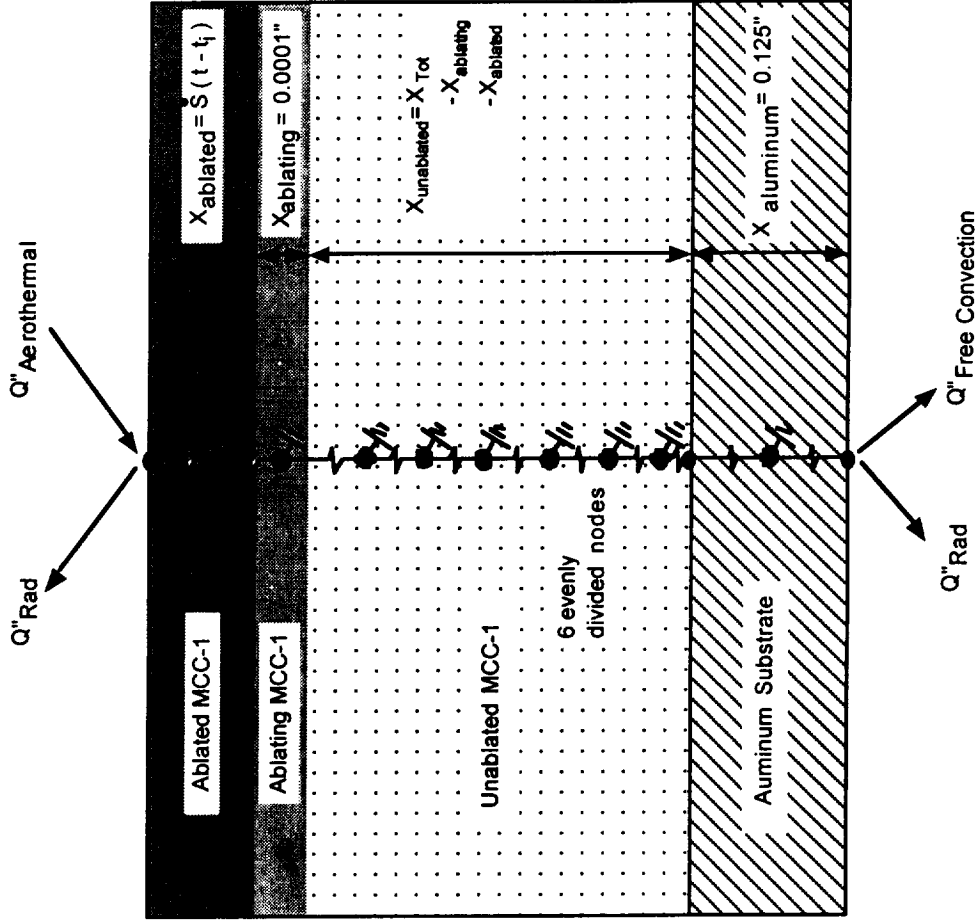
| Test Series | Cold Wall Heat Flux (Btu/s/ft ²) | Test Run Length (s) | Aluminum Substrate Thickness (in) | MCC-1 Thickness (in) |
|-------------|--|---------------------|-----------------------------------|----------------------|
| T96-690 | 4.6 | 114 | 0.125 | 0.158 |
| T96-693 | 4.6 | 114 | 0.125 | 0.158 |
| T96-697 | 4.6 | 114 | 0.125 | 0.056 |
| T96-699 | 4.6 | 114 | 0.125 | 0.056 |
| T96-684 | 4.6 | 200 | 0.125 | 0.344 |
| T96-686 | 4.6 | 200 | 0.125 | 0.343 |



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TRANSIENT THERMAL MODEL



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TRANSIENT THERMAL MODEL

(Continued)

- Key assumptions
 - ⇒ 1-D heat transfer
 - ⇒ Constant ablation recession rate (determined from pre- and post-test measurements)
 - ⇒ Ablation temperature 540°F
 - ⇒ Char left behind ablation front
 - ⇒ Temperature Jump Correction for Incident Heat Transfer Coefficient

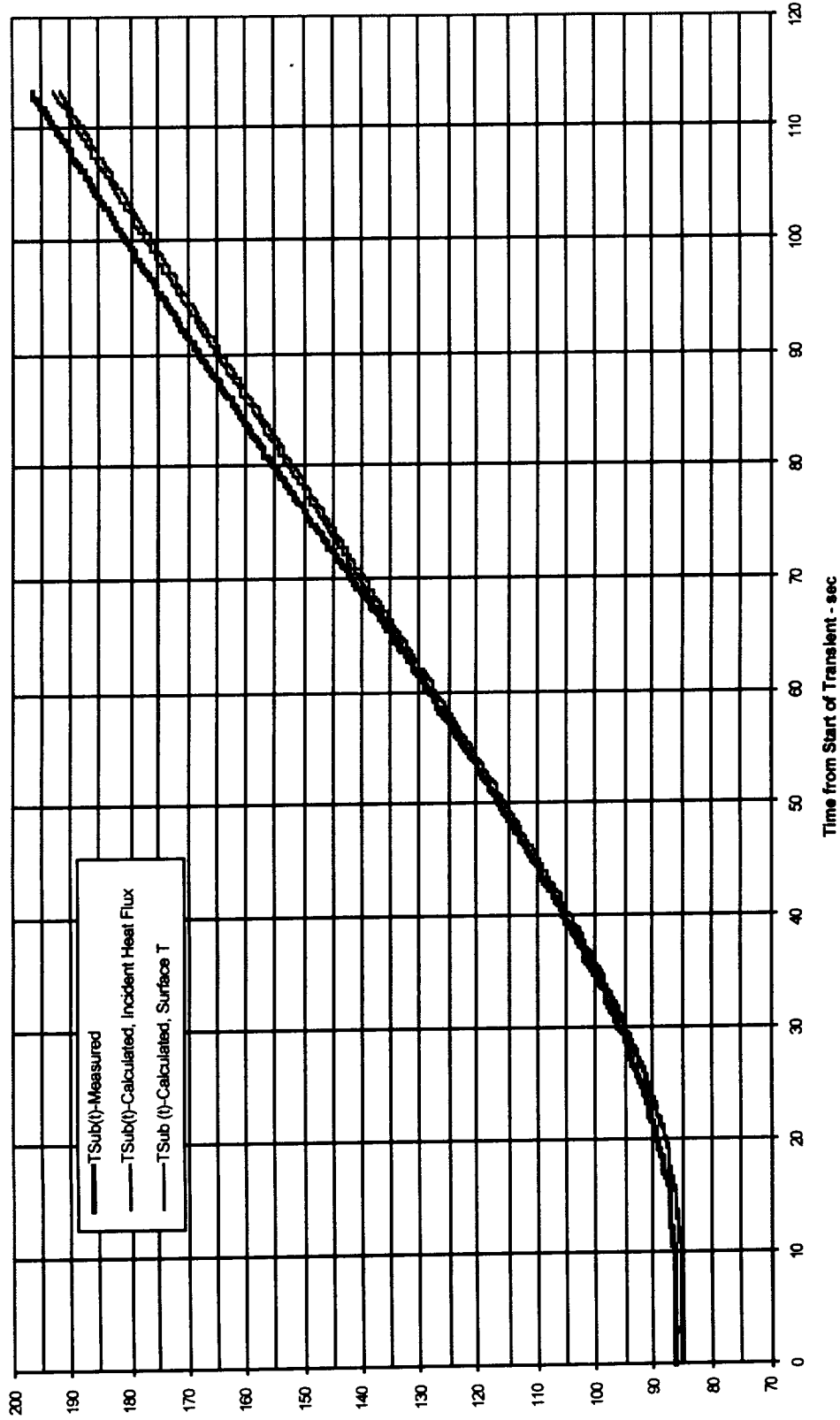


TRANSIENT THERMAL MODEL (Continued)

- Two Methods Used to Model Heating of Bare MCC-1
 - ⇒ Directly Input Surface Temperature as a Function of Time, $T_s(t)$, from IR Measurement
 - ⇒ Aerothermal Heating Using Calibration Plate Data, Subtracting Radiation Losses to Tunnel Walls

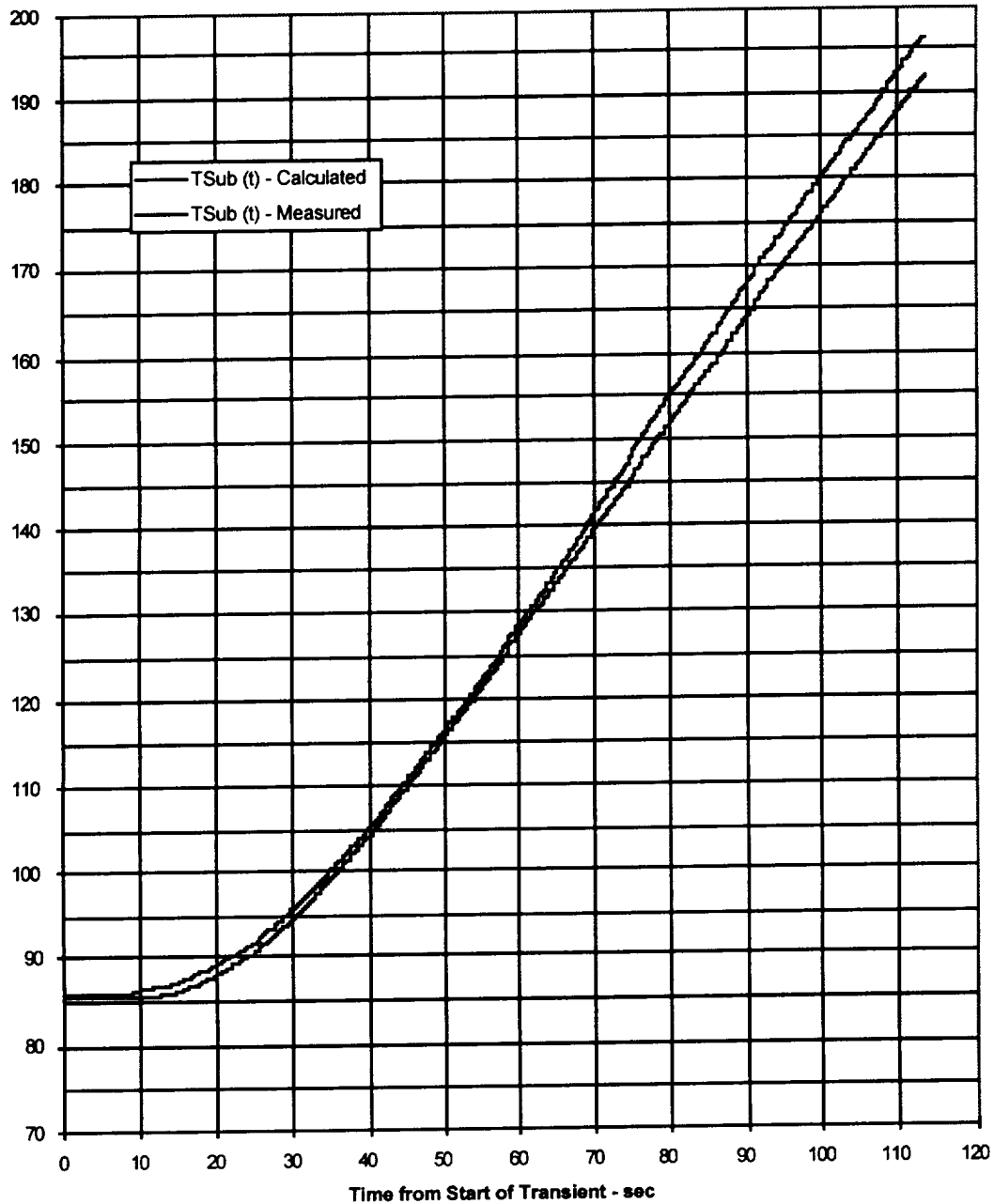


RESULTS

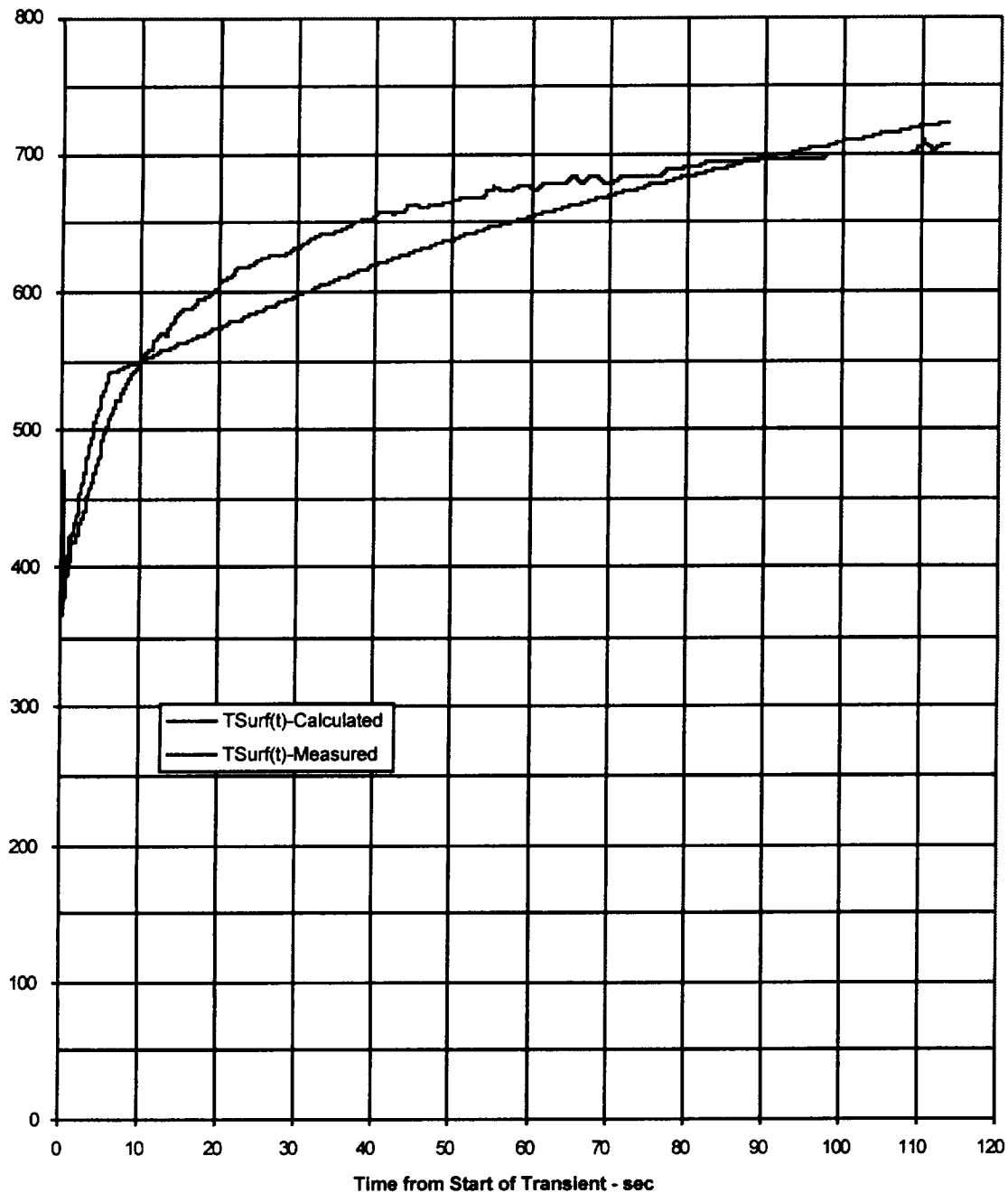


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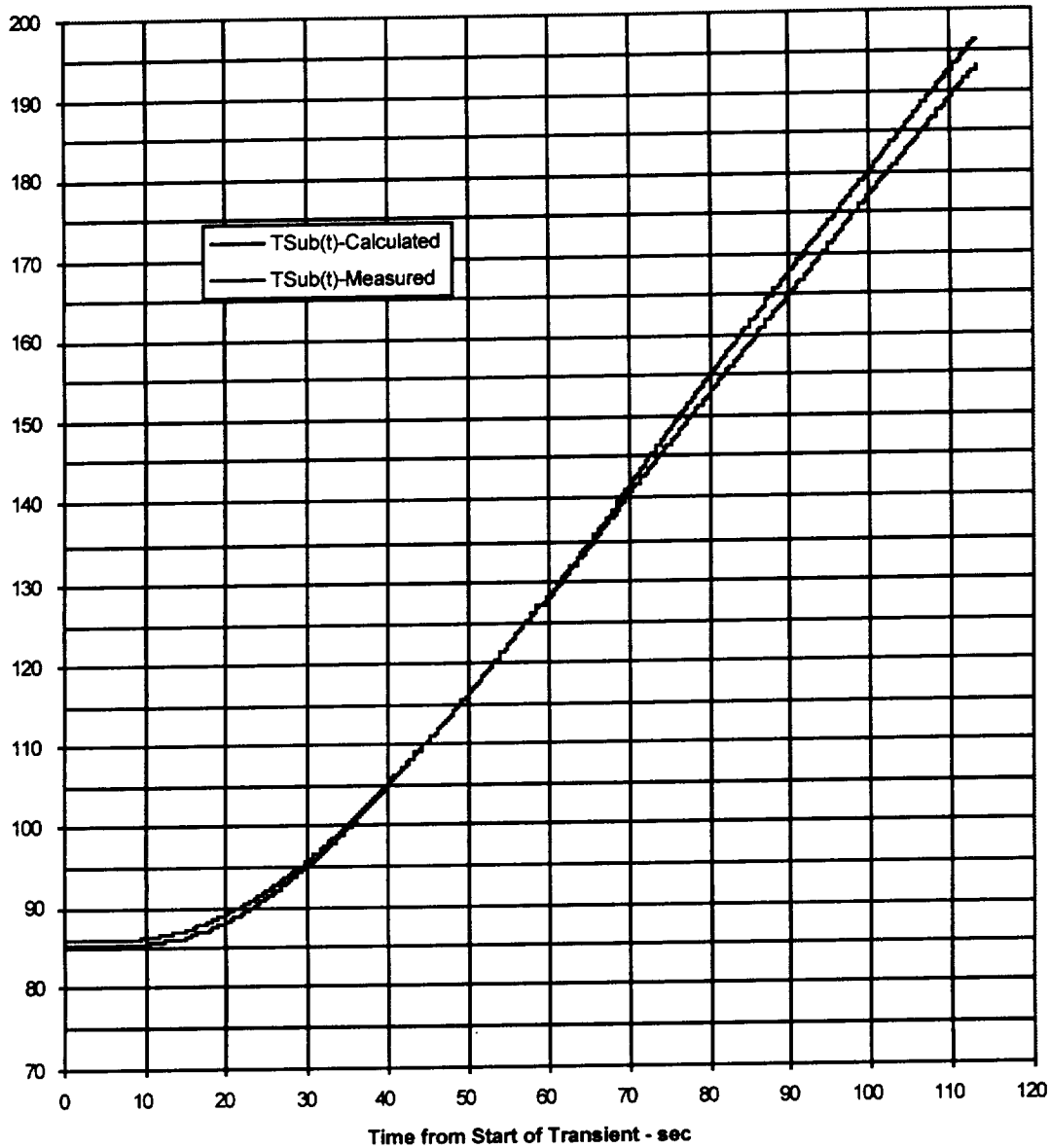
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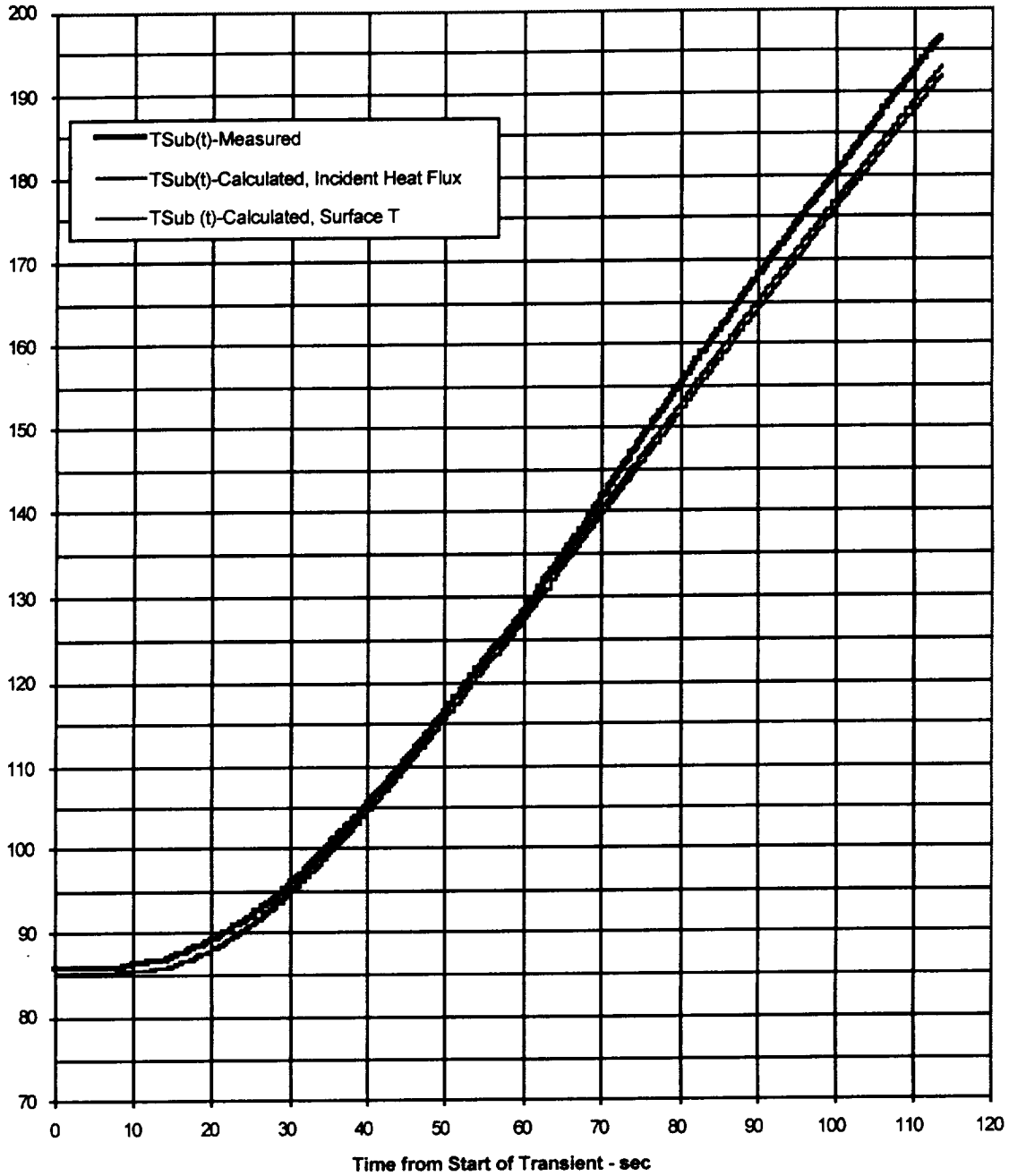
Comparison of $T_{sub}(t)$ Measured and Predicted Values with Imposed $T_{surf}(t)$ Boundary Conditions ($q''_{cw} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.158 in.)



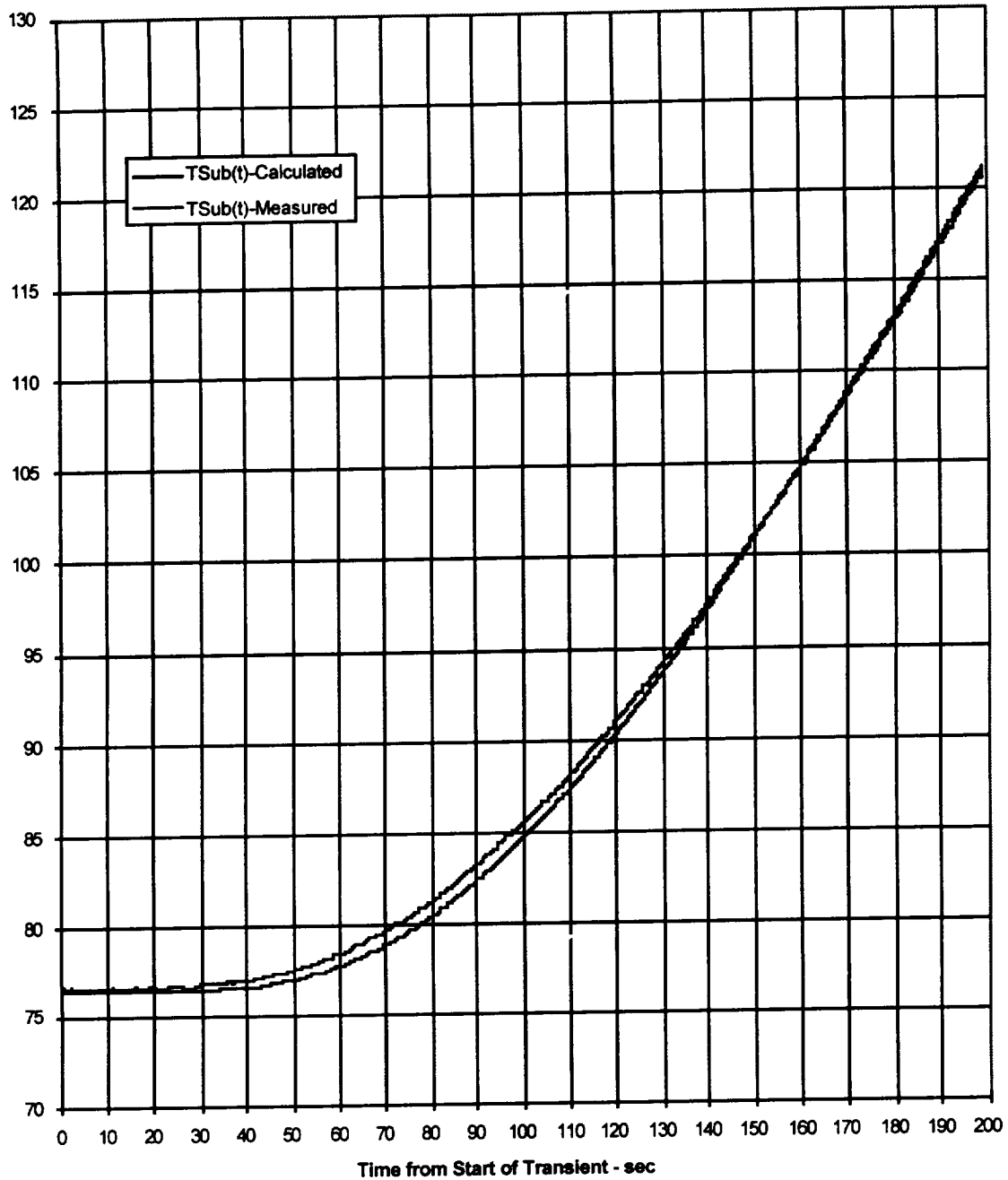
Comparison of T_{surf} (t) Measured and Calculated Values with Incident Heat Flux Conditions Specified from Calibration Testing
 (q''_{cw} = 4.6 Btu/s/ft², Al thickness = 0.125 in., MCC-1 thickness =0.158 in.)



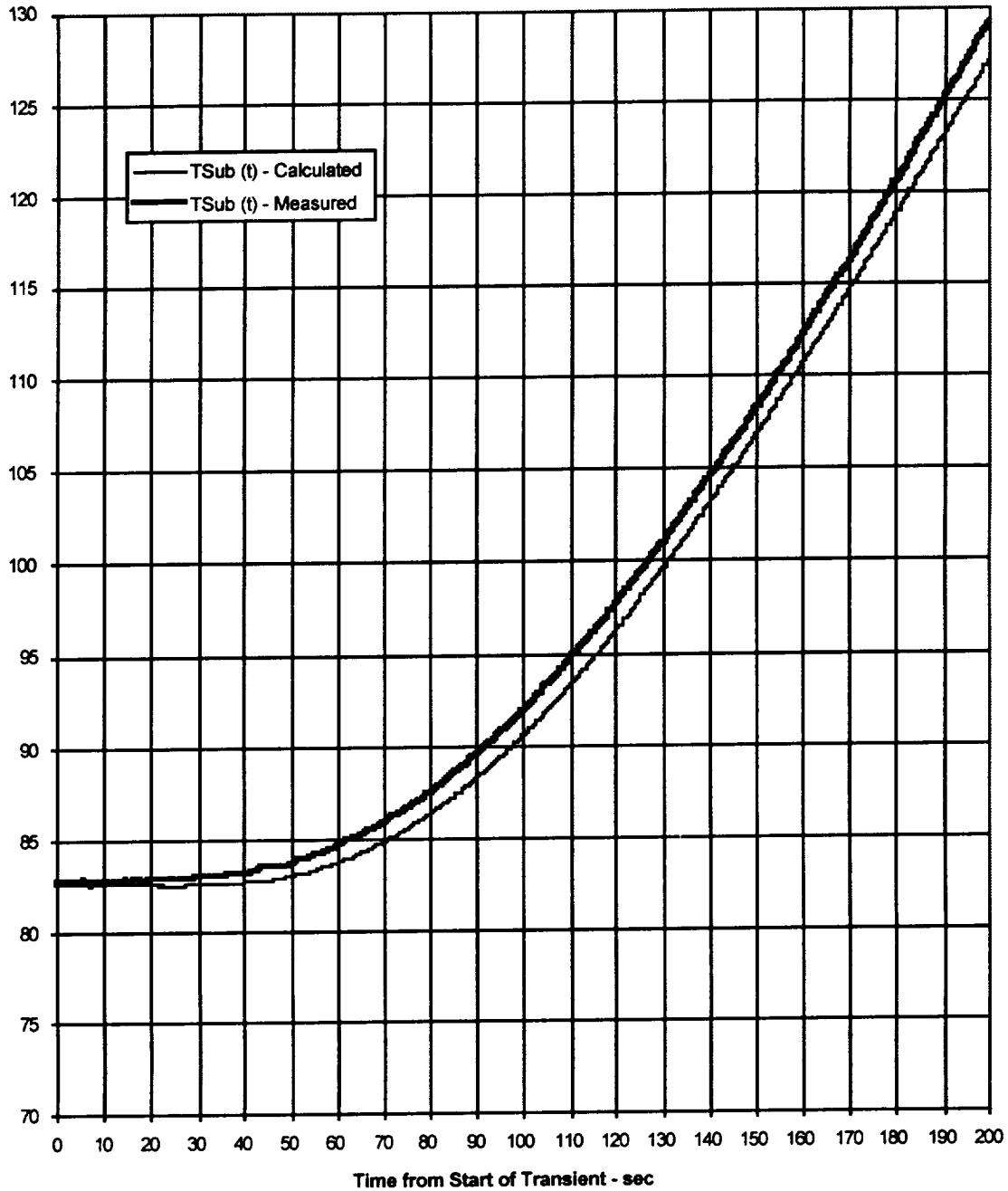
Comparison of $T_{sub}(t)$ Measured and Calculated Values with Incident Heat Flux Conditions Specified from Calibration Testing ($q''_{cw} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.158 in.)



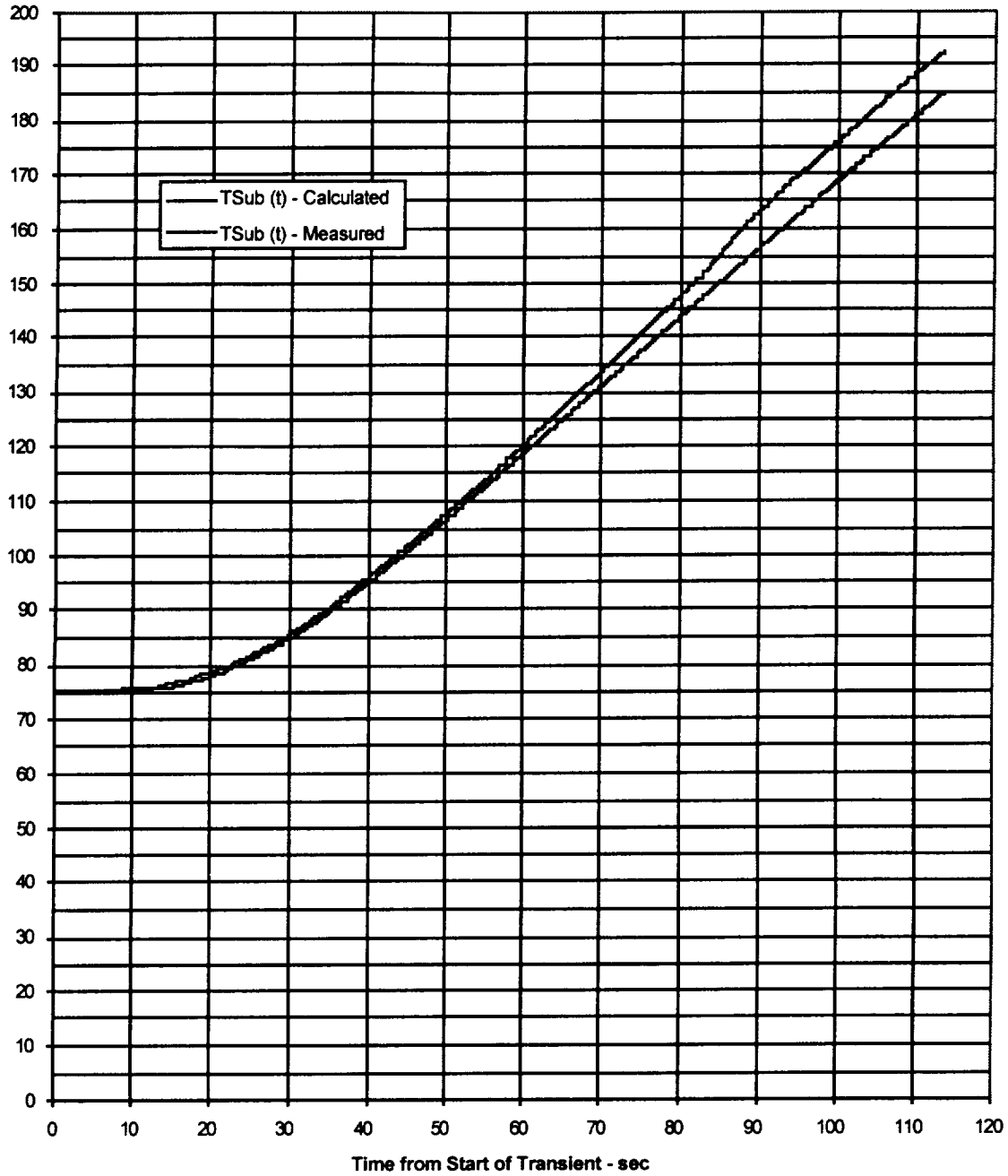
Comparison of Predicted Aluminum Substrate Temperatures Using Both the Imposed $T_{\text{Surf}}(t)$ and the Incident Heat Flux Boundary Conditions
 ($q''_{\text{cw}} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.158 in.)



Comparison of $T_{sub}(t)$ Measured and Calculated Values with Incident Heat Flux Conditions Specified from Calibration Testing
 ($q''_{cw} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.344 in.)



Comparison of T_{Sub} (t) Measured and Calculated Values for Incident Heat Flux Conditions Specified from Calibration Testing
 ($q''_{cw} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.343 in.)



Comparison of $T_{Sub}(t)$ Measured and Calculated Values Incident Heat Flux Conditions Specified from Calibration Testing
 ($q''_{cw} = 4.6 \text{ Btu/s/ft}^2$, Al thickness = 0.125 in., MCC-1 thickness = 0.158 in.)