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## Roth

#### [54] PULSE-ECHO ULTRASONIC IMAGING METHOD FOR ELIMINATING SAMPLE THICKNESS VARIATION EFFECTS

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- [73] Assignee: The United States of America as represented by the Administrator of the National Aeronautics and Space Administration, Washington, D.C.
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- [22] Filed: Oct. 23, 1995
- [51] Int. Cl.<sup>6</sup> ...... G01N 29/00; G01N 29/04
- - 73/600

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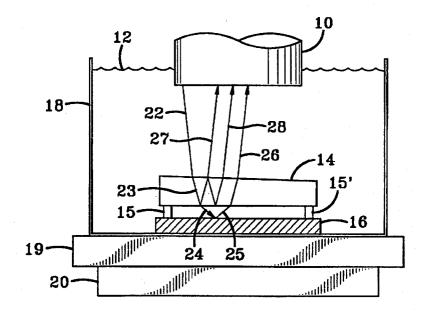
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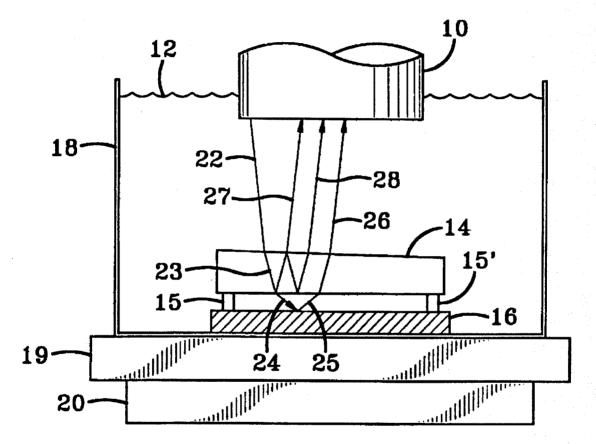
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#### [57] ABSTRACT

A pulse-echo, immersion method for ultrasonic evaluation of a material which accounts for and eliminates nonlevelness in the equipment set-up and sample thickness variation effects employs a single transducer and automatic scanning and digital imaging to obtain an image of a property of the material, such as pore fraction. The nonlevelness and thickness variation effects are accounted for by pre-scan adjustments of the time window to insure that the echoes received at each scan point are gated in the center of the window. This information is input into the scan file so that, during the automatic scanning for the material evaluation, each received echo is centered in its time window. A crosscorrelation function calculates the velocity at each scan point, which is then proportionalized to a color or grey scale and displayed on a video screen.

> 15 Claims, 5 Drawing Sheets (1 of 5 Drawings in Color)





**FIG. 1** 

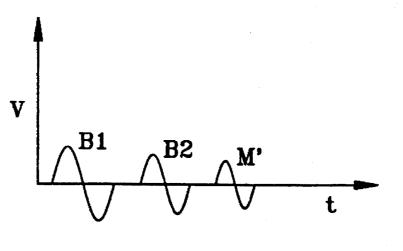


FIG. 2A

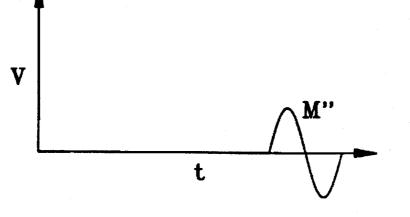
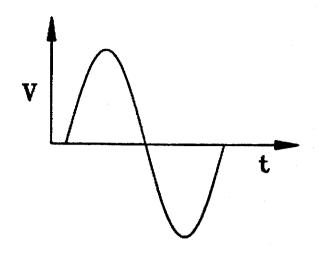


FIG. 2B





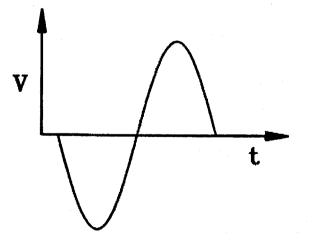


FIG. 3b

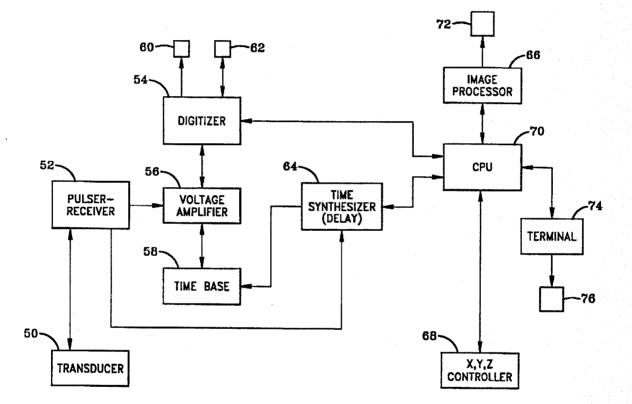
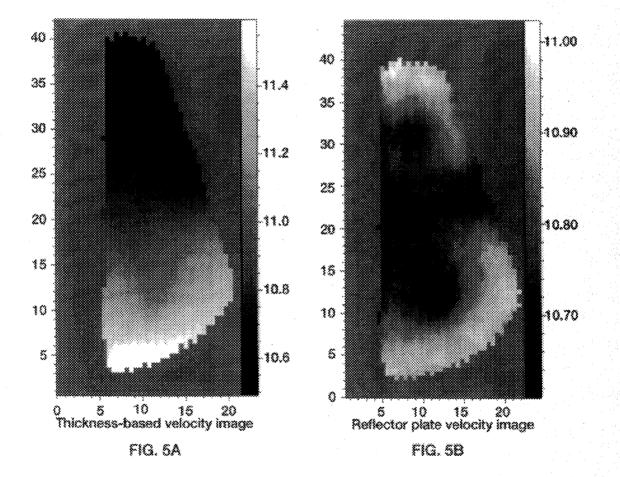


FIG. 4



### PULSE-ECHO ULTRASONIC IMAGING METHOD FOR ELIMINATING SAMPLE THICKNESS VARIATION EFFECTS

## ORIGIN OF THE INVENTION

The invention described herein was made by an employee of the United States Government and may be manufactured and used by or for the Government for governmental purposes without payment of any royalties thereon or therefor.

## BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

The invention relates to ultrasonic evaluation of material properties. More particularly, the invention relates to nondestructive ultrasonic evaluation of materials by measuring velocity using a single transducer pulse-echo immersion system, automatic scanning and digital imaging, which provides a video image of the sample in color or grey scale which is a map of a material property such as porosity fraction.

2. Background Of the Disclosure

Nondestructive evaluation applicable to evaluating properties of materials such as ceramics, metals, plastics and various composites are known to those skilled in the art and 25 include x-radiography, ultrasound or ultrasonic evaluation, and thermal methods. These methods provide an efficient, quasi-quantitative measure of material homogeneity, but often lack the precision necessary for microstructure evaluation of high-performance materials, such as high tempera- 30 ture oxidation resistant ceramics and the like. The development and use of materials for high-performance applications requires detailed, quantitative knowledge of microstructural and compositional variability for defining acceptable levels of variability and for rejecting those materials and processes 35 that yield sample-to-sample and within-sample variations likely to result in unacceptable property (e.g., strength, thermal conductivity, oxidation resistance, resistance to spalling, etc.) variations. Such variability must be precisely characterized either directly in terms of property measure- 40 ment or indirectly through microstructural characterization where microstructure-property relations have been previously established.

Repeated, uniformly spaced ultrasonic contact measurements have been successful for quantifying and mapping 45 inhomogeneity in various ceramics (e.g., SiC, Al<sub>2</sub>O<sub>3</sub>,  $YBa_2Cu_3O_7$  and  $Si_3N_4$ ) and metals in terms of ultrasonic material properties such as reflection coefficient, velocity and attenuation coefficient as mentioned, for example, by Roth, et. al. in Quantitative Mapping of Pore Fraction 50 Variations in Silicon Nitride Using an Ultrasonic Contact Scan Technique, NASA TP 3377 (1993). This publication describes quantitatively characterizing material (e.g.,  $Si_3N_4$ ) microstructure in terms of actual ultrasonic wave parameters. The wave parameters include reflection coefficient, 55 attenuation coefficient and velocity. A post-scan interactive data display system is used for comparing ultrasonic properties at different locations within samples and viewing the resultant ultrasonic images. Further refinement of this process is disclosed by Roth, et. al. in PSIDD: A Post-Scan 60 Interactive Data Display System for Ultrasonic Scans, NASA TM-4545 (1993). This process relates to contact scans and does not disclose how to account for thickness variations in the sample being measured. Piche discloses a single transducer immersion method for evaluating plastic 65 using a technique in which 16 scan points are pulsed for the sample and the results evaluated using regression analysis

[L. Piche, Ultrasonic Velocity Measurement for the Determination of Density in Polyethylene, Polymer Eng. &. Sci.,v. 24, n.17, p. 1358-58 (Dec. 1984]. This method does not relate to forming an image of the sample property, nor does 5 it provide an experimental technique that automatically accounts for nonlevelness and thickness variation during a scan procedure required to form an image. Consequently, a need still exists for a method which will permit ultrasonic material evaluation that will account for nonlevelness and 10 thickness variations in the material, require only a single transducer, eliminate problems associated with physical contact between the transducer and sample or buffer rod, and display, on a video screen in gray scale or color, an image of the scanned material which is a map of an internal structural 15 property of the material, such as porosity fraction.

#### SUMMARY OF THE INVENTION

The invention relates to a method for nondestructive ultrasonic evaluation of materials by measuring velocity 20 using a pulse-echo immersion system with automatic scanning, echo cross-correlation and digital imaging to obtain a grey scale or color image of the sample. The velocity values obtained for each scan point are scaled on a grey or color scale and displayed on a video screen which shows a material property, such as porosity fraction. Prior to the automatic scanning, nonlevelness in the set-up and sample thickness variation effects are accounted for and eliminated by insuring that the echoes at each scan point are first gated and input into a scan parameter file in a computer, so that during the subsequent automatic scanning each received echo is centered in the time window set for it. While it is possible, but not practical to do a manual prescan at each and every scan point needed for a two dimensional video image of the material property being evaluated, many sample thickness variations are in the form of a uniform thickness variation from one edge to another. In this case of uniform thickness variations from one edge to another, preliminary scans are performed along a single line in both the x- and y-directions of the sample to provide slant correction factors. The slant correction factors are input into the scan parameter file so that any wedge-shape variations are taken into account during the automatic scanning for the material evaluation, to insure that each echo received during the automatic scanning is centered within the time window. A single transducer is used in a preferred embodiment of the invention.

In the immersion method of the invention, the material to be evaluated is surrounded by a liquid and positioned over an acoustic reflector which is also immersed in the liquid. An ultrasonic wave of a known frequency is transmitted through the liquid and four separate echoes are recorded and evaluated at each scan point. Each echo is received as an analog waveform which is digitized and stored in a computer. The echoes received, digitized and stored during the sample evaluation scans are the first two succesive echoes reflected off the back surface of the sample, the first echo reflected off the front surface of the accoustic reflector in which the received wave has passed through the sample, and the forth is the first echo reflected off the front surface of the reflector with the sample not present, so that the received wave does not pass through the sample. This means that at least two separate scans must be made, with and without the sample present between the transducer and reflector. However, as a practical matter it is difficult from both a hardware and software perspective to accomplish this in just two scans and obtain maximum time resolution and thus maximum accuracy. Consequently three or four separate scans are

performed, with three being faster and four being more accurate. The choice is left to the discretion of the practitioner. In the embodiment in which four separate scans are performed during the sample evaluation, the ultrasonic wave goes through both the liquid and the material during the first 5 three scans. For the forth scan the material sample is removed so that the transmitted wave is reflected off the front surface of the reflector without going through the material. Although the order is not important, it is convenient to receive the first echo reflected off the back surface 10 of the material during the first scan and the second successive echo reflected off the back surface of the sample during the second scan. During the third scan in which the transmitted wave goes through both the immersion liquid and the material sample, the first echo reflected off the front surface 15 of the reflector is received. The first echo reflected off the front reflector surface is received during the fourth scan when the sample is not present. This process is repeated at a plurality of scan points sufficient to produce a video image of a microstructural property, such as porosity, of the mate- 20 rial. After the scanning is completed, the digitized waveforms are retrieved from the computer and the time delay between the first two successive echoes received from the back surface of the material at each scan point is determined. The time delay between the two different reflections or 25 echoes received off the reflector (with and without the transmitted wave going through the sample) is also determined for each scan point. The wave velocity at each scan point is then calculated from the time delays and the speed of the transmitted wave in the liquid. The velocity values for 30 instrumentation used in the invention. all of the scan points are scaled to corresponding proportional color or grey scale values which are then displayed on a video screen or cathode ray tube (CRT). Thus, in this embodiment of the invention, four separate scans are made at each scan point to separately receive, as analog 35 waveforms, the first two successive ultrasonic echoes off the back surface of the sample and the first echo off the front surface of the reflector both with and without going through said sample; digitizing and storing the waveforms; retrieving the digitized waveforms; determining the received time 40 delay between the first two successive sample back surface echoes and between the two reflector front surface echoes; calculating the wave velocity at each scan point; scaling the calculated velocities to corresponding proportional color or gray scale values, and displaying the resulting image. The 45 wave velocity at each scan point is calculated from

$$v = c \left( \frac{\Delta t}{2\tau} + 1 \right)$$

wherein  $2\tau$  is the received time delay between the two successive sample back surface echoes, wherein  $\Delta t$  is the time delay between the two different echoes received from the reflector with and without going through the sample, and wherein c is the speed of the transmitted ultrasound wave in 55 the liquid. The embodiment in which three separate scans are made is similar to that in which four separate scans are made, with the difference being that during the first scan the first two succesive reflections or echoes off the back surface of the sample are received, digitized and stored. It will be 60 noted that above equation does not include the sample thickness value. This means that the thickness of the sample need not be measured or known.

As set forth above, prior to the two, three or four scans during which the sample is evaluated, nonlevelness and 65 sample thickness variations are accounted for and eliminated by pre-scans to insure that the received reflections or echoes

are within their set time windows to provide a complete waveform for evaluation and cross-correlation to accurately obtain the time delay data used in calculating the velocity values. In the case of a sample having a thickness variation in the form of a uniform thickness variation from one edge to another, preliminary scans are performed along a single line in both the the x- and y-directions of the sample to provide slant correction factors. The slant correction factors are input into the computer scan parameter file so these variations are taken into account during the automatic scanning for the material evaluation.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The file of this patent contains at least one drawing executed in color. Copies of this patent with color drawing(s) will be provided by the Patent and Trademark Office upon request and payment of the necessary fee.

FIG. 1 schematically illustrates the spatial relationship between the transducer, liquid, material sample, reflector plate and the transmitted and reflected ultrasonic echo waves in the practice of the invention.

FIGS. 2(a) and 2(b) graphically illustrate the amplitude and time delay of the received analog ultrasonic echoes reflected off the material sample and reflector.

FIGS. 3(a) and 3(b) graphically illustrate respective first and second sample back surface echoes in which the second is inverted with respect to the first.

FIG. 4 is a block diagram schematically illustrating the

FIGS. 5(a) and 5(b) are photographs of video grey scale displays of a thickness based ultrasonic velocity image of a ceramic according to the prior art method and the method of the invention, respectively.

#### DETAILED DESCRIPTION

Referring to FIG. 1, transducer 10 is schematically shown as partially immersed in a liquid 12 which is the immersion fluid. Material sample 14 is shown positioned in the fluid 12 between the transducer 10 and reflector plate 16 in container or tank 18 located on top of x- and y-direction motorized stages 19 and 20. Supports 15 and 15' maintain sample 14 above reflector 16. The transducer 10 and motorized x- and y-direction stages 19 and 20 are electrically connected by means not shown to a pulser-receiver (not shown) and to means (not shown) for moving the x- and y- stages in their respective directions. Similarly, liquid 12 is connected to means not shown for maintaining the temperature of the liquid preferably within at least about  $\pm 1^{\circ}$  F. of the temperature at which the scans are to be run. It is possible to maintain the liquid temperature within ±0.1° F. The better the temperature control, the more accurate the results will be, For example, if the temperature of the immersion liquid is  $\pm 1^{\circ}$  F. and the liquid is water, a 1.5% error in velocity is possible. If the porosity fraction or other property of the material at a particular point is such as to result in a velocity value difference in the sample of 2%, only a 0.5% microstructural velocity difference might be detected if a  $\pm 1^{\circ}$  F. temperature variation is present during the scan. At each scan point an ultrasonic wave 22 of a known frequency is transmitted from transducer 10 through liquid 12 and into material sample 14. Entering material 14 causes part of wave 22 to be reflected (not shown) off the top surface of the sample, with the rest of the wave passing through the material as 23. Part of wave 23 continues through the material and to the top surface of accoustic reflector 16 as 24, is reflected back off the top surface of reflector 16 as 25,

passes back through the sample 14 and returns to the transducer 10 as wave 26. A portion of wave 23 is reflected off the back surface of the sample and returns to the transducer as 27. Part of the wave 23 reflected off the back surface of the material is reflected off the top surface, returns to the back surface, is again reflected back to the top surface and exits as wave 28. Waves 27 and 28 are the first two successive back surface reflected waves used in the method of the invention at each scan point. Not shown is the wave transmitted through the liquid and reflected back to the 10 transducer without going through the material. This wave which is not shown and wave 26 are the two reflector front surface echoes used in the method of the invention. Motorized stages 19 and 20 form part of an automated scanning system which incrementally moves in both the x- and 15 y-directions to obtain an ordered array of points across the entire surface of the material sample. A 20 MHz, broadband transducer was used in the practice of the invention. Broadband transducers emit a broadband frequency content dominated by a center frequency. That is, they are made to emit 20 at a nominal frequency proximate that of the design frequency (e.g., 20 MHz), with a Gaussian fall-off on either side of the nominal center frequency. Thus, a 20 MHz broadband transducer will also emit frequencies slightly above and below the nominal center frequency of 20 MHz. 25 In the Piche article referred to above, although the two different reflector front surface echoes are captured and recorded, the first front surface echo and the first back surface echo are captured and recorded. This is different from the method of the invention which captures and records 30 the first two successive sample back surface echoes and not the first front sample surface echo. Further, Piche does not use automatic sample scanning or digital imaging. FIGS. 2(a) and 2(b) graphically illustrate the reflected waveforms received and displayed on the CRT of an oscilloscope as 35 time domain analog waveforms. Turning to FIGS. 2(a) and 2(b), the intensity or strength of the received waveform is displayed as voltage amplitude, which is the ordinate of the graph, and the received time delay as the abscissa. In this representation, B1, B2 and M' refer to waves 27.28 and 26 40 of FIG. 1, respectively, with M" representing the wave transmitted through the liquid and reflected off the front surface of the reflector without passing through the material sample. The time delay between the first two successive echoes reflected from the back or bottom surface of the 45 material back to the transducer, B1 and B2, is readily obtained, as is the time delay between the two reflections received from the front surface of the reflector, M' and M". Since the velocity of the ultrasonic wave is faster in denser media than in less dense media, voids, delaminations, poros- 50 ity and other density variables within the material are obtained as a function of the speed of the wave, which is determined by the time delay between the first two successive echoes received which have been reflected off the back of the material, and the time delay between the two different 55 reflections from the front surface of the reflector. As set forth above under SUMMARY, the speed or velocity of the transmitted wave traveling through the material sample is determined according to the simple equation:

 $v = c \left( \frac{\Delta t}{2\tau} + 1 \right)$ 

wherein  $2\tau$  is the received time delay between the two successive material sample back surface echoes, wherein at 65 is the time delay between the two different echoes received from the reflector with and without going through said

sample, and wherein c is the speed of the transmitted wave in the liquid. This equation is accurate for a single point measurement. Prior art ultrasonic velocity scan techniques such as that of Roth et. al. in the quantitative mapping publication referred to above, assume that the material sample is of uniform thickness and do not take into account nonlevelness and material thickness variations as does the method of the invention.

In the practice of the method of the invention, tank 18 may be made of any suitable material. Clear plastic such as polymethylmethacrylate (e,g., Lucite or Plexoglass) has been found useful. The sample tank contains a suitable elastic liquid, such as water, as the immersion fluid to provide an accoustic coupling between the transducer, material and reflector plate. Since the x-, y-direction scans made across the sample surface in the method of the invention can take a significant amount of time compared to that for a single point measurement and since the speed of sound in a liquid is also a function of temperature, the water is maintained at a constant temperature during the scanning. This is readily accomplished simply by using a constant temperature regulating means, such as a constant temperature water circulator, for maintaining the desired temperature constant during the ultrasonic scanning. It is convenient to keep the temperature of the water at about ambient or 68° F. ±1° F. during the scan, although other temperatures may be used if desired, as long as the temperature is maintained within no more than  $\pm 1^{\circ}$  F. In the case of distilled, deionized water, the wave velocity may be obtained from published tables. However, tap water may be used as long as the velocity in the water is actually measured. The reflector is placed on the bottom of the tank. Other immersion liquids may be used, if desired, such as Dow Corning 704 vacuum pump oil.

The reflector is a solid plate of material having an accoustic impedance significantly different from that of the liquid or water. A flat plate of tungsten (e.g., 1/16"-1/8" thick) is preferably used, because tungsten has an accoustic impedance almost two orders of magnitude higher than water in units of g/cm<sup>2</sup>-sec. The use of a tungsten plate results in the highest possible reflection amplitude of any solid material for the echoes reflecting off the front surface of the reflector plate. This large difference in accoustic impedance is important when attempting to obtain ultrasonic echoes that have to travel into and through immersion liquid and the sample, bounce off the reflector plate, and travel back through the liquid and sample to the the transducer for reception. High frequency ultrasound provides greater time resolution than lower frequencies and is therefore more desireable for greater accuracy of the velocity of the ultrasound through the sample and corresponding velocity image. The higher the frequency, the greater the velocity accuracy. By having the highest reflection amplitude possible, it is possible to use the method of the invention (a) at higher frequencies where attenuation through the sample is greater than if using lower frequencies and (b) with materials that significantly attenuate ultrasound, such as composite materials. By high frequency ultrasound is meant from 1-100 MHz, typically 3-50 MHz and more typically 10-30 MHz.

The material sample is easily positioned over the reflector plate by using spacers on top of the plate and placing the material on top of the spacers. It is important that the spacers have the same height or thickness so that the material is as level as possible. Lucite is available as sheets which are very uniformly thick and it is convenient to use 0.5" cubes of this plastic as spacers. The material sample, such as a plate of silicon nitride ceramic, is placed on the plastic spacers over the tungsten reflector plate prior to scanning.

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FIG. 4 schematically illustrates, in block diagram fashion, the basic system and instrumentation used for the scanning

and ultrasonic imaging according to an embodiment used in the practice of the invention.

Thus, referring to FIG. 4, the basic instrumentation includes a transducer 50, a pulser-receiver 52, and a programmable waveform digitizer 54 having associated with it a vertical voltage amplifier 56, programmable time base 58, and anolog and digital monitors 60 and 62, respectively. Also included are a time delay or synthesizer 64, an image processor 66, an X, Y, Z controller 68, computer or central processing unit (CPU) 70, and video display 72. In the embodiment shown, the computer 70 is a CPU with terminal 10 74 and associated video display 76 also forming part of the system. Monitors 60 and 62, along with digitizer 54, voltage amplifier 56 and time base 58 also serve as respective analog and digital oscilloscopes. The time synthesizer, time base, voltage amplifier and waveform digitizer are all general purpose interface [IEEE- 488]bus (hereinafter "GPIB") programmable and interconnected via GPIB cables. The computer 70 is programmed in Fortran and contains an image processor system which is connected to the video color and gray scale display 72. The computer controls the GPIB instrumentation and acquiring of the desired waveforms via the GPIB. The process includes data acquisition, analysis/ calculation, image processing and display. The Fortran software, with callable routines in in IEX-VMS interface software to communicate with the GPIB instruments is written for instrument control and waveform acquisition 25 following the method of Generazio, et. al. in Interfacing Laboratory Instruments to Multiuser Virtual Memory Computers, NASA Technical Memorandum 4106 (1985), the disclosure of which is incorporated herein by reference. The Fortran programs used in the practice of the invention 30 including the scanning program, the analysis and crosscorrelation program, the grey scale imagemaker program, and the display program are contained in the attached Appendix. The wave form digitizer is a Tektronics 7912 AD Programmable Digitizer along with a Tektronics 7A16 P 35 Programmable Vertical Voltage Amplifier (voltage base) and a Tektronics 7B90 P Programmable Time Base. The time delay (time synthesizer) is a Hewlett Packard Model 5359A and the X, Y, Z programmable stepper motor controller and associated tables is a Klinger Scientific C-1.22. The ultrasonic pulser-receiver is a Panametrics Model 5601 and the 40 transducer used in the scanning of the silicon nitride ceramic disk in the example below is a Panametrics 20 MHz, longitudinal, unfocused, broad band transducer. The computer is a Digital Equipment model Microvax II.

In the practice of the invention, the image processer is a 45 Grinnell Systems Grinnell 274 Image Processing System and the Grinnell Systems GMR Series Software Package, Release 2.2, Jun. 19,1981, available from McLoud Associates, 165-F Croftich Lane, Campbell, Calif. 95008, the disclosure of which is also incorporated herein by 50 reference. Two video displays are used, one of which is a DEC VT340 terminal, which is the user terminal attached to the computer, and a Mitsubishi 20LP is the video display monitor attached to the image processing system. High level VAX Fortran software used for driving the system is 55 included in the Appendix as set forth above. The Grinnell library of Fortran subroutines is called from this high level software. The video display shows ultrasonic images.

The pulser-receiver applies the voltage pulse to the transducer to generate the ultrasonic waves into the sample and to the reflector plate and also receives the raw ultrasonic <sup>60</sup> echo waveforms from the transducer. The approximate times where the echo waveforms are expected to occur are determined a priori (prior to the automatic scanning for the material evaluation) using the time systhesizer to find and position the echo waveforms on the oscilloscope. The time 65 base and voltage amplifier are used to modify the time and voltage scales to view the waveforms on the oscilloscope.

Both the time base and the time synthesizer are externally triggered by the pulser-receiver (a+2 volt synchronizing pulse). Triggering occurs on the positive slope of the pulse. The time base is adjustable over the range of from 1 psec-500 msec/div on the oscilloscope, with the optimum setting for each waveform determined a priori and input to a data file in the computer. The pulser-receiver output is connected to the voltage amplifier. The voltage amplifier, selectable over the range 50 mV-1V/div, is automatically adjusted by the digitizer so that the entire received analog waveform is digitized with maximum amplitude fit onto the digital waveform monitor. The digitizer digitizes each waveform received into 512 point arrays (at a sampling rate ranging from 0.512 -1.024 GHz depending on the time base time/division setting). Each waveform is acquired 64 times and averaged to obtain a smoother waveform with averaged noise levels using a Fortran algorithm included in the scanning program in the Appendix and which is also found in the NASA Technical Memorandum 4106 referred to above. The X and Y positional and Z intensity outputs from the waveform digitizer are attached to the analog and digital monitors 60 and 62. The analog monitor is used for the prescans and the digital for the automatic scanning.

As set forth under the SUMMARY, prior to the two, three or four scans during which the sample is evaluated, nonlevelness and sample thickness variations are accounted for and eliminated by pre-scans to insure that the received reflections or echoes are within their set time windows to provide a complete waveform for evaluation and cross-correlation to accurately obtain the time delay data used in calculating the velocity values. That is, during the nonlevelness and material thickness variation scans, the operator notes if the time delay of each echo received at each scan point is such that it is no longer centered within the oscilloscope time window. If a received echo is not centered within the time window on the scope, this is noted and the time window changed for each such echo received until the received echo time domain waveform is completely within the new time window set for it to insure that the complete time domain waveform is captured or gated completely within the new window. This time delay information at each scan point is inputted into the scan parameter file and recalled during the actual scanning during the material evaluation, to automatically adjust the time delay for the received echoes at each scan point so that each echo received during the scanning is centered within the time window set for it. This is very time consuming to do for each scan point. However, in the case of a sample having a thickness variation in the form of a uniform thickness variation from one edge to another, preliminary scans are performed along a single line in both the the x- and v-directions of the sample to provide slant correction factors. The slant correction factors are input into the computer scan parameter file so these variations are taken into account during the automatic scanning for the material evaluation. It is important that the echo at each scan point is centered in its time window, because the whole pulse or echo time domain waveform is needed to give the precise time delay between echoes for the cross-correlation which provides the velocity value. In doing this for a wedge shaped sample, prior to the automatic scan, the transducer scans along two straight lines over the sample, once in the the x-direction and once in the y-direction, during which an operator notes the echo received from the first and last scan points, starting from the first scan point which is generally at one corner of the area defined for scanning. The time difference from the sample end-to-end in each of the x- and y-directions of the first and last scan point is noted by the operator who then adjusts the time base for each echo if needed to insure that it is centered within the time frame set for it. This is done so that so that each echo received during the scans in which the material is being evaluated is centered (gated) within the

oscilloscope time window set for it so that the received waveform is displayed with the maximum possible amplitude on the CRT and still have the complete waveform. This permits the maximum time resolution of individual echoes without losing any part of the time domain waveform which appears on the CRT screen as a function of voltage (amplitude) and time, wherein time is the x- axis and voltage or amplitude is the y- axis. It is important and forms an aspect of the invention that the complete waveform or pulse echo be captured or "gated" on the CRT screen in order to perform an accurate cross-correlation later on in the procedure of the process of the invention. The cross-correlation of echoes provides the precise time delay between received echoes or pulses which is required to calculate the velocity or speed of the ultrasound in the material evaluated which, in turn, provides the information to gray or color scale the 15 velocity data into a digitized map of the material density. This slant correction procedure also allows an accurate evaluation to be made without the need for specialized leveling equipment. These x- and y-direction time window corrections are called slant correction factors and they are 20 inputted into the scan parameter file in units of "nsec/pm" where (a) the number of nsec is the time extent from sample end-to-end that is required to keep the specific echo centered and is determined using the (a) time synthesizer to reposition echoes in time and (b) the number of µm is the distance traveled by the transducer for which this slant factor is determined. By way of an illustrative, but nonlimiting example, the first scan point (0.0) along the x- direction may have a B1 echo centered at a time=6.77 usec, while the last scan point (40,0), may have B1 centered at time=7.14 µsec. If the x- direction scan line length is 40 mm, the x-direction

#### $W_{DT} = T_{I} + [(X_{SC})(X_{SN})(X_{SI}) + (Y_{SC})(Y_{SN})(Y_{SI})]$

wherein  $W_{DT}$  is the correct delay time window at a particular scan location,  $T_I$  is the time delay at the the initial scan location,  $X_{SC}$  and  $Y_{SC}$  are the x- and y-direction slant correction factors,  $X_{SN}$  and  $Y_{SN}$  are the scan point numbers in the x- and y-directions, and  $X_{SI}$  and  $Y_{SI}$  are the x- and y-direction scan increments. With many samples it has been found that the slant correction factors turn out to be the same for the B1, B2 echoes and the slant correction factors for the M', M" echoes are the same. However, for some samples (e.g., thick samples), they may not be the same. In such cases a first x- and y-direction scan is made for the B1 echoes and a second x- and y-direction scan made for the B2 echoes. The same holds for the M' and M" echoes for which two separate scans are made in the x- and y-directions.

A scan parameter file is input into a computer which contains all of the information necessary to automatically scan the material sample being evaluated. This information includes a predefined and ordered array of scan points over which to run the scan. By way of an illustrative, but nonlimiting example, in an example of the method of the invention in which the material being evaluated was a monolithic ceramic wedge, the scan consisted of a 41 (X-direction) by 81 (y-direction) grid of measurements for a total of 3,200 scan points, with each measurement or scan point separated by 1 mm (x-) and y- scan increment). Information input into the scan parameter file (NOTHICK\_ ALLSHAPE1.DAT) includes the following:

C **TTTLE** NOTHICK ALLSHAPE1.DAT	
C ** SCAN INCREMENT (uM) IN X-DIRECTION IS:	
1000.	
C ** SCAN INCREMENT (uM) IN Y-DIRECTION IS:	
C ** SCAN LENGTH (uM) IN X-DIRECTION IS:	
40000. C ** SCAN LENGTH (uM) IN Y-DIRECTION IS:	
80000.	
C ** X-DIRECTION SLANT CORRECTION FACTOR (nsec/uM) FOR B1 & B2 ECHOES IS:	
C ** Y-DIRECTION SLANT CORRECTION FACTOR (nesec/uM) FOR REFLECTOR ECHOES	S IS:
-0.0055	
C ** Y-DIRECTION SLANT CORRECTION FACTOR (nsec/uM) FOR B1 & B2 ECHOES IS:	
-0.00175	
C ** Y-DIRECTION SLANT CORRECTION FACTOR (nsec/uM) FOR REFLECTOR ECHOES	IS
0.0	
C ** TIME LOCATION (USEC) OF B1 ECHO AT SCAN ORIGIN IS:	
52.83 C ** TIME LOCATION (USEC) OF B2 ECHO AT SCAN ORIGIN IS:	
52.31	
C ** TIME LOCATION (USEC) OF REFLECTOR ECHO W/SAMPLE PRESENT AT SCAN LO	CATION
IS:	
69.46	
C ** TIME LOCATION (USEC) OF REFLECTOR ECHO W/O SAMPLE PRESENT AT SCAN I	LOCATION
IS:	
72.48	
C ** IMMERSION FLUID VELOCITY (cm/uSEC) IS:	
C ** B2 PHASE-INVERTED WRT B1 (Y/N)?: N	
C ** M" PHASE INVERIED WRT M' (Y/N)?:	
N	
41	

slant correction factor is obtained from (7.14-6.77)/40 µsec/ mm. It should be noted that slant correction factors can be negative as well as positive numbers. The location of the 65 time window during scanning for the material evaluation is automatically adjusted via computer control by using the formula:

As set forth above, in the method of the invention, the transducer is activated so that the first front surface echo off the sample, the first two successive back surface echoes, and the first echo off the reflector plate are all seen in the oscilloscope display at the same time by adjusting the the time base to the appropriate time per division setting and

adjusting the time synthesizer delay time. Viewing the first front surface echo off the sample enables the operator to know if the back surface echoes are also on the CRT screen. The unfocused transducer is positioned above the sample at a distance determined initially by the natural focal distance. 5 When using an unfocused transducer a good initial starting height is approximately one to two inches above the sample. The reflector plate front surface echo may be low in amplitude compared to the sample back surface echoes, so that the the pulser-receiver gain/attenuation or vertical amplifier gain 10 settings may have to be increased to see this echo. It is important not to confuse the echoes off the front surface of the reflector plate with the second set of echoes originating from the front and back surfaces of the sample. The second set of echoes originating from the front and back surface of 15 the sample will always occur at twice the delay time where the first set of these echoes appears. For example, if the first set of echoes begins at 50 msec on the digital oscilloscope, the second set will begin at 100 msec. If using, for example, a three milimeter thick sample placed on 0.5" thick plastic 20 supports on the reflector plate, the first reflector echo will occur at about 20 msec after the time where the first set of echoes originates and thus the reflector echo will be seen at about 70 msec in this illustration. Another way to note the reflector plate echo is to raise and lower the sample while 25 noting the location of the stationary echo corresponding to the stationary reflector plate. It is essential to have reflector plate echoes that will not interfere with the second set of echoes originating from the front and back sample surfaces. Attention is next focused on the first back surface echo from 30 the sample, B1. The echo is centered in the oscilloscope time window to obtaining maximum time resolution by adjusting the time base time per division and the time synthesizer delay. The synthesizer time is recorded and inputted into the scan parameter computer file. This procedure is repeated for 35 the second back surface sample echo, B2, the first front surface echo off the reflector plate with the sample present, M' and the first echo off the reflector plate with the sample removed, M". The next step is to account for and eliminate any nonlevelness in the set-up and also sample thickness 40 variations. This done at each scan point, except that in the case of uniform thickness variations in the sample, the slant correction factors outlined above are determined and input into the scan parameter file in the computer.

The scanning is then automatically performed through the 45 remainder of the scanning points previously inputted into the scan parameter file in the computer using a program written in Fortran and IEX GPIB to perform the scanning and also to obtain maximum vertical voltage resolution of the received ultrasonic waveforms. Scanning is accomplished 50 through the use of computer controlled x-, and y- microscanning tables used to reposition the sample in the x- or y-direction in a 1 mm increment (other increments may be used at the convenience and discretion of the practitioner) for the next measurement. The ultrasonic waveforms 55 received are then digitized (512×512 pixel resolution) at each scan location and stored successively in the scan data file in the computer. Four separate ultrasonic scans are performed at each scan location. As set forth above, the echoes are B1 (first echo off sample back surface, obtained 60 in first scan), B2 (second echo off sample back surface, obtained in second scan), M' (first echo off front surface of reflector plate with the sample present, obtained in third scan), and M" (first echo off front surface of reflector plate without the sample present, obtained in fourth scan). Each of 65 the four echoes is obtained in a separate scan to obtain the maximum time resolution for each echo by setting, before

each scan during the nonlevelness and material thickness variation procedure, the optimum time per division setting on the oscilloscope time base that allows maximum time resolution. The minimum number of scans for this thicknesselimination procedure is two, but the time per division setting for only two scans cannot be obtained in this case as the time per division setting would be fixed for all three echoes obtained in the first of the scans using this scan procedure.

The following is an algorithm of a scanning program which accounts for and eliminates the nonlevelness of the set-up and uniform thickness variation effects of the sample in the resulting ultrasonic image displayed on the video, the code for which is included in the Appendix.

- 1) Determine the scan lengths and scan increments in the x- and y-directions, time positions of echoes at scan origin, slant correction factors, and immersion fluid velocity.
- 2) Edit NOTHICK\_ALLSHAPE1.DAT FILE, which is the scan parameter file, and input information from 1) above.
- 3) Start scanner fortran program on computer which automatically does the following:

A) Initialize all GPIB instrumentation, which includes the time synthesizer, digitizer, time base, voltage amplifier, Klinger X, Y stages.

- B) Perform scan to digitize B1 echoes and store in fileI) Digitize B1 at scan origin
  - Adjust voltage base for echo with maximum amplitude in video/oscilloscope window
  - Move Klinger tables under transducer in x- direction specified x- direction increment
  - Time synthesizer moves to delay time position determined by B1, B2, slant correction factors. This results in echo in video being centered in the Tektronics analog video/oscilloscope display and subsequently digitized and stored.
- Time position= $T_{O}$ +[( $S_{X}$ )( $N_{X}$ )( $I_{X}$ )+( $S_{y}$ )( $N_{y}$ )( $I_{y}$ )]
  - where  $T_0$ =correct delay time window at a particular scan location  $S_x$ =x- direction slant correction factor (nsec/µm)
  - $N_x$ =scan point number in x- direction
  - $I_x = x$  direction scan increment (µm)
  - $S_y=y$  direction slant correction factor (nsec/µm)
  - $\dot{N_y}$ =scan point number in y- direction
  - I,=y- direction scan increment (µm)
- II) Repeat I) until one scan line in x- direction is completed.
- III) Increment transducer in y- direction specified ydirection increment and repeat I)-II).
- IV) Repeat I)-III) until y- scan length is traversed and scan is completed.
- V) Return Klinger tables to scan origin.
- C) Perform scan to digitize **B2** echoes and store in file by repeating steps B(I–V)
- D) Perform scan to digitize reflector echoes with sample present and store in file by repeating steps B(I-V), but using reflector echo slant correction factor
- E) Remove sample. Perform scan to digitize reflector echoes without sample present and store in file by repeating steps B(I–V), but using reflector echo slant correction factor
- 4) Start velocity calculation Fortran program on computer to produce a file of velocities at each scan location by performing the cross-correlation algorithm.

- 5) Start image formation Fortran program on computer which results in a file of values between 0 and 255 which scale directly with the velocity values.
- 6) Start image display program which brings grey scale level image up on video.

Before initiating the scanning procedure, the temperature of the water or other immersion fluid is measured. If the fluid is water, published tables or graphs of temperature and velocity can be used to determine the velocity of the ultrasound in the constant temperature water bath. If the <sup>10</sup> immersion liquid is a liquid other than water, or if a more precise temperature than that available in published graphs and tables is desired, the velocity of the ultrasound in the liquid is determined by recording the times (T<sub>P</sub>) where ultrasonic peaks occur for two different vertical positions <sup>15</sup> (Z1 and Z2) of the transducer above the reflector plate. The velocity, V, is then determined from

#### $V = (Z1 - Z2)/(T_P1 - T_P2)$

The phase relationships of (a) B1 compared to B2 and also (2) the reflector front surface echo with the sample present (M') compared to that without the sample present (M") are examined. These phase relationships are important for the computation of the velocity image of the scanned sample. 25 The quantity  $2\tau$  is obtained by cross-correlating echoes B1 and B2 which is defined as the precise time delay between the B1 and B2 echoes. If B1 and B2 are phase inverted with respect to each other, the time occurrence of the minimum in the cross-correlation function is used to obtain 27. If M' 30 and M" are phase inverted with respect to each other, the time occurrence of the minimum in the cross-correlation function is used to obtain  $\Delta t$ . Otherwise, at the time occurence of the maximum in the cross-correlation function is used. 35

FIGS. 3(a) and 3(b) graphically illustrate the case in which B2 is phase inverted with respect to B1. The same holds for M' and M". Phase relationships generally remain the same throughout the scan, unless significant discrete microstructural defects are encountered by the ultrasonic  $_{40}$  wave.

After the scan has been completed and all the received echoes have been digitized and stored in the scan data file in the computer, they are recalled from the data file to perform the velocity image calculation for each scan location. In 45 performing this cross-correlation, an overlap method is used by the computer based on a cross-correlation program using Fast Fourier transforms published in pages 415 and 416 (Correlation and Autocorrolation Using the FFT) in the book Numerical Recipes-The Art of Scientific Computing, by 50 Press, et. al., 1988 Edition, Cambridge Univ. Press.. The Fortran program used is in the Appendix. Echoes M' and M" are also cross-correlated to obtain  $\Delta t$  where where M' is the echo reflected off the reflector plate front surface with the sample present, M" is the echo reflected off the reflector plate front surface without the sample present, and  $\Delta t$  is the time delay between them. If M' and M" are phase inverted with respect to each other, the time occurrence of the minimum in the cross-correlation function is used to obtain  $\Delta t$ . Otherwise the time occurence of the maximum in the cross-correlation function is used. The velocity, V, at each

scan location is then calculated from the equation referred to above. The velocity value for each scan location is sequentially stored in the computer. After the scan is completed the velocity values are scaled on a gray or color scale with a value directly proportional to the velocity values, with the highest and lowest scale values corresponding to the highest and lowest velocity values.

The invention will be further understood with reference to the example below.

#### EXAMPLE

In this example, a sample of silicon nitride ceramic was evaluated using the thickness based velocity image method disclosed in the NASA Technical Memorandum TP 3377 referred to under Background. This method is based on a velocity, cross-correlation ultrasonic imaging method without the pre-scan to account for and eliminate nonlevelness in the set-up and sample thickness variations. In this method, only the first two sample back surface echoes are captured and evaluated. The silicon nitride ceramic was 3.5 mm thick with a uniform 300 micron thickness gradient. Very coarse time scaling was used so that the B1 and B2 echoes stayed in the time window while the sample thickness changed as the scan proceeded.

The same silicon nitride ceramic sample was also scanned and velocity imaged on a grey scale according to the method of the invention which included the prescans to eliminate set-up and sample thickness variations and which also captured and cross-corrolated both the first two successive sample back surface echoes and the two different reflector front surface echoes.

In both cases, the 20 MHz broad band transducer was used, the immersion liquid was water and the back plate was tungsten as set forth above.

FIGS. 5(a) and 5(b) are photographs of video grey scale displays of the thickness based ultrasonic velocity image of a ceramic according to the prior art method, and an image according to the method of the invention which included the prescans, respectively. Referring to FIG. 5(a), it is seen that the top defect is masked due to that part of the sample being thicker than the bottom part. Also, the defect near the bottom is not too discernable and the lower portion is very light due to it being thinner. In marked contrast and as shown in FIG. 5(b), the method of the invention clearly and correctly illustrates the defect areas, including resolution of the upper defect and an overall porosity gradient in the sample. It is believed that this demonstrates the efficacy and improvement to the art of the invention.

It is understood that various other embodiments and modifications in the practice of the invention will be apparent to, and can be readily made by, those skilled in the art without departing from the scope and spirit of the invention described above. Accordingly, it is not intended that the scope of the claims appended hereto be limited to the exact description set forth above, but rather that the claims be construed as encompassing all of the features of patentable novelty which reside in the present invention, including all the features and embodiments which would be treated as equivalents thereof by those skilled in the art to which the invention pertains.

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Docket No. NASA LEW-16,257-1 Serial No. 08/546,972

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Sent by Express Mail to Addressee under Mailing Label Number: EH462213576US on October 10, 1996 52357 15050 Kent nothing

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APPENNIX

# APPENDIX

С С nothick SCAN.FOR --- 4 SCAN METHOD C C C C Scan and data aquisition for the modified ultrasonic Immersion scanner by Don J.Roth C С PLEASE USE CLNEW.COM TO COMPILE & LINK Ċ C C Latest Update 20-sep-94 integer\*4 SCANSTEP, INDXSTEP integer\*4 SCANAXIS, INDXAXIS, ZSTEP INTEGER\*4 I17 character VOLANS\*1,TSCHEME\*1,UOLANS\*1 CHARACTER LOOPANS\*1, SHAPEANS\*1, ZIGANS\*1, FLAG\*1 character TBUF\*8,SCHEME\*1,FILENAME\*34,SCANMODE\*1 real DELAY(0:4), VOLTSET(0:4), MAXVALF, MAXVALT, VOL(4) rcal slant1,slant2,slant3,slant4 integer\*2 NSCAN, NINDX,PLACE,ZIGCOUNT,JXXX,SCANKNT integer\*2 A(512).NAVE,CHECKP,WWFLAG INTEGER\*2 115,116,126,127,MAXFS1P,MAXFS1PT 136,137,146,147 INTEGER\*2 LOOPTHRU\_II,LOOPTHRU\_S,LLL,IT,I,J,JJ,II INTEGER\*2 BYTE WRK0(80) common /IBLK/ WRK0,BUFFER common /SBLK/ A, DELAY, VOLTSET, MAI CHECKP/0/ZIGCOUNT/1/ data DATA 16/1/115/1/116/1/117/1/PLACE/0/ data 126/1/127/1/136/1/137/1/146/1/147/1/ 10010 format( A ) 10012 format(A2) 10020 format(I) 10030 format(F) OPEN( unit=8, file='TXA1:', status='NEW' ) CALL ENTERPARAM( SCANSTEP, INDXSTEP, NSCAN, NINDX, NAVE, VOLTAGEL ,VOLTAGEU, VOLTAGE\_MAX, SHAPEANS, LOOPANS, LOOPTHRU\_H, LOOPTHRU\_S, 1 ZIGANS, SCHEME, TSCHEME, UZEROO, FILENAME, 115, SCANMODE, SLANT1, SLANT2 1 1 ,SLANT3,SLANT4) SCANAXIS - I 4328 INDXAXIS = 2 ZSTEP = 10CALL STRTGPIB DO 1800 IADDR= 5,1,-1 1800 CALL INITINSTR( IADDR ) С С Setup of 7912: begin with V/D =.5, then automatically find С the best intensity and Digitize Defects С С NOTE: MAY NEED TO CHANGE THIS V/D TO START С 2000 CALL TEKGTL \*\*\*\*\* C\*\*\*\*

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E0 FORMAT (3F) READ (10,65403) DELAY1 **INOTHICK - STARTING 1ST BACK SURFACE ECHO** WINDOW TIME READ (10,65403) DELAY2 **INOTHICK - STARTING 2ND BACK SURFACE ECHO** WINDOW TIME READ (10,65403) DELAY3 INOTHICK - STARTING (W/SAMPLE) REFLECTOR ECHO WINDOW TIME READ (10,65403) DELAY4 **INOTHICK - STARTING (WO/SAMPLE) REFLECTOR** ECHO WINDOW TIME READ (10,65402) VOLANS READ (10,65403) VOL(1) READ (10,65403) VOL(2) READ (10,65403) VOL(3) READ (10,65402) UOLANS READ (10,65403) VOL(4) 65402 FORMAT (A) 65403 FORMAT (F) 51 FORMAT(A32) 52 FORMAT(A2) FORMAT(A4) 53 54 FORMAT(A2) TYPE \*, 'DELAY TIMES (B1, B2, RS, RNS)' TYPE \*,'DELAY1=',DELAY1 TYPE \*,'DELAY2=',DELAY2 TYPE \*,'DELAY3=',DELAY3 TYPE \*,'DELAY3=",DELAY3 TYPE \*,'DELAY4=",DELAY4 TYPE \*,' ' CLOSE (10) DELAY(1)=DELAY1/(1.\*10.\*\*6.) DELAY(2)=DELAY2/(1.\*10.\*\*6.) DELAY(3)=DELAY3/(1.\*10.\*\*6.) DELAY(4)=DELAY4/(1.\*10.\*\*6.) TYPE \*,' ' TYPE \*,DELAY TYPE \*,' CALL INITINSTR(0) CALL SETVOLTDIV(0.5) CALL TEKGTL CALL GETMAI(MAI) CALL TEKGTL CALL PUTTIME(DELAY(1)) CALL TEKGTL CALL GETBESTMAI( MAI ) CALL DIGDEF C C C Preliminary Digitizations to get Watch level and Timeset (Time/div) CALL TEKGTL CALL AUTOSETVOLTS( MAI, VOLTSET(1), NUMINT ) С TYPE \*,'AUTOSET VOLTS' IF( VOLTSET(1).EQ. 999. )THEN TYPE \*, DIGITIZER IS SCREWED UP GOTO 2000 ENDIF

```
CALL GETGRID( TIMESET, X )
         CALL GETSA( NAVE, MAI, A )
         CALL TEKGTL
         TYPE *, 'Timeset=', TIMESET,' Delay=', DELAY(1),
              Voltset=',VOLTSET(1)
    +
         TYPE *,'116= ',116,' 117= ',117
                  C********
         WRITE(16,rec=116,fmt=53)TIMESET
         116=116+1
С
   Get WATCH - standard ground level
         TYPE *,' '
TYPE *,' '
         TYPE *, '
TYPE *, '
                   ,
         W = A(1)/NAVE
         WATCH = W - 100,
WRITE( 8,12030 )WATCH
         TYPE *,' '
TYPE *,' '
        TYPE *,' '
TYPE *,' '
12030 format( 'Minimum acceptable ground level =',F)
        SCANSTEP = 1000*SCANSTEP
         INDXSTEP = 1000*INDXSTEP
         CALL SETXYZ( SCANSTEP, INDXSTEP, ZSTEP )
WRITE(5,12140)
12140 format(/// ### SCANNING ###//)
         IDIR-1
         WWFLAG=0
        do 2600 noth_I = 1,4
                                  ! nothickness mod
        if (noth_l.ge.2)then
        CALL MOVORGXY (ZIGANS, SCANAXIS, NSCAN, INDXAXIS, NINDX)
         REWIND(12) ! .DATHS FILE
         IF (ZIGANS.EQ.'Y')ZIGCOUNT=1
        ENDIF
       IF (NOTH_LEQ.4)THEN

type *,' '

type *,' '

type *,' '

type *,' ******* Finished w/ Sample Scan ************

type *,' **** Remove Sample from tray & Hit <RET> to perform water scan'

type *,' '
        type *,'
type *,'
```

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Read (5,10020) IO

ENDIF

DO 2400 I=I.NINDX

DO 2200 J=1,NSCAN

! Outer loop over index ! Inner loop over scan

IF (NOTH\_I.ge.2)THEN READ(12)JJ,II,FLAG,SCANKNT !READ WHETHER 'H' OR 'S'

type \*,' type \*,' ' type \*,' ' type \*,'FLAG =',FLAG type \*,' ' type \*,'second time around for', jj,ii type \*,' '

# ENDIF

IF ((SCANMODE.EQ.'P'.OR.SCANMODE.EQ.'L').AND.I.GT.1)GOTO 2400 IMOD FOR LINE / POINT

SCAN

IF (NOTH\_I.EQ.1)TYPE \*,'I= ',I,' AND J=',J PLACE=PLACE+1 WRITE( 8,13000 )J,I,PLACE IF (SHAPEANS.EQ.'N')THEN CALL TAKEDATA\_O(FILENAME, VOLANS, UOLANS, VOL, 116, 117, 126, 127, 1 136,137,146,147,NAVE,WATCH,I,J,noth\_I,SLANTI, 1 SLANT2, SLANT3, SLANT4, SCANSTEP, INDXSTEP, ZIGANS, NSCAN) ELSEIF (SHAPEANS.EO,'Y')THEN CALL TAKEDATA(PLACE,SCHEME,TSCHEME,VOLANS,VOL,UZEROO,FILENAME, UOLANS,126,127,NOTH\_1,136,137,146,147, 1 SLANTI, SLANT2, SLANT3, SLANT4, SCANSTEP, INDXSTEP, ZIGANS, NSCAN, 1 1 RCMAX,MAXFS1P,MAXVALF,RF1,RF2,MAXFS1PT,MAXVALT,RT1,RT2,I16,I17, NAVE, WATCH, J, I, 115, IT) 1 ENDIF

3429 CONTINUE IF (NOTH I.EQ.1.AND.IT.LT.4)THEN TYPE \*,'II6= ',II6,' II7= ',II7

ELSEIF (NOTH I.EQ.1.AND.IT.EQ.4)THEN TYPE \*,'I46= ',I46,' 147= ',147 ENDIF

IF( J.EQ.NSCAN )GOTO 2200

IF (LOOPANS.EQ.'N')GOTO 22001 IDON'T PICK UP XDUCER EACH TIME

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IF (NOTH\_I.EQ.1)TYPE \*,'IT=',IT IF (NOTH\_LEQ.1)TYPE \*,' '

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25

ENDIF

CONTINUE

CONTINUE

12305 CONTINUE

2200 CONTINUE

CALL WAIT2(1000) CALL WAIT2(1000)

12306

C\*\*\*\* \*\*\*\*

2402

с

IF (NOTH\_I.EQ.1)TYPE \*,' '

t ----IF( I.EQ.NINDX )GOTO 2400

CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000)

IF (ZIGANS.EQ.'Y')GOTO 12305

IF (LOOPANS.EQ.'N')GOTO 2200

INOTHICK

C IFOR LINE SCAN OR POINT MEASURE, DON'T MOVE Y-AXIS

CALL MOVXYZ(INDXAXIS, 1) ! Move

ţ

5

IF (SCANMODE.EQ.'P'.OR.SCANMODE.EQ.'L')GOTO 2401

IF (NOTH\_I.EQ.1)TYPE \*, 'VOLANS (WRT "ON SAMPLE")= ', VOLANS IF (NOTH\_I.EQ.1)TYPE \*,'UOLANS (WRT "NOT ON SAMPLE)=',UOLANS IF (NOTH\_I.EQ.1)TYPE \*,' '

IF (SCANMODE.EQ.'P')GOTO 12306 !FOR POINT MEASURE, DON'T MOVE X-AXIS

ELSEIF (ZIGANS.EQ.'Y'AND.ZIGCOUNT.EQ.I)THEN IF (SCANMODE.EQ.'P')GOTO 12306 FOR POINT MEASURE, DON'T MOVE X-AXIS

KLINGER STAGES STOP MOVING

IF (SCANMODE.EQ.'P')GOTO 2402 IFOR POINT MEASURE, DON'T MOVE X-AXIS

CALL WAIT2(1000) ADD DELAY SO THAT DATA IS NOT TAKEN BEFORE

22001 IF (ZIGANS.EQ.'Y'.AND.ZIGCOUNT.EQ.0)THEN !ZIGZAG SCAN

CALL MOVXYZ(SCANAXIS,-1) ! MOVE X-AXIS BACKWARD

CALL MOVXYZ(SCANAXIS,1) !MOVE X-AXIS FORWARD

CALL WAIT2(1000) CALL WAIT2(1000)

CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) CALL WAIT2(1000) 2401 NTOGO = NINDX-I I IF (ZIGANS.EQ.'N')THEN !NORMAL SCAN CALL MOVORG(SCANAXIS,NSCAN, VOLTAGEL, VOLTAGEU, LOOPTHRU\_H) !Move back to the X origin 1 ELSEIF (ZIGANS.EQ.'Y')THEN IF (ZIGCOUNT.EQ.I)THEN ZIGCOUNT=0 GOTO 15021 ELSEIF(ZIGCOUNT.EQ.0)THEN ZIGCOUNT=1 ENDIF ENDIF 15021 CONTINUE INOTHICK 2400 CONTINUE ! ----2600 continue CALL TIME(TBUF) WRITE( 8,13100 )TBUF CLOSE(8) CLOSE(6) CLOSE(14) IF (SCANMODE.EQ.'L'.OR.SCANMODE.EQ.'P')JXXX=1 IMOD FOR LINE SCAN & POINT MEASURE WRITE(15,REC-115,FMT=52)JXXX 115=115+1 С ENDIF STOP

13000 format('',13,13,15) 13100 format('',A8)

end

SUBROUTINE TAKEDATA\_O(FILENAME,VOLANS,UOLANS,VOL,116,117,126,127, 1 136,137,146,147,NAVE,WATCH,LJ,noth\_I,SLANTI, 1 SLANT2,SLANT3,SLANT4,SCANSTEP,INDXSTEP,ZIGANS,NSCAN) integer\*2 A(512), WFLAG,116,126,WWFLAG,I,J,ILOCX,NSCAN,ILOCY,136,146 INTEGER\*4 I17SUB,117,127,SCANSTEP,INDXSTEP INTEGER\*4 I17SUB,117,127,SCANSTEP,INDXSTEP

INTEGER\*4 I27SUB,I37SUB,I47SUB

30

```
real DELAY(0:4), VOLTSET(0:4), VOLTAGE(4), VOL(4), SLANTI, SLANT2, SLANT
       REAL SLANT3, SLANT4
       character DAY*9, TIM*9, VOLANS*1, UOLANS*1, C1*80, FILENAME*34, ZIGANS*1
   common /SBLK/ A, DELAY, VOLTSET, MAI
С
       DATA 114/0/
С
                if (noth_I.eq.1)then
                OPEN(unit=14, file-'[ROTH.MENU]DONSCAN_INTERP.LOG',
   t
                        status='NEW', ACCESS='SEQUENTIAL',
                        FORM='UNFORMATTED')
   +
               endif
С
51
       FORMAT(A32)
       FORMAT(A2)
52
53
       FORMAT(A4)
54
        FORMAT(A2)
        WFLAG = 0
10600 format('',115)
       if (noth_I.eq.1)then
       IX=1
       IY=I
       clseif (noth_1.eq.2)THEN
       IX=2
       IY-2
        elseif (noth_1.eq.3)THEN
        IX=3
       [Y=3
       elseif (noth_1.eq.4)THEN
       IX≈4
       IY=4
       ENDIF
       DO 600 IT → IX,IY
        IF (IT.EQ.1.OR.IT.EQ.2)THEN
        SLANTX=SLANTI
        SLANTY=SLANT3
        ELSEIF (IT.EQ.3.OR.IT.EQ.4)THEN
        SLANTXR=SLANT2
        SLANTYR=SLANT4
        ENDIF
C ***** MODIFICATION FOR ZIGZAG SCAN *********************************
       IF (ZIGANS.EQ.'Y')THEN
        IF (I.EQ.2.OR.I.EQ.4.OR.I.EQ.6.OR.I.EQ.8.OR.I.EQ.10
   1.OR.I.EQ.12.OR.I.EQ.14.OR.I.EQ.16.OR.I.EQ.18.OR.I.
   1 EQ.20.OR.I.EQ.22.OR.I.EQ.24.OR.I.EQ.26.OR.I.EQ.28.OR.
  1 I.EQ.30.OR.I.EQ.32.OR.I.EQ.34.OR.I.EQ.36.OR.I.EQ.38.
1 OR.I.EQ.40.OR.I.EQ.42.OR.I.EQ.44.OR.I.EQ.46.OR.I.EQ.
1 48.OR.I.EQ.50.OR.I.EQ.52.OR.I.EQ.54.OR.I.EQ.56.OR.
   1 J.EQ.58.OR.I.EQ.60.OR.I.EQ.62.OR.I.EQ.64.OR.I.EQ.66
   1.OR.I.EQ.68.OR.I.EQ.70.OR.I.EQ.72.OR.I.EQ.74.OR.I.
   1 EQ.76.OR.I.EQ.78.OR.I.EQ.80.OR.I.EQ.82.OR.I.EQ.84.OR
```

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1 .I.EQ.86.OR.I.EQ.88.OR.I.EQ.90.OR.I.EQ.92.OR.I. 1 EQ.94.OR.I.EQ.96.OR.I.EQ.98.OR.I.EQ.100)THEN ILOCX-NSCAN-J IFOR ZIGZAG SCAN, REVERSE BACK FOR DISPLAY ELSE ILOCX=J-1 ENDIF elscif(zigans.eq.'N')then !george wood addition ILOCX=J-I !George Wood addition ENDIF ILOCY=I-I IF (IT.EQ.I.OR.IT.EQ.2)THEN CORRECT DELAY WINDOW FOR NONLEVELNESS DELAY\_CORR=DELAY(IT)+(SLANTX\*ILOCX\*SCANSTEP)+(SLANTY\*II.OCY\*INDXSTEP) ELSEIF (IT.EQ.3.OR.IT.EQ.4)THEN DELAY\_CORR=DELAY(IT)+(SLANTXR\*ILOCX\*SCANSTEP)+(SLANTYR\*ILOCY\*INDXSTEP) ENDIF TYPE \*,' ' TYPE \*,' ' TYPE \*,' ' TYPE \*,'J=',J,' DELAY(',IT,')= ',DELAY(IT) TYPE \*,'DELAY\_CORR= ',DELAY\_CORR TYPE \*,' ' TYPE \*,' ' CALL PUTTIME( DELAY CORR ) ! Set delay 100 CONTINUE IF ((IT.NE.4.AND.VOLANS.EQ.'U').OR.(IT.EQ.4.AND.UOLANS.EQ.'U'))THEN С **!!!! USER-DEFINED VOLTAGE SETTINGS** VOLTS=VOL(IT) CALL SETVOLTDIV(VOLTS) GOTO 1132 ENDIF CALL AUTOSETVOLTS( MAI, VOLTS, NUMINT ) ! Set V/D 1132 IF((VOLTS.GT.1.0).OR.(VOLTS.LT.0.01))THEN WRITE(5,1131)VOLTS FORMAT('+','BAD VOLTAGE SETTING',E10.5) 1131 CALL TEKRESET(MAI) GOTO 100 ENDIF CALL GETSA(NAVE,MAI,A) ! Get waveform WATCHI = A(1)/ NAVE ! Make sure its acceptable TYPE \*,' ' TYPE \*,' ' TYPE \*, ' WRITE(5,1133)WATCH1,WATCH 1133 FORMAT('+','CURRENT WATCH LEVEL IS',F10.5,'MIN =',F10.5) TYPE \*.' TYPE \*

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IF ((IT.NE.4.AND.VOLANS.EQ.'U').OR.(IT.EQ.4.AND.UOLANS.EQ.'U'))GOTO 56732

**!!!! USER-DEFINED VOLTAGE SETTINGS** 

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IF (VOLANS.EQ.'U')GOTO 56732 II SKIP WATCH IF( WATCHILT.WATCH )THEN WWFLAG - WWFLAG+1 IF (WWFLAG.EQ.1)THEN OPEN( unit=88, file='[ROTH.MENU]DONSCAN.LOG', status='NEW') + ENDIF WRITE( 5,10200 ) CALL TIME(TIM) CALL DATE(DAY) TYPE \*,' ' TYPE \*,' ' TYPE \*,' ' type \*,'watch1=',watch1,' < watch=',watch TYPE \*. TYPE \*, ' TYPE \*, ' TYPE \*,' ' WRITE( 88,10201 )FILENAME, DAY, TIM, J, I, CI format('',A,'',A,' X=',I3,' Y=',I2,'MAY LEAD TO BAD PROPERTY VALUE') format(' WAVEFORM BELOW "WATCH",MAY LEAD TO BAD PROPERTY VALUE') 10201 10200 GOTO 100 ENDIF 56732 CONTINUE IF (noth\_I.eq.1)then WRITE(16,REC=116,FMT=53)DELAY\_CORR 500 116=[16+1 WRITE(16,REC=116,FMT=53)VOLTS 116=116+1 С DO 54321 IJI=1,512 I17SUB=((I17-1)\*512)+IJI 54321 WRITE(17,REC=117SUB,FMT=54) A(1JI) 117=I17+1 elseif (noth\_1.eq.2)then 5500 WRITE(26,REC=I26,FMT=53)DELAY\_CORR 126=126+1 WRITE(26,REC=126,FMT=53)VOLTS 126=126+1 С DO 54329 IJI-1,512

- I27SUB=((I27-1)\*512)+IJI 54329 WRITE(27,REC=I27SUB,FMT=54) A(IJI)
- 9

TYPE \*,' '

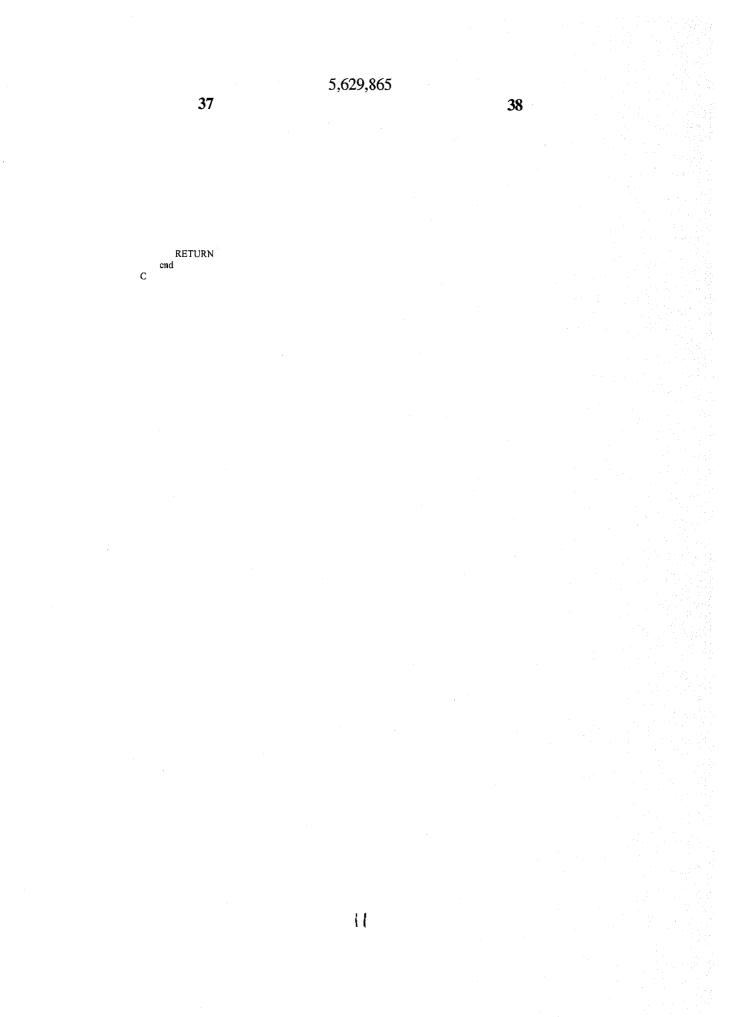
С С

С

#### 127=127+1

elseif (noth\_I.eq.3)then

5800 WRITE(36,REC=I36,FMT=53)DELAY\_CORR 136-136+1 WRITE(36,REC=J36,FMT=53)VOLTS 136=136+1 С DO 58329 IJI=1,512 I37SUB=((I37-1)\*512)+IJI WRITE(37,REC=137SUB,FMT=54) A(IJI) 58329 137=137+1 elseif (noth\_1.cq.4)then 5900 WRITE(46,REC=146,FMT=53)DELAY\_CORR 146=146+1 WRITE(46,REC=146,FMT=53)VOLTS 146-146+1 С DO 59329 IJI=1,512 I47SUB=((I47-1)\*512)+IJI 59329 WRITE(47, REC=147SUB, FMT=54) A(IJI) 147=147+1 endif IF (IT.EQ.1)VOLTAGE(1)=VOLTS IF (IT.EQ.2)VOLTAGE(2)=VOLTS IF (IT.EQ.3)VOLTAGE(3)=VOLTS IF (IT.EQ.4)VOLTAGE(4)=VOLTS C\*\*\*\*\*\*\* 600 CONTINUE IF (I.EQ.0.AND.J.EQ.0) GOTO 20000 !SKIP NEXT STEP (NOISE MEASURE) C C CHECK FOR ERROR IN FS2 VOLTSET с IF (VOLTAGE(1).EQ..01) THEN WRITE (14) I.J.' VOLT FOR FS2=', VOLTAGE(1), ¢ + '#INT.PO.= ',NUMINT с с **GOTO 100** ENDIF с С С CHECK FOR ERROR IN B1 VOLTSET С С IF (VOLTAGE(1).LT.VOLTAGE(2)) THEN WRITE (14) I,J,' VOLT FOR B1= ',VOLTAGE(1), '#INT.PO.= ',NUMINT с с ÷ C **GOTO 100** ENDIF ¢ 7 FORMAT (A4) \*\*\*\*\*\*\*\* C\*\*\*\*\*\*\*\*\* 20000 CONTINUE



1 UOLANS, 126, 127, NOTH\_1, 136, 137, 146, 147, SLANT1, SLANT2, SLANT3, SLANT4, SCANSTEP, INDXSTEP. ZIGANS, NSCAN, 1 RCMAX,MAXFS1P,MAXVALF,RF1,RF2,MAXFS1PT,MAXVALT,RT1,RT2,I16, 1 I17,NAVE,WATCH,J,I,I15,IT) 1 integer\*2 A11(512),I26,I,J,ILOCX,NSCAN,WFLAG,I16,MAXFS1PT,PLACE INTEGER\*2 WATCH\_COUNT, IIIT, ILOCY, I36, I46 INTEGER\*2 MAXFSIP,NAVE,A(512),IT,SCANKNT INTEGER\*4 117SUB,117,ISTAT,127,SCANSTEP,INDXSTEP,137,147 INTEGER\*4 I27SUB,I37SUB,I47SUB REAL\*4 ASPECF1(1024),PHASE(1024),MAXVALF,MAXVALT,VOL(3),SLANT3,SLANT4 real\*4 DELAY(0:4),VOLTSET(0:4),VOLTAGE(4),SLANT,SLANT1,SLAN12,F1(512) COMPLEX CF1(1024),CSPEC(1024) character SCHEME\*1,FLAG\*1,FILENAME\*34,UOLANS\*1,ZIGANS\*1 CHARACTER VOLANS\*1.TSCHEME\*1 common /SBLK/ A, DELAY, VOLTSET, MAI С DATA 114/0/IIJT/0/ С IF (NOTH\_I.EQ.1)THEN OPEN( unit=14, file="[ROTH.MENU]DONSCAN INTERP.LOG', status='NEW', ACCESS='SEQUENTIAL', -ŀ FORM='UNFORMATTED') + ENDIF С 51 FORMAT(A32) 52 FORMAT(A2) 53 FORMAT(A4) 54 FORMAT(A2) WFLAG = 0С WATCH\_COUNT=0 10600 format(",115) IF (noth 1.eq.1.and.PLACE.EQ.1)THEN OPEN(unit=12, file=FILENAME//'HS', status='NEW', + form='UNFORMATTED', ORGANIZATION='SEQUENTIAL') SCANKNT=0 ENDIF if (noth\_l.cq.1)then IX=1 IY=1elseif (noth\_I.eq.2)THEN IX=2 IY=2 elseif (noth\_1.eq.3)THEN 1X=3IY=3elseif (noth\_1.eq.4)'THEN IX=4 IY=4ENDIF

12

SUBROUTINE TAKEDATA(PLACE,SCHEME,TSCHEME,VOLANS,VOL,UZEROO,FILENAME,

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#### 10386 DO 600 IT - IX,IY

IF (ZIGANS.EQ.'Y')THEN IF (I.EQ.2.OR.I.EQ.4.OR.I.EQ.6.OR.I.EQ.8.OR.I.EQ.10 1. OR.I.EQ.12. OR.I.EQ.14. OR.I.EQ. 16. OR.I.EQ. 18. OR.I. 1 EQ.20.OR.I.EQ.22.OR.I.EQ.24.OR.I.EQ.26.OR.I.EQ.28.OR. 1 LEQ.30.OR.I.EQ.32.OR.I.EQ.34.OR.I.EQ.36.OR.I.EQ.35 1 OR.I.EQ.40.OR.I.EQ.42.OR.I.EQ.44.OR.I.EQ.46.OR.I.EQ. 1 48.OR.I.EQ.50.OR.I.EQ.52.OR.I.EQ.54.OR.I.EQ.56.OR. 1 I.EQ.58.OR.I.EQ.60.OR.I.EQ.62.OR.I.EQ.64.OR.I.EQ.66 1.OR.I.EQ.68.OR.I.EQ.70.OR.I.EQ.72.OR.I.EQ.74.OR.I. 1 EQ.76.OR.I.EQ.78.OR.I.EQ.80.OR.I.EQ.82.OR.I.EQ.84.OR 1.1.EQ.86.OR.I.EQ.88.OR.I.EQ.90.OR.I.EQ.92.OR.I. 1 EQ.94.OR.I.EQ.96.OR.I.EQ.98.OR.I.EQ.100)THEN ILOCX=NSCAN-J !FOR ZIGZAG SCAN, REVERSE BACK FOR DISPLAY ELSE ILOCX=J-1 ENDIF elseif(zigans.eq.'N')then !george wood addition ILOCX-J-1 !George Wood addition ENDIF ILOCY=I-I

IF (IT.EQ.1.OR.IT.EQ.2)THEN SLANTX=SLANT1 SLANTY=SLANT3 ELSEIF (IT.EQ.3.OR.IT.EQ.4)THEN SLANTXR=SLANT2 SLANTYR=SLANT4 ENDIF

IF (NOTH\_LEQ.1)TYPE \*,' ' IF (NOTH\_LEQ.1)TYPE \*,'IT=',IT IF (NOTH\_LEQ.1)TYPE \*,'PLACE=',PLACE IF (NOTH\_LEQ.1)TYPE \*,'SCHEME=',SCHEME IF (NOTH\_LEQ.1)TYPE \*,' '

IF (IT.EQ.1.OR.IT.EQ.2)THEN !CORRECT DELAY WINDOW FOR NONLEVELNESS DELAY\_CORR=DELAY(IT)+(SLANTX\*ILOCX\*SCANSTEP)+(SLANTY\*ILOCY\*INDXSTEP) ELSEIF (IT.EQ.3.OR.IT.EQ.4)THEN DELAY\_CORR=DELAY(IT)+(SLANTXR\*ILOCX\*SCANSTEP)+(SLANTYR\*ILOCY\*INDXSTEP) ENDIF

TYPE \*.' ' TYPE \*,' ' TYPE \*,'-',J=',J,' DELAY(',IT,')=',DELAY(IT) TYPE \*,'DELAY\_CORR=',DELAY\_CORR TYPE \*,' ' TYPE \*,' ' TYPE \*,' '

. . .....

	VOLTS=VOL(2) CALL SETVOLTDIV(VOLTS) ENDIF IF (VOLANS.EQ.'A')CALL AUTOSETVOLTS( MAI, VOLTS, NUMINT )!Set V/D GOTO 1132 ENDIF
C IKI	EP TRACK OF POSITION WHERE DATA IS ACTUALLY TAKEN WITH A COUNTER IF (IT.EQ.1.AND.PLACE.GE.1.AND.SCHEME.EQ.'X')SCANKNT=SCANKNT+1 IF (NOTH_I.EQ.1)TYPE *,' IF (NOTH_I.EQ.1)TYPE *,' X=',I,' Y=',I,' SCANKNT=',SCANKNT IF (NOTHI_I.EQ.1)TYPE *,' '
	CALL PUTTIME( DELAY_CORR ) ! Set delay AS USUAL
100	CONTINUE
1	IF ((VOLANS.EQ.'U'.AND.(IT.EQ.1.OR.IT.EQ.2.OR.IT.EQ.3)).OR. (UOLANS.EQ.'U'.AND.IT.EQ.4))THEN !!! USER-DEFINE VOLTAGE SETTINGS VOLTS=VOL(IT) CALL SETVOLTDIV(VOLTS) GOTO 1132 ENDIF
1132 1131	CALL AUTOSETVOLTS( MAI, VOLTS, NUMINT ) ! Set V/D IF((VOLTS.GT.1.0).OR.(VOLTS.LT.0.01))THEN WRITE(5,1131)VOLTS FORMAT(+','BAD VOLTAGE SETTING',E10.5) CALL TEKRESET(MAI) GOTO 100 ENDIF
1133	CALL GETSA(NAVE,MAI,A) ! Get waveform WATCH1 = A(1)/ NAVE ! Make sure its acceptable TYPE *, ' TYPE *, ' WRITE(5,1133)WATCH1,WATCH FORMAT('+','CURRENT WATCH LEVEL IS',F10.5,'MIN =',F10.5) TYPE *, ' TYPE *, '

IF (VOLANS.EQ.'U'.OR.UOLANS.EQ.'U')GOTO 56732 !! SKIP WATCH

DELAY\_CORR=DELAY(2)+(SLANTX\*ILOCX\*SCANSTEP)+(SLANTY\*ILOCY\*INE CALL PUTTIME(DELAY\_CORR) ! Set dolay FOR B2

IF (PLACE.GE.1.AND.SCHEME.EQ.'B'.AND.NOTH\_I.EQ.1)THEN IIIT=2 !CORRECT DELAY WINDOW FOR NONLEVELNESS DELAY\_CORR=DELAY(2)+(SLANTX\*ILOCX\*SCANSTEP)+(SLANTY\*ILOCY\*INDXSTEP)

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!!! USER-DEFINE VOLTAGE SETTINGS? IF (VOLANS.EQ.'U')THEN

IF( WATCH1.LT.WATCH )THEN WFLAG = 1 WRITE( 5,10200 ) FLAG='H' !H = SAMPLE HOLDER TYPE \*,'FLAG=',FLAG С C !COUNTER FOR BAD WATCH LEVEL, IE. ON WHICH WAVEFORM (BI OR B2) DOES IT OCCUR С С IF (SCHEME.EQ.'X'.AND.IT.EQ.1)WATCH\_COUNT=1 с IF (SCHEME.EQ.'X'.AND.IT.EQ.2)WATCH\_COUNT=2 TYPE \*, WATCH\_COUNT=', WATCH\_COUNT č GOTO 20000 format(' ',A,' ',A,' X= ',I3,' Y= ',I3 ) format(' WAVEFORM BELOW "WATCH", GOING TO NEXT SCAN POINT') 10201 10200 GOTO 100 C ENDIE C\*\*\*\*\*\*\* \*\*\*\*\*\*\* 56732 CONTINUE C\*\*\*\*\*\*\*\*\* \*\*\*\*\* IF (NOTH LEQ.1)TYPE \*,' ' IF (NOTH\_I.EQ.I)TYPE \*,'PLACE-',PLACE IF (NOTH\_I.EQ.I)TYPE \*,'SCHEME=',SCHEME IF (NOTH\_I.EQ.I)TYPE \*,'TSCHEME=',TSCHEME IF (NOTH\_I.EQ.1) TYPE \*,'ZEROO=',ZEROO IF (NOTH\_I.EQ.1) TYPE \*,'ZEROO=',ZEROO IF (NOTH\_I.EQ.1) TYPE \*,'IIIT=',IIIT IF (NOTH\_I.EQ.1) TYPE \*,'WATCH\_COUNT=',WATCH\_COUNT IF (NOTH\_I.EQ.1) TYPE \*,' С C \*\*\*\* EXAMINE B2(t) APPROACH FOR SAMPLE HOLDER \*\*\*\*\*\*\* C IF (PLACE.GE.I.AND.SCHEME.EQ.'B'.AND.IIIT.EQ.2)THEN AA = 0.DO 499 III=1,512 ! Subtract average from wave, A11(III)=A(III)AII(III)=A11(III)/NAVE 499 AA=AA + A11(III)! REALWAVE = Waveform in volts ZERO = AA/512. IF (NOTH\_LEQ.1)TYPE \*, 'ZERO-', ZERO FF-0. DO 599 III=1,512 F1(III) = ( REAL(A11(III)) - ZERO )\*( VOLTS )\*10./512. FF=FF ABS(F1(III)) 599 ZEROO=FF/512. IF (NOTH\_LEQ.1) TYPE \*,' ' IF (NOTH\_I.EQ.1)TYPE \*,'ZEROO=',ZEROO IF (NOTH I.EQ.1)TYPE \*,' ' C SET UZEROO = 2\*(FIRST "NOISE" LEVEL DETECTED --> ASSUME WE ARE STARTING С ON SAMPLE HOLDER) IF (TSCHEME.EQ.'A'.AND.PLACE.EQ.I)THEN UZEROO=2\*ZEROO IF (NOTH\_1.EQ.1)TYPE \*,' ' IF (NOTH\_I.EQ.I)TYPE \*,' AUTO THRESHOLD VOLTAGE NOISE LEVEL =',UZEROO IF (NOTH\_I.EQ.I)TYPE \*,'

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ELSEIF (TSCHEME.EQ.'M'.AND.PLACE.EQ.1)THEN IF (NOTH\_I.EQ.1)TYPE \*,' ' IF (NOTH\_I.EQ.1)TYPE \*,' MANUALLY-SET THRESHOLD VOLTAGE NOISE LEVEL =',UZEROO IF (NOTH\_I.EQ.1)TYPE \*,' ' ENDIF C \*\*\*\*\* \*\*\*\*\*\* IF (ZEROO.LT.UZEROO)THEN !!!< EX..002 VOLTS - ON SAMPLE HOLDER 56120 FLAG='H' !H = SAMPLE HOLDER IF (NOTH\_I.EQ.1)TYPE \*, 'FLAG=', FLAG GOTO 20000 ELSEIF (ZEROO.GE.UZEROO)THEN !!!> EX..002 VOLTS - ON SAMPLE 56121 FLAG='S' IS = SAMPLE IF (NOTH\_1,EQ.1)TYPE \*,'FLAG=',FLAG SCHEME-'X' GOTO 10386 ISTART TAKEDATA LOOP AGAIN ENDIF ENDIF IF (NOTH I.EQ.1)THEN 500 WRITE(16,REC=116,FMT=53)DELAY\_CORR 116=116+1 WRITE(16,REC=116,FMT=53)VOLTS I16=I16+1 С DO 54321 IJI=1,512 117SUB=((117-1)\*512)+IJI 54321 WRITE(17,REC=117SUB,FMT=54) A(IJI) 117=117+1 elseif (noth\_1.eq.2)then 5500 WRITE(26,REC=I26,FMT=53)DELAY\_CORR 126=126+1 WRITE(26,REC-126,FMT-53)VOLTS 126=I26+1 С DO 54329 IJI=1,512 127SUB=((I27-1)\*512)+IJI 54329 WRITE(27,REC=127SUB,FMT=54) A(IJI) 127=127+1 elseif (noth\_Leq.3)then 5800 WRITE(36,REC=I36,FMT=53)DELAY\_CORR I36=I36+1 WRITE(36,REC=I36,FMT=53)VOLTS 136=136+1 С DO 58329 IJI=1,512 I37SUB-((I37-1)\*512)-IJI WRITE(37,REC=137SUB,FMT=54) A(IJI) 58329 137=137+1

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elseif (noth\_I.eq.4)then

5900 WRITE(46,REC=146,FMT=53)DELAY\_CORR 146=146+1 WRITE(46,REC=146,FMT-53)VOLTS 146=146+1 C DO 59329 IJI=1,512 147SUB=((147-1)\*512)+IJI 59329 WRITE(47,REC=147SUB,FMT=54) A(IJI) 147=147+1

endif

С WRITE( 8,10600 )A(200) С C\*\*\* IF (IT.EQ.1)VOLTAGE(1)=VOLTS IF (IT.EQ.2)VOLTAGE(2)=VOLTS IF (IT.EQ.3)VOLTAGE(3)=VOLTS IF (IT.EQ.4)VOLTAGE(4)=VOLTS C\*\*\*\*\*\*\* 600 CONTINUE C\*\*\*\* 7 FORMAT (A4) 20000 IF( WFLAG.EQ.1 )THEN CLOSE(8) OPEN( unit=8, file="I'XA1:', status='OLD' ) ENDIF IF (SCHEME.EQ.'X')SCHEME='B' !RESET BACK TO 'B' FOR NEXT SCAN POINT С IF (I.NE.0.AND.J.NE.0)THEN C !RESET COUNTERS TO EXCLUDE DATA GATHERED ON POINT C WHERE BAD WATCH LEVEL WAS FOUND IF (WATCH\_COUNT.EQ.I)THEN IBI HAD BAD WATCH LEVEL Ċ С SCANKNT=SCANKNT-1 ¢ 116=116-2 С 117=117-1 С С С ELSEIF (WATCH\_COUNT.EQ.2)THEN 182 HAD BAD WATCH LEVEL SCANKNT-SCANKNT-I 116=116-4 С 117=117-2 С ENDIF if (noth\_1.eq.1)WRITE(12)J,I,FLAG,SCANKNT INOTE LOCATION WITH FLAG & LEAVE SUBR. IF (NOTH\_I.EQ.I)TYPE \*,' ' IF (NOTH\_I.EQ.I)TYPE \*,' ' IF (NOTH\_I.EQ.I)TYPE \*,' ' IF (NOTH\_I.EQ.1)TYPE \*'NOW IN TAKEDATA:','X=',J,' Y=',I,' FLAG=',FLAG IF (NOTH\_I.EQ.1)TYPE \*', '

IF (NOTH\_I.EQ.1)TYPE \*; ' IF (NOTH\_I.EQ.1)TYPE \*; ' IF (NOTH\_I.EQ.1)TYPE \*; ' ENDIF

C WATCH\_COUNT=0 RETURN end

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SUBROUTINE PRESSURE(VOLTAGEL, VOLTAGEU)
С
C **** PRESSURE=20*VOLTAGE **** (PLOWER.LE.VOLTAGE.GE.PUPPER)
С
C
C
C
C
      Adjust Z axis to get good pressure (PSI)
        <<< 11 = DOWN >>>
       PUPPER -- .85 ! Upper Pressure = 17
00000000
       PLOWER = .75 ! Lower Pressure = 15
       PUPPER = .3 ! UPPER PRESSURE = 6
PLOWER = .2 ! LOWER PRESSURE = 4
       PUPPER = .5
                     ! UPPER PRESSURE = 10
       PLOWER = .4
                     !
                       LOWER PRESSURE = 8
       PLOWER = .5 !
                       LOWER PRESSURE = 10
       PUPPER = .6
                       UPPER PRESSURE = 12
                     1
C
C
C
       PLOWER = .7 ! LOWER PRESSURE = 14
       PUPPER = .8
                    ! UPPER PRESSURE = 16
       PLOWER = .6 ! LOWER PRESSURE = 12
С
       PUPPER = .61 ! UPPER PRESSURE = 12.2
       PLOWER=VOLTAGEL
       PUPPER=VOLTAGEU
       CALL GETFLUKE( P )
 200
       IF( P.GE.PLOWER AND. P.LE.PUPPER )GOTO 900
       IF( P.LT.PLOWER )CALL MOVXYZ( 3, 1 )
       IF( P.GT.PUPPER )CALL MOVXYZ( 3, -1 )
       GOTO 200
 900 RETURN
       end
С
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SUBROUTINE PRESSURE MAX(VOLTAGE\_MAX,LLL,FILENAME,J,I,115,CHECKP) с **CHARACTER FILENAME\*34** INTEGER\*2 CHECKP, LLL, LINCR, I, J, JXXX, 115, 11TT 52 FORMAT(A2) P\_MAX=VOLTAGE\_MAX CALL GETFLUKE(P) 200 IF( P.GT.P\_MAX)THEN CHECKP=CHECKP+1 IF (CHECKP.EQ.1)LINCR=LLL/3 IF (CHECKP.EQ.2)LINCR=LLL/2 IF (CHECKP.EQ.2)LINCR=1000 DO 2900 ITTT=1,LINCR 2900 CALL MOVXYZ(3,-1) !3 IS Z-AXIS, MOVE Z-AXIS UP IF (CHECKP.EQ.3)THEN JXXX-1-1 11 IS Y-LOC; GO BACK TO PREVIOUS ROW WRITE(15,REC-I15,FMT=52)JXXX 115-115+1 STOP ENDIF ENDIF 900 RETURN end С

C C

С

C

С

C C C

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SUBROUTINE MOVORG( SCANAXIS, NSTEPS, VOLTAGEL, VOLTAGEU, 1 LOOPTHRU\_H) Run the thing back to the SCANAXIS origin integer\*4 SCANAXIS integer\*2 NSTEPS,LOOPTHRU\_H DO 1000 K=1,LOOPTHRU\_H C 1000 CALL MOVXYZ( 3,-1 ) ! Move up DO 1200 K=1,NSTEPS-1 1200 CALL MOVXYZ( SCANAXIS, -1 ) ! Move back DO 1400 K=1,LOOPTHRU\_H CALL MOVXYZ(3,1) ! Move down C 1400 CALL MOVXYZ(3,1) ! Move down C CALL PRESSURE(VOLTAGEL, VOLTAGEU) !nothick CALL MOVXYZ( SCANAXIS, -1 ) ! Move back & forth CALL MOVXYZ( SCANAXIS, 1 ) RETURN end SUBROUTINE MOVORGXY( ZIGANS, SCANAXIS, NSCAN, INDXAXIS, NINDX) Run the thing back to the SCAN origin CHARACTER ZIGANS\*1 integer\*4 SCANAXIS, INDXAXIS integer\*2 NSCAN,NINDX,I IF (ZIGANS.EQ.'Y')THEN I=Nindx IF (I.EQ.1.OR.I.EQ.3.OR.I.EQ.5.OR.I.EQ.7.OR.I.EQ.9 1.OR.I.EQ.11.OR.I.EQ.13.OR.I.EQ.15.OR.I.EQ.17.OR.I. 1 EQ.19.OR.I.EQ.21.OR.I.EQ.23.OR.I.EQ.25.OR.I.EQ.27.OR. 1 LEQ.29.OR.LEQ.31.OR.LEQ.33.OR.LEQ.35.OR.LEQ.37. 1 OR.LEQ.39.OR.LEQ.41.OR.LEQ.43.OR.LEQ.45.OR.LEQ. 1 47.OR.LEQ.49.OR.LEQ.51.OR.LEQ.53.OR.LEQ.55.OR. 1 I.EQ.57.OR.I.EQ.59.OR.I.EQ.61.OR.I.EQ.63.OR.I.EQ.65 1 .OR.I.EQ.67.OR.I.EQ.69.OR.I.EQ.71.OR.I.EQ.73.OR.I. 1 EQ.75.OR.I.EQ.77.OR.I.EQ.79.OR.I.EQ.81.OR.I.EQ.83.OR 1. J.EQ.85.OR.I.EQ.87.OR.I.EQ.89.OR.I.EQ.91.OR.I. 1 EQ.93.OR.I.EQ.95.OR.I.EQ.97.OR.I.EQ.99)THEN DO 1200 K=1,NSCAN-1 1200 CALL MOVXYZ(SCANAXIS, -1) ! Move back X ENDIF ENDIF DO 1400 K=1,NINDX-1 1400 CALL MOVXYZ(INDXAXIS, -1) ! Move back Y

21

RETURN end

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SUBROUTINE ENTERPARAM( SCANSTEP.INDXSTEP.NSCAN.NINDX.NAVE.VOLTAGEL

    VOLTAGEU, VOLTAGE MAX, SHAPEANS, LOOPANS, LOOPTHRU H, LOOPTHRU S,
    ZIGANS, SCHEME, TSCHEME, UZEROO, FILENAME, 115, SCANMODE, SLANT1, SLANT2,

  1 SLANT3, SLANT4)
       integer*4 SCANSTEP, INDXSTEP
       real SCANDIST, INDXDIST, PU, PL, SLANT, rslant1, RSLANT2, SLANT1, SLANT2
       REAL
                SLANT3, SLANT4, RSLANT3, RSLANT4
       INTEGER*2 LOOPTHRU_H,LOOPTHRU S,ISLANTI,ISLANT2
       integer*2 NSCAN,NINDX, IDIST1,1DIST2,16,115
       integer*2 FREQ,NAVE,ISLANT3,ISLANT4
       character FILENAME*34, FILEEXT*23, CHEADER*32
       CHARACTER LOOPANS*1,SCHEME*1
       CHARACTER SHAPEANS*1,ZIGANS*1
       CHARACTER TSCHEME*1,SCANMODE*1
       DATA 16/1/
       115=1
10010 format( A )
10012 format( A2 )
10020 format(1)
10030 format(F)
C Initialization and entry of parameters
С
c
c
       TYPE *,''
       TYPE *,' *****> DONSCAN.FOR......AUTO SCAN'
TYPE *,' '
       OPEN (UNIT=10,FILE='NOTHICK_ALLSHAPE1.DAT',STATUS-'OLD',
  1
       FORM='FORMATTED')
       READ (10,93764) SCANMODE
       READ (10,93765) XSCANSTEP !(X IND)
       IF (SCANMODE.EQ.'P')XSCANSTEP=2000.
       READ (10,93765) YINDXSTEP !(Y IND)
       IF (SCANMODE.EQ.'P')YINDXSTEP=2000.
       SCANSTEP=JNINT(XSCANSTEP)
       INDXSTEP=JNINT(YINDXSTEP)
       READ (10,93765) SCANDIST !(X DIST)
       IF (SCANMODE.EQ.'P')SCANDIST=2000.
       READ (10,93765) INDXDIST !(Y DIST)
       IF (SCANMODE.EQ.'P')INDXDIST=2000.
       IF (SCANMODE.EQ.'L')THEN
       YINDXSTEP=20000.
       INDXSTEP=JNINT(YINDXSTEP)
       INDXDIST=20000.
       ENDIF
       READ (10,93764) ZIGANS
```

READ (10,93765) PL

000000000000000000000000000000000000000	THAT THE EC EXPERIMENT INCORPORATI SUBTRACTIVI MULTIPLYINC IN THE X-DIRI BEING PERFO VALUE TO EA BEFORE THE SC AN ECHO, SAY B1 AND B2 FC FACTOR WILL	
С	READ (10,93765) SLANTI SLANTI=SLANTI/10.**9. RSLANTI=SLANTI*10.**13. ISLANTI=IINT(RSLANTI)	CONVERT SLANT TO INTEGER FOR STORAGE IN .DATI2 FILE
с	READ (10,93765) SLANT2 SLANT2=SLANT2/10.**9. RSLANT2=SLANT2*10.**13. ISLANT2=IINT(RSLANT2)	ICONVERT SLANT TO INTEGER FOR STORAGE IN .DATI2 FILE
С	READ (10,93765) SLANT3 SLANT3=SLANT3/10.**9. RSLANT3=SLANT3*10.**13. ISLANT3=1INT(RSLANT3)	CONVERT SLANT TO INTEGER FOR STORAGE IN .DATI2 FILE
с	READ (10,93765) SLANT4 SLANT4=SLANT4/10.**9. RSLANT4=SLANT4*10.**13. ISLANT4=IINT(RSLANT4)	CONVERT SLANT TO INTEGER FOR STORAGE IN .DATI2 FILE
	READ (10,93765) FREQUENCY READ (10,93764) FILEEXT	
126	K=0 K=K+1	

63

.

## IF( FILEEXT(K:K).NE.'')GOTO 126 ! FILEEXT(K+1:K+4)='.DAT'

! UNIT 6 = raw data

READ (10,93764) CHEADER 93764 FORMAT (A) FORMAT (F) 93765 93766 FORMAT (I) С VOLTAGEL-PL/20. С VOLTAGEU=PU/20. С VOLTAGE MAX=PM/20. TYPE \*, 'RUN TEMPDIRSCAN\_COM - DIRSCAN SMALLTRANS\_DATA.DAT' С TYPE \*, KON TEMPDIRSCAN\_COM - DIRSCAN SMALLTRANS\_DATA.DAT TYPE \*, 'DATA FOR ULTRASONIC SCAN (ALL FLOATING PT. EXCEPT INDEXES)' TYPE \*,'SCAN DIMENSIONS/INDEXING DATA (MICRONS)' TYPE \*,'X INDEX - INTEGER EXPRESSION' TYPE \*,SCANSTEP TYPE \*, 'N DIREX - INTEGER EXPRESSION' TYPE \*,'Y INDEX - INTEGER EXPRESSION' TYPE \*, INDXSTEP TYPE \*,' X SCAN DISTANCE (MICRONS) - FLOATING POINT' TYPE\*,SCANDIST TYPE \*, 'X SCAN DISTANCE (MICRONS) - FLOATING POINT' TYPE \*, INDXDIST TYPE \*, 'LOWER & UPPER PRESSURES FOR CONTACT SCAN' С С TYPE \*,PL,PU TYPE \*, 'THICKNESS (MM)' С TYPE \*, SLANT1 (X-LEVELNESS TIME CORRECTION FACTOR for b1,b2) (nsec / um )' TYPE \*, SLANT1 (X-LEVELNESS TIME CORRECTION FACTOR for reflector echoes) (nsec / um )' TYPE \*, SLANT2 (X-LEVELNESS TIME CORRECTION FACTOR for reflector echoes) (nsec / um )' с TYPE \*,SLANT2 TYPE \*,'SLANT3 (Y-LEVELNESS TIME CORRECTION FACTOR for b1,b2) (nsec / um )' TYPE \*,SLANT3 TYPE \*, SLANT4 (Y-LEVELNESS TIME CORRECTION FACTOR for reflector echoes) (nsec / um )' TYPE \*, SLANT4 TYPE \*, TRANSDUCER CENTER FREQUENCY (FLOATING POINT)' TYPE \*, FREQUENCY TYPE \*, FILENAME FOR RAW DATA ' TYPE \*, FILEEXT TYPE \*, 'CHEADER INFO (UP TP 32 CHARACTERS)' TYPE \*, CHEADER TYPE \*. NSCAN = (SCANDIST/SCANSTEP) + 1 1000 NINDX = (INDXDIST/INDXSTEP) - I SCANDIST = SCANSTEP\*(NSCAN-1) ! SCANDIST = negative INDXDIST = INDXSTEP\*(NINDX-1) IF (SCANMODE.EQ.'S')THEN WRITE( 5,11100 )SCANDIST, NSCAN, SCANSTEP, INDXDIST, NINDX, INDXSTEP + ELSEIF (SCANMODE.EQ.'L')THEN WRITE( 5,11200 )SCANDIST, NSCAN, SCANSTEP ELSEIF (SCANMODE.EQ.'P')THEN WRITE( 5,11300 ) ENDIF 11100 format( /' ', + // X scan to ',F7.0,', ',I3,' steps of ',I5, + // Y index to ',F7.0,', ',I3,' steps of ',I5)

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11200 format( /' ',

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FORMAT(A32)

FORMAT(A2)

FORMAT(A4)

FORMAT(A2)

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- // Line scan to ',F7.0,', ',I3,' steps of ',I5) 11300 format (/'', //" Point Measure repeated 2 times') SCHEME='B'

WRITE( 5,11690 )

\*\*\*\*\*\*

THICK= IINT(THICKN\*1000.) FREQ=FREQUENCY NAVE=64

FILENAME = '[ROTH.DATA]'//FILEEXT

11690 format( /'SNUMBER OF AVERAGES SET AT 64' )

DIRECT ACCESS STORAGE

OPEN( unit=6, file=FILENAME//'CH', status='NEW',

OPEN( unit=15, file=FILENAME//'12', status='NEW', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2,

OPEN( unit=16, file=FILENAME//'R4', status='NEW'

OPEN( unit=17, file=FILENAME//'WAV', status='NEW', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2.

OPEN( unit=26, file=FILENAME//'RR4', status='NEW',

OPEN( unit=27, file=FILENAME//'RWAV', status='NEW', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2,

OPEN( unit=37, file=FILENAME//'SWAV', status-'NEW',

OPEN( unit=36, file=FILENAME//'SR4', status='NEW', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4,

ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=32,

ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4,

ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4,

form='FORMATTED', ORGANIZATION='SEQUENTIAL')

form='FORMATTED', ORGANIZATION='SEQUENTIAL' )

form='FORMATTED', ORGANIZATION='SEQUENTIAL' )

form='FORMATTED', ORGANIZATION='SEQUENTIAL' )

form='FORMATTED', ORGANIZATION='SEQUENTIAL')

form-'FORMATTED', ORGANIZATION='SEQUENTIAL' )

form-'FORMATTED', ORGANIZATION='SEQUENTIAL' )

ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2, form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) OPEN( unit=46, file=FILENAME//'TR4', status='NEW' ACCESS='DIRECT', RECORDT'YPE='FIXED', RECL=4, form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) OPEN( unit=47, file=FILENAME//'TWAV', status='NEW', ACCESS='DIRECT', RECORDTYPE-'FIXED', RECL-2, form='FORMATTED', ORGANIZATION='SEQUENTIAL') Write header : X, Y dist, X, Y scan points, dummies

WRITE(6,REC=16,FMT=51)CHEADER 16=16+1 WRITE(6,REC=I6,FMT=51)SHAPEANS

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C C C

16=16+1 WRITE(6,REC=I6,FMT=51)ZIGANS I6=I6+1 IDIST1 = - IIFIX(SCANDIST/1000.) IDIST2 = IIFIX(INDXDIST/1000.) IF (IDIST2.LT.1)IDIST2=1 !TRICK TO ALLOW DISPLAY OF IMAGE ON PSIDD WRITE(15,REC=115,FMT=52)IDIST1 115=115+1 WRITE(15,REC=115,FMT=52)IDIST2 115=115+1 WRITE(15,REC=115,FMT=52)NSCAN 115=[15+1 IF (SCANMODE.EQ.'L'.OR.SCANMODE.EQ.'P')NINDX=1 !MOD FOR LINE/POINT SCAN WRITE(15,REC=I15,FMT=52)NINDX I15=I15+1 WRITE(15,REC=115,FMT=52)THICK WRITE(15,REC=115,FMT=52)ISLANT1 115=115+1 WRITE(15,REC=115,FMT=52)ISLANT2 115=115+1 WRITE(15,REC-II5,FMT=52)ISLANT3 115=115+1 WRITE(15,REC-I15,FMT=52)ISLANT4 115=115+1 WRITE(15,REC=115,FMT=52)DENS 115=115+1 WRITE(15,REC=I15,FMT=52)FREQ 115 = 115 + 1WRITE(15,REC=115,FMT=52)NAVE I15=I15+I RETURN end SUBROUTINE XPARAM( SCANSTEP, INDXSTEP, NSCAN, NINDX ) integer\*4 SCANSTEP, INDXSTEP integer\*2 NSCAN,NINDX SCANSTEP = 50 INDXSTEP = 50 NSCAN = 50 NINDX = 50 THICK = 1OPEN( unit=6, file='XXX.DAT', status='OLD', form='UNFORMATTED' ) + SCANSTEP = 50 RETURN end SUBROUTINE MOVKLING (AXIS, DIST) MOVE KLINGER A SPECIFIED DISTANCE IN SPECIFIED DIRECTION byte IXYZ character\*1 XYZ equivalence( XYZ, IXYZ ) common WRK0,BUFFER

27

CALL STRTGPIB CALL INITINSTR(2) CALL INITINSTR(3) CALL INITINSTR(4) 10010 format(A) 10020 format(] 10100 format(]SDistance ?') 100 WRITE(5,10000) 10000 format(/SX, Y, or Z ?') READ(5,10010)XYZ IF(1XYZ.GT.90. OR.IXYZ.LT.88)GOTO 900 IPORN=1 WRITE(5,10100) READ(5,10020)IREQ IF(IREQ.LT.0)THEN IPORN=-1 IREQ=ABS(IREQ) ENDIF CALL SETXYZ(IREQ,IREQ,IREQ) IAXIS = IXYZ - 87 CALL MOVXYZ(IAXIS,IPORN) GOTO 100 900 STOP RETURN end

INCLUDE '[ROTH.MENU]BASE0\_2SEC\_M.FOR'

5,629,865

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C nothick\_crunch.for --- 4 SCAN METHOD

C Crunch program for Nothickness velocity scan

C Don Roth 20-scp-1994

integer\*2 SCANDIST,INDXDIST,NSCAN,NINDX,JI,II,SCANKNT integer\*2 DENS,TRFREQ,AVES,NPOINT,I6,I15,I16,I18,I26 integer\*2 ARRAYSIZE,KCOUNT,SELFREQ,ENDFREQ,I85,I36,I46 INTEGER\*2 islant1,islant2,ISLANT3,ISLANT4,ACTPOINT,JXXX integer\*2 rawwaveb1(512),rawwaveb2(512),rawwavers(512),rawwaverns(512) INTEGER\*4 II7,I7,REC,I27,I7SUB,I37,I47,I27SUB,I37SUB,I47SUB,I17SUB real\*4 L\_VEL,U\_VEL,AV\_VEL real\*4 ASPECB1(1024), ASPECB2(1024) real\*4 B1ASPEC(256), B2ASPEC(256) real\*4 ASPECRS(1024), ASPECRNS(1024)

real\*4 RSASPEC(256), RNSASPEC(256) REAL\*4 B1PHASE(256), PHASEB1(1024) REAL\*4 B2PHASE(256), PHASEB2(1024) REAL\*4 RSPHASE(256), PHASERS(1024) REAL\*4 RSPHASE(256), PHASERNS(1024) REAL\*4 B1(512), BB2(512), RRS(512), RRNS(512) REAL\*4 VEL(5000), TRDIAM, BUFLENGTH character FILENAME\*32, FILEEXT\*26, CHEADER\*32, NOISANS\*1 character FS1EXT\*16, CALNAME\*32, FLAG\*1

CHARACTER DIFFANS\*1,PHASE\*1,PHASE1\*1 CHARACTER SELFREQANS\*1 CHARACTER SHAPEANS\*1,ZIGANS\*1,DIR\*5 CHARACTER CRUNCH\_CODE\*2,CFILTER\*1 character actual\_selfreqans\*1

byte FILEFS1IN equivalence ( B1ASPEC,ASPECB1 ) equivalence ( B2ASPEC,ASPECB2 ) equivalence ( RSASPEC,ASPECRS ) equivalence ( RNSASPEC,ASPECRNS ) EQUIVALENCE (B1PHASE,PHASEB1) EQUIVALENCE (B2PHASE,PHASEB2) EQUIVALENCE (RSPHASE,PHASERS) EQUIVALENCE (RNSPHASE,PHASERS) EQUIVALENCE (RNSPHASE,PHASERS) equivalence ( FS1EXT, FILEFS1IN )

DATA 16/1/115/1/116/1/17/1/17/1/18/1/ DATA 126/1/127/1/185/1/136/1/137/1/146/1/147/1/

NIPI=0

10010 format(A) 10014 format('',A ) 10020 format(I) 10030 format(F) C 74

\*ASPEC 256

\*ASPEC 256

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OPEN (UNIT=14, FILE='NOTHICK SELFREQ1.DAT', STATUS='OLD',FORM='FORMATTED') 1 READ (14,98652) FILEEXT READ (14,98652) DRIVE READ (14,98652) PHASE READ (14,98652) PHASE1 READ (14,98652) DIFFANS READ (14,10030) BUFLENGTH READ (14,10030) BUFVEL READ (14,10030) TRDIAM CLOSE (14) 98652 FORMAT (A) C \*\*\*\*\*\*\*\*\* OPEN FILTER FILE FOR UPPER & LOWER LIMITS \*\*\*\*\*\*\*\*\*\* C OPEN (UNIT=24, FILE="NOTHICK\_LIMITS1.DAT", STATUS='OLD',FORM='FORMATTED') 1 READ (24,98652) CFILTER READ (24,10030) L\_VEL READ (24,10030) U\_VEL L\_VEL=L\_VEL U\_VEL=U\_VEL  $AV_VEL=(L_VEL+U_VEL)/2.$ K=0 K = K + 1126 IF( FILEEXT(K:K).NE.'')GOTO 126 ! ! UNIT 6 = raw data FILEEXT(K+1:K+4)='.DAT' IF (DRIVE.EQ.'A')DIR='DUC2:' IF (DRIVE.EQ.'C')DIR='DUC0:' FILENAME = '[ROTH.DATA]'//FILEEXT C\* \*\*\*\*\* C C DIRECT ACCESS STORAGE OPEN( unit=76, file=DIR//FILENAME//'GB', status='NEW', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4. + form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) ÷ OPEN( unit=66, file=FILENAME//'CH', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=32, + ÷ form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) OPEN( unit=15, file=FILENAME//12', status='OLD', ACCESS='DIRECT, RECORDTYPE='FIXED', RECL=2, -+ form='FORMATTED', ORGANIZATION='SEQUENTIAL') + OPEN( unit=16, file=FILENAME//'R4', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4, + form='FORMAT'TED', ORGANIZATION='SEQUENTIAL' ) + OPEN( unit=17, file=FILENAME//WAV', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2, +

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+	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
Ŧ	OPEN( unit=26, file=FILENAME//RR4', status='OLD',
÷	ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4.
+	form='FORMATTED',ORGANIZATION='SEQUENTIAL')
	OPEN( unit=27, file=F1LENAME//RWAV', status='OLD',
+	ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2.
+	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
•	OPEN( unit=36, file=FILENAME//SR4', status='OLD',
+	ACCESS='DIRECT, RECORDTYPE='FIXED', RECL=4,
4	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
•	OPEN( unit=37, file=FILENAME//SWAV, status='OLD',
+	ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2,
+	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
	OPEN( unit=46, file=FILENAME//'TR4', status='OLD',
+	ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4,
+	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
	OPEN( unit=47, file=FILENAME//'TWAV', status='OLD',
+	ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2,
4	form='FORMATTED', ORGANIZATION='SEQUENTIAL')
С	
51	FORMAT(A32)
52	FORMAT(A2)
53	FORMAT(A4)
153	FORMAT(1X,14,1X,14,1X,14,1X,E12.5,1X,E12.5,1X,E12.5,1X,E12.5,1X,E12.5,1X,
+	E12.5,1X,E12.5)
54	FORMAT(A2)
	K≈0
120	K=K+1
	IF( FILEEXT(K:K).NE.'')GOTO 120 1
	FILEEXT(K+1:K+3)='SPC' ! UNIT 6 = raw data
	FILENAME = "[ROTH.DATA]"//FILEEXT !
С	
	**************************************
С	
	OPEN( unit=7, file=DIR//FILENAME, status='NEW', ACCESS='DIRECT',
+	RECORDTYPE='FIXED', RECL=4, FORM='FORMA'TTED',
+	ORGANIZATION='SEQUENTIAL')
	WRITE( 6,10200 )FILENAME ! UNIT 8 = calibration
10200	format('Filename of analyzed data is 'A)
10200	FILEEXT(K+1:K+3)='CAL'
	CALNAME = '[ROTH.DATA]'/FILEEXT
	OPEN( unit=8, file=CALNAME, status='NEW', ACCESS='DIRECT',
+	RECORDTYPE='FIXED', RECL=4, FORM='FORMATTED',
+	ORGANIZATION='SEQUENTIAL')
•	OKOMNIZATION-BEQUENTIAC /
89651	DO 76065 IOPI=1,1024
07051	PHASEB1(IOPI)=0.
	PHASEB2(IOPI)=0.
	PHASERS(IOPI)=0.
	PHASERNS(10P1)=0.
	ASPECBI(IOPI)=0.
	ASPECB2(IOPI)=0.
	ASPECRS(1OPI)=0,
76065	ASPECRNS(IOPI)=0.

## KCOUNT=1

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C #### Read preliminary scan info #### С

79193 READ(66,REC=16,FMT=51)CHEADER I6=I6+1 READ(66,REC=16,FMT=51)SHAPEANS l6≕l6+1 READ(66,REC=16,FMT=51)ZIGANS

I6≂I6+1 IF (SHAPEANS.NE.'Y')GOTO 89714 OPEN(UNIT=12,FILE='[ROTH.DATA]'//FILEEXT(1:K)//DATHS', STATUS='OLD', FORM='UNFORMATTED') !INFO ON WHETHER WE ARE ON HOLDER/SAMPLE

89714 READ(15,REC=115,FMT=52)SCANDIST 115=115+1 READ(15,REC=I15,FMT=52)INDXDIST 115=I15+1 READ(15,REC=115,FMT=52)NSCAN [15=[15+] READ(15,REC=115,FMT=52)NINDX 115=115+1 READ(15,REC=115,FMT=52)islant1 115=115+1 READ(15,REC=I15,FMT=52)islant2 115=115+1 READ(15,REC=I15,FMT=52)islant3 115=115+1 READ(15,REC=115,FMT=52)islant4 115=115+1 READ(15,REC=1)5,FMT=52)DENS 115=115+1 READ(15,REC=115,FMT=52)TRFREQ 115=115+1 READ(15,REC=115,FMT=52)AVES 115=115+1 READ(15,REC=115,FMT=52)JXXX [15=]15+1 ARRAYSIZE=(NSCAN)\*(JXXX) !IF SCAN FINISHED PROPERLY,JXXX-NINDX

READ(16,REC=116,FMT=53)TIMESET I16=I16+1

ENDFREO=TRFREQ\*2.5 CALL POINT\_FROM\_FREQ(ENDFREQ,TIMESET,ACTPOINT)

DELTAF = 1./(TIMESET\*20.)NPOINT=NSCAN\*JXXX IIF SCAN FINISHED PROPERLY, JXXX=NINDX NWAVES = 3\*NPOINT

С !!! Loop thru scan data

ITEM\_COUNT=0

SCANKNT=NIP

ITEM\_COUNT=ITEM\_COUNT+1 IF (SHAPEANS.EQ.'N'.AND.NIP.GE.2)ITEM\_COUNT=2 TYPE \*,' ' TYPE \*,'ITEM\_COUNT= ',ITEM\_COUNT TYPE \*,' CRUNCH\_CODE= ',CRUNCH\_CODE TYPE \* CCVACCUM=0. 67519 CONTINUE NIPJ=((NIP-1)/NSCAN)+1 IY LOCATION NIPI=NIPI+1 IX LOCATION IF (NIPI.EQ.(NSCAN+1))NIPI=1 !RESET X LOCATION C \*\*\*\*\* MODIFICATION FOR ZIGZAG SCAN \* IF (ZIGANS.EQ.'Y')THEN IF (NIPJ.EQ.2.OR.NIPJ.EQ.4.OR.NIPJ.EQ.6.OR.NIPJ.EQ.8.OR.NIPJ.EQ.10 1. OR.NIPJ.EQ.12.OR.NIPJ.EQ.14.OR.NIPJ.EQ.16.OR.NIPJ.EQ.18.OR.NIPJ. 1 EQ.20.OR.NIPJ.EQ.22.OR.NIPJ.EQ.24.OR.NIPJ.EQ.26.OR.NIPJ.EQ.28.OR. 1 NIPJ.EQ.30.OR.NIPJ.EQ.32.OR.NIPJ.EQ.34.OR.NIPJ.EQ.36.OR.NIPJ.EQ.38. 1 OR.NIPJ.EQ.40.OR.NIPJ.EQ.42.OR.NIPJ.EQ.44.OR.NIPJ.EQ.46.OR.NIPJ.EQ. 1 48.OR.NIPJ.EQ.50.OR.NIPJ.EQ.52.OR.NIPJ.EQ.54.OR.NIPJ.EQ.56.OR. 1 NIPJ.EQ.58.OR.NIPJ.EQ.60.OR.NIPJ.EQ.62.OR.NIPJ.EQ.64.OR.NIPJ.EQ.66 1 .OR.NIPJ.EQ.68.OR.NIPJ.EQ.70.OR.NIPJ.EQ.72.OR.NIPJ.EQ.74.OR.NIPJ. 1 EQ.76.OR.NIPJ.EQ.78.OR.NIPJ.EQ.80.OR.NIPJ.EQ.82.OR.NIPJ.EQ.84.OR 1.NIPJ.EQ.86.OR.NIPJ.EQ.88.OR.NIPJ.EQ.90.OR.NIPJ.EQ.92.OR.NIPJ. 1 EQ.94.OR.NIPJ.EQ.96.OR.NIPJ.EQ.98.OR.NIPJ.EQ.100)THEN NIPG=NSCAN-NIPI+1 !FOR ZIGZAG SCAN, REVERSE BACK FOR DISPLAY ELSE NIPG=NIPI ENDIF elseif(zigans.eq.'N')then !george wood addition nipg=nipi !George Wood addition ENDIF TYPE \*,' ' TYPE \*.' ' IF (SHAPEANS.EO.'N')GOTO 89715 READ(12)JJ,II,FLAG,SCANKNT IREAD WHETHER 'H' OR 'S' TYPE \*,'X=',NIPG,' Y=',NIPJ,' FLAG= ',FLAG IF (FLAG.EQ.'S')THEN

99651 DO 1890 NIP=1,NPOINT !!NPOINT IS TOTAL OF ALL POINTS

89715 READ(16,REC=116,FMT=53)DELAYB1 116=116+1 READ(16,REC=116,FMT=53)VOLTSETB1 116=116+1 READ(26,REC=126,FMT=53)DELAYB2 126=126+1 READ(26,REC=126,FMT=53)VOLTSETB2 126=126+1

READ(36,REC=136,FMT=53)DELAYRS 136=136+1 READ(36,REC=I36.FMT=53)VOLTSETRS 136=136÷1 READ(46,REC=I46,FMT=53)DELAYRNS 146=146+1 READ(46,REC=I46,FMT=53)VOLTSETRNS 146=146+1 DO 54322 IJI=1,512 54322 READ(17,REC=((I17-1)\*512)+IJI,FMT=54)RAWWAVEB1(IJI) 117=[17+1 DO 54323 IJI=1,512 54323 READ(27,REC=((127-1)\*512)+IJI,FMT=54)RAWWAVEB2(IJI) 127=127+1 DO 54324 IJI=1,512 READ(37,REC=((I37-1)\*512)+IJI,FMT=54)RAWWAVERS(IJI) 54324 137=137+1 DO 54325 JJI=1,512 54325 READ(47,REC=((147-1)\*512)+1JI,FMT=54)RAWWAVERNS(IJI) 147=147+1 ELSEIF (FLAG.EQ.'H')THEN GOTO 1890 ENDIF II≈II+1 A = 0. DO 1400 I=1,512 RAWWAVEB1(I)=RAWWAVEB1(I)/AVES 1400 A=A + RAWWAVEB1(1) ZERO = A/512. DO 1560 I=1,512 1560 BB1(I) = ( REAL(RAWWAVEB1(I)) - ZERO )\*( VOLTSETB1 )\*10./512. II=II+1 A = 0.DO 1401 I=1,512 RAWWAVEB2(I)=RAWWAVEB2(I)/AVES 1401 A=A + RAWWAVEB2(I) ZERO ≈ A/512. DO 1570 1=1,512 1570 BB2(I) = ( REAL(RAWWAVEB2(I)) - ZERO )\*( VOLTSETB2 )\*10./512. [**]**≂]]+1 A ≃ 0. DO 1402 I=1,512 RAWWAVERS(I)=RAWWAVERS(I)/AVES 1402 A=A + RAWWAVERS(I) ZERO = A/512.DO 1580 1=1,512 RRS(I) = ( REAL(RAWWAVERS(I)) - ZERO )\*( VOLTSETRS )\*10./512. 1580

11=11+1

. ....

1590	RRNS(I) = ( REAL(RAWWAVERNS(1)) - ZERO )*( VOLTSETRNS )*10./512.	
	IF (PHASE.EQ.'N')THEN CALL CORR(BB1,BB2,TWOTAU_DELAY) !for time delay in sample ELSEIF (PHASE.EQ.'Y')THEN !PHASE INVERSION FOR BETWEEN B1 & B2 CALL MCORR(BB1,BB2,TWOTAU_DELAY) !for time delay in sample ENDIF	
С	IF (PHASE1.EQ.'N')THEN CALL CORR(RRS,RRNS,DELTAT_DELAY) !for delay between reflector peaks (sample vs. no sample) ELSEIF (PHASE1.EQ.'Y')THEN !PHASE INVERSION FOR BETWEEN RN & RNS CALL MCORR(RRS,RRNS,DELTAT_DELAY) !for delay between reflector peaks ENDIF	
	CALL OBTAIN_MAGNITUDE_SPECTRA(BB1,ASPECB1) CALL OBTAIN_MAGNITUDE_SPECTRA(BB2,ASPECB2) CALL OBTAIN_MAGNITUDE_SPECTRA(RRS,ASPECRS) CALL OBTAIN_MAGNITUDE_SPECTRA(RRNS,ASPECRNS)	
	ADELAYS = DELAYB2 - DELAYB1 ADELAYR = DELAYRNS - DELAYRS	
С	TWOTAU=ADELAYS+(TIMESET/51.2)*TWOTAU_DELAY !for time delay in sample DELTAT=ADELAYR+(TIMESET/51.2)*DELTAT_DELAY !for delay between reflector peaKS (sample vs. no sample)	
	CALL NOTHICK_VEL_CALC(DELTAT,TWOTAU,VEL_NOTHICK) type *,'vel_nothick=',vel_nothick	
1	CALL FILTER(VEL_NOTHICK,VELPREV,CFILTER,SHAPEANS,L_VEL,U_VEL, AV_VEL,NIPG,NIPJ,SCANKNT,I18) EL(SCANKNT)=VEL_NOTHICK	
۷Ľ		
	VELPREV=VEL_NOTHICK	
POINT	CALL STORE_SPECTRA(ASPECB1,ACTPOINT,I7,I7SUB) ISTORE SPECTRAS AT EACH S	CAN
	CALL STORE_SPECTRA(ASPECB2,ACTPOINT,I7,I7SUB) CALL STORE_SPECTRA(ASPECRS,ACTPOINT,I7,I7SUB) CALL STORE_SPECTRA(ASPECRNS,ACTPOINT,I7,I7SUB)	

A = 0. DO 1403 I=1,512 RAWWAVERNS(I)=RAWWAVERNS(I)/ $\Lambda$ VES 1403 A=A + RAWWAVERNS(I) ZERO = A/512. DO 1590 I=1,512 LCO

85

с

С

CONTINUE

1890

С

.SPC FILE

END

CALL STORE VEL(I7SUB, 185, SCANKNT, ACTPOINT, VEL) ISTORE VELOCITIES AT END OF

88

SUBROUTINE POINT\_FROM\_FREQ(FREQ,TIMEPERDIV,ACTPOINT)

DETERMINE SPECTRA POINT FROM FROM SPECIFIC FREQUENCY IN SPECTRA

SEE SUBROUTINE CENTERFREQ FOR SIMILAR PROCESSING EXPLANATION

**INTEGER\*4 DUMMYFREQ** 

36

WRITE(7,REC=17SUB,FMT-53)VEL(1JI) 94326 I7SUB=17SUB+1 53 FORMAT(A4)

RETURN END

CCCCC

VAVE=VACCUM/NPOINT WRITE(8,REC=185,FMT=53)VUP 185=185+1 WRITE(8,REC=I85,FMT=53)VLO

185=185+1 WRITE(8,REC=185,FMT=53)VAVE

VMAX=AMAX1(VUP,VEL(IJI)) VUP=VMAX VMIN=AMIN1(VLO,VEL(IJI)) VLO=VMIN

VACCUM=VACCUM+VEL(IJI)

VACCUM=0.

INTEGER\*2 NPOINT, 185, ACTPOINT

REAL\*4 VEL(5000)

**INTEGER\*4 I7SUB** 

VUP=0.0 VLO=10.\*\*8.

I7SUB=I7SUB+1 DO 94326 IJI=1,NPOINT

SUBROUTINE STORE\_VEL(17SUB,185,NPOINT,ACTPOINT,VEL)

!! STORE VELOCITIES AND FIND MAX.MIN & STORE IN CAL FILE

IF (SHAPEANS.EQ.'N')SCANKNT=NPOINT

INTEGER\*2 FREQ, ACTPOINT

DUMMYFREQ=FREQ\*1E+06 DELFREQ=(1./(2.\*(10.\*TIMEPERDIV))) TEMPPOINT=DUMMYFREQ/DELFREQ ACTPOINT-JNINT(TEMPPOINT)

90

SUBROUTINE OBTAIN\_MAGNITUDE\_SPECTRA(TWAVE,DUMMY\_ASPEC) COMPLEX C1(1024),CSPEC(1024) INTEGER\*4 ISTAT DUMMY\_ASPEC(1024), PHASE(1024), TWAVE(512) real\*4 DO 500 I=1,512 C1(I)=CMPLX(TWAVE(I)) CALL LSPSFFT COMPLEX(CI, CSPEC, 1024,0.ISTAT) CALL LSP\$PHASE\_ANGLE( CSPEC, PHASE, DUMMY\_ASPEC, 1024 ) RETURN END SUBROUTINE STORE\_SPECTRA(DUMMY\_ASPEC,ACTPOINT,I7,I7SUB) INTEGER\*2 ACTPOINT INTEGER\*4 REC, 17, 17SUB DUMMY\_ASPEC(1024) REAL\*4 DO 94326 IJI=1,ACTPOINT I7SUB=((17-1)\*ACTPOINT)+IJI WRITE(7,REC-I7SUB,FMT=53)DUMMY\_ASPEC(IJI) 17=17+1 FORMAT(A4) RETURN END SUBROUTINE FILTER(VEL\_NOTHICK, VELPREV, CFILTER, SHAPEANS, L\_VEL, U\_VEL, 1 AV\_VEL,NIPG,NIPJ,SCANKNT,I18)

- 53
- 94326

CHARACTER CFILTER\*1, CRUNCH\_CODE\*2, SHAPEANS\*1

IF (CFILTER.EQ.'Y'.AND.(VEL nothick.LT.L VEL.OR.VEL nothick.GT.U VEL))THEN

37

C \*\*\*\*\*\*\*\* TEST FOR VELOCITY OUTSIDE FILTER LIMITS \*\*\*\*\* C

INTEGER\*2 NIPG,NIPJ,I18,SCANKNT REAL\*4 L VEL,U VEL,AV VEL

IF (SCANKNT.EQ.1)VELPREV=AV\_VEL

VEL NOTHICK=VELPREV CRUNCH CODE='BC'

500 1580

TIMEPERDIV.DELFREO, TEMPPOINT

RETURN END

REAL\*4

С

С č

ICRUNCH\_CODE\_COUNT=1 TYPE \*, BAD POINT AT ', NIPG, NIPJ ENDIF

IF (ICRUNCH\_CODE\_COUNT.EQ.0)CRUNCH\_CODE='G' WRITE(76.REC=I18,FMT=53)CRUNCH\_CODE I18=I18+1 WRITE(76.REC=I18,FMT=53)NIPG I18=I18+1 WRITE(76,REC=I18,FMT=53)NIPI I18=I18+1

53 FORMAT(A4)

RETURN END

SUBROUTINE NOTHICK\_VEL\_CALC(DELTAT, TWOTAU, VEL\_NOTHICK)

VELWATER=0.149 !CM/USEC

VEL\_NOTHICK=VELWATER\*((DELTAT/TWOTAU)+1) RETURN END

SUBROUTINE CORR(B1,B2,CXX) C CORRELATE TWO WAVEFORMS COMPLEX\*8 NC11(512),NC12(512),NC13(512) COMPLEX\*8 NC14(512),NC15(512),NC22(512) REAL\*4 NC16(512),B1(512),B2(512),CXX INTEGER\*4 STATUS

> DO 333 I=1,512 NC11(I)=CMPLX(B1(I)) NC22(I)=CMPLX(B2(I)) CONTINUE

CALL LSP\$FFT\_COMPLEX(NC11,NC12,512,0,STATUS) CALL LSP\$FFT\_COMPLEX(NC22,NC13,512,0,STATUS)

DO 777 IO=1,512 NC14(IO)=NC12(IO)\*CONJG(NC13(IO)) 777 CONTINUE CALL LSP\$FFT\_COMPLEX(NC14,NC15,512,0,STATUS) IF (.NOT. STATUS) CALL LIB\$SIGNAL(%VAL(STATUS))

> AMAX=0.0 CXX=0.0

333

DO 765 I=1,256 NC16(I+256)=REAL(NC15(I)) NC16(I)=REAL(NC15(I+256)) 765 CONTINUE

CORRRELATE TWO WAVEFORMS !!! modified by using absolute value of minimum of correlation function to take into account phase inversion of B2 w/ respect to B1 such as what happens w/ PMCs COMPLEX\*8 NC11(512),NC12(512),NC13(512) COMPLEX\*8 NC14(512), NC15(512), NC22(512) REAL\*4 NC16(512),B1(512),B2(512),CXX INTEGER\*4 STATUS DO 333 I=1,512 NC11(I)=CMPLX(BI(I)) NC22(I)=CMPLX(B2(I)) CONTINUE CALL LSP\$FFT COMPLEX(NC11,NC12,512,0,STATUS) CALL LSP\$FFT\_COMPLEX(NC22,NC13,512,0,STATUS) DO 777 IO=1,512 NC14(IO)=NC12(IO)\*CONJG(NC13(IO)) CONTINUE CALL LSP\$FFT\_COMPLEX(NC14,NC15,512,0,STATUS) IF (.NOT. STATUS) CALL LIB\$SIGNAL(%VAL(STATUS)) AMAX=0.0 AMIN=1.0E+6

IF(NC16(1).GT.AMAX)THEN AMAX=NC16(1) CXX=T ENDIF CONTINUE CXX=CXX-257. RETURN END SUBROUTINE MCORR(B1,B2,CXX) CORRRELATE TWO WAVEFORMS of minim

93

DO 881 1=1,512

881

00000

333

777

765

С

С

CXX=0.0 DXX=0.0

DO 765 I=1,256

CONTINUE DO 881 I=1,512

AMAX=NC16(I) CXX=1 ENDIF

NC16(I+256)=REAL(NC15(I)) NC16(I)=REAL(NC15(I+256))

IF(NC16(1).GT.AMAX)THEN

CORRRELATE TWO WAVEFORMS !!! modified by using absolute value

of minimum of correlation function

39

5,629,865

с с с to take into account phase inversion of B2 w/ respect to B1 such as what happens w/ PMCs

## IF(NC16(I).LT.AMIN)THEN AMIN≈NC16(I) DXX=I ENDIF

881 CONTINUE

CXX=DXX

CXX=CXX-257. RETURN END 5,629,865

97

 $\mathbf{CC}$ PROGRAM: NOTHICK\_IMAGEMAKER.FOR С С Read Data file written by CRUNCH and place data into c c "Grinnell-ready" files С Header: X3, Y3 Dimension of scan (SCAN DIRECTION, INDEX DIRECTION) С N1, N2 Number of points (SCAN, INDEX) С INTEGER\*2 ACTPOINT BFILEEXT(23) BYTE CHARACTER FILENAME\*44, FILEEXT\*23, DRIVE\*1 CHARACTER CALNAME\*44,SELFREQANS\*1,SHAPEANS\*1,DISKT\*5 CHARACTER HEAD\*23,DIR\*16 EQUIVALENCE (FILEEXT, BFILEEXT) JMARK=0 185=1 OPEN (UNIT=10, FILE='NOTHICK DADQ1.DAT', STATUS='OLD', FORM='FORMATTED') 1 READ (10,34572) FILEEXT READ (10,34572) DRIVE 34572 FORMAT (A) 4321 CONTINUE HEAD=FILEEXT IF (DRIVE.EQ.'A')DIR='DUC2:[ROTH.IMAG]' IF (DRIVE.EQ.'A')DISKT='DUC2:' IF (DRIVE.EQ.'C')DIR='DUC0:[ROTH.IMAG]' IF (DRIVE.EQ.'C')DISKT='DUC0:' ICHA=0 DO I=1,LEN(FILEEXT) IF (ICHA.NE.0) GOTO 98564 IF (BFILEEXT(I).EQ.32) THEN ICHA=I FILEEXT(ICHA:ICHA+4)='.SPC' ENDIF 98564 END DO FILENAME = '[ROTH.DATA]'//FILEEXT K=0 K≓K+1 20 IF (FILEEXT(K:K).NE.'.') GOTO 20 FILEEXT(K+1:K+3) = 'CAL' CALNAME = '[ROTH.DATA]'//FILEEXT CALL DONDISP1S (ICHA, FILENAME, CALNAME, HEAD, DIR, DISKT, SHAPEANS, SELFREQANS, ACTPOINT) 1

CLOSE(10) END

	SUBROUTINE DONDISPIS (ICHA,FILENAME,CALNAME,HEAD,DIR,DISKT, SHAPEANS,SELFREQANS,ACTPOINT)
С	
C C C C C	Read Data file written by CRUNCII and write values to Grinnell -UNCORRECTED & CORRECTED DATA IS DISPLAYED
C C C C C C C	Header: X3, Y3 Dimension of scan (SCAN, INDEX) N1, N2 Number of points (SCAN, INDEX)
	INTEGER*4 REC, SCANPOS, XXX INTEGER*2 IXLENGTH_A, IXLENGTH, ACTPOINT INTEGER*2 X3, Y3, Y87, N1, N2, NNNNN2, NNNNN1 INTEGER*2 DENS, NFREQ, AVES, X4, Y4, I87 INTEGER*2 COUNT, NCOUNT, NSCAN, NINDX INTEGER*2 COUNT, NCOUNT, NSCAN, NINDX INTEGER*2 C(1024), D(460) INTEGER*2 SCANDIST, INDXDIST, TRFREQ, ENDFREQ, 116 INTEGER*2 D_SHAPE(460), 189, 16, 115 INTEGER*2 D_SHAPE(460), 189, 16, 115 INTEGER*2 PSEUDOGRNL(460, 1024), SELFREQ REAL FREQ, MEAN REAL RNUP(7), RNLO(7), CBUFFER(81) BYTE BSCALEMARK(4), CHFREQ(3) BYTE BSUFFREQ BYTE BSUFFREQ BYTE BFILENAME(44), BNAMELAB(20), BDATA_STATUS(40) CHARACTER FILENAME*44, FILEEXT*23, SELFREQANS*1, FFLAG*1 CHARACTER CALNAME*44, CHEADER*32, SHAPEANS*1, ZIGANS*1 CHARACTER NAMELAB*20, DATA_STATUS*40, NEWHEADER*35, ACTUAL_SELFREQANS*1 CHARACTER CORNAME*15, CHFREQ_C*3, PHASE*1, PHASE1*1 CHARACTER SCALEMARK*4, SUFFREQ*4, HEAD*23, DIR*16, DISKT*5 EQUIVALENCE (CHFREQ, CHFREQ C)
	EQUIVALENCE (BNAMELAB, NAMELAB) EQUIVALENCE (BDATA_STATUS, DATA_STATUS) EQUIVALENCE (BSCALEMARK, SCALEMARK) EQUIVALENCE (BSUFFREQ, SUFFREQ)
с	SCALEMARK='1 MM' SUFFREQ=' MHZ'
c c	TAKE CHARACTER "FILENAME" AND DECODE TO BYTE "BFILENAME"
533	DECODE (44,533,FILENAME) BFILENAME FORMAT(44A1)

С

42

С DETERMINE SHORTENED (-.SPC) FILENAME POSITION С 16=1 115=1 116=1 KMARK=0 DO 4321 IPR=12,44 IF (KMARK.EQ.1) GOTO 4321 IF (BFILENAME(IPR).EQ.46) THEN **!PERIOD/DOT IS ASCII 46** IEND=IPR KMARK=1 ENDIF 4321 CONTINUE 34572 FORMAT (A) 34573 FORMAT (I) 51 FORMAT(A32) 52 FORMAT(A2) 53 FORMAT(A4) OPEN( unit=15, file=FILENAME(1:IEND-1)//'.datl2', status='OLD', ACCESS='DIRECT'.RECORDTYPE='FIXED',RECL=2, +form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) + OPEN( unit=16, file=FILENAME(1:IEND-1)//.datR4', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4, + + form='FORMATTED', ORGANIZATION='SEQUENTIAL' ) OPEN( unit=26, file=FILENAME(1:IEND-1)//".datRR4', status='OLD', С č c ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=4, + form='FORMATTED', ORGANIZATION-'SEQUENTIAL') + OPEN( unit=66, file=FILENAME(1:1END-1)//'.datCII', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=32, + form='FORMATTED', ORGANIZATION='SEQUENTIAL') + C\*\*\*\*\*\*\*\*\*\*\*\*\*UNIT=7,.SPC FILE FOR SPECTRA, vel, FOR DIRECT ACCESS\*\*\*\*\*\*\*C С OPEN( unit=7, file=FILENAME, status='OLD', ACCESS='DIRECT', С с с RECORDTYPE='FIXED',RECL=4,FORM='FORMATTED', \_ 4 ORGANIZATION='SEQUENTIAL') OPEN (UNIT=14, FILE='NOTHICK\_SELFREQ1.DAT', 1 STATUS='OLD', FORM='FORMATTED') 79193 READ(66,REC=16,FMT-51)CHEADER **I6=I6**+1 READ(66,REC=16,FMT=51)SHAPEANS 16=16+1

.

102

READ(66,REC=16,FMT=51)ZIGANS 16=16+1

READ (14,98652) FILEEXT READ (14,98652) DRIVE READ (14,98652) PHASE READ (14,98652) PHASE READ (14,98652) DIFFANS READ (14,10030) BUFLENGTH READ (14,10030) BUFVEL READ (14,10030) TRDIAM CLOSE (14) 98652 FORMAT (A)

- 10020 FORMAT (I)
- 10030 FORMAT (F)
- 89714 READ(15,REC=I15,FMT=52)SCANDIST 115=I15+i READ(15,REC=I15,FMT=52)INDXDIST I15=115+l READ(15,REC=115,FMT=52)NSCAN 115=115+1 READ(15,REC=115,FMT=52)NINDX 115=115+1 READ(15,REC=115,FMT=52)islant1 115-115+1 READ(15,REC=I15,FMT=52)islant2 115=115+1 READ(15,REC=115,FMT=52)islant3 115-115+1 READ(15,REC=I15,FMT=52)islant4 I15=I15+1 READ(15,REC=115,FMT=52)DENS 115=115+1 READ(15,REC=115,FMT=52)TRFREQ 115=115+1 READ(15,REC=115,FMT=52)AVES [15=[15+1 READ(15,REC=115,FMT=52)JXXX 115=115+1 С ARRAYSIZE=(NSCAN)\*(JXXX) !IF SCAN FINISHED PROPERLY,JXXX=NINDX

ENCODE (3,19878,CHFREQ) TRFREQ IANALYSIS FREQUENCY 19878 FORMAT (13)

> READ(16,REC=116,FMT=53)TIMESET 116=116+1

ENDFREQ=2.5\*TRFREQ CALL POINT\_FROM\_FREQ(ENDFREQ,TIMESET,ACTPOINT)

ENDIF 89318 PTS = REAL(NSCAN)\*REAL(JXXX) X3=ABS(SCANDIST) Y3=INDXDIST N1--NSCAN N2=JXXX IF (LEQ.1) THEN NNNNN1=N1 NNNNN1=N1 ENDIF

- DO 5697 I=1.NPTS 5697 READ(UNIT=52, END=89318)IABC,JABC,FFLAG,SCANKNT ENDIF 89318 PTS = REAL(NSCAN)\*REAL(JXXX)
- NPTS = NSCAN\*JXXX !!!!IF SCAN COMPLETED PROPERLY, J> IF (SHAPEANS.EQ.'Y')THEN DO 5697 I=1.NPTS

89317 SCANDIST=ABS(SCANDIST) AD=NSCAN XREAL = REAL(ABS(SCANDIST)) YREAL = REAL(INDXDIST)) NPTS = NSCAN\*JXXX !!!!!F SCAN COMPLETED PROPERLY, JXXX=NINDX

- STATUS='OLD', FORM='UNFORMATTED') INFO ON WHETHER WE ARE ON HOLDER/SAMPLE
- IF (SHAPEANS.NE.'Y')GOTO 89317 OPEN(UNIT=52,FILE=FILENAME(1:ICHA+10)/\*DATHS', STATUTATION OF DEPENDENT INFORMATION UNFORMATION WE ARE ON HOLDER (SAMPL

45

10149 CONTINUE

1

IF (JMARK.EQ.1) GOTO 89306

- 90 CONTINUE
- 30 CONTINUE
- 12345 IF (JMARK.EQ.1) GOTO 90 PILES ARE ALREADY OPEN

NEWU1=45 NEWU2=69

- OPEN (UNIT=NEWU1,FILE=DISKT//FILENAME(1:IEND-1)//CORNAME// + '.CORHEADER',STATUS='NEW',FORM='UNFORMATTED')
- ACCUM=0. NBAD=0 IF (ICHOICE.EQ.1) THEN NAMELAB='VELOCITY CM/US' CORNAME='\_VEL\_C\_'//CHFREQ\_C NEWHEADER='CORRECTED DATA FOR VELOCITY' NEWU=25

DO 9999 ICHOICE=1,1 187=1

ENDIF

C C C

108

XREAL = REAL(ABS(X3))YREAL = REAL(Y3)FREQ = REAL(NFREQ) PTS = REAL(N1)\*REAL(N2) Proportion GRINNELL window similar to scan dimensions Y87 = ININT( REAL(Y3)\*8./7. ) 200 IF( Y87.GE.X3 )THEN R1 = FLOAT(X3)/FLOAT(Y3)X4 = 400 Y4 - ININT(400./R1) IF (Y4.GE.480)THEN X4=300 Y4 = ININT(300./R1)ENDIF IF (Y4.GE.480)THEN X4=200 Y4 = ININT(200./R1) ENDIF IF (Y4,GE.480)THEN X4=100 Y4 = ININT(100./R1)ENDIF IF (Y4.GE.480)THEN X4=50 Y4 = ININT(50./R1) ENDIF IF (Y4.GE.480)THEN X4=25 Y4 = ININT(25./R1)ENDIF IF (Y4.GE.480)THEN X4=10 Y4 = ININT(10/R1)ENDIF ELSEIF( Y87.LT.X3 ) THEN RI - FLOAT(Y3) / FLOAT(X3) Y4 = IFIX(400.\*R1)X4 = 400IF (Y4.GE.480)THEN X4=300 Y4 - ININT(300.\*R1) ENDIF IF (Y4.GE.480)THEN X4=200 Y4 = ININT(200.\*R1)ENDIF IF (Y4.GE.480)THEN X4=100Y4 = ININT(100.\*R1) ENDIF IF (Y4.GE.480)THEN

X4=50 Y4 = ININT(50.\*R1)ENDIF IF (Y4.GE.480)THEN X4=25 Y4 - ININT(25.\*R1) ENDIF IF (Y4.GE.480)THEN X4=10 Y4 -= ININT(10.\*R1) ENDIF

CC

ENDIF

XD2G = REAL(N1)/REAL(X4)YD2G = REAL(N2)/REAL(Y4)

XD2X = REAL(X4)/REAL(N1) YD2Y = REAL(Y4)/REAL(N2)

I\_INT=JINT(XD2X)-1 J\_INT=JINT(YD2Y)+1

89306 CONTINUE

10300 format( // \$Enter choice :')

FORMAT (A) FORMAT ('+','VALUE=',F) 54322 4319

TYPE \*,' ' TYPE \*,'Working...' TYPE \*,' '

- 43191 FORMAT ('4','BAD PTS/TOT. PTS:',I5,'#,I4, + 'CURRENT VALUE=',F11.2)
- 7493 FORMAT (F11.2)
- 7494 FORMAT(I)

ł

с RETURN MAX/MIN OF DATA FOR GRINNELL DISPLAY & PRODUCE LINE C C OF GRINNELL DATA (CBUFFER)

CALL RETMAXMIN\_FILTER (FILENAME, CORNAME, CALNAME, NAMELAB, DISKT, IEND, JXXX,

NSCAN, SCANKNT, SHAPEANS, ZIGANS, ICHOICE, TIMESET, 189, COUNT, ACTPOINT, NEWU, GRBOT, GRTOP, MEAN) 1

7487 COUNT=NCOUNT RMIN-GRBOT RMAX=GRTOP 187=1

RNLO(ICHOICE)=RMIN RNUP(ICHOICE)=RMAX

	DO 500 KI=1,JXXX DO 49721 JJ=1,NSCAN NIPI=JJ NIPJ=KI SCANPOS=((NIPJ-1)*NSCAN)+NIPI
49721 462	187=SCANPOS READ (NEWU,REC=187,FMT=53) CBUFFER(JI) 187=187+1 FORMAT (F11.2) CALL SCGREAL (CBUFFER, C, N1,GRBOT,GRTOP,MEAN) !GREY SCALED DATA STATUS='CORRECTED DATA FOR '//NAMELAB
C C C	INTERPOLATE DATA GRID (EX.81X81) FOR X4 x Y4 GRINNELL DISPLAY
C	CALL INTR ( C,D,NSCAN,X4 )
С	IF (KI.EQ.20)TYPE *,'D=',D
C ****	****** MOD TO GET RID OF FALSE BORDER ****************** C IF (SHAPEANS.EQ.'Y')THEN
655 555	IIXCOUNT=0 D0 555 10P=1,X4 !FORWARD X-DIRECTION IF (D(10P).EQ.1)GOTO 555 IIXCOUNT=IIXCOUNT+1 IF (IIXCOUNT.EQ.1)THEN D0 655 IJQ=1,1_INT D(10P+IJQ-1)=1 ENDIF CONTINUE
855 755	IIXCOUNT=0 DO 755 IOP=X4,1,-1 IBACKWARD X-DIRECTION IF (D(IOP).EQ.1)GOTO 755 IIXCOUNT=IIXCOUNT+1 IF (IIXCOUNT.EQ.1)THEN DO 855 IJQ=1,1_INT D(IOP-IJQ+1)=I ENDIF CONTINUE
с	IF (KI.EQ.20)TYPE *,'D=',D
÷	
0 ****	
C ********** MOD TO GET RID OF FALSE BORDER ********** C	

DO 480 J= 1, X4 480 PSEUDOGRNL( J,NIPJ ) = D( J ) 500 CONTINUE

## C \*\*\*\*\*\*\*\*\*\* MOD TO GET RID OF FALSE BORDER \*\*\*\*\*\*\*\*\*\* C

ENDIF

- С IF (IJ.EQ.200)TYPE \*,'D=',D
- ENDIF 1755 CONTINUE
- IIXCOUNT=0 DO 1755 IOP=Y4,1,-1 IBACKWARD Y-DIRECTION IF (D(IOP).EQ.1)GOTO 1755 IIXCOUNT=IIXCOUNT+I IF (IIXCOUNT.EQ.1)THEN DO 1855 IJQ=1,J\_INT 1855 D(IOP-IJQ+I)=1
- ENDIF 1555 CONTINUE
- IIXCOUNT=0 DO 1555 IOP=1,Y4 IFORWARD Y-DIRECTION IF (D(IOP).EQ.1)GOTO 1555 IIXCOUNT=IIXCOUNT+1 IF (IIXCOUNT.EQ.1)THEN DO 1655 IJQ=1,J\_INT 1655 D(IOP+IJQ-1)=1

IF (SHAPEANS.EQ.'Y')THEN

C \*\*\*\*\*\*\*\*\*\* MOD TO GET RID OF FALSE BORDER \*

С IF (IJ.EQ.200)TYPE \*,'D=',D

CALL INTR (C,D,JXXX,Y4)

- DO 540 J= 1, N2 540 C(J) = PSEUDOGRNL(IJ,J)
- IXLENGTH=0 DO 800 IJ= 1, X4 605 IX = IJ-1

TYPE \*,X4,Y4,N1,N2,ICHOICE TYPE \*,SCANDIST,TRFREQ TYPE \*,RMIN,RMAX,MEAN

WRITE(NEWU2) X4, Y4, N1, N2, ICHOICE WRITE(NEWU2) SCANDIST, TRFREQ WRITE(NEWU2) RMIN, RMAX, MEAN

FORM='UNFORMATTED')

CC

+

OPEN (UNIT=NEWU2, FILE=DIR//HEAD//CORNAME//'.PDK',STATUS-'NEW',

C***********MODIFICATION FOR COMPLEX SHAPE **************		
IF (SHAPEANS.NE.'Y')GOTO 675 !NOT A COMPLEX SHAPE IF (SHAPEANS.EQ.'Y')THEN		
XXX=1		
IXSTART=IJ		
IYLENGTH=0		
NKEEP=0		
DO 8970 J=1,Y4		
IF (D(J).LT.2)GOTO 8970 11 IS CODED FOR LUCITE (IN SCGREAL)		
IF (D(J).GE.2)THEN ISAMPLE DATA		
IF (NKEEP.EQ.0)IYSTART=J		
NKEEP=1		
C**** FURTHER MOD FOR GEORGE'S DISCONTINUITY ON YBCO HEX SAMPLE *****		
IF (IYLENGTH.GT.I.AND.D(J).GE.2.AND.D(J-1).LT.2)THEN		
8875 XXX=XXX+1		
IYLENGTH=IYLENGTH+1		
D_SHAPE(IYLENGTH)=1		
IF (D(J-XXX),LT.2)GOTO 8875		
ENDIF C**** FURTHER MOD FOR GEORGE'S DISCONTINUITY ON YBCO HEX SAMPLE *****		
IYLENGTH=IYLENGTH+1		
D SHAPE(IYLENGTH)=D(J)		
ENDIF		
8970 CONTINUE		
C TYPE *,'IXSTART=',IXSTART,'IYSTART=',IYSTART,'IYLENGTH=',		
C 1 IYLENGTH		
IF (IYLENGTH.EQ.0)GOTO 800 ALL LUCITE IN THIS COLUMN		
IXLENGTH=IXLENGTII+1		
WRITE(NEWU2)IXSTART,IYSTART,IYLENGTH		
DO 8979 IJK=1,IYLENGTH		
8979 WRITE(NEWU2)D SHAPE(IJK)		
GOTO 800		
ENDIF		
C ************************************		
675 WRITE(NEWU2) D		
800 CONTINUE		

TYPE \*,' ' TYPE \*,' HIGHEST ',NAMELAB,' IS ',RMAX TYPE \*,' LOWEST ',NAMELAB,' IS ',RMIN TYPE \*,' '

WRITE (NEWU1)NEWHEADER WRITE (NEWU1)RMIN,RMAX WRITE (NEWU1)MEAN WRITE (NEWU1) ISCALEF -

97364 FORMAT (A) CLOSE (NEWU) CLOSE (NEWUI) CLOSE (NEWU2) TYPE \*, DONE CLOSING ', HEAD//CORNAME//'.PDK'

JMARK=1

- IF (SHAPEANS.NE.'Y')GOTO 9999 5001 REWIND(52) 9999 CONTINUE IXLENGTH\_A=IXLENGTH WRITE(15,REC=115,FMT=52)IXLENGTH A CLOSE(15)
- CLOSE(52) 87124 CONTINUE

CLOSE (6)

RETURN end

С

C C GRNLBASE.FOR C - A set of su C with the GRI - A set of subroutines useful for applications with the GRINNELL image processor. С GRINIT must be called in main program before calling these C C C subroutines.

David B. Stang latest update 19-APR-88

SUBROUTINE SCGREAL( CC,DD, N, BOT,TOP,MEAN )

000000 Convert values in CC to 1 thru 255 ( same as SCGR, with CC REAL ) CC(N) Input Data

```
DD(N)
           Output Data
```

- BOT Desired Min for Gray Scale ( units of CC )
- тор Desired Max for Gray Scale

INTEGER\*2 N DD(N) INTEGER\*2 REAL CC(N), MEAN

RAN - TOP - BOT IF (RAN.EQ.0.)RAN=1. DO 2000 J = I,N C0 = CC(J)Q = (C0 - BOT) / RANIF (Q.LE.0.) Q = 0. IF (Q.GT.1.) Q = 1.

> RETURN END

CC SUBROUTINE INTR CC CC C C C C Interpolate values in C(N2) to "fit" into D(NN) SUBROUTINE INTR ( CC,DD,N2,NN ) INTEGER\*2 N2,NN INTEGER\*2 CC(N2), DD(NN) RN = FLOAT(N2) / FLOAT(NN) DO 3000 K = 1,NN R = FLOAT(K)\*RNIR = IFIX(R)IR = IINT(R)IRPI = IR+1RR = R - FLOAT(IR)IF( IR.LT.1 ) IR=1 IF( NN.GT.N2 .AND. IRP1.GT.NN ) THEN IR=NN-1 IRP1=NN ENDIF C0 = FLOAT( CC(IR) ) C1 = FLOAT( CC(IRP1) ) D0 = (1.-RR)\*C0 + RR\*C1C 3000 DD(K) = IFIX(D0)C 3000 DD(K) = IINT(D0)C C C RETURN END

> SUBROUTINE RETMAXMIN\_FILTER(FILENAME,CORNAME,CALNAME,NAMELAB,DISKT, IEND,JXXX,NSCAN,SCANKNT,SHAPEANS,ZIGANS,ICHOICE,TIMESET,I89, COUNT,ACTPOINT,NEWU,GRBOT,GRTOP,MEAN)

> > 52

INTEGER\*4 REC,SCANPOS,I7 INTEGER\*2 NSCAN,ACTPOINT

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	INTEGER*2 185,187,SCANKNT INTEGER*2 IABC,JABC,JXXX,189 INTEGER*2 NCOUNT INTEGER*2 ZIGCOUNT INTEGER*2 NBAD,COUNT,LCOUNTER REAL DATATHING(1024,9) REAL MEAN,VEL(5000) REAL CBUFFER(81) CHARACTER FILENAME*44,CORNAME*15,NAMELAB*20,FFLAG*1 CHARACTER SHAPEANS*1,ZIGANS*1,DISKT*5,CALNAME*44 INTEGER*4 SCANPOS1
	TYPE *,NAMELAB LCOUNTER=1 ZIGCOUNT=1 ACCUM=0. SCANPOS=0 SCANPOS1=0 NBAD=COUNT 187=1 XMAX=0. XMIN=10000000. PTS = REAL(NSCAN)*REAL(JXXX) NPTS=NSCAN*JXXX
	CAL FILE WITH MAX/MIN/MEAN
+ +	OPEN( unit=8, file=CALNAME, status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED',RECL=4,FORM='FORMA'TTED', ORGANIZATION='SEQUENTIAL') 185=1
	read(8,REC=185,FMT=53)VUP
	185=185+1
	read(8,REC=185,FMT-53)VLO 185=185+1
	read(8,REC=185,FMT=53)VAVE
	IF (SHAPEANS.EQ.'Y')THEN NPTS=SCANKNT REWIND(52) ENDIF
	I7=NPTS*4*ACTPOINT+1 START OF VELOCITY READS IN SPC FILE
	SPC FILE (UNIT=7) CONTAINS ALL VELOCITY & SPECTRA DATA
+ +	OPEN (UNIT=7,FILE=DISKT//FILENAME,STATUS='OLD',ACCESS='DIRECT', RECORDTYPE='FIXED',RECL=4,FORM='FORMATTED', ORGANIZATION='SEQUENTIAL')
	OPEN (UNIT=NEWU,FILE=DISKT//FILENAME(1:IEND-1)//CORNAME//.COR',
	53

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124

DO 500 NIPJ=1,JXXX DO 450 NIPI=1,NSCAN 410 C\*\*\*\*\* GET INFO FROM HOLDER.DAT (FFLAG='S' -> SAMPLE) (FFLAG='H' -> HOLDER) KCON=KCON+I J=NIP] SCANPOSI=((NIPJ-1)\*NSCAN)+NIPI !TRUE SCAN POSITION IF (SHAPEANS.NE.'Y')GOTO 87123 READ(52)IABC, JABC, FFLAG, SCANKNT TYPE \*, 'XH=', IABC, 'YH=', JABC, ' FFLAG=', FFLAG С IF (FFLAG.NE.'S')GOTO 8702 !TRANSDUCER IS ON HOLDER/GOTO NEXT PT. 87123 SCANPOS=SCANPOS+1 CC !! 'SCANPOS' FOR FILE RETRIEVAL FOR CIRCLE DISK SCANS READ(7,REC=I7,FMT-53)VEL(SCANPOS)

STATUS='NEW',ACCESS='DIRECT', RECORDTYPE='FIXED',RECL=4,FORM='FORMATTED',

ORGANIZATION='SEQUENTIAL')

17=17+1

DATATHING(J,5)=VEL(SCANPOS)

IF (ICHOICE.EQ.1)THEN

IF (SHAPEANS.NE.'Y')GOTO 87651

RMIN=AMIN1(CBUFFER(J),XMIN)

ENDIF

CBUFFER(J)=0.0 GOTO 450 ENDIF

CONTINUE

XMAX=RMAX XMIN=RMIN

87651 CBUFFER(J)=DATATHING(J,5)

NPTS=(NIPJ-1)\*NSCAN+NIPI IF (NPTS.EQ.NSCAN\*JXXX)NPTS=NSCAN\*JXXX

IF (SCANPOS.EQ.1)DATATHINGPREVIOUS=VAVE

C\*\*\*\*\*KEEP TRACK OF MAX & MIN LIMITS OF CORRECTED DATA\*\*\*\*\*\*\*C C \*\*\*\* FOR FFLAG.NE.'S' --- WE SKIP THIS STEP SO THAT '0' IS NOT CONSIDERED RMAX=AMAX1(CBUFFER(J),XMAX)

IF (DATATHING(J,5).LT.(VLO+VLO\*0.001).OR. DATATHING(J,5).GT.(VUP-VUP\*0.001))DATATHING(J,5).~DATATHINGPREVIOUS

IF (FFLAG.NE.'S')THEN ISET TO 0 // TRANSDUCER IS ON HOLDER/GOTO NEXT PT.

SUBROUTINE POINT\_FROM\_FREQ(SELFREQ,TIMEPERDIV,ACTPOINT)

DO 49721 JI=1,NSCAN WRITE (NEWU, REC=187, FMT=53) CBUFFER(JI) ACCUM=ACCUM + CBUFFER(JI) TYPE \*,'CBUFFER(JI)-',CBUFFER(JI) С 49721 187=187+1 ELSEIF (ZIGANS.EQ.'Y'.AND.ZIGCOUNT.EQ.0)THEN !ZIGZAG/RIGHT->LEFT DO 49722 JI=NSCAN,1,-1 WRITE (NEWU, REC=187, FMT=53) CBUFFER(JI) ACCUM=ACCUM + CBUFFER(JI) TYPE \*,'CBUFFER(JI)=',CBUFFER(JI) C 49722 [87=]87+1 ENDIF C\*\*\*\*\* FOR ZIGZAG SCANS - TO ALTER ROW STORAGE \*\*\*\*\*\*\*\*\*\*C IF (ZIGANS.EQ.'Y'.AND.ZIGCOUNT.EQ.1)THEN ZIGCOUNT=0 **GOTO 500** ELSEIF (ZIGANS.EQ.'Y'.AND.ZIGCOUNT.EQ.0)THEN ZIGCOUNT=1 ENDIF C500 TYPE \*,'Y=',JABC,'CBUFFER--',CBUFFER 500 CONTINUE GRBOT = RMIN GRTOP = RMAX 5001 TYPE \*.' ' TYPE \*,'RMIN=',GRBOT TYPE \*, 'RMAX=', GRTOP MEAN = ACCUM/SCANPOS TYPE \*,'MEAN=',MEAN IF (SHAPEANS.NE.'Y')GOTO 88888 REWIND(52) 88888 CONTINUE FORMAT (A4) 53 43191 FORMAT ('+', 'BAD PTS =', 15,' AT LOCATION (SCANPOS) =',15) RETURN END

IF (ZIGANS.EQ.'N')THEN INOT A ZIGZAG SCAN - A NORMAL SCAN

ELSEIF (ZIGANS.EQ.'Y'.AND.ZIGCOUNT.EQ.1)THEN !ZIGZAG/LEFT->RIGHT

DATATHINGPREVIOUS=CBUFFER(J)

WRITE (NEWU, REC=187, FMT=53) CBUFFER(JI)

CONTINUE

49720 187=187+1

DO 49720 JI=1,NSCAN

ACCUM=ACCUM + CBUFFER(JI)

450

С

С DETERMINE SPECTRA POINT FROM FROM SPECIFIC FREQUENCY IN SPECTRA C C SEE SUBROUTINE CENTERFREQ FOR SIMILAR PROCESSING EXPLANATION С **INTEGER\*4 DUMMYFREQ** INTEGER\*2 SELFREQ.ACTPOINT REAL\*4 TIMEPERDIV, DELFREQ, TEMPPOINT С С DUMMYFREQ=SELFREQ\*1E+06 DELFREQ=(1./(2.\*(10.\*TIMEPERDIV))) TEMPPOINT=DUMMYFREQ/DELFREQ ACTPOINT=JNINT(TEMPPOINT) С RETURN END SUBROUTINE CENTERFREQ(DUMMYP,TIMEPERDIV,ACTFREQ) С c c DETERMINE FREQUENCY FROM POINT IN B1(F) SPECTRA INTEGER\*2 DUMMYP, ACTFREQ TIMEPERDIV, DELFREQ, TEMPFREQ REAL\*4 WE KNOW THAT DELFREQ=(1/(2N\*DELTIME)) =(1/(2N\*(10\*TIMEPERDIV/N))) -(1/(2\*(10\*TIMPERDIV))) WHERE N = 512 POINTS/ACQUISITION (SCREEN) TIMEPERDIV = TIME SETTING PER DIVISION (EX. 50 NSEC) 2 = WE EXTENDED 512 ARRAY TO 1024 ARRAY FOR PROCESSING 10 = THE NUMBER OF DIVISIONS/SCREEN FOR EXAMPLE: WE CAN DETERMINE THE FREQUENCY FOR WHICH THE POINT "MAXBIP" CORRESPONDS TO BY JUST MULTIPLYING (DELFREQ) \* (MAXB1P) DELFREQ=(1./(2.\*(10.\*TIMEPERDIV))) TEMPFREQ=DELFREQ\*DUMMYP TEMPFREQ=TEMPFREQ/1E+06 ACTFREQ=JNINT(TEMPFREQ) TYPE \*. C C C C C TYPE \*, 'POINT=', DUMMYP,' FREQ=', ACTFREQ,' MHZ' TYPE \*,' RETURN END С С С C C SUBROUTINE INTR (F1, F2, N, M) C C

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IMPLICIT NONE INTEGER\*2 I, M, N INTEGER\*2 F1(N), F2(M) REAL\*4 X, XA(512), Y, YA(512) DO I = 1, N XA(I) = FLOATI(I)END DO DO I = 1, N YA(I) = FLOATI(FI(I))END DO DO I = 1, MX = FLOATI(I-1) \* FLOATI(N-1) / FLOATI(M-1) + 1.0CALL LINEAR\_INTERPOLATION (XA, YA, N, X, Y) F2(I) = ININT(Y)END DO RETURN END LINEAR\_INTERPOLATION computes the value of the piecewise linear spline interpolant of the points in the arrays XA and YA at the point X. This routine is a modified version of the FORTRAN routine SPLINT found in the book "Numerical Recipes: The Art of Scientific Computing" by Press, Flannery, Teukolsky, and Vetterling published by the Cambridge University Press, 1986. Variables: NMAX : A constant which determines the array sizes for U, X, and Y. K: The midpoint between KHI and KLO ... used to find the two indices into the XA table such that XA(KLO) < X < XA(KIII). $\ensuremath{\mathsf{KHI}}$  : The greater of the two indices into the XA array such that XA(KLO) < X < XA(KHI). KLO: The lesser of the two indices into the XA array such that XA(KLO) < X < XA(KHI). N: The index of the arrays and Y that contain interpolation points. A : Weight given to YA(KLO). B: Weight given to YA(KHI). H: The difference of XA(KHI) and XA(KLO). X: The value of X at which to compute the value of the interpolation function. XA : The table of X coordinates of the interpolation points. Y: The value of the interpolation function evaluated at X. YA : The table of Y coordinates of the interpolation points. SUBROUTINE LINEAR\_INTERPOLATION (XA, YA, N, X, Y)

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C C IMPLICIT NONE С INTEGER NMAX PARAMETER (NMAX=512) С INTEGER\*2 K, KHI, KLO, N REAL\*4 A, B, H REAL\*4 X, XA(NMAX), Y, YA(NMAX) C C KLO = 1 KHI = N DO WHILE (KHI-KLO.GT.1) K = (KHI + KLO) / 2IF (XA(K).GT.X) THEN KHI = K ELSE KLO = K END IF END DO С H = XA(KHI) - XA(KLO)H = XA(KLO)IF (H.NE.0.0) THEN A = (XA(KHI) - X) / HB = (X - XA(KLO)) / HY = A \* YA(KLO) + B \* YA(KIII)END IF C C RETURN END

C \*\*\*\*\*\* NOTHICK\_DRAW.FOR \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*C

INTEGER\*2 TRFREQ, JXXX, IXLENGTH INTEGER\*2 SCANDIST, INDXDIST, NSCAN, NINDX, DENS INTEGER\*2 SELFREQ, AVES, I6, 115, ISLANT1, ISLANT2, ISLANT3, ISLANT4 CHARACTER RESP1\*1,SELFREQANS\*1,RESP2\*2 CHARACTER NEWOLD\*3, SHAPEANS\*1, ZIGANS\*1, CHFREQ C\*3, CHDRI\*1 BYTE B, CHFREQ(3), BSUFFREQ(4) BYTE BSCALEMARK(4) BDATA STATUS(40), BLABEL(30), BFILEEXT(23) BYTE CHARACTER LABEL\*30, FILEEXT\*23, CHEADER\*32, TEBAR\*1 CHARACTER L\*48, DIR\*16, DRIVE\*1, NOISANS\*1, DIFFANS\*1 CHARACTER SUFFREQ\*4, FILENAME\*34, SCALEMARK\*4, DATA\_STATUS\*40 CHARACTER ACTUAL\_SELFREQANS\*1,SASANS\*1,PHASE\*1,PHASE1\*1

EQUIVALENCE (BFILEEXT, FILEEXT) EQUIVALENCE (CHFREQ\_C) EQUIVALENCE ( L,B ) EQUIVALENCE ( BSCALEMARK, SCALEMARK ) EQUIVALENCE (BSUFFREQ, SUFFREQ) EQUIVALENCE (BDATA\_STATUS, DATA\_STATUS) EQUIVALENCE (BLABEL, LABEL)

NEWOLD='OLD'

OPEN (UNIT=10,FILE='NOTHICK\_DADQ1.DAT',STATUS=NEWOLD, IFORM='FORMATTED')

READ (10,511) FILEEXT READ (10,511) DRIVE FORMAT (A)

- 511 FORMAT (A32) 51
- FORMAT (A2) 52
- 53
- FORMAT (A4)
- 677 FORMAT (I)

OPEN( unit=66, file='[ROTH.DATA]'//FILEEXT//'.datCH', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=32,

form='FORMATTED', ORGANIZATION='SEQUENTIAL')

OPEN (UNIT=14,FILE="NOTHICK\_SELFREQ1.DAT, 1

STATUS='OLD', FORM='FORMATTED')

OPEN( unit=15, file='[ROTH.DATA]'//FILEEXT//'.datl2', status='OLD', ACCESS='DIRECT', RECORDTYPE='FIXED', RECL=2,

÷ form='FORMATTED', ORGANIZATION='SEQUENTIAL')

16=1

+

+

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79193 READ(66,REC=I6,FMT=51)CHEADER 16=I6+1 READ(66,REC=I6,FMT=51)SHAPEANS 16=16+1 READ(66,REC=16,FMT=51)ZIGANS

READ(15,REC=115,FMT=52)TRFREQ 115-115+1 READ(15,REC=115,FMT=52)AVES 115=115+1 READ(15,REC=I15,FMT=52)JXXX 115=115+1 READ(15,REC=115,FMT=52)IXLENGTH ENCODE (3,19878,CHFREQ) TRFREQ !ANALYSIS FREQUENCY 19878 FORMAT (I3) DETERMINE SHORTENED (-.DAT) FILEEXT POSITION

115=1 89714 READ(15,REC=I15,FMT=52)SCANDIST 115=115+1 READ(15,REC-I15,FMT-52)INDXDIST 115=115+1 READ(15,REC=I15,FMT=52)NSCAN 115 = 115 + 1READ(15,REC=I15,FMT=52)NINDX I15=I15-1 READ(15,REC=115,FMT=52)islant1 115=115+1 READ(15,REC=115,FMT=52)islant2 [15=115+1]READ(15,REC=I15,FMT=52)islant3 115=115+1 READ(15,REC=I15,FMT=52)islant4 115=115+1 READ(15,REC=115,FMT=52)DENS [15=[15+1 С ARRAYSIZE=(NSCAN)\*(JXXX) !IF SCAN FINISHED PROPERLY, JXXX=NINDX

60

READ (14,98652) FILEEXT READ (14,98652) DRIVE READ (14,98652) PHASE READ (14,98652) PHASE1 READ (14,98652) DIFFANS READ (14,10030) BUFLENGTH READ (14,10030) BUFVEL READ (14,10030) TRDIAM

**16=16**+1

CLOSE (14) 98652 FORMAT (A) 10020 FORMAT (I) 10030 FORMAT (F)

C C C C C

С

KMARK=0 DO 4321 IPR=1,34

IF (KMARK.EQ.1) GOTO 4321

TYPE \*,' ' TYPE \*,'IMAGE FREQUENCY (MHz) = ',TRFREQ ENCODE (3,9878,CHFREQ) TRFREQ 9878 FORMAT (I3) 234 WRITE (5,394) FORMAT ('\$',' COLOR (C) OR B&W (B) IMAGE? ') 394

READ (5,2222) RESP1

TYPE \*,' \*\*\*\*\*\* NOTHICKNESS VELOCITY IMAGE \*\*\*\*\*\* '
TYPE \*,' '

FILENAME='[ROTH.DATA]'//FILEEXT CALL GRINIT CALL GRSRST

)?' READ (5,51)CHDRI IF (CHDRI.NE.'Y'.AND.CHDRI.NE.'N')GOTO 5321 IF (CHDRI.EQ.'Y')DIR='DUC0:[ROTH.IMAG]' ENDIF TYPE \*,' ' TYPE \*,' DO YOU WANT TO SEE TEXT AND COLORBAR (Y/N)?" READ (5,51)TEBAR

IF (TEBAR.NE.'Y'.AND.TEBAR.NE.'N')GOTO 211

IF (DIR(1:5).EQ.'DUC0:')THEN TYPE \*, DO YOU WANT TO CHANGE TO DUC2: (Y/N )?' READ (5,51)CHDRI IF (CHDRI.NE.'Y'.AND.CHDRI.NE.'N')GOTO 5321 IF (CHDRI.EQ.'Y')DIR='DUC2:[ROTH.IMAG]' ELSEIF (DIR(1:5).EQ.'DUC2:')THEN TYPE \*,'DO YOU WANT TO CHANGE TO DUCO: (Y/N

IF (DRIVE.EQ.'A')DIR='DUC2:[ROTH.IMAG]' IF (DRIVE.EQ.'C')DIR='DUC0:[ROTH.IMAG]' TYPE \*,'CURRENT DRIVE TO READ IMAGES IS ',DIR(1:5)

TYPE \*,' IF YOU WANT A DIFFERENT IMAGE FILE, YOU MUST' TYPE \*,' RECALL AN OLDER "NOTHICK\_DADQ1.DAT" FILE' TYPE \*,' '

5321

TYPE \*,' CURRENT IMAGE FILE IS ', FILEEXT

IF (BFILEEXT(IPR).EQ.46) THEN PERIOD/DOT IS ASCII 46

137

IEND=IPR KMARK=1

CONTINUE

FILEEXT=FILEEXT(1:1END-1)

ENDIF

C C C

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C4321

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211

CONTINUE

2222 FORMAT(A) IF (RESP1.NE.'C'.AND.RESP1.NE.'B')GOTO 234 IF (RESP1.EQ.'C')THEN TYPE \*,' '

TYPE \*,' ' WRITE (5,499) 499 FORMAT ('\$',' "COLORRED" (R) OR NORMAL COLOR (C) SCHEME? ') READ (5,2222) RESP2 ENDIF

- 500 CALL IMAGE(NEWOLD,FILEEXT,CHFREQ\_C,RESP1,RESP2,SHAPEANS,IXLENGTH, I FILENAME,DIR,TEBAR)
- 444 CONTINUE STOP END

1

SUBROUTINE IMAGE(NEWOLD,FILEEXT,CHFREQ\_C,RESP1,RESP2,SHAPEANS,IXLENGTH, FILENAME,DIR,TEBAR)

INTEGER\*2 D(460), CHANNEL, INPUT, IXLENGTH INTEGER\*2 X4,Y4,N1,N2,TRFREQ,SCANDIST CHARACTER\*1 RESP1\*1, SHAPEANS\*1, RESP2\*1, TEBAR CHARACTER CHFREQ\_C\*3 REAL RMIN, RMAX, MEAN BYTE B, CHFREQ(3), BSUFFREQ(4), BZERO(2) BYTE BFILENAME(34), BSCALEMARK(4) BYTE BDATA\_STATUS(40), BLABEL(30) BYTE CHMEAN(5),CHRMAX(5),CHRMIN(5) CHARACTER FILNAM\*48, LABEL\*30, FILEEXT\*23 CHARACTER L\*48, DIR\*16, CZERO\*2 CHARACTER SUFFREQ\*4, FILENAME\*34, SCALEMARK\*4, DATA\_STATUS\*40

EQUIVALENCE ( L,B ) EQUIVALENCE ( BSCALEMARK, SCALEMARK ) FQUIVALENCE ( BSUFFREQ, SUFFREQ ) EQUIVALENCE ( BDATA\_STATUS, DATA\_STATUS ) EQUIVALENCE ( BLABEL, LABEL ) EQUIVALENCE ( CZERO, BZERO )

CZERO='0 ' LLLL=0 IIIMAGE=1

212 CONTINUE

IF (IIIMAGE.EQ.I)FILNAM='\_VEL\_C\_'//CHFREQ\_C//'.PDK'

501 CONTINUE CHANNEL=0 IF (CHANNEL.NE.0.AND.CHANNEL.NE.2.AND.CHANNEL.NE.3) GOTO 501 IF (CHANNEL.EQ.0) THEN INPUT=0

62

MASK=1 ELSEIF (CHANNEL.EQ.2) THEN INPUT=1 MASK=4 ELSEIF(CHANNEL.EQ.3) THEN INPUT=2 MASK=8 ENDIF

CALL ERASE

OPEN (UNIT-6,FILE=DIR//FILEEXT//FILNAM,STATUS='OLD', 19 IFORM='UNFORMATTED')

> READ(6) X4,Y4,N1,N2,IVALUE READ(6) SCANDIST,TRFREQ READ(6) RMIN, RMAX, MEAN

IF ( IVALUE.EQ.1 ) LABEL='VELOCITY CM/US'

ICOLORBAR=0 SUFFREQ=' MIIZ' SCALEMARK='1 MM' DATA STATUS=LABEL

CALL GRNIN(1, INPUT, INPUT, INPUT) CALL GRNBY(1,1,1,1) CALL GRSBFD

IF (SHAPEANS.NE.'Y')IX49=X4

IF (SHAPEANS.EQ.'Y')THEN IX49=IXLENGTH ENDIF

DO 100 I=1,IX49 IF (SHAPEANS.NE.'Y')THEN IXSTART=I-I IYSTART=1 IYLENGTH-Y4 READ(6)D GOTO 789 ELSEIF (SHAPEANS.EQ.'Y')THEN IF (I.NE.1.AND.IYLENGTH.EQ.1)GOTO 100 READ(6,END=100)IXSTART,IYSTART,IYLENGTH DO 7897 IJK=1,IYLENGTH 7897 READ(6)D(IJK) 789 CONTINUE ENDIF CALL GRWAW(D,IXSTART,IYSTART,I,IYLENGTH,0,0,0,1,1) C \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\* CALL GRSBFD CONTINUE

100

IF (RESP1.EQ.'B')THEN IF (TEBAR.EQ.'N')GOTO 213 CALL PLACEBAR(0) GOTO 8999 ELSEIF (RESP1.NE.'B')THEN

IF (RESP2.EQ.'C')THEN CALL COLORS (IVALUE,ICOLORBAR) ELSEIF (RESP2.EQ.'R')THEN CALL COLORRED (IVALUE,ICOLORBAR) ENDIF

ENDIF

### IF (TEBAR.EQ.'N')GOTO 213

- 8999
   DECODE (34,8989,FILENAME) BFILENAME

   8989
   FORMAT (34A1)
- ENCODE (3,909,CHFREQ) TRFREQ 909 FORMAT (I3)

CALL GRFCD (1,255,0,0,BFILENAME,1,441,6,0,34,0,0,0) CALL GRFCD (1,255,0,0,CHFREQ,200,441,6,0,3,0,0,0) CALL GRFCD (1,255,0,0,BSUFFREQ,215,441,6,0,4,0,0,0)

CC

CC PRINT LABEL TO GRINNELL CC

```
NCHAR=LEN(DATA_STATUS)
DO 765 1KY=1,NCHAR
IKX=400-(IKY-1)*13
CALL GRFCD (1,255,0,0,BDATA_STATUS(IKY),505,IKX,0,0,1,0,0,0)
CALL GRSBFD
CONTINUE
```

765 CC

CC CALCULATE MAX, MIN, AND MEAN CC

IF (IVALUE.EQ.1.OR.IVALUE.EQ.2.OR.IVALUE.EQ.6.OR.IVALUE.EQ.7) THEN IF (IVALUE.EQ.1) THEN IF (RMAX.EQ.1.0) RMAX=.9999 ENDIF RRMAX=RMAX\*10.\*\*4. RRMIN=RMIN\*10.\*\*4. RMEAN=MEAN\*10.\*\*4.

ELSEIF (IVALUE.EQ.3.OR.IVALUE.EQ.4) THEN RRMAX=RMAX/100.

73921 IF (IRMIN.GE.1.0\*10.\*\* ENCODE (5,9878,CHRM 73922 CONTINUE 9878 FORMAT (15)

IF (IMEAN.GE.1.0\*10.\*\*5.) GOTO 73920 ENCODE (5,9878,CHMEAN) IMEAN 73920 IF (IRMAX.GE.1.0\*10.\*\*5.) GOTO 73921 ENCODE (5,9878,CHRMAX) IRMAX 73921 IF (IRMIN.GE.1.0\*10.\*\*5.) GOTO 73922 ENCODE (5,9878,CHRMIN) IRMIN

TYPE \*,' ' TYPE \*,'CORRECTED:' TYPE \*,'IRMAX=',IRMAX TYPE \*,'IRMIN=',IRMIN TYPE \*,'IMEAN=',IMEAN TYPE \*,' '

IMEAN=JNINT(RMEAN) IRMAX=JNINT(RRMAX) IRMIN=JNINT(RRMIN)

DO 9879 IUY=0,350,350 CALL GRFAR (1,255,0,0,JKMN,IUY,1,1) CALL GRSBFD 9879 CONTINUE

CC DRAW DECIMAL POINT FOR MIN AND MAX TO GRINNELL

ELSEIF (IVALUE.EQ.5) THEN IF (RMAX.GE.100.)RMAX=99.9 IF (RMIN.GE.100.)RMIN=99.9 IF (MEAN.GE.100.)MEAN=99.9 IF (RMAX.LT.10.)THEN RRMAX=RMAX\*10.\*\*4 RRMIN=RMIN\*10,\*\*4. RMEAN=MEAN\*10.\*\*4. ELSE RRMAX=RMAX\*10.\*\*3. RRMIN=RMIN\*10.\*\*3. RMEAN=MEAN\*10.\*\*3. ENDIF ENDIF IF (IVALUE.EQ.2.OR.IVALUE.EQ.6.OR.IVALUE.EQ.7) THEN JKMN=465 ELSEIF (IVALUE.EQ.I.OR.IVALUE.EQ.3.OR.IVALUE.EQ.4)THEN JKMN=463 ELSEIF (IVALUE.EQ.5)THEN JKMN≕470 ENDIF

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RRMIN=RMIN/100. RMEAN=MEAN/100.

```
9877
      CONTINUE
      IF (IVALUE.EQ.2) THEN
     JKMN=465
        ELSEIF (IVALUE.EQ.I.OR.IVALUE.EQ.3.OR.IVALUE.EQ.4.OR.IVALUE.EQ.6
             .OR.IVALUE.EQ.7)THEN
  1
       JKMN=463
      ELSEIF (IVALUE.EQ.5)THEN
        JKMN=470
        ENDIF
      CALL GRFAR (1,255,0,0,JKMN,ISCALEF,1,1)
      CALL GRSBFD
95631 CONTINUE
CC
CC DRAW SCALE ONTO IMAGE
сс
      RSCANDIST=FLOATI(SCANDIST)
      PIXELS=(X4*1,)/(RSCANDIST)
      IPIXELS=ININT(PIXELS)
      CALL GRFVCS (1,255,340,420,340+IPIXELS,420)
      CALL GRFCDS (1,255,BSCALEMARK,345,410,6,0,4)
      CALL GRSBFD
C! FOR DRAWING INITIAL ZEROES FOR ATTENUATION COEFF. < 0.1
      IF (IVALUE.EQ.2.AND.RRMIN.LT.1000.)THEN
      CALL GRFCDS (1,255,BZERO,JKMN,0,6,0,2)
      CALL GRSBFD
      ENDIF
      CONTINUE
213
201
      CLOSE(6)
 1
      FORMAT($',' WHICH IMAGE TO VIEW [*.PDK IN ROTH.IMAG]?')
      FORMAT(A)
2
```

FORMAT('\$','Channel (0,2,3) ?')

3

```
IF (IMEAN.GE.1.0*10.**6.)GOTO 93920
ZZZZZZ=RRMAX-RRMIN
IF (ZZZZZZ.EQ.0.)ZZZZZ=1.
SCALEF=((RMEAN-RRMIN)/(ZZZZZZ))*350. !SC. MEAN TO CLR BAR
ISCALEF=ININT(SCALEF)
93920 CONTINUE
```

IF (IMEAN.GE.1.0\*10.\*\*6.)GOTO 83920

IF (IRMAX.GE.1.0\*10.\*\*6.)GOTO 83921

CALL GRFCDS (1,255,CHRMAX,458,350,60,4) 83921 IF (IRMIN.GE.1.0\*10.\*\*6.)GOTO 83922 CALL GRFCDS (1,255,CHRMIN,458,0,60,4)

CALL GRSBFD

83922 CONTINUE

83920

CALL GRFCDS (1,255,CHMEAN,458,ISCALEF,6,0,4)

4 5 FORMAT( '\$Description ?? ')

- FORMAT('0') 6
- 7
- FORMAT('',A) FORMAT(' Range = ',A,', ',A) FORMAT(' Mean = ',A15,' ',A) FORMAT(I) 8
- 9

TYPE \*,''

999 CALL GRSEND

CONTINUE 444 RETURN END

SUBROUTINE COLORSUB (IVALUE, ICOLORBAR)

INTEGER\*2 NR(256),NB(256),NG(256),IARRAY(18) DATA IARRAY/0,2,1,0,1,2,1,0,2,1,2,0,2,0,1,2,1,0/

IF (IVALUE.GT.10) GOTO 9876 CALL GRINIT\_OLD CALL GRSRST CALL GRZFC(0,0) CALL GRZCL(0,255,255) CALL GRZON(0,1) CALL GRSBFD

B=4 A=2

L=256 IL=L/B JL=A\*IL

DO 100 I=1,IL NB(1)=255 NR(I)=0 NG(I)=B\*I IF(NG(I).GT.255)THEN NG(I)=255 ENDIF

100 CONTINUE

DO 200 I=IL+1,JL BB=((B/(1-A))\*I)+((A/(A-1))\*L) NG(I)=255 NR(I)=0NB(I)=BB IF (NB(I).GT.255)THEN NB(I)=255 ENDIF 200 CONTINUE

DO 300 1=JL+1,JL+IL

IF (NR(I).GT.255)THEN

DO 400 I=JL+IL+1,L GG=((-B)\*I)+(B\*L) NR(I)=255

NB(1)=0 NG(1)=GG IF(NG(1).GT.255)THEN

RR=(B\*I)-(A\*L) NG(I)=255 NB(I)=0 NR(I)=RR

NR(I)=255 ENDIF 300 CONTINUE

NG(I)=255 ENDIF 400 CONTINUE

> NR(1)=0 NG(1)=0 NR(256)=255 NG(256)=255 NB(256)=255

800 KC=0

889

С

CALL GRSBFD IF (IVALUE.EQ.1.OR.IVALUE.EQ.3.OR.IVALUE.EQ.5.OR.IVALUE.EQ.7) THEN DO 1111 J=1 200

CALL GRNWR(1,NB,IARRAY(1+KC),0,256,0) CALL GRNWR(1,NG,IARRAY(2+KC),0,256,0)

CALL GRNWR(1,NR,IARRAY(3+KC),0,256,0)

DO 1111 I=1,300 DO 1111 J=1,900 1111 CONTINUE GOTO 950

ENDIF

CALL GRSBFD CALL GRNIN(0,0,0,0) IF (ICOLORBAR.EQ.1) THEN CALL GRNBY (0,0,0,0)

- 950 KC=0
- 9876 RETURN END

## SUBROUTINE PLACEBAR (ICOLORBAR)

CC ----- Draw colorbar at right side of screen------

INTEGER\*2 NA(45)

IF (ICOLORBAR.EQ.1) GOTO 1010 CONTINUE DO 1000 I=0,350 DO 2000 J=1,19 G=1\*(254.0/350.0) NA(J)=G 2000 CONTINUE CALL GRWLW(NA,410,I,19,0,0,1,1) CALL GRSBFD 1000 CONTINUE 1010 CONTINUE RETURN

# SUBROUTINE SAVEBAR

INTEGER\*2 BAR(6)

END

TYPE \*,' ' TYPE \*,'Creating and saving the color bar...' TYPE \*,' '

OPEN(UNIT=34,NAME='BARFILE',STATUS='NEW', IFORM='UNFORMATTED',BLOCKSIZE=1024)

CALL GRNIN(1,0,0,0) CALL GRNBY(1,1,1,1) CALL GRSBFD

DO 2060 IBBEL=0,459,3 CALL GRRLW (410,IBBEL,6,1,BAR) WRITE(34) BAR 2060 CONTINUE

> CALL GRSBFD CLOSE(34) RETURN END

#### SUBROUTINE ERASE

M=4095 N=4095 CALL GRFER (M,N,0) CALL GRSBFD END

SUBROUTINE COLORS (IVALUE, ICOLORBAR)

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INTEGER\*2 NR(256),NB(256),NG(256),IARRAY(18) DATA IARRAY/0,2,1,0,1,2,1,0,2,1,2,0,2,0,1,2,1,0/ INTEGER\*2 NA(45)

IF (IVALUE.GT.10) GOTO 9876 CALL GRINIT\_OLD CALL GRSRST CALL GRZFC(0,0) CALL GRZCL(0,255,255) CALL GRZON(0,1) CALL GRSBFD

B=4 A=2

L=256 IL=L/B JL=A\*IL

DO 100 I=1,IL NB(I)=255 NR(I)=0 NG(I)=B\*1 IF(NG(I).GT.255)THEN NG(I)=255 ENDIF 100 CONTINUE

> DO 200 I=IL+1,JL BB=((B/(1-A))\*1)+((A/(A-1))\*L) NG(1)=255 NR(I)=0 NB(I)=BB IF (NB(I).GT.255)THEN NB(1)=255 ENDIF

200 CONTINUE

DO 300 l=JL+1,JL+1L RR=(B\*I)-(A\*L) NG(I)=255 NB(I)=0 NR(I)=RR IF (NR(I).GT.255)THEN NR(I)=255 ENDIF 300 CONTINUE

> DO 400 I=JL+IL+1,L GG=((-B)\*I)+(B\*L) NR(I)=255

NB(I)=0 NG(I)=GG IF(NG(I).GT.255)THEN NG(I)=255 ENDIF 400 CONTINUE

800 KC=0

NR(1)=0 NG(1)=0 NB(1)=0 NR(256)=255 NG(256)=255 NB(256)=255

 889 CALL GRNWR(1,NB,IARRAY(1+KC),0,256,0) CALL GRNWR(1,NG,IARRAY(2+KC),0,256,0) CALL GRNWR(1,NR,IARRAY(3+KC),0,256,0) CALL GRSBFD CALL GRNIN(0,0,0,0) IF (ICOLORBAR.EQ.1) THEN CALL GRNBY (0,0,0,0) ENDIF CALL GRSBFD DO 1111 I=1,300 DO 1111 J=1,900
 1111 CONTINUE

1111 CONTINUE GOTO 950 950 KC=0

CC ------Draw colorbar at right side of screen------

9876 IF (ICOLORBAR.EQ.1) GOTO 1010 CONTINUE DO 1000 1=0,350 DO 2000 J=1,19 G=I\*(254.0/350.0) NA(J)=G 2000 CONTINUE CALL GRWLW(NA,410,I,19,0,0,1,1) CALL GRSBFD 1000 CONTINUE 1010 CONTINUE RETURN END

Subroutine colorred(IVALUE,ICOLORBAR)

INTEGER\*2 NR(256),NB(256),NG(256),IARRAY(18) DATA JARRAY/0,1,2,0,2,1,1,0,2,1,2,0,2,0,1,2,1,0/ INTEGER\*2 NA(45)

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159

10010 format(A) 10020 format(I) NM256 = 0

### IF (IVALUE.GT.10) GOTO 9876

CALL GRINIT\_OLD

CALL GRSRST CALL GRSBFD L=256 IL=L/3 JL=2\*1L NM256=255

с

DO 100 I=1,IL NB(I)=0 NR(I)=1\*3 NG(I)=0 IF( NR(I).GT.253 )NR(I)=253 100 CONTINUE

DO 200 I=IL+1,JL NG(I)=3\*(I-IL) NR(I)=253 NB(I)=0 IF( NG(I).GT.253 )NG(I)=253 200 CONTINUE

> DO 300 I=JL+1,255 NG(I)=253 NR(I)=253 NB(I)=3\*(I-JL) IF( NR(I).GT.253 )NR(I)=253 CONTINUE

800 KC=6

300

NR(1)=0 NG(1)=0 NR(1)=0 NR(256)=NM256 NG(256)=NM256 NB(256)=NM256

840 CALL GRNWR(1,NB,IARRAY(1+KC),0,256,0) CALL GRNWR(1,NG,IARRAY(2+KC),0,256,0) CALL GRNWR(1,NR,IARRAY(2+KC),0,256,0) CALL GRSBFD CALL GRSBFD

C10860 format( \$ <CR> for next color scheme, Q to quit :' ) C READ( 5,10010 )ANS

C IF( ANS.EQ.'Q' .OR. ANS.EQ.'q' )GOTO 9876 GOTO 9876 KC = KC+3 IF (KC.GE.18) KC=0 GOTO 840

CC ------Draw colorbar at right side of screen------

 9876
 IF (ICOLORBAR.EQ.1) GOTO 1010

 CONTINUE
 DO 1000 I=0,350

 DO 2000 J=1,19
 G=1\*(254.0/350.0)

 NA(J)=G
 2000

 2000
 CONTINUE

 CALL GRWLW(NA,410,1,19,0,0,1,1)
 CALL GRSBFD

 1000
 CONTINUE

 1010
 CONTINUE

C 900 CALL GRSEND return END

L

What is claimed is:

1. A pulse-echo, immersion method for ultrasonic evaluation of a material, employing automatic scanning and digital imaging to obtain an image of a property of said material, wherein said material is held in a holding apparatus which is positioned in an immersion liquid over an acoustic reflector, said reflector having an acoustic impedance which is greater than that of said liquid, and wherein nonlevelness in said holding apparatus and material thickness are accounted for and eliminated, said method comprising:

- (i) ultrasonically scanning said material at a plurality of scan points and receiving the first and second echoes, each of which is a complete waveform, reflected off the back surface of said material and the first echo reflected off the front surface of said reflector both with and without the presence of said material; 15
- (ii) adjusting the time delay for each said received echo from each said scan point during said scanning in (i) above, gating each said received echo so that it is centered within its respective time window;
- (iii) automatically scanning said material at said scan
   points to receive said first and second back surface echoes and said two front surface echoes using the information obtained in (ii) above, so that each echo received from each scan point during said automatic scanning is centered within its time window;
- (iv) digitizing each echo received during said automatic scanning and determining the time delay between said first two successive sample back surface echoes,  $2\tau$ , and the time delay,  $\Delta t$ , between the two different reflector front surface echoes received at each scan point during said automatic scanning and calculating the wave velocity, using a cross correlation function, at each said scan point from

$$v = c \left( \frac{\Delta t}{2\tau} + 1 \right)$$

where c is the speed of the ultrasonic wave transmitted in said liquid, and

(v) scaling the velocity values obtained in (iv) to corresponding proportional color or grey scale values and displaying the resulting image.

2. A method according to claim 1 wherein a single transducer is used.

3. A method according to claim 2 wherein said transducer is a high frequency transducer which emits a frequency between 1-100 MHz.

4. A pulse-echo, immersion method for ultrasonic evaluation of a material employing a single transducer, automatic 50 scanning and digital imaging to obtain an image of a property of said material, wherein said material has a uniform thickness variation and is positioned in an immersion liquid between said transducer and an accoustic reflector, said method comprising: 55

- (I) accounting for and eliminating nonlevelness in the set-up and said material thickness variation by;
  - (a) performing a preliminary scan along both the x-and y-directions of the material to provide slant correction factors which are input into a computer to 60 account for said nonlevelness and thickness variation during the subsequent automatic scanning for said material evaluation in (ii) below;
  - (b) adjusting the time delay during said preliminary scan for any received echoes which are not centered 65 in the scan time window, so that each received echo is centered in its time window;

- (ii) automatically scanning said material at a plurality of scan points in both the x- and y-directions to receive the first and second back surface echoes and front surface echoes with and without the presence of said material between said transducer and reflector using the information obtained in (i) above, so that each echo received from each scan point during said automatic scanning is centered within its time window;
- (iii) digitizing each echo received during said automatic scanning and determining the time delay between said first two successive sample back surface echoes,  $2\tau$ , and the time delay,  $\Delta t$ , between the two different reflector front surface echoes received at each scan point during said automatic scanning and calculating the wave velocity at each said scan point from

$$v = c \left( \frac{\Delta t}{2\tau} + 1 \right)$$

where c is the speed of the ultrasonic wave transmitted in said liquid, and

(iv) scaling the velocity values obtained in (iii) to corresponding proportional color or grey scale values and displaying the resulting image.

5. A method according to claim 4 wherein said back and front surface echoes received from the first and last scan points in both the x- and y-directions during said preliminary scan determine said time base adjustments needed for each echo to be centered within the time frame for it.

6. A method according to claim 5 wherein the location of the time window during said automatic scanning for said material evaluation is automatically adjusted via computer control by using the formula:

 $W_{DT} = T_{I} + [(X_{SC})(X_{SN})(X_{SI}) + (Y_{SC})(Y_{SN})(YSI)]$ 

wherein  $W_{DT}$  is the correct delay time window at a particular scan location,  $T_I$  is the time delay at the the initial scan location,  $X_{SC}$  and  $Y_{SC}$  are the x- and y-direction slant correction factors,  $X_{SN}$  and  $Y_{SN}$  are the scan point numbers in the x- and y-directions, and  $X_{SI}$  and  $Y_{SI}$  are the x- and y-direction scan increments.

7. A method according to claim 6 wherein two scans are automatically made to obtain said first two back surface echoes and said two different reflector front surface echoes.

8. A method according to claim 7 wherein said first two back surface echoes and said reflector echo with said material present are made in said first scan.

9. A method according to claim 6 wherein three scans are automatically made to obtain said first two back surface echoes and said two different reflector front surface echoes.

10. A method according to claim 9 wherein said first two back surface echoes are received in one scan, wherein said reflector echo with said material present is made in another scan, and wherein and said reflector echo without said material present is received in yet another scan.

11. A method according to claim 9 wherein said first back surface echo is received in said first scan, wherein said second back surface echo is received in said second scan, wherein said reflector echo with said material present is made in said third scan, and wherein said reflector echo without said material present is received in said fourth scan.

12. A method according to claim 6 wherein four scans are automatically made to obtain said first two back surface echoes and said two different reflector front surface echoes.

13. An ultrasonic, pulse-echo, immersion method employing automatic scanning and digital imaging to obtain an

image of a microstructural property of a material positioned in an immersion liquid between a transducer and an acoustic reflector, said method comprising:

- (i) automatically scanning said material at least three times at a plurality of scan points in both the x- and <sup>5</sup> y-directions to receive the first and second back surface echoes and front surface echoes with and without the presence of said material between said transducer and reflector, each of said echoes received being a complete waveform and gated within a time window; <sup>10</sup>
- (ii) digitizing each echo received during said automatic scanning and determining the time delay between said first two successive sample back surface echoes,  $2\tau$  and the time delay,  $\Delta t$ , between the two different reflector front surface echoes received at each scan point during <sup>15</sup> said automatic scanning and calculating the wave velocity at each said scan point from

 $v = c \left( \frac{\Delta t}{2\tau} + 1 \right)$ 

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where c is the speed of the ultrasonic wave transmitted in said liquid, and

(iii) scaling the velocity values obtained in (ii) to corresponding proportional color or grey scale values and displaying the resulting image.

14. A method according to claim 13 wherein four scans are automatically made to obtain said first two back surface echoes and said two different reflector front surface echoes.

15. A method according to claim 14 wherein said first back surface echo is received in said first scan, wherein said second back surface echo is received in said second scan, wherein said reflector echo with said material present is made in said third scan, and wherein and said reflector echo without said material present is received in said fourth scan.

\* \* \*