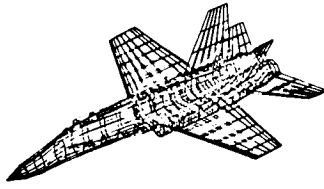


N87-11742

SENSITIVITY ANALYSIS IN COMPUTATIONAL AERODYNAMICS

Dean R. Bristow
McDonnell Aircraft Company
St. Louis, MO

SUBSONIC INVISCID PANEL METHOD



MCAERO

INPUT: GEOMETRY

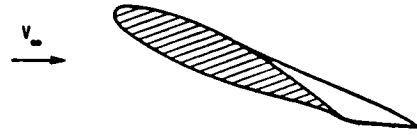
OUTPUT: PRESSURE

DMCAERO

INPUT: GEOMETRY

OUTPUT: $\frac{\partial \text{PRESSURE}}{\partial \text{GEOMETRY}}$

INTERACTING VISCOUS AND INVISCID THEORIES FOR HIGH α



INVISCID THEORY $\rightarrow \frac{\partial \text{PRESSURE}}{\partial \text{GEOMETRY}}$

VISCOUS THEORY $\rightarrow \frac{\partial \text{GEOMETRY}}{\partial \text{PRESSURE}}$

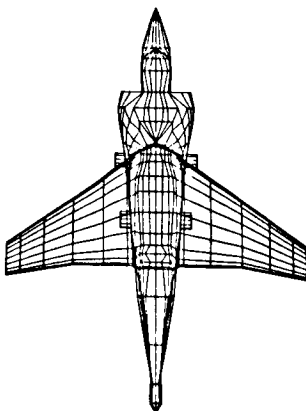


$$\left[P + \frac{\partial P}{\partial G} \Delta G \right]_{\text{INVISCID}} = \left[P + \left(\frac{\partial G}{\partial P} \right)^{-1} \Delta G \right]_{\text{VISCOUS}}$$

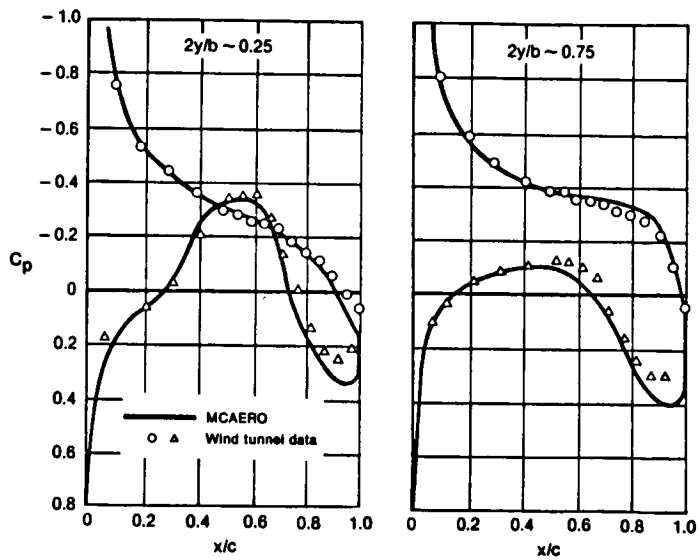
PREDICTION ACCURACY OF MCAERO

CONVENTIONAL ANALYSIS MODE

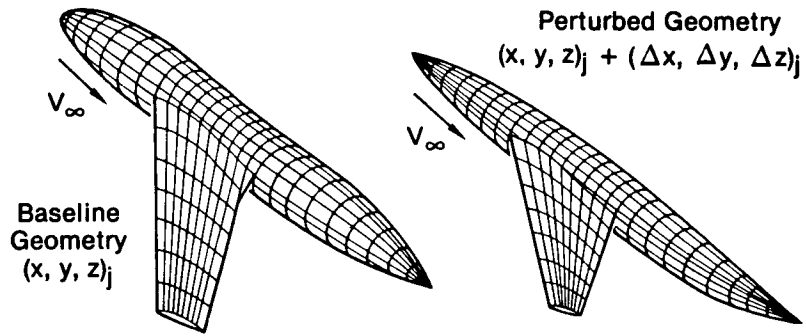
6.4° ANGLE-OF-ATTACK MACH 0.50



YAV-6B Surface Panel Modeling



PERTURBATION ANALYSIS METHOD



Objective

- Subsonic Inviscid Analysis of Multiple Geometry Perturbations at Small Additional Cost

Approach

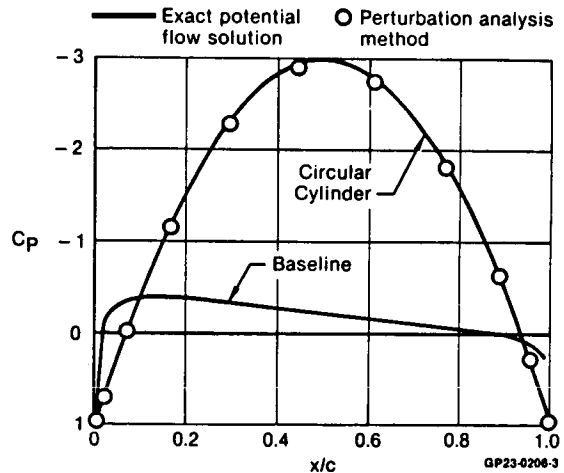
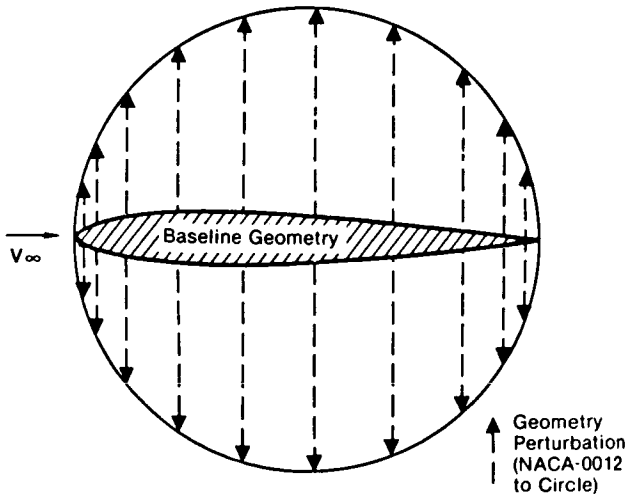
- Precalculated Baseline Matrix of Potential

$$\text{Derivatives } \left\{ \frac{\partial \phi_i}{\partial x_j}, \frac{\partial \phi_i}{\partial y_j}, \frac{\partial \phi_i}{\partial z_j} \right\}$$

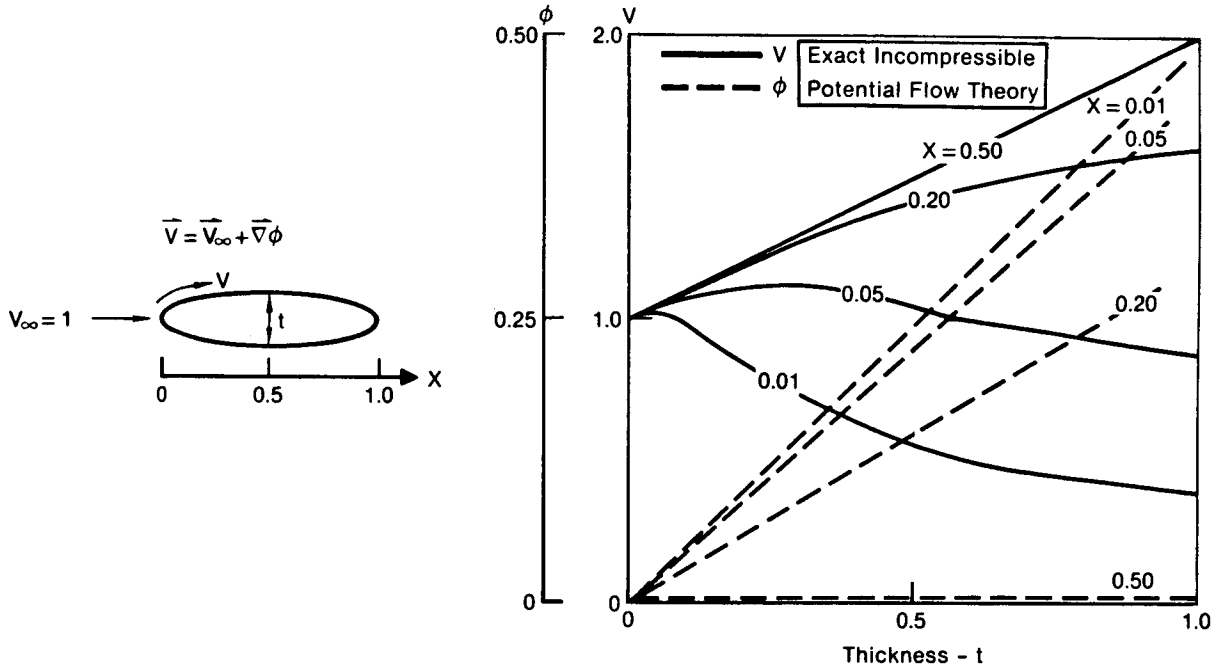
- Linear Extrapolation

$$(\phi_i + \Delta \phi_i) = \phi_i + \sum_j \left\{ \frac{\partial \phi_i}{\partial x_j} \Delta x_j + \frac{\partial \phi_i}{\partial y_j} \Delta y_j + \frac{\partial \phi_i}{\partial z_j} \Delta z_j \right\}$$

SIMPLE DEMONSTRATION OF PERTURBATION ANALYSIS METHOD 2-D INCOMPRESSIBLE FLOW



VARIATION OF FLOW PROPERTIES WITH THICKNESS ELLIPTICAL CYLINDER AT 0° INCIDENCE



Procedure for Calculating Perturbation Matrix

1. Conventional Panel Method Calculations

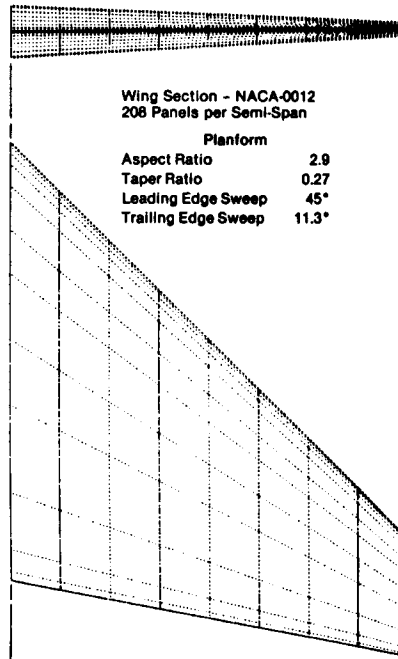
$$[A_{ij}] \cdot \phi_j = BC_i \rightarrow \phi_i = [A_{ij}]^{-1} \cdot BC_j$$

2. First-Order Expansion

$$[A_{ij}] \cdot \frac{\partial \phi_j}{\partial z_k} + \phi_j \cdot \left[\frac{\partial A_{ij}}{\partial z_k} \right] = \frac{\partial BC_i}{\partial z_k}$$

$$\frac{\partial \phi_i}{\partial z_k} = [A_{ij}]^{-1} \cdot \left\{ \frac{\partial BC_j}{\partial z_k} - \phi_l \cdot \left[\frac{\partial A_{jl}}{\partial z_k} \right] \right\}$$

**BASELINE WING PANELING
FOR PERTURBATION
ANALYSIS TEST CASES**



Wing Section - NACA-0012
208 Panels per Semi-Span

Planform

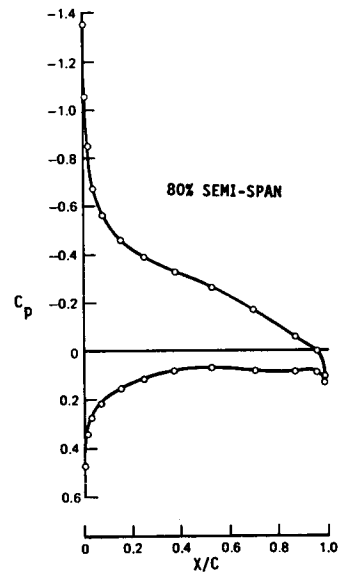
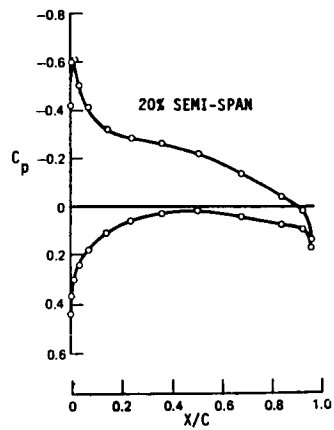
Aspect Ratio 2.9
Taper Ratio 0.27
Leading Edge Sweep 45°
Trailing Edge Sweep 11.3°

**FIGHTER WING
AT 5° ANGLE OF ATTACK**

BASELINE	PERTURBED
ROOT	ROOT
TIP	TIP

COMPUTING TIME

— CONVENTIONAL "EXACT" ANALYSIS	245 SECS
○ PERTURBATION ANALYSIS METHOD	7SECS



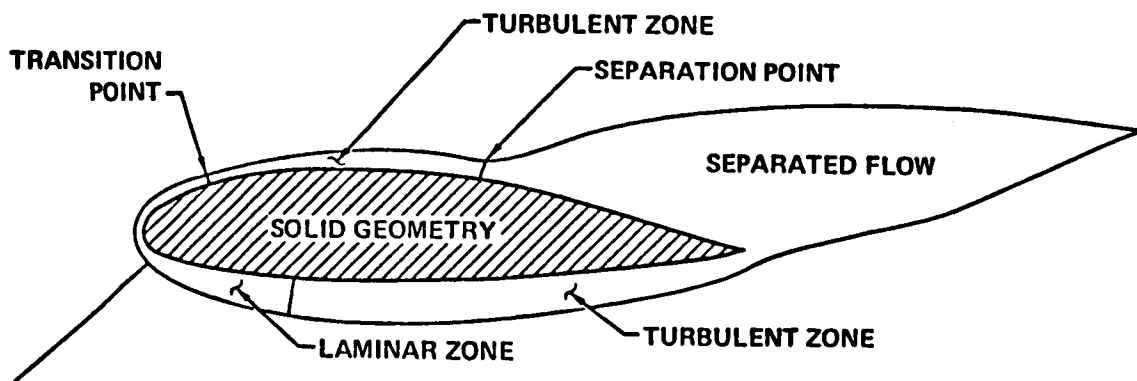
APPLICATIONS OF INVISCID SENSITIVITY MATRIX

- EFFICIENT ANALYSIS OF MULTIPLE GEOMETRY PERTURBATIONS
- PRESCRIBED PRESSURE WING DESIGN
- UNSTEADY AERODYNAMICS
- AERODYNAMIC-STRUCTURAL DESIGN OPTIMIZATION
- STRONG VISCOUS-INVISCID INTERACTIONS

TWO-DIMENSIONAL AIRFOIL VISCOUS AERODYNAMICS (LOW SPEED)

GIVEN

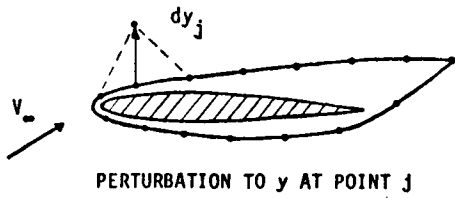
- SOLID GEOMETRY
- REYNOLDS NUMBER



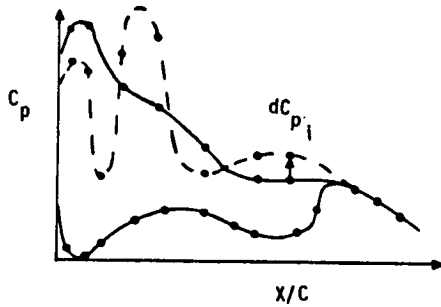
SOLUTION - GENERAL CASE

- PRESSURE DISTRIBUTION
- LIFT, DRAG, AND PITCHING MOMENT
- SEPARATION POINT
- TRANSITION POINT

CALCULATED INVISCID PRESSURE GEOMETRY SENSITIVITY MATRIX



PERTURBATION TO y AT POINT j



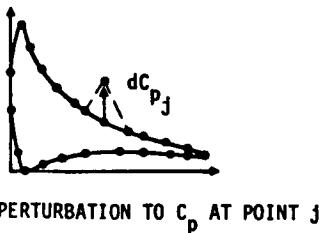
RESULTING PERTURBATION TO C_p DISTRIBUTION

$$\begin{bmatrix} & & & & j \\ & & & & | \\ & & & & | \\ & & & & | \\ & & & & | \\ & & & & | \\ i & \text{---} & \frac{\partial C_{p_i}}{\partial y_j} & \text{---} & \\ & & & & | \\ & & & & | \\ & & & & | \end{bmatrix}$$

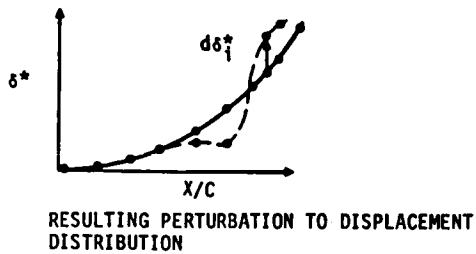
CALCULATED MATRIX

- APPROACH: ANALYTICAL EXPANSION TO MCAIR PANEL METHOD

CALCULATED VISCOUS DISPLACEMENT-PRESSURE SENSITIVITY MATRIX



PERTURBATION TO C_p AT POINT j



RESULTING PERTURBATION TO DISPLACEMENT DISTRIBUTION

$$\begin{bmatrix} & & & & j \\ & & & & | \\ & & & & | \\ & & & & | \\ & & & & | \\ & & & & | \\ i & \text{---} & \frac{\partial \delta^*_i}{\partial C_{p_j}} & \text{---} & \\ & & & & | \\ & & & & | \\ & & & & | \end{bmatrix}$$

CALCULATED MATRIX

- APPROACH: ANALYTICAL EXPANSION TO BOUNDARY LAYER METHOD

MATCHING PROCEDURE FOR VISCOUS - INVISCID INTERACTION

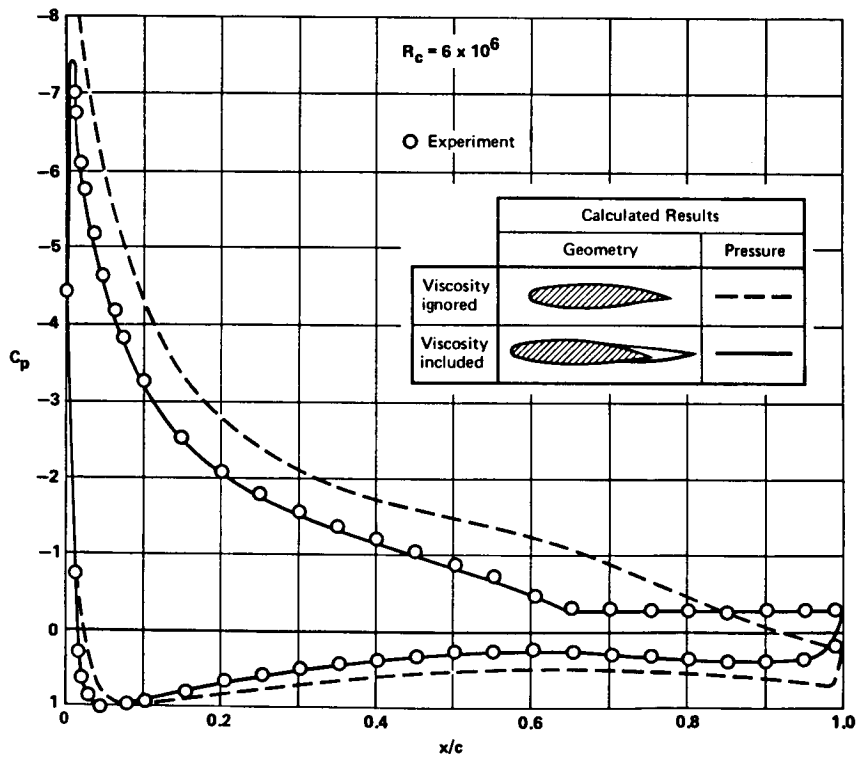
← INVISCID THEORY →

← VISCOUS THEORY →

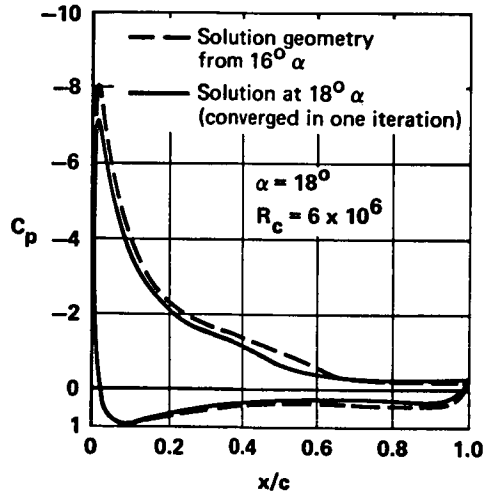
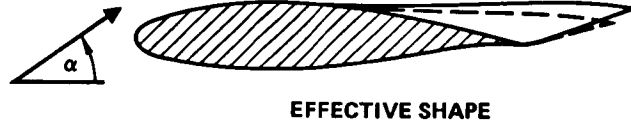
$$Y_i + \Delta Y_i = \delta_i^* + \sum_j \left(\frac{\partial \delta_i^*}{\partial C_{P_j}} \cdot \Delta C_{P_j} \right)$$

$$C_{P_i} + \sum_j \left(\frac{\partial C_{P_i}}{\partial Y_j} \cdot \Delta Y_j \right) = C_{P_i} + \Delta C_{P_i}$$

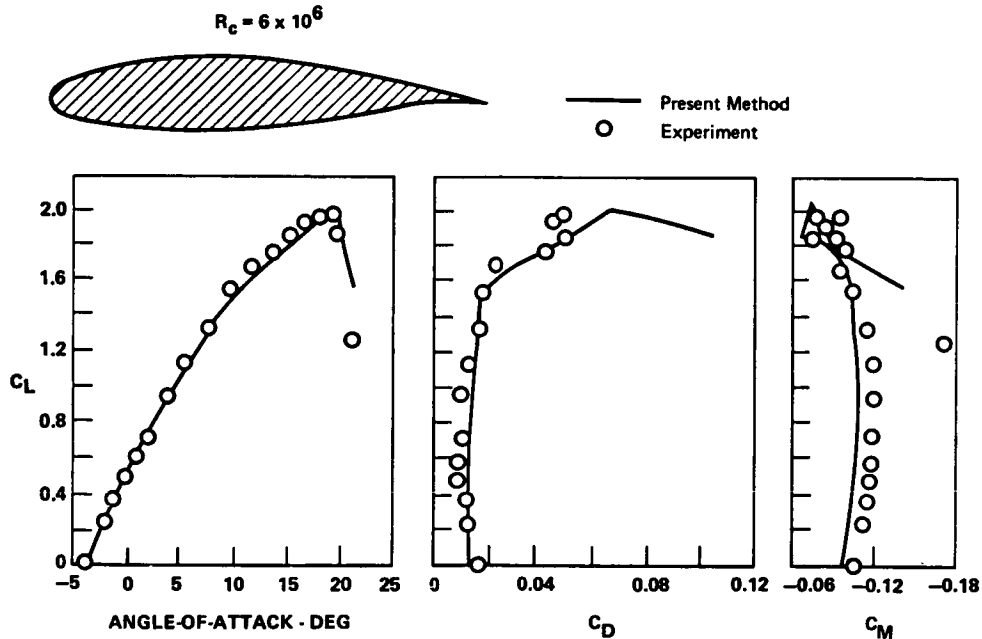
PREDICTION ACCURACY AT HIGH ANGLE-OF-ATTACK (16°α) GA(W)-1 AIRFOIL



TYPICAL CHANGE BETWEEN SUCCESSIVE ANGLES OF ATTACK



ACCURACY OF FORCE AND MOMENT PREDICTIONS NASA GA(W)-1



EFFECT OF REYNOLDS NUMBER ON AIRFOIL PERFORMANCE



MS₁- 0313 AIRFOIL

STALLED AIRFOIL
ANALYSIS PROGRAM

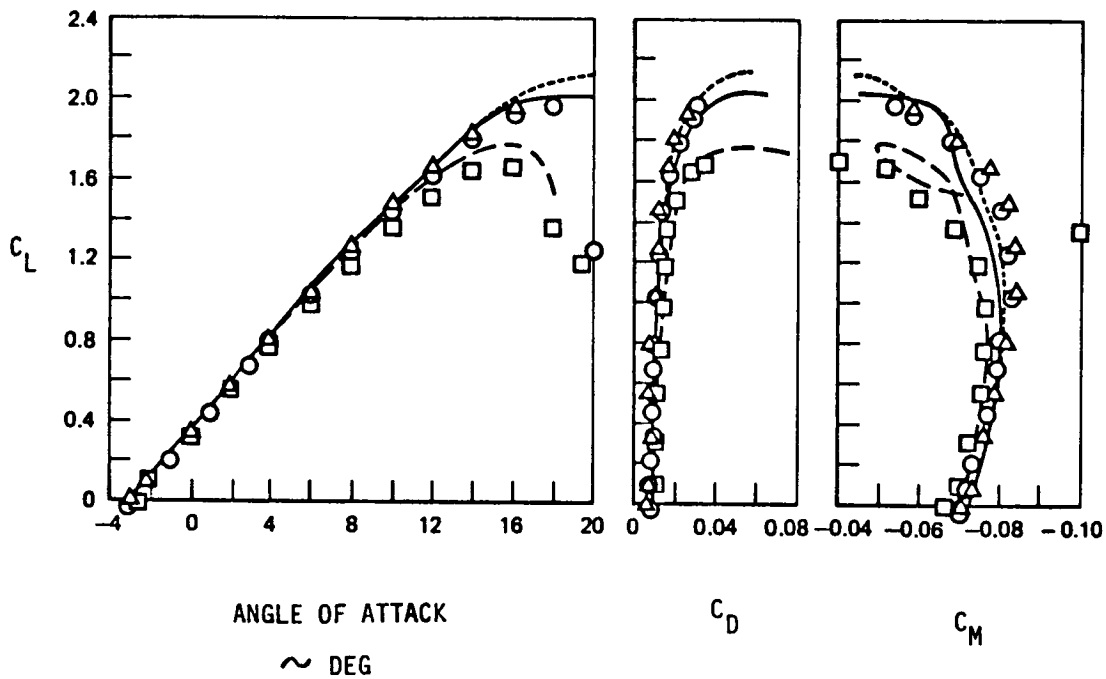
EXPERIMENT

REYNOLDS NUMBER

—
.....

□
○
△

2×10^6
 6×10^6
 9×10^6



CONCLUSIONS REGARDING SENSITIVITY ANALYSIS APPROACH

- POWERFUL EXTRAPOLATION TOOL
- APPROPRIATE FOR STRONG INTERACTION BETWEEN DISTINCT THEORIES