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[54] SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR

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- [73] Assignce: The United States of America as represented by the Administrator of the National Aeronautics and Space Administration, Washington, D.C.
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- 358/104; 358/109; 434/4; 434/38 [58] Field of Search 434/4, 38; 356/1, 4; 358/109, 104

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[57] ABSTRACT

The object of the invention is to provide an improved laser altimeter for a flight simulator which will allow measurement of the height of the simulator probe above the terrain directly below the probe tip.

A laser beam 22 is directed from the probe 13 at an angle θ to the horizontal to produce a beam spot 20 on the terrain. The angle θ that the laser beam 22 makes with the horizontal is varied so as to bring the beam spot into coincidence with a plumb line 18 coaxial with the longitudinal axis of the probe 13. A television altimeter camera 30 observes the beam spot and has a raster line aligned with the plumb line 18. Spot detector circuit 26 coupled to the output of the TV camera monitors the position of the beam spot relative to the plumb line 18. An error signal is produced by computer 28 driving, via a servo motor 23, the laser beam optics so as to cause the beam spot to come into coincidence with the plumb line 18. At coincidence, computer 28 looks up in a table the altitude of the probe for the given angle θ and reads out the altitude to an altimeter readout 31.

11 Claims, 9 Drawing Figures







JUMP TO SUBROUTINE "MOTOR MOVEMENT" 4,391,514





Fig_7







5

15

camera.

SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR

ORIGIN OF THE INVENTION

The invention described herein was made by an employee of the U.S. Government and may be manufactured and used by or for the Government for Governmental purposes without the payment of any royalties thereon or therefor. 10

TECHNICAL FIELD

The technical field of the present invention relates in general to laser altimeters for flight simulators.

BACKGROUND ART

Heretofore a laser altimeter system has been proposed for determining the altitude of a flight simulation probe over a model board. Such a prior art system is disclosed in an article entitled, "Probe Protection In 20 Camera/Model Visual Systems" appearing in the Proceedings of the 1980 Summer Computer Simulation Conference, Olympic Hotel, Seattle, Wash., Aug. 25-27, 1980.

In this system, a laser beam is directed vertically from 25 the flight simulator TV camera probe along a side of the probe to strike a point on the model board radially displaced from a point directly below the center line of the probe, hereafter referred to as a plumb line. The incident beam produces a beam spot on the terrain of 30 the model which is thence imaged onto a linear array sensor. As the height of the probe is varied, while holding the probe otherwise stationary, from a point of minimum altitude to a point of maximum altitude the beam spot traverses a vertical imaginary line focused 35 onto the linear array sensor. The position of the imaged beam spot along the linear array sensor is representative of altitude. A major problem with this system is that the altitude being measured is not the altitude of the probe (altitude measured along the plumb line) but rather the 40 altitude of the laser beam source which is displaced horizontally from the probe. The actual distance between the plumb line and the laser beam must be multiplied by the scale of the model. Error will be produced whenever the terrain elevation at the plumb line differs 45 from the terrain elevation at the laser beam. For example, an appreciable error would exist if the plumb line was over a depression and the laser beam impinged on a hill, mountain or tall building.

Thus, it is desirable to obtain a probe height sensor $_{50}$ which more accurately measures the height of the probe above the terrain directly below the probe.

[STATEMENT OF INVENTION]

DISCLOSURE OF INVENTION

In the present invention, pilot altitude as represented by the distance h is measured by a technique that locates the point of intersection of the plumb line and the terrain (hereinafter known as the convergence point). A laser beam is directed from the probe at an angle to the 60 plumb line and coaxial with the longitudinal axis of the probe. The point where the beam strikes the terrain is varied by changing the angle of the laser beam relative to the longitudinal axis of the probe so that the beam spot is brought to a point on the longitudinal axis of the 65 probe where it intersects the terrain. A TV camera, carried from the probe views the region below the probe and has a predetermined linear detection region,

such as a raster line, coaxially aligned with the image of the plumb line. A detection circuit receives the output of the TV camera and determines the position of the laser dot in the raster. Using this information, a computer determines the position of the beam spot relative to the plumb line. A resolver coupled to the laser beam angle control reads out the angular position θ of the laser beam to a computer. The computer looks up the height of the probe in a look up table for the angle θ of the laser beam. The measured height is then read out to an altimeter and to a flight simulation monitor station. If the laser dot does not reside on the plumb line, a computer directs a stepper motor to relocate the beam such that the dot will reside on the plumb line. If the operative laser beam is unable to be relocated at the convergence point because it is blocked by a terrain obstruction, an alternative laser beam at a different angle around the probe is selected. Also, if the TV camera's

BRIEF DESCRIPTION OF THE DRAWINGS

view is blocked the computer selects an alternative TV

FIG. 1 is a schematic perspective view, partly in block diagram form, of an altimeter system for a flight simulator incorporating features of the present invention.

FIG. 2 is a longitudinal sectional view of the flight simulator probe and model board,

FIG. 3 is a schematic transverse sectional view, partly in block diagram form, of a portion of the structure of FIG. 2 taken along line 3-3 in the direction of the arrows.

FIG. 4 is a schematic side elevational view of the TV camera optics for beam spot detection,

FIG. 5 is a schematic block diagram of a laser altimeter system incorporating features of the present invention,

FIG. 6 is a logic flow diagram for the computer program for the system of the present invention, and

FIGS. 7, 8, and 9 are logic flow diagrams for subroutines of the computer program flow diagram depicted in FIG. 6.

DETAILED DESCRIPTION OF THE INVENTION

Referring now to FIG. 1 there is shown a laser altimeter system 11 for a flight simulator and incorporating features of the present invention. The flight simulator system includes a model board 12 comprising a scale model of terrain over which simulated flights are to be conducted. The pilot sits in a cockpit, not shown, and views a television screen displaying a view seen through a probe 13 movable with respect to the terrain of the model board 12 in accordance with flight control 55 commands given by the pilot over the aircraft controls. The probe 13 is carried from a gantry, not shown, disposed over the terrain of the model board 12. Relative movement in three orthogonal directions, X, Y, and Z is obtained between the probe and the model board. In some embodiments, the gantry moves relative to a stationary model board to provide movement in all three orthogonal directions, whereas, in other embodiments the model board is moved relative to the probe to simulate flight.

Referring now to FIG. 2, the optical system for the probe 13 is shown in greater detail. More particularly, the probe 13 includes an elongated barrel portion 14

projecting in the Z direction toward the model board. At the end or tip of the probe 15 there is a mirror 16 which projects a visual scene corresponding to that which would be seen by the pilot, up along the longitudinal axis of the probe barrel 14 to a TV camera 17. The 5 scene picked up by the TV camera is then transmitted to and displayed on a cathode ray tube outside the windshield of the simulated aircraft. The altitude h of the simulated aircraft is that scale distance from the mirror 16 is taken along a plumb line 18 for the modeled terrain 10 to a point of intersection of the plumb line with the terrain at 19.

Referring again to FIG. 1, a laser 21 is carried from a frame coupled to and movable with the probe 13. The laser directs a pencil-like beam 22 of monochromatic 15 nondivergent radiation of visible wavelength onto the terrain below the probe 13 having been deflected by pitchable mirror 35 to produce a beam spot 20 on the terrain. A servo motor 23 is coupled to the mirror 35 in such a way as to vary the angle θ that the laser beam 20 makes to the horizontal or XY plane of the model board 12. The laser beam is rotatable about an axis of revolution parallel to the horizontal XY plane and such beam being rotatable in a plane normal to said axis of revolution, such plane also containing the plumb line 18.

An altimeter TV camera optical system 30 is also carried from the probe frame. The altimeter TV camera system 30 includes some optics, not shown, and views the region of the model board directly below the probe 13. The TV camera optics are such that the point of intersection of plumb line 18 with the model board surface is within the view of the TV camera system 30 for all values of altitude h from minimum to maximum above the surface of the model board 12. Which includes the plumb line 18. A θ angle resolver 29 is coupled to each of the motor-mirror drive trains for giving an output determinative of the angle θ . The other half of the output of the first beam splitting mirror 33 is directed downward along the Z axis to a 45° mirror, not shown, which thence directs the beam parallel to the Y axis to a second 45° mirror 37 and thence parallel to the X axis to another 45° mirror 38 which thence directs the beam through a second beam

A single raster line is made coincident with the plumb 35 line 18 through appropriate mechanical alignment. An output from the altimeter TV camera 30 goes to a spot detector circuit 26 of the type similar to that disclosed in U.S. Pat. No. 3,320,360 issued May 16, 1967 entitled, "Television Tracking Error Detector", for determina- 40 tion of the location of the beam spot 20 relative to the plumb line 18.

The output of spot detector 26 is fed to a computer 28. This output consists of the raster line number and displacement along the raster line of all of the detected 45 elements of the laser spot 20. The computer determines the location of the center of the laser spot 20 in the raster of the altimeter TV camera system 30. To be coincident with the end of the plumb line 18, the laser spot 20 must lie somewhere along the altimeter TV 50 camera system raster line which was made coincident with the plumb line 18. The computer 28 compares the raster line number of the center of the laser spot 20 with the raster line number of the raster line which is coincident with the plumb line 18. If the two are equal then 55 the laser spot 20 must be located on the terrain at the end of plumb line 18 where it intersects the terrain. The exact length of plumb line 18 may then be determined. If the two are not equal, the laser spot 20 is not located at the end of plumb line 18 where it intersects the ter- 60 rain. An error signal is generated which causes servo driver 27 to reposition laser spot 20 until the two raster line numbers are equal. The computer 28 also receives the angle θ input from a resolver 29 mechanically coupled to the laser beam deflection system so that at the 65 point of convergence of the beam spot 20 with the point of entry of the plumb line 18 into the terrain, the computer reads the θ angle and looks up, in its look up table,

the value of altitude corresponding to the given values of altitude for various values of θ as the probe is moved from a position of minimum altitude to maximum altitude over the model board.

Referring now to FIG. 3 there is shown the optical distribution system for deriving the various laser beams and for televising the beam spot 20 on the model board. The laser 21 is affixed to a probe frame member 32, and directs its output beam through first and second beam splitters 33 and 34. Beam splitter 33 is arranged to direct the reflected portion of the beam downward along the Z axis whereas the other half of the beam passes through the first beam splitter 33, to the second beam splitter 34 which serves to further divide the beam into a first beam directed parallel to the X axis and a second beam of equal amplitude directed along the Y axis. Each of the beams outputted from the second beam splitter 34 is directed onto a 45° angle mirror 35 for bending the respective beam by 90° toward the plumb line 18. Each of the mirrors is driven from a stepping servo motor 23 about respective axes of revolution. In one instance the axis of revolution is parallel to the X axis and in the other to the Y axis and both are in the XY plane so as to cause the beams to be rotated within respective planes which are perpendicular to the XY plane and each of which includes the plumb line 18. A θ angle resolver 29 is coupled to each of the motor-mirror drive trains for giving an output determinative of the angle θ .

The other half of the output of the first beam splitting 45° mirror, not shown, which thence directs the beam parallel to the Y axis to a second 45° mirror 37 and thence parallel to the X axis to another 45° mirror 38 which thence directs the beam through a second beam splitting mirror 39 for splitting the beam into two equal components, one parallel to the Y axis and the other parallel to the X axis. The beams are then reflected off of respective 45° mirrors 35 driven from the stepping motors 23 which include resolvers 29. Thus, the second beam produces a pair of beams directed onto the model board 12 which are orthogonal to each other and which are 180° displaced from the first pair of beams. The beams are rotatable in the XZ and YZ planes, such planes each including the plumb line 18. The respective mirrors 35 are positioned such that their output beams will intersect the plumb line 18 at the point that the plumb line 18 intersects the surface of the model 12.

The orthogonality between each of the laser beams is not a requirement. For example, it could be three beams at 120° angular spacing from each other with the camera optics similarly angularly separated from each other by 120° and being spaced at 60° angles from each of the respective beams.

A pair of altimeter TV camera optics are carried from the probe frame structure 32 and are positioned at 180° intervals about an axis of revolution coaxial with the plumb line 18 and preferably at 45° angular spacing from the ZX or ZY planes but on the XY plane containing the respective laser beams. This positioning of the altimeter TV camera optics 30 permits viewing of the respective beam spot 20 at the plumb line 18, regardless of various buildings, hills, or trees or other obstructions in the terrain of the model board 12. In other words there is some combination of laser beam 22 and altimeter TV camera optics 30 which will permit viewing of the beam spot 20 at the plumb line 18 regardless of the obstructions represented by the terrain of the model 12, with the exception of a well or deep ravine. The laser

beams 22 which are not in use, i.e., three of the four are "parked" by rotating their respective mirrors 35 so as to project the beam spot 20 onto the probe body 41 or 42.

Referring now to FIG. 4 there is shown one of the optical systems 30 for each of the TV altimeter cameras. 5 More particularly, a condensing lens 45 receives the light emanating from the beam spot 20 and focuses the image of the beam spot onto the entrance plane 46 of a light pipe 47 such as a fiber optics bundle. The bundle 47 may have a suitable length as of 3-5 feet to bring the 10image of the beam spot 20 to a convenient location of the TV camera 50, typically somewhere on the gantry. Another lens 48 receives the beam spot image at the output face of the light pipe 47 and converts the image into a beam of parallel light 49 which is thence directed 15 through a narrow pass filter 51 having a pass band at the wavelength of the laser beam 22 so as to filter out undesired background illumination. The filtered beam is thence fed to a condensing lens 52 which focuses the 20 beam spot image onto the receiving face of the TV camera 50. The input face of the light pipe 46 is cut at the Scheimpflug angle, as described in U.S. Pat. No. 751,347 issued Feb. 2, 1904, so that the plumb line 18 of the probe is maintained in focus on the input face of the 25 TV camera 50.

Referring now to FIG. 5 there is shown, in block diagram form, the laser altimeter system 11 of the present invention. The output beam 22 of the laser 21 is fed through an optical distribution system 40 as shown in 30 FIG. 3. One of the output beams 22 is selected and directed onto the terrain of the model 12 under the probe 14. The beam spot image 20 is picked up by both of the camera optical systems 30. Their output video signals are fed to a multiplexer 55. The computer 28 35 selects one or the other of the camera optic systems 30

and feeds a control signal to the multiplexer 55 for controlling which one of the camera optic systems 30 is utilized. The output of the multiplexer 55 is fed to the spot detector 26 which tracks the image of the beam spot 20 relative to the plumb line 18 which is inputted to the computer 28 and thence outputted to the motor driver 27 and respective motor 23. In a typical example, the computer 28 comprises a Motorola 6800 Exorcisor. The resolver 29 outputs the angle θ for the selected beam 22 to an analog-to-digital converter in the computer 28. When the computer 28 detects zero error, i.e., the beam spot is at the plumb line 18, the computer 28 by its software looks up in a table the altitude corresponding to the respective angle θ and outputs that data via a digital-to-analog converter to a driver 56 which thence inputs it to the altimeters or other read out devices 31.

Referring now to FIG. 6, there is shown the logic flow chart for the software program for the computer 28. FIGS. 7-9 depict the logic flow charts for program subroutines, namely, MOTOR MOVEMENT, DATA FETCH, and SCAN, respectively. The program listing is shown in Appendix I, below.

One of the advantages of the laser altimeter system of the present invention for a flight simulator includes detecting the altitude of the probe above a position directly below the probe as opposed to a position displaced in the horizontal plane from the probe. This makes the concept inherently accurate. Secondly, the provision of angularly displaced laser beams 22 and camera optics 30 allows reading of the altitude regardless of the obstructions represented by features in the terrain which might otherwise obstruct viewing of the beam spot.

APPENDIX I

00010	00001					*****	******	*******	*******				
00020	00002					ж	* LASER *						
00030	00003					ж	* OPERATING *						
00040	00004					ж	* SYSTEM >						
00050	08005					*****	****	******	*************************************				
00060	00006						NAM	LASOP					
00070	00007A	5000					ORG	\$5000					
08060	00008						OPT	CRE, L, P	=43, U, LLE=90				
00090	00009A	5000		019F	A	CONV	FDB	\$019F	CONVERGENT RASTER LINE				
00100	00010A	5002		04	A	SMMV	FCB	\$4	SMALL MVT THRESHOLD				
00110	00011A	5003		80	Α	MDMV	FCB	\$8	MEDIUM MVT THRESHOLD				
09120	00012A	5004		10	A	LCmV	FCB	\$10	LARGE MYT THRESHOLD				
00130	00013A	5005		03CF	A	BIAS	FDB	\$03CF	BIAS FOR ALTIM. ZERO				
00140	00014A	500Z	ZF	任F 41	A	•	CLR	\$EF41	SET UP COLLECT PIA'S				
00150	000156	500A	ΖF	EF 43	A		CL.R	\$EF43					
00160	000166	500D	. 1 .	EF 54	Α		CLR	非任何等于					
00170	0001ZA	5010	7F	EF53	- A		CLR	\$EF53					
00180	00018A	5013	212	EF40	Ĥ	•	CLR	\$6.1740					
00190	000196	5013	7F	EF42	A		CLR	\$EF42	,				
00200	A02000	5019	ZF	EF50	A		CL.F	\$EF 50	*				
00210	00021A	501C	88	90	A		LDAA	##9C					
00220	00022A	501E	67	1992	é		STAA	#EF52	·•.				
00230	00023A	5621	83	04	- 6		LDAA	小					
00240	00024A	5023	67	EF 53	iA.		STAA	\$6753					
0.0250	000256	5026	£27	EE 43	A		STAA	\$EF43					
00260	000266	5029	2F	EF 52	_ A		, CLR	\$EF52	STOP HARDWARE SYSTEM				
00270	0002ZA	502C	£ 6	0 $%$	` ∩ ·		LDAA	1 C					
00230	00020A	5020	62	EF 41	Â		STAA	\$EE 11					
00290	00029A	5031	EZ.	EF 51	Δ		STAA	\$CE51					
00300	00030A	5034	Đ3	EFS0	Α		LDAA	\$EE 50	CLR INTERRUPT				
00310	00031A	5032	ESS	EF52	A	FLAG	LDAA	\$EF52	INITIALIZE EVENT COUNTER				
00320	00032A	503A	84	20	Ĥ		ANDA	非事态:0					
00338	000336	140/30	27	0A 50	43		BEQ	OUTLOP	ERREFER EMPITY?				
00340	000346	50 BE	05	2.0	Α		LDAA	4410	RAISE READ ENABLE				
00350	00835A	5040	6. ⁷	EFSZ	Δ		STAA	\$EE52					

00360	00036A	5043	2F	EF 52 - A		CLR	\$EF52	
00370	00002A	5043	20	EF 5032	251 1001 2540-	BRA	FLAC	RETURN, INITIAL. DONE?
00200	00030A	5048 ©nac	74° 2100	500A A	ourra _b	CLR	STARLE	LINE STABILITY CHUCK
00370	000328	5.020	2.17	00-07 M		CLIX CLID	AD FIELD I I I I I I I I I I I I I I I I I I I	AF UP INU LUUT PRASES.5
00410	000436	5051	83	EE A		1000 1000	- 中に作之 』 - 遺虫国作	CARGA FARMA ZES PHOTORS CO.M.
00420	00042A	5053	192	EFZ0 A		STAA	\$FF70	
06430	00043A	5054	83	06 Å		LDAA	# 6	
00440	000446	5658	E:Z	FF21 A		STAA	\$EF71	
00450	000355	5050	ED.	5062 6	co	JSR	COLECT	GO GET DATA FROM VIDEO
00460	00046A	5058	DD	525A A	0.0	JSR	DIST	GO CALC ALTITUDE
00470	00047A	50.61	FE	5306 A		LDX	DOT	
00480	00048A	50.64	27	0A 5070		BEQ	STAL	IS DOT (NOT) THERE?
00490	00049A	5066	76	5339 A		CLR	STB1	IF DOT/ CLR # NO DOTS
00500	00050A	5069	3C	0001 A	FILTER	CPX	#:1	·
00510	00051A	506C	27	ED 5050		EEQ	GO	SYSTEM ERROR, TRY AGAIN
00520	00052A	506E	20	14 5084		BRA	RUN	RUN SYSTEM WITH GOUD DUT
00530	00053A	5020	-86	01 A	STAL		48-3. Common	# UP CUNSER NU DUT PASS
0.05240	0000040	- 078772 - 600 Million	130	0337 A		DUDA DCO	00000 01001	NO DOT TUTCES
00550	0000000	5025	20	- 00 0070 - 6230 (A		TNC	STE1	ACK ONE NO DOT PASS
00520	000576	5076	20	DE SASE		ERA	GO	
00580	00058A	507C	76	5339 A	SEND	CLR	STE1	CLR # OF NO DOT PASSES
00590	00059A	507F	ВÐ	5179 A		JSR	HUNT	GO HUNT FOR MISSING DOT
00600	00060A	5082	20	DZ 5058		BRA	GO	RETURN AND TRY AGAIN
08610	00061A	5084	÷С	5000 A	RUN	CPX	CONV	RASTER LINE STAB. TEST
00620	00032A	5087	27	0C 5095		BEQ	SET1	CONVERGENT?
00630	00063A	5082	86	-01. A		LDAA	-10:1.	PUT STABLE BIT HERE
00640	00034A	500B	60	533A A		SUBA	STABLE	and and and and the statement and and by the same
00650	00035A	508E	27	00 5090		BEQ	DRIVE	T2 DUI NUT CUNV?
00660	000666	5020	70	533A A			STABLE CO	BUN NUT LUNV PHOO DETLIDN AND TOY ACATM
000/0	0000070	- 3073 - Enor	20	- US 0000 - COOK - A	orna.	CLD	OTADE E	KETOKIA MIAD TIKT MUMLIN
00000	0000000	- 0020 - 6000	i z r Tors	- JOOH - H - S2SA - A	OL. F.L	JSB	DTST	CALC DIST FOR ALTIM
00200	0000204	5020	20	BE SOSE	•	ERA	60	RETURN AND PROCESS AGAIN
00710	000716	5020	80	5200 A	DRIVE	JSR	MOVE	GO TO MIRROR ADJUST SR.
00720	00072A	50A0	20	89 5058		BRA	GO .	RETURN AND REPROCESS
00730	000736	5062	7F	5359 A	COLECT	CLR	LDATA	INITIALIZE DATA REGIS
00740	00074A	50A5	2F	535A A		CLR	LDATA+1	·
00750	00075A	5068	ZE.	5325 A		CLR	DDATA	
00760	00076A	50AB	215	5396 A		CLR	DDATA+1	
007/0	000776	CUAL:	ZI:	- 5301 - A		CLK	CUUDRELL MERMON	
00230	-000286 -000296	- 006a - 96684	26	- 52DS A		CLR	COUNT?	
00800	00080A	5032	1:6	EE50 A		LDAA	\$EF50	CLR H-WARE INTERRUPT
00810	00081A	5006	86	80 6		LDAA	4480	
00820	00082A	50DC	82	EF52 A		STAA	\$EF52	START HARDRARE RUNNING
00830	00063A	508F	86	EFE. A		LDAA	北部門門	LOOP TIMER
00840	00084A	50C1	Fð	CES1 A	JMP2	LDAB	第世紀51	CHECK FOR DOT INTERRUPT
00850	0000SA	. <u>5</u> 004	213	39 SOFF		BMI	READ	IF SEE DOT, READ DATA
00850	00086A	50C3	E.E.	53D3 A		STX	DUMMY	PAD LOOP TIME
00870	00087A	- 50C9	1.1.	-5303 A		STX	DUMMY	
08880	000830	- 139UU - ©0041	11	- 5303 A		SPX	DUMMY	
00000	0000074	- 500r - 5002	1715 1717	- 5505 H - 5909 A		CTV	DUMMY	
00910	00091A	5005	i i pr	-5303 A		STX	DUMMY	
00920	00092A	5008	F F	53D3 A		STX	DUMMY	
00530	00093A	50DB	ГF.	5003 A		STX	DUMMY	
00940	000946	50DE	E la	53D3 A		ŞTX	DUMMY	
00250	0.0.095A	5001	le te	53D3 A		STX	DUMMY	
00960	00096A	50E4	I.I.	- <u>5003</u> A		STX	DUMMY	
00970	000976	- 30EZ	- Pri Pri Li Pri Li	53D3 A		SIX	DUMMY	
00700	-00070H -866QQA	- 00000 - 15600	ere:	- 0-003 - A - 5-003 - A		51X 6177	DUPPT	
01000	000776	-50E0 -50E0	20	- 5203 H		TNC	COUNT1	
01010	00101A	5013	-131	-53D1 A		CMPA	COUNT1	\$FF 100PS?
01020	00102A	50115	26	C9 50C1		ENE	JMP2	RETURN AND TRY AGAIN
01030	00103A	50F8	ÛĔ	-0000 A		LDX	# Ü	
01040	001046	50FB	- E.F.	-53D& A		STX	DOT	NO DOT FOUND
01050	00105A	-50FE	39			RTS		RETURN TO MAIN PROG
01069	00103A	-500F	- 71°	EF52 A	READ	CLR	\$EF52	STOP HARDWARE SYSTEM
010/0	-00107A	- 01.02 - 84.00	- 1:16 - 0:4	ntroz A ⊇n	CHECK	LUAA	webrook webrook	CALIFICARY ENDERING AND DESCRIPTION
01000	-00100A -00100A	- 0100 - 5462	- 64 - 77	- 20		ENRUAR ENECO	重率でひ 1375に243-05	ALL DATA THE CET CHTD
01100	001106	5109	- 84	ుణ చూడు 10 ది		LDAA	##10	ENABLE READ FNAFLE
01110	001114	5108	-67	EF52 A		STAA	¢EF52	where it is a many way is a struct that the base of the backet
01120	001126	51.0E	68	EF 40 A		LDAA	\$CF40	CET WIDTH AND UNPACK
01130	00113A	5111	16			TAB	•	SAVE FOR FUTURE UNPACKIN
01140	001146	5112	84	F0 A		ANDA	重步行力	MASK OTHER INFO
01150	001156	5114	44			LSRA		

8

ATA REGIS NTERRUPT RE RUNNANG T INTERRUPT ATAG DATA Ξ _00PS RY AGAIN · . IN PROG E SYSTEM NOT EMPTÝ GET CNTR ENABLE D UNPACK URE UNPACKING NFO

			્રપ્ર)					10
01130	00116A	5115	44				LSRA		
01170	00117A	5116	44				LSRA		servers and search and the servers and the
01180	00118A	5117	81	03.	- fi 		CMPA	#3 102のAD	MINIMUM MIRAH
01190	00119A	5119	21	23 51	36		BLE.	DISAB	The LOD Shutter Strength
01200	001204	5110	2D	53D5	A		TST	COUNTZ	FIRSTUGUUD WILLING
01210	00121A	5116	26	18 51	38		ENR:	dine to	TTEET COOD I TNE
01220	001220	5120	50	E.F. 922	Ĥ		COMA	140.11 1120	PURGI GOOD CLINE
01230	001230	0123 0123	43	ECOR.A		MADIZO	CURIN	1.DATA41	STORE USE OF RASTER LINE
01290	001286	0129	1002	0.0.014	1-1	LU-BACAY	TEA	6.67Pt 1 P1 + 35	
012300	001246	5129	42				COMA		
01220	001204	5129	84	ñ1	A		ANDA	#1	
01280	001286	5128	BZ.	5552	A		STAA	LDATA	STORE MSB OF RASTER LINE
01290	00129A	512E	06	EF SO	A		LDAA	\$CF 50	GET DISPLACEMENT DATA
01300	001304	5131	E:Z	5396	6	MARICO	STAA	DDATA+1	STORE LSB OF DISPLACEMENT
01310	00131A	5134	17		• •		TBA		
01320	00102A	5135	84	0E.	A		ANDA	#\$0E	
01330	00133A	5137	44				LSRA		
01340	00134A	5138	ΒZ	5395	A		STAA	DDATA	POUNT & OF COOR NOTE
01350	00135A	513B	ZC	5305	Ą	JMP-4	INC	COUNT2	CUUNT T UP GUUD DUTS
01360	00136A	513E	76	EF52	A	DISAB	CLR	争した 32 のしののビ	DIDHELL KEND LANDLE
01320	00137A	5141	20	EF DI	102	0000000	1044	CODUTS	. OF LINES WITH A DOT
01330	0013366	0143	60	5305	F1	DULTOR	CTAA	UNCNT	
01320	0013076	. S140	642	5252	5		LDX	LDATA	GET FIRST LINE #
01410	00141A	5140	r r	5308	A		STX	LINE	
01420	00142A	514F	FE	5395	A		LDX	DDATA	GET FIRST DISPLACEMENT
01430	00143A	5152	FF	530A	A		STX	MAX	
01440	00199A	5155	74	53DC	é		LSR	NDCNT	DIV BY TWO (FOR CENTER)
01450	00145A	5158	66	5309	- A		LDAA	LINE+1	D.P. ADD FUR DOT CENTER
01360	00146A	5150	ER	5300	- 6		9009 9100	DOTe1	STORF LSB
014/0	0014/0	00.045 19474	67	6.000	- 11			I TNF	
01400	00140A	5161	00	0.0	۲۱ ۵		ADCA	10	MSB ADD
01500	0011776	5172	67	5304	A		STAA	DOT	MSB STORE
01510	001516	5169	86	5007	A		LDAA	DOT+1	~
01520	00152A	5160	84	01	A		ANDA	#1	TEST FOR ODD (NESS)
01530	00153A	516E	27	01 5	171		BEQ	ADD1	ADD ONE IF EVEN
01540	00154A	5170	-39				RTS		RETURN TO MAIN PRUGRAM
01550	00155A	5171	T E	5306	A	ADD1.	LDX	DOT	ADD UNE TO PIARE ODD
01560	001566	5174	08		~ .	-	XNL	007	
01570	0030ZA	- D170 - S170	- F P - 200	0008	64		RTS	001	RETURN TO MAIN PROGRAM
01000	001000	5170		0.056	A	HUNT	LDX	* \$FF	
01600	0016076	5170	FF	530F	A		STX	INFIN	MIRROR AT INFINITE DIST
01610	00161A	517F	CE.	FB54	≙		LDX	#\$FD54	
01620	00162A	5182	F F	5300	6		STX	ZERO	MIRROR AT ZERO DISLANCE
01630	00163A	5185	ЕÐ	50A2	Ĥ	M2ERO	JSR	COLECT	MOVE MIRRUR IN ZERN
01640	001640	15188	- F 6.	-5306	í.		LDX	DUT	DETHEN TO MATN
01650	00165A	5188	26	72.5	181		LDAA	45508	RETURN TO TRAFT
01660	001620	0180	0.3	rrua	1-1		NOP	441 04.2	
010/0	- 00162M - 00162M	- S191	64	FE08	ΪA		LDX	\$EF08	CHECK MIRROR POSITION
01490	001696	5194	- In In	50F1	A		STX	LOCA	STORE MIRROF LOCATION
01700	00170A	5197	E-6	50E2	A		1.DAA	L0004+1	D P. SUBTR-DIFF TO ZERO
01710	00171A	51?A	80	53DE	A		SUPA	ZERO (1	LSP SUPTRACT
01720	00172A	512D	E:2	53E4	Ĥ		STAA	• DTEF + 1	L'SU RESULT STORE
01730	00173A	51A0	86	53E1	A		LDAA	LOCA	· · · · · · · · · · · · · · · · · · ·
01740	00174A	51A3	82	5300	A		SECA	ZERO	MSB SUBTRACT
01750	00175A	51A6	67	53E3	A		STAA	DIFF	STORE MSB RESULT
01760	00176A	51A9	FE	53E3	A		LDX	DTFF	TELT ZERO MOUE TO INFIN
01//0	001//A	51AC	2.1	11 5	166		CLD	45°6°70	OTHERWISE MOVE TO ZERO
01780	001786	0101 - 8104	. 71*	EFZU	F1		NOP	+c.r70	OTTERVA,OL TOTE TE
01220	001299	5162	01				NOF		
01810	00131A	5183	01				NOP		
01820	00182A	5184	01				NOP		
01830	00183A	5185	0.1				NOP		
01840	001846	5186	01				NOF		
01950	00185A	5187	01				NOP	A.#:00	
01860	001864	5168	86	88	Â		LUAA CTAA	不少なる まににプロ	MOVE MIRROR DOWN
01870	00187A	SIDO SIDO	1 157	CA 5	61 (2010)		BRA	MZERO	a stad of Basic of State Stat
01890	001894	518F	60	50A2	A	MINFIN	JSR	COLECT	LOOK FOR DOT
01900	00190A	51C2	FE	5306	A		L.DX	DOT	DOT THERE?
01910	0.0191A	5105	26	- 38 - 5	1.FF		BNE	JUMP	IF DOT THERE, RETURN
01920	00192A	5107	66	EF 08	A	l .	LDAA	\$CF08	
01930	001934	51CA	01				NOP		ለማስከተለ እና እና የሚከተረም ነበር በተማኅረግ የተማኅረግ እና
01940	001946	5100	: 11	EF08	- 6	I Contraction of the second	LDX	\$EF 03	OFF MUREOR FUSILIUR -

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			-	a					14
01950	00195A	51CE	F F	53E1	A		STX	LOCA	STORE MIRROR LOCATION
01960	00196A	51D1	86	53E2	A		LDAA	LOCA+1	D. P. SUBTR FOR DONE TEST
01970	00197A	51D4	80	5300	A		SUBA	INFIN+1	LSB SUBTRACT
01980	00198A	5107	B7	53E4	A		STAA	DIFF+1	STORE LSB RESULT
01990	00199A	51DA	86	53E1	`A	~ .	LDAA	LOCA .	
02000	00200A	S1DD	82	53DF	A		SBCA	INFIN	MSB SUBTRACT
02010	00201A	51E0	87	53E3	A		STAA	DIFF	STORE MSB RESULT
02020	00202A	5163	FE	53E3	Α		L.DX	DIFF	CHECK IF DONE
02030	00203A	51E6	2C	11 51	°9		EGE	DIE	XF NO DOT, DIE
02040	00204A	51E8	7F	EF70	A		CLR	\$EF70	MOVE MIRROR TO INFINITY
02050	00205A	51EB	01				NOP		
02060	00206A	51EC	01				NOF.		
02020	00207A	SIED	01				NOP		
02080	00208A	SILL	01				NOF		
02100	002096	5168	01				NOP .	1	
02110	002106	510	0.1				NOP		
02120	00211A	5162	84	AP	۵			1-8-A-R	
02130	002136	5164	82	FE70	6		STAA	4EE70	MOUE MIREOR
02140	002136	51F7	20	C6 51			BRA	NTNETN	RETURN AND LOOK FOR DOT
02150	00215A	5169	86	3F	A	DIF	LDAA	#\$36	
02160	002166	511.6	E?Z	51FE	A		STAA	BK.	
02120	00217A	SILE	01			BK	NOP		
02180	00218A	51FF	39			JUMP	RTS		
02190	00219					*****	******	*******	******
02200	00220			• .		* MI	ERROR M	OVE CADUUS	ST) SUBROUTINE **
02210	00221					*****	******	********	*******************************
02220	00222A	5200	136	570.0.1	A	MOVE	L.DAA	CONV+1	D. P. SUBTR FOR M. O. C.
02220	002200A	5203	190	5307	A.		SUBA	DOT+1	L. O. C. =LINES OFF CENTER
022200	003230 66729A	5206	10Z	500 M	Ĥ		STAA	1.0C+1	STORE LSB RESULT
02220	002246	5200	120	0000 ©002	6) A		LDAA	CONV	Sectors and the sector of the
02220	002220	5206	6.7	9000	**		SBUA	DUT	MSB SUBTRACT
02280	00228A	5212	217	SOFS	6		01 MM (** 10	1UU. MM	CLEAR MOTOR MOUSMENT LAR
02290	00229A	5245	FE	53F3	Ä		LDX	LOC	GEERA FID (OK HOVEFILIRT VHIN
02300	00230A	5218	27	3F 525	99		BEQ	COBCK	NO MOVE IF CONVERGENT
02310	002316	521A	23	01A0	Δ		CFX	##1A0	
02320	00232A	521D	27	GA 529	59		BEQ	GOBCK	SYSTEM ERROR FILTER
02330	00233A	521F	F.F.	53f 3	ē.		L.DX	LOC	GET LOC FOR BRANCH
02340	00234A	5222	$\mathbb{C}\mathbb{D}$	18 500	36		BMI	NUUP	IF LOC NEG, MOVE DOT UP
02350	0.053224	5274	83	20	ĥ.	NODM	LDAA	#\$20	,
02360	00236A	5226	1.67	5365	A.		STAA	MM	
02370	002326	5229	£3O	SPIE	Ô.		JSR	CLCMV	
02380	0.0238A	522C	ZE	EF770	Α		CLR	\$EF70	
02370	002396	52.2F 6250	01				NOP		
02410	002.70M	02.3U 82294	01				MOI»		
02420	002426	5201 5209	01		•		NOP		
02430	002404	5232	01				NOD		•
02440	002446	5234	01				NOP		
02450	002456	5235	01				NOP		
02460	00246A	5236	56	5005	A		LDAA	1111	CET MOTOR MOURMENT
02420	00247A	5239	\mathbb{B}^{2}	EF 70	۰A		STAA	\$EF70	
02480	0.0248A	523C	7E	5259	A		UMP	GOBCK	RETURN TO MAIN PROG
02490	00249A	520F	EeS	5364.	ê	MUUP	LDAA	L0C+1	
02500	0.05200	5242.	40				NECA		
02510	00251A	5243	82	53F 4	A		STAA	LOC+1	ABSOLUTE VALUE OF LOC
02020	00202A	0236	F:D	DEFE FC20	A		JSR	CLCMV	· · · ·
02530	0.02030	32.°C7 15:0-0-0	04	E.F 7,0	ค		ULR	\$£F70	•
02550	●●よい当台 自自之形態入	UCAU ROAD	10.4				18.JP		
02000	0025304	5-2 AC	01.				MON.		
02570	002524	52.40	01				MOD		
02580	0.02525	5250	01				NOB		
0.25.00	00280A	02000	0.4				NOP:		
02400	002.074	10726072	03				NOP		
02610	002414	525.02	64	Maria	۵		L DAA	MM	GET MOTOR MOVEMENT
02620	002624	5254	67	EE20	6		STAA	\$EF70	STORE IN MOTOR FIA
02630	00263A	5259	39		~	COBCK	RTS		
02640	00264A	525A	ВŚ	EF 08	A	DIIST	LDAA	\$EF08	
02650	00265A	5250	0.1				NOP		•
02660	00266A	5256	FE.	EF08	A		LDX	\$EF08	GET MIRROR VOLTAGE
02370	00267A	5261	E.E.	SBEF	A		STX	MIRAD	STORE IN MIRROR A/D
02680	0.02680	5264	ů3	53F0	A		LDAA	MJRAD+1	D. F. ADD- MIRROR A/D PLUS
02690	00269A	5267	643	e e	A		ADDA	#\$FF	\$3FF (BIAS FOR TABLE)
02700	00270A	5239	ΒZ	53F2	A		STAA	TOFSET+1	STORE LSB IN TABLE OFFSET
02710	00271A	526C	136	53EF	A		LDAA	MIRAD	MODE ADD
02720	00272A 00270A	026F 6024	89	03	A		ADCA ATAA	aoboeu. ≇ra	STORE MOR TH TADLE OFFORT
14. F STU	0047.00	N. 1. 1	1.11		- (- i)		31 (9 M	1 (.7) (.7)	SET STATE FRAME AND TRUCKE WER OF F

			1	,					
02740	00274A	5224	63	53F2	A		LDAÁ	TOFSET +1	MULTATAELEFOFFSETYBYWTWO
02 2/50	0.0275A	522 7	648	53F2	A		ADDA	TOFSET+1	FUR D. P. DATA
02760	00276A	527A	62	53F2	ê.		STAA	TOFSET+1	STORE LOD
02770	00277A	527D	66	53F1	6		LDAA	TOPSET	ADD MCP
02730	00278A	5200 5200	E92 - 1977 -	531-1. 5-2014	A -		ADUA CTAA	TOPOET	STORE MSB
022790	002004	0200 0701	107 127	erenti. Riterit	0 A		CDAA	TOPSET	ADD IN TABLE INITIALIZE
02000	002000	0000 10000	OD:	ພະຍາ ເ 1740)	A .		6006 6006	#\$25	LOCATE TABLE AT \$7000
0.2020	0.02024	0202 #9200	00	7 W 1973013	м А		CTAA	TOFSET	STORE IN MSB
02020	002020	SOOF	ere:	5011	6		LDX	TOFSET	GET TABLE OFFSET
02840	002846	5291	FF	5225	Ä		STX	FLAG1+1	INJECT IN DATA RETR. LOCA
02850	00285A	5294	F E.	2000	A.	FLAG1	L.DX	\$2000	GET OUTPUT DATA FROM TABLE
02860	00286A	5297	F F	50 ° 6	A'		STX	TEMP2	STORE TO DO BIAS & SCALE
02870	00287A	529A	t F	5369	fa -		STX	ER1	STORE FUR ENRUR CALL
02890	00288A	5290	86	53FZ	é.		LDAA	TEMP2+1	ADD ESS SIGS FRUIDS
02890	00289A	52A0	68	5006	A		ADDA	1911 (A 1977) 1 1917 - A 1972) 1 4	CTODE DIAGED LER
02900	00220A	5203	EZ -	538 Z	Ĥ		5166	T 10,000 (20,70). 10,000 (20,70)	STORE BERGED COC
02910	002916	0200	1940	2008-00 1060-00	6		LU99 ADCA	HEND &	ADD MSR RIAS FACTOR -
022220	0.02028	0.061% 50000	10.7	0000 . E004	.61 		90009 8166	TEME2	STORE BLASED MOB
02730	002738	STELE	ωz	9.91.0	[**]	ж. M18.111	PLY BY	1 5 TO AL	FROX SCALE OUTPUT**
022240	0.020555	SCAF	БA	SOCA	۵	* HOLTA	LDAA	TEMP2	GET MSB OF VOLTAGE
022200	002934	5262	44	(Jac) 12			LSRA		DIVIDE BY 2
02970	002976	52133	82	sone	A		STAA	TEMP'3	STORE MSB QUOTIENT
02980	00298A	5286	8.5	53F7	ń.		LDAA	TEMP2+1	GET LOD OF VOLTAGE
02990	00299A	5269	46				RORA		DIVIDE BY 2 (PULL CARRY IN)
03000	00300A	52PA	67	53E9	A		STAA	TEMP3+1	STORE LSE QUOTIENT
03010	00001A	52.BD	83	SBEZ	A		LDAA	1:59P3F1	ADD FOR 1 5 SCALE FACTOR
03020	00302A	5200	66	53F9	Α		adda	TEMP3+1	LSE ADD
03030	00303A	5209	67	53FB	A		STAA	INSOUT+1	STORE LSE OF ALTIM DUIFUT
03040	003046	5206	186	5398	A		LDAA	TEMPS	
03050	00305A	5209	62	53h6 ©2014	Рі А		ADUA	TACOUT	STORE MOR OF ALTIM OUTPUT
03060	003066	ROCE	107	SSEA	6			TNSOUT	GET BIASED AND SCALED VALUE
0/20/20	003026	5202	(° (°)	EE20	6		STX	\$EE20	DO D/A CONV FOR ALTIM OUTFUT
0.2020	00300A	5205	ŕΕ	5369	A		LDX	ER1	GET ORIG TABLE VALUE
03100	00310A	5208	E.E.	EF24	A		STX	\$EF24	DO D/A FOR STRIP CHART
03110	003116	52126	£55	EF0C	A		LDAA	\$EFOC	
03120	00312A	52DE	Ü 1				NOP	•	
03130	.003130	52DF	FIE	EFOC	A		L.DX	\$EFOC	GET TRACK VULTAGE
03140	00314A	52E2	te te	5308	Â		STX	ER2	D D CHETE FOR FRRBR CALC
03150	003156	5265	Bo	DGLA	A		LUAA	ERL+1 CD2+1	LOD CHETE
03150	003168	021.0	150 1977	COLLU RECEDE			SUDH	ERECE+1	LSB ERROR
03120	003126	52136	86	53E9	商		LDAA	ER1	
03120	00319A	52F1	02	SOLB	A		SBCA	ER2	MSB SUBTRACT
03200	00320A	52114	ΒZ	5000	A	•	STAA	ERROR	MSB ERROR
03210	00321A	5267	FE	SBED	Α		LDX	ERROR	GET FINAL ERROR VALUE
03220	00322A	52EA	F F	EF22	Ĥ		STX	\$EF22	DO D/A FOR STRIF CHART
03230	88323A	52FD	39				RTS		
03240	00324A	52FE	1:6	53F 4	A	CLCMV	LDAA	LOC+1	MALLE A CMALL MOLLET?
03520	00325A	530 J	ED.	5002	A.		CMPA	SMAV	MAKE A SHALL HOV FI
03260	00326A	5304	20	27 53	3D 		DEL I	STIML.L.	MAKE A MEDIUM MOV'T?
03270	00327A	5305	1.5.1	-3003 -10 69	-0	•		MED	
03280	003200	- 0.30 V E/2012	10:1	- 30 00. - 5084	ം		CMPA	LGMV	MAKE A LARGE MOVIT?
03300	0032224	5306	20	0A 53	1.6		BLT	LARGE	
03310	00331A	5010	86	84	A	LCST	LDAA	4484	LARGEST POSS MOVIT
03320	00332A	5312	F6	50F5	A		LDAB	MM	GET DIRECTION
03330	003334	5315	18				ABA		COMPITNE
03340	003346	5316	137	5065	A		STAA	MM	STORE COMPLETED MUV'I
03350	0.0335A	5319	38				RTS		1. A month - X40114 m
03360	00336A	591A	86	83	Â	LARGE	LDAA	**83	LARGE MOVIL
03370	0.0337A	531C	1.6	2352	Ĥ		LUAR	ោះខា	COMPTME
03380	00338A	531F	18	COUNT	~		ADA CTAA	мм	STORE COMPLETED MM
03390	003376	- 3320 - 60000	- 67,	331 0 02		MED	51 MM	#\$32	MEDIUM MOV'T
03400	003104	- U.O.C.O - 19 (2/9)	- 67. - 67.4	e operationed Constant	- A	1.01.1.7	LDAB	MM	CET DIRECTION
03420	003426	5028	18	1.91.91 U.V	•••		ABA		COMBINE
03430	000434	5329	E.Z	53115	A		STAA	1115	STORE MOTOR MOV'T
03440	003444	5320	39				RTS		
03450	00345A	532D	83	81	A	SMALL.	LDAA	# #81	SMALLEST POSS MOV'T
03460	00346A	532F	۴ð	53F5	A		LDAB	MM	GET DIRECTION
03470	003476	5332	18			,	ABA		COMEINE
03480	00348A	5333	87	53F5	A		STAA	MM	STORE MOV'T
03490	00349A	5336	39				RTS	0	
03500	00350A	5337		0002	A	VARI	RMB	1	+ OF NO DOT DARGER
03510	00351A	5339		0001	A	STEL OTADUM	RME	J. 1	N UP NU UUT PHOSED Æ DE LINE CIARIE BACCEC
03520	00352A	533A		0001	A	to FPISUA:	IXPU:	J.	ግድ አለተ በ "አርተናርሬ። እንግ ተገባሪክሬሮሩ። በግግሩን ቆንደራ መ

03530	00353A	5338	001E	A	NDATA	RMB	30
03540	00354A	5359	003C	A	LDATA	RMB	60
03550	00355A	5395	003C	A	DDATA	RMB	60
03560	00356A	5301	0001	Α	COUNT1	RMB	1
03570	00357A	53D2	0001	A	NUMB1	RMB	1
03580	00358A	5303	0002	Α	DUMMY	RMB	2
03590	00359A	5305	0001	Α	COUNT2	RMB	Ĵ,
03900	00360A	5306	0002	Α	DOT	RMB	2
03610	00361A	5308	0002	ĥ	LINE	RMB	2
03620	00362A	53DA	0002	A	MAX	RMB	2
03630	00363A	53DC	0001	۵	NDCNT	RMB	1.
03640	00364A	53DD	0002	A	ZERO	RMB	2
03650	00365A	53DF	0002	A	INFIN	RMB	2
03660	00366A	53E1	0002	Α	LOCA	RMB	2
03670	00367A	53E3	0002	A	DIFF	RMB	2
03680	00338A	53E5	0002	A	TEMP1	RMB	2
03690	00369A	53EZ	0002	۵	TADD	RMB	2
03700	00370A	53E9 -	0002	Α	ER1	RMB	2
03710	00371A	SBEE	0002	A	ER2	RMB	2
03720	00372A	53ED	0002	Α	ÊRROR	RMB	2
03730	00373A	538F	0002	Α	MIRAD	RMB	2
03740	00374A	53F1	0002	Α	TOFSET	RMB	2
03750	00375A	53F3	0002	A	LOC	RMB	2
03760	00376A	53F5	0001	A	MM	RMB	1
03770	00377A	53F6	0002	A	TEMP2	RMB	2
03780	00378A	53F8	0002	Α	TEMP3	RMB	2
03790	00379A	53FA	0002	A	INSOUT	RMB	2
03800	00380A	53FC 39			RETU	RTS	
03810	00381					END	
TOTAL.	ERRORS	00000	00000			•	

WIDTH OF DOT DATA RASTER LINE & DATA DISPLACEMENT DATA # OF COLLECT PASSES DUMMY TIME PAD VAR. ✿ OF LINES WITH A GOOD DOT LOCATION OF DOT CENTER TEMP STORE FOR DOT CENTER SAME AS ABOVE # OF LINES W/ A GOOD DOT MIRROR VOLTAGE @ DIST=0 MIRROR VOLTAGE @ D=INFIN CURRENT VOLTAGE OF MIRROR DIFF BETW LOCA AND GOAL TEMP REG FOR MOVIT CALC TABLE ADDRESS SYSTEM ERROR VAR 1 SYSTEM ERROR VAR 2 RESULTANT SYSTEM ERROR MIRROR VOLTAGE FOR DIST TABLE OFFSET (BIAS) OF LINES OFF CONVERGE MOTOR MOVEMENT TEMP REG FOR DIST CALC TEMP REG FOR DIST CALC ALTIMETER OUTPUT VOLTAGE

5171 ADD1 00153 00155× 5005 BTAS 00013*00289 00292 51FF BK 00216 00217* 5102 CHECK 00107*00137 00237 00252 00324× 52FE CLCMV 50A2 COLECT 00045 000/3*00163 00189 5000 CONV 00009*00061 00222 00225 53D1 COUNT1 00077 00100 00101 00356* 53D5 COUNT2 00079 00120 00135 00138 00359* 5143 DCENTR 00109 00138* 5395 DDATA 00075 00076 00130 00134 00142 00355× 51F9 DIE 00203 00215× 53E3 DIFF 00172 00175 00176 00198 00201 00202 00367* 513E DISAB 00119 00136* 00046 00069 00264* 525A DIST 00047 00104 00147 00150 00151 00155 00157 00164 00190 00223 00226 00360* 53D6 DOT 509D DRIVE 00065 00071× 00085 00087 00088 00089 00090 00091 00092 00093 00094 00095 00095 00097 00098 00099 00358* 53D3 DUMMY 53E9 ER1 00287 00309 00315 00318 00370× 53EB ER2 00314 00316 00319 00371* 00317 00320 00321 00372* 53ED ERROR 5069 FILTER 00050× 5037 FLAG 00031×00037 5294 FLAG1 00284 00285× 00045×00051 00057 00060 00067 00070 00072 00230 00232 00248 00263* 5058 GO 5259 GOBCK 5179 HUNT 00059 00159× 53DF INFIN 00160 00197 00200 00365* 53FA INSOUT 00303 00306 00307 00379* 50C1 JMP2 00084*00102 5138 JMP4 00121 00135× 51FF JUMP 00165 00191 00218* 531A LARGE 00330 00336* 5359 LDATA 00073 00074 00124 00128 00140 00354* 5004 LGHV 00012*00329 5310 LGST 00331× 50D8 LINE 00141 00145 00148 00361* 00224 00227 00229 00233 00249 00251 00324 00375× 53F3 LOC 53E1 LOCA 00169 00170 00173 00195 00196 00199 00366* 5124 MARK2 00124x 5131 MARK3 00130* 00143 00362* 53DA MAX 5003 MDMV 00011*00322 5323 MED 00328 00340*

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51BF	MINFIN	00177 0	0189*	00214									
53EF	MIRAD	00267 0	0268	00271	003738	c							
53F5	MM	00228 0	0236	00246	00261	00332	00334	00337	00339	00341	00343	00346	00348
		00376×											
5200	MOVE	00071 0	0222×	č									
5224	MUDN	00235×											
523F	MVUP	00234 0	0249×	ć		1							
5185	MZERO	00163×0	0188										
53D2	NUME:1	00078 (00357*	(
5048	OUTLOP	00033 0)0038×	ζ									
50FF	READ	00085 0	01106×	¢									
53FC	RETU	00380×											
5084	RUN	00052 0	0061×	(
507C	SEND	00055 0	0 0 58*	¢									
5095	SET1	00062 0	0038*	¢									
532D	SMALL	00326 0	00345×	¢									
5002	SMMV	00010×0	0325								,		
5070	STA1	00048 0	00053×	c									
533A	STABLE	00038 0	0064	00066	00048	00352*	(
5339	STB1	00039 0	0049	00054	00056	00058	00351×	¢ (
53E7	TADD	00369×											
53E5	TEMP1	00368×										••.	
53F6	TEMP2	00286 0	0288	00290	00291	00293	00295	00298	00301	00305	00377×	C	
53F8	TEMP3	00297 0	00300	00302	00304	00378×	¢						
53F1	TOFSET	00270 0	00273	00274	00275	00276	00277	00278	00279	00280	00282	00283	00374×
5337	VARI	00350×		~									
533B	NDATA	00353×		- · •									
53DC	WDCNT	00139 0	0144	00146	00363×	(
53DD	ZERO	00162 0	0171	00174	00364*	(-					

I claim:

1. In a method for determining the altitude of a flight simulator probe moving relative to and above the ter-³⁰ rain of a flight simulator model wherein the imaginary line extending from the probe in a direction normal to the model is characterized as the probe plumb line, the steps of:

- directing a pencil-like beam of radiation from said ³⁵ probe onto the model keeping said beam within a plane containing said probe plumb line to produce a beam spot on said model;
- detecting the location of said beam spot relative to two orthogonal coordinates with a detector situated remote from said probe plumb line and having a linear sensitivity zone optically aligned with said probe plumb line;
- varying the angular orientation of the beam within 45 said probe plumb line plane and relative to a reference plane so as to cause said beam spot to impinge on the model site intersected by said probe plumb line;
- determining the angular orientation of the beam rela- 50 tive to said reference plane; and
- utilizing the determined angular orientation of said beam to determine the altitude of said probe over the terrain of the model.

2. The method of claim 1 including the step of, direct-⁵⁵ ing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxially of said probe plumb line; and detecting the second beam spot when said first beam spot is obstructed by the terrain from reaching the intersection of the model and the probe plumb line.

3. The method of claim 1 wherein said beam of radiation is a beam of monochromatic, collimated light.

4. The method of claim 1 wherein the step of detecting the beam spot includes the step of directing a beam spot image through a light pipe on a path between the beam spot and the detector. 5. The method of claim 2 wherein the step of directing the second beam of radiation onto the terrain includes the step of splitting off of the first beam a portion of its energy to produce said second beam.

6. In a flight simulator apparatus of the type where a probe simulates an aircraft and the simulator operator controls the motion of the probe relative to the terrain of a model while viewing said model via a video monitor on said probe:

- means for directing a pencil-like beam of radiation from the probe onto the terrain of the model to produce a beam spot on the model where the beam impinges on the model, an imaginary line extending from said probe normal to said model being known as the probe plumb line;
- means supported by said probe for detecting the location of said beam impingement on said model, said means being remote from said probe plumb line, being two-dimensionally sensitive, and having a linear sensitivity zone in optical alignment with said probe plumb line;
- servo means coupled to said beam directing means and said detecting means for varying the angular direction of the beam in a plane containing the probe plumb line and maintaining the beam spot on the model at the site where the probe plumb line intersects the model;
- means for determining the angular orientation of the beam relative to a reference plane; and
- means for utilizing the determined angular orientation of said beam to determine the distance between said probe and said model measured along said probe plumb line.
- 7. The apparatus of claim 6 including:
- means for directing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxial of said probe plumb line; and
- means for detecting the second beam spot when said first beam spot is obstructed by the terrain from

reaching the model site intersected by the probe plumb line.

8. The apparatus of claim 6 wherein said means for directing a pencil-like beam of radiation includes means for directing a pencil-like beam of monochromatic, collimated light.

9. The apparatus of claim 6 including light pipe means

for directing an image of said beam spot to said detecting means.

10. The apparatus of claim 7 including beam splitter means for splitting off a portion of said first beam to produce said second beam.

11. The apparatus of claim 6 wherein said detecting means includes a video camera. *

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