REVIEW OF AIDS DEVELOPMENT

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#### SUMMARY

Since the introduction of the wide-body aircraft KLM, SAS and Swissair have been able to collect a mass of experience, meager as will as excellent and in total profitable. All three are very determined to continue with AIDS on A300/310 Airbus (Swissair also on the DC-9-80). The A300/310 AIDS as selected by KSS (KLM, SAS and Swissair) and Lufthansa has been developed into a very powerful Engine Monitoring System (EMS) and engineering tool capable to enhance aircraft regularity, reliability and economic operation.

#### INTRODUCTION

KLM, SAS and Swissair started with AIDS at the introduction of the widebody aircraft in 1970. The AIDS hardware specification for the Boeing 747 and McDonnel Douglas DC-10 aircraft was based on the experience obtained from:

- . A digital recording experiment by KLM on a Douglas DC-8 in 1963 and 1964 (3) and DC-9 trials with prototype equipment in 1969.
- . The development of the ARINC 573 specification for a Flight Data Acquisition Unit (FDAU) to satisfy the new FAA requirements.

The initial objectives of KSSU with respect to the AIDS were primarily directed to the monitoring of parameters related to:

- . the safety of the flight
- . the performance of the aircraft
- . the performance of the flight guidance system
- . the performance and condition of the engines.

The AIDS-EMS function was and still is considered supplemental to the existing monitoring tools.

For AIDS-EMS practically the same parameters were selected as already provided for display on the cockpit instrument panels with a few exceptions. Table I provides a list of EMS parameters monitored on KSSU aircraft. The total number of parameters monitored on KSSU 747 and DC-10 aircraft amounts to 380 and 280 respectively of which more than 50% are discretes (on/off signals). In order to accomodate all these parameters and enable sampling at reasonable rates the system was configured around 3 Data Acquisition Units and a Data Management Unit (DMU) with limited data acquisition capability. Figure 1 depicts the system block diagram.

#### AIDS OPERATION

In KSS the AIDS is primarily applied as an engineering tool with a strong emphasis on analysis of recorded information. A printer was added to the airborne system because it was recognized rather early that hard copies of exceedance reporting could provide a very effective aid in trouble reporting. The application of on-board processing for limit exceedance monitoring and recording control allowed to add a printer which could provide hard copy reports on request by the crew or automatically.

The tape-cassette is removed every landing made at the home-base and is subsequently transcribed to IBM compatible tape and processed. The routine programs applied comprise o.a.: flights logging, AIDS status reporting, EMS programs, autoland verification, etc.

For a good understanding of the function of AIDS in an EMS, it is essential to give some details on the functions of two specific software programs: the AIDS flight logs and the plot/list program. The first program provides a listing of all recorded flights per aircraft registration and the second program allows users to request a time history of a set of 8 analog plus 8 discrete type parameters either in table format or plotted. The user can call the AIDS flight log, select the airplane, the flightleg and the parameterset of interest and request a listing either for a specified flight mode or a GMT time span using the VDU terminals of KLM's data handling system. The very successful use of this program proved that AIDS is an invaluable engineering tool and fully met the set objectives.

#### CURRENT AIDS EMS APPLICATIONS

# ON BOARD

For short-term trend analysis KLM relies on a trendchart that is updated by the flight engineer on every flight that lasts more than 4 flight hours. The flight engineer then selects a stabilized flight condition to request and engine data print (table 2). The flight engineer uses this print to calculate the trend delta's with the aid of an engine performance calculator provided by the engine manufacturer and enters the delta values in his trend chart. Engine bleed and engine indicating problems, serious compressor/turbine problems and EGT-margin losses can be detected by the flight engineer using these short term trends. In addition these trends are checked by powerplant engineers on a regular basis and in case of crew complaints.

The engine data prints are also automatically presented during take-off and in case of limit exceedance e.g. the print of table 2 shows an automatically reported impending hotstart on engine nr. 1. The take-off prints are used to monitor the hot-day EGT margin, thrust settings etc. Crew complaints are supported by prints selected by the flight engineer and/or limit exceedance prints. In case of critical engine problems the flight engineer will contact the main-base via a single-sideband company channel for expert advise. With aid of the print he is able to provide exact information on the characteristics of the trouble or exceedance, the exact durations and the peak values of exceedances.

Strict adherence to the manufacturers engine operating limits could increase the number of engine removals because of the capability of EMS to very accurately report exceedances of operating limits that are based on experience, which include the human factor. It is obvious that these limits need to be adapted when an advanced EMS is used to prevent increased removals or inspection rates. KLM was able to obtain the approval to extend the limit on the allowable EGT exceedance time-limit on a particular engine when using the AIDS printer. This printer function has proven an invaluable tool for short-term engine monitoring, incident reporting and trouble-shooting to the extent that powerplant engineers consider this feature alone was worth the investment in AIDS.

# GROUND-BASED LONG TERM ANALYSIS

For long term trend analysis the AIDS provides weekly trend reports on KLM's JT9D and CF6 engines. These trend reports consist of 3 parts viz. an engine start trend (fig. 2a), an engine take-off trend (fig. 2b) and an engine cruise trend (fig. 2c). The trends shown apply to the Pratt&Whitney JT9D engine as installed in KSS 747 airplanes.

#### Engine start trend

Of the engine start trend one important feature should be adressed. After careful analysis using the AIDS plot/list program KLM engineering decided to trend the initial fuel flow (IFF) at the moment of "fuel-on". This analysis showed that by monitoring this value it was possible to relate a positive or negative deviation from the required value to a fuel control adjustment. Although the fuel control adjustment screw was by design meant for shop use only, it is now used for on-wing adjustment. This meant that by monitoring the IFF trend, hot and hung starts and consequent fuel control removals are reduced considerably and related unnecessary engine test runs avoided. Since its introduction more airlines became interested and have requested the engine manufacturer to provide proper means for on-wing adjustment.

# Take-off and cruise trends

The take-off and cruise trends are both used for monitoring of engine deterioriation, primarily by checking EGT rise and EGT margin, blade failures, compressor and turbine problems and indicating system errors. The take-off trends is also used to monitor powerlever-alignment which avoids valid crew complaints and allows to neglect invalid crew complaints and save on otherwise necessary follow-on actions.

#### Gas path analysis

SAS first started using GPA based on testcell data to analyze modular deficiencies on the JT9D engine. After showing positive results KLM installed the same program but to analyze the CF6 engine. After an extensive evaluation and calibration program to determine sensitivity, performance levels and ability to find degraded modules, the program also at KLM is deemed useable to identify problems on preshop tested engines.

The function of the test-cell however has always been primarily to verify that an overhauled or repaired engine meets performance requirements. The identification of modules degraded below limits should therefore preferably occur on-wing such that an engine's work scope can be predicted prior to shop entry.

SAS and KLM has therefore decided to develop the necessary procedures and know how with GPA based on AIDS recorded data.

SAS has started with JT9D-7 engines installed in Boeing 747 while KLM will analyze CF6 engines installed in DC-10. The JT9D program will use only partly instrumented engines while the CF6-DC10 will be fully instrumented. Future aircrafts within KLM, SAS and SWR will always be fully instrumented and in particular the A310 with also a PMUX, presently the only one specified with PMUX, will already from the beginning be monitored by programs capable of modular performance analysis.

Table 5 shows the parameters used in the presently ongoing GPA programs. As can be seen the SAS JT9D-7 GPA uses the least number of parameters and there fore also has the least capability. This program however has advanced the most and a discussion showing some results follows. Because of the small number of parameters that are available to describe the engine operating characteristics, some assumptions have been necessary to do on the modular deterioration that is analyzed. The assumptions are a fixed ratio between change in efficiency and air pumping capacity on the compressor modules and also both the FAN and the LPC are treated as one module. The main disadvantage with the hard coupling between efficiency and air pumping capacity is expected to be seen in the HPC where the front stator vane stages are variable and changes in pumping capacity might be induced this way.

Figure 12 shows the variation in ambient conditions under which data is collected for GPA. Each datapoint being used is a stable frame that has been recorded by the airborne system. The measurements are reduced to sea level static and corrected for effects of Reynolds number, engine service bleed and the offset initially found in the actual installation position. This the corrected value is compared to a fleet average baseline and the percentage difference is calculated. This difference known as "gross delta" is first used to look for apparent sensor errors. If the datapoint is deemed erroneous an appropriate message will be issued and no further analysis is done. The accepted datapoints are used for further analysis.

Figure 13 shows one month worth of data in terms of gross deltas. The result when using each individual gross delta point for analysis is shown in figure 14. As can be seen the scatter is significant and therefore with this combination of sensors and the this way obtained accuracy of gross deltas the result is not accurate enough to correctly analyze module performance based on the data point. The way to get around the problem that is presently used, is that gross-deltas from individual flights are calculated, checked for apparent sensor errors and if found within sensor check limits the gross deltas are passed on to a ten flight average calculation. The gross deltas again in the average calculation will be checked for outliers in a simple correlation analysis. The result from using averaged gross deltas as input to GPA is seen on figure 15.

This particular engine had been installed for several months already at the beginning of this trending, why very limited deterioration is to be expected over the trend period. The 13 trend points now corresponds to 130 flights with stable data, or on this particular route-net approx. 200 cycles.

GPA based on the very limited parameter set used in this trial can not replace pre-shop tests of engines. It gives however additional valuable information on top of the normal trending and will be further studied for use in our preventive removal concept.

# LAP, Life Accounting Program

This program is used to bookkeep the amount of damage on critical parts based on actual engine performance and routes flown.

The High Pressure Turbine airfoils on the JT9D-7 are amongst the most critical parts in that engine and are deemed possible to be modelled accurate enough for an analysis. The basic program, written bij PWS, uses precalculated severity factors for each mission and actual AIDS data from each flight to define engine performance levels and routes flown.

The actual life consumption depends upon the mission and the performance status of the engine. The mission is described by a sverity factor that has been precalculated by a Mission Analysis Program using statistical data. Each citypair has several severity factors that varies with respect to season of the year and actual failure mode accounted for, see table 3.

The reason for useage of precalculated statistical severity factors is, that the KSSU airborne 747 AIDS program at the time of specification was not defined to collect mission analysis/life accounting data.

The following failure modes are referred to in the program.

Nozzle Guide Vane crack	- NGV
lst blade creep-fatigue	- 1 BCF
lst blade oxidation corrosion	- 1 BOC
2nd vane deflection	- 2V
2nd blade creep	<b>-</b> 2B

The 1BOC is the only life useage that can be reset by repair e g recoating. All other failure modes refer to life useage that is incremented at each flight throughout the service life of the part.

A typical output generated on a monthly basis is shown on table 4 where the percentage life used is shown for each failure mode. 100 means that expected service life is completely used up.

# Experience

The most critical part is 1st blade and therefore, the experience on LAP-

life compared to actual failures non-failures is shown in figure 11. A curve ending with F means failure and FO means failure due to overtemperature or where also overtemperature has been confirmed. As shown by the graph there is a good correlation between actual failures and 100% life used for IBCF. The weak point with this program is that statistical missions are used instead of actual. Missions significantly deviating from nominal as well as engine exceedances for example, higher temperatures than normal during take-off, startup or reverse if encountered is not accounted for.

# Autoland verification program

This program produces per aircraft a two-monthly review of Autoland performance. Per line the Autopilot disconnect heights, ILS tracking quality, wind at 100 ft, touch-down dispersion and touch-down maximum g-loads are presented. For the total fleet a two-monthly statistical performance review is presented. The program is used to demonstrate an acceptable Autoland success rate to the authorities and keep control over the maintenance of the Autoland system.

# 747 APU monitoring

The AIDS system allows to apply a very effective means of health monitoring to the Auxiliary Power Unit. The groundbased computer monitors acceleration time, EGT peak and rotor speed at peak EGT, airduct pressure during airconditioning system operation with 3 packs and EGT at no-load condition. This program provides indication of and/or clues to mechanical problems, starting problems, airleaks, compressor and turbine inefficiencies.

# 747/DC-10 aircraft structure lifecycle programs

Since many years KLM collects AIDS recorded data for assessment of service load experience. Results allow comparison to Boeing's fatigue integrity program with the objective to compare the severity and schedule structural inspections on this basis.

Studies on the recorded data also revealed that changes in pressurisation procedures would extend the life of the pressurised structure.

# TROUBLE AND INCIDENT ANALYSIS

In reference (2) the analysis and monitoring of JT9D starting problems and the analysis of JT9D auto-accelerations was presented with the cures.

Since that presentation the CF6 compressor stall problem has been solved. The total story is as follows:

## CF6 compressor stalls

Although the KSSU CF6 compressor stall-rate reached a low level of 0.06 per 1000 engine hours, the nature of this problem urged to aim for elimination. The major reason is that stalls can occur in critical phases of the flight and thus might endanger the safety of the flight or comfort of the passengers. Several of the experienced CF6 compressor stalls in the winter period of 1979/ 1980 occurred at the moment the airplane entered a rainshower (fig. 3). Apparently the compressor inlet temperature (cit), measured at the high pressure compressor inlet, drops at constant N2 rotor speed and constant total air temperature, causing the variable stator vane (vsv) to move with the ultimate result that the NI rotor speed increases at constant N2, causing some individual engines to stall.

First action was to monitor N1 vs N2 to avoid an N1/N2 matching critical to stall. At the same time the study and analysis of all AIDS recorded compressor stalls by a group of specialists was performed with the objective to ultimately eliminate in-flight stalls.

The studies resulted in two actions:

First : Protective rainshields around the CIT sensors were installed figure 4. Second : In the testcell the Variable Stator Vane (VSV) schedule was adjusted to the more closed position figure 5.

By these actions the engine stall-rate started to drop significantly as can be seen in figure 6.

Today CF6-50 aero stalls are practically eliminated. The cost of aero stalls to the airline were negligable for CF6's with steel compressor casing but amounted to over \$ 200 000 each for CF6's with titanium casing. The savings resulting from elimination of aero stalls alone paid for a very substantial part of the AIDS investments if not complete.

It should be noted that all CF6 operators benefit through the AIDS EMS system as used by KLM and the engineering efforts that KLM and other AIDS users put into the task of solving problems like the CF6 compressor stalls.

# Flight Technical

Special Flight Technical analysis programs provide means to analyze crew complaints more thoroughly. Programs developed for this purpose are: - an ILS beam quality check program

- a runway surface analysis program

and - a windshear analysis program

# Fuel Consumption Management

In order to ensure accurate flightplan fuel determination KSS uses a computerprogram to monitor the consumption levels per airplane type and per individual airplane. Accounting for consumption levels of individual airplanes allow tighter fuel reserves. In order to more effectively analyze individual high consumers KLM developed a program based on AIDS data that enables engineering to verify effects of maintenance actions on consumption on a short notice. Figure 8 shows CF6 gas generator curves developed from AIDS recorded data on one flight using a least squares approximation.

It demonstrates the high degree of repeatability achieveable with AIDS recorded data. The maximum deviations of individual data points from the curves are 0,4% corrected fuel flow, 0.13% corrected N2 RPM and 0.05 corrected EPR.

#### GENERAL ASPECTS

From the examples of the previous paragraphs AIDS appears as a reliable and useful source. Because of its accurate observations, lessons can be learned fast, proper actions can be subsequently applied and cockpit procedures optimized. AIDS also demonstrated on various occasions the ability to observe and report problems outside the observation capability of the crew, it does not conceal human imperfections nor human excellence in performance. Careful treatment of problems where the human factor is involved is a must when disturbance of human relations is to be avoided.

#### A300/310 AIDS

## Development

Ten years of experience with expanded AIDS systems have demonstrated to KLM, SAS and Swissair that the AIDS has matured into an effective engineering tool as predicted. With increasing positive experience it became evident that more effective airborne software was desirable but prohibited by the capacity of the system and the extreme costs of fleet modifications. With the advance of digitalisation of aircraft systems ARINC started to develop new characteristics for these systems known as their 700 series characteristics. In the Boeing 757 and 767 and the Airbus 310 these 700 series digital systems are extensively used. The impact of this development can best be illustrated by comparing the types of KSS AIDS inputs for the 747 and A310:

747 : 210 discretes, 170 analog and 4 digital data bussesA310 : 39 discretes, 49 analog and 38 digital data busses.

Taking advantage of this progress in the application of digital technology, KSSU and the ATLAS European group of airlines, with full cooperation of Airbus Industrie, started to develop an Expanded AIDS for the A310 (ref. 8) based on ARINC 717 (ref. 9). Early 1980 this effort was successfully completed. A block diagram of this system is shown in fig. Subsequently KSSU developed a specification which in more detail specified the desired software functions and specific features derived from KSSU AIDS experience over the years and contracted the system to a major U.S. supplier. In general the increased capacity of the A310, both in terms of parameter inputs and installed software, is used to enhance the AIDS as an engineering tool and expand its troubleshooting capabilities. The relative expansion on parameter inputs partially comes by itself on a digital airplane where most parameters can be sampled from ARINC 429 data busses.

# Justification

As previously stated AIDS proved to be an effective engineering tool and provided to KSS an ample return on investments.

Of course the 747 AIDS was not an optimum system compared to the possibilities and the available experience of today. Therefore applying the lessons learned to the A310 AIDS application will result in a still more cost effective system. The conditions have also changed, c.q. the amount of sensor wiring in the airplane has been decreased compared to the 747 and DC-10 AIDS and the capacity of the electronics increased drastically with the result that the costs of a complete installed system is less than of its predecessors.

Translating the investments to costs per flighthour and assuming a reasonable aircraft utilisation these costs will rougly amount to \$ 10.- per flighthour. The total costs will double when the AIDS operating costs are added.

A KSS return on investment study for the A310 AIDS did not produce a homogeneous result between KSS partners because there were several differences in estimated savings per individual program or different emphasis on values of benefits.

The ultimate conclusion as derived from past experience can therefore best be presented schematically. Figure 8 shows that the level of quantifyable savings will more than balance the AIDS operating costs.

# Characteristics of the KSS A310 AIDS

The control of the recording, printing and display functions is performed by the Data Management Unit (fig. 9). In this unit an Intel 8086 16 bit microprocessor is installed to perform the required functions. The memory comprises 58 K bytes PROM, 18 K bytes RAM, 29 K bytes protected RAM and 39 K bytes EAROM.

Depending on the flight mode the DMU commands continuous recording or selective recording.

All data that is to be recorded passes a 20 second delay buffer such that at detection of specific events always 20 seconds pre-event data is available on the tape-cassette. 75% of the cassette-tape capacity is used for routine recording and the remaining 25% is programmable via the Control Display Unit (CDU). This feature provides to engineering a tool to analyse and solve persistent problems.

The on-board printer can be used by the crew for hard copy engine data but its primary purpose is to provide maintenance with all necessary information. For this reason all maintenance prints are stored during flight and a light on the CDU will inform the maintenance crew that exceedance reports are stored in the DMU memory. In case of specific events as defined in the program, 20 seconds of data prior and 20 seconds of data after the event will be stored and can be recalled by the maintenance engineer using the printer. The memory section used for this feature is called the replay buffer. From the replay buffer the maintenance engineer can select "canned" sets of parameters prividing a second by second listing of the event occurrance.

For the objectives set for the EMS part of the program it became necessary to provide additional sensors on the engines. KSS and ATLAS in close cooperation with Airbus Industrie and the engine manufacturers succeeded to specify a Powerplant Multiplexer (PMUX) as standard part of an A310 Expanded AIDS.

This PMUX multiplexes temperature and pressure signals, combines these with the output of the Electronic Engine Control (EEC) or Power Management Control (PMC) and sends all this information with the engine serial number via an ARINC 429 dataline to the DMU. This improvement ensures a tighter maintenance control on the quality level of those inputs not monitored by the flightcrew.

#### A310 ENGINE MONITORING

KSSU formed a team of engine monitoring experts to participate in the specification work on the A310 AIDS. This group being able to take advantage of experience with already existing programs has defined a system incorporating several new features that have never before been available.

# Program functions

## New functions

Two of the new program functions namely the "history buffer" and the "replay memory" are briefly described already above. One other is known as "stored prints" and works such that the printer does not print in real time, with some very few exceptions, but data that shall be printed is stored in a "print buffer" until a special request is made. There is capacity for storeage of 11 prints with the distribution as defined in table **6** 

#### Exceedance Control

The software of course is capable of defining flight modes and to compare selected engine parameters against flight mode related limits throughout the mission.

In case of an exceedance, different actions will be taken. An exceedance can thus cause:

- 1. Update of exceedance print buffer
- 2. Recording without 20 sec. pre-event data
- 3. Recording with 20 sec pre-event data
- 4. Update of replay memory.

# Stable Condition search

The search for stable conditions is, done with a new logic. The method can be described as a window sliding in time over actual and previous data, that are remembered in the computer, looking for stability. Old data is compressed in such a way that it is represented by its average over a 16 sec. period. A maximum of 8 periods will be kept in memory this way. Previously, normally was used a method that stored a reference sample to which actual data was compared over a predefined stable time period or until out of stability occurred leading to a new sample being set.

If a stable period occurs that is not considerably longer, than the predefined stable time period, it is very likely so, that the old logic should not be able to find it. The A300/310 is a short haul aircraft and the time during cruise is so short that an improved search method for stable data was needed.

# Divergence monitoring

Another new feature will be the "EGT divergence monitoring" (EDM). The purpose of EDM is to have a method that immediately can recognize a sudden gas path damage through its effect on monitored engine parameters. The influence coefficients for a typical twinspool engine show that regardles of performance deterioration, except for fan flow capacity any gas path damage will affect EGT in an increased direction. Therefore during specified conditions EGT of the two engines are compared.

Both engines are operating in the same ambient conditions so that no correction for that has to be done. One engine is corrected for its offset in thrust setting to the reference engine and the resulting difference in EGT between the two engines is compared to a reference difference established first flight every day. If the difference between actual EGT delta and reference EGT delta exceeds a certain value, the one engine with the increased EGT is automatically pointed out as the unhealthy one by the AIDS system.

# Recording Control General

Continuous recording takes place in the following flight modes, engine start, take-off and approach landing. Selective recording is performed in the other flight modes, which means one frame every 100 sec. will be recorded.

# Exceedance recording

20 sec. of pre exceedance data and additional data min 20 sec, max 120 sec. or until the exceedance is passed is recorded.

# Corner points

Corner points are recorded to better define the mission. The corner points are used in groundbased programs for mission analysis with respect to life accounting on critical parts and refined cycle counting on life limited parts. These points are defined as end of climb or start of descent.

Recording of selected frames for oil consumption monitoring

Either during taxi before and after the flight or prior to engine start and after shut down, data can be recorded for the purpose of oil consumption monitoring.

#### Recording of stable data

Above a certain altitude, mach number and in cruise, stable conditions are continuously searched for. When stable conditions are found data is automatically recorded.

# Recording of APU

Every time the APU is started on external or engine power, 16 frames worth of data will be recorded.

# Other planned A310 AIDS applications

As for the current KSSU wide-body aircraft the A310 AIDS will also be used for:

- . verification of satisfactory autoland system operation
- . trouble and incident analysis
- . assessment of service load experience

and the monitoring of:

- . the condition of the auxiliary power unit
- . the braking and anti-skid system
- . aircraft performance deterioration
- . safety limit exceedances

# A310 AIDS ground system

The system proposed for KLM is depicted in figure 10. It shows again the emphasis KSS lays on the function of AIDS as an engineering tool. The AIDS data as recorded on a cassette continuously will update a data-base in the main EDP center where in paralell also data is stored providing information on crew complaints, maintenance actions, etc. This EMS data base provides periodic trend reports, status reports and automatic exceedance reports and is via terminals accessible by line maintenance and engineering

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IRPLANE	BOEI	NG 747	: DC 10	AIRBUS A310
NGINE	PEN JT9D	GE CF6-50E	GE CF6-50C	GE CF6-8041
NGINE PERFORMANCE PARAMETERS:		-	. •	. '
AN ROTOR SPEED	; ; X	: x	i X	: X
ORE ROTOR SPEED	; X	1 X	: X	: X
XHAUST GAS TEMPERATURE (EGT)	; X	; X	: X	: X
VEL FLOW	t X	: X	: X	: X
PC DISCHARGE PRESSURE	: -	: -	: X	; X
PC DISCHARGE TEMPERATURE	: -	: -	: X	: X
PC DISCHARGE PRESSURE	; X	: X	: X	: X
PC DISCHARGE TENPERATURE	: -	-	: X	: X
NGINE PRESSURE RATIO	: X	: -	: -	1 -
ARIABLE STATOR VANE POS. (VSV)	: -		: X	: X
PT INLET PRESSURE	-	: X	: X	: X
IBRATION FAN ROTOR	: X	: X	: X	: X
IBRATION CORE ROTOR	: X	1 X	i X	: X
NGINE OIL QUANTITY	: X	X	i x	: X
NGINE OIL PRESSURE	! -	-	-	: X
NGINE DIL TENPERATURE		-		: x
OWER LEVER ANGLE	x	X	i x	1 X
IGNITION	: x	Î	; x	x
FUEL SHUT-OFF VALVE	: X	i x	i x	X X
BLEED RELATED PARAMETERS:	:	:	:	1
	;	: : X	: X	: ; X
START VALVE POSITION	: X : X		i X	÷ x
PREUNATIC BLEED VALVE POSITION	-	-	i x	: x
ISOLATION VALVES	; -	- X	: x	i î
PACK HODE SELECTOR	•		: X	: x
ENGINE INLET ANTI-ICE	: X	: X : X	: X	i x
JING ANTI-ICE	: X	•	· · ·	i x
VARIABLE BLEEB VALVES	-		x	i x
APU SHUT-OFF VALVE	: <u>-</u>	X		i x
NACELLE TENPERATURE	•	: X	X	Î
BLEED PRESSURE	1 X 1 X	: X	Î	i x
RLEED TEMPERATURE	i A 1			
ANBIENT PARAMETERS:		1	1	
FLIGHT IDENT	i x	X	i x	i x
DATE	1 X	1 X	1 X	; X
GNT	ł X	: X	; X	: X
FLIGHT HODE	t X	: X	1 X	: X
PRESSURE ALTITUDE	: X	: X	: X	: X
TOTAL AIR TEMPERATURE	: X	: X	: X	: X
MACH NUMBER	; X	: X	t X	: X
STEADY STATE IDENT	1 X	: X	: X	: X
AUTO THROTTLE ENGAGED	i X	: X	: X	: X

# EMS PARAMETERS MONITORED ON KSS AIRCRAFT

TABLE 1

#### SAMPLE ENGINE DATA PRINT FROM AIDS ON-BOARD PRINTER

A/C 7	478 1	MODE	2
FLT	488	ALT	4770
BATE	11.05	CAS	46
<b>GH</b> T	1734	MACH	
SCAN	1781	TAT	29
FLCT	1251		
SCAN	1781		
EPR	1.007 1.	012 1.01	7 1.016
NT	13.1 2	3.9 28.	0 28.3
EGT	629.5 45	1.6 408.	8 399.1
¥2	39.9 6	0.3 63.	
<b>F</b> F	153	572 64	7 635
VID I	.0	.0 .	1 .0
VID T	.2	.1 .	3.3
BR.P	.2	.2 .	3.9
WATER	0	0	0 0
PURL	- 1	0 -	1 - 2
PS4	12.4 2	8.3 37.	4 38.1
APU E	GT 460	APU RPH	100.2
DUCT	PRL 30	DUCT PR	R 29
IGH 1	0	0	0 0
IGN 2	0	0	0 0
PN.VA	LVE O	0	0 0
OIL T	45	57 8	5 87
NACT	A 1.6	1.7 1.	9 2.0
MACT	3 2.0	1.7 1.	7 1.7
EAI	0	0	0 0
UAI	0	EPR LIN	1.445
EPR N	OBE 2	APU EGT	L 900
EST L	. 647.7 64	9.9 649.	9 649.9
N1 LI	M 104.2 10	4.2 104.	2 104.2
BR.T	43.6 6	1.0 88.	7 85.1

#### NOTE: IMPENDING NOT START NUMBER 1 ENGINE (AT MEXICO CITY AIRPORT).

TABLE 2

#### TABLE 3

SEVERITY FACTORS PER CITY PAIR & FAILURE MODE

city-		sea-	sea-	sea-	sea-	failure
pair		son1	son2	son3	son4	mode
AMS FRA	7.9	2169	2371	2898	2616	NGV
AMS FRA	7.9	1240	1656	3410	2089	1 BCF
AMS FRA	7.9	0936	1418	3836	2107	1 BOC
AMS FRA	7.9	0190	0350	1440	0571	2 V
AMS FRA	7.9	7465	8643	11800	8673	2 B

# TABLE 4

OUTPUT FROM MAP-LAP

•

PROCESSING DATE 27MAR81 REFERENCE STOMK-R FRANZEN

SORTED BY A/C REG NO

THE FOLLOWING IS A SUMMARY OF THE DAMAGE ACCUMULATED ON EACH PART

		1-			X LIFE	USE	D			I
INST	ENGINE	M	GV	1BCF	190	)C	2	V		28
<b>P</b> 03	NO									
DDL1	563074	5	2	<b>6</b> i	?	3	76		3	-
DDL2	562987	18	8	16 0	19	1	16	2	5	. 9
DDL3	562841	93	.3	17 8	7	1	76		50	
DDL 4	663067	95	.7	37 8	23	9	31	8	23	2
MILAA		05	~	<b>FA</b> 4	•		83	0	26	c
KHA1	562814	95		54 1	8		49		3	
KHA2	662999	7	-	74			47.		39	
KHA3	562750		. 8 . 5	63.7 98	8 11		76	-		.9
KHA4	562909	0	. 3	7 🛡	11	÷	10	2	5	. 7
IGAI		92	-	63 6	2		72		49	
IGA2		50	-	52 4		-	46.		1	-
IGA3	563079	110		23 9	21		95		67	
IGA4	562803	96	5	55 9	31	9	52	5	56	5
ICB1	562927	47	1	14 0	7	Ģ	46	9	55	2
IGB2	585537	35	2	25 6	24	9	27	2	11	2
ICB3	562982	95	3	78 7	7	3	40.	3	4	1
ICB4	585636	58	2	44.5	9	i	48	2	57	9
BUA1	585616	36		18 3	10		43		36	
BUA2	663011	90	_	4.3	4		49		1	
BUAJ	562818	98	2	<b>8</b> 5 2		1	<b>9</b> 5		80	
BUA4	585635	95	.2	19.0	16	1	21	7	ii	
BUB1	662754	94	•	873	•	9	80	4	71	٥
BUB1 BUB2	562979	79	-	41 9	24		32			9
BUB3	562577	91		31 5	18		54		44	
BUB4	562946	97		52 1		1	84		92	
<b>DUD</b> 4	301040		•			•		-		•

# TABLE 5

 PARAMETERS USED IN KLM.SAS
 GPA PROGRAM

 KLM
 CF6-DC10
 GAS
 JT9D-B747

 N1
 N1
 N1

 N2
 N2
 N2

 WF
 WF
 UGT

 FS2C
 PS4

 TT2C
 EPR

 PS3
 TT3

 PT5.4
 VGV #

\* VSV ON SAMPLE ENGINE ONLY

# TABLE 6

PRINT FORMATS / NAMES	
COMPARISON REPORT - PRINT/EVENT - STARLE - EXCCEDANCE - TAKE OFF - CDU REQUESTED	1 2 2 1
TAKE OFF TREND REPORT Cruise trend report	1 1
FAILED ENGINE START REPORT	1
MAINTENANCE REPORT Load/flight control report	1 1

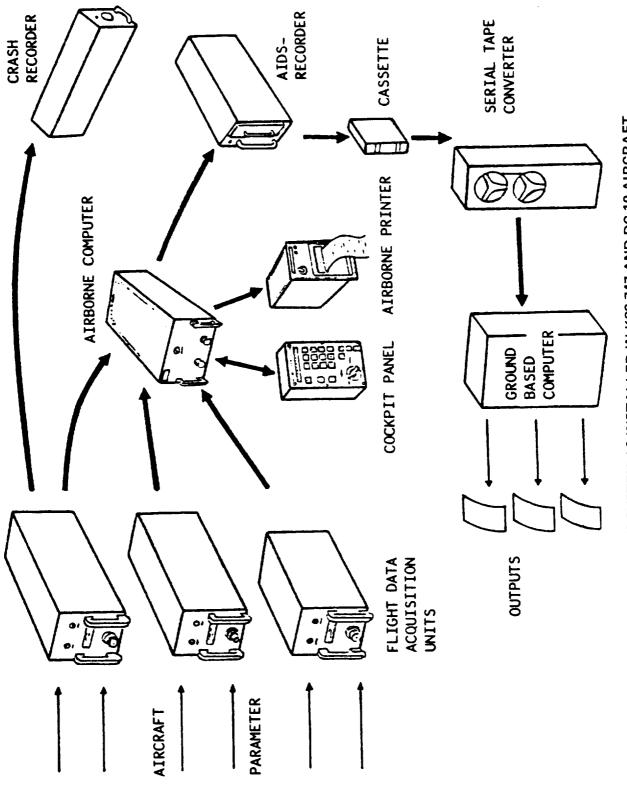
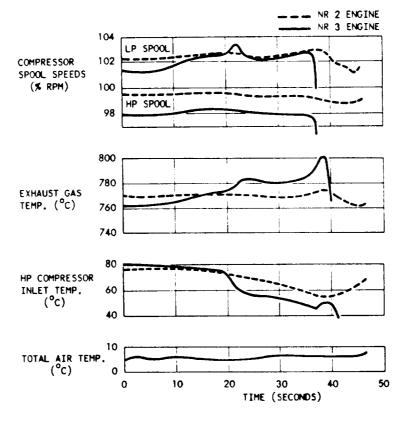


FIG. 1 AIDS SYSTEM AS INSTALLED IN KSS 747 AND DC-10 AIRCRAFT

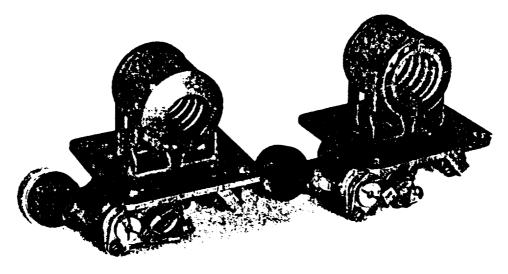
ENGINE ANALYSIS 7478 A Output type : Daily	/C PH-BUB POS 2	2 ENGINE 662879	INSTALLED 10J.		30 PRINT DATE 7 APR	of Phile 4
FLIGHT EXCEEDANCES		ND EXCEEDANCES				
START TREND						GLV
DAY GNT FLT DEP/ARR 302 723 845 CHB/SIN		BLP BLT 0/T PALT 29-3 155 91 80	TAT APUN EGTP 48 101-1 533	NIP N2P IFF	SF F 705	1234
302 1329 845 SIN/MEB 302 2215 845 MEB/SYD 402 455 846 SYD/MEB	15 5 15 14 6 15	35.8 160 35 90 33.7 143 78 483 35.7 144 56 222	23 101.0 458 19 101.0 487 29 100.8 474	14.0 40.6 376 13.9 47.4 345 14.2 47.2 1555	744 717 726	0100
403 707 846 202 1859 845 SPL/DX8 302 217 845 DX8/ 302 723 845 CM8/SIN	18 12 16 000 10 14	35+8 151 91 526 36+2 141 12 -333 33+6 148 85 -73	21 100.8 474 9 101.2 459 17 101.1 460 48 101.1 533	14.2 47.2 \$000 14.5 47.7 415 13.9 46.0 349	8400 825 737	0100 0100 0100
302 1329 845 SIN/MEB 302 2215 845 MEB/SYD	19 6 16 15 5 15	29.3 155 91 80 35.8 160 35 90 33.7 143 78 483	23 101.0 468	14.0 4C.2 2460 14.0 4C.6 376 13.9 47.4 345	705 744 717	0101 0100 0100
402 455 846 SYD/MEH 403 707 846 / 304 1241 641 SPL/JFK 304 2307 642 JFK/SPL	19 6 604	35.7 144 56 222 35.8 151 91 526 35.7 142 16 -296	29 100.8 474 21 100.8 474 13 99.6 469	14.2 47.2 1555 14.2 47.2 0000 22.1 58.6 397	726 **** 762	0100 0100 0101
304 2307 642 JFK/SPL 504 1210 611 SPL/ORD 504 2241 612 ORD/SPL 404 1227 677 SPL/YMX	10 5 15	30.3 143 58 -01 37.5 140 42 -285 36.6 134 61 488 37.7 134 30 -350	12 100-1 435 13 99-6 433 6 99-6 435	13-0 40-0 338 13-9 40-9 401 14-4 47-5 329	735 708 755	0101 0101 0101
404 2336 678 YYZ/YHX 304 1241 641 SPL/JFK 304 2307 642 JFK/SPL	16 5 15 19 6 cat	37.7 134 30 -350 35.2 138 72 835 35.7 142 16 -296 36.3 143 58 -61	12 99.6 424 16 99.6 463 13 99.6 469 12 100.1 435	14+4 47+1 385 13+5 40+4 331 22+1 58+6 397 13+0 40+0 338	793 689 762 735	0101 0110 0101
TAKE-OFF TREND	•••EGTM••2••••4		12 100.1 435			0101
1P52+	X10C -5PLH		× -64	···-2{PR2	BRP68 PS1 0/C0.51 QU/HR	11.5
INITIAL -1 T E 10-FLT -1 T E	•••	D	2 1 2 1	с: с.	8 . O	
AVERAGE .1 T E -1 T E -1 T E	: :	D D D	•2 1	٤:	B 0. B 0.	0
L T E	•••	D		٤:		
202 845 1 T 302 845 1 T E 302 845 T E		D D 2	* 1 *2 1 * 2 1	· · · · · · · · · · · · · · · · · · ·	8 Ŭ 8 • 0	
302 845 1 T E 302 845 I T E 402 846 I T E 403 846 -	• •	D D	2. 1 . 2 1 . 2 1	د . د .	•8 • 0 8 H 8 H	
0 304 - 304 641 - 1 T E 304 642 - 1 T E		B	· · · · · · · · · · · · · · · · · · ·	ç		h
504 611 1 T 504 612 1 T E 404 677 T T			• 2 1 • 1 • 2 1	••••	• 8 • 0 • 8 • 0	
404 677 1 T E 404 678 1 T E 504 678 1 T E			· 2 1 · 2 1 · 2 1	č. c. c.	• • • • • • • • • • • • • • • • • • •	0 0
0 304 - 304 641 -1 T E 304 642 -1 T E		<b>D</b>	2 1	c :		C 0 0 0 A
TAKE-OFF PERFORMANCE					· · •	•••
TAKE-OFF PERFURMANCE		NORMAL NUMBER	OF A/C PACKS IS	3		8 E I
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JEK/SPI	1.411 1.42 818	F/F N1 N2 P54	BPR O/T I-VIB-T	THE PALT TAT CAS	ACP TTO TTA A-NT-8 123	LĀNĞ VIIN
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JEK/SPI	1.411 1.42 818	F/F N1 N2 P54	BPR 0/T 1-VI8-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1	THP PALT TAT CAS 69 -56 11 125 72 -275 8 129 63 491 6 127	TTO TTA A-NT-8 123 0-0 0 1.6 1.8 111 0-0 0 1.7 1.9 111	L Ä W G V I I N 1 0 0 B 1 1 0 B 1 0 0 B
DAY GMT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/ORD 504 2251 3599 612 ORD/SPL 404 1243 1717 677 SPL/YM2 404 2030 2242 677 HYX/YY2 404 2347 1512 678 YY2/YM2 504 146 657 678 YY2/YM2	1.411 1.42 818 1.427 1.44 841 1.378 1.39 781 1.378 1.38 802 1.303 1.39 823 1.364 1.38 802	F/F N1 N2 P54 7664 90.4 94.1 291.7 8135 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 88.0 92.4 280.9 7101 80.6 95.2 270.5 6917 88.6 94.1 266.7 7104 89.3 94.5 272.9	BPR 0/T 1-VIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 88 0.5 1.7 4.7 82 0.5 2.3 4.0 93 0.5 2.2 4.5 92 0.6 2.9	THP         PALT         TAT         CAS           69         -56         11         125           72         -275         8         129           63         491         6         127           64         -35         7         121           71         524         22         134           66         850         15         124	TTO         TTA         A-NT-B         123           0.0         0         1.6         1.8         111           0.0         0         1.7         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111	L Ā W Ġ V I I N 1 0 0 B 1 1 0 B 1 0 0 B 1 0 0 B 1 0 0 B 1 0 0 B
DAY GMT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/DRD 504 2251 3599 612 DRD/SPL 404 1243 1717 677 SPL/YMX 404 2039 2242 677 YHX/Y12 404 2347 1512 678 YHX/Y2 509 146 657 678 YMX/SPL	. 1.411 1.42 818 1.427 1.44 841 1.378 1.39 781 (1.378 1.36 802 1.363 1.39 823 1.364 1.38 802 1.361 1.38 802 1.361 1.38 802	F/F N1 N2 P54 7664 90.4 94.1 291.7 8135 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 89.6 95.2 270.5 6017 86.6 95.2 270.5	BPR 0/T 1-YIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 88 0.6 1.7 4.7 80 0.5 1.7 4.7 93 0.5 2.2 4.5 92 0.6 2.9 4.5 92 0.4 2.7	THP         PALT         TAT         CAS           69         -56         11         125           72         -275         8         129           63         491         6         127           64         -35         7         121           71         524         22         134           66         850         15         124	TTO         TTA         A-NT-B         123           0.0         0         1.6         1.8         111           0.0         0         1.7         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111	L Ā W Ġ V I I N 1 0 0 B 1 0 0 8 1 0 0 8 1 0 0 8
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/DRD 504 2251 3599 612 ORD/SPL 404 1243 1717 67 SPL/YHX 404 2309 2242 077 YHX/YHX 404 2347 1512 678 YHX/SPL 504 146 657 678 YHX/SPL 304 1257 940 641 SPL/JFK 304 2321 1060 642 JFK/SPL CRUISE TREND	. 1.411 1.42 616 1.427 1.44 641 1.378 1.39 781 1.378 1.38 602 1.378 1.38 602 1.364 1.38 602 1.364 1.38 613 1.364 1.38 613 1.410 1.41 818 1.411 1.42 818	F/F N1 N2 P54 7664 90.4 94.1 291.7 8136 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 88.0 92.4 280.9 7101 86.6 95.2 270.5 6917 88.6 94.1 266.7 7104 80.5 94.1 293.6 7010 70.5 64.1 293.6 7664 90.4 94.1 291.7	BPR 0/T 1-YIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 88 0.6 1.7 4.7 80 0.5 1.7 4.7 93 0.5 2.2 4.5 92 0.6 2.9 4.5 92 0.4 2.7	THP         PALT         TAT         CAS           69         -56         11         125           72         -275         8         129           63         +91         6         127           64         -335         7         121           71         524         22         134           66         850         15         126           67         409         17         125           68         -281         10         134	TTO         TTA         A-NT-B         123           0.0         0         1.6         1.8         111           0.0         0         1.7         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.9         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.8         111           0.0         0         1.6         1.9         111	L A W G V I I N 1 0 0 B 1 0 0 B
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/DRD 504 2251 3599 612 ORD/SPL 404 1243 1717 67 SPL/YHX 404 2309 2242 077 YHX/YHX 404 2347 1512 678 YHX/SPL 504 146 657 678 YHX/SPL 304 1257 940 641 SPL/JFK 304 2321 1060 642 JFK/SPL CRUISE TREND	. 1-411 1.42 616 1.427 1.44 841 1.378 1.39 781 1.378 1.38 802 1.364 1.38 802 1.371 1.38 813 1.311 1.38 813 1.410 1.41 818 1.411 1.42 818 	F/F N1 N2 P54 7664 90.4 94.1 291.7 8135 91.0 93.6 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 86.6 95.2 270.5 6917 86.6 94.1 266.7 7104 80.3 94.5 272.9 NO TO-DATA 7710 90.5 94.1 291.7 6 -212	BPR 0/T 1-YIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 88 0.6 1.7 4.7 80 0.5 1.7 4.7 93 0.5 2.2 4.5 92 0.6 2.9 4.5 92 0.4 2.7	THP         PALT         TAT         CAS           69         -56         11         125           72         -275         8         129           63         -901         6         127           64         -335         7         121           71         524         2         134           66         850         15         124           67         469         17         125           68         -281         10         134           69         -56         11         125	TTO TTA A-NT-B 123 0.0 0 1.6 1.8 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.6 1.8 111	L A W G V I I N 1 0 0 B 1 1 0 6 1 0 0 8 1 0 0 8
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/ORD 504 2251 3599 612 ORD/SPL 404 1243 1717 677 SPL/MX 404 203 2242 677 HVX/Y12 404 2347 1512 678 YY2/MX 504 1265 7618 YY2/MX/SPL 0 304 XXX/ 304 1257 940 641 SPL/JFK 304 1257 940 641 SPL/JFK/SPL CRUISE TREND Y1812 IN111AL .I T	. 1-411 1.42 616 1.427 1.44 841 1.378 1.39 781 1.378 1.38 802 1.364 1.38 802 1.371 1.38 813 1.410 1.41 818 	F/F N1 N2 PS4 7664 90.4 94.1 291.7 8136 91.0 93.8 298.5 7032 87.7 82.7 276.4 7377 86.0 92.4 280.9 7101 80.6 95.2 270.5 6917 86.6 94.1 266.7 7104 80.3 94.5 272.9 NG TO-DATA 7710 90.4 94.1 291.6 7664 90.4 94.1 291.7 6 -212 100KG/HH F .	BPR         0/T         I-VIB-T           4.9         91         0.6         2.3           4.6         84         0.6         2.1           4.7         88         0.5         1.7           4.7         82         0.5         1.7           4.7         82         0.5         2.3           4.0         93         0.5         2.2           4.5         92         0.6         2.9           4.5         92         0.4         2.7           5.0         84         0.6         2.4           4.9         91         0.6         2.3	THP         PALT         TAT         CAS           60         -56         11         125           72         -275         8         120           63         901         6         127           63         901         6         127           71         525         7         121           60         850         15         124           67         409         17         125           68         -281         10         134           69         -56         11         125	ТТО ТТА А-NT-В 123 0.0 0 1.6 1.8 111 0.0 0 1.7 1.9 111 0.0 0 1.6 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.6 1.8 111 0.0 0 1.8 18 18 18 18 18 18 18 18 18 18 18 18 18	L À W G V I I N 1 0 0 B 1 1 0 8 1 1 0 8 1 0 0 8
DAY GHT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/ORD 504 2251 3509 612 ORD/SPL 404 1243 1717 677 SPL/MX 404 203 2242 677 HYX/YYZ 404 2347 1512 678 YYZ/HX 509 146 657 678 YMX/SPL 304 1257 940 641 SPL/JFK 304 2321 1060 642 JFK/SPL CRUISE TRENO 41812 1P5	. 1-411 1.42 616 1.427 1.44 841 1.378 1.39 781 1.378 1.38 602 1.378 1.38 602 1.371 1.38 613 1.3104 1.38 613 1.310 1.41 618 1.411 1.42 818 EGT24. X10C -21. X1 E. E. E. E. E. E.	F/F N1 N2 P54 7664 90.4 94.1 291.7 8135 91.0 93.6 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 80.6 95.2 270.5 6917 86.6 94.1 266.7 7104 80.3 94.5 272.9 NO TO-DATA 7710 90.5 94.1 291.7 6 -21 100KG/HR F . F .	BPR         0/T         I-VIB-T           4.9         91         0.6         2.3           4.6         84         0.6         2.1           4.7         88         0.5         1.7           4.7         82         0.5         1.7           4.7         82         0.5         2.3           4.0         93         0.5         2.2           4.5         92         0.6         2.9           4.5         92         0.4         2.7           5.0         84         0.6         2.4           4.9         91         0.6         2.3	HHP         PAL T         TAT         CAS           69         -56         11         125           72<-275	TTO TTA A-NT-8 123 0-0 0 1.6 1.8 111 0-0 0 1.7 1.9 111 0-0 0 1.6 1.9 111 0-0 0 1.6 1.9 111 0-0 0 1.6 1.8 111 0-0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	L A W G V I I N 1 0 0 B 1 0 0 B
DAY GMT SCAN FLT DEP/ARR 304 2321 1060 G42 JFK/SPL 504 1223 1897 611 SPL/DRD 504 2251 3599 612 ORD/SPL 404 2030 2242 677 WK/YY2 404 2347 1512 678 YY2/WK 504 146 657 678 YY2/WK 304 1257 940 641 SPL/JFK 304 1257 940 641 SPL/JFK 304 2321 1000 642 JFK/SPL CRUISE TREND Y1812 INITIAL I T 10-FL1 I T AVEHAGE I T 1 1 DAILY FLTS 403 840.	. 1-411 1.42 818 1.427 1.44 841 1.378 1.39 781 1.378 1.38 802 1.364 1.38 802 1.371 1.38 813 1.410 1.41 818 	F/F N1 N2 P54 7664 90.4 94.1 291.7 8136 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 80.6 95.2 270.5 6917 86.6 94.1 266.7 7104 80.3 94.5 272.9 NG TO-DATA 7710 90.5 94.1 293.6 7664 90.4 94.1 291.7 6 -21 100KG/HH F . -	BPR 0/T 1-VI8-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 82 0.5 1.7 4.7 82 0.5 2.3 4.6 92 0.6 2.9 4.5 92 0.4 2.9 5.0 84 0.6 2.4 4.9 91 0.6 2.3 N/11.22 x -21 1	THP         PALT         TAT         CAS           69         -56         11         125           72         -275         8         129           63         901         6         127           64         -335         7         121           71         524         22         134           66         850         15         124           67         409         17         125           68         -281         10         134           69         -56         11         125	TTO TTA A-NT-8 123 0-0 0 1.6 1.8 111 0-0 0 1.7 1.9 111 0-0 0 1.6 1.9 111 0-0 0 1.6 1.9 111 0-0 0 1.6 1.8 111 0-0 0 0 1.6 1.8 111	L A W G V I I N 1 0 0 B 1 0 0 B
DAY GMT SCAN FLT DEP/ARR 304 2321 1060 642 JFK/SPL 504 1223 1897 611 SPL/ORD 504 2251 3599 612 ORD/SPL 404 203 2242 677 YML/YM2 404 203 2242 677 YML/YM2 404 2347 1512 678 YM2/YM2 504 1265 040 641 SPL/JFK 304 1257 040 641 SPL/JFK 304 2321 1060 642 JFK/SPL CRUISE TREND VIB2 INITIAL I T 10-FL1 I T 10-FL3 I T 0 JL FLTS 403 840 202 845 1000 1000 1000 1000 1000 1000 1000 10	. 1-411 1.42 616 1.427 1.44 841 1.378 1.39 781 1.378 1.38 602 1.378 1.38 602 1.371 1.38 613 1.3104 1.38 613 1.310 1.41 618 1.411 1.42 818 EGT24. X10C -21. X1 E. E. E. E. E. E.	F/F N1 N2 P54 7664 90.4 94.1 291.7 8135 91.0 93.6 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 80.6 95.2 270.5 6917 86.6 94.1 266.7 7104 80.3 94.5 272.9 NO TO-DATA 7710 90.5 94.1 291.7 6 -21 100KG/HR F . F .	BPR 0/T 1-VI8-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 82 0.5 1.7 4.7 82 0.5 2.3 4.6 92 0.6 2.9 4.5 92 0.4 2.9 5.0 84 0.6 2.4 4.9 91 0.6 2.3 N/11.22 x -21 1	HHP         PAL T         TAT         CAS           69         -56         11         125           72<-275	TTO TTA A-NT-8 123 0.0 0 1.6 1.8 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.7 1.9 111 0.0 0 1.6 1.8 111 0.0 0 1.8 1.	L A W G V I I N 1 0 0 B 1 0 0 B
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DAY GMT SCAN FLT DEP/ARR 304 2321 1060 G42 JFK/SPL 504 1223 1897 G11 SPL/0RD 504 2251 3590 G12 OPD/SPL 404 1243 1717 G7 SPL/MX 509 146 057 G78 YYL/YWX 509 146 057 G78 YYL/YWX 509 146 057 G78 YYL/YWX 304 2321 1060 G42 JFK/SPL CRUISE TREND Y1812 10-FL1 I T 10-FL1 I T 10-FL1 I T AVEHAGE I T 10 J J 02 845 J 302 845 J 302 845 J 303 845 J 304 641 J 304 677 SCAN FLT DEP/ARR 304 653 B 1600 G11 SPL/ORD 504 653 B 1600 G11 SPL/ORD	E	F/F N1 N2 PS4 7664 90.4 94.1 291.7 8136 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 80.6 95.2 270.5 6917 86.6 94.1 266.7 710 80.3 94.5 272.9 NO TO-DATA 7710 90.4 94.1 291.7 7664 90.4 94.1 291.7 7664 90.4 94.1 291.7 F. F. F. F. F. F. F. F. F. F.	BPR Q/T 1-VIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 82 0.5 2.3 4.0 92 0.6 2.9 4.5 92 0.4 2.7 5.0 84 0.6 2.4 4.9 91 0.6 2.3 N/11.2 x -21 1 1 1 1 1 1 1 1 1 1 1 1 1	1HF       PAL T       TAT       CAS         60       -56       11       125         72       -275       8       120         63       901       6       127         64       -335       7       121         71       524       22       134         66       850       15       126         67       409       -50       11       125         68       -281       10       134       69       -50       11       125         7       -2	TTO       TTA       A-NT-B       123         0-0       0       1.6       1.8       111         0-0       0       1.7       1.9       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.9       111         0       0       1.6       1.8       111         0 <t< td=""><td>C A W G V I I N I O B I O O D D O D I O O O D I O O O D I O O O D I O O O O O O O O O O O O O O O O O O O</td></t<>	C A W G V I I N I O B I O O D D O D I O O O D I O O O D I O O O D I O O O O O O O O O O O O O O O O O O O
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DAY GMT SCAN FLT DEP/ARR 304 2321 1000 GA2 JFK/SPL 504 1223 1897 G11 SPL/ORD 504 2251 3590 G12 OPD/SPL 404 1243 1717 G7 SPL/MX/SPL 504 1243 1717 G7 SPL/MX/SPL 504 12657 940 G41 SPL/JFK 304 1257 940 G41 SPL/JFK 304 2321 1000 G42 JFK/SPL CRUISE TREND 404 201 244 17 10-FL1 I I T 404 64 11 T 10-FL1 I I T 403 840 - 202 845 - 304 641 -1 T 304 641 -1 T 304 641 -1 T 304 677 - 403 642 - 504 617 -1 T 403 642 - 504 617 -1 T 404 678 - 0 304 - 304 641 -1 T 304 678 - 0 304 -	E - E - E - E - E - E - E - E - E - E -	F/F N1 N2 PS4 7664 90.4 94.1 291.7 8136 91.0 93.8 298.5 7032 87.7 92.7 276.4 7377 86.0 92.4 280.9 7101 80.6 94.1 266.7 7104 80.3 94.5 272.9 NO TO-DATA 7710 90.5 94.1 293.6 7664 90.4 94.1 291.7 6 F	BPR 0/T 1-VIB-T 4.9 91 0.6 2.3 4.8 84 0.6 2.1 4.7 82 0.5 2.3 4.6 92 0.6 2.9 4.5 92 0.4 2.9 4.5 92 0.4 2.9 5.0 84 0.6 2.4 4.9 91 0.6 2.3 N/11 1 1 1 1 1 1 1 1 1 1 1 1 1	IHP PALT TAT CAS         60       -56       11       125         72       -275       8       120         63       901       6       127         64       -335       7       121         71       524       22       134         66       850       15       124         67       409       -50       11       125         68       -281       10       134       69       -50       11       125         7       2       -2	TTO       TTA       A-NT-B       123         0-0       0       1.6       1.9       111         0-0       0       1.7       1.9       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.8       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.9       111         0-0       0       1.6       1.9       1.1         0       0       1.6       1.9       1.9         0 <t< td=""><td>L À W G V I I N I O O B I O O D I O O B I O O B I O O B I O O O B I O O D I O O O O O O O O O O O O O O O O O O O</td></t<>	L À W G V I I N I O O B I O O D I O O B I O O B I O O B I O O O B I O O D I O O O O O O O O O O O O O O O O O O O

FIG. 2 AIDS LONG TERM TREND JT9D ENGINE









With Rainshield

4

# **Standard Sensor**

FIG. 4 CIT SENSOR

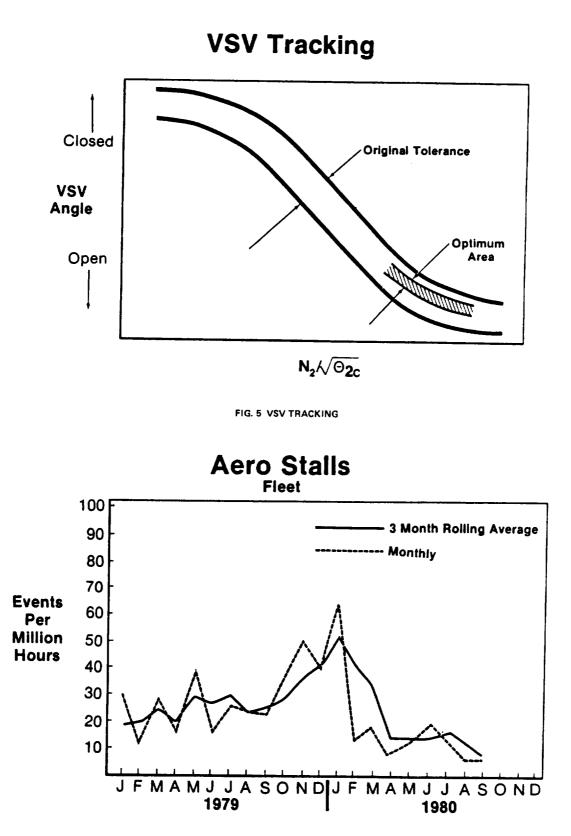


FIG. 6 CF6 AERO STALLS

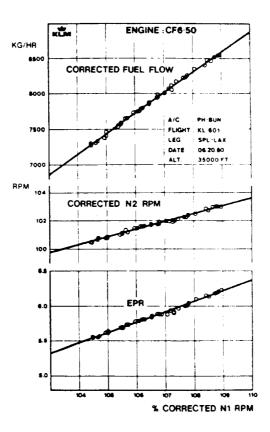


FIG. 7 AIDS CF6 GAS GENERATOR CURVES

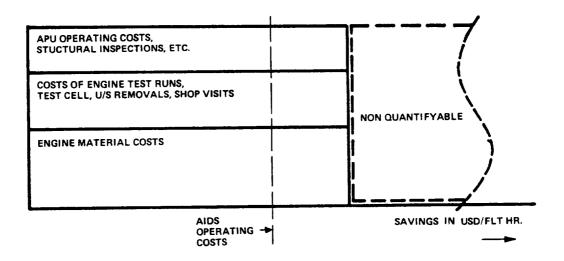


FIG. 8 PROJECTED A310 AIDS RETURN ON INVESTMENT

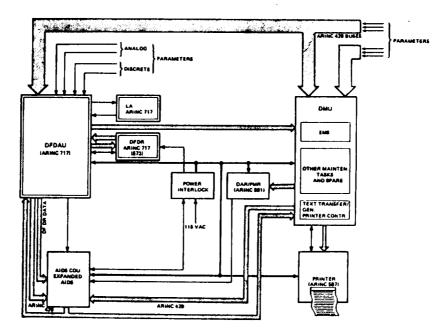


FIG. 9 AIRBUS A310 AIDS SYSTEM DIAGRAM

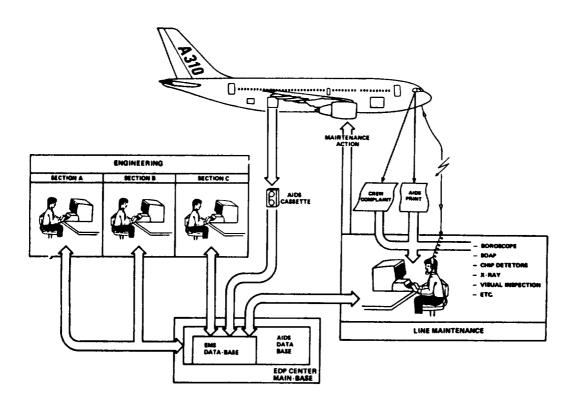


FIG. 10 A310 AIDS GROUND SYSTEM

LIFE USED FOR FIRST TURBINE BLADE

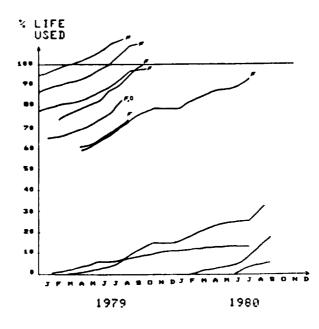


FIG 11

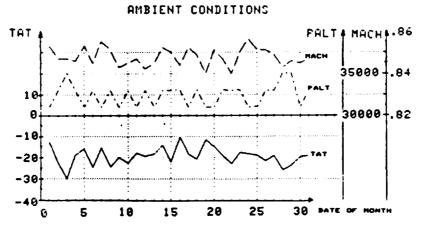
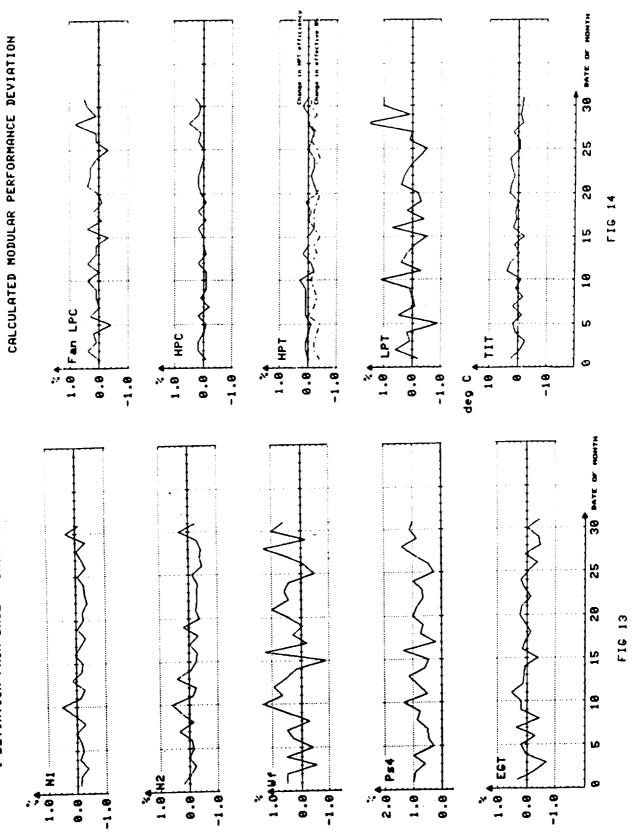


FIG 12





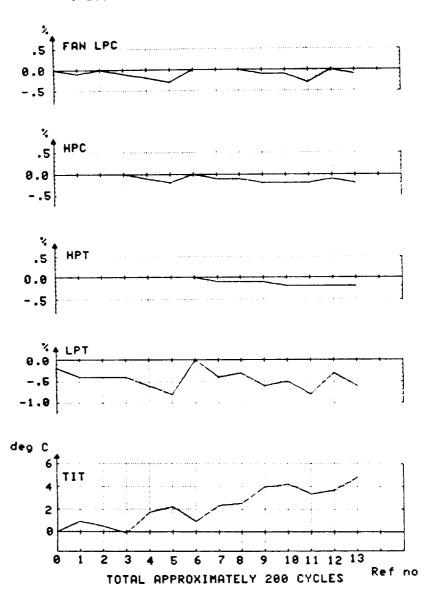


FIG 15