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**Thickness-dependent thermal properties of amorphous insulating thin films  
measured by photoreflectance microscopy**

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**Abstract**

In this work, we report on the measurement of the thermal conductivity of thin insulating films of SiO<sub>2</sub> obtained by thermal oxidation, and Al<sub>2</sub>O<sub>3</sub> grown by atomic layer deposition (ALD), both on Si wafers. We used photoreflectance microscopy to determine the thermal properties of the films as a function of thickness in the 2 nm to 1000 nm range. The effective thermal conductivity of the Al<sub>2</sub>O<sub>3</sub> layer is shown to decrease with thickness down to 70% for the thinnest layers. The data were analyzed upon considering that the change in the effective thermal conductivity corresponds to an intrinsic thermal conductivity associated to an additional interfacial thermal resistance. The intrinsic conductivity and interfacial thermal resistance of SiO<sub>2</sub> were found to be equal to 0.95

W/m.K and  $5.1 \times 10^{-9}$  m<sup>2</sup>K/W respectively; those of Al<sub>2</sub>O<sub>3</sub> were found to be 1.56 W/m.K and  $4.3 \times 10^{-9}$  m<sup>2</sup>K/W.

### **Keywords**

Thermal conductivity, thermal diffusivity, interfacial thermal resistance, frequency-domain photorefectance, Atomic layer deposition

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## 1. Introduction

Thermal and electronic conductivities are strongly correlated in most materials. However, many applications demand the maximization of one of these properties while minimizing the other. In microelectronics for instance, good electrical insulation is essential (capacitors, interconnects), but low-k dielectrics usually come with poor thermal conductivity, hampering heat dissipation. Conversely, high electrical conductivity and thermal insulation are crucial for thermoelectric conversion, in order to avoid Joule heating while preserving the temperature gradient [1, 2]. Nanostructured materials offer a new way to act on these antagonistic requirements, since nanoscale thermal properties can significantly differ from bulk values [3, 4]. A lot of attention has been focused recently on understanding the underlying physics, like phonon scattering [5] and heat transport phenomena [6, 7].

In this paper, we investigate the thermal properties of two electrical insulators,  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  thin films.  $\text{SiO}_2$  is essential to microelectronics and other industrial applications. It has therefore received a lot of attention, and its thermal properties are relatively well known. Some research groups have studied the thermal conductivity of  $\text{Al}_2\text{O}_3$  amorphous thin films [8-11], but the evaluation of their interfacial thermal resistances is still very incomplete [12].  $\text{Al}_2\text{O}_3$  amorphous thin films are promising, since they can reduce electronic recombination losses in solar cells by the passivation of silicon surfaces, thus enabling higher efficiency [13]. Moreover, thin amorphous  $\text{Al}_2\text{O}_3$  films are good thermal insulators as well as excellent moisture barriers [14] that can be fabricated at low temperatures [15, 16], making them highly desirable in electronic components [17].

A broad range of experimental methods is available in order to determine the thermal properties of materials. They essentially differ in their heat generation process (optical, Joule,...), in the property which is probed (temperature of the surface, sample or air, acoustic waves, etc...), and in the probing mechanism (refractive index, thermal emission, interferometry, fluorescence, electrical resistance...). Temporally, various strategies have also been developed: steady state, transient or modulated. Several reviews of thin films characterization techniques have been proposed [18, 19]. Among these techniques, modulated photoreflectance microscopy has the advantages of being contactless, non-destructive and, owing to the high spatial resolution of visible light microscopy, allows measurements on relatively small samples ( $>10\ \mu\text{m}$ ). It is based on the generation of thermal “waves” by intensity-modulated optical excitation. This technique was first proposed by A. Rosencwaig et al. [20], and then widely used to determine the thermal properties of bulk materials [21, 22], grains [23], coatings and thin films [24, 25]. In this work, the frequency domain photoreflectance method is used to study the effect of thickness on the thermal properties of amorphous  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  thin films. The method requires the deposition of a gold layer to opacify the surface, but is well adapted to this kind of study, where different nanoscale layers have to be distinguished. A 3D heat diffusion model was used to extract the thermal properties of each material independently [22].

## 2. Experimental

The  $\text{SiO}_2$  thin films with different thicknesses were fabricated by Kelvin Nanotechnology Ltd (KNT), in collaboration with Glasgow University. The starting material is a thick layer of  $\text{SiO}_2$  grown by thermal oxidation on a p-type Si wafer. Repeated photolithography steps, followed by timed hydrofluoric acid (HF) etching, were performed to obtain the required thicknesses of 12,

30, 65, 145, 237, 530 and 950 nm, as depicted in Fig. 1 a). The layer thickness was measured by white light interferometry [26].

The studied  $\text{Al}_2\text{O}_3$  samples were fabricated by Picosun using a Picosun<sup>TM</sup> ALD reactor. ALD is a powerful method to grow fully conformal, pinhole-free layers with atomic accuracy [26]. This is based on the self-terminating nature of gas-solid reactions taking place at the sample surface. The studied thin films were grown on silicon wafer with a 10-14  $\mu\text{m}$  n-type epilayer of resistivity 3-6 ohm.cm and a native  $\text{SiO}_2$  layer (thickness of approximately 1.5 nm). The values of the obtained thicknesses (2, 5, 9.5, 24, 48, 98, 152, 196, 490 nm) were measured by ellipsometry [28], as shown in Fig. 1 b).

The frequency-domain photoreflectance microscopy is one of the most convenient photothermal techniques to measure the thermal diffusivity of solid materials. It uses an intensity-modulated green laser ( $\lambda=532$  nm) focused by an optical microscope onto the surface of the sample [21, 29]. The modulated beam excites thermal “waves”, and the resulting distribution of the surface temperature modulation is read by a second probe laser ( $\lambda =670$  nm) using the temperature dependence of the reflectivity, which is proportional to temperature in a first approximation, and depends on the nature of the reflecting material. The amplitude and the phase of the modulated photoreflectance signals are extracted by lock-in detection and recorded as a function of the distance between the two spots. This method requires a good absorption of the heating laser, for efficient thermal wave generation, and an efficient reflection of the probe laser. In the case of transparent materials, an opaque and reflective transducing surface is therefore always needed in order to create and probe the thermal waves. In our case, the  $\text{Al}_2\text{O}_3$  and  $\text{SiO}_2$  samples were coated with a 100 nm thick gold layer. The measurements were performed at room temperature, with an excitation frequency of 150 kHz. The heat diffusion theoretical model depends on an effective

diameter, which is obtained by a convolution of the heating laser spot and the probing laser spot. This effective diameter was found to be 3  $\mu\text{m}$ , a value which can be either determined by convolution of the Airy discs associated to the laser wavelengths and the numerical aperture of the objective, or by fitting measurements obtained on a known sample.

### 3. Results and Discussion

The thermal diffusivity  $D$  of an optically and thermally thick, isotropic, bulk material can be straightforwardly extracted from the slope  $\frac{dP}{dx} = \sqrt{\frac{\pi f}{D}}$  of the phase lag  $P$  of the surface temperature rise with respect to the excitation at a distance  $x$  from the excitation, where  $f$  is the excitation frequency [30]. For a multilayered sample, there is no such simple relation, since the phase slope  $\frac{dP}{dx}$  is then a function of the diffusivities and conductivities of the different layers [29]. However, the surface temperature modulation can be calculated using a thermal quadrupole formalism [25]. The thermal diffusivity and conductivity of one layer of known thickness is therefore obtained by using this model and determining the thermal properties which best fit the measured amplitude and phase of the surface temperature modulation. The samples are considered homogenous laterally over the studied region (40  $\mu\text{m}$ ), and the anisotropy of the diffusion coefficient, i.e. differences between the in-plane and through-plane diffusion coefficients,  $D_{//}$  and  $D_{\perp}$  respectively, are neglected. Moreover, the diffusivity and conductivity are not determined independently, but rather upon assuming that the ratio of thermal conductivity  $k$  to thermal diffusivity  $D$  is constant  $\frac{k}{D} = \rho C = \text{cst}$ , with  $\rho$  the density and  $C$  the specific heat of the bulk material, taken from the literature. In some cases, e.g. when the thermal contrast and the measurement Signal to Noise Ratio are sufficient, the thermal parameters of up to two media [29] can be obtained simultaneously. However, because the number of variables increases with each

additional layer, a reliable determination of the thermal properties of a given layer requires the precise knowledge of the thicknesses and thermal properties of the other layers. Therefore, the thermal properties of the different layers composing the samples were determined in three steps, depicted in Fig. 2:

- Step 1: A gold layer was deposited simultaneously on glass and on the studied samples. Since its thermal properties are well known, and because it is thermally insulating, glass is an appropriate choice to study the properties of the 100 nm gold layer which essentially drive the surface temperature.
- Step 2: An identical gold layer was deposited on a bare Si substrate, to characterize the thermal properties of the substrate.
- Step 3: An identical substrate, supporting the layers to be characterized and the same gold layers was fabricated. Using the properties obtained in steps 1 and 2, the thermal properties of the relevant layer can finally be measured.

In two separate runs, using different adhesion layers and under different conditions, gold was deposited on SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> thin films along with a glass reference sample for each run. On top of the SiO<sub>2</sub> layer, we measured a thermal diffusivity  $D = 9.6 \times 10^{-5} \text{ m}^2/\text{s}$  and a thermal conductivity  $k = 238 \text{ W/m.K}$  for the gold layer. The density of gold and its specific heat were taken from literature [31] :  $19.3 \times 10^3 \text{ kg/m}^3$  and  $128 \text{ J/kg.K}$  respectively. On top of the Al<sub>2</sub>O<sub>3</sub> layers, the measured thermal diffusivity and conductivity of gold were found to be  $D = 6.2 \times 10^{-5} \text{ m}^2/\text{s}$  and  $k = 155 \text{ W/m.K}$  respectively. The same gold is deposited simultaneously over all samples of the same kind; thus it is reasonably assumed that the gold coating measured in step 1 has identical properties over the same series.



Similarly, a precise substrate characterization was then obtained by taking measurements on substrates coated simultaneously with the same gold film (step 2). The substrate for both series is silicon, and the ratio  $\frac{k}{D} = \rho C$  was kept constant [32] at  $16.7 \times 10^5 \text{ J/m}^3\text{K}$ , following the Dulong-Petit law. The substrate used for all the  $\text{SiO}_2$  samples is a p-type (boron) doped silicon with 0.001-0.01 Ohm.cm resistivity. Its thermal properties were found to be  $D = 4.5 \times 10^{-5} \text{ m}^2/\text{s}$  and  $k = 75 \text{ W/m.K}$ . The substrate for the  $\text{Al}_2\text{O}_3$  films, as described above, was not vertically homogeneous since the silicon wafers comprise an epilayer of 10-14  $\mu\text{m}$  n-doped Si. However, at our excitation frequency  $f = 150 \text{ kHz}$ , the penetration depth of thermal waves is given by  $\mu = \sqrt{\frac{D}{\pi f}}$  = 13  $\mu\text{m}$ . Therefore, thermal waves do not significantly penetrate the underlying undoped silicon, and this substrate can be safely considered as homogeneous, semi-infinite, n-doped silicon. The obtained substrate thermal properties are  $D = 8 \times 10^{-5} \text{ m}^2/\text{s}$  and  $k = 135 \text{ W/m.K}$ . Finally (step 3), the properties of each material was determined using the parameters of the appropriate gold coating and substrate obtained in step 1 and 2.

Let us consider  $\text{SiO}_2$ , a well-studied material, in order to allow comparison with existing measurements. The reported values of micrometric thick films thermal conductivity essentially depend on the deposition technique, and range from 1 to 1.4  $\text{W/m.K}$  for  $\text{SiO}_2$  grown by thermal oxidation [33-35]. Fig. 3 shows the obtained values of the effective thermal conductivity as a function of thickness. Typical examples of the measurements and theoretical fits quality are shown in the next section. As we scale down thickness ( $< 100 \text{ nm}$ ), thin

films can be modeled as thermal resistances. In other words, the theoretical fit is mainly affected by the value of  $l.k^{-1}$ , where  $l$  is the thickness. In this case, the change in the thermal properties only affects the amplitude and not the phase, which is dictated by the diffusivity. The inset in Fig. 3 shows the fit of the thermal conductivities of these thin layers as a function of thickness  $l$ , by a resistance model [35]:

$$l.k^{-1} = l.k_i^{-1} + R_{th} \quad (1)$$

where  $l.k^{-1}$  is the total thermal resistance,  $R_{th}$  is the additional interfacial thermal resistance (metal/film and film/substrate interfaces),  $k_i$  is the intrinsic thermal conductivity which stands for the upper limit of the effective thermal conductivity reached for the thickest layers. The best fit corresponds to an intrinsic thermal conductivity of  $(0.95 \pm 0.03)$  W/m.K, a value identical (within 5%) to the one reported by Govorkov et al. [33]. We noticed higher discrepancies (30%) compared to values reported by the  $3\omega$  method [34] and some similar techniques [35]. These discrepancies could be related to the heat generation/collection method. Photorefectance excites a sub- $\mu\text{m}$  circular region and probes laterally, whereas resistors used to excite and probe in the  $3\omega$  method are usually tens of micrometers wide. While both methods probe a combination of in-plane and through-plane thermal properties, photorefectance is comparatively more sensitive to in-plane thermal properties, and the  $3\omega$  method to through-plane properties. Moreover, it is important to point out that even for the thickest layer, 1  $\mu\text{m}$ , the value of bulk fused silica (1.38 W/m.K) [37] may not be attained. Since thermal transport across multilayer systems is influenced by the thermal boundary resistance, it is important to extract this quantity. In the current study, we deduce the influence of the two interfaces through the best fit of the resistance model (equation 1). This resistance was found to be  $(5.1 \pm 1) \times 10^{-9}$   $\text{m}^2\text{K/W}$ , approximately 7 times smaller than the values reported by Chien et al.[35]. The uncertainties on  $k_i$  and  $R_{th}$  are the

standard deviation errors on the fitting parameters. For the thicker layers ( $>100$  nm), the penetration depth, which is in this case equal to  $1.3\ \mu\text{m}$ , becomes comparable to the layer thickness; in this range, the thermal resistance model does not hold.

Fig. 4 shows the results obtained over 9 samples with different  $\text{Al}_2\text{O}_3$  layer thicknesses. Fig. 4a) represents the amplitudes (log scale) and Fig. 4b) the phases of the photorefectance signals versus the distance from the heating point. The symbols are the experimental results, and solid lines are the corresponding best fits. As can be noticed, each layer thickness yields a measurement which can be clearly distinguished, owing to the fact that  $\text{Al}_2\text{O}_3$ , like  $\text{SiO}_2$ , is a very insulating material, strongly contrasting with the silicon substrate and gold layer. Each of these measurements is accurately fitted using the parameters measured for the substrate and the gold coating, with the thermal properties of  $\text{Al}_2\text{O}_3$  as the only variable parameters. In order to avoid any rough assumptions on the native oxide layer (approx.  $1.5$  nm) found on the Si substrate and the possible presence of a thermal boundary resistance, we used a single equivalent layer with an effective thermal conductivity to describe the oxide and the resistance. The values of  $\text{Al}_2\text{O}_3$  effective thermal conductivity and thermal diffusivity used to fit the measurements are shown in Fig. 5 as a function of the layer thickness. The ratio  $\frac{k}{D} = \rho C = 2.2 \times 10^6$  J/m<sup>3</sup>K was kept constant upon fitting all the measurements, with  $\rho$  the density of amorphous  $\text{Al}_2\text{O}_3$  and  $C$  the specific heat taken from literature [16] to be  $2.95 \times 10^3$  kg/m<sup>3</sup> and  $755$  J/K.kg, respectively. The precision on the reported values of thermal conductivity and diffusivity is presented in Fig. 5 by error bars. The error bars were determined by varying the fitting parameters until all measurement points, both in amplitude and in phase, were comprised between curves corresponding to  $D \pm \Delta D$  or  $k \pm \Delta k$ . These values of  $\Delta D$  or  $\Delta k$  were then adopted as measurement uncertainties. The values of the effective thermal conductivity were found to vary between  $1.65$  and  $0.465$  W/m.K, and those of the

diffusivity between  $(0.74 \text{ and } 0.22) \times 10^{-6} \text{ m}^2/\text{s}$  depending on the thickness. One can note a strong drop in the thermal conductivity of  $\text{Al}_2\text{O}_3$  below 20 nm, which could possibly be caused by mechanical stress in the first few atomic layers. Indeed, optical refractive index measurements in sub-50 nm films [38] have shown that annealing, which precisely relieves this stress, has a strong influence on these properties, and could similarly impact the thermal properties. However, between 98 nm and 2 nm layer thickness,  $\text{Al}_2\text{O}_3$  films behave as thermal resistances, and we used the model expressed in equation (1), as shown in the inset in Fig. 5. Note that we retrieve a value for the intrinsic thermal conductivity of  $k_i = (1.56 \pm 0.08) \text{ W/m.K}$ , which is close to the value of effective thermal conductivity of the thickest layer. The thermal resistance was found to be equal to  $(4.26 \pm 0.67) \times 10^{-9} \text{ m}^2\text{K/W}$ , which corresponds to the effective resistance of the two interfaces. Let us remark that the analysis of the experimental data based on Fourier's heat equation seems to stay reasonable despite the few-nanometers thicknesses involved. We could not identify clearly a further reduction of the thermal conductivity, as would be the case if ballistic transport were happening, for the smallest thicknesses within our experimental accuracy. This could be due to the fact that diffusion still holds at such scale for amorphous, i.e. disordered, media.

#### 4. Conclusion

In summary, we presented a study of the thermal properties of  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  thin films as a function of thickness. For low thicknesses, 12 nm for  $\text{SiO}_2$  and 2-5 nm for  $\text{Al}_2\text{O}_3$ , we measured reductions of the effective thermal conductivity by 30% and 70% compared to the values

obtained for micrometric layers of SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> respectively. The interfacial thermal resistance was small in both cases, suggesting good thermal transport across the interfaces. The diffusivity and conductivity are not measured independently, but rather upon the assumption that  $\rho C = \text{cst}$ , though the effect of diffusivity is clearly revealed by the change of the phase of the photorefectance signal for the thick layers (down to 100 nm). The thermal conductivity and diffusivity were determined with an average precision of 15%, except for the 10, 5 and 2 nm thick layers of Al<sub>2</sub>O<sub>3</sub>. For these very thin films, the precision is 20%, although the absolute value of the uncertainty is unchanged. The different recorded response for each measured layer proves that frequency domain photorefectance microscopy is a well-adapted robust technique to analyze thin films down to the nanometric scale.

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### Figures captions

Figure 1: Schematic of the fabricated samples, a) the SiO<sub>2</sub> layers and b) the Al<sub>2</sub>O<sub>3</sub> layers.

Figure 2: Schematic of the analysis procedure.

Figure 3: Effective thermal conductivity and diffusivity versus thickness of SiO<sub>2</sub> layer over doped Si substrate. The symbols are the measured values along with the corresponding uncertainties.

The inset solid line corresponds to the best fit following equation (1); the obtained parameters are

$$k_f = 0.95 \text{ W/m.K and } R_{th} = 5.1 \times 10^{-9} \text{ m}^2\text{K/W.}$$

Figure 4: a) Amplitude and, b) phase of the measured photoreflectance signals along with corresponding fits for different thicknesses of Al<sub>2</sub>O<sub>3</sub>. The experimental error on the measurement is 5%, and was estimated by repeating each measurement 5 times.

Figure 5: Effective thermal conductivity and diffusivity versus thickness of Al<sub>2</sub>O<sub>3</sub> layer over Si substrate. The symbols are the measured values along with the corresponding uncertainties. The inset solid line corresponds to the best fit following equation (1); the obtained parameters are  $k_i = 1.56$  W/m.K and  $R_{th} = 4.26 \times 10^{-9}$  m<sup>2</sup>K/W.

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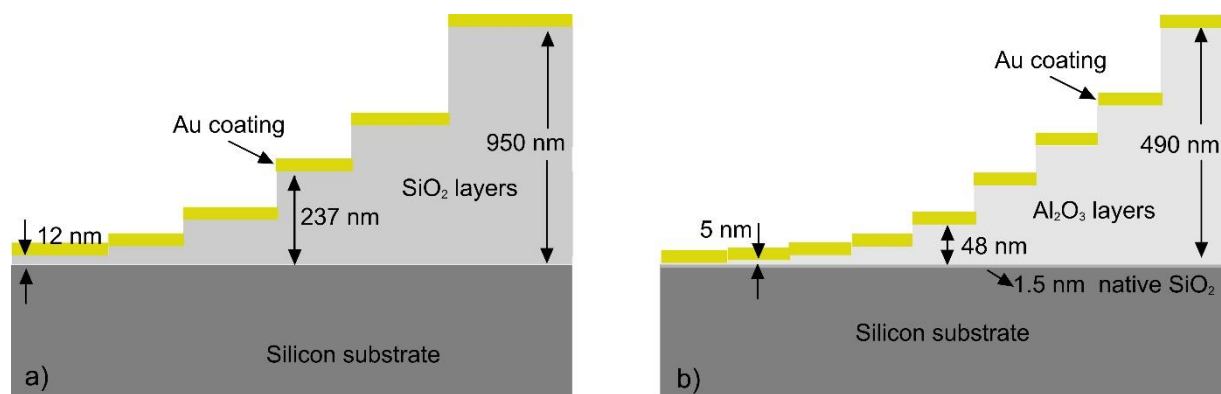


Fig. 1

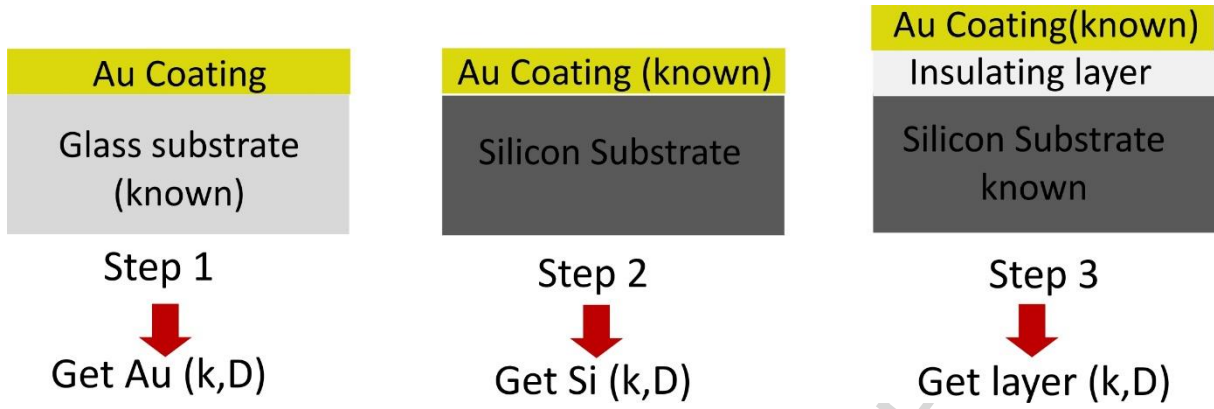


Fig. 2

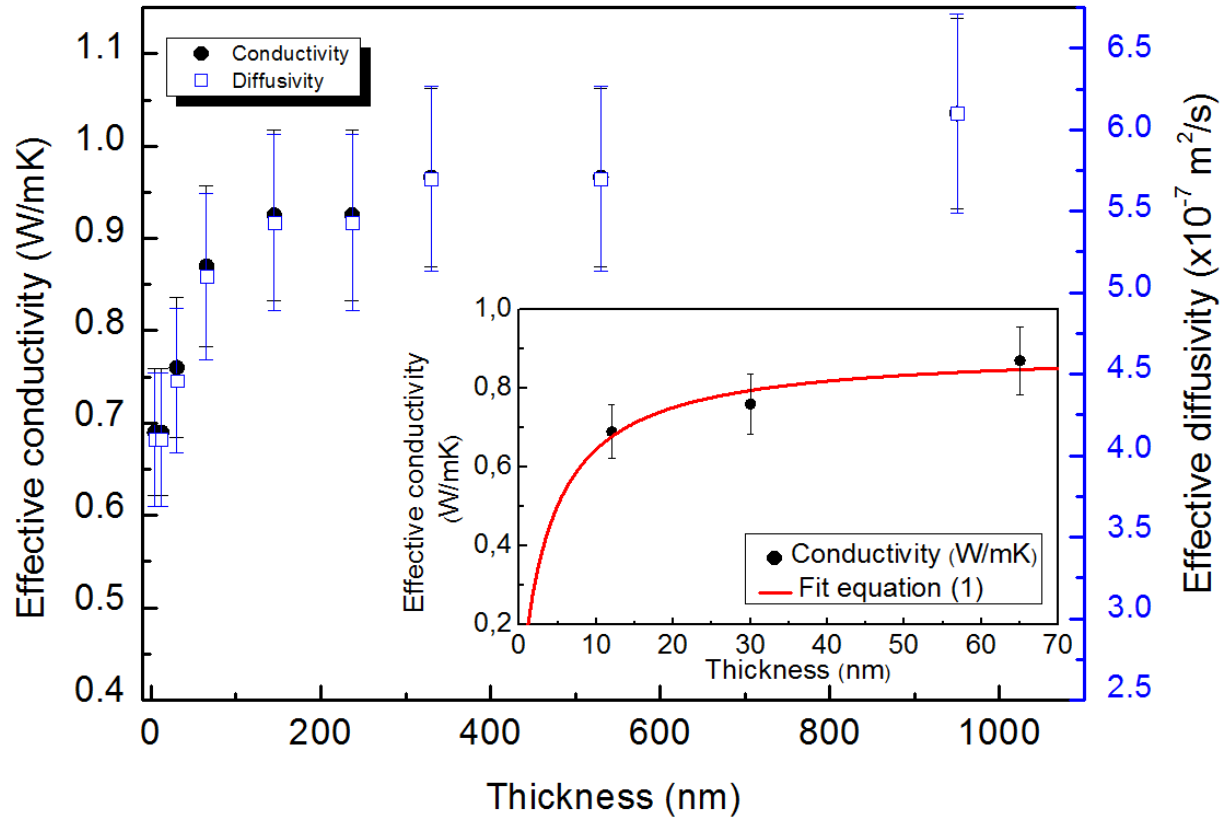


Fig. 3

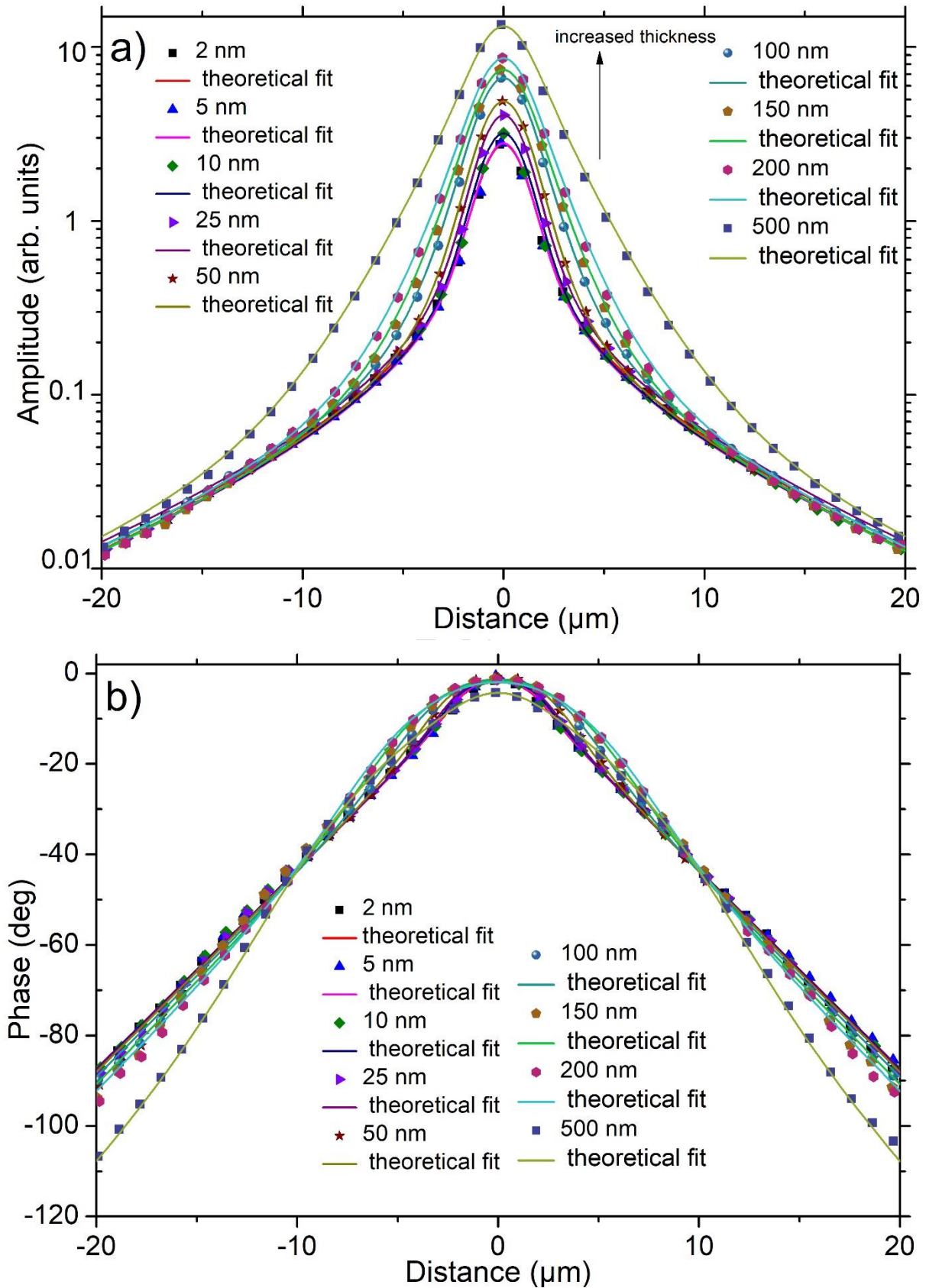


Fig. 4

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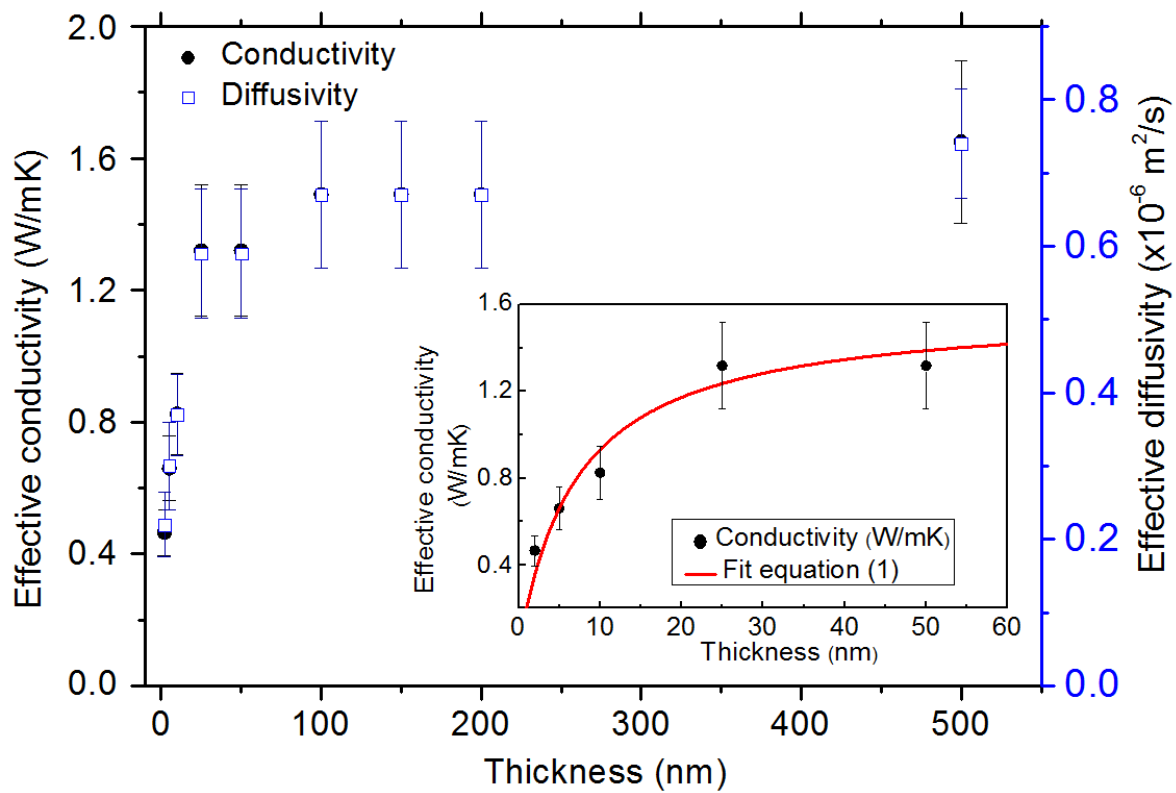


Fig. 5