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Title	A randomized double-blinded clinical trial to evaluate the safety and efficacy of a novel superelastic nickel–titanium spinal rod in adolescent idiopathic scoliosis: 5-year follow-up
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Citation	European Spine Journal, 2018, v. 27 n. 2, p. 327-339
Issued Date	2018
URL	http://hdl.handle.net/10722/245162
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A Randomized Double-Blinded Clinical Trial to Evaluate the Safety and Efficacy of a Novel Super-Elastic Nickel-Titanium Spinal Rod in Adolescent Idiopathic Scoliosis – 5 year follow-up

1 ABSTRACT

Purpose: To evaluate the safety and efficacy of a super-elastic shape-memory alloy (SNT) rod in
treatment of adolescent idiopathic scoliosis (AIS).

Methods: Patients with AIS Lenke 1 curves undergoing fusion surgery were randomized (1:1) at
the time of surgery to receive either the SNT or a conventional titanium alloy (CTA) rod.
Radiographs were obtained preoperative and postoperatively up to 5 years follow-up. Parameters
assessed included coronal and sagittal Cobb angles, overall truncal and shoulder balance. Sagittal
profiles were subcategorized into Types A (<20°), B (20-40°) and C (>40°).

9 Results: Twenty-four patients with mean age of 15 years were recruited. A total of 87.0% of 10 subjects were followed-up till postoperative 5-years but all patients had minimum 2-years 11 follow-up. The fulcrum-bending correction index for the SNT group was 113% at postoperative 12 day 4 and 127% at half-year while the CTA group was 112% at postoperative day 4 and only 13 106% at half-year. In terms of sagittal profile, the SNT group moved towards type B profile at 14 half-year follow-up with a mean correction of 7.6° while no significant change was observed in 15 the CTA group (-0.7°). Nickel levels remained normal and there were no complications.

16 **Conclusions:** This is the first randomized clinical trial of a novel SNT rod for treating patients 17 with AIS, noting it to be safe and has potential to gradually correct scoliosis over time. This 18 study serves as a pilot and platform to properly power future large-scale studies to demonstrate 19 efficacy and superiority.

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21 Keywords: Adolescent idiopathic scoliosis; super-elastic; nickel; titanium; rod

1 Introduction

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3 The aim of spinal surgery for adolescent idiopathic scoliosis (AIS) is to correct the deformity, obtain a balanced spine and prevent curve deterioration.¹ Posterior instrumentation 4 utilizes a combination of screws, hooks or wires with rod constructs for deformity correction.² 5 6 No difference in correction rates have been demonstrated between different instrumentation strategies.² However, up to 2-10% of subjects may have experienced loss of correction 7 postoperatively.³⁻⁶ Risk factors for loss of correction over time can be contributed to large 8 9 magnitude curves and apical translation. This phenomenon may be contributed to tissue viscoelasticity.7-11 10

Viscoelasticity is a time-dependent phenomenon. Correction forces applied by 11 12 instrumentation reduce over time as the tissues relax, leading to some recurrence of the deformity. In an attempt to achieve better correction, higher corrective forces are generally 13 14 applied intraoperatively and with the use of more bone anchors to share out such forces. However, high correctional forces has potential to plastically deform rods and cause screw 15 pullout or pedicle fracture.² Thus, the current trend in AIS correction surgery is to use higher 16 17 implant density with stiff rod constructs like Cobalt-Chromium or stainless steel. In theory, these 18 rods should be able to positively influence the coronal and sagittal plane correction. Nevertheless, this is based mainly on biomechanical studies^{12,13}, whereas clinical results yield 19 insufficient evidence in regards to correction in the coronal plane¹⁴⁻¹⁶ or the sagittal plane.^{17,18} In 20 21 addition, due to the increased forces generated by the stiffer rods, higher density screws are required to dissipate the forces more evenly.¹⁸⁻²⁰ 22

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Sagittal alignment has gained significant attention in recent years. Decreased thoracic

kyphosis can lead to increased risk of adjacent segment disease and poorer quality of life.^{21,22} As thoracic hypokyphosis is a main feature of most AIS patients with Lenke 1 curves^{23,24}, there is increasing interest to correct the sagittal alignment. However, the current approach towards AIS correction may not be effective in achieving this outcome. Postoperative hypokyphosis has been associated with increased screw density. This has been attributed to different corrective maneuvers such as direct vertebral rotation.²⁵⁻²⁸ More pedicle screws increase the overall cost of the surgery^{8,19} and neurological risks related to malpositioning.²⁹⁻³¹

8 The viscoelastic relaxation of spinal tissues may be overcome by applying a progressive 9 and constant correction force resulting in further deformity correction after rod implantation. The 10 force required to obtain this progressive correction is likely to be less than the force applied 11 using current instrumentation and hence avoid the risks associated with stiff rods. As a result, 12 perhaps fewer anchors can be used to reach the same end-point. Nickel-titanium (NiTi) alloy is a 13 metal that has the ability to return to a previously defined shape when subjected to thermal 14 treatment (shape-memory effect). A lesser utilized property is its super-elasticity. This is a property whereby regardless of the strain or deformation placed on the rod, the rod exerts the 15 same recovery force, thereby making it predictable and ideal for use in scoliosis patients, as 16 17 curve magnitude varies. Thus, it can provide a predictable recovery force regardless of the 18 severity of the spinal deformity. The authors have developed such a new super-elastic nickeltitanium spinal rod (SNT) with maximal superplastic properties at human body temperature.³² 19 20 Moreover, when the rod is cooled to below 20°C, it has a low yield strength and can be deformed 21 easily into the shape of the spinal deformity, making surgical insertion easy. Then when the rod 22 is warmed to human body temperature (37°C), the rod becomes maximally super-elastic and will 23 attempt to return to its pre-designed contour. We have made a 6.0mm spinal rod, which under

laboratory conditions can produce 300N recovery force in bending and torsion. This force can be 1 2 tailored to requirements by heat treatment processing, but our preliminary *in-vivo* study suggest 3 that a 300N force should be sufficient to result in curve correction in our patient population 4 (unpublished data). The time it takes for the rod to return to its initial shape, will depend on the 5 stiffness of the spine. In-vivo goat studies performed in our laboratory, suggest that maximal 6 recovery of the rod occurs by 3-4 weeks and should not affect fusion process. These goat 7 experiments were not published but it is important to note that deformity was observed immediately and progression of deformity up to one week postoperatively after implantation of 8 pre-contoured superelastic rods. 9

10 Although nickel alloys are commonly used in implant materials, the high proportion of 11 nickel present in the SNT rod, raises potential concerns with allergic reactions or even toxicities 12 in humans.³³ To enhance its safety profile, the rods undergo a surface treatment process called 13 plasma immersion ion implantation, whereby a layer of titanium nitride (TiN) is formed on the 14 surface making the rod more mechanically durable and reduces the chance of nickel release into 15 the blood stream [30, 36-38]. The safety and efficacy of this surface modified spinal rod has been 16 established in *in-vitro* and animal studies with rabbit and goat models³⁴⁻⁴³.

This is the first randomized controlled human clinical trial that addresses the safety and
efficacy of a surface treated SNT rod in comparison to a conventional titanium alloy rod (CTA)
for correction of deformity in AIS subjects.

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1 Methods

2 Study Design, subject recruitment and randomization

3 This was a prospective parallel randomized, controlled double-blinded pilot clinical trial 4 conducted at a single center. Institutional review board approval was acquired and informed 5 consent was obtained by all participants in this study. Inclusion criteria included female or male of less than 25 years of age, thoracic or thoracolumbar curve, single spinal curve of >45° 6 7 requiring selective thoracic fusion and those with more than 2-years follow-up. Exclusion criteria 8 included subjects with stiff curves and a residual curve on fulcrum bending of $\geq 40^{\circ}$, having more 9 than one curve that needs fusion, received any previous spinal surgery, known and skin tested 10 allergy to nickel (Ni) or other implant materials. Stiff curves were excluded as this was the first trial of the SNT rods and we wanted the proof of principle to be tested in flexible curves first. 11 12 Eligible patients with AIS and Lenke 1 curves were randomized at the time of surgery into two 13 groups, to receive either SNT rods (treatment group) or CTA rods (control group).

14 The Clinical Trials Centre (CTC) at the University of Hong Kong (HKU) was involved in 15 monitoring the study (reference no. CTC 0484). Block randomization by computer program was 16 performed by a statistician in the Medical Statistics Department of the CTC. The randomization 17 involved allocating trial subjects in equal proportion (1:1 ratio) to each of the two treatment 18 groups. This randomizer was not involved in subject recruitment, conduct of the study, data 19 management and statistical analysis. No other study personnel had access to the randomization 20 list. Investigators were required to submit the trial subjects' particulars to the randomizer for 21 assigning the trial treatment.

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For the blinding details, both patients and assessors of collected data were blinded to the

rod material used. The rod material used was not disclosed to the patients until 2 years after the
 surgery. Surgeons were not informed of the rod material used until immediately prior to surgery,
 thus at the time of patient recruitment, the surgeon was not influenced by the rod material during
 consent for surgery. All subsequent follow-up assessments were performed by assessors without
 knowledge of the rod material up to the 5-year follow-up.

6

7 Intervention

8 The rods were made of NiTi (Ti-50.8at% Ni; Nitinol Device Company, Fremont, U.S.A) with a customized heat treatment protocol.³⁸ As SNT rods are super-elastic, they cannot be 9 10 manually contoured during surgery. For the purposes of this study, the rods were prebent in the 11 factory to 30° kyphosis in the thoracic portion and 30° lordosis in the lumbar portion. This was based on suggested "normal" values⁴⁴ of sagittal contour and to avoid over-aggressive sagittal 12 13 correction. Variable contouring was possible depending on need. Different lengths of rods were 14 available depending on the size of the patient, and the rods were then cut to the appropriate 15 length to fit a specific region of the spine. The rods used in the control group (CTA) was a 16 conventional titanium alloy (Universal Spinal System, USS; Synthes® Inc, USA). To ensure that 17 they were contoured appropriately, an intraoperative template was used to ensure curvatures 18 created were the same as those of the factory pre-bent SNT rods. The screws and anchors for 19 both the control and the study group were the same (Synthes® Inc, USA), the titanium (Ti) 20 cables were manufactured by Medtronic®, USA.

Surgical procedures were standardized regardless of the rod material. Standard posterior
 spinal exposure appropriate for the length of thoracic curve to be instrumented was performed

based on fulcrum-bending radiographs.⁴⁵⁻⁴⁹. If possible, pedicle screws were applied to the upper 1 2 and lower instrumented vertebra and the one adjacent vertebrae, thus a total of 4 screws were 3 used at both ends. In order to allow continued correction after surgery, 4 sub-laminar titanium 4 cables were used at the intermediate levels. During surgery, the rods were inserted into the 5 anchors using the same techniques as traditional rods. In all patients, the concave rod was 6 inserted first and then rotated to correct the curvature. Then all screws were tightly locked. 7 However, with the SNT rods, because they were more elastic, we found that the rod often bent 8 back into the curvature more, but with warming of the patient to body temperature, rod shape 9 recovery could be seen. No osteotomies were performed in either group except for our usual 10 method of removing the inferior articular processes of intermediate facet joints for interfacet 11 fusion.

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13 *Outcome Assessments*

14 After recruitment, all subjects had an initial preoperative clinical and radiological assessment which included standing anteroposterior (AP) and lateral radiographs and fulcrum-15 bending radiographs.^{46,48} Subsequent assessment intervals were made postoperatively on the first 16 17 day after patient was able to stand after the surgery (usually day 1-4) and day 7. Further 18 assessments were made on postoperative 4 weeks, 12 weeks and 24 weeks, and postoperative 1 19 year, 2 years and 5 years. All parameters were collected on the radiographs using the DICOM based Radworks 5.1 (Applicare Medical Imaging BV, Zeist, The Netherlands) computer 20 software program. 21

The primary objective of study was to evaluate the safety and efficacy of the SNT in AIS patients. Safety was evaluated based on lack of any major intra and postoperative adverse events that could be related to the implant. Events, such as intraoperative fracture or postoperative implant displacement and loosening, loss of scoliosis correction, neurologic deficit, failure to correct the curvature, delayed wound healing and wound infection, and Ni-related toxicity. Serum Ni levels were thus also noted.

Efficacy was evaluated by comparing SNT with CTA in achieving coronal deformity correction, using the Fulcrum Bending Correction Index (FBCI). This index is a ratio of the actual correction based on the correction rate, and the predicted correction based on the fulcrum flexibility^{46,48}. It has been previously shown to allow comparison of correction between patients by taking flexibility of the curvatures into account.²

10 Secondary objectives included evaluation of sagittal deformity correction (degree of 11 kyphosis), coronal balance (truncal shift, listing, shoulder height, clavicle angle and T1 tilt), and 12 patient perceived outcome (SRS-22). Sagittal profiles were subcategorized into Types A ($<20^{\circ}$), 13 B (20-40°) and C (>40°) to define whether the kyphosis correction was hypokyphotic (A), 14 normal (B) or hyperkyphotic (C). These were normality figures based on the proposed sagittal alignment in previous studies.^{50,51} A hypokyphotic sagittal alignment usually increased and 15 hyperkyphotic spines usually decreased in alignment.⁵⁰ Thus, the change in sagittal alignment 16 17 towards normality was recorded (- if away from $20-40^{\circ}$ and + if towards $20-40^{\circ}$).

Both surgeons and patients were blinded to the type of rod used prior to the surgery, and the rod material to be used was only revealed to the operating surgeon at the time of surgery. All radiographs were measured by independent observers who were also orthopaedic surgeons, but were not involved in the surgical procedure or the subsequent care of the patients. When the difference in the measurements between the two assessors was less than 5°, the mean of the two measurements were reported. When the discrepancy in the measurements between the two 1 assessors was more than 5° , then a consensus between the individuals was determined.

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3 Statistical analysis

A statistician not involved with the radiographic assessment and clinical data collection performed the statistical analyses using SPSS version 19.0. Descriptive and frequency analyses were performed for all efficacy and safety parameters. All data passed Shapiro-Wilk testing for normality and Chi-square test and student t-test were performed to compare the two groups. A pvalue of <0.05 was considered statistically significant.

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11 **Results**

Twenty-four patients with AIS, mean age of 15 years (SD ± 2.3), were recruited. One patient dropped out at the time of surgery due to lack of the correct sized rods. Thus 11 subjects (4 males, 7 females) were in the SNT group and 12 subjects (2 males, 10 females) were in the CTA group. 20 subjects (87.0%) were followed-up for a minimum of 5 years postoperatively while the remaining 3 subjects (two SNT and one CTA) were followed-up for at least 2 years postoperatively. These three patients emigrated away after the 2 year follow-up and their contact information were unable to be retrieved.

Patients in both groups were comparable as there were no statistical differences noted between the two groups in terms of clinical (**Table 1**), spine radiographic (**Table 2**) or balance (**Table 3**) parameters (p>0.05). Both groups had similar maintenance of the coronal Cobb angles (**Figure 1**), FBCI (**Figure 2**) and sagittal profile (**Figure 3**) postoperatively up to 5-years followup. However, the overall FBCI change (**Table 2**) was better for the SNT (**Figure 4**) with a steady

increase up to at least 1 month and up to 6 months postoperatively as compared with CTA
 (Figure 5).

3 For the sagittal profile analysis (**Table 4**), there was no significant difference in the 4 sagittal profile from preoperatively to half-year follow-up (p=0.11). However, there were 5 significantly more type A profiled subjects in the SNT group preoperatively and 45.5% of SNT 6 subjects in either type A or type C preoperatively corrected to type B at half-year follow-up. This 7 amounted to a mean change of 7.6° (±SD 9.3) towards the 20-40° range. In contrast, the CTA 8 group had more type B profiled subjects preoperatively which reduced at postoperative half-year. 9 Hence, only a mean change of -0.7° (±SD 13.6) towards the 20-40° range was observed in the 10 CTA group.

11 Compared to the immediate postoperative result, there was a gradual change in both the 12 coronal and sagittal Cobb angles in the SNT rods. In **Table 2**, the coronal Cobb angle at Day 4 13 after surgery is 20.2°, this was reduced to between 14 to 17° subsequently. While in the sagittal 14 plane, for both SNT and CTA rods, the Cobb angles significantly increased from Day 4 15 postoperatively to Day 7 and subsequent follow-up. This suggested some restoration of kyphosis 16 in both systems with time.

There was a slight increase in Ni levels (**Table 5**) postoperatively for the SNT group but returned to baseline at 6 months postoperatively and remained the same since then. There were no allergic reactions, wound complications, loss of balance, implant breakage or non-union. SRS-22 scores were similar for both groups at all intervals (**Table 6**).

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1 Discussion

The novelty of the current study is three-fold. This is the first study that uses the superelastic properties of a NiTi alloy to attempt to gradually correct a spinal deformity over time. Secondly, this is the first time that a novel surface treatment process is applied to the SNT rod to reduce risk of Ni reactions and enhance the mechanical and wear properties of the rod. Thirdly, it is the first randomized controlled human clinical trial with 5 years of follow-up data.

The idea of gradual deformity correction is not new, Ilizarov⁵² described the techniques 7 8 of gradual deformity correction of long bones using an external fixator frame, and even in spinal 9 applications, halo-pelvic, halo-gravity tractions and internal distractions using "growing implants" have been described to gradually correct deformities over time.⁵³ What is novel is that 10 11 we have harnessed the super-elastic properties of NiTi to allow gradual internal correction 12 without the need for repeated surgeries or prolonged in-hospital treatment. The authors have previously demonstrated the mechanical, chemical properties and biocompatibility of the 13 14 implant, as well as establishing its efficacy and safety through *in-vitro* and *in-vivo* animal studies.³⁷⁻⁴³ Specifically, a patented technology named nitrogen plasma immersion ion 15 implantation on nitinol surface was invented that not only suppresses nickel release from the 16 material surface, but also enhances the surface mechanical properties.⁴¹ It is believed that this 17 newly modified surface is able to reduce the metal release due to mechanical fretting. The 18 19 advantage and importance of harnessing super-elasticity is that the recovery force of the rod 20 remains constant regardless of the size of the spinal deformity, thus the force is predictable and 21 controllable, an important aspect for human use.

A clear distinction should be made between the shape-memory effect of NiTi alloys and super-elasticity. The former is in relation to change in the shape of the rod with temperature, this has been previously used to correct the deformity instantaneously at the time of surgery⁵⁴⁻⁵⁶, but is not so different from manual manipulation of the rod during surgery, and is unable to provide the gradual correction of deformity that is a desirable effect. While NiTi (shape-memory) rods are usually super-elastic at or above their transition temperature, conventional NiTi rods are not optimised for super-elasticity at human body temperature. We have tailor-made heat treatment processes that optimizes this, and thus these rods are fundamentally different from conventional shape-memory alloy rods.³²

8 This is thus the first human clinical study using this novel spinal rod. This pilot clinical 9 trial serves 3 main purposes. Firstly as the surface treated NiTi rods are used for the first time in 10 human subjects, we need to demonstrate that they are safe and does not result in either a rise in 11 the serum Ni level or any untoward side-effects; secondly, we need to demonstrate that the 12 concept of gradual correction is possible, and that the results are at least comparable to standard 13 techniques; and thirdly we need to have an idea of the effect size, so that we can properly power 14 future studies.

15 If the flexibility of the curvatures is taken into account using the FBCI (Table 2/Figure 16 2), one is able to see a consistent trend that SNT produces a superior degree of correction, 17 although this does not reach statistical significance. Of interest is that the SNT rod, which is very 18 easy to bend, compared to a titanium rod, is able to produce the same degree of correction as a 19 standard titanium rod. This can be a potential advantage for some surgeons, as the rod is much 20 easier to manipulate intraoperatively, making rod insertion easier, and risk of implant pull-out 21 lower. Based on this effect size, we estimate that 64 cases will be required in each arm of the 22 study to demonstrate superiority at 2 years of follow-up (a = 0.05, power = 0.95). This will be the aim of future studies. 23

1 In the sagittal plane, a built-in kyphotic contour to the SNT rod can also allow continuous 2 correction postoperatively. The thoracic sagittal profile in AIS is usually hypokyphotic, and 3 efforts should be made during surgery to correct it. This may be common sequelae of posterior spinal fusion²⁶ since most consecutive all-pedicle screw constructs may lead to flatback.^{8,9,57,58} In 4 5 this study, there are no statistical differences between the overall sagittal alignment of the two 6 groups. However, subgroup analysis of the different sagittal patterns show that more corrective 7 potential is observed in the SNT group. Subjects with hypokyphosis has increases in sagittal 8 profile while those with hyperkyphosis has decreases in sagittal profile, moving towards the more "normal" 20-40° range.^{50,51} This indicates a potential to further improve the kyphosis and 9 10 overall posture postoperatively. The shape-memory and super-elastic properties of NiTi 11 contributes to this effect shown in the SNT subjects. Nevertheless, a tendency for progressive 12 correction over time has also been observed in the CTA group. The inherent elasticity of titanium 13 rods is likely responsible for these changes.

In terms of overall function, improvement in SRS-22 scores are observed in both groups up to 5 years follow-up. All subgroup scores improved and the rate of improvement is similar in both groups. This is a comparable finding to Carreon *et al*⁵⁹ where longitudinal cohort of 745 patients with surgical correction for AIS showed improvement in the general SRS-22 scores up to 2 years of follow-up. Comparably, the average score of 4.3 reported in her study is also similar to the findings in our study.

The main safety concern with these rods is the release of Ni after implantation. Kim *et* al³³ showed that metal ions can be detected in the serum after surgery with stainless steel rods. High levels of Ni have been noted postoperatively up to 3.8ng/ml and remains persistently elevated even at 4 years after surgery (normal: 0.3ng/ml). Similar findings can be found for Ti-

based instrumentation up to 12 months postoperatively.⁶⁰ Ni is known to be toxic to cells, can 1 2 cause allergic reactions and maybe carcinogenic. However, the chemical properties of Ni is altered when formed into an alloy with Ti, drastically reducing the possibility of Ni liberation.⁶¹ 3 NiTi material is therefore believed to be biocompatible and have less corrosion problems 4 5 because of the strong bonding between the Ni and Ti atoms, and the presence of a mainly passive Ti-oxide-based surface layer.⁶¹⁻⁶³ However, with deformity correction, there will be some 6 7 unavoidable contact with the rods, which may result in the Ti-oxide layer being rubbed off. Thus 8 to minimize the Ni safety concern even further, we have surface treated the rod with a technique 9 called plasma immersion ion implantation.[38] The treated surface has been shown to show 10 improved corrosion and wear resistance. Raised serum Ni can also be observed in this study but 11 the elevated amount is well under the recommended safety limit (i.e. <10ng/mL or <170.33nmol/L).⁶⁴. No complications arising from Ni is reported in this study suggesting that the 12 13 surface-treated NiTi spinal rod is biocompatible in humans. It is also important to note that there 14 is a baseline Ni level even in the control group as usual daily edible vegetable oils may include Ni concentrations of 0.026-0.075ug/g which poses no human health risk.⁶⁵ 15

16 This is a randomized double-blinded clinical trial based upon a novel implant for 17 managing patients with AIS. The main limitation of the study is its small sample size. However, 18 as this concept is new with no previous comparable studies, it is not possible to perform a sample 19 size calculation prior to the initiation of the study. This unique study compares the safety and 20 efficacy of the novel SNT rod to CTA rods. Thus it serves the purpose of informing us of the 21 safety profile of the rod, and also allow us to power future studies properly. SNT rods have 22 super-elastic properties that allows the potential to gradual correction of the deformity following 23 surgery by a constant corrective force. Moreover, the study shows the potential of improved

1	sagittal correction by the SNT rods. Adequate safety and function has been observed by the
2	absence of Ni and surgical related complications and improved SRS-22 scores. This study has
3	successfully verified its efficacy and safety in managing AIS patients.
4	
5	Acknowledgement
6	We would like to thank Dr. Kin Cheung Mak for clinical care of the patients in this study
7	and Dr. Guneet Makkar from the CTC of HKU for statistical support.
8	
9	Funding Sources
10	This study was financially supported by Hong Kong Research Grants Council (HKU
11	7283/00M and CityU 1/04C); Scoliosis Research Society (9667002); Hong Kong Innovation
12	Technology Fund Tier 2 Grant (GHP 019/05).
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1 Figure Legends

2

3	Figure 1: Major curve Cobb angle comparison between conventional titanium alloy rod (CTA)
4	and super-elastic nickel-titanium alloy rod (SNT).
5	Figure 2: Change in Fulcrum Bending Correction Index (FBCI%) Comparison between
6	conventional titanium alloy rod (CTA) and super-elastic nickel-titanium alloy rod (SNT).
7	Figure 3: Change in Sagittal Profile Comparison between conventional titanium alloy rod (CTA)
8	and super-elastic nickel-titanium alloy rod (SNT).
9	Figure 4: An 18-year-old female with super-elastic nickel-titanium alloy rod implanted.
10	Standing anteroposterior radiographs at postoperative 1 week (a) and postoperative 4 weeks (b)
11	shows progressive correction of primary Cobb angle. Thus, there is improvement in FBCI from
12	116% at postoperative 1 week to 184% at postoperative 4 weeks.
13	Figure 5: A 17-year-old female with conventional titanium alloy rod implanted. Standing
14	anteroposterior radiographs at postoperative 1 week (a) and postoperative 4 weeks (b) shows no
15	further correction but even loss of correction of the primary Cobb angle. Thus, there is a

16 reduction in FBCI from 121% at postoperative 1 week to 99% at postoperative 4 weeks.