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Short Communication

Study of Al₂O₃/SiC particle loading on the microstructural strengthening characteristics of Zn–Al₂O₃–SiC matrix composite coating

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ABSTRACT

In this paper, the microstructure, and mechanical performance of Zn–Al₂O₃–SiC film co-deposited on mild steel substrate were produced by electrodeposition method. The structural characteristic of the composite coating was analyzed by scanning electron microscope (SEM) equipped with energy dispersive spectrometer (EDS), X-ray diffraction (XRD) and atomic force microscope (AFM). Mechanical examination was done using durascan hardness tester. The result showed that the influence of individual particle loading greatly alter the structural properties and hardness behavior. The increase in hardness is attributed to the perfect homogeneity and characteristics of the particulate which led to the formation of uniform distribution, coherent and interfacial precipitation within the zinc lattice.

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1. Introduction

The existence of Zn coating over year has tremendously been attested to exhibits resilient mechanical and corrosion

resistance to a considerable level [1,2]. Meanwhile their service performance decreases due to scar piled up in mechanical application and aggressive medium resulting from corrosion product [3–7]. Metal and ceramics composite deposition are appreciated surface modification technology

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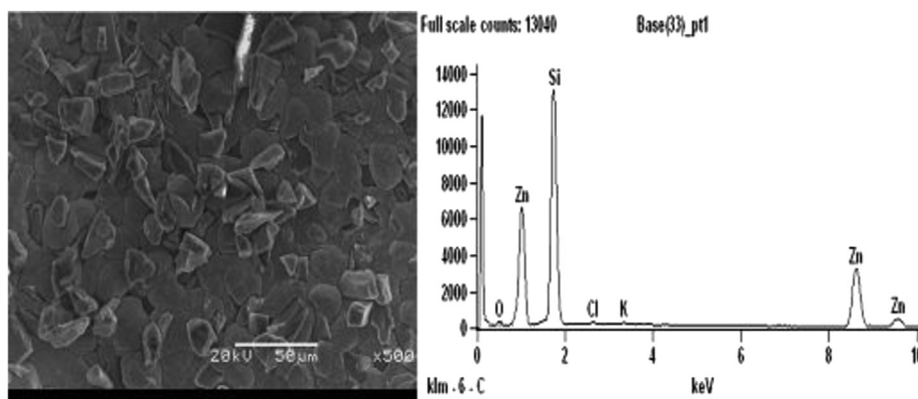


Fig. 2 – SEM/EDS micrographs of Zn–15SiC sample.

in distilled water. Analytical grade chemicals and distilled water were used to prepare the plating solution at room temperature, prior to plating. The formulations were then placed in a stir for a day while heated to 40 °C to easily admix and to allow for dissolution of any agglomerate in the bath solution. The bath produced is concurrently stirred as heating trend lasted for hours before plating [8]. ZnSO₄·7H₂O 70 g/L, Al₂O₃ 5–10 g/L, SiC 10–15 g/L, Boric acid 5 g/L, Glycine 5 g/L, Thiourea 5 g/L, Temp 40 °C, pH 4.5, Current density 0.5–1.0 A/cm².

2.3. Preparation of the coatings

The prepared Zn–Al₂O₃–SiC composite was heated for 2 h and intermittently stirred to obtain clear solution before it was prepared by electrolytic deposition process over mild steel. The prepared cathode and anodes were connected to the D.C. power supply through a rectifier as presented in Fig. 1. Deposition was carried out at varying applied current between 0.5 and 1.0 A/cm² for 15 min.

The distance between the anode and the cathode and the immersion depth was kept constant. Thereafter, the samples were rinsed in water and dried. The formulated design plan for the coating is described in Table 1.

2.4. Structural characterization of the coatings

The structural studies and elemental analysis of the fabricated alloy samples were verified using a TESCAN scanning

electron microscope with an attached energy dispersive spectrometer (SEM/EDS). The phase property was observed with the help of X-ray diffractogram. The adhesion profile, topography and morphology of the coating were observed with the help of atomic force microscope (AFM). High optic diamond based durascan microhardness tester was used to estimate the average microhardness of the deposit in an equal interval range.

3. Results and discussion

3.1. SEM/EDS of deposited alloy

Figs. 2 and 3 show the SEM/EDS structure of represented Zn–Al₂O₃–SiC fabricated ceramic coating with reference to (Zn–15SiC and Zn–10Al–15SiC) matrix respectively. From the two figures it is obvious that the crystal flakes of the deposits were homogeneously dispersed on the interface. It is quite evident that at 1.0 A/cm² for Zn–15SiC a noticeable crystal nucleus patched along the interface was observed. Apparently there are two distinctive phases, the initial having a homogeneously uniform stable precipitate and the latter with hexagonal patches. In fact, the incorporation of the SiC along the zinc interfacial could be seen to provide a refine microstructure with dominating nodular particle.

The deposition appearance with coating interferes of Al₂O₃/SiC was quite appreciated in that both particulate

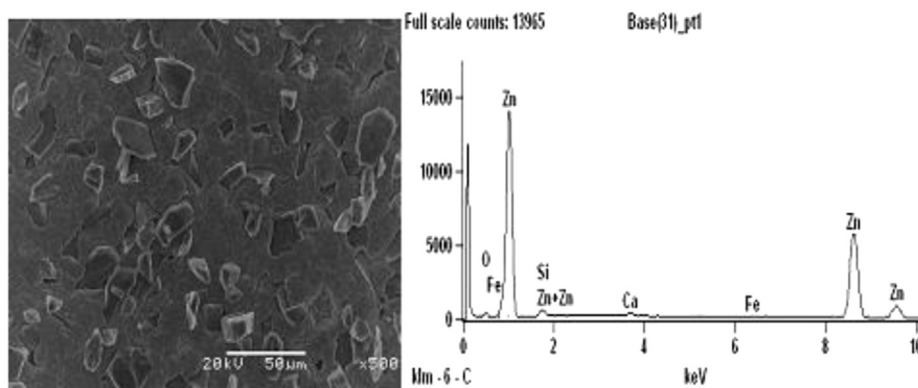


Fig. 3 – SEM/EDS micrographs of Zn–10Al₂O₃–15SiC sample.

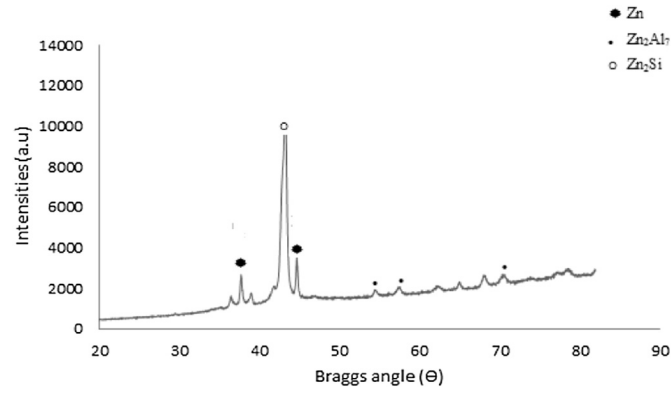


Fig. 4 – XRD pattern of Zn–10Al₂O₃–15SiC sample.

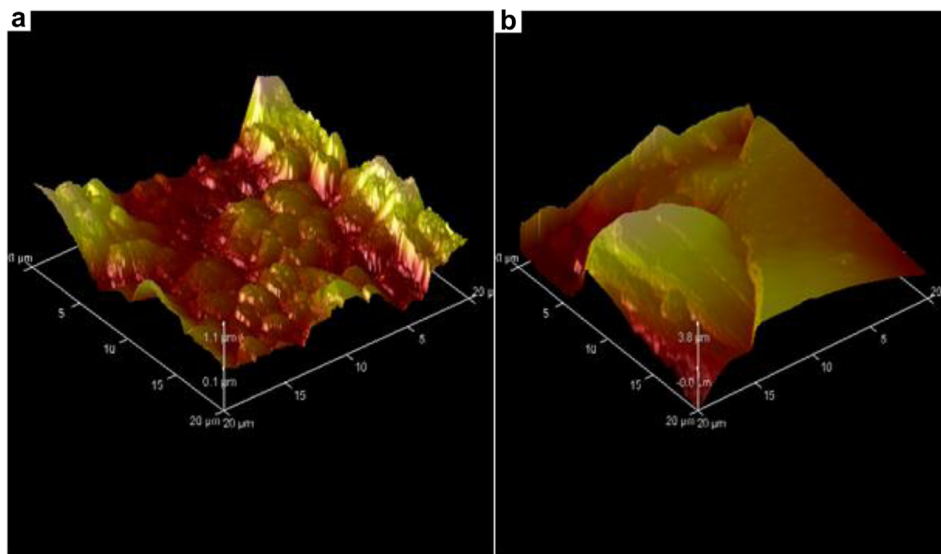


Fig. 5 – 3D AFM images of a) Zn–15SiC b) Zn–Al₂O₃–15SiC particle reinforced.

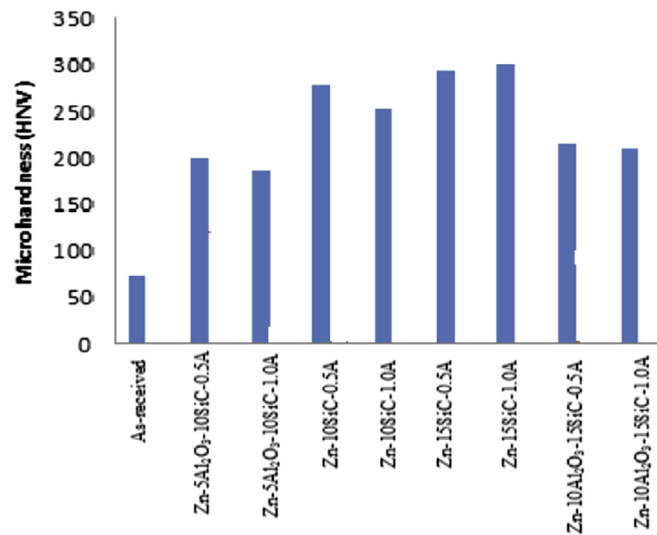


Fig. 6 – Hardness properties of varied loading particle of Zn/Al₂O₃/SiC matrix deposited on mild steel.

strengthen composite find their way expressly doped into the zinc metal matrix. The structural behavior was quite expected because the nucleation process proceed from the zinc metal as load bearer, the dispersion of the particulate cover the nucleation site and strengthening the produced alloy [11,13,14] Fig. 3. In other words, it is necessary to mention that morphological change may be associated to the strong blocking influence of the induced composite leading to good precipitation and better orientation. Sometime the conditioning parameter in relation to the degree of additive impede also play a vital role in re-modification of the crystal orientation and surface texture of a deposited as attested [3].

Fig. 4 shows the XRD pattern of the Zn–Al₂O₃–SiC deposit prepared with 10Al₂O₃/15SiC nanoparticle concentration from the plating bath. The diffractogram give the major diffraction peak as 38°, 42°, 45° 55° and 72°.

The intermetallic growth phases observed are Zn, Zn₂Al₇, Zn₂Si etc. The presence of the individual dispatched metal-particulate phases was noticeable on the coating as it seems to influence the phase change through the help of inter-diffusion mechanism and ion of each particulate [1,14]. The phase orientations of the metal matrix are indication of the harness performance and remarkable effect of the coating produced.

3.2. Atomic force microscope analysis

Fig. 5a–b shows the 3D atomic force micrographs of the deposited Zn–SiC and Zn–Al₂O₃–SiC samples. Zn–20SiC matrix had fairly grain size and uniform crystal growth with crystallites. For Zn–Al₂O₃–SiC matrix as observed in Fig. 5b, the inclusion of the composite ceramic Al₂O₃/SiC provide a robust inter-link at the interfacial pool of the Zn based matrix. Although the growing of crystal and topography of a deposit is a combined contribution of diffusion of ions into the nucleus, meaning that the adsorbed atom wanders to a growth point on the cathode and is incorporated in the growing lattice under the influence of the applied voltage and applied electrodeposition time. Ref. [5] affirmed further that surface roughness and adhesion increases most times as a result of the applied voltage on the deposited metal with coalesced crystallite, hence film thicknesses are influenced by metallurgical parameters. Compatibility was seen with Zn–Al₂O₃–SiC adhesion compared to the Zn–SiC matrix with undulation.

3.3. Microhardness studies

The microhardness study shown in Fig. 6 was carried out in order to observe the impact of the composite particulate and its concentration loading on the hardness properties of Zn–SiC and Zn–Al₂O₃–SiC coatings. From general observation, all composite fabricated alloys produced an excellent and significant improvement as compared to the as-received mild steel substrate.

The unexpected result seen among the coating matrix is the less hardness observed from the ternary matrix as against the Zn–SiC alloys. Reason for this behavior is not well as certain, however according to Popoola et al. [8] and Rahman et al. [11], the micro-hardness of the

electrodeposited layers can depend on many factors such as electrolyte composition, operating conditions and diffusion mechanism. On the hand, the hardness improvement for Zn–SiC with about 290HVN can be linked to the agglomeration of SiC influence rather than the network of additives that constitute the electrolyte composition for Zn–Al₂O₃–SiC coatings that possess 205HVN value. Invariably particle loading might not necessitate dramatic improvement but rather refinement and proper nucleation of the bath constitute.

4. Conclusion

- 1) In incorporation of the Al₂O₃/SiC ceramics composite particles in the zinc matrix as reinforcement increases the hardness properties of the substrate.
- 2) The hardness properties increase as the concentration of additive increases.
- 3) There are good uniform particle distribution and better crystal orientation with compactable structure within the ternary alloy coating.

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