Shear viscosity and out of equilibrium dynam ics

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## Abstract

U sing G rad's m ethod, we calculate the entropy production and derive a form ula for the secondorder shear viscosity coe cient in a one-dimensionally expanding particle system, which can also be considered out of chem ical equilibrium. For a one-dimensional expansion of gluon matter with B jorken boost invariance, the shear tensor and the shear viscosity to entropy density ratio =s are num erically calculated by an iterative and self-consistent prescription within the second-order Israel-Stewart hydrodynam ics and by a m icroscopic parton cascade transport theory. C om pared with =s obtained using the Navier-Stokes approximation, the present result is about 20% larger at a QCD coupling s 0:3(with =s0:18) and is a factor of 2 3 larger at a sm all coupling 0:01. We dem onstrate an agreem ent between the viscous hydrodynam ic calculations and the s m icroscopic transport results on =s, except when employing a sm all s. On the other hand, we dem onstrate that for such small s, the gluon system is far from kinetic and chem ical equilibrium, which indicates the break down of second-order hydrodynam ics because of the strong noneqilibrium evolution. In addition, for large  $_{\rm s}$  (0:3 0:6), the Israel-Stewart hydrodynam ics form ally breaks down at large momentum  $p_T > 3 \text{ GeV}$  but is still a reasonably good approximation.

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#### I. IN TRODUCTION

Recent experimental measurements on the elliptic ow parameter  $v_2$  at the BNL Relativistic Heavy Ion Collider (RHIC) [1, 2, 3] show a strong collectivity of the decon ned quark-gluon matter. The matter produced was thus specified as a strongly coupled quarkgluon plasma (sQGP) [4, 5, 6] or as a perfect uid [7]. Further attempts to determ ine how imperfect the sQGP really is have drawn attention to transport coe cients like viscosity [8,9,10,11,12,13,14,15,16] and to the derivation and solution of viscous hydrodynamics [17,18,19,20,21,22,23,24], which is still a mathematical challenge.

M ost current viscous hydrodynam ic equations are based on second-order Israel-Stewart kinetic theory [25]. They are solved num erically using the given viscosity coe cients and initial conditions as well as parton and hadron equation of state. In particular, the shear viscosity to entropy density ratio =s is determined by comparing the elliptic ow from the viscous hydrodynam ical calculations with the data at RHIC, as has been done recently in R efs. [26,27], where the value =s 0:1 was obtained. On the other hand, even though the early partonic phase m ay be well described by ideal hydrodynam ics (= 0), the hadronic afterburning [28] has a larger dissipative e ect, which m ay be enough to slow down the generation of the elliptic ow and bring its nalvalue into agreem ent with the data.

D issipative phenom ena can be alternatively described in transport calculations solving B oltzm ann equations of matter constituents [29, 30, 31, 32, 33, 34, 35, 36]. This approach is applicable for investigations of such phenom ena as therm alization, kinetic decoupling, and dynam ics of high-energy particles in systems far from equilibrium, i.e., in a regime where the second-order viscous hydrodynam ics breaks down [37].

Recently, an on-shell parton cascade Boltzm ann Approach of MultiParton Scatterings (BAM PS) has been developed to study them alization [34, 38, 39], elliptic ow  $v_2$  [40, 41, 42], and the energy loss [43] of gluons produced in Au+ Au collisions at RH IC energy. Also the generation and evolution of viscous shock waves are surprisingly well realized in BAM PS calculations [44]. The shear viscosity of the gluon matter at RH IC has been estimated from BAM PS calculations [41, 42] within the Navier-Stokes approximation [12]. The authors found that to produce large  $v_2$  comparable with the experimental data, the gluon matter should have an =s between 0.08 and 0.2 constrained by details of the hadronization and the kinetic freeze out. This is in line with the dissipative hydrodynam ic approach [26].

Perturbative QCD (pQCD) gluon brem sstrahlung  $gg \$  ggg is responsible for the low =s ratio and for the generation of large elliptic ow.

Beyond the Navier-Stokes approximation, which has been used in Refs.[11, 12], we derive a new microscopic formula for the shear viscosity coeccient from the kinetic theory using the second-order G rad's method. This is one of the goals in the present article. The derivation follows Ref. [45] and is generalized for a particle system out of chemical equilibrium.

A nother goal is to elaborate on the breakdown region of the second-order viscous hydrodynam ics. To do this we investigate the tim e evolution of a gluon matter in a one-dimensional expansion with B jorken boost invariance [46] by solving the Israel-Stewart hydrodynam ic equations [37] as well as by performing similar BAM PS transport calculations for comparison. We quantify the deviation of the gluon distribution function from kinetic equilibrium and show the region with large deviation, where the applicability of the Israel-Stewart hydrodynam ics is questionable.

The article is organized as follows. In Sec. II we introduce theoretical framework for deriving viscosity from the kinetic theory using second-order G rad's method. We consider a massless particle system, which undergoes a one-dimensional expansion with B prken boost invariance. A comparison with the results obtained by the Navier-Stokes approximation [12] is given in Sec. III. Using the formula derived in Sec. II we calculate the shear viscosity to entropy density ratio =s of gluon matter: in Sec. IV an iterative and self-consistent approach is introduced to calculate =s from the Israel-Stewart hydrodynamics, whereas the results from BAM PS calculations are presented in Sec. V. For both hydrodynamic and transport calculations, deviations from kinetic as well as chemical equilibrium are shown and analyzed. Conclusions are given in Sec. VI.

# II. SHEAR VISCOSITY COEFFICIENT FROM SECOND-ORDER KINETIC THEORY

Relativistic causal dissipative hydrodynam ic equations can be derived from the kinetic theory by applying G rad's method of moments [47]. A detailed derivation is reported in Refs. [45, 48] and a prescription for calculating transport coe cients is also given there. In this section we will follow Ref. [45] to derive an expression for the shear viscosity coe cient when the considered system is out of chemical equilibrium.

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The basic equation of relativistic kinetic theory is the Boltzm ann equation

$$p @ f(x;p) = C [f(x;p)]$$
 (1)

for a one-particle phase-space distribution function  $f(x;p) = \frac{dN}{\frac{1}{(2-)^3} d^3p d^3x}$ . C [f(x;p)]denotes the collision term, which accounts for all microscopic interaction processes among particles. The entropy four-current is defined by [45, 49]

$$s = \frac{Z}{(2)^{3}p^{0}} p f(x;p) [ln(f(x;p)) 1]:$$
(2)

The entropy production is then given by

$$Z \qquad Z \qquad Z \qquad Z \qquad dw \ C \ f(x;p) \ln f(x;p) = dw \ C \ C \ f(x;p) \ln f(x;p) \qquad (3)$$

with the short notation  $dw = \frac{d^3p}{(2)^3p^0}$ .

We now assume that the deviation of f(x;p) from the equilibrium distribution  $f_{eq}(x;p)$  is small:

$$f(x;p) = f_{eq}(x;p)(1 + (x;p))$$
 (4)

where (x;p) 1 and

$$f_{eq}(x;p) = e^{\frac{u \cdot p}{T}} :$$
(5)

(x) and T (x) denote the local fugacity and tem perature, respectively. u (x) is the hydrodynam ic four-velocity of the medium. Equation (5) is the standard form for Boltzmann particles. The derivation below can be easily extended for Bose and Ferm i particles. In addition, we will restrict the following discussions to the case of massless particles (e.g., gluons).

We expand (x;p) up to second order in momentum, that is,

$$(x;p) = (x) (x)p + (x)p p;$$
 (6)

where the momentum -independent coe cients can be expressed in terms of the dissipative currents , q and denoting bulk pressure, heat ux and shear tensor [45, 48]:

$$= A_2(3u u) \qquad B_1u_(q) + C_0 \tag{7}$$

$$= A_1 u \qquad B_0 q \tag{8}$$

$$= A_0 \tag{9}$$

with the projector = g uu and symmetrization operation  $u_{(q_{)}} = \frac{1}{2}(u q + u q)$ . The metric used in this work is g = diag(1; 1; 1; 1). In general, the dissipative uxes are dened as projections of deviations of the energy-momentum tensor T and particle four-current N from their equilibrium form [45, 48]:

$$= \frac{1}{3} \qquad T \tag{10}$$

$$q = u T \frac{4}{3} N \tag{11}$$

$$= T^{< >} = \frac{1}{2} + \frac{1}{2} \qquad \frac{1}{3} \qquad T \qquad (12)$$

with the denitions N =  $\stackrel{R}{dwpf}$ , T =  $\stackrel{R}{dwpf}$  and T = T  $T_{eq}$ , N = N  $N_{eq}$ .

W e use the following local matching conditions on the energy and particle densities:

$$e = e_{eq} = \frac{3 T^4}{2}$$
 (13)

$$n = n_{eq} = \frac{T^3}{2}$$
(14)

with the de nitions for the densities e = u T u and n = u N. The local tem perature simply follows as T = e=3n. The fugacity is then calculated via  $= n=(\frac{1}{2}T^3)$ . One obtains immediately u T u = 0 and u N = 0. The bulk pressure from Eq. (10) then becomes

$$(g \quad u u) T = T = 0$$
 (15)

for massless particles, since the energy momentum tensor is traceless in this case. Thus,

= 0 according to Eq. 0).

In the follow ing, we will consider a one-dimensional B jorken expansion [46]. This implies that in the local rest frame, the distribution function f(x;p) is symmetric when transforming p to p. Thus in the local rest frame,  $T^{0i} = 0$  and  $N^{i} = 0$ , where i = 1;2;3. The heat ux q (11) vanishes in the local rest frame because

$$q = g u T \quad u u T \quad \frac{4}{3}g N + \frac{4}{3}u u N = u T \quad \frac{4}{3}N = 0:$$
 (16)

We obtain then p = 0 [see Eq. (9)].

For a one-dimensionally expanding system, Eq. (6) thus reduces to

$$(x;p) = (x)pp :$$
 (17)

Putting  $f = f_{eq}(1 + \cdot)$  into Eq. (3) and using the linearization

$$\ln(1 + ) = (x)pp$$
 (18)

we rewrite Eq.(3) as

U

For the second-last identity in Eq. (20), we used the energy-momentum conservation:  $\begin{bmatrix} R \\ dw p \ C \ [f(x;p)] = \ 0 \\ dw p p \ f = \ 0 \\ T = 0. Equation (20) describes entropy pro$ duction due to particle production (0 N > 0 for < 1) and absorption (0 N < 0 for> 1).

W ith the de nitions

$$P = \frac{Z}{dwppC[f(x;p)]}$$
(21)

$$C = dw C [f(x;p)] = Q N ;$$
 (22)

which are the 2nd and the 0th moment of the collision term the entropy production in Eq.(19) can be now written in a more compact form

$$Q s = C \ln P :$$
 (23)

In general, the entropy production in an imperfect uid can be expressed by the positive de nite form [25, 50, 51]

where , , and are non-negative coe cients denoting the bulk viscosity, heat conductivity and shear viscosity, respectively. J = 0 N is the source of particle production [50, 51] and is identical with C (22). For a chemically equilibrated system J vanishes. Com paring Eq. (23) to (24) we nd

$$P = (2 T)^{\perp}$$
; (25)

because in our case = 0 and q q = 0 as discussed above. The expression (25) is exactly the same as obtained in [45] and describes entropy production due to shear viscous e ects.

We then obtain the nalexpression for the shear viscosity coe cient

$$= \frac{1}{2T P} = \frac{1}{2TC_0 P}$$
(26)

The last identity is due to the fact that q vanishes in the local rest fram e and thus  $u_{(q)}P = 0$ . We note that the derived formula (26) is an approximate expression of the true shear viscosity. We call the \second-order" shear viscosity, because we have used term s up to second order in momentum for (x;p) [see Eq. (6)].

To calculate  $C_0$  we go to the local rest fram e, i.e., u = (1;0;0;0), where

$$= T = T \qquad T_{eq} = dw p p p p f_{eq}(x;p)$$
(27)

is valid according to Eqs. (12) and (17) for a (0+1) dimensional expansion. In this frame

[see Eq. (7)] reduces to

$$= C_0$$
 : (28)

Calculating the integrals in Eq. (27) with  $f_{eq} = e^{E = T}$  gives

$$(1 \quad C_0 40 \quad T^6 = {}^2)^{0j} = 0; \quad j = 1;2;3$$
 (29)

$$(1 \quad C_0 8 \quad T^6 = {}^2)^{ij} = 0; \quad i; j = 1; 2; 3:$$
 (30)

We have used the fact that is traceless and  $^{00} = 0$  due to the m atching condition (13) and T<sup>00</sup> = e in the local rest fram e. For a system undergoing a one-dimensional B jorken expansion, i.e., in a (0+1) dimensional case, all o -diagonal elements of T - and thus as well - vanish in the local rest fram e, particularly T<sup>0j</sup> =  $^{0j} = 0; j = 1; 2; 3$ . Thus we obtain

$$C_0 = \frac{2}{8 T^6}$$
 (31)

If the third spatial coordinate is chosen as the expansion axis, we have  $T^{11} = T^{22}$ , and in the local rest fram e the shear tensor takes the form

which is also given in [51]. We thus obtain

$$=\frac{3}{2}^{2}$$
 (33)

$$P = C_0 \quad P = \frac{C_0}{2} (3P^{33} P^{00}); \qquad (34)$$

where we have used  $P^{11} + P^{22} = P^{00} P^{33}$ , because P is traceless following from the de nition (21). Putting Eqs. (27) and (34) into (26) gives the shear viscosity coe cient for a (0+1) dimensionally expanding system of massless particles:

$$= \frac{3}{2TC_{0}(3P^{33} P^{00})} = 4n \frac{T^{2}}{P^{33} \frac{1}{3}P^{00}} :$$
(35)

For the last identity, we have used the matching conditions (14) and Eq. (31).

The energy density e, the tem perature T and the shear component in a (0+1) dimensional expansion can be calculated by solving viscous hydrodynam ic equations with a given value of shear viscosity . If is known, the distribution function f is known too [see Eqs. (4), (17) and (28)]. One can thus evaluate P<sup>00</sup> and P<sup>33</sup> according to their de nitions (21). Then can be calculated employing Eq. (35). In sSec. IV we will introduce an iterative and self-consistent prescription to calculate the second-order shear viscosity.

On the other hand, f can be obtained by solving the Boltzm ann equation (1) directly employing transport simulations. Then can be easily extracted using Eq. (35). Such calculations will be presented in section V. The results will be compared with those obtained in Sec. IV. As it turns out, a ratio of m can transport free path to expansion time being larger than unity and the variance of (x;p) being larger than unity will possibly indicate the breakdown of the second-order viscous hydrodynam ics. In this regime the validity of (35) is also questionable.

III. COMPARISON TO SHEAR VISCOSITY FROM NAVIER-STOKES AP-PROXIMATION

In R ef. [12], the shear viscosity coe cient was derived assuming the Navier-Stokes approximation

$$= 2 r^{<} u^{>}$$
: (36)

It reads

$$_{NS} = \frac{1}{5}n \frac{hE = 3}{\frac{1}{3}} \frac{p_{2}^{2} = E}{hp_{2}^{2} = E^{2}i} \frac{p_{2}}{P} \frac{1}{R^{tr} + \frac{3}{4}\theta_{t}(\ln n)}$$
(37)

where

Х

$$R^{tr} = \frac{R}{\frac{dw}{E^{2}}} \frac{\frac{p_{z}^{2}}{E} C [f]}{n (\frac{1}{3})} \frac{h_{z}^{2} = E^{2} i R}{h_{z}^{2} = E^{2} i}$$
(38)

is the total transport collision rate, which was introduced in [38]. A ll integrals are expressed in the local rest fram e. hi denotes the average over particle m om entum .

Equation (26) can be used to calculate the shear viscosity if the shear tensor obeys the Israel-Stewart equation [51]

$$- + = 2$$
 T Q  $\frac{1}{2}$  T U ; (39)

where = r < u > and denotes the relaxation time [see also Eq. (47) below ]. Equation (39) is more general than (36) in the rst-order (Navier-Stokes) theory.

Ifwede ne

$$R_{G rad}^{tr} = \frac{P^{33} \frac{1}{3}P^{00}}{n \frac{1}{3}hE^{2}i hg^{2}i};$$
(40)

then the shear viscosity from the G rad's method (35) can be rewritten to

Х

$$_{G rad} = 4n \frac{T^{2}hE = 3}{\frac{1}{3}hE^{2}i} \frac{p^{2}=Ei}{hg^{2}i} \frac{p}{R_{G rad}^{tr}}; \qquad (41)$$

where we have used =  $T^{33}$   $T_{eq}^{33} = T^{33}$   $\frac{1}{3}T^{00} = nhp_2^2 = E$  E = 3i. R em em ber that P is the second m om ent of the collision term [see Eq. (21)]. The expression (41) is sim ilar to Eq. (37) except for the term  $\frac{3}{4}Q_t(\ln )$ , which indicates that chem ical equilibration contributes explicitly to the shear viscosity in the N avier-Stokes approximation rather than in the Israel-Stewart approach.

In the next section, we calculate the shear viscosity in a gluon system within the Israel-Stewart approach and compare the result with that obtained using the Navier-Stokes approximation [12].

# IV. CALCULATION OF SHEAR VISCOSITY IN A GLUON SYSTEM :AN ITER-ATIVE AND SELF-CONSISTENT PRESCRIPTION

In this section we want to calculate the shear viscosity to the entropy density ratio =s for a gluonic system, which undergoes a one-dimensional expansion with B jorken boost invariance, i.e., a (0+1) dimensional expansion.

#### A. Prescription

For a (0+1) dimensional case the shear tensor in the local rest frame is given by Eq. (32). Then the gluon distribution function in the local rest frame reads

$$f(x;p) = e^{\frac{E}{T}} 1 C_0 (p_z^2 p_z^2 = 2)$$
 (42)

according to Eqs. (4), (17), (28) and (32). If , T and are known, the shear viscosity can be calculated according to Eq. (35), where P are evaluated by Eq. (21) via Eq. (42). Note that for the case of a gluonic system the value of has to be amplied by the degeneracy factor of gluons  $d_G = 16$ . We thus de ne  $_g = d_G$ . In addition, the gluon entropy density is given by

$$s_{g} = u \ s = d_{g} \ dw \ p_{0} f(x;p)(\ln f(x;p) \ 1) \ (4 \ \ln )_{g} \ \frac{9 \ g^{2}}{8n_{g}T^{2}};$$
(43)

where  $n_g = d_G T^3 = 2$  and  $g = d_G$  are the gluon number density and the gluon shear component, and we have used the approximation  $\ln(1+)$  for small =  $G(p_z^2 p_z^2=2)$ . We note that can be larger than unity for large momenta. In these cases, the expansion [also for Eq. (19)] fails. On the other hand, the distribution function f(x;p) becomes very smallat large momenta. The elect of the invalid expansion on the integrated quantity  $s_g$  is thus negligible at this point.

In principle, = (f  $f_{eq}$ )= $f_{eq}$  gives the relative deviation from kinetic equilibrium. However, is also a function of m on entum. The average h (x;p) $i_{eq}$  over m on entum distributed in equilibrium, i.e., using f(x;p) in zeroth order of , is obviously zero. We introduce the variance =  $p \frac{p}{h^2 i_{eq}}$  as the quantity determ ining the deviation from kinetic equilibrium and we nd  $p_{-}$ 

$$= \frac{9^{2} \overline{2}}{4} \frac{j_{g} j_{g}}{e_{g}}; \qquad (44)$$

where  $e_g = 3n_g T$  is the gluon energy density.

If the deviation from the local kinetic equilibrium is su ciently small, then the dynamical expansion in a (0+1) dimensional case can be well described by the Israel-Stewart (IS)

viscous hydrodynam ic equations [25, 37, 45, 48, 51, 52]:

$$\frac{\mathrm{d}n_{\mathrm{g}}}{\mathrm{d}} = \frac{\mathrm{n}_{\mathrm{g}}}{\mathrm{r}}; \tag{45}$$

$$\frac{\mathrm{d}\mathbf{e}_{\mathrm{g}}}{\mathrm{d}} = \frac{4}{3} \frac{\mathrm{e}_{\mathrm{g}}}{\mathrm{g}} + \frac{\mathrm{g}}{\mathrm{g}}; \tag{46}$$

$$\frac{d_{g}}{d} = -\frac{g}{2} \frac{1}{2} \frac{1}{g} \frac{1}{2} + \frac{1}{2}T\frac{\theta}{\theta}(\frac{2}{T}) + \frac{2}{3}\frac{1}{2}; \qquad (47)$$

where  $_2 = 9 = (4e_g)$  and  $= 2_{2g}$  denotes the relaxation time. Equation (47) is just Eq. (39) expressed in the local rest frame using the hydrodynamic velocity  $u = \frac{1}{2}(t;0;0;z)$ , where  $= \frac{p}{t^2} \frac{1}{z^2}$ . In derivation of Eq. (39), which is discussed in Ref. [51], only terms of second order in gradients and dissipative ux have been included. If in Eq. (44) is larger than unity, further terms containing  $2 (=e_1^2) (1_2)^2$  are no longer small enough anymore to be ommitted in derivation of Eq. (39) and thus in Eq. (47) as well, i.e., a higher order hydrodynamic equation is needed. Thus the value of is an indicator for a breakdown of second-order hydrodynamic theory.

Equation (45) for the gluon density can be easily solved:

$$n_{g}() = n_{g}(_{0}) - \frac{0}{3};$$
 (48)

which is identical with the result from ideal hydrodynam ics. On the other hand, the energy density decreases slower than in ideal hydrodynam ics due to the viscous elects:

$$e_{g}() = e_{g}(_{0}) - \frac{0}{3}; \quad \frac{4}{3}:$$
 (49)

Thus we obtain the gluon fugacity

$$( ) = \frac{n_{g}( )}{n_{g}^{eq}( )} = \frac{n_{g}}{\frac{d_{g}}{2}T^{3}} = \frac{n_{g}}{\frac{d_{g}}{2}(e_{g}=3n_{g})^{3}} = {}_{0} {}_{0} {}_{0} {}_{0} {}_{0} {}_{i} (50)$$

where  $_0 = (_0)$ . The system will be continuously out of chemical equilibrium during the expansion, even if it is initially at local therm al equilibrium ( $_0 = 1$ ). The larger the viscosity, the smaller is the value of and the faster is the decrease of the fugacity. Inclusion of production and annihilation processes such as the gluon brem sstrahlung and its back reaction (gg \$ ggg) m akes chemical equilibration possible and thus, of course, Eq. (45) has to be m odi ed! However, in this work we will use Eq.(45) without any m odi cations. The derivation of new and altered equations and their solutions will be given in a forthcom ing publication [53].

O ne can solve Eqs. (46) and (47), if the initial values of  $n_g$ ,  $e_g$ ,  $_g$  and also the value of the shear viscosity  $_g$  are given. On the other hand, to calculate  $_g$  using Eq. (35) via Eq. (42) we need  $n_g$ ,  $e_g$ , and  $_g$ . It is obvious that an iterative algorithm has to be developed to calculate  $n_g$ ,  $e_g$ ,  $_g$  and  $_g$  self-consistently. This algorithm is as follows:

- 1. We solve Eqs. (45)–(47) with a guessed value of  $_{g}$ . The guessed value can be chosen arbitrarily because the nal result does not depend on it.  $_{g}=n_{g}$  is assumed to be a constant of time.
- 2. The obtained n<sub>g</sub>(), e<sub>g</sub>() and <sub>g</sub>() at a time are used to calculate <sub>g</sub>() according to (35). We calculate rst the moments P using f(x;p) in Eq. (42) with given n<sub>g</sub>();e<sub>g</sub>() and <sub>g</sub>().

3. We turn back to step 1. The value of  $_{q}()$  is used to solve Eqs. (46) and (47) again.

Iterations will continue, until the relative deviation of  $_{g}$  from the previous one is su cient sm all. The iterative procedure allows to calculate (), e() and n() as well as =s() in a consistent way for given interactions. We note that if  $_{g}=n_{g}$  is strongly time dependent, further iterations will be required to account for this time dependence. A re ned algorithm will be presented in [53].

To obtain  $_{g}$ , P has to be rst evaluated by (21) via (42). P is a second moment of the collision term and thus is determined by gluon interactions considered. The compact forms of the collision terms can be found in [34]. In this article elastic (gg ! gg) as well as brem sstrahlung (gg \$ ggg) processes inspired within perturbative QCD are responsible for the gluon dynamics. The di erential cross section and the elastic matrix element are taken as in Refs. [34, 39]:

$$\frac{d^{qq^{1} qg}}{dq_{p}^{2}} = \frac{9^{2}}{(q_{p}^{2} + m_{D}^{2})^{2}};$$
(51)

$$\mathbb{M}_{gg! ggg} \int^{2} = \frac{9g^{4}}{2} \frac{s^{2}}{(q_{2}^{2} + m_{D}^{2})^{2}} \frac{12g^{2}q_{2}^{2}}{k_{2}^{2} [(k_{2} - q_{2})^{2} + m_{D}^{2}]} (k_{2} - g_{2}) ($$

where  $g^2 = 4$  s. The D ebye screening mass

$$m_{D}^{2} = d_{G} \qquad s \qquad dw N_{c} f(x;p)$$
(53)

with  $N_c = 3$  is applied to regularize infrared divergences. A lthough gg \$ ggg processes are considered, they contribute only to the shear viscosity but not to chem ical equilibration,

because as mentioned above, particle number conservation is assumed at present to derive Eq. (45)). Im provements will be done in a forthcoming publication [53].

#### B. Results

Figure 1(a) shows  $_{g}=s_{g}$  as a function of the expansion time for two values of the coupling constant  $_{s} = 0.05$  and 0.3. The initial gluon system at  $_{0} = 0.4$  fm /c is assumed to be in therm all equilibrium with a temperature of  $T_{0} = 500$  MeV. Each of the results indicated by the symbols in Fig. 1 is obtained by about 40 iterations with a guessed value of  $_{g}$  (guessed) =  $0.5 s_{g}^{eq}$ . From Fig. 1(a) we see that the ratio  $_{g}=s_{g}$  is almost constant in time for  $_{s} = 0.3$ , whereas for  $_{s} = 0.05$ ,  $_{g}=s_{g}$  increases moderately. The assumption underlying the iterative algorithm that  $_{g}=n_{g}$   $4_{g}=s_{g}$  does not depend on time is justiled accordingly. One nds that  $_{g}=s_{g}$  0:18 for a coupling of  $_{s} = 0.3$  and  $_{g}=s_{g}$  3 for  $_{s} = 0.05$ .

The results for the gluon fugacity (obtained from the solution of Eqs.(45)-(47)) depicted in Fig. 1(b) show a strong time dependence. The smaller the value of  $_{s}$ , i.e., the larger the  $_{g}=s_{g}$ , the faster is the deviation from the chemical equilibrium. This quantitatively demonstrates the consideration from above [see Eqs. (50)].

W hen putting Eq. (42) into Eq. (21) one realizes that P  ${}^{2}C_{0}$  in leading order of . Thus  ${}_{g}$  does not depend on . Secondly, from Eq. (43) we obtain  ${}_{s}=T^{3}$  (1 ln ). Thus,  ${}_{g}={}_{s}$  1= (1 ln ) and will increase slower than a logarithm ical behavior when decreases: a stronger decrease of (com paring the result for  ${}_{s} = 0.05$  with that for  ${}_{s} = 0.3$ in the lower panel of Fig. 1) will lead to stronger increase of  ${}_{g}={}_{s}$ , as seen in the num erical results shown in Fig. 1(a).

Figure 2(a) shows the deviation from kinetic equilibrium, from Eq. (44), as a function of time scaled with the initial time. For  $_{\rm s} = 0.3$  the value of starts at zero (equilibrium), increases until 3  $_{0}$  and then relaxes to zero. The system rst evolves out of equilibrium and then relaxes back to equilibrium . On the contrary, increases continuously when employing a much weaker (and unphysically low) coupling  $_{\rm s} = 0.05$ . In this case the system is always out of equilibrium. To explain the di erent behaviors we de ne R  $_{\rm OE}$  as the ratio of the mean transport free path,  $1={P \atop {\rm R} {\rm tr}_{\rm Grad}} {\rm de ned}$  by Eq. (40), to the Hubble-like expansion time scale :

$$R_{OE} = \frac{tr}{R} = \frac{P}{R_{Grad}^{tr}}$$
(54)

O ur concept of  $R_{OE}$  is similar to that introduced in [37], where the authors demonstrate that the ratio of expansion time to the mean free path controls the deviation from equilibrium. For a xed  $_{g}=s_{g}$  the mean transport path  $^{tr} = 1 = {}^{P} R_{Grad}^{tr}$  changes with time. At full equilibrium  $^{tr}$  1=T  $^{1=3}$  and thus  $^{tr}=$   $^{2=3}$ . If  $R_{OE}$  is larger than unity, the system starts to depart from equilibrium. If  $R_{OE}$  is smaller than unity, the system relaxes to equilibrium  $R_{OE}$  () is shown in Fig.2(b). With  $_{s} = 0.05$  the system evolves far away from equilibrium and the evolution is dominated by free stream ing. The ratio  $R_{OE}$  is a measure of the ability of the system to relax to kinetic equilibrium. For  $_{s} = 0.05$  kinetic equilibration is not possible for the timescales shown. The regime for which the system can not come close to kinetic equilibrium is for the coupling  $_{s} = 0.1$  0.2 corresponding to a shear viscosity to entropy density ratio =s = 0.8 0.4.

In addition, is larger than unity at  $> 3_0$  for  $_s = 0.05$ . The true entropy density  $s_g$  should be smaller than that estimated according to Eq. (43), because the expansion  $\ln(1 + )$  is not valid any more for large. The derivation of the shear viscosity in Eq. (35) becomes questionable as well, since the same expansion is used to obtain the entropy production (19).

Finally, in Figs. 3 and 4 we compare the results on  $a=s_a$  from the second-order (IS) kinetic theory with those presented in Ref. [12] using the Navier-Stokes approximation. The solid (dotted) curve in Fig. 3 depicts the contribution of gg ! gg (gg gg) to  $_{g} = s_{g}$ obtained in [12]. The solid (dotted) curve with sym bols depicts the results from the present calculations at  $= 2_0$ , at which the system is still near therm all equilibrium. We see that the results following from the second-order expansion are mostly larger than those based on the Navier-Stokes scheme, both for gg ! gg and for gg \$ ggg processes. At (unphysical) small  $_{\rm s}$  the dierence between the results is given by a factor of 2 3. In particular, the dierence between the second-order and the Navier-Stokes results for brem sstrahlung gg  $\$  ggg is bigger than that for elastic gg ! gg process. At large  $_{\rm s}$  the gg  $\$  ggg processes play a dom inant role (com pared with gg ! gg) in low ering  $_{q}=s_{q}$ , whereas at sm all s this dom inance becomes weaker [11]. In Fig. 4 the results on =s im plementing both elastic and inelastic processes are shown for the physical region of s. Here the di erence between second-order and N avier-Stokes based calculations is approximately 50% (  $_{\rm s}$  = 0.2)-20% (  $_{\rm s} = 0.3$ )-0% (  $_{\rm s} = 0.6$ ).

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V. CALCULATION OF SHEAR VISCOSITY IN A GLUON SYSTEM : TRANS-PORT SIMULATIONS EMPLOYING BAMPS

In this section, we solve the Boltzm ann equation for gluons using the parton cascade Boltzm ann Approach of MultiParton Scatterings and repeat the task in the previous section to calculate the shear viscosity to entropy density ratio  $_g=s_g$  in a B prken-type onedimensional (0+1) expansion. We calculate  $_g$  and  $s_g$  according to Eqs. (35) and (43) by extracting P ,  $_g$ ,  $n_g$  and  $e_g$  from the transport simulations.

The partonic cascade BAM PS which was introduced in [34, 38] has been applied for a (0+1) dimensional expansion to study them alization of a color glass condensate potentially produced in ultrarelativistic heavy ion collisions [39]. We take the same numerical setup for BAM PS as considered in [39]. The initial condition and interactions of gluons are the same as given in the previous section. In the parton cascade calculations, di erent from calculations using the viscous hydrodynamic equations (45)-(47), the inelastic gg \$ ggg processes lead to a net particle production or absorption, i.e.,  $@N_g \notin 0$ , which drives the chemical equilibration.

We note that particle num ber changing processes are implemented in BAMPS, whereas the particle num ber was considered to be constant in previous section. Therefore we are not able to make a direct comparison between BAPMS results and those calculated by solving Israel-Stewart equations.

Figure 5 shows  $_{g}=s_{g}$  extracted within the space time rapidity interval  $_{s} 2$  [ 0:1:0:1], where  $_{s} = \frac{1}{2} \ln[(t+z)=(t-z)]$ . When comparing these results with those shown in the upper panel of Fig. 1 we not that they are almost the same for  $_{s} = 0.3$ , whereas for  $_{s} = 0.05$  the increase of  $_{g}=s_{g}$  is slightly weaker in BAM PS calculations than in viscous hydrodynamic ones. The reason for this difference is the different behavior of the gluon fugacity (remember that  $_{g}=s_{g} = 1 = (1 - \ln - 1)$ ). The gluon fugacity extracted from BAM PS is shown in Fig.6. Its value is larger than that shown in the lower panel of Fig. 1, because ongoing chemical equilibration is realized in the BAM PS calculations.

The kinetic equilibration is demonstrated in Fig. 7(a) via the variance and in Fig. 8 via the momentum isotropy Q (t) =  $\langle \frac{p_z^2}{E^2} \rangle$ . The results on are similar to those in Fig. 2 and can be well understood by the out-of-equilibrium ratio R<sub>0E</sub> shown in Fig. 7(b). For <sub>s</sub> = 0:3 the transport mean free path is shorter than the expansion rate whereas for

 $_{s}$  = 0.05 the evolution is dominated by expansion. M on entum isotropization, shown in Fig. 8, is practically restored for  $_{s}$  = 0.3 at later times, whereas for  $_{s}$  = 0.05 this restoration is not possible. Here again the dimension between transport and viscous hydrodynamic calculations stem from the dimension of the gluon fugacity. To make fair comparisons, modications in the hydrodynamic equations will be done in the near future [53] to take into account the chemical equilibration.

As pointed out already in the previous section, the parameters for which the system cannot come close to kinetic equilibrium are the couplings of  $_{s}$  0:1 0:2 corresponding to a ratio = s 0:8 0:4. For such parameters, the ratio  $^{tr}$ = is of the order of 1 at late times and the system becomes highly di usive and viscous.

Finally, in Fig. 9 we investigate deviations from equilibrium of the gluon distribution in BAMPS calculations at large momentum. Figure 9 shows the non-equilibrium part of the transverse spectrum (normalized to the equilibrium spectrum )  $\frac{dN = (p_T dp_T d)}{dN e_q = (p_T dp_T d)}$ 1 from BAM PS calculations and the quantity  $\langle \rangle_{p_z}$  (;T;) =  $\int_{eq}^{T} f_{eq}$  (;T;) dp<sub>z</sub> =  $\int_{eq}^{T} f_{eq} dp_z$  [with  $(x;p) = \frac{2}{8 \pi^6} (p_z^2 - \frac{1}{2}p_T^2)$ , which is the analytically calculated second-order contribution to the transverse spectrum, as a function of the transverse momentum  $p_T$  at  $= 4_0$ . The average  $\langle \rangle_{p_z}$  is calculated using ;T; extracted from the particular BAM PS calculations. The comparison of  $\frac{dN = (p_T dp_T d)}{dN_{eq} = (p_T dp_T d)}$  1 and  $\langle \rangle_{p_z}$  from Fig. 9 shows that for  $_{\rm s}$  = 0.05 the distribution function in BAM PS contains contributions higher order in  $\rm p_{T}$ and thus the second-order ansatz (17) is not su cient to describe the evolution in and BAM PS. In contrast, for s = 0.3 the distribution function is reasonably good approximated by second-order kinetic theory over the shown momentum range. Thus we argue that the dependence of on  $=(T^4)$  is stronger than given by ansatz (17), since  $=(T^4)$ quanti es the strength of dissipative e ects, which are stronger at  $_{s} = 0.05$ . Inclusion of additional terms in Eq. (17) would lead to a modi cation of the evolution equation for , which follows from the conservation law for the energy momentum tensor: 0 = 0 T  $\binom{R}{P} p p f_{eq}(1 + )$ . If employing s = 0.05(=s 3) for large p > 2.3 GeV the variance < ><sub>pz</sub> becomes larger than 1. For <sub>s</sub> = 0.3 this happens at  $p_T$  > 2.75 GeV. For transverse m on enta larger than these critical values the expansion  $\ln(1+)$  done to obtain Eq.(9) is invalidated. Thus in the calculation of the entropy density (and entropy production) the  $\frac{2}{2}$  (p<sub>T</sub> p<sub>crit</sub>), i.e. higher order  $\ln(1+)$  term should be approximated by  $\ln(1+)$ terms should be taken into account in the integration over the momentum for  $p_T > p_{T crit}$ .

However, with =s = 0.18 this correction is less than 0.5%, which is due to the sm allness of . With =s = 3 the correction is 6%. Thus for physical values of =s - 0.2 second-order hydrodynam ics is valid, even though form ally breaking down at large  $p_T$ . In the unphysical regim e =s - 3 higher order corrections are not negligible. This deserves future investigation [53].

### VI. CONCLUSIONS

We have derived the shear viscosity coe cient from kinetic theory for massless particle system undergoing a one-dimensional expansion with B jorken boost-invariance. The derivation makes use of G rad's moment method [45, 47] and is based on an expansion of the distribution function up to second order in momentum. The nalexpression obtained in the present work is similar to the one based on the Navier-Stokes theory [12], but the transport rate has to be calculated in a di erent way. How close the result obtained using G rad's m ethod approxim ates the true value determ ined using the K ubo-G reen form ula [54] will be studied and reported in a forthcoming publication. The values needed to calculate the shear viscosity [Eq. (35)] are shear tensor , the particle and energy densities e and n, the fugacity and nally the second moments P of the collision term from the underlying kinetic process. They can be calculated either using transport setup solving the kinetic theory or from dissipative hydrodynam ic (Israel-Stewart) equations (45)-(47). However, the IS equations them selves need the value of shear viscosity as a param eter. Thus we introduce a new iterative method that allows us to solve Israel-Stewart equations and calculate =s as a function of time and coupling constant s. The results on s =s calculated in the partonic cascade BAM PS and from IS theory are in a good agreem ent for physical coupling s = 0.3. In this regime we obtain =s = 0.18. As a further demonstration even for unphysical small coupling  $_{s} = 0.05$  the di erence between BAM PS and second-order hydrodynam ic calculations of =s is small. We obtain =s 3 in this regime. At such small coupling =s increases slightly in BAM PS and som ewhat stronger in hydrodynam ic calculations. This increase is due to the intrinsic fugacity, which evolves di erently in both calculations.

U sing IS theory, we calculate =s ratio for a system close to equilibrium as a function of  $_{s}$ . For physical coupling  $_{s}$  0:3 the second-order result is approximately 20% higher than in calculations based on rst order Navier-Stokes theory [12]. For  $_{s} = 0.6 = s = 0.08$ 

within the Israel-Stewart and Navier-Stokes prescription.

Deviations of hydrodynamic evolution from equilibrium are quantied in the present work introducing the variance of the nonequilibrium part of the distribution function. We demonstrate that its value is smaller than unity and later decreases with time at a physical coupling s = 0.3 and thus our expression of is valid in this case. Here again hydrodynam ic and BAMPS results are in good agreement. For small coupling  $_{s} = 0.05$ hydrodynam ics does not relax back to equilibrium and G rad's method becomes invalid. In BAMPS in this regime the deviation of from equilibrium is smaller, which is an e ect of the ongoing chem ical equilibration. The ability of the system to restore kinetic equilibrium is quanti ed by the ratio of the m ean transport free path to the expansion time. We conclude that the second-order dissipative hydrodynam ics is applicable in the regim  $e = s^{<} 0.2$  which corresponds to values of  $s^{>}$  0.3. At high m om enta  $p_T > 3 \text{ GeV}$  it from ally breaks down, how ever for =s 0:2 0:4 it is applicable even for di erential observables. For really high 3 the applicability of hydrodynam ics certainly breaks down. For the interm ediate =s regime 0.3 < = s < 0.8 a m ore detailed analysis in the comparison of m icroscopic transport description to dissipative second- (or even higher) order hydrodynam ics is required.

To make consistent comparisons between the kinetic transport model BAM PS and IS solutions we have to modify the hydrodynam ic equation to take into account particle production and absorption. These calculations will be reported in a forthcom ing publication.

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FIG. 1: (Color online) (a) =s ratio and (b) fugacity calculated by the iterative procedure described in the text for  $_{s} = 0.05$  and  $_{s} = 0.3$  at ten di erent time points, with initial time  $_{0} = 0.4$  fm /c, T ( $_{0}$ ) = 500 M eV. The initial input value of =s is 0.5.



FIG.2: (Color online) (a)Variance and (b) ratio  $R_{0E}$  calculated by the iterative procedure.  $_{0} = 0.4$  fm /c.



FIG.3: (Color online) Ratio =s (contributions due to elastic and inelastic processes) as function of the coupling constant  $_{\rm s}$ . The result (solid line) is compared with results of Ref. [12] (dotted line)



FIG.4: (Color online) Ratio =s (all processes) as function of the coupling constant  $_{s}$ . The result is compared with result of Ref. [12]



FIG.5: (Color online) Ratio =s from the m icroscopic BAM PS simulation. Results are calculated using Eq. (35) for simulations with two dimensions for  $_{s.0} = 0.4$  fm =c



FIG. 6: (Color online) Fugacity =  $n=n_{eq}$  from BAMPS calculation. Results are shown for simulations with di erent (constant) values of s = 0.4 fm/c.



FIG.7: (Color online) (a) Variance and (b) ratio  $R_{OE}$  calculated by BAM PS.  $_0 = 0.4$  fm /c.



FIG.8: (Color online) M om entum isotropy <  $p_z^2 = E^2$  > calculated by BAM PS.  $_0 = 0.4$  fm /c.



FIG.9: (Color online) Nonequilibrium part of the transverse spectrum (normalized to the equilibrium spectrum)  $\frac{dN = (p_T dp_T d)}{dN_{eq} = (p_T dp_T d)}$  1 from BAMPS calculations (lines with points) and the second-order contribution to the transverse spectrum  $\frac{\int f_{eq} (f_T; dp_Z)}{\int f_{eq} dp_Z}$  (lines) as function of  $p_T$  at  $= 4_0$  with ;T; extracted from BAMPS.