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JN-METD1

A FORTRAN-IV PROGRAMME FOR SOLVING NEUTRON TRANSPORT PROBLEMS WITH ISOTROPIC SCATTERING IN BARE SPHERES AND HOMOGENEOUS SLABS BY THE j_N METHOD

by

T. ASAOKA

1971

Joint Nuclear Research Centre Ispra Establishment - Italy **Reactor Physics Department Reactor Theory and Analysis**

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The method has the practical advantage that the eigenvalues and eigenfunctions of the integral equation converge to the exact values very rapidly as the order of the j_x approximation increases. The eigenvalues can be computed in the j_x method without any knowledge of the eigenfunctions which are therefore only evaluated by the code if required (e.g. the flux in selected energy groups at selected space points). This fact makes for a high computational efficiency.

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ABSTRACT

This report summarizes the mathematical solution of neutron transport problems in a bare sphere and infinite homogeneous slab according to the new analytical j_x method, spherically symmetric scattering in the laboratory system being assumed. It also describes in detail a Fortran-IV computer programme JN-METDl for accurately solving both the stationary and time-dependent problems.

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KEYWORDS

FORTRAN PROGRAMMING NEUTRON TRANSFER ISOTROPY SCATTERING SPHERES MATHEMATICS COMPUTERS EIGENVALUES EIGENFUNCTIONS INTEGRAL EQUATIONS

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JN-METDl, A FORTRAN-IV PROGRAMME FOR SOLVING NEUTRON TRANSPORT PROBLEMS WITH ISOTROPIC SCATTERING IN BARE SPHERES AND HOMOGENEOUS SLABS BY THE j_N METHOD *)

1. Int roduct ion

N *'*

The j_{N} method has been developed during the last ten years to achieve a simple but accurate analytical approach to neutron transport in a finite system. One of the essential points of the method lies in the expansion into spherical Bessel functions of the Laplace-Fourier transformed emission density of neutrons (or the distribution of secondary neutrons) and the kernel of the integral equation (resulting from the Laplace and Fourier transformations of an integral transport equation with respect to time and space, respectively). For spherical and plane geometries, the expansion of the transformed flux rather than the transformed emission density with respect to the Fourier transform variable is equivalent to an expansion of the original flux in Legendre polynomials with respect to space¹⁾²⁾. Due to the expansion of the emission density, our final ex $t \sim t$ space . Due to the expansion of the emission density, our final ex- t and t pression of the flux exactly satisfies the boundary conditions independently of the order of the j_w approximation (truncation order of the expansion).

The method has already been applied successfully to space-energy timedependent transport problems in a bare spherical system³ as well as dependent transport problems in a bare spherical system as well as space-angle energy-time dependent problems in an infinite homogeneous slab with finite thickness⁴) (always assuming that the scattering of neutrons is spherically symmetric in the laboratory system). The neutron flux for a stationary state has also been obtained as a simple limiting case of for a stationary state has also been obtained as a simple limiting case of time-dependent problems. A computer code for stationary problems in a homogeneous slab has been adapted for calculating also the first and second time moments of the flux due to an incident delta function source⁵).

An extention of this approach to take into account anisotropic scattering of neutrons as well as multilayer slab systems can easily be performed, as already shown by several authors $6)$ -9). Furthermore, the application of the method to convex geometries has recently been demonstrated for a homogeneous medium in which the neutron scattering is isotropic^{1o)}. In this work, an expansion into ordinary Bessel functions of odd order was adopted for an infinite cylinder instead of the spherical Bessel functions for the slab and spherical geometries.

*) Manuscript received on 16 September 1970

The present report is concerned mainly with the computer code JN-METDl designed to solve neutron transport problems for bare spheres and infinite homogeneous slabs within the context of the multlgroup and (up to) j_{τ} approximation (scattering being assumed spherically symmetric). The code can deal with the following problems:

- (a) Stationary problems in bare spherical reactors to obtain the asymptotic time constant (decay constant of the fundamental mode), the value of the effective multiplication factor k_{eff} or the critical $\sum_{n=0}^{\infty}$ radius, and the flux distribution as a function of space and energy.
- (b) Stationary problems in homogeneous slabs to obtain the space, angle and energy dependent flux due to a plane isotropic, point isotropic or monodirectional boundary source. Also the first and second time moments are calculated for the time-dependent flux in the slab with a point isotropic or monodirectional delta function source on one boundary.
- (c) Time-dependent problems in a non-multiplying bare sphere without upscattering of neutrons to evaluate the space, energy and time dependent flux resulting from the incidence of an external source at the centre, the time behaviour of the source being described by a delta-function or the Gaussian distribution.
- (d) Time-dependent problems in a non-multiplying homogeneous slab without up-scattering of neutrons to evaluate the space, angle, energy and time dependent flux in the slab with a point isotropic or monodirectional source (described by a delta function or the Gaussian distribution in time) on one boundary.

2. Mathematical Formulae

Under the assumption of spherically symmetric scattering in the laboratory system, the j_N method has already been developed to deal with neutron transport in a bare sphere and an infinite homogeneous slab with finite thickness³⁾⁴⁾. We therefore only summarize the mathematical formulae here.

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2.1 Time-dependent problems in a bare sphere

We consider first a bare sphere of radius R within the context of a multigroup (G energy groups) model and the j_N approximation (with an odd value of N). Let Σ_j and V_j be the macroscopic total cross section and speed of neutrons in the g-th group respectively and $C(1^2)$ the mean number of secondaryneutrons produced in the g-th group as a result of a collision in the g¹th group.

The number of neutrons at the radial co-ordinate r and at time t resulting from a neutron source $S_{\zeta}S(t)S(\zeta)/(\partial \pi \zeta^2)$, in the case where R/V_{ζ} is finite, is written as³⁾ ([M] being the largest integer less than or equal to M)

$$
v_j n_j(r, t) = S_j exp(-\frac{1}{4}v_j t) S(t-r/v_j)/(4\pi r^2)
$$

+ $(1/r) \sum_{j=1}^{C(M+1)/2} \sum_{n=0}^{2M+1} B_{2n+1}(3, 4j) G_{2n+1}(5R, 5/R, 5444j) exp[54V_1(4j-1)t], (1)$

where

$$
G_m(\alpha_1, \xi, \Delta) \equiv \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{dR}{2} exp(-i\alpha_1 \xi R) \int_{m}^{\infty} (\alpha_1 R) \int_{0}^{\infty} \frac{dH}{4} exp(-\beta_1 \xi) \, \lim_{\Delta m} (\xi \xi) \, , \tag{2}
$$

in which $\dot{f}_m(\mathfrak{X})$ is the n-th order spherical Bessel function and P_i *i*-($I_1V_1\nrightarrow$ *x*(I_2V_2). The explicit expression for $G_{\mathcal{M}}(k'_1, \mathbf{y}, \mathbf{z})$ is shown in the Appendix 1, Section 4. In Eq. (1), $\mathcal{A} = \mathcal{I} \mathcal{U}_i \mathcal{A}_j$ and $\mathcal{B}_{\text{ML}}(\mathcal{J}_i \mathcal{A}_j)$ stand for a real pole and the residue of $B_{\mathfrak{M}}(q,\lambda)$ which satisfies the following linear equations (the notation $\sum_{n=0}^{N}$ indicates a sum only over odd values of n)î

$$
\frac{1}{2m+1} B_m(g/A) = \sum_{j=1}^{G} C(j+2) \sum_{n=0}^{N} J_{mn}(\Sigma_j R, \Delta) B_n(\Sigma_j A)
$$

+ $\frac{i}{2\pi} \sum_{j=1}^{G} S_j C(j+2) Z_j A_m(\Sigma_j R, \Delta), m=1, 3, \cdots, N,$ (3)

where

$$
J_{mn}(\alpha_1, \Delta) = \frac{\alpha_1}{\pi} \int_{-\infty}^{\infty} \frac{dP}{2} \int_m (\alpha_1 P) \int_n (\alpha_1 P) \int_0^{\infty} \frac{dP}{2} \exp(-P_1 Y) \sin(PY), \qquad (4)
$$

$$
\mathcal{A}_{m}(\alpha_{j},\Delta) \equiv \frac{\alpha_{j}}{\pi} \int_{0}^{\alpha_{j}} dy \exp(-P_{j}y) \int_{-\infty}^{\infty} \mathcal{A}^{2} \mathcal{A} \int_{0}^{\infty} (y^{2}) \int_{m} (\alpha_{j}^{2}) \, . \tag{5}
$$

The expressions for $\int_{\mathbf{M}\mathbf{R}} (\alpha'_1, \lambda)$ and $\mathcal{A}_\mathbf{M} (\alpha'_1, \lambda)$ are summarized respectively in the Appendix 1, Sections 1 and 8.

In the absence of up-scattering of neutrons in a non-multiplying bare sphere, Eq. (3) is reduced to

$$
\begin{split}\n\sum_{\substack{d\\ \text{atm}\\ \text{atm}}} & - c(g^{\prime}+g^{\prime}) \int_{\text{num}} (z_{\mathbf{j}'}R, \, d) \, \text{Im}(g^{\prime}, \, d) - c(g^{\prime}+g^{\prime}) \sum_{\substack{n=0\\ n+m}}^{N} \int_{\text{num}} (z_{\mathbf{j}}R, \, d) \, \text{Im}(q^{\prime}, \, d) \\
& = \frac{i}{2\pi} \sum_{i=1}^{d} S_{i} c(g^{\prime}+g^{\prime}) \sum_{\substack{n\\ \text{atm}\\ \text{atm}}} A_{\text{min}}(z_{\mathbf{j}}R, \, d) + \sum_{\substack{n=1\\ \text{atm}}}^{d} c(g^{\prime}+g^{\prime}) \sum_{n=0}^{N} \int_{\text{num}} (z_{\mathbf{j}}R, \, d) \, \text{Im}(q, \, d) \\
& = 4, 3, \cdots, N.\n\end{split}
$$
\n
$$
(6)
$$

This equation indicates that the problem of finding the pole $J = T_i N_i J_i$ of $B_m(q, \lambda)$ is the same as that in a one-group model:

$$
\det \left| \frac{\delta_{mn}}{2m+4} - c(3-\delta) J_{mn}(x_1R, d) \right| = 0, \quad m, n = 1, 3, 5, \cdots, N, \tag{7}
$$

and the total number of poles for the g-th group is $((N+1)/2)$? instead of $[(N+1)/2]G$, including all poles of the higher groups due to the presence of the last term on the right-hand side of Eq. (6).

2.2 Stationary problems in a bare sphere

From Eq. (1), the asymptotic behaviour as $t \rightarrow \infty$ can be written as

$$
\psi_{1}^{(1/2)}\left(\gamma,t\right)\sim(1/\gamma)\sum_{n=0}^{\lceil 1/\gamma/2\rceil}B_{2n+1}(3,\Delta_{1})G_{2n+1}(2n,R,\gamma/R),\chi\psi_{1}(\Delta_{1})\exp(\chi\psi_{1}(\Delta_{1}-1)t),
$$
\n(8)

 $-8 -$

where $\mathcal{A} = \Sigma_1 V_1 \mathcal{A}_1$ stands for the largest pole of $B_m(q, \mathcal{A})$ whose value is to be obtained by solving the determinantal equation:

$$
\det \left| \frac{S_{11'} S_{m1}}{2^{m+1}} - c (1^2)^2 \right| J_{m1}(Z_1 R, Z_1 V_1 A_1) \right| = 0,
$$
\n(9)

which gives the asymptotic time constant J_4 - $/$ as a function of the physical properties of a reactor and the geometrical dimension.

For a critical reactor, \mathcal{A}_j must be equal to unity and Eq. (9) with $\mathcal{A}_j = \{$ therefore gives the critical condition. In order to obtain the value of the effective multiplication factor k_{eff} for a given reactor, $C(3 \rightarrow 3')$ is divided into two parts. These are the scattering part $C_4(1+1)$ = Σ_1 (\uparrow ²)/ Σ_1 and the fission part C_f (\uparrow ²)'= χ_p (ν I_f)₁/ Σ_1 where χ_p stands for the proportion of fission neutrons born in the g-th group. Using this separation, the value of k_{eff} is obtained by solving Eq. (9) with $\mathbf{A}_i = \mathbf{A}$ and

$$
C(1^2)^{1/2} = C_4(1^2)^{1/2} + C_5(1^2)^{1/2} + C_6(1^2)^{1/2}
$$
 (10)

The ratios between the residues $B_m(q, \lambda_4)$ can now be obtained by the use of Eq. (3) with $S_q=0$ and Eq. (9) for any of the above-mentioned three problems, that is, the evaluation of the time constant, critical condition or $k_{eff}^{}$. Having thus obtained the residues, the flux distribution can be obtained from Eq. (8) for each problem.

2.3 Time-dependent problems in a homogeneous slab

We now consider here an infinite homogeneous slab with finite thickness a by assuming a neutron source $S_{\mathbf{g}}(\mu, t)$ incident with the direction cosine μ upon the surface at the space co-ordinate $\chi = 0$ *·* The number of the g-th group neutrons is then written as $4)$

$$
\iota_{\mathbf{y}} \eta_{\mathbf{y}}(x,\mu,t) = (\iota/\mu) S_{\mathbf{y}}(\mu,t-x/(\nu_{\mathbf{y}}\mu)) \exp(-z_{\mathbf{y}}x/\mu)
$$

+ $z_{\mathbf{y}} \sum_{n=0}^{N} B_{n}(\mathbf{y},\lambda_{\mathbf{j}}) F_{n}(z_{\mathbf{y}}a/2, x/a, \mu, z_{\mathbf{i}}\nu_{\mathbf{i}}\lambda_{\mathbf{j}}) \exp[z\nu_{\mathbf{y}}\nu_{\mathbf{j}}-1] + \frac{1}{2N} \int_{-\infty}^{\infty} d\mu \exp[-(z_{\mathbf{y}}\nu_{\mathbf{y}}-i\mathbf{y})t] \sum_{n=0}^{N} B_{n}(\mathbf{y},i\mathbf{y}+z_{\mathbf{y}}\nu_{\mathbf{y}}-z_{\mathbf{y}}\nu_{\mathbf{j}}) \times F_{n}(z_{\mathbf{y}}a/2, x/a, \mu, i\mathbf{y}+z_{\mathbf{y}}\nu_{\mathbf{y}}-z_{\mathbf{y}}\nu_{\mathbf{j}}),$

wheye

$$
F_{n}(\alpha_{1}',\xi,\mu,\Lambda)=\frac{1}{4\pi}\int_{-\infty}^{\infty}d\xi \exp[i\alpha_{1}'\xi(1-2\xi)]\int_{\mathcal{M}}(\alpha_{1}'\xi)\int_{0}^{\infty}d\eta \exp[-(\beta_{1}-i\xi\mu)\eta]\int_{\mathcal{M}}(12)
$$

(11)

the explicit expressions for $\overline{f}_M(x_1, \overline{5}, \mu, \Delta)$ and $\overline{f}_M(x_1, \overline{5}, \mu, \overline{t_1}+\overline{t_1}v_1-\overline{t_1}v_2)$ being given respectively in the Appendix 1, Sections 6 and 7. In the second term on the right-hand side of Eq. (11), the summation is performed only over the contribution coming from the poles of the $g^{\dagger}-th$ group $(g^{\dagger}=1,2,$..,g,...,G) which satisfy the condition $A_{j'j'} >$ $\frac{1}{7}V_{j'}(1/\sqrt[n]{})$ [at most, $j = 1,2,...$, $(N+1)G$. The function $B_{\mathcal{H}}(1,1)$ satisfies the following equation:

$$
\frac{1}{2n+1}B_n(1/A) = \sum_{j=1}^{G} C(1-j) \sum_{k=0}^{N} J_{nm}(I_j/2,A) B_m(1,A)
$$

+ $\sum_{j=1}^{G} C(1-j) \sum_{j} a S_j C_n(T_j/2,A) = n=0,1,2,\cdots,N,$ (13)

where

$$
S_{\mathbf{q}} C_{\mathbf{n}} (\alpha_{\mathbf{j}}, \Delta) = \frac{1}{2\pi} \int_{-\infty}^{\infty} d\mathbf{k} \exp(-i\alpha_{\mathbf{j}} \mathbf{z}) \int_{0}^{1} d\mu \int_{0}^{\infty} d\mathbf{t} S_{\mathbf{j}} (\mu, t) \exp[-(4 - \mathbf{i} \mu) + 1]
$$

$$
X \int_{0}^{\infty} d\mathbf{y} \exp[-(\beta_{\mathbf{j}} - i \mathbf{x} \mu) + 1]
$$
 (14)

For three cases where

- (a) $\hat{S}_1(\mu, t) = \hat{S}_1(s(t))$ (plane isotropic source),
- (b) $S_{\mathbf{J}}(\mu, t) = 2 S_{\mathbf{J}} \mu \delta(t)$ (point isotropic source),

(c)
$$
S_{\gamma}(\mu, t) = S_{\gamma} S(\mu - \mu)
$$
 $S(t)$ (monodirectional source),

the integral $\mathcal{C}_n(\alpha_j, \lambda)$ takes respectively the following forms:

$$
C_n^{\ a}(\alpha_j, \Delta) = \frac{1}{2\pi L} \int_{-\infty}^{\infty} \frac{dR}{2} \exp\left(-i\alpha_j R\right) \int_{-\infty}^{\infty} \frac{d\alpha_j}{2} \frac{1}{2} \pi R^j \left(\frac{e^{i2\alpha_j L}}{L}\right) \tag{15}
$$

$$
C_n^{\oint} (\alpha_1, \lambda) = \frac{1}{\pi \iota} \int_{-\infty}^{\infty} \frac{d\beta}{\beta} \exp\left(-i\alpha_1 \beta\right) \int_n (\alpha_1 \beta) \int_0^{\infty} \frac{d\beta}{\beta} \bar{\mathcal{L}}^{\beta}{}^{\beta} \left[\left(4 + \frac{i}{\beta \beta} \right) \bar{\mathcal{L}}^{i \beta} \right] - \frac{i}{\beta \beta} \right],
$$
 (16)

$$
C_n^c(\alpha_j, \Delta) = 2F_n(\alpha_j, 1, \mu_0, \Delta), \qquad (17)
$$

the explicit expressions for $C_n^a(\alpha_j, \lambda)$, $C_n^b(\alpha_j, \lambda)$ and $C_n^c(\alpha_j, \lambda)$ being shown in the Appendix 1, Sections 9, 10 and 12, respectively.

Since $J_{m,n}(x_j, \lambda) = 0$ when $m+n = odd$, a system of linear equations (13) can be split into two sets; one contains only the terms with even values of n and m and the other contains only those with odd values of n and m. Hence, for a non-multiplying slab in which there is no up-scattering of neutrons, the poles of $B_n(1, 1)$ are to be obtained by solving two determinantal equations $[$ see Eq. (7) $]$:

$$
\det \left| \frac{\delta_{nm}}{2\pi H} - c(3) \delta_{nm} (x_1 q/2, \Delta) \right| = 0,
$$
 (18)

$$
n,m = 0,2,4,...,N-1
$$
 or $n,m = 1,3,5,...,N$,

under the condition that the value $\mathcal{A} = \mathcal{I}\mathcal{W}_i\mathcal{A}_j$ should be larger than $\mathcal{I}\mathcal{W}_i - \mathcal{Z}_j\mathcal{V}_j$. In this case, the maximum number of the poles for the g-th group is (N+1)g instead of (N+1)G.

Upon integrating Eq. (11) over μ from -1 to 1, the total flux is obtained in the form:

$$
V_{j}\eta_{j}(x,t)=\int_{0}^{4} \frac{d\mu}{\mu} S_{j}(\mu,t-\frac{\chi}{\mu\mu}) \exp(-\frac{x\chi}{\mu})
$$

+
$$
\frac{1}{f} \sum_{n=0}^{N} B_{n}(1,1_{j}) G_{n}(z_{j}a/2,2x/a-1, z_{i}w_{i}a_{j}) \exp[z_{i}w_{i}(1_{j}-1)t]
$$

+
$$
\frac{1}{2\pi} \int_{-\infty}^{\infty} d y \exp[-(z_{j}v_{j}-iy)t] \sum_{n=0}^{N} B_{n}(1,i_{j}^{2}+z_{i}v_{i}-z_{j}v_{j})
$$

$$
\times G_{n}(z_{j}a/2,2x/a-1,i_{j}^{2}+z_{i}v_{i}-z_{j}v_{j}).
$$
 (19)

The expression for $G_{n}(\alpha_{1}, 2\xi \gamma_{1}, i'_{1}+\sum_{i}V_{i}-\zeta_{j}V_{j})$ is shown in the Appendix 1, Section 5. Furthermore, the total number of neutrons reflected by or transmitted through the slab is obtained by integrating $|\mu| \psi_j \eta_j (\chi_o, \mu, t)$ ($\chi_o = 0$ to observe neutrons reflected by the slab or $\mathcal{X}_0 = \mathcal{A}$ for neutrons transmitted through it) over μ from -1 to zero or from zero to 1. This gives the form [see Appendix 1, Section 11 for the expression of C_{α}^4 $(c_{\alpha j}, i'j+ \lambda_i v_j - \lambda_j v_j)$]:

$$
\int d\mu \, |\mu| \nu_{\hat{j}} \eta_{\hat{j}}(x_o, \mu, t) = \int_0^4 d\mu \, S_{\hat{j}}(\mu, t - \frac{a}{\mu_{\hat{j}}\mu}) \exp\left(-\frac{2a}{\mu}\right) \Big|_{x_o = a}
$$

+ $\frac{1}{4} \sum_{i} \sum_{n=0}^M (2\frac{x}{\alpha} - 1)^n B_n(g, \lambda_j) C_n^4(\frac{x_{\hat{j}^2}}{2}, x, \nu, \lambda_j) \exp\left(x_i \nu_j - 1\right) t \Big] + \frac{1}{8\pi} \int_{-\infty}^{\infty} d\mu \exp\left[-\left(x_i \nu_{\hat{j}} - i\mu\right) + \left(\frac{y_i}{\mu_{\hat{i}^0}}\right)^2 \frac{(\mu - 1)^n B_n(g, \nu_j + z, \nu_j - z_j \nu_j)}{\mu_{\hat{i}^0}}\right) \times C_n^4(z_j \alpha/2, \nu_j + z, \nu_j - z_j \nu_j).$ \n(20)

2.4 Stationary problems in a homogeneous slab

For a subcritical system with a stationary boundary source $S_2(\mu)$, only one largest pole $\lambda = Z_1 Y_1$ of B_{m} (g, λ) is of importance. Hence, by multiplying $\mathcal{J}-\Sigma_i\mathcal{V}_i$ on both sides of Eq. (13) and taking the limit $\mathcal{J}\rightarrow \Sigma_i\mathcal{V}_i$, we get

$$
\frac{1}{2n+1}B_n(g') = \sum_{j=1}^{G} c(j+j')\sum_{m=0}^{N} J_{nm}(z_j a/2, \Sigma_i V_i) B_m(g)
$$
\n
$$
+ \sum_{j=1}^{G} c(j+j')\sum_{j} a S_j C_n (\Sigma_j a/2), \quad n=0,1,2,\cdots,N,
$$
\n(21)

where $B_n(g) = \lim_{A \to \mathcal{I}(V_1)} (A - \mathcal{I}(V_1) B_n(g, A))$ and $S_g C_n(\alpha_g) = \lim_{A \to \mathcal{I}(V_1)} (A - \mathcal{I}(V_1) S_g C_n(\alpha_g, A))$
which takes the form given by Eq. (15), (16) or (17) with $A = \mathcal{I}(V_1$ when the angular distribution of the source is plane isotropic, point isotropic or monodirectional.

The stationary vector flux, scalar flux and the total number of leakage neutrons can thus be written as follows:

$$
\mathcal{V}_{\mathbf{J}}\mathcal{N}_{\mathbf{J}}(x,\mu)=\frac{1}{\mu}\mathcal{S}_{\mathbf{J}}(\mu)\exp(-\mathcal{I}_{\mathbf{I}}x/\mu)+\sum_{n=0}^{N}B_{n}(\mathbf{J})F_{n}(x_{\mathbf{J}}\alpha/2,\mathcal{K}/a,\mu,\mathcal{I}_{\mathcal{N}}\nu_{\mathbf{J}}),
$$
 (22)

$$
V_1 n_1(x) = \int_0^1 \frac{d\mu}{\mu} S_1(\mu) exp(-\Sigma_1 x/\mu) + \sum_{n=0}^N B_n(g) G_n(x_1 a/2, 2x/a-1, x_1 v_1),
$$
 (23)

$$
\int d\mu |\mu| \psi_{\mathbf{j}} \eta_{\mathbf{j}}(x_{0}, \mu) = \int_{0}^{1} d\mu S_{\mathbf{j}}(\mu) \exp\left(-\sum_{\mathbf{j}} a/\mu\right) \int_{\mathcal{X}_{0}=a} a
$$
\n
$$
+ \frac{\lambda}{4} \sum_{k=0}^{N} (2\frac{\gamma_{k}}{k} - 1)^{k} B_{n}(\mathbf{j}) C_{n}^{+} (z_{\mathbf{j}} a/2, z_{\mathbf{i}} u_{\mathbf{j}}).
$$
\n(24)

In addition, it is also easy to obtain the time moments of the time-dependent flux. For example, the first three time moments of the angular flux (11) is written as⁵⁾

$$
\int_{0}^{\infty} dt \, V_{\eta} n_{1}(x,\mu,t) = \int_{0}^{\infty} dt \, \frac{1}{\mu} S_{\eta}(\mu,t - \frac{\chi}{V_{\eta}\mu}) \exp\left(-\frac{x\pi}{2}\right) + \sum_{n=0}^{N} B_{n}(1, \Sigma_{1}V_{1}) F_{n}(Z_{1}a/2, \chi/a, \mu, \Sigma_{1}V_{1})
$$
\n(25)

$$
\int_{0}^{\infty} dt \, t \, \nu_{\mathbf{j}} n_{\mathbf{j}}(x, \mu, t) = \int_{0}^{\infty} dt \, t \, \frac{1}{\mu} S_{\mathbf{j}}(\mu, t - \frac{x}{\nu_{\mathbf{j}}\mu}) \exp\left(-\frac{2\pi}{3}\right) \\
-\frac{d}{\mu} \left(\sum_{n=0}^{\infty} B_{n}(s, \lambda) F_{n}(z_{\mathbf{j}} a/2, x/a, \mu, \lambda)\right)_{A = x_{\mathbf{i}} \nu_{\mathbf{i}}},
$$
\n(26)

$$
\int_{0}^{\infty} dt \ t^{2} v_{j} n_{j} (x, \mu, t) = \int_{0}^{\infty} dt \ t^{2} \frac{1}{\mu} S_{j} (\mu, t - \frac{x}{v_{j} \mu}) \exp(-\frac{x_{j} x}{\mu})
$$

+ $\frac{d^{2}}{d d^{2}} \left(\sum_{k=0}^{N} B_{n} (q, \lambda) F_{n} (z_{j} q/2, x/a, \mu, \lambda) \right]_{d = z_{i} v_{j}}.$ (27)

From a comparison between Eqs. (13) and (21), it is seen as expected that the zeroth moment of the flux due to an incident delta function source $S_1(\mu, t) = S_1(\mu) S(t)$ is equal to the stationary flux (22

3. Procedures for Evaluating the Pole. Residue and Contribution of the

Continuous Spectrum for a Non-Multiplying Medium without Up-scattering of Neutrons

3.1 Approximate values of the pole

We summarize here the procedure to find an approximate value of the pole, which is required for solving Eq. (7) or (18).

Figure 1 shows the curves giving $1/c$ as a function of $\Sigma \mathcal{L}$ obtained by solving the determinantal equation (18) of the elements with even values of n and m by fixing the value $A = \Sigma V$, within the context of a onegroup model and the j_3 , j_5 or j_7 approximation (N = 3,5 or 7). (Note that the smallest c gives the value required to keep a slab of thickness ZA critical). In order to find the poles of the g-th group with $C(\frac{a}{f})$ and $\Sigma_1 a$, the diagonal of a rectangle with sides $1/C(1-i)$ and $\Sigma_1 a$ is drawn as illustrated in Fig. 1. The points of intersection between the curves and the diagonal should have the abscissa $\Sigma_i d\hat{F}_i$. In the example shown in Fig. 1 $\left\{C(\frac{3}{2})=1\right\}$ and $\sum_{i=1}^{\infty} a_i = 45$, it is not clear if the lowest curve of the $j₇$ approximation intersects with the diagonal. In such cases, the asymptotic expression for the pole with a small absolute value of $\Sigma_j \mathcal{A} P_j$ should be taken into consideration. The expressions in the j_3 , j_5 and j_7 approximations are respectively written as follows ζ *C* α _j = *C*(g+g) Σ ₁a/2 and γ being the Euler Mascheroni constant]:

$$
\sum_{i} a_i^2 \sim exp\left[\frac{3}{2} - \gamma - \frac{1}{c\alpha_3} - \left\{\frac{1}{12} \frac{1}{1 - 12\sqrt{5c\alpha_3}} \frac{1}{1}, \frac{1 + 14\sqrt{35c\alpha_3}}{1 - 2.200260\sqrt{c\alpha_3}}\right\} - \left\{\frac{1}{10} \frac{1 + 2.200260\sqrt{c\alpha_3}}{1 - 2.200260\sqrt{c\alpha_3}}\right\} \frac{1}{1 - \frac{89}{1 - 2.498539\sqrt{c\alpha_3}}}{1 - \frac{2.498547}{1 - 2.4985475}} \frac{1}{1} - \frac{2.255908}{1 - \frac{2.255908}{1 - 2.4985475}}}{1} \right\},
$$
 (28)

which shows that, for example, in the $j₇$ approximation there are 4 poles for $C\alpha_1 > 9.265908$, 3 poles for 9.265908 $>C\alpha_1 > 4.279830_{\rm g}$, 2 poles for 4.279830₅ > $c\alpha_1$ > 2.198517₅ and only 1 pole for 2.198517₅ > $c\alpha_1$ > 0 On the other hand, when $\Sigma_q a \overline{P}_q \gg 1$, the value of P_q is approximately equal to $c(1)$ + 1)

The approximate value of the pole coming out of Eq. (18) with odd values of n and m or Eq. (7) can be found by following the same procedure as mentioned above with the help of Fig. 2. (Note that the negative values of P_3 are applicable only for spherical geometry.) In this case, the asymptotic expressions for the pole with small $|\alpha_j P_j|$ $(\alpha_j = \sum_j a/2$ or $\Sigma_j R$) in the j_3 , j_5 and j_7 approximations are respectively given by

$$
\alpha_{1}P_{1} \sim\n\begin{cases}\n\frac{35}{24} \left(1 - \frac{1.277171}{C\alpha_{1}} \right) \left(1 - \frac{3.865686}{C\alpha_{1}} \right) / \left(1 - \frac{16}{5C\alpha_{1}} \right), \\
\frac{5005}{3856} \frac{[1 - 1.277148/(C\alpha_{1})][1 - 3.281372/(C\alpha_{1})][1 - 7.285614/(C\alpha_{1})]}{[1 - 2.775481/(C\alpha_{1})][1 - 6.570257/(C\alpha_{1})]} \\
\frac{5005}{3856} \frac{[1 - 1.2775481/(C\alpha_{1})][1 - 6.570257/(C\alpha_{1})]}{[1 - \frac{2.263428}{C\alpha_{1}}][1 - \frac{5.423544}{C\alpha_{1}}][1 - \frac{11.748177}{C\alpha_{1}}]} \\
\frac{[1 - \frac{2.7741677}{C\alpha_{1}}][1 - \frac{4.914004}{C\alpha_{1}}][1 - \frac{11.010041}{C\alpha_{1}}] \\
\frac{[1 - \frac{2.744677}{C\alpha_{1}}][1 - \frac{4.914004}{C\alpha_{1}}][1 - \frac{11.010041}{C\alpha_{1}}] \\
\frac{2.062875}{C\alpha_{1}}\n\end{cases}
$$
\n(29)

From these expressions, it is seen that, for example, in the $j₇$ approximation there are 4 positive poles when $C\alpha_j > 11.748197$, 3 when 11.748197 > $C\alpha$ ₂ > 5.423541, 2 when 5.423541 > $C\alpha$ ₂ > 3.263428, 1 when 3.263428 > $ca_1 > 1.277137$ and none when 1.277137 > $ca_1 > 0$.

3.2 Evaluation of the residue

The procedure to evaluate the residue by solving Eq. (6) or (13) for a non-multiplying sphere or slab will be shown here by the use of Eq. (13) with odd values of n in the j_5 approximation $[c]_{nm} \equiv c(3-3) J_{nm}(23a/2,1)$:

$$
\begin{pmatrix} \frac{1}{3} - c \, J_{11} & -c \, J_{12} & -c \, J_{15} \\ -c \, J_{13} & \frac{1}{7} - c \, J_{33} & -c \, J_{35} \\ -c \, J_{15} & -c \, J_{35} & \frac{1}{41} - c \, J_{55} \end{pmatrix} \begin{pmatrix} B_1(1, \lambda) \\ B_3(1, \lambda) \\ B_5(1, \lambda) \end{pmatrix} = \begin{pmatrix} Z_1(1, \lambda) \\ Z_3(1, \lambda) \\ Z_5(1, \lambda) \end{pmatrix}
$$
 (30)

where

$$
Z_{m}(q, \lambda) = \sum_{j=1}^{q} S_{j} C(q^{2} + q) \sum_{j} a C_{m}(Z_{j}, a/2, \lambda)
$$

+
$$
\sum_{j=1}^{q} C(q^{2} + q) \sum_{n=1,3,5} J_{mn}(Z_{j}, a/2, \lambda) B_{n}(q, \lambda).
$$
 (31)

Equation (30) leads, for example, to

$$
B_{3}(q, \lambda_{j}) = \lim_{\Delta \to \Sigma_{1} V_{1} \Delta_{j}} \frac{\Delta - \Sigma_{1} V_{1} \Delta_{j}}{\Delta} \begin{vmatrix} 3cJ_{11} - 4 & -3Z_{1}(9, \lambda) & 3cJ_{15} \\ 7cJ_{13} & -7Z_{3}(9, \lambda) & 7cJ_{35} \\ 14cJ_{15} & -44Z_{5}(9, \lambda) & 14cJ_{55} - 4 \end{vmatrix}
$$
 (32)

where

 $\ddot{}$

 \bar{z}

$$
\Delta \equiv \begin{vmatrix} 3c J_{41} - 4 & 3c J_{43} & 3c J_{45} \\ 7c J_{43} & 7c J_{33} - 4 & 7c J_{35} \\ 11c J_{45} & 7c J_{35} & 11c J_{55} - 4 \end{vmatrix} .
$$
 (33)

 \mathbb{R}^2

 $\ddot{}$

Hence, for the pole $\mathcal{A} = \Sigma_1 \mathcal{V}_1 \mathcal{A}_{j}$ of the g-th group obtained from the equation $\Delta = 0$,

$$
B_{3}(\mathbf{1}, \mathbf{A}_{\mathbf{j}\mathbf{1}}) = \begin{vmatrix} 3cJ_{4} - 3Z_{1}(3\lambda) & 3cJ_{45} \\ 7cJ_{43} & -7Z_{3}(3\lambda) & 7cJ_{35} \\ 14cJ_{45} & -41Z_{5}(3\lambda) & 4cJ_{55} - 1 \end{vmatrix} \begin{vmatrix} 1 & 3cJ_{4} - 4 & 3cJ_{45} \\ \frac{d}{d\lambda} & 7cJ_{43} & 7cJ_{33} - 4 & 7cJ_{35} \\ 16J_{45} & 4cJ_{35} & 16cJ_{55} - 1 \end{vmatrix} \begin{vmatrix} 3cJ_{4} - 4 & 3cJ_{45} \\ 7cJ_{45} & 7cJ_{45} & 7cJ_{55} \\ 16cJ_{45} & 4cJ_{35} & 16cJ_{55} - 1 \end{vmatrix} \begin{vmatrix} 3cJ_{45} & 3cJ_{45} \\ 7cJ_{45} & 7cJ_{45} & 7cJ_{45} \\ 7cJ_{45} & 7cJ_{45} & 7cJ_{45} \end{vmatrix}
$$
 (34)

the explicit expression for $\frac{d}{d\delta} \int_{n,m} (\alpha_i, \delta)$ being given in Appendix 1, Section 3.

On the other hand, for the pole $\lambda = \sum_i \mathcal{V}_i \lambda_{ij}$ of the higher g'-th group,

$$
B_{3}(q, \lambda_{jq'}) = \frac{1}{\Delta_{d=2j}v_{l}\lambda_{jq'}} \begin{vmatrix} 3cJ_{H} - 3\frac{7J}{k-2}c(k-3)\sum_{n=1,3,5}J_{1n}(z_{n}a_{1}a_{2},\lambda)B_{n}(k,\lambda_{jq'}) & 3cJ_{45} \\ 7cJ_{43} - 7\sum_{n=2}c(k-3)\sum_{n=1}^{3}J_{3n}(z_{n}a_{1}a_{2},\lambda)B_{n}(k,\lambda_{jq'}) & 7cJ_{35} \\ 14cJ_{45} - 44\sum_{n=1}^{3}c(k-3)\sum_{n=1}^{3}J_{5n}(z_{n}a_{1}a_{2},\lambda)B_{n}(k,\lambda_{jq'}) & 14cJ_{55} - 4 \end{vmatrix}
$$
(35)

which shows that all poles of the higher g^{\dagger} -the group $(g^{\dagger} = 1, 2, ..., g-1)$ are also the poles for the g-th group if all values of $C(9^2+9^2+1)$ are not equal to zero (this condition means that there is the slowing down of neutrons from a certain group to the next group). For a homogeneous slab, however, the condition that $\lambda_{jj'} > 1 - \lambda_j \nu_j / (\lambda_j \nu_j)$ excludes some poles because the \mathcal{A}_{j} ?' has been obtained under the condition that \mathcal{A}_{j} ? $\frac{1}{4} - \sum_{j} \frac{1}{2} \int \frac{1}{4} \int$ for $h = 1, 2, ..., g'$ -1, as seen from the presence of the second term on the right-hand side of Eq. (31)]. In other words, some poles of the g'-th $\Sigma_{\mathbf{1}'}\mathcal{V}_{\mathbf{1}'} > \Sigma_{\mathbf{1}}\mathcal{V}_{\mathbf{1}}$ may not be the poles of interest for group for which the g-th group.

3.3 Contribution of the continuous spectrum

For time-dependent problems in a homogeneous slab, we have to evaluate the last term on the right-hand side of Eq. (11), (19) or (20). The contribution of the continuous spectrum represented by, for example, the last term of Eq. (20) can be rewritten in the j_{5} approximation as follows:

$$
\frac{V_1}{2\pi a} \exp(-z_1 v_1 t) \int_0^{\infty} \frac{d^4}{4^2} \sum_{n=0}^{\infty} (2\frac{7}{a} - 1)^n \left[(B_{n_1} C_{n_1} - B_{n_2} C_{n_3} + B_{n_4} C_{n_5} + D_{n_6} C_{n_7} + D_{n_7} C_{n_7} + D_{n_8} C_{n_7} + D_{n_9} C_{n_9} + D_{n_1} C_{n_9} + D_{n_1} C_{n_9} + D_{n_1} C_{n_9} + D_{n_1} C_{n_1} + D_{n_1} C_{n_2} + D_{n_1} C_{n_3} + D_{n_1} C_{n_1} + D_{n_1} C_{n_2} + D_{n_1} C_{n_3} + D_{n_1} C_{n_1} + D_{n_2} C_{n_3} + D_{n_3} C_{n_4} + D_{n_1} C_{n_2} + D_{n_1} C_{n_3} + D_{n_1} C_{n_4} + D_{n_1} C_{n_1} + D_{n_2} C_{n_2} + D_{n_3} C_{n_3} + D_{n_4} C_{n_4} + D_{n_1} C_{n_4} + D_{n_2} C_{n_5} + D_{n_3} C_{n_6} + D_{n_4} C_{n_7} + D_{n_5} C_{n_8} + D_{n_6} C_{n_9} + D_{n_7} C_{n_1} + D_{n_8} C_{n_1} + D_{n_1} C_{n_2} + D_{n_2} C_{n_3} + D_{n_3} C_{n_4} + D_{n_4} C_{n_5} + D_{n_5} C_{n_6} + D_{n_6} C_{n_7} + D_{n_7} C_{n_8} + D_{n_8} C_{n_9} + D_{n_9} C_{n_1} + D_{n_1} C_{n_2} + D_{n_2} C_{n_3} + D_{n_3} C_{n_4} + D_{n_4} C_{n_5} + D_{n_4} C_{n_6} + D_{n_5} C_{n_7} + D_{n_6} C_{n_7} + D_{n_7} C_{n_8} + D_{n_8} C_{n_9} + D_{n_9} C_{n_1
$$

where

$$
B_n(3, i'j + \bar{z}/\nu_1 - \bar{z}_1 \nu_3) = \frac{1}{4} (B_{n'i} j + i B_{n2j}),
$$

$$
C_n^{\ell} (\bar{z}_j a/2, i'j + \bar{z}_1 \nu_1 - \bar{z}_j \nu_3) = \frac{2 \nu_1}{a j} (C_{n'i} j + i C_{n2j}),
$$

and use has been made of the fact that $B_{n,m}$ () and $C_{n,m}$ () are even or odd functions of y depending on whether $n+m = even$ or odd. Since $B_n(g, iy+I\psi - \Sigma_j v_j)$ is written as $[C\mathcal{F}_{nm} \equiv c(g+g)\mathcal{F}_{nm}(x_j\psi/2, iy+I\psi - \Sigma_j v_j);$ see Eqs. (30), (31) and (33)]

$$
B_{3}(q,i'_{1}+x\omega_{1}z_{1}\omega_{1})=\frac{1}{\Delta_{d=i'_{1}+x\omega_{1}z_{1}\omega_{1}}}\begin{vmatrix}3C_{J_{11}}-1&-3Z_{1}(q,i'_{1}+x\omega_{1}-z_{1}\omega_{1})&3C_{J_{15}}\\7C_{J_{13}}&-7Z_{3}(q,i'_{1}+x\omega_{1}-z_{1}\omega_{1})&7C_{J_{35}}\\7C_{J_{15}}&-4(Z_{5}(q,i'_{1}+x\omega_{1}-z_{1}\omega_{1})&4C_{J_{35}}-4\end{vmatrix}
$$
(37)

can be evaluated successively starting with $g = 1$ by $B_{\eta_1\eta}$ and $B_{\eta_2\eta}$ using the expressions shown in the Appendix 1 [Section 2 for $J_{nm}(\alpha_1)$ $i\frac{y}{1} + \frac{y}{y} - \frac{y}{y}$ and Section 11 or 13 for C_n^{\dagger} or C_n^{\dagger} (α_j , $i\frac{y}{1} + \frac{y}{y} - \frac{y}{y}$) to obtain $Z_n(q, iy+I\psi_i-I_j\psi_j)$ for the case where the angular distribution of the boundary source is point isotropic or monodirectional J . When $\frac{1}{2}$ \neq ∞ , however, the value of the integrand of Eq. (36) changes very rapidly as a function of y. The evaluation of the integral over y from $\frac{1}{4}$ \gg 1 to ∞ is therefore performed separately by the use of asymptotic expressions for the functions $J_{n,m}$, C_n^f , C_n^c , G_n and/or F_n for large y [or for large $a/\sqrt{2v_1}$], which can easily be obtained from the expressions shown in the Appendix 1, Sections 2, 11, 13, 5 and/or 7. In the case where the boundary source is monodirectional, this gives in the $j₇$ approximation the following forms $(\xi \equiv \chi/a)$:

(a) For the angular flux $v_j n_j(x, \mu, t)$ with $\mu > 0$ written by Eq. (11);

$$
\int_{y_{0}}^{\infty} \frac{d^{4}_{4}}{4^{4}} \sum_{n=0}^{7} [(B_{n13}F_{n13}-B_{n23}F_{n23}) \cot(\frac{1}{3}t) - (B_{n23}F_{n13}+B_{n13}F_{n23}) \sin(\frac{1}{3}t)]
$$
\n
$$
\sim \frac{1}{4} (3+7+11+15+1+5+9+13) \sum_{j=1}^{3} c(3^{2}+3) \sum_{j} v_{j}^{2} \cdot \sum_{j}^{6} \frac{d^{4}_{2}}{4^{2}} \cos(\frac{1}{y_{j}}) \sum_{j=1}^{6} c(3^{2}-1) \sum_{j}^{7} (3^{2}+7) \sum_{j=1}^{5} (-1)^{2} \sum_{j} (3^{2}+7) \sum_{j} (3^{2}+
$$

 (38)

where

$$
\chi_2 \equiv 4-2\xi, \quad \chi_3 \equiv (4-2\xi)\left\{4-40\xi(4-\xi)\right\}, \quad \chi_4 \equiv (4-2\xi)\left\{4-2\xi\xi(4-\xi)(4-\frac{9}{2}\xi(4-\xi))\right\},
$$
\n
$$
\chi_5 \equiv (4-2\xi)\left\{4-54\xi(4-\xi)(4-4\xi(4-\xi)(4-\frac{26}{4}\xi(4-\xi))\right\}, \quad \chi_6 \equiv 4-6\xi(4-\xi),
$$
\n
$$
\chi_{\eta} \equiv 4-20\xi(4-\xi)\left\{4-\frac{9}{2}\xi(4-\xi)\right\}, \quad \chi_{g} \equiv 4-42\xi(4-\xi)\left\{4-9\xi(4-\xi)(4-\frac{22}{4}\xi(4-\xi))\right\}.
$$

Since $\overline{F}_n(\alpha_3, \overline{S}, \mu, \lambda) = (-1)^n F_n(\alpha_3, +\overline{S}, -\mu, \lambda)$, the value for the angle $-\mu$ and the space $a-\chi$ (or κ) can be obtained by changing the sign of the first 4 terms in the parentheses of each term on the right-hand side of Eq. (38).

(b) For the total flux $v_j n_j(x,t)$ with $\chi \leq a/2$ written by Eq. (19);

$$
\int_{4}^{10} \frac{d4}{4} \frac{4}{\pi} \sum_{n=0}^{1} \left(\left(B_{n13} G_{n13} - B_{n23} G_{n23} \right) \cos \left(4t \right) - \left(B_{n23} G_{n13} + B_{n13} G_{n23} \right) \sin \left(4t \right) \right]
$$

$$
\begin{pmatrix}\n-\frac{1}{4}(3+7+11+15+1+5+9+13)\sum_{i=1}^{3}c(3+2)\sum_{i}v_{i}\sum_{j}\left(\frac{d^{2}y}{y^{2}}\cos(4t) - \frac{1}{4}(3+7+11+15-1-5-9-13)\sum_{i=1}^{3}c(3+2)v_{i}\sum_{j}v_{j}\left(\frac{d^{2}y}{y^{2}}\cos\left(\frac{a}{y_{j}}\pi - t\right) y\right)\right) \\
-\frac{1}{2}(3X_{2}+7X_{3}+11X_{4}+15X_{5}+1+5X_{6}+9X_{7}+13X_{8})\sum_{i=1}^{3}c(3+2y_{i})\sum_{i}v_{i}\sum_{j}\left(\frac{d^{2}y}{y^{2}}\cos(4t) - \frac{1}{2}(3X_{2}+7X_{3}+11X_{4}+15X_{5}-1-5X_{6}-9X_{7}-13X_{8})\right) \\
-\frac{1}{2}(3X_{2}+7X_{3}+11X_{4}+15X_{5}-1-5X_{6}-9X_{7}-13X_{8})\n\end{pmatrix}
$$
\n
$$
\times \sum_{j=1}^{3}c(3+2y_{j})\sum_{i}v_{i}\sum_{j}\left(\frac{d^{2}y}{y_{j}}\cos\left(\frac{a}{y_{i}}\pi - t\right) y\right), \text{ for } 0.5 \ge 5 > 0.
$$
\n(39)

The value for $\zeta > 0.5$ can be obtained by changing the sign of the first 4 terms in the parentheses of each term on the right-hand side because $G_{n}(\alpha_{1}, \xi, \lambda) = (1)^{n} G_{n}(\alpha_{1}, 1-\xi, \lambda).$

(c) For the total number of leakage neutrons $\int d\mu |\mu|\nu_{\gamma} \eta_{\gamma}(x_{o},\mu,t)$ written by Eq. (20);

$$
\int_{y_{0}}^{\infty} \frac{d^{4}_{1}}{4^{4}} \frac{1}{\pi^{3}} (2 \frac{\pi}{6} - 4)^{n} \left[(B_{m1} \frac{1}{6} - B_{m21} C_{n2} \frac{1}{3}) \cot(\frac{1}{3} t) - (B_{m21} C_{m1} \frac{1}{9} + B_{m1} C_{n2} \frac{1}{3}) \sin(\frac{1}{3} t) \right]
$$
\n
$$
\sim \frac{1}{2} \left[(2 \frac{\pi}{6} - 4) (3 + 7 + 1/4 + 15) - (1 + 5 + 7 + 13) \right] \frac{1}{3} \left[c_{1} \frac{1}{3} \right] \int_{y_{0}}^{\infty} \frac{d^{4}_{1}}{y_{0}^{3}} \cos(\frac{1}{3} t) + \frac{1}{2} \left[(2 \frac{\pi}{6} - 4) (3 + 7 + 1/4 + 15) - (1 + 5 + 7 + 13) \right] \frac{1}{3} \left[c_{1} \frac{1}{3} \right] \int_{y_{0}}^{\infty} \frac{d^{4}_{2}}{y_{0}^{2}} \cos\left[\left(\frac{1}{4} - 1 \right) y \right].
$$

(40)

In the j_N approximation, the first $N(N+1)/2$ terms out of the first 4 and out of the last 4 terms remain in the parentheses of each term . on the right-hand side of Eq. (38), (39) or (40). In addition, when the boundary source is point isotropic, the total number of terms on the right-hand side is reduced to be half, for example, only the first 2 terms remain in Eq. (38).

4. JN-METDl Computer Code

4.1 Input data (see the Appendix 3)

After an ID card with a 20A4 format, 26 integers are read with a 2613 format. These integers are defined as follows:

Next, 12 floating-point numbers are read with a 6E12.5 format. These are defined as follows:

 ~ 10

 $\sim 10^{-1}$

 \sim

 $\hat{\mathcal{A}}$

In the subroutine JNMETD, the following data ordered respectively by energygroup beginning with g=l are read with 8F10.6:

The total number of these cards is therefore $3 [(IGRP+7)/8]$. Next, the cross section XSEC is read with (8F9.6, F8.5) for all types of reactions arranged as mentioned above in the first group, then for those in the second group and so on, the total number of cards being $[(\text{IHLx1GRP+8})/9]$. The remaining input data depending on the input integers are:

(a) When NSTATY=1 and NSPH=1, one card is read with 8F10.6 in the subroutine JNMETD. These are

If R2, S2 or CK2 is equal to zero, the input value Rl, SI or CK1 is regarded as the critical radius, time constant or $k_{\alpha f\theta}$ without any iterations.

(b) When NSTATY=1, NSPH=0 and NUPSAT=1, one card is read with 7F10.7 in the subroutine RESCAL to evaluate the fundamental decay constant of neutrons in the system $\Sigma_i V_i (1-\lambda_i)$.

- (c) When NSTATY=2, NSPH=0, NSTAT1=0 and LLL=0, a punched card dump for the stationary flux with a (5E15.8) format is read in the JNMETD in the same order as in the punched output or in the output print [for each of (NNN+1) energy groups beginning with the JNKK-th group, NOM values for the angular flux for each space point (when $JJJJZ3$) followed by NOS values for the total flux (when $JJJZ 2$) and then 2 cards for the total number of leakage neutrons at $\chi = a$ and $\chi = 0$ (when JJJJ $\neq 3$)]. The total number of cards is 2(NNN+1) when JJJJ=1, $(2+\text{NOS}+4)/5\text{J})x(NNN+1)$ when $JJJJ=2$, $($ [(NOS+4)/5]+[(NOM+4)/5]NOS)(NNN+1) when JJJJ=3 or $(2+\text{[(NOS+4)/5]}+\text{[(NOM+4)/5]}NOS)(NNN+1)$ when JJJJ=4.
- (d) When NSTATY=2, NKK>0 and LLL=0 £in case of NSPH=0 and NSTAT1=0, the present data follow the cards described in the Subsection (c)], a punched card dump with a (5E15.8) format for the pole and residue is read in the JNMETD beginning with K=l and M=l when NSPH=0 or with K=2 and M=1 when NSPH=1. $K=1$ or 2 represents the fact that the values come from Eq. (13) with even or odd values of n and M=m stands for the m-th eigenvalue (or the pole) for each K and the associated residues.] Following the cards for (K,M) , those for $(K,M+1)$ are read if $M+1 \leq JHL$ \equiv [(IIO+1)/2] when K<JOD or M+1≤JJJ when K=JOD. Then, the cards for K+1 (K+1 \leq JOD \leq 2) are read beginning with M=l till M=JHL or JJJ. For each set of values of K and M, the cards should be ordered as follows $NN \equiv IGRP$ except for $(K,M)=(JOD,JJJ)$ where $NN \equiv NKK$;

 $- 25 -$

(e) When NSTATY=2 and NKK<IGRP, following the data mentioned in the Subsections (c) and (d) if any, the first and second guesses for the poles $SP(1,g)$, $g=1,2,\ldots$, IGRP, and $SP(2,g)$, $g=1,2,\ldots$, IGRP, for K=JOD and M=JJJ are read first with 7F10.7 in the RESCAL ([(2*IGRP+6)/73 cards). If no pole exists for the g-th group, $SP(1,g)=SP(2,g)=0$. If no iteration process is required for obtaining the value, $SP(2,g)=0$ $SP(1,g)$ is regarded as the pole J . Furthermore, if the value of $\Sigma_q \alpha P_q$ is very small for the case where K=1 [see Eq. (28)], SP(1,g)=0, SP(2,g) \neq 0 (any value) and the first and second guess for the value of P_{gr} is read next with 5
÷-2E15.8. The total number of cards for P is therefore the same as the number of groups for which $SP(1,g)=0$ and $SP(2,g)\neq 0$ for each value of M for K=1. These input data are repeated in the same order as mentioned in the last subsection (d) till K=2 and M=JHL. If NKK=IGRP and JOD=1 or JJJ<JHL, the present input begins with the data for (K,M) next to $(K=JOD, M=JJJ)$.

4.2 Computer programme

4.2.1 General

The JN-METDl package consists of 24 programmes; MAIN, JNMETD, RESCAL, FLUXCA, INTCAL, PULSE, ITRTON, DET, SOLEQ, EP, F, FSML, DEROF, SDERF, CCALC, DEROC, GCAL, FMCAL, VARIAC, ADJPUL, FNCUT1, IFNCAL, GIMAG and FMIMG. In addition, the code makes use of the library subprogrammes, MAXO, EXP, DEXP, DLOG, DATAN, DSIN, DCOS and DSICI (see below).

Almost all input integers and floating-point numbers are transmitted through a COMMON where, in addition, all subscript variables and their dimension information are stored for the use of the adjustable dimensioning. The present size of the floating COMMON for all subscript variables is set to be 72,000 bytes so as to the programme requires the core storage less than 300 K bytes in the Fortran-IV, Version G on the IBM-360/65.

For altering the dimension of the floating COMMON to fit core storage, the following 27 statements should be adjusted (all 24 programmes are numbered respectively): In the MAIN programme, the 45th card (dimension of BCOM), 47th card (COMMON), 55th card (clear-COMMON), 318th card (available \le required storage?), 321st card (available \le required storage only for the stationary problem?) and 340th card (available \leq required storage for the time-dependent problem?). In the JNMETD, the 24th card (COMMON) and 32nd card (dimension of ECOM). In the INTCAL, the 17th card (COMMON) and 24th card (dimension of ECOM). Seventeen cards for COMMON.: the 21st of RESCAL, 28th of FLUXCA, 13th of PULSE, 14th of EP, 5th of ITRTON, 18th of F, 14th of FSML, 16th of DEROF, 10th of SDERF, 18th of CCALC, 13th of DEROC, 17th of GCAL, 16th of FMCAL, 35th of FNCUT1, 14th of IFNCAL, 12th of GIMAG and 12th of FMIMG.

4.2.2 MAIN

In the main programme, sizes of the required arrays are computed based on input paramters and then first-word addresses are calculated for these arrays. The locations of these pointers and the associated arrays with their dummy dimensions are shown in Table I where the arrays which share

the same storage locations are written in one block (for example, Real^{*4} subscript variables FNPOL, TFLUX and FFLUX share the same storage locations as for Real $*8$ arrays DELTA, E, ED and SS in the case where NSTATY=1.) The actual values for these integer variables specifying the sizes of arrays are summarized in Table II. The first-word addresses and the dimensions are transferred through a call statement and a part of a vector in COMMON is treated as a multi-dimensioned array in subprogrammes. The flow chart of the main programme is shown in the Appendix 2, Section 1.

4.2.3 JNMETD, DET, ITRTON, F, FSML and EP

The subroutine JNMETD (see the Appendix 2, Section 2) is devoted mainly to solve stationary problems in a bare sphere (NSTATY=1 and NSPH=1). As can be seen in the Section 2.1 of Appendix 2, for the time-constant calculation to obtain the value of S, for example, Eq. (9) is solved by using the two guesses S1 and S2, the function subprogramme F for evaluating J_{nm} , the subroutine DET to evaluate the determinant and the subroutine ITRTON to iterate the process for making the value of the determinant zero until the difference between two successive values of S becomes smaller than the product of the last value of S by EPSS. After having been obtained the value of S, the ratios between the residues are calculated by evaluating the cofactors of the determinant, then the subroutine FLUXCA (see below) is called for the calculation of the total flux Eq. (8) and in the end the neutron balance is calculated by normalizing the total number of fission neutrons produced in the reactor to the value of k_{off} .

 ϵ f the series expansion shown in the Appendix 1, Section 1 is used if the absolute value of $\alpha = \alpha_{1}P_{1}$ is less than 2 (K=2 in the programme). The argument N stands for n and m $\int N = 1, 2, 3, ..., 20$ corresponding to $(n,m) = (0,0), (1,1), (0,2), (2,2), (1,3), (3,3), \ldots, (7,7)$, As regards the control integers transmitted through the COMMON, LG=2 is for reducing execution time required for calculating $P_q J_{nm}(\alpha_1, \lambda)$ different indices n and m but with the same value of α (LG=1 otherwise). In addition, JOD=1 or 2 is for evaluating the function with even

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or odd values of the indices. When JOD=1 and $|\alpha|$ > 2, as is seen from the expression for P_1J_{oo} , it uses the function subprogramme $E P(m,\chi,\cancel{f},\dots)$ to evaluate the exponential integral $E_{\mu}(\chi)$. On the other hand, when $|\alpha| < 2$, it uses the function subprogramme FSML(α ,M,...) which evaluates $P_3 J_{nm}(\alpha_1, \Delta)/\alpha$ with even values of n and m by the use of the series expansion $\{ M=1,2,3,...,10$ corresponding to $(n,m)=(0,0),(0,2),$ $(2,2), \ldots, (6,6)$]. The control integer LF=2 is for computing $P_3 J_{mm}/\alpha$ with the different indices but with the same *0<* (LF=1 otherwise). The EP(π, χ, χ, \ldots) evaluates also the integral $\int_{\gamma}^{\phi} \chi \, dz \, dz^2 / 2$ numerically based on the generalized Simpson's rule when $\beta > 0$ [note that the integral is equal to $F_t[-\frac{1}{2}(\frac{1}{2}, \frac{1}{2})] - F_t(-\frac{1}{2}\chi)$ if $\frac{1}{2} < 0$, For $\frac{1}{2} = 0$, it uses the asymptotic expansion for large $\boldsymbol{\chi}$ or small $\boldsymbol{\chi}^{11}$ depending on whether $\chi > 17$ or $0 < \chi < 0.05$ for evaluating $E_n(\chi)$ with $0 < n < 10$. For $0.05 < \mathcal{X} < 0.5$, $E_4(\mathcal{X})$ is calculated by using the asymptotic expansion for small $\mathcal X$ and then $E_{\eta}(\mathcal X)$ with $n > 1$ is evaluated by the use of the recurrence relation. Furthermore, for $0.5 < \chi <$ 17, $E_4(\chi)$ is obtained through the numerical integration and then the recurrence relation is used for calculating the value of $E_{\mathcal{H}}(\mathbf{X})$. The control integer LFF is fixed to be 2 for computing $E_m(\Upsilon)$ with different n but with the same Υ (LFF=1 otherwise).

For other problems than the stationary neutron transport in a bare sphere, the JNMETD calls the subroutines RESCAL, FLUXCA, INTCAL and then PULSE. In the case where NSTATY=2, NSPH=0 and NSTAT1=1, the stationary problem is solved first by calling RESCAL and FLUXCA, and then the time-dependent problem is treated by putting NSTAT1=0 and by calling again these subroutines. When NUPSAT=1 and LLL=0, following the calculation of the neutron flux by going through RESCAL, FLUXCA and INTCAL, the fundamental decay constant $\sum_i \gamma_i (1-\lambda_i)$ is evaluated by fixing LLL=1 and by calling once more RESCAL.

4.2.4 RESCAL, SOLEQ, DEROF, SDERF, CCALC and DEROC

For time-dependent problems, the subroutine RESCAL (see the Appendix 2, Section 3) computes the pole on the basis of two guesses for its value

[see Sections 3.1 and $4.1(e)$]. The procedure for solving Eq. (7) or (18) to evaluate the pole is the same as that mentioned above for obtaining the time constant in the JNMETD. When, as an input, the guesses for the value of P_3 have been read instead of $\frac{1}{4}$ (KKK=2 in this case and KKK=1 otherwise), the programme deals with, for example, Eq. (33) with the elements divided by $C(f\rightarrow f)\alpha_g$ (instead of the unmodified equation) by using the function subprogramme FSML directly (not via the function F).

After having been evaluated the pole $($ $\frac{1}{4}$ $\frac{1}{4}$ = 0 for stationary problems), if required (LLL=0), the residues at this pole and at the poles of higher energy groups are calculated as mentioned in Section 3.2 with the help of the subprogrammes DEROF, DET, CCALC and F (see the Appendix 2, Section 3.1). In the case where NSTAT1=1, also the first and second derivatives of the residue with respect to the Laplace transform variable *Λ* at the point *Α=ΣιΊ/ι* are evaluated by calling the subroutines DEROC, DEROF and SDERF to obtain the first and second time moments of the neutron flux (26) and (27). On the other hand, for problems with NUPSAT=1 (one cannot deal with only one energy group, successively, beginning with the highest group), it calls the subroutine SOLEQ to evaluate the residues (or their derivatives) by solving a system of simultaneous linear equations.

When NSTATY=2 and LLL=0, the RESCAL produces punched cards, with a 5E15.8 format, for the residue and the pole ordered by Κ and M in the same way as for the input mentioned in the Subsection (d) of Section 4.1. For each set of the values of K and M, the cards for the residue $B_M(g, A_y)$, $g' = 1, 2, ..., g$, are punched in order of n $(n=1,2,\ldots, JHL)$, separately) for $g=g''+1$, then for $g=g''+2$ and so on till $g=$ IGRP. When, as an input, the guesses for P_2 have been read for $g=g''+1, g''+2, \ldots, g'''$, the cards for P_g for $g=1,2,\ldots,g''$ ($P_3 \equiv 0$ for $g=1,2,...,g''$) are produced following those for the residue of the g'" -th group. All these cards are followed by those for the poles $f - \mathcal{A}_g$ for $g = 1, 2, ..., I$ GRP ($f - \mathcal{A}_g = 0$ for $g = 1, 2, ..., g'$).

The subroutine DEROF (α , CAXV, KKK,) evaluates CAXV* (21th) $I_1V_1P_1^2\frac{1}{4}J_1J_2m(\alpha_1,\Delta)$ when KKK=1, by making use of the explicit expression if $|a|>2$ or the series expansion otherwise (see the Appendix 1, Section 3). The control integer JOD transmitted through the COMMON is fixed to be 1 for even values of η and m [the functions with $(n,m)=(0,0)$, $(0,2)$, $(2,2)$,,.., $(110-1,110-1)$ being evaluated]

or 2 for odd values of n and m [the values for $(n,m)=(1,1),(1,3),(3,3),...$ (IIO, IIO) being obtained J . On the other hand, when KKK=2, it calculates CAXV * $(2n+4)$ $\mathcal{I}_1 \mathcal{V}_2 P_3^2 \frac{d}{dx} J_{nm}$ $(\alpha_3, \Delta)/\alpha$ with even values of n and m by the use of the series expansion.

The subroutine SDERF(α ,....) calculates $(\lambda_1^2 \lambda_1^2)^2 P_1^3 \frac{d^2}{d\lambda^2} J_{nm}(\alpha_1, \lambda)$ by using the explicit expression or the series expansion depending on whether the value $|X|$ is larger or smaller than 3, for n=0 and 1 ($m \le 7$) and for $m=7$ ($n \le 7$). For other values of n and m, it adopts a linear relation among the functions:

 $\frac{d^2}{dx^2} J_{m+1,m} = \frac{2m+1}{2m+1} \left(\frac{d^2}{dx^2} J_{n,m+1} + \frac{d^2}{dx^2} J_{n,m+1} \right) - \frac{d^2}{dx^2} J_{n-1,m}$

with the help of the symmetric relation $\frac{d^2}{dt^2} J_{nm} = \frac{d^2}{dt^2} J_{mn}$.

The subroutine CCALC(2 α ,....) evaluates $2\alpha C_{2n}^{q}$ (α_3 , b) (when $JOD=1$) or $2\alpha C_{2n+1}^{a}$ (α_{3} , A)/i (when JOD=2), n=0,1,..., (IIO-1)/2, in the case where IIII=0, DMU1=0 and NSPH=0. In addition, it computes $2\alpha C_2 n^4(\alpha_1, \lambda)$ or $2\alpha C_{2n+1}^{\{8\}}(\alpha_3, \beta)/i$ in the case where IIII=1, DMU1=0 and NSPH=0. The explicit expressions are adopted for these calculations when $|2\alpha| > 2.5$, with the help of the function EP (the series expansions otherwise; see the Appendix 1, Sections 9 and 10). Furthermore, in the case where DMU1>0 and NSPH=0, it calculates $2\alpha C_{2n}^c(\alpha_1,\lambda)$ or $2\alpha C_{2n+1}^c(\alpha_1,\lambda)/i$, the series expansion shown in the Appendix 1, Section 12 being used when $|2\alpha/\mu_1| < 3$. It also computes (Appendix 1, Section 8) in the case where NSPH=1 by $2\alpha A_{2n+1}(2\alpha_2, \lambda)$ using the explicit expression when $|2\alpha|>0.3$ or the series expansion otherwise.

The first and second derivatives of the function $C_n^{\phi}(\alpha_1, \lambda)$ or $C_n^{\phi}(\alpha_1, \lambda)$ with respect to s are evaluated in the subroutine DEROC(α ,...). In the case where DMU1=0, it computes $2\alpha (\Sigma_1 V_1 P_2 \frac{d}{dt} \int_0^m C_{2n}^4 (\alpha_1, \Delta)$ or $2\alpha (\Sigma_1 V_1 P_2 \frac{d}{dt} \int_0^m C_{2n+1}^4 (\alpha_1, \Delta) / \Delta)$ $(m=1$ and 2) depending on whether JOD=1 or 2, by the use of the series expansion (when $|2\alpha| < 4$) or the explicit expression with the help of the EP (when $|2\alpha| > 4$). On the other hand, in the case where DMU1>0, it calculates $2\alpha(\Sigma_1V_1P_2\frac{d}{dx})^mC_{2n}(\alpha_1, \Delta)$ or $2\alpha(\Sigma_1V_2P_2\frac{d}{dx})^mC_{2n+1}(\alpha_1, \Delta)/i$ by adopting the series expansion when $|2\alpha/\mu_1|<4$ or the explicit expression otherwise.

4.2.5 FLUXCA, GCAL, FMCAL and VARIAC

The subroutine FLUXCA (see the Appendix 2, Section 4) calculates the contribution of the poles to the total number of neutrons leaking out of a slab \lceil when JJJ (or JJJJ in the main programme) = 1,2 or 4 \rfloor , to the total flux in a sphere or slab (when *333=2,* 3 or 4) or to the angular flux in a slab (when $JJJ = 3$ or 4).

The contribution to the total number of leakage neutrons is evaluated for two boundaries of a slab according to the second term on the right-hand side of Eq. (20) or (24) by calling therefore the subroutine CCALC for evaluating C_4^{\bullet} . In addition, in the case where NSTAT1=1, the first and second time moments [multiplied respectively by $\Sigma_i \mathcal{V}_j$ and $(\mathcal{I}_i \mathcal{V}_i)^2$] of the leakage neutrons due to a $S(t)$ source are calculated on the basis of the expressions similar to Eqs. (26) and (27) (the contribution of uncollided neutrons being excluded) by calling the DEROC for evaluating the derivatives of C_n^* .

For computing the contribution to the total flux (and the first and second time moments), that is the second term on the right-hand side of Eq. (1) , (19), (23) or the right-hand side of Eq. (8), it calls the subroutine GCAL $(\alpha, \xi, JIK,...,m)$ to calculate the values of $4\alpha(\xi_1\psi_1\zeta_4)\frac{d}{dx}$ $(\alpha_1, \alpha_2,\xi_1,\xi)$ when JOD=1 or $\frac{4\alpha i}{\pi \sqrt[n]{4}} (\frac{1}{4} \frac{1}{4} \frac{1}{4})^{m+1} f_{2m+1}(\alpha_1, 2\frac{1}{2} \alpha_1, \alpha_2)$

when JOD=2 $[n=0,1,\ldots, (110-1)/2]$, the integer JIK=2 being for evaluating the functions with a different value of $m(-1, 0 \text{ or } 1)$ but with the same $\alpha = \alpha_1 P_1$ and 5 (JIK=1 otherwise). [Note that $(\frac{d}{d\lambda})^m G_{2n}(\alpha_1, 25-4, \lambda)$ = *(JLT'Y* Q Μ (Oft 4-2X A") ~l* As is seen in the Appendix 1, Section 4, in t_{min} (*II*) $\frac{1}{2}$ (*XI*) $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ crfc is used ($\frac{1}{2}$ (*X*| \geq 4 the case where the explicit expression for $\left(\frac{d}{d\delta}\right)^{n}$ G_{n} is used ($\frac{1}{2}$ $\frac{1}{\sqrt{1}}$ in the programme), the integrals E_i {2 α (i - ξ)] and E_i (2 α ξ) for G_i (only for $\alpha > 0$, that is LLL=1) and $\int_{\alpha}^{25} d\theta \, \bar{\ell}^{\alpha}$ ℓ^2 for G_n with a positive integer of n $\gamma \propto$ may be negative (LLL=2) J are evaluated first in the calling programme FLUXCA by using the function subprogramme EP. For $|2\alpha|$ < 4 , the subroutine GCAL uses the series expansion for $\left(4T\right)^{m}G_{n}$. In addition, when NSPH=1, it is required to evaluate $\lim_{Y\to 0} 4\alpha i G_{2\pi H}(\alpha_1, Y, \lambda)/\gamma$ as can be seen from Eqs. (1) and (8). Also these values are calculated in the GCAL according to the following forms (the series expansion being used when $|2\alpha| < 2$):
$$
\lim_{\gamma \to 0} \frac{4\alpha i}{\gamma} G_1 (\alpha_1, \gamma, \lambda) = 2 (1 - \bar{\ell}^{\alpha}) = -2 \sum_{n=1}^{\infty} \frac{1}{n!} (-\alpha)^n,
$$
\n
$$
\lim_{\gamma \to 0} \frac{4\alpha i}{\gamma} G_3 = 3 - \frac{10}{\alpha^2} + 2 (1 + \frac{5}{\alpha} + \frac{5}{\alpha^2}) \bar{\ell}^{\alpha} = 2 \sum_{n=1}^{\infty} \frac{1}{(n+2)!} (n+1)(n-3)(-\alpha)^n,
$$
\n
$$
\lim_{\gamma \to 0} \frac{4\alpha i}{\gamma} G_5 = \frac{15}{4} - \frac{35}{\alpha^2} + \frac{376}{\alpha^4} - 2 (1 + \frac{14}{\alpha} + \frac{77}{\alpha^2} + \frac{189}{\alpha^3} + \frac{189}{\alpha^4}) \bar{\ell}^{\alpha}
$$
\n
$$
= -2 \sum_{n=1}^{\infty} \frac{1}{(n+1)!} (n+3)(n+1)(n-3)(n-5)(-\alpha)^n,
$$
\n
$$
\lim_{\gamma \to 0} \frac{4\alpha i}{\gamma} G_1 = \frac{35}{8} - \frac{315}{4\alpha^2} + \frac{2079}{\alpha^4} - \frac{38610}{\alpha^4} + 2 (1 + \frac{27}{\alpha} + \frac{324}{\alpha^2} + \frac{2176}{\alpha^3} + \frac{8613}{\alpha^4} + \frac{11305}{\alpha^5} + \frac{19305}{\alpha^6}) \bar{\ell}^{\alpha}
$$
\n
$$
= 2 \sum_{n=1}^{\infty} \frac{1}{(n+5)!} (n+5)(n+3)(n+1)(n-3)(n-5)(n-7)(-\alpha)^n.
$$

The contribution to the angular flux (and to the first and second time moments), that is the second term on the right-hand side of Eq. (11) or (22) \int and the second terms of Eqs. (26) and (27) \int are calculated in the FLUXCA by calling the subroutine FMCAL(α , ξ , μ , JII,...,m) which evaluates 4α ($\overline{z_1}v_1P_1d_3$)^{m+1} F_{2n} (α_1 , $\overline{z_1}\mu$, Δ) with μ > 0 when JOD=1 or 4α i ($\overline{z_1}v_2P_1d_3$)^{m+1} $X F_{2m+1}(\alpha_1, \xi, \mu, \lambda)$ with $\mu > 0$ when JOD=2 $[\mathcal{M} = -1, 0, 1 \text{ and } n = 0, 1, ..., (110-1)/2]$. This subroutine uses the explicit expression or the series expansion shown in the Appendix 1, Section 6, depending on whether the value $|25\alpha/\mu|$ is larger or smaller than 4. The integer JII=2 is for calculating the functions with different values of m and μ but with the same values of α and ζ (JII=1 otherwise). [Note that $\left(\frac{d}{d\delta}\right)^m F_n(\alpha_1, \zeta, \mu, \Delta) = (-1)^n \left(\frac{d}{d\delta}\right)^m F_n(\alpha_1, \delta, \zeta, \mu, \Delta)$.]

In the case where NSTAT1=1, the above-mentioned calculations are followd by the evaluation of the mean emission time \vec{t} and the variance σ^2 of the time-dependent flux due to a $\delta(t)$ source. For the angular flux, these are written as $[$ see Eqs. (25), (26) and (27) $]$

$$
\bar{t} = \int_0^\infty dt \, t \, v_j \, n_j \, (x, \mu, t) \Big/ \int_0^\infty dt \, v_j \, n_j \, (x, \mu, t) \Big), \tag{41}
$$

$$
\sigma^2 = \int_0^\infty dt \ t^2 \nu_\mathbf{j} n_\mathbf{j} (x, \mu, t) \Big/ \int_0^\infty dt \ \nu_\mathbf{j} n_\mathbf{j} (x, \mu, t) - (\bar{t})^2. \tag{42}
$$

 $\mathcal{L}_{\mathcal{A}}^{\mathcal{A}}$

The \overline{t} and σ^2 are evaluated in the subroutine VARIAC(...., K, NSTAT2) when K=2 and 3, respectively. When K=1 and NSTAT2=2, it produces punched cards for the stationary flux [see Section 4.1 (c)].

4.2.6 INTCAL, FNCUT1, IFNCAL, GIMAG, FMIMG and ADJPUL

The subroutine INTCAL evaluates the contribution of the continuous spectrum to the time-dependent flux when NSTATY (NCURVE in this subroutine)=2,NSPH=0 and LLL=0. It calculates also the contribution of uncollided neutrons to the flux. The flow chart of the INTCAL is shown in the Appendix 2, Section 5. For the evaluation of the contribution of the continuous spectrum, it calls the function subprogramme FNCUT1 (see the Appendix 2, Section 5.1). The control integer KKKK=1, 3 or 5 is for evaluating the contribution to the total number of leakage neutrons, to the total flux or to the angular flux. Therefore, when JJJ (or JJJJ in the main programme) = $1, 2, 3$ or $4,$ KKKK takes the value 1 only, 1 and 3, 3 and 5 or 1,3 and 5. For the calculation of the last term on the right-hand side of Eq. (20), it uses the fact that only the factor *(2Χο/Λ-4")^η* depends on the value of χ_{0} . For the evaluation of the last terms of Eqs. (19) and (11), on the other hand, it makes use of the symmetric relations, $G_{n}(\alpha_{1},\xi,\lambda) = (-1)^{n}G_{n}(\alpha_{1},\xi,\lambda)$ and F_n $(\alpha_1, \xi, \mu, \lambda) = (-1)^n F_n$ $(\alpha_1, \xi, -\mu, \lambda)$, respectively. The newly defined integer NCURVE (\neq NSTATY only in the routine) is therefore put to be 1 immediately after the calculation with NCURVE=0 for evaluating the contribution for the mirrored point, for example, the contribution to $\frac{1}{2}M_{\epsilon}(d-\chi,-\mu,+)$ immediately after the calculation of that to $v_{\gamma} \mathcal{M}_{\gamma}(\chi, \mu, t)$ for NOT time points.

As shown in the Appendix 2, Section 6, in the FNCUT1 (g, t, ξ, \ldots) the value of $\frac{1}{4}$ is first chosen to satisfy the conditions $\frac{1}{4}$ $>>$ 4 and $\frac{1}{4}$ $\frac{1}{4}$ $\frac{1}{2}\frac{1}{2}$ $>>$ for all groups g of interest \int only at the first time when the subprogramme is called (LF=1) *]*. The numerical integration from $y=0$ to y_0 is divided into two parts at $y = \tan (0.9 \tan^{-1} y_0)$. The real and imaginary parts of the integrand are then evaluated for each value of $y = \tan \left[0.9(m/2N)\tan^4\frac{1}{40}\right]$, $m=0,1,...,2N$ (JJJ=1), and $y' = \tan \int 0.9 \tan^4 y_0 + 0.1 (m/2N) \tan^4 y_0$, $m=1,2,...,2N$ (JJJ=2). Since $\overline{B}_n(q,i'j+Z_jv_j-z_jv_j)$ depends only

on g and $\frac{1}{2}$ [see Eq. (37)], the values for $4N+1$ points of $\frac{1}{2}$ are calculated only once for the group g (LOGCL=1 and IGRP=1, these integers being different from those defined in the main programme) by calling the subroutine IFNCAL and then the integrand is evaluated, by the use of these values of β_n , for different time, space or angle points.

In the course of evaluating $B_n(g, i+I_iV_i-T_jV_j)$, the values of $S_j,Z_j/\mathcal{Q}$ $X C_m(\Sigma_j, \mathcal{A}/2, \Lambda) + \sum_{m} J_{nm}(\Sigma_{j'}\mathcal{A}/2, \Lambda) B_m(\mathbf{j'},\Lambda)$ with $\mathcal{A} = i + \mathcal{I} + \mathcal{I} + \mathcal{I} + \mathcal{I} - \mathcal{I} + \mathcal{I} + \mathcal{I} - \mathcal{I} + \mathcal$ the array Y1 or Y2 for $g' = 1, 2, ..., g-1$, in order to use them for computing $Z_n(j, i'j + \sum_i \mathcal{V}_j - \sum_j \mathcal{V}_j)$ and $B_n(j, i'j + \sum_i \mathcal{V}_i - \sum_j \mathcal{V}_j)$, $j = g, g+1, ..., I \text{GRPP}$ [see Eq. (31)]. This is the reason why the calculation begins always with $g=1$, the highest energy-group, when $LF=1$. Since the arrays Y1 and Y2 require generally very big storage, it is recommended, in the case where these arrays are used (NSPH=0, NSTATY=2, LLL=0 and IGRPP =JNKK +NNN>0), to estimate the required size of the floating COMMON according to Tables I and II in advance of the execution so as to be sure that the size is less than the available storage.

After having been obtained the B_{m} 's (Bl in the programme), the coefficients of cos(yt) and sin(yt) [see Eq. (36)] are evaluated by calling the subroutine GIMAG or FMIMG when KKKK=3 or 5 \int for KKKK=1, C_{M1}^* and C_{M2}^* have already been evaluated as a result of calling the IFNCAL (see below) J. The coefficients ZZA are then used to compute the integrand, and the integral is calculated on the basis of the generalized Simpson's rule £ see Eq. (36) J . For evaluating the contribution for different time points [for the same energy-group, space-(and angle-) point and KKKK J , it uses directly the coefficients (L0GCL=2 and IGRP=2). In addition, for the mirrored point (NCURVE=1), the sign of a part of the coefficients is changed due to the control integers, L0GCL=2 and IGRP=1, to obtain new values of the coefficients. For computing the integral for different space- (or/and angle-) points and/or different values of KKKK (but for the same energy-group), the calculated values of B_{α} (β , $i'j+ \lambda_i v_j - \lambda_j v_j$) are used to evaluate the coefficients for this problem (L0GCL=1 and IGRP=2). The last part of the FNCUT1 is devoted to the calculation of the integral over \sharp from $\frac{1}{2}$ to ∞ according to Eq. (38), (39) or (40).

The subroutine IFNCAL ($a\frac{y}{2v}$), KKK,...) evaluates c_n^c and c_{nz}^c (KKK=1 or 2 for odd or even n) shown in the Appendix 1, Section 13, when the angular distribution of the boundary source is monodirectional. When

 $\frac{dy}{2y\mu_1}$ < 1.5, the values are obtained by the use of the series expansion. In addition, this subroutine calculates J_{nm} and J_{nm2} (KKK=1 for odd values of m and n) shown in the Appendix 1, Section 2, and $\zeta_{\mathbf{M}}^{\mathbf{f}}$ and *Ca** (KKK=1 for odd n) shown in the Section 11, the series expansions being used if $a\frac{y}{(2\vartheta_j)} < 1.5$.

The subroutine GIMAG(\bar{y} , $a\frac{y}{12v_j}$, KKK,...) calculates the values of $G_{\bar{m}i}$ and G_{n2} shown in the Appendix 1, Section 5 (the series expansion is used for evaluating the function with $a\sqrt{v_j} < 2.5$) and the FMIMG(\overline{y} , $a\sqrt{v_j\mu}$) KKK,...) evaluates F_{M4} and F_{M2} with a positive value of μ shown in the Section 7, the series expansions being used if $|A/\sqrt{C\gamma}\mu| < 4$. In these two subroutines, KKK=1 or 2 is for evaluating the functions with odd or even n . The control integer LFF transferred through COMMON is put to be 2, instead of 1, for computing the functions with different values of $a\frac{y}{2v_1}$ or $a\frac{y}{y}$ ($v_i\mu$) but with the same value of ζ

The subprogrammes FNCUT1, IFNCAL and GIMAG make use of the library routine $DSICI(SI,CI, X)$ to evaluate the sine and cosine integrals:

$$
\zeta I = \int_{\infty}^{\mathcal{I}} d\bar{z} \frac{\sin \bar{z}}{\bar{z}} = \mathcal{L}i(x) \text{ and } C I = \int_{\infty}^{\mathcal{I}} d\bar{z} \frac{\cos \bar{z}}{\bar{z}} = Ci(x).
$$

Following the evaluation of the continuous spectrum, the INTCAL adjusts the calculated values of the flux by calling the subroutine ADJPUL, because it has been found that the contribution of the continuous spectrum does not converge to the exact value so rapidly (as the order of the j_N approximation increases). The adjustment uses the fact that the integral of the time-dependent flux due to a delta function source, Eq. (25), is equal tothe value of the stationary flux (22).

The ADJPUL therefore evaluates the integral of the time-dependent flux (the contribution of uncollided neutrons being not included) over time from 0 to *OO* under the assumption that the g-th group flux decays exponentially, after the time T(NOT), with the asymptotic decay constant $\Sigma_i \mathcal{V}_i (1 - \lambda_{ij}).$ £rhe Simpson's rule is repeatedly adopted for the integration over time from T(NOT) to 0.] If the calculated value of the integral is larger than the stationary flux, the values of the time-dependent flux are put to be

zero beginning with the flux at t=0 until the integral becomes smaller than the stationary flux. Then, as for the case where the integral of the unmodified flux is smaller than the stationary flux, the first positive flux is adjusted so as to achieve the equality.

To show the measure of the accuracy of the adjusted time-dependent flux, the ADJPUL calculates also the mean emission time \bar{t} (41) and the variance *Q-** (42) of the adjusted flux distribution, which should be equal to the values obtained previously from the stationary calculation (NSTAT1=1) in the FLUXCA.

As mentioned already, the INTCAL evaluates also the contribution of uncollided neutrons to the total number of leakage neutrons (for NSPH=0 and JJJ \neq 3), to the total flux (for JJJ \neq 1) or to the angular flux (for NSPH=0 and JJJ \geq 3) according to the following forms \lceil for NSPH=1, see the first term on the right-hand side of Eq. (1) :

(a) When NSPH=0 and NSTATY=1 ζ see Eqs. (24), (23) and (22)],

$$
\int_0^4 \mathrm{d}\mu \, S_{\mathbf{j}}(\mu) \exp\left(-\frac{\Sigma_{\mathbf{j}}a}{\mu}\right) = S_{\mathbf{j}} E_{\mathbf{2}}(z_{\mathbf{j}}a), 2S_{\mathbf{j}} E_{\mathbf{3}}(z_{\mathbf{j}}a) \text{ or } S_{\mathbf{j}} \exp\left(-\frac{\Sigma_{\mathbf{i}}a}{\mu}\right), \tag{43}
$$

$$
\int_0^A \frac{du}{\lambda} S_{\mathbf{j}}(\mu) exp\left(-\frac{\Sigma_1 \chi}{\lambda}\right) = S_{\mathbf{j}} E_{\mathbf{i}}(\Sigma_{\mathbf{j}} \chi), 2S_{\mathbf{j}} E_{\mathbf{i}}(\Sigma_{\mathbf{j}} \chi) \text{ or } S_{\mathbf{j}} exp\left(-\frac{\Sigma_1 \chi}{\lambda_{\mathbf{i}}}\right) / \mu_{\mathbf{i}}, \qquad (44)
$$

$$
S_3(\mu)exp(-\frac{Z_3\chi}{\mu})/\mu = S_3exp(-\frac{Z_3\chi}{\mu})/\mu, 2S_3exp(-\frac{Z_3\chi}{\mu}) \text{ or } S_3exp(-\frac{Z_3\chi}{\mu})S(\mu-\mu_3)/\mu_{3,(45)}
$$

depending on whether the boundary source is plane isotropic (IIII=0), point isotropic (IIII=1) or monodirectional $(DMUI>0)$.

(b) When NSPH=0 and NSTATY=2 $\left[$ see Eqs. (20), (19) and (11)],

$$
\int_{0}^{1} d\mu \, \zeta_{1}(\mu, t - \frac{a}{v_{1}\mu}) \exp\left(-\frac{z_{1}a}{\mu}\right) = \begin{cases} 2\zeta_{1} \exp\left(-\frac{z_{1}v_{1}t}{2}\right) a^{3}/(\frac{v_{1}^{2}t^{3}}{2}) \\ \text{for } t > a/v_{1} \end{cases}
$$
 (o otherwise), (46b)

$$
\zeta_{1} \exp\left(-\frac{z_{1}a}{\mu_{1}}\right) \zeta(t - \frac{a}{v_{1}\mu_{1}}),
$$
 (46c)

$$
\int_0^4 \frac{du}{\sqrt{u}} S_f(\mu, t - \frac{\gamma}{\sqrt{u}}) \exp\left(-\frac{Z_f \chi}{\mu}\right) = \begin{cases} 2S_f \chi \exp\left(-Z_f \nu_f t\right) / (\nu_f t^2) & \text{for } t > \chi/\nu_f > 0, \\ 2S_f S(t) & \text{for } \chi = 0 \end{cases}
$$
 (20 otherwise), (47b)

$$
S_f \exp\left(-Z_f \chi/\mu_f\right) S(t - \chi/\nu_f \mu_f) / \mu_f
$$
 (47c)

$$
\int 2\tilde{S}_1 \exp(-\Sigma_1 \chi/\mu) \delta(t - \chi/v_1 \mu))
$$
\n(48b)

$$
\pi S_1(\mu, t-\frac{1}{\sqrt[3]{\mu}})\mu \mu \left(-\frac{1}{\mu} \right) = \\ S_1 \exp(-\frac{1}{2}(2/\mu_1)S(\mu_1\mu_1)S(t-\frac{1}{2}(v_1\mu_1))/\mu_1, \qquad (48c)
$$

depending on whether the boundary source is point isotropic or monodirectional.

As seen from Eqs. (43) and (44), the function subprogramme EP is used for evaluating the exponential integral $E_{\mathcal{M}}(R)$. The flow diagramme of this routine is shown in the Appendix 2, Section 5.2.

4.2.7 PULSE

The subroutine PULSE calculates the neutron flux due to a pulse source of the Gaussian distribution in time, $\exp \left\{-\alpha (t-t_o)^2\right\}$ for $T_4 < t < T_2$ (the value of α may be equal to zero), by performing the integration of $\delta(t)$ -source computed in the INTCAL: the flux resulted from a

$$
\varphi_{\rho}(t) = \int_{T_1}^{T_2} dt' \exp\left[-\alpha(t'-t_0)^2\right] \varphi_{\delta}(t-t') = \int_{t-T_2}^{t-T_4} dt' \exp\left[-\alpha(t-t_0-t')\right] \varphi_{\delta}(t') \tag{49}
$$

The integration over t' is performed numerically on the basis of the generalized Simpson's rule. However, for the case where the contribution of uncollided neutrons to $\phi_s(t)$ is written in the form which contains a delta function in time, the contribution to $\phi_p(t)$ is evaluated according to the following analytical expression:

(a) When $NSPH=1$ [see Eq. (1)],

 $\ddot{}$

$$
\int_{t-T_2}^{t-T_1} dt' exp[-\alpha (t-t- t')^2] S_1 exp(-Z_1V_1 t') S(t'-\gamma/V_1) / (4\pi r^2)
$$

= S₁ exp(-Z₁Y) exp[-\alpha (t-t- \gamma/V_1)^2]/(4\pi r^2)
for t-T₁ \ge \gamma/V_1 \ge t-T_2 (0 otherwise), (50)

(b) When NSPH=0 and the boundary source is monodirectional [see Eqs. (46c), $(47c)$ and $(48c)$],

$$
\begin{cases} S_{1} \exp(-z_{1}a/\mu_{1}) S(t^{2} - 4/(v_{1}\mu_{1})) \\ \int_{t^{-1}a}^{t^{-1}a} dt' \exp[-\alpha(t^{-1}t^{-1})^{2}] \times \begin{cases} S_{1} \exp(-z_{1}x/\mu_{1}) S(t^{2} - x/(v_{1}\mu_{1}))/\mu_{1} \\ S_{1} \exp(-z_{1}x/\mu_{1}) S(\mu^{-1}u_{1}) S(t^{2} - x/(v_{1}\mu_{1})) / \mu_{1} \end{cases} \\ S_{1} \exp(-z_{1}x/\mu_{1}) S(\mu^{-1}u_{1}) S(t^{2} - x/(v_{1}\mu_{1})) / \mu_{1} \end{cases}
$$

$$
= \left\{\n\begin{array}{l}\n\tilde{\delta}_{\mathbf{j}} \exp\left(-\frac{\mathbf{y}_{\mathbf{j}}}{2}a/\mu_{\mathbf{i}}\right) \exp\left[-\alpha(t-t_{\mathbf{o}}-\frac{a}{\nu_{\mathbf{j}}\mu_{\mathbf{i}}}\right)^{2}\right] & \text{for } t-T_{\mathbf{i}} \geq \frac{a}{\nu_{\mathbf{i}}\mu_{\mathbf{i}}} \geq t-T_{\mathbf{i}} \text{ (o otherwise)}, \qquad \text{(51c)} \\
\tilde{\delta}_{\mathbf{j}} \exp\left(-\frac{\mathbf{y}_{\mathbf{i}}\mathbf{x}}{2\mu_{\mathbf{i}}}\right) \exp\left[-\alpha(t-t_{\mathbf{o}}-\frac{\mathbf{x}}{\nu_{\mathbf{j}}\mu_{\mathbf{i}}}\right)^{s}\right] & / \mu_{\mathbf{i}}, \qquad \text{(52c)} \\
\tilde{\delta}_{\mathbf{j}} \exp\left(-\frac{\mathbf{y}_{\mathbf{i}}\mathbf{x}}{2\mu_{\mathbf{i}}}\right) \mathcal{S}(\mu_{\mathbf{j}}\mu_{\mathbf{i}}) \exp\left[-\alpha(t-t_{\mathbf{o}}-\frac{\mathbf{x}}{\nu_{\mathbf{j}}\mu_{\mathbf{i}}}\right)^{2}\right] & / \mu_{\mathbf{i}}, \qquad \text{(53c)}\n\end{array}\n\right\}\n\text{ (c) otherwise)},
$$

(c) For the total flux at $\chi=0$ and the angular flux in the case where NSPH=0 and the boundary source is point isotropic [see Eqs. (47b) and $(48b)$],

$$
\int_{t-T_2}^{t-T_1} dt' \exp\{-\alpha(t-t_0-t')^2\} \times \begin{cases} 2S_3 S(t') \\ 2S_1 \exp(-\frac{X_1 X}{y}) S(t'-\frac{X}{y_1}) t \\ 2S_1 \exp(-\frac{X_1 X}{y}) S(t'-\frac{X}{y_1}) t' \end{cases}
$$

= 2S_1 \exp(-\frac{X_1}{y}) \exp[-\alpha(t-t_0-X(v_1)\mu)]² J
for $t-T_1 \geq \frac{X}{y} \Rightarrow t-T_2$ (0 otherwise). (53b)

For these cases, as is shown in the Appendix 2, Section 7, the contribution of uncollided neutrons to $\phi_k(t)$ is first subtracted from $\phi_k(t)$, the numerical integration is performed by using the thus modified $\mathcal{P}_s(t)$ and then the contribution of uncollided neutrons to $\phi_p(t)$ is added to the result. For other two cases where the total number of leakage neutrons and the total flux at $\chi >0$ in a slab with a point isotropic boundary source are calculated, Eq. (49) is used without any modification.

In addition, this subroutine calculates again the integral of $\frac{A}{B}(t)$ [not including the contribution of uncollided neutrons written in the form of a $\delta(t)$] over t from 0 to T(NOT), the mean emission time of $\phi_k(t)$ and the variance Γ the integration is performed only from t=0 to T(NOT)]. Furthermore, it computes the integral of $\phi_{\rho}(t)$ (including the contribution of uncollided neutrons) over t from W(1) to W(NOP), the maximum value of $\phi_{\rm s}(t)$ for W(l) *< t <* W(NOP), the pulse width at half maximum, the mean emission time of $\phi_p(t)$ and the variance of the time distribution.

5. Remarks

It should be mentioned here first how the present computer code deals with neutron transport in a medium with highly anisotropic scattering by the use of the transport approximation. For such media, the values of $C(\frac{4}{3})$ are sometimes negative as seen, for example, in the hydrogen cross section of the LASL 16-group set 12). The code JN-METD1 accepts also a negative value of $C(1)$ but gives all values of the g-th group flux coming from the pole zero (for stationary problems, it makes the value zero to avoid the negative flux and for time-dependent problems there exists no pole). As a result, the calculated flux consists only of the contribution of uncollided neutrons which cannot be treated correctly in the transport approximation. The results for the g-th group with a negative value of $C(j \rightarrow j)$ are therefore not correct (as so the S_N calculation in the transport approximation) but those for other groups with positive values of $C(1,2)$ have been found in a good agreement with the values obtained from the S_{N} calculation taking

Ν

5) into account the linear anisotropic scattering . This defect will be cleared Up when our present work will be completed for dealing with multiregion slab systems with anisotropic scattering.

As already mentioned in the Section 4.2.6, the multigroup calculation of time-dependent problems in a homogeneous slab requires a big computer storage, so that the total number of integral points for evaluating the contribution of the continuous spectrum (the value of N in the input) is sometimes limited to be small $(N<50)$. Since the contribution is dominant only for thin slabs (and for times close to the moment when the wave front of the direct neutron beam arrives), it will be recommended in such cases to use the j^5 approximation instead of j^2 so as to adopt a larger number of $N>70$. It saves also execution time of the computation by about 30% .

Typical running time on the IBM-360/65 is nearly 4 min. to obtain the timedependent lowest group angular and total flux in a slab within the context of a 7-group $j₇$ approximation with 2 space, 3 angle and 56 time points, including the time required for obtaining the stationary flux as well as the time-dependent flux due to a pulse source. The calculation of the stationary angular, total and leakage flux in a slab takes 1 to 2 min. (depending on the slab thickness) in a 7-group $j₇$ approximation with 11 space and angle points. All four sample problems shown in the Appendix 3 take about 2 min.

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The explicit expressions and series expansions of functions in the solution of the $j₇$ approximation are summarized here by introducing the abbreviations $\alpha \equiv \alpha_3 P_3$, $P_3 \equiv \left(-\frac{(x_1v_1 - x_3)}{(x_3v_3)}, \frac{y_1 z_1}{(x_3v_3)}\right)$ $(\alpha = i \gamma$ when $j = i \frac{y_1 + x_1v_1 - x_1v_3}{(x_3v_3 + x_1v_3)}$

$$
\frac{1}{P_3} \int_{0.0}^{1} f(x_3) dx
$$
\n
$$
\frac{1}{P_3} \int_{0.0}^{1} f(x_3) dx
$$
\n
$$
= \alpha (-\ln 20x^2 + \frac{1}{2}x) + \sum_{n=2}^{\infty} \frac{1}{(n+1)(n+1)} (-20x)^n
$$
\n
$$
\frac{1}{P_3} \int_{44}^{1} f(x_3) dx
$$
\n
$$
\frac{1}{P_3} \int_{44}^{1} f(x_3) dx
$$
\n
$$
\frac{1}{P_3} \int_{0.0}^{1} f(x_3) dx
$$
\n
$$
\frac{1}{P_3} \int_{0.0}^{
$$

 \sim

P₁ J₁₅ =
$$
-\frac{1}{4\alpha} + \frac{7}{3\alpha^2}(t-\frac{3}{2\alpha^2}t^{2\alpha}) - \frac{45}{7\alpha^2}(t+\frac{23}{7\alpha^2}t^{2\alpha}) + \frac{63}{2\alpha^2}(t+\frac{17}{4\alpha^2}t^{2\alpha}) - \frac{475}{4\alpha^2}(t+\frac{7}{4\alpha^2}t^{2\alpha})
$$

\n $-\frac{245}{12\alpha^2}t^{2\alpha} + \frac{145}{4\alpha^2}(t-\frac{1}{2}\alpha^2) - \frac{165}{6\alpha^2}(t+\frac{17}{2\alpha^2}t^{2\alpha}) - \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^{2\alpha})$
\nP₁ J₃₅ = $\frac{1}{4\alpha} - \frac{3}{2\alpha^2}(t+\frac{1}{4\alpha}t^2)^2 + \frac{145}{4\alpha^2}(t+\frac{17}{4\alpha}t^2)^2 - \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}(t+\frac{175}{4\alpha^2}t^{2\alpha}) + \frac{235}{2\alpha^2}t^{2\alpha} - \frac{215}{4\alpha^2}(t+\frac{17}{4\alpha^2}t^2)^2 - \frac{175}{4\alpha^2}(t+\frac{175}{4\alpha^2}t^2)^2 + \frac{1755}{4\alpha^2}(t+\frac{175}{4\alpha^2}t^2)^2$
\n $- \frac{25}{4\alpha}(t+\frac{17}{4\alpha^2}t^2)^2 + \frac{175}{4\alpha^2}($

$$
P_{3} J_{57} = \frac{1}{4\alpha} - \frac{13}{6\alpha^{2}} (1 - \frac{3}{26} \bar{\epsilon}^{2\alpha}) + \frac{63}{8\alpha^{3}} (1 + \frac{63}{63} \bar{\epsilon}^{2\alpha}) + \frac{205}{64} \bar{\epsilon}^{2\alpha} - \frac{115}{2\alpha^{5}} (1 - \frac{1013}{35} \bar{\epsilon}^{2\alpha}) + \frac{21645}{66} \bar{\epsilon}^{2\alpha} + \frac{6615}{64} (1 + \frac{1702}{24} \bar{\epsilon}^{2\alpha}) + \frac{612910}{66} \bar{\epsilon}^{2\alpha} - \frac{127515}{4\alpha^{3}} (1 - \frac{1754}{27} \bar{\epsilon}^{2\alpha}) + \frac{20322225}{4\alpha^{10}} \bar{\epsilon}^{2\alpha} + \frac{1002075}{6611} (1 + \frac{1821}{77} \bar{\epsilon}^{2\alpha})
$$

+ $\frac{18243225}{2\alpha^{12}} \bar{\epsilon}^{2\alpha} - \frac{18243225}{4\alpha^{13}} (1 - \bar{\epsilon}^{2\alpha}) = \sum_{\pi=1}^{\infty} \frac{(n-11)(n-1)(n-1)(n-5)(n+3)\pi}{(n+1)(n+1)(n+1)(n+1)(n+5)(n+3)} (-2\alpha)^{n}$
+ $\frac{1}{2\alpha^{12}} \sum_{\pi=1}^{\infty} \frac{1}{4\alpha^{2}} \bar{\epsilon}^{2\alpha} + \frac{1}{2\alpha^{3}} (1 - \frac{103}{26} \bar{\epsilon}^{2\alpha}) - \frac{1431}{4\alpha^{4}} \bar{\epsilon}^{2\alpha} - \frac{161}{2\alpha^{5}} (1 + \frac{5301}{64} \bar{\epsilon}^{2\alpha}) - \frac{564525}{8\alpha^{6}} \bar{\epsilon}^{2\alpha}$
+ $\frac{23625}{8\alpha^{7}} (1 - \frac{16533}{50} \bar{\epsilon}^{2\alpha}) - \frac{16821505}{4\alpha^{6}} \bar{\epsilon}^{2\alpha} - \frac{363825}{4\alpha^{4}} (1 + \frac{$

$$
J_{334} = -\frac{1}{4\pi^3} \left\{ i + \frac{1}{4} \sin(27) + \frac{1}{2\pi^2} \left\{ j - 2 \cos(27) \right\} + \frac{16}{2\pi^2} \sin(27) + \frac{16}{2\pi^2} \left\{ j + 2 \sin(27) \right\} - \frac{26}{2\pi^2} \left\{ k + \frac{1}{2} \sin(27) \right\} = -2 \frac{26}{6\pi^2} \left\{ k + \frac{1}{2} \sin(27) \right\} = -2 \frac{26}{6\pi^2} \left\{ k + \frac{1}{2} \sin(27) \right\} = -2 \frac{26}{6\pi^2} \left\{ k + \frac{1}{2} \sin(27) - \frac{24}{2\pi^2} \left\{ j + \frac{1}{2} \sin(27) - \frac{1}{2} \frac{2}{\pi^2} \left\{ j + \frac{1}{2} \cos(27) \right\} \right\} \right\}
$$

\n
$$
J_{pq} = -\frac{1}{7\pi^2} \left\{ j + \frac{1}{2} \sin(27) - \frac{1}{2} \frac{1}{2} \left\{ j + \
$$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^d} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2\left(\frac{1}{\sqrt{2}}\right)^2.$

 $\mathcal{L}^{\text{max}}_{\text{max}}$

$$
J_{352} = \frac{1}{479} \left\{6 - \cot (27) + \frac{23}{27} \sin (27) + \frac{474}{17} \cot (27) - \frac{7125}{272} \sin (27) - \frac{5335}{272} \cot (27) + \frac{20475}{472} \sin (27) + \frac{5576}{272} \cot (27) - \frac{2835}{272} \sin (27) \right\} = \frac{456}{272} \left\{ - \frac{1}{272} \sin (27) + \frac{20475}{272} \sin (27) \right\} = \frac{4567}{272} \sin (27) - \frac{1037}{272} \sin (27) \frac{404}{272} \cos (27) - \frac{1635}{272} \sin (27) + \frac{5576}{272} \left\{ - \frac{1}{7} \sin (27) + \frac{3}{272} \left[5 + 19 \cot (27) \right] + \frac{278}{215} \sin (27) + \frac{1576}{215} \left[1 + 12 \tan (27) \right] - \frac{1635}{27} \sin (27) \right\}
$$

+ \frac{2767}{27} \left\{ 5 - 14 \cot (27) \right\} = - \frac{25}{476} \left\{ - \frac{1}{17} \frac{1}{17} \cos (27) \right\} = - \frac{276}{476} \left\{ - \frac{1}{17} \left(\frac{1}{17} \cos (27) \right) - \frac{1776}{27} \cos (27) \right\} = \frac{271675}{27} \sin (27) - \frac{27765}{27} \sin (27) \right\}

$$
- \frac{271675}{27} \left\{ - \frac{1}{17} \cos (27) - \frac{1771}{27} \sin (27) - \frac{1771}{27} \cos (27) - \frac{2775}{27} \sin (27) \right\}
$$

$$
- \frac{276}{27} \left\{ - 14 \cos (27) - \frac{1771}{27
$$

$$
J_{572} = \frac{4}{73} \int \frac{13}{6} - \frac{1}{4} \int \frac{13}{6} - \frac{13}{6} \int \frac{13}{6} - \frac{143325}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{13322525}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{1332525}{27} \int \frac{13}{6} - \frac{1332525}{47} \int \frac{13}{6} - \frac{1332525}{47} \int \frac{13}{6} - \frac{1332525}{6} \int \frac{13}{6} - \frac{13325}{6} \int \frac{13}{6} - \frac{1
$$

 $\mathcal{L}^{\text{max}}_{\text{max}}$ and $\mathcal{L}^{\text{max}}_{\text{max}}$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^{2}}\left|\frac{d\mu}{\mu}\right|^{2}d\mu\left(\frac{d\mu}{\mu}\right)\left|\frac{d\mu}{\mu}\right|^{2}d\mu.$

3. $\frac{d}{ds} J_{nm}(\alpha_1, \lambda)$

$$
\Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{00} = -4 + \frac{1}{2\alpha} (4 - \bar{\ell}^{2\alpha}) = \frac{29}{\pi\epsilon} \frac{4}{(\pi + \lambda)!} (-2\alpha)^{n}
$$
\n
$$
\Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{44} = -\frac{4}{3} + \frac{1}{2\alpha} (4 + \frac{1}{\alpha}) \left(1 - \frac{1}{\alpha} + (4 + \frac{1}{\alpha}) \bar{\ell}^{2\alpha} \right) = -\frac{29}{\pi\epsilon} \frac{(\pi - 1)(\pi + 2)}{(\pi + 3)!} (-2\alpha)^{n}
$$
\n
$$
\Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{02} = -\frac{4}{2\alpha} \left(4 - \frac{3}{\alpha} + \frac{3}{\alpha^{2}} - (4 + \frac{3}{\alpha} + \frac{3}{\alpha^{2}}) \bar{\ell}^{2\alpha} \right] = -\frac{29}{\pi\epsilon} \frac{(\pi - 1) n}{(\pi + 3)!} (-2\alpha)^{n}
$$
\n
$$
\Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{22} = -\frac{1}{5} + \frac{1}{2\alpha} (4 + \frac{3}{\alpha} + \frac{3}{\alpha^{2}}) \left[-2\alpha \Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{02} \right] = \frac{29}{\pi\epsilon} \frac{(\pi - 3)(n - 1)(\pi + 2)}{(\pi + 5)(n + 3)!} (-2\alpha)^{n}
$$
\n
$$
\Sigma_{1}V_{1}P_{1}^{2} \frac{d}{dx} J_{13} = -\frac{1}{2\alpha} (4 + \frac{1}{\alpha}) \left(1 - \frac{1}{\alpha} + \frac{15}{\alpha^{2}} - \frac{15}{\alpha^{2}} + (4 + \frac{15}{\alpha} + \frac{15}{\alpha^{2}}) \frac{1}{\alpha^{2}} \frac{d}{dx} J_{13} \right) (-\frac{10}{\alpha^{2}} - \frac{10}{\alpha^{2}} \frac{(\pi - 3)(n - 1)\pi}{(\pi + 5)(n + 3)!} (-2\alpha)^{n}
$$

$$
\sum_{i} \sum_{j} P_{i}^{2} \frac{1}{44} J_{14} = -\frac{1}{4} + \frac{1}{44} (1 + \frac{10}{64} + \frac{25}{64} + \frac{105}{64} + \frac{105}{
$$

 $\mathcal{L}^{\text{max}}_{\text{max}}$ $\frac{1}{\sqrt{2}}\int_{0}^{\sqrt{2}}\frac{1}{\sqrt{2}}\left(\frac{1}{2}\right) \left(\frac{1}{2$

 $\sigma_{\rm{max}}$

$$
\frac{4.66(69-25.1,3)^{23}}{4066-[(+2^{20(1+5)}+20(1+5))^2} + \frac{49}{27}e^{20(1+5)/2} + [5+5]^2
$$
\n
$$
= 20([-h)(20(1+5))+1+2+5h((\frac{1+5}{5})]+ \frac{6}{60} + \frac{1}{10}(1+5)^{20/4} + (25)^{20/4} [(-6)^{20/4}]
$$
\n
$$
40i61 = [25-1-(5+\frac{1}{20})\bar{p}^{20(1+5)} + 20(5+5) (\frac{1}{10})\bar{p}^{2} + \frac{6}{60} + \frac{1}{10}(1+21+5) (25)^{20/4} [(-6)^{20/4}]
$$
\n
$$
= (25-1)(7-205(1+5))h((\frac{1+5}{5}) + \frac{2}{60} + \frac{1}{10}(1+21+5)) (25)^{20/4} [(-6/3^{20/4})]
$$
\n
$$
40662 = [(5(1+5)+1-\frac{1}{60}+15)(35-1)+\frac{1}{60}+5(\frac{1}{10}+1)(35-1)(45)^{20/4} + \frac{1}{60}+15(35-1)+(\frac{1}{60}+1)(30-1)(35)^{20/4} [(-6/3^{20/4})]
$$
\n
$$
+ [5+1.5] = 20(25(1+5)-\frac{1}{6}+5(1+5)(3-4))h((\frac{1+5}{5}) - \frac{6}{60} + \frac{1}{10}(1+2)(15-1)+15(3-1)+
$$

$$
G_{n}(\alpha_{3}, 25-1, i'_{1}+2i\alpha_{-}+i\gamma_{3}) \equiv \frac{1}{7}(G_{n1}+iG_{n2})^{1/2}
$$
\n
$$
2G_{04} = \left\{\frac{1}{2}sin(2\eta(i+5) + \eta(i+5))\right\}^{2} + \left\{\frac{1}{2}cos(2\eta(i+5) + \xi)\right\} + \left\{\frac{1}{2}cos(2\eta(i+5) + \xi)\right\}
$$
\n
$$
= \eta \left\{-\ln[2\eta(i+5) + \xi] + \eta \frac{1}{2}\ln(\frac{1-\xi}{5}) - \frac{52}{2}(-1)^{n} \frac{1}{4\eta(2\eta+i) + 1}[(2(i+5))^{2\eta+i} + (25)^{2\eta+i})\right] \eta^{2\eta+i} + 2G_{02} = -1 + \left\{\frac{1}{2}cos(2\eta(i+5) - \eta(i+5))\right\}^{2} + \left\{\frac{1}{2}sin(2\eta(i+5) + \xi)\right\} + \left\{\frac{1}{2}cos(2\eta(i+5) - \eta(i+5))\right\}^{2} + \left\{\frac{1}{2}cos(2\eta(i+5) + \xi)\right\}
$$
\n
$$
= -\frac{\pi}{2}\eta - \frac{52}{2}(-1)^{n} \frac{1}{2(2\eta+i)(2\eta)}[(2(i+5))^{2\eta} + (25)^{2\eta} \frac{1}{2}\eta^{2\eta} + 25\eta^{2\eta} \frac{1}{2}cos(2\eta(i+5) + \xi)\eta^{2\eta} +
$$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2}d\mu\left(\frac{1}{\sqrt{2\pi}}\right) \frac{d\mu}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2}d\mu\left(\frac{1}{\sqrt{2\pi}}\right).$

2G₁₂ = -{
$$
\frac{1}{4}\sqrt{3}sin[2(1/5)] + \frac{1}{47}cos[2(1/5)] + {5+5}-25(1-5)\frac{33}{248}cos(1/2)
\n= $\frac{1}{2}(1+35)\pi + (25(1-5)\pi + (\frac{15}{5}) + \frac{5}{24}(1/5 + \frac{1}{47(27)(21)}[C2(1+35)(21+5))^{28}cos(1/2)
\n= $\frac{1}{2}(1+35)+\frac{1}{47}[sin[2(1/5)] - \frac{1}{47}(1+35)cos[2(1/5)] + {5+5} - 18(1+35)(1+35)
\n= $\frac{1}{12}[5(1+35)+\frac{1}{47}[sin[2(1/5)] - \frac{1}{47}(1+35)cos[2(1/5)] + {5+5} + 18(-5)(1+35)
\n= $\frac{1}{12}[5(1+35)+\frac{1}{47}[sin[2(1/5)] - \frac{1}{47}(1+35)cos[2(1/5)] + {5+5} - 18(-5)(1+35)
\n= $\frac{1}{12}[5(1+35)+\frac{1}{47}[sin[2(1/5)] - \frac{1}{47}(1+35)cos[2(1/5)] + {5+5} - 18(-5)(1+35)
\n+ $[3(1+3)(3+4)] = 2\frac{3}{44}(1+\frac{1}{2}(1+35)(1+35)) = \frac{5}{44}(1+\frac{1}{2}(1+35)(1+35)) = \frac{5}{47}(1+\frac{1}{27}(1+35)+\frac{1}{27}(1+\frac{1}{27}(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1}{27})(1+\frac{1$$$$$$
$$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\$

$$
2G_{52} = -\left{\frac{1}{2}\left{\frac{1}{2}\left{5}\left{(l-H_{\overline{5}}\left(l-3\overline{5}\left(l-3\overline{5}\left(l-5\right)\right)\right)-\frac{1}{l_{\overline{1}2}}\left(l+5+3\overline{5}^3\right)+\frac{l_{\overline{2}2}}{l_{\overline{1}2}}\left{(2+\overline{5}\right)\right]\right}+\frac{1}{l_{\overline{1}1}}\left{(l+5\overline{5}\right)^2+\frac{1}{l_{\overline{1}2}}\left{(2+\overline{5}\right)^2\right}+\frac{l_{\overline{2}2}}{l_{\overline{1}2}}\left{(2+\overline{5}\right)^2\right}+\frac{l_{\overline{2}2}}{l_{\overline{1}2}}\left{(l+5\overline{5}\right)^2\left{-2\left{\frac{1}{2} - l_{\overline{1}2}\left(l-3\right)\left\{-H_{\overline{3}}\left(l+3\right)\left(l+3\right)\right\}}\right\}}\right}
$$

\n
$$
\times \int_{2(l+\overline{3})}^{2\overline{5}} \frac{d_2}{2} \cos\left(\frac{\eta z}{2}\right) = \frac{1}{30}\left(l-2\overline{5}\right)\left{\frac{1}{2} + l_{0}5\overline{5}\left(l+3\right)\left(l+6\overline{5}\left(l+3\right)\right)}\right} \frac{1}{l_{\overline{1}2}\left(l+5\right)\left{\frac{1}{2} + l_{1}5\left(l+5\right)\left(l+4\overline{5}\left(l+5\right)\right)\left(l+3\overline{5}\left(l+3\right)\right)}\right\}}{\times \ln\left(\frac{4-\overline{5}}{5}\right) + \sum_{i=1}^{\infty} \left(-i\right)\frac{\eta}{l_{\overline{1}1}\left(2l_{\overline{1}1}+\overline{6}\right)}}{\left(n+3\right)\eta}\left\{\frac{\eta}{2} + \frac{\eta}{2}\eta\right\}}
$$

$$
2G_{64} = \left\{\frac{1}{2}[\xi(1\cdot25)(1\cdot3(1\cdot3(1\cdot65)(1\cdot5))) + \frac{1}{72}(10+13\cdot4185^2-333^2+665^4) - \frac{9}{74}(50+333+223^2) + \frac{1485}{76}\right\}
$$

\n
$$
\times \sin [27(1\cdot3) - \frac{1}{47}(1+23-185^2+1025^2-1985^4+1325^5 - \frac{9}{72}(20+175+115^2+225^3) + \frac{195}{74}(5+25)\right]
$$

\n
$$
\times \cos [27(1\cdot3) - \frac{1}{47}(3+3\cdot3\cdot4) - 3\cdot3\cdot4\cdot5] + 75(1\cdot5)(1\cdot25)\left\{-5(1\cdot5)(18-65(1\cdot3))\right\} \int_{2(1\cdot3)}^{25} \frac{d^2}{2} \omega_3(7/2)
$$

\n
$$
= \left\{\frac{1}{10} \cdot 5(1\cdot5)(39-10\cdot5)(4\cdot7\cdot325(1\cdot5)) - \frac{1}{42}\right\} \left\{-75(1\cdot5)(1\cdot25)\right\} \left\{-5(1\cdot5)(18-65)(1\cdot3)(18-65(1\cdot3))\right\} \int_{2(1\cdot3)}^{25} \mu_1(\frac{1\cdot3}{5})
$$

\n
$$
+ \sum_{n=1}^{\infty} (-1)^n \frac{1}{4n(2n+1)!} \left\{-n\cdot32n\right\} \frac{1}{2^{2n+1}}
$$

$$
2G_{71} = (25-1)\{1-6\frac{1}{3}(1-3)(1-1)\{1-6\frac{1}{3}(1-3)(1-1)\{1-3(1-3)(1-2)\} - \frac{42}{72}(1-3)(1-1)\{1-3(1-3)(1-1)\} - \frac{19305}{76}\} - \frac{1}{2}[5(1-35(1-3)(1-115(1-3)(6-135(1-3)))] - \frac{3}{272}(1+15+663-1435^4+1435^5) + \frac{91}{274}(25+195+1435^2+1435^3)- \frac{19305}{47}(3+5)\} \text{cos}(29(1+5)) - \frac{4}{47}(1+275^2-1985^3+6275^4-8585^5) + \frac{91}{274}(125+195+1435^3+1435^3)- \frac{19305}{476}(3+5)\} \text{cos}(29(1+5)) - \frac{4}{47}(1+275^2-1985^3+6275^4-8585^5) + \frac{91}{274}(75+665+165+165+165^2+1435^4)+ \frac{495}{274}(45+265+135^2)- \frac{135135}{476}\} \text{sin}(129(1+5)) \} + \{5\} - \frac{4}{774}(1-3)(1-35(1+5))\{1-35(1+5)(1-435(1+5))\} \} \frac{1}{2} - \sum_{n=1}^{\infty} (-1)^n \frac{1}{2(n+1)(2n+1)} \{n \rightarrow 2n-1\} \frac{1}{2} \frac
$$

$$
4572 = 1519 - 3314 - 3311 - 3314 - 3311 - 33514 - 3311 - 354 - 3311 - 354 - 3111 - 3514 - 3111 - 3314 - 3111 - 3314 - 3111 - 412 + 311 + 4111 - 411 - 4111 - 411
$$

 $\label{eq:2} \mathcal{L} = \mathcal{L} \left(\mathcal{L} \right) \left(\mathcal{L} \right) \left(\mathcal{L} \right) \left(\mathcal{L} \right)$

 $\label{eq:1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty} \frac{1}{\sqrt{2\pi}}\,d\mu\,d\mu\,.$

<u>6. Fx</u> $(\alpha_1, \overline{s}, \mu, \lambda)$, $\mu > 0^c$ $4\alpha F_0 = 1 - \mathcal{L}^{2\alpha}$ $\mathcal{L}^{\mu} = -\sum_{k=1}^{\infty} \frac{1}{2n!} (-2\alpha \frac{1}{2k})^n$ $4\alpha i F_1 = 23 - 4 - \frac{\mu}{\alpha} + (4 + \frac{\mu}{\alpha}) \bar{\ell}^{2\alpha} = \frac{69}{\pi} \frac{1}{(0.44)}$ (n+4-23) (-2 $\alpha \frac{3}{\mu} \gamma^{\alpha}$ $40F_2 = 65(F3)-1-3(F25)+2-3(F+1)+3(4+3F+3)(4^2) e^{-205/4}$ $=\sum_{n=1}^{\infty}\frac{4}{(n+2)!}\left\{ n^2+3n(n-25)+2(1-15)(1-5) \right\} (-20+1)^n$ $4\alpha i F_3 = (4-23)[1+103(1-3)]+6[1-53(1-3)]\frac{\mu}{\alpha}+15(1-23)(\frac{\mu}{\alpha})^2+15(\frac{\mu}{\alpha})^3-[1+6\frac{\mu}{\alpha}+15(\frac{\mu}{\alpha})^2+15(\frac{\mu}{\alpha})^3]\bar{L}^{2\alpha}$ $=-\sum_{n=1}^{\infty}\frac{1}{(n+3)!}\Big\{n^3+(n^2(1-25)+n(11-605(1-5))] + (1-23)(1-105(1-5))] + (20\frac{3}{11})^n$ $40F_4$ = 1-205(+3){1- $\frac{7}{2}$ 3(+3)]+10(423){1-73(1-3)] $\frac{11}{10}$ +45{1- $\frac{12}{3}$ J($\frac{11}{3}$)⁺105(423)($\frac{11}{10}$)³+105($\frac{17}{10}$)⁴ $-[1+10\frac{\mu}{\alpha}+45(\frac{\mu}{\alpha})^2+105(\frac{\mu}{\alpha})^3+105(\frac{\mu}{\alpha})^6]$ $Ie^{-2\alpha}$ $J/\mu=-\sum_{n=1}^{\infty}\frac{1}{(n+1)!}\left\{n^2+10n^3(1-25)+5n^2(7-3654-3)\right\}$ +10n(1-23){5-423(+3)]+24-4803(43){1- $\frac{7}{2}$ 5(+3)]}(-2a $\frac{7}{2}$)ⁿ, $4aiF_6 = (25-1)\{1-28\}(1-\frac{9}{2})\{1-\frac{9}{2}\}(1-\frac{9}{2})\}-15\{1-11\}(1-\frac{9}{2})\{1-3\}(1-\frac{9}{2})\}$ $\frac{11}{12} - 105(1-25)\{1-6\}(1-\frac{9}{2})\{(1-\frac{9}{2})^2\}$ -42011-25(1-3)](2)-945(1-23)(2)-945(2)-1-15(2)-11-15/2+105(2)-1-20(2)³+945(2)⁹+945(2)⁵] $X \bar{E}^{20.5/\mu} = \sum_{n=1}^{\infty} \frac{4}{(n+5)!} \Big\{ n^5 + 45 n^4 (1-25) + 5n^3 (17-845)(1-5) + 15n^2 (1-25) (15-1125)(1-5) \Big\}$ $+2n(137-314-3)(2310-7560811-3)) +120(1-23)11-3(1-3)(28-126311-3))]\big\}(-20,1)$ $4\alpha F_6$ = 423(+3){1-93(+3){1- $\frac{22}{9}$ 3(+3)]}-1-21(1-23){1-183(+3){1-4}5(+3)]} $\frac{\mu}{\alpha}$ -210{1-123(+3) x {4-\$\\$(+3)]}{{#}²-1260(1-25){1-\$\\$(1-3)]{#}³-4725{1-²²}5(1-3)]{#J¹-10395(1-23){#J⁵ $-40395\left(\frac{\mu}{G}\right)^{2}+\left[1+21\frac{\mu}{G}+210\left(\frac{\mu}{G}\right)^{2}+1260\left(\frac{\mu}{G}\right)^{2}+4725\left(\frac{\mu}{G}\right)^{4}+10395\left(\frac{\mu}{G}\right)^{5}+10395\left(\frac{\mu}{G}\right)^{6}\right]\left[\frac{203\mu}{G}\right]$ $=\sum_{i=1}^{\infty}\frac{1}{(n+i)}\left\{n^6+24n^5(4-25)+35n^4(5-2454-5)\right\}+405n^3(4-25)(7-485(4-5))+56n^2(29-5)(15)$ $X(435-1350)(15))$] +252n(1-23)17-3(13)(160-6603(1-3))] +720 $-302405(1-3)(1-5(1-3)(9-225(1-3)))$ }(-20 $\frac{5}{10}$) 40 i F_n = (1-25) {1-543l+3) [1-115l+3) (1- $\frac{26}{7}$ 5l1-3) } + 2⁰ 1-275 (1-3) [1- $\frac{22}{3}$ 5l1-3) (1- $\frac{13}{6}$ 5l+3))] } $\frac{1}{60}$ $+378(1-25)\{1-\frac{41}{35}(1+5)(1-\frac{13}{25}(1+5))] \}$ $(\frac{\mu}{\alpha})^2+3150\{1-115(1+5)(1-\frac{13}{55}(1+5))\}$ $(\frac{\mu}{\alpha})^3$ +17325(4-23){1- $\frac{26}{5}$ 5(4-3)]($\frac{14}{6}$)⁴+62370{1- $\frac{13}{3}$ 5(1-3)]($\frac{14}{6}$)⁵+135135(1-23)($\frac{14}{6}$)⁴+135135($\frac{14}{6}$)⁷ -[4+2δ* +31δ(#) +3450(#) +47325(#) +42370(#) - 435435(#) +435435(#) 7] ε^{-2α} ^y/ $=-\sum_{i=1}^{52}\frac{1}{(i!+1)!}\left\{ n^7+28n^4(4-25)+14n^5[23-1085(1-3)]+280n^4(1-25)[7-153(1-3)]+7n^3[1967+123(1-3)]\right\}$ $-5(1 - 3)(13320 - 396005(1 - 3))3 + 2871^2(1 - 25)(129 - 351105(1 - 3))3 + 3671563$ –5(1-3)(12488–3(1-3)(103180–2402403(1-3)))]+5040(1-23)[1-3(1-3)(51-3(1-3)(594-17163(1-3)))]} $X(-2\alpha\frac{1}{M})^n$

7.
$$
\Gamma_n (\alpha_1, \overline{s}, \mu, i^1 + \overline{z_1} \alpha_1 - \overline{z_1} \alpha_1 - \overline{z_1} \alpha_1 + \overline{z_1} \alpha_1 + \overline{z_1} \alpha_1 - \overline{z_1} \alpha_1 -
$$

$$
4F_{q1} = (25-1)\{1-54514\cdot5\}(1-14514\cdot5)(1-\frac{26}{9}\cdot5(1-5))1-378\cdot1-\frac{44}{3}\cdot5(1-5)(1-\frac{12}{4}\cdot5(1\cdot5))1(\frac{14}{17})^{2}
$$

+17325\cdot1-\frac{26}{5}\cdot5(1\cdot5)1(\frac{14}{17}-135435(\frac{14}{17})^{6}+1(1-378(\frac{14}{17})^{2}+17325(\frac{14}{17})^{6}+135135(\frac{14}{17})^{6}]\cot(27\frac{7}{6})
-7\frac{14}{1}(1-150(\frac{14}{17})^{2}+8910(\frac{14}{17})^{4}-19305(\frac{14}{17})^{6}]\sin(27\frac{7}{6}) = \sum_{n=1}^{\infty}(-1)^{n}\frac{1}{(2n+1)!}\{n\cdot2n\}\{27\frac{7}{6}n\}^{2n}

$$
4F_{q2}=7\frac{14}{17}\{4(1-27)\cdot5(1-\frac{22}{3}\cdot5(1-3)(1-\frac{12}{6}\cdot5(1-3))11-150(1-115(1+3)(1+\frac{12}{3}\cdot5(1-3))1(\frac{14}{17})^{2}
$$

+891011-\frac{12}{3}\cdot5(1\cdot5)1(\frac{14}{17}-19305(\frac{14}{17})^{6}-11\cdot378(\frac{14}{17})^{2}+17325(\frac{14}{17})^{6}-135135(\frac{14}{17})^{6}]\sin(27\frac{7}{6})
-7\frac{14}{7}(19-150(\frac{14}{17})^{2}+8910(\frac{14}{17})^{6}-19305(\frac{14}{17})^{6}]\cos(27\frac{7}{6})=\sum_{n=1}^{\infty}(-1)^{n}\frac{1}{(2n+6)}\{n\cdot3n-4\}(27\frac{7}{6})^{2n+1}

8.
$$
A_n(\alpha_1, \lambda)
$$

\n $\alpha A_1 = 1 - \bar{\ell}^{\alpha} = -\sum_{n=1}^{\infty} \frac{1}{n!} (-\alpha)^n$
\n $\alpha A_3 = \frac{3}{2} - \frac{5}{\alpha^2} + (1 + \frac{5}{\alpha} + \frac{5}{\alpha^2}) \bar{\ell}^{\alpha} = \sum_{n=1}^{\infty} \frac{1}{(n+2)!} (n-3)(n+1)(-\alpha)^n$
\n $\alpha A_5 = \frac{45}{8} - \frac{35}{2\alpha^2} + \frac{378}{04} - (\frac{74}{8} + \frac{91}{2\alpha} + \frac{343}{2\alpha^2} + \frac{378}{01^3} + \frac{978}{01^3}) \bar{\ell}^{\alpha} = -\sum_{n=1}^{\infty} \frac{1}{8(n+1)!} (n+1)(n+3)(n+1)(n+1)(\alpha) (-\alpha)^n$
\n $\alpha A_7 = \frac{35}{16} - \frac{345}{80^2} + \frac{3079}{0^4} - \frac{115830}{0^6} + (\frac{367}{4} + \frac{5265}{80} + \frac{30609}{60^2} + \frac{11236}{0^3} + \frac{55836}{0^4} + \frac{115830}{0^5} + \frac{145830}{0^6}) \bar{\ell}^{\alpha}$
\n $= \sum_{n=1}^{\infty} \frac{1}{8(n+6)!} (n+3)(n+5) \left[(n+4)(n+6)(734n^2-3063n+24547) - 4752(219n+109) \right] (-\alpha)^n$

$$
\frac{9. C_{n}^{a} (\alpha_{1}, \beta)}{2N C_{0}^{a} = 4 - \frac{7}{2} \alpha + 2 \alpha \int_{1}^{\infty} \frac{dP}{2} \bar{E}^{2N} \bar{Z} = 2 \alpha [1 - \gamma - \ln(2\alpha)] + \sum_{n=1}^{\infty} \frac{1}{n(n+1)!} (-2 \alpha)^{n+1}
$$
\n
$$
2N C_{4}^{a} = -\frac{1}{2} \alpha + \frac{1}{2} \alpha \frac{1}{2} \alpha^{2N} = -\sum_{n=0}^{\infty} \frac{1}{(n+2)!} (-2 \alpha)^{n+1}
$$
\n
$$
2N C_{4}^{a} = -1 + \frac{3}{2} \alpha - \frac{1}{\alpha^{2}} + \frac{1}{\alpha} (\frac{1}{2} + \frac{1}{\alpha}) \bar{E}^{2N} = -\sum_{n=0}^{\infty} \frac{1}{(n+3)!} (n+1)(-2 \alpha)^{n+1}
$$
\n
$$
2N C_{4}^{a} = -1 + \frac{3}{2} \alpha - \frac{1}{\alpha^{2}} + \frac{1}{4} \overline{\alpha^{2}} - \frac{1}{2 \alpha} (1 + \frac{5}{\alpha} + \frac{15}{2 \alpha^{2}}) \bar{E}^{2N} = \sum_{n=0}^{\infty} \frac{1}{(n+1)!} (n-1)(n-2)(-2 \alpha)^{n+1}
$$
\n
$$
2N C_{4}^{a} = -\frac{1}{2} \alpha + \frac{15}{\alpha^{2}} - \frac{105}{4 \alpha^{2}} + \frac{34}{\alpha^{4}} - \frac{1}{\alpha} (\frac{1}{2} + \frac{9}{2 \alpha} + \frac{12}{2 \alpha^{2}} + \frac{24}{\alpha^{2}}) \bar{E}^{-2N} = \sum_{n=0}^{\infty} \frac{1}{(n+5)!} (n-1)(n-2)(n-3)(-2 \alpha)^{n+1}
$$
\n
$$
2N C_{4}^{a} = -\frac{1}{2 \alpha} + \frac{15}{\alpha^{2}} - \frac{105}{\alpha^{2}} + \frac{181}{\alpha^{2}} - \frac{215}{\alpha^{2}} + \frac{1}{\alpha} (\frac{1}{2} + \frac{1}{\alpha}
$$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

10.
$$
\int_{-\pi}^{1} (a_1, \Delta)
$$

\n2*N* $\int_{0}^{1} = 4 - \bar{g}^{2N} + 2N \int_{1}^{\infty} \frac{d_2^3}{4^{23}} \bar{L}^{2M} = 4N + 4\alpha^2 \bar{L} Y + \ln(2\alpha) - \frac{2}{2} \bar{J} + 2 \sum_{n=2}^{\infty} \frac{4}{(n+1)(n+1)!} (-2\alpha)^{n+1} (n+1) \sqrt{2N} + 2\alpha \bar{L} \int_{1}^{\infty} \frac{d_2^3}{4^{23}} \bar{L}^{2M} = \frac{4\alpha^2 \bar{L}^2}{4^{23}} \int_{0}^{\infty} \frac{d_2^3}{4^{23}} \bar{L}^{2M} = \frac{4\alpha^2 \bar{L}^2}{4^{23}} \int_{0}^{\infty} \frac{d_1}{2} \ln(2\alpha) - \bar{Y} \int_{1}^{1} - 2\alpha \bar{Y} \Big|_{1}^{\infty}$
\n2*N* $(\frac{1}{3} = -4 + \frac{2}{\alpha} - \frac{2}{2\alpha^2} + \frac{4}{\alpha} \Big(1 + \frac{2}{2\alpha} \Big) \bar{L}^{2M} = -2 \sum_{n=1}^{\infty} \frac{4}{(n+3)!} \pi (1 - 2\alpha)^{n+1}$
\n2*N* $(\frac{1}{3} = -4 + \frac{2}{\alpha} - \frac{1}{2\alpha^2} + \frac{4}{\alpha^2} - \frac{4}{\alpha^2} \Big(1 + \frac{4}{2\alpha} + \frac{4}{\alpha^2} - \frac{1}{\alpha^2} \Big) \bar{L}^{2M} = 2 \sum_{n=1}^{\infty} \frac{4}{(n+3)!} \pi (n-2\alpha)^{n+1}$
\n2*N* $(\frac{1}{3} = -\frac{1}{3\alpha} + \frac{45}{2\alpha} - \frac{45}{1\alpha^2} + \frac{315}{2\alpha} - \frac{4}{\alpha} \Big(1 + \frac{47}{2\alpha} + \frac{27}{2\alpha} + \frac{37}{2\alpha} + \frac{37}{2\$

2
$$
C_{02}^{\beta} = -2\ell \sin (2\ell) + \cos (2\ell) - 4 - (2\ell)^2 \int_1^{\alpha} \frac{d\ell}{2} \cos (2\ell/2) = (2\ell)^2 (\ell + \ln (2\ell) - \frac{3}{2}) - \sum_{k=2}^{\infty} (-\ell)^k \frac{4}{(2\ell)^2 (k+1)} (2\ell)^2
$$

\n2 $C_1^{\beta} = \frac{2\ell}{3} \sin (2\ell) - 4 - \frac{1}{3} \cos (2\ell) + \frac{2}{3\ell} \sin (2\ell) + \frac{1}{3} (2\ell)^3 \int_1^{\infty} \frac{d\ell}{2} \cos (2\ell/2)$
\n $= \frac{1}{3} (2\ell)^3 \left[\frac{5}{6} - \ln (2\ell) - \frac{3}{2} \frac{1}{12} \left(-4 \frac{1}{\ell} \frac{1}{(2\ell)^2 (2\ell + 1)} \right) (2\ell - 1)(2\ell)^{2\ell} \right]$
\n2 $C_{12}^{\beta} = \frac{2\ell}{3} \cos (2\ell) + \frac{1}{3} \sin (2\ell) - \frac{2}{3\ell} \left(4 - \cos (2\ell) \right) - \frac{1}{3} (2\ell)^3 \int_1^{\infty} \frac{d\ell}{2} \sin (2\ell/2)$
\n $= - \frac{2}{3} \pi \ell^2 - 4 \frac{e^2}{\ell^2} (-4 \frac{1}{\ell} \frac{1}{\ell^2 + \ell^2 \ell^2 + \ell^2 \frac{1}{\ell^2 + \ell^2 \ell^2 + \ell^2 \frac{1}{\ell^2}}) \pi (2\ell)^{2\ell + 1}$
\n2 $C_{21}^{\beta} = - \frac{2}{\ell} \left[1 + \frac{1}{2} \cos (2\ell) \right] + \frac{3}{2\ell^2} \sin (2\ell) = 4 \frac{e^2}{\ell^2} (-4 \frac{\ell}{\ell} \frac{1}{\ell^2 + \ell^2 \ell^2 + \ell^2 \frac{1}{\ell^2 + \ell^2 \ell^2 + \ell^2 \frac{1}{\ell^2 + \ell^2 \ell^2}}) \pi (2\ell)^{2\ell + 1} \pi$

2
$$
C_4 = \frac{1}{7}[3\frac{12}{3}+164(2\pi)]-\frac{4}{2}\frac{1}{7}\frac{1}{2}+3+2164(2\pi)]+\frac{35}{7}\frac{1}{
$$

$$
\frac{12. C_{n}^{c}(\alpha_{1}, \lambda)}{2\alpha C_{0}^{c} = 1 - \bar{\lambda}^{2\alpha/\mu_{1}} = -\sum_{n=1}^{\infty} \frac{1}{n!} \left(-\frac{2\alpha}{\mu_{1}}\right)^{n},
$$
\n
$$
2\alpha i C_{1}^{c} = 1 - \frac{\mu_{1}}{\alpha} + \left(1 + \frac{\mu_{1}}{\alpha}\right) \bar{\lambda}^{2\alpha/\mu_{1}} = \sum_{n=2}^{\infty} \frac{1}{(n+1)!} \left(n\cdot1\right) \left(-\frac{2\alpha}{\mu_{1}}\right)^{n},
$$
\n
$$
2\alpha C_{2}^{c} = -1 + 3\frac{\mu_{1}}{\alpha} - 3\left(\frac{\mu_{1}}{\alpha}\right)^{2} + \left(1 + 3\frac{\mu_{1}}{\alpha} + 3\left(\frac{\mu_{1}}{\alpha}\right)^{2}\right) \bar{\lambda}^{2\alpha/\mu_{1}} = \sum_{n=3}^{\infty} \frac{1}{(n+2)!} \left(n\cdot1\right) \left(n-2\right) \left(-\frac{2\alpha}{\mu_{1}}\right)^{n},
$$
\n
$$
2\alpha i C_{3}^{c} = -1 + 6\frac{\mu_{1}}{\alpha} - 15\left(\frac{\mu_{1}}{\alpha}\right)^{3} + 15\left(\frac{\mu_{1}}{\alpha}\right)^{3} - \left(1 + 6\frac{\mu_{1}}{\alpha} + 15\left(\frac{\mu_{1}}{\alpha}\right)^{2} + 15\left(\frac{\mu_{1}}{\alpha}\right)^{3}\right) \bar{\lambda}^{2\alpha/\mu_{1}} = -\sum_{n=3}^{\infty} \frac{1}{(n+3)!} \left(n\cdot1\right) \left(n+3\right) \left(n+3\right) \left(-\frac{2\alpha}{\mu_{1}}\right)^{n},
$$
\n
$$
2\alpha C_{4}^{c} = 1 - 10\frac{\mu_{1}}{\alpha} + 45\left(\frac{\mu_{1}}{\alpha}\right)^{2} - 105\left(\frac{\mu_{1}}{\alpha}\right)^{3} + 105\left(\frac{\mu_{1}}{\alpha}\right)^{4} - \left(1 + 10\frac{\mu_{1}}{\alpha} + 15\left(\frac{\mu_{1}}{\alpha}\right)^{2} + 105\
$$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

 $\frac{1}{2}$

$$
2\alpha i C_{s}^{c} = 4-45\frac{\mu_{1}}{64}+405(\frac{\mu_{1}}{64})^{2}-420(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}-945(\frac{\mu_{1}}{64})^{2}+14+15(\frac{\mu_{1}}{64})+105(\frac{\mu_{1}}{64})+100(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+945(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+125(\frac{\mu_{1}}{64})^{2}+12570(\frac{\mu_{1}}{64})^{2}+12570(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}{64})^{2}+12575(\frac{\mu_{1}}
$$

$$
2C_{44}^5 = \sin(\frac{27}{74}) + 10\frac{\mu_1}{7}\left(1 + \cos(\frac{27}{74})\right) - 45\left(\frac{\mu_1}{7}\right)^2 \sin(\frac{27}{74}) - 405\left(\frac{\mu_1}{7}\right)^2 \left(1 + \cos(\frac{27}{74})\right) + 405\left(\frac{\mu_1}{7}\right)^4 \sin(\frac{27}{74})
$$

= $4\sum_{n=2}^\infty (-1)^n \frac{4}{(2n+5)!} n(2n+1)(2n+3) (\frac{27}{74})^{2n+1}$

$$
\mathcal{L}C_{42}^{c} = \cos\left(\frac{2\eta}{\mu_{4}}\right) - 4 - 40\frac{\mu_{4}}{\eta}\sin\left(\frac{2\eta}{\mu_{4}}\right) + 45\left(\frac{\mu_{4}}{\eta}\right)^{2}\left(-\cos\left(\frac{2\eta}{\mu_{4}}\right)\right) + 405\left(\frac{\mu_{4}}{\eta}\right)^{3}\sin\left(\frac{2\eta}{\mu_{4}}\right) - 405\left(\frac{\mu_{4}}{\eta}\right)^{4}\left(-\cos\left(\frac{2\eta}{\mu_{4}}\right)\right)
$$

= $4\sum_{n=3}^{\infty} (-4)^{n} \frac{1}{(2n+1)!} (2n+1)(n+1)(2n+3)(n+2)\left(\frac{2\eta}{\mu_{4}}\right)^{2}n$

$$
2C_{54}^{c} = -4-\cos\left(\frac{2\pi}{\mu_{4}}\right)+15\frac{\mu_{4}}{T}\sin\left(\frac{2\pi}{\mu_{4}}\right)+105\left(\frac{\mu_{4}}{T}\right)^{2}(\frac{1}{2}+\cos\left(\frac{2\pi}{\mu_{4}}\right)-420\left(\frac{\mu_{4}}{T}\right)^{2}\sin\left(\frac{2\pi}{\mu_{4}}\right)-445\left(\frac{\mu_{4}}{T}\right)^{T}(\frac{1}{2}+\cos\left(\frac{2\pi}{\mu_{4}}\right)-\frac{1}{2}\sin\left(\frac{2\pi}{\
$$

 $\bar{\gamma}$

 $\hat{\mathcal{A}}$

2C₃₂^c = sin(
$$
\frac{2\pi}{14}
$$
)-15⁴4 $\sqrt{1}$ -cos($\frac{2\pi}{14}$)]-105($\frac{4\pi}{14}$) $\sqrt{3}$ ^d +120($\frac{2\pi}{14}$) $\sqrt{1}$ -cos($\frac{2\pi}{14}$) $\sqrt{1}$
\n-145($\frac{4\pi}{14}$) $\sqrt{1}$ -cos($\frac{2\pi}{14}$)] $\sqrt{1}$ = 8 $\sum_{n=3}^{\infty}$ (-1) $\frac{n}{(2n+1)}$ (12 n 110 n 110 n 100 n 100 n 2)($\frac{2\pi}{14}$) $\sqrt{2}$ π ³
\n2C₄^c = - λ in ($\frac{2\pi}{14}$)-24 $\frac{4}{1}$ 1+cos($\frac{2\pi}{14}$))1+210($\frac{4\pi}{14}$)+1210($\frac{4\pi}{14}$)+1210($\frac{4\pi}{14}$) π
\n-10375($\frac{4\pi}{14}$) π ²1+100 π ($\frac{2\pi}{14}$) π ²1+100($\frac{2\pi}{14}$) π ²1+100 π ($\frac{2\pi}{14}$) π ²1+100

- a) $\left[\right.5 \rightarrow 1.5$ indicates that the expression is the same as shown just before except for replacing ξ by ℓ - ξ .
- b) $\{n \to 2n-1\}$ or $\{n \to 2n\}$ in the series expansion of G_{m1} or G_{m2} (F_{m1}) or F_{m2}) shows that the expression is the same as shown in braces of the series expansion of G_m (see Section 4) [F_m (see Section 6)] e_2 cept for replacing n by 2n-1 or 2n.
- c) For $\mu < 0$, $F_m(\alpha_1, \xi, \mu, \lambda) = (-1)^n F_m(\alpha_1, 1 \xi, -\mu, \lambda)$.

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2. JNMETD

 \blacksquare \mathfrak{g}_2 \mathbf{r}

3.1 Calculation of the pole (SP or/and SSPP) or/and the residue (RES) of the J-th group in RESCAL

Contract Avenue

 $-68 -$

 $\sim 10^{-10}$

4. FLUXCA

Yes, $MMM=3$ $NSTAT1 > 0$ $MMMM=1$ **ENTER** No $\operatorname{TT}_\mathfrak{m}^=\mathfrak{X}/\mathfrak{V}_\mathfrak{f}$ or $\mathfrak{f}/\mathfrak{V}_\mathfrak{f}$ **NSTATY** NOS space points, $\chi_{\text{ex}} = \chi/a$ or γ/R $=1$ Yes. $JC=1$ NOT time points, $T_{\rm m}$ NSPH=0 NOM angle points, $ANGL_m = \mu$ No $JOD=1$, $III=1$ ${\bf J}\!=\!\!{\bf N}{\bf K}{\bf K}$ $=2$ $T_m = SCAL \star T_m$ **NSTATY** AA= α_T $=1$ $X_m = (1 + r/R)2$ No NSPH=0 **Yes** $JOD=2$, $III=1$ NQ, NQQQ $=2$ **NSTATY** $I = JC$ $JC = J$ Calculation of the total number of leakage neutrons, total flux or/an angular flux for the J^{+th} group (see Appendix 2, \S 4.1) Yes Yes, No $\mathbf{I} \text{=} \mathbf{I} \text{+} \mathbf{I} \leq \mathbf{J}$ NSTATY=2.AND.III<IHL $III = III + 1$ No $=1$ $=2$ **JOD** No, NSTATY=1.AND.NSPH=1 NPRINT Yes ∌ Yes ïΩ No. $X_m = r/R$ NSPH=0 WRITE J $JOD=1$, $J = J + 1$ $III=1$ \leq IGRPP Yes =2 $\sqrt{}$ No **NSTATY** ${\tt TFLUX}$ WRITE X and intermediate re-**RETURN** sults for the flux $=1$ No $NSTAT1 > 0$ Yes RES_{m} = WRITE the mean time t and variance σ^2 by calling VARIAC [see Eqs. (41) and (42)] total flux at X_m

4.1 Calculation of the total number of leakage neutrons, total flux or/and angular flux for the J-th group in FLUXCA

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5.1 Calculation of the contribution of the continuous spectrum to the J-th group flux

5.2 Calculation of the contribution of uncollided neutrons to the J-th group flux in INTCAL

 \mathbf{L} $\overline{14}$ \mathbf{r}

6. FNCUT1 (g, t, ξ, \ldots)

Y Next page

6.1 Analytical intgration over y from Y_o to ∞ in FNCUT1 (see the second half of §3.3)

$$
\begin{array}{|c|l|}\n\hline\n\text{FM} = \int_{0}^{T(NOT)} dt \frac{1}{2} \left(t \right), \text{ TMD} = \int_{0}^{T(NOT)} dt t \frac{1}{2} \left(t \right) / PM, \text{ VAD} = \int_{0}^{T(NOT)} dt (t - \text{TMD})^{2} \frac{1}{2} \left(t \right) / PM, \text{ where } \frac{1}{2} \left(t \right) = \text{FFLUX}, \text{TFLUX or FNNOL}(t) \\
\hline\n\hline\n\text{TFLCW}_{m} = \int_{0}^{T} dt' \exp[-TCONK(W_{m} - TO - t')^{2}] \frac{1}{2} \left(t' \right) \text{ [see Eq. (49)]}\n\hline\n\end{array}
$$
\n
$$
\begin{array}{|c|l|}\n\hline\n\text{Addition of the contribution of uncollided neutrons (UNCOPAEEX)}\n\hline\n\text{to the flux due to a pulse source TFL: For NSPHO and } r > 0, \text{ TFLUP-TF1+Eq. (550),\n\end{array}
$$
\n
$$
\begin{array}{|c|l|}\n\hline\n\text{For NSPH} = 0 \text{ and } \mu_{1} > 0, \text{ TFLUP-TF1+Eq. (55b) when KKK = 3 and x=0, or KKK = 5}\n\hline\n\text{For NSPH} = 0 \text{ and } \mu_{1} = 0, \text{ TFLUP-TF1+Eq. (53b) when KKK = 3 and x=0, or KKK = 5}\n\hline\n\text{W(NO)}\n\end{array}
$$
\n
$$
\begin{array}{|c|c|c|}\n\hline\n\text{W(NO)}\n\hline\n\text{TMP} = \int_{W(1)}^{W(NO)} dt t \frac{1}{\phi}(t), \text{ TMAX} = \oint_{W(1)} \text{MOL} = \int_{W(1)}^{W(NOP)} dt (t - \text{TMP})^{2} \frac{1}{\phi}(t) / PMP, \text{ with } \frac{1}{\phi}(t) \
$$

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1. STATIONARY PROBLEM FOR A SPHERE TO EVALUATE TIME-CONSTANT, KA AND CRITICAL RADIUS, AND THE FLUX DISTRIBUTION BY THE USE OF A 1 ENERGY-GROUP MODEL AND THE j_{7} APPROXIMATION

Appendix 3. Input Data for Four Sample Problems 2. STATIONARY PROBLEM FOR A SLAB (WITH UP-SCATTERING OF NEUTRONS) TO OBTAIN 7TH GROUP ANGULAR FLUX, TOTAL FLUX AND TOTAL NUMBER OF LEAKAGE NEUTRONS DUE TO A POINT ISOTROPIC BUUNDARY SOURCE BY THE USE OF A 7-GROUP MODEL AND THE j_7 APPROXIMATION (ALSO THE 1ST AND 2ND TIME MOMENTS OF THE FLUXES DUE TO S(t)-SOURCE AND THE FUNDAMENTAL DECAY CONSTANT ARE CALCULATED)

3. TIME-DEPENDENT PROBLEM FOR A SPHERE FOR EVALUATING THE TIME-DEPENDENT TOTAL FLUX DUE TO THE INCIDENCE OF A SIT)-SOURCE AT THE CENTRE, BY THE USE OF A 1-GROUP MODEL AND THE \dot{ds} APPROXIMATION (USING PREVIOUSLY OBTAINED PUNCHED CARDS FOR THE POLES AND RESIDUES)

 \mathbf{I} $\overline{28}$ \mathbf{r}

4. TIME-DEPENDENT PROBLEM FOR A SLAB TO OBTAIN THE TIME-DEPENDENT ANGULAR FLUX, TOTAL FLUX AND THE TOTAL NUMBER OF LEAKAGE NEUTRONS FROM THE SLAB WITH A MONODIRECTIONAL BOUNDARY SOURCE ($M₁=1$) OF THE TIME BEHAVIOUR DESCRIBED BY A RECTANGULAR PULSE, BY THE USE OF A 1-GROUP MODEL AND THE j_5 APPROXIMATION (ALSO THE FLUXES DUE TO THE S(t)-SOURCE AND THE FIRST 3 TIME MOMENTS ARE CALCULATED AND COMPARED WITH THE STATIONARY VALUES)

 \mathbf{I} \mathbf{g} \bullet

 \bar{z}

Table I Locations of the first elements of Real*8 (or.Real*4) arrays stored in the floating COMMON and their dimensions

to be continued

Table I (continued)

 $\sim 10^6$

 $\label{eq:2.1} \frac{1}{2} \sum_{i=1}^n \frac{1}{2} \sum_{j=1}^n \frac{$

 $\frac{1}{2}$

 $\mathcal{L}^{\text{max}}_{\text{max}}$, where $\mathcal{L}^{\text{max}}_{\text{max}}$

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $\frac{1}{2}$

Table II Computed integers for specifying the array dimensions [JHL = (IIO+1)/2, NNNN = NNN+1, IGRPP= JNKK+NNN and NOSMN= NOS*NOM* *NNNNJ

(To be continued)

00 \mathbf{L}

 \mathbf{r}

Table II (Continued)

(To be continued)

Table II (Continued)

	NSTATY=1		NSTATY=2	
	$NSPH=1$	NSPH=0	$NSPH=1$	$NSPH=O$
IA(39)		\mathbf{o}	$\bar{\mathcal{A}}$	•8 (for $JJJ=2,3$ or 4)
IA(40)		O		$^{\bullet}$ IIO+1
IA(41)		\circ		• 16 (for $IIOZ5$)
IA(42)		0		\bullet 3
IA(43)		Ω		• 4 $\big\setminus$ (JJJJ=2,3 or 4)
IA(44)		0		\bullet 2
IA(45)		O		\bullet 7 (for JJJJ= 3 or 4)
IA(47)		o		\bullet 6 (for IIO \geq 5)
IA(49)	\mathbf{o}	IGRP (for NSTAT1=1)	\mathbf{o}	IGRP (for NSTAT=1)
IA(50)		\mathbf{o}		• IIO+1 (for IGRPP>1)
IA(51)		O		\bullet IIO+1 (for IIO \geq 5)
IA(53)		O		• 8 (for $II0=7$)
	$($ JHL+1)*JHL, $)$	(JHL+1)*JHL(NSTAT1=0),	$2\star$ (JHL) ²	• $2\star(JHL)^2$ (NSTAT1=0),
IA(54)	Max NOS	$Max(2\star (JHL)^2, 6\star JHL)$ (for NSTAT1=1)		• Max $(2\star(\text{JHL})^2,6\star\text{JHL})$ (for NSTAT1=1)
IA(55)	\bullet IGRP			
IA(56)	o	ı	0	\bullet JHL
IA(57)	o	IGRP	O	\bullet IGRP
IA(59)	o	\mathbf{o}	o	\bullet IGRPP-1
IA(60)	$\mathbf O$	o	\mathbf{o}	\bullet 4*N+1 (if IGRPP>1)
IA(62)	\circ	\bullet NOM	\mathbf{o}	\bullet NOM
IA(63)	ı		\bullet NOT	
IA(64)	o		\bullet NOT	
IA(65)	\mathbf{o}		\bullet NOS	
IA(67)	0	NOS*NNNN (JJJJ=2 or 4 and NSTAT1=0),	\mathbf{O}	3*NOS*NNNN(JJJJ=2 or 4 and NSTAT1=1)
		3*NOS*NNNN(JJJJ=2 or 4 and NSTAT1=1)		
IA(68)	0	0	NFLUXK (if TPINT>0)	
IA(69)	JHL*IGRP	JHL (for NUPSAT=0), JHL*IGRP+2 $for NUPSAT=1)$	JHL	
IA(94)	0	2 (for NSTAT1=1)	0	2 (for NSTAT1=1)

• Only if LLL=0 (or NFLUXR, NFLUXS or NFLUXK>0 for NSTATY=1 and NSPH=J)

φ Dimension for the integer array II at the location IA(140)

 \triangle Dimension for the stationary total flux which is included in IA(8)

find poles Σ_1 V₁S_j in the j_7 appr. for the g-th group [c(g+g)=1 & Σ_9 Q=15]

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\alpha} \frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{\alpha} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\$ $\mathcal{L}(\mathcal{L})$ and $\mathcal{L}(\mathcal{L})$. In the $\mathcal{L}(\mathcal{L})$ $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$

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Alfred Nobel

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