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# Experimental Hamiltonian identification for controlled two-level systems

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We present a strategy to empirically determine the internal and control Hamiltonians for an unknown two-level system (black box) subject to various (piecewise constant) control fields when direct readout by measurement is limited to a single, fixed observable.

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Accurate determination of the dynamics of physical systems and their response to external (control) fields is crucial for many applications, especially quantum information processing (QIP). Quantum process tomography (QPT) is a general procedure to identify the unitary (or completely positive) processes acting on a system by experimentally determining the expectation values of a complete set of observables [1].

However, QPT is only a partial solution in many cases. One problem is the assumption that one can experimentally determine the expectation values of a complete set of observables, or at least perform arbitrary single qubit measurements for a register of  $n$  qubits. However, most QIP proposals rely on a single readout process, i.e. measurement in one basis. For example, qubits encoded in internal electronic states of trapped ions [2] or neutral atoms [3] are read out by quantum jump detection via a cycling transition [4]. In solid-state systems based on Cooper-pair boxes [5], Josephson junctions [6], or electrons in double-well potentials [7], final readout is via charge localization using single electron transistors [8] or similar devices. Finally, solid state architectures based on electron or nuclear spin qubits [9], are expected to be limited to  $\sigma_z$  measurements via spin-charge transfer.

Generally, one assumes that a single projective measurement per qubit is sufficient since arbitrary one-qubit measurements can be realized by performing a local unitary transformation before measuring to achieve a change of basis. However, implementing these basis changes requires accurate knowledge of the dynamics of each individual qubit and its response to control fields in the first place. Yet, in particular for solid-state qubits [5, 6, 7, 9, 10], it is difficult to *predict* the actual dynamics of a qubit precisely based on computer models and theory alone, since they may be sensitive to fabrication variance and even vary from one qubit to the next as a result. We address this problem of system identification with a single fixed measurement basis and present a general strategy to identify the internal and control Hamiltonians for a qubit subject a number of piecewise

constant controls using a single, fixed readout process. We can then bootstrap this process to implement QPT.

Although the technique may be adapted to dissipative systems, in this paper we assume Hamiltonian evolution for the purpose of identifying the dynamics relevant for the implementation of local unitary operations, i.e. decoherence times much greater than the gate operation times, which is crucial for systems of interest in QIP. The system evolution is thus governed by a unitary operator  $U(t, t_0)$ , via  $\rho(t) = U(t, t_0)\rho(t_0)U(t, t_0)^\dagger$ , where  $\rho(t)$  is the system density operator, and  $U(t, t_0)$  satisfies the Schrödinger equation

$$i\hbar \frac{d}{dt}U(t, t_0) = H[\mathbf{f}(t)]U(t, t_0), \quad (1)$$

where  $H$  is the Hamiltonian of the system. The case of interest is when  $H$  depends on external fields  $\{f_m\}$ , which we can control. Assuming the fields are sufficiently weak and act independently,  $H$  has the form

$$H[\mathbf{f}(t)] = H_0 + \sum_{m=1}^M f_m(t)H_m, \quad (2)$$

where  $H_0$  is the free evolution Hamiltonian and  $H_m$  for  $m > 0$  describes the interaction of the system with field  $f_m$ . Each  $H_m$  can in turn be expanded in terms of the Lie algebra generators; for a two-level system, the Pauli matrices  $\sigma_j$  for  $j \in \{x, y, z\}$ :

$$2H_m = d_{m0}I + d_{mx}\sigma_x + d_{my}\sigma_y + d_{mz}\sigma_z. \quad (3)$$

Thus we need to determine the real constants  $d_{mx}$ ,  $d_{my}$  and  $d_{mz}$  for  $m = 0, 1, \dots, M$  (the  $d_{m0}$  can be ignored since they result only in an unobservable global phase factor).

Geometrically, we can represent the state of the system by its Bloch vector  $\mathbf{s}(t) = (s_x, s_y, s_z)^T$  where  $s_j = \text{Tr}[\sigma_j \rho(t)]$ . If the system satisfies Eqs.(1-3), its Bloch vector evolves as

$$\dot{\mathbf{s}}(t) = \left( R_0 + \sum_{m=0}^M f_m(t)R_m \right) \mathbf{s}(t) \quad (4)$$

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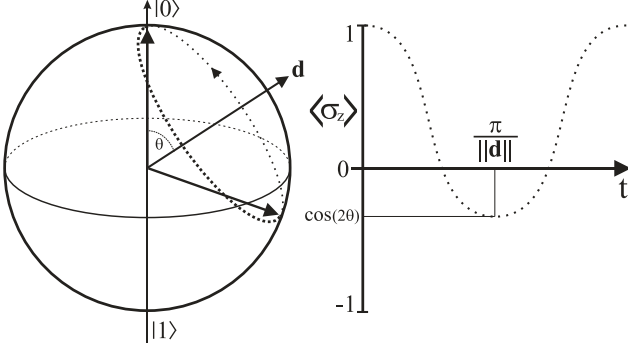


FIG. 1: Rotation about axis  $\mathbf{d}$  and observable  $z(\alpha_t)$ . The expectation value of the measurement operator will oscillate sinusoidally, amplitude and frequency are directly related to the declination and length of the vector representing the applied Hamiltonian.

where  $R_m$  are the real anti-symmetric rotation generators

$$R_m = \begin{pmatrix} 0 & d_{mz} & -d_{my} \\ -d_{mz} & 0 & d_{mx} \\ d_{my} & -d_{mx} & 0 \end{pmatrix} \quad (5)$$

and  $R = R_0 + \sum_{m=1}^M f_m R_m$  generates a rotation about

$$\mathbf{d} = \mathbf{d}_0 + \sum_{m=1}^M f_m \mathbf{d}_m \quad (6)$$

with  $\mathbf{d}_m = (d_{mx}, d_{my}, d_{mz})^T$  for  $m = 0, 1, \dots, M$ . If  $f_m(t)$  vary in time then so does  $\mathbf{d}$ . If they are piecewise constant, having fixed values  $f_m$  for  $t_0 \leq t \leq t_1$ , then  $\mathbf{s}(t)$  for  $t \in [t_0, t_1]$  rotates about the fixed axis  $\mathbf{d}$ , where  $\|\mathbf{d}\|$  is the rotation frequency, and the unit vector  $\hat{\mathbf{d}} = \frac{1}{\|\mathbf{d}\|} \mathbf{d}$  specifies the rotation axis. This allows us to give an explicit formula for the trajectory of  $\mathbf{s}(t)$  with  $\mathbf{s}(0) = \mathbf{s}_0$ :

$$\begin{aligned} \mathbf{s}(\alpha_t) &= \mathbf{s}_0 \cos \alpha_t + \hat{\mathbf{d}}(\mathbf{s}_0 \cdot \hat{\mathbf{d}})(1 - \cos \alpha_t) + (\mathbf{s}_0 \times \hat{\mathbf{d}}) \sin \alpha_t \\ &= [I \cos \alpha_t + A(1 - \cos \alpha_t) + B \sin \alpha_t] \mathbf{s}_0. \end{aligned} \quad (7)$$

where the rotation angle is  $\alpha_t = \alpha(t) = \|\mathbf{d}\|(t - t_0)$  and

$$A = \frac{1}{2} \begin{pmatrix} 2 \sin^2 \theta \cos^2 \phi & \sin^2 \theta \sin(2\phi) & \sin(2\theta) \cos \phi \\ \sin^2 \theta \sin(2\phi) & 2 \sin^2 \theta \sin^2 \phi & \sin(2\theta) \sin \phi \\ \sin(2\theta) \cos \phi & \sin(2\theta) \sin \phi & 2 \cos^2 \theta \end{pmatrix},$$

$$B = \begin{pmatrix} 0 & \cos \theta & -\sin \theta \sin \phi \\ -\cos \theta & 0 & \sin \theta \cos \phi \\ \sin \theta \sin \phi & -\sin \theta \cos \phi & 0 \end{pmatrix},$$

and the unit vector  $\hat{\mathbf{d}}$  is expressed in spherical coordinates,  $\hat{\mathbf{d}} = (\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta)^T$ .

Without loss of generality we shall assume that we can initialize the system in the state  $\mathbf{s}_0 = |0\rangle = (0, 0, 1)^T$  with respect to the measurement basis, and that we can experimentally determine the value of the  $z$ -component of the

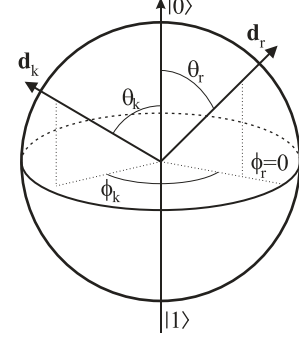


FIG. 2: Bloch sphere and arrangement of rotation axes. We can define the relative angular displacement of the vectors  $\mathbf{d}_k$  representing applied Hamiltonians with respect to a reference vector  $\mathbf{d}_r$  ( $\neq z$ -axis).

Bloch vector  $z = \langle \sigma_z \rangle$  by repeated measurements. Inserting the expressions for  $A$  and  $B$  into Eq.(7), a rotation about the axis  $\mathbf{d}$  by the angle  $\alpha_t = \|\mathbf{d}\|(t - t_0)$  transforms the initial state  $\mathbf{s}_0$  into  $\mathbf{s}(\alpha_t)$  whose  $z$ -component is

$$z(\alpha_t) = \cos(\alpha_t) \sin^2 \theta + \cos^2 \theta. \quad (8)$$

$z(\alpha_t)$  is constant exactly if  $\theta = 0$ . Otherwise, it oscillates and with minimum  $z_{min} = \cos^2 \theta - \sin^2 \theta = \cos(2\theta)$  for  $\cos(\alpha_t) = -1$  or  $\alpha_t = (2n + 1)\pi$  (for some integer  $n$ ). Hence, if  $\theta \neq 0$  then we can experimentally find  $\|\mathbf{d}\|$  and  $\theta$  by determining the  $t_{min} = \frac{\pi}{\|\mathbf{d}\|}$  and  $z_{min}$  (Fig. 1).

For a single rotation it is sufficient to determine  $\|\mathbf{d}\|$  and  $\theta$  and set  $\phi = 0$ . For multiple rotations about different axes  $\mathbf{d}_k$ , however, we must also determine the relative azimuthal angles  $\phi_k = \phi'_k - \phi'_r$  with respect to a fixed reference axis  $\mathbf{d}_r$  (Fig. 2). The reference axis should have a vertical tilt angle  $\theta_r \in [\frac{\pi}{4}, \frac{3\pi}{4}]$  and we shall focus on this case in this paper [11]. Having determined  $\|\mathbf{d}\|$  and  $\theta$  of the axes, and chosen a suitable reference axis  $\mathbf{d}_r$ , we can initialize the system in the state  $\mathbf{s}_1 = (\cos \beta, \sin \beta, 0)^T$  by rotating  $\mathbf{s}_0$  about the axis  $\mathbf{d}_r$  by  $\alpha_r = \cos^{-1} \left( \frac{\cos(2\theta_r) + 1}{\cos(2\theta_r) - 1} \right)$ , where  $\beta = \tan^{-1}(-\sqrt{-2 \cos(2\theta_r)} \sec \theta_r)$ . Rotating  $\mathbf{s}_1$  by various angles  $\alpha$  about the axis  $\mathbf{d}_k$  then gives  $z(\alpha) = C(1 - \cos \alpha) + D \sin \alpha$  with  $C = \frac{1}{2} \sin(2\theta_k) \cos(\phi_k - \beta)$  and  $D = \sin \theta_k \sin(\phi_k - \beta)$ , or equivalently

$$z(\alpha) = \gamma \sin(\alpha + \delta) - \gamma \sin \delta, \quad (9)$$

where  $C = \gamma \sin \delta$  and  $D = \gamma \cos \delta$ . Hence, we can obtain  $\phi$  from experimental data for  $z(\alpha)$  by finding  $\delta$  and  $\gamma$ .

To determine the evolution of the system subject to the several external fields we choose several field strengths  $f_m^{(\ell)}$  ( $\ell = 1, \dots, L$ ) for each control  $f_m$  ( $m = 1, \dots, M$ ) and compute the rotation axes

$$\mathbf{d}_{0+m}^{(\ell)} = \mathbf{d}_0 + f_m^{(\ell)} \mathbf{d}_m \quad (10)$$

by finding  $\theta_{0+m}^{(\ell)}$  and  $\|\mathbf{d}_{0+m}^{(\ell)}\|$  for all control settings, choosing a reference axis, and determining all the relative azimuthal angles  $\phi_{0+m}^{(\ell)}$  using the strategy outlined

above. Then we plot the  $x$ ,  $y$  and  $z$ -components of  $\mathbf{d}_{0+m}^{(\ell)}$  for  $\ell = 1, 2, \dots, L$  versus the field strengths  $f_m^{(\ell)}$  for each field, and fit a straight line to each set of data points. The vertical axis intercepts of the lines then give the  $x$ ,  $y$ , and  $z$ -component of  $\mathbf{d}_0$ , and their slopes determine the  $x$ ,  $y$ , and  $z$ -component of  $\mathbf{d}_m$ .

To evaluate our strategy and find the best ways to extract the information from noisy data we use computer simulations. We choose various sets of Hamiltonians, use the proposed strategy to identify them and compare these results with the actual values. Experiments are simulated by computing individual  $\sigma_z$  measurements of  $\mathbf{s}(t)$  according to Eq.(7), generating  $N$  pseudo-random numbers  $r_n \in [0, 1]$ , where  $N$  is the number of times the experiment is repeated, and taking the result of the  $n^{\text{th}}$  measurement  $M_n$  to be 1 if  $r_n < (1+z)/2$  and 0 otherwise. To account for measurement errors we introduce a symmetric error probability  $\eta \in [0, 1]$  indicating the frequency of erroneous measurement results, i.e., registering 1 when we should have measured 0, and vice versa. This is achieved by choosing another  $N$  random numbers  $e_n \in [0, 1]$ , and changing  $M_n$  to  $1 - M_n$  whenever  $e_n < \eta$ . Finally, we set  $\langle \sigma_z \rangle = -1 + \frac{2}{N} \sum_{n=1}^N M_n$ .

We illustrate our Hamiltonian identification strategy in detail with a specific test system:

$$\begin{aligned} 2H_0 &= 0.2\sigma_x + 0.1\sigma_z, & 2H_1 &= \sigma_x + 0.9\sigma_y + 0.1\sigma_z, \\ 2H_2 &= 0.2\sigma_x + 0.9\sigma_z. \end{aligned} \quad (11)$$

This Hamiltonian may arise, for instance, for a charge qubit [7] consisting of two quantum dots sharing a single electron, and two voltage gates  $B$  and  $S$ , intended to enable us to change the potential barrier between them and induce asymmetries in the double well potential. The measurement basis states  $|0\rangle$  and  $|1\rangle$  are the localized ground states of the charge in either of the two dots, and projective measurements onto them can be performed via a single electron transistor placed next to one of the dots.  $H_0$  indicates some tunneling between the dots when no control voltages are applied to the gates and a slight potential asymmetry, which might be due to imperfect placement of the donor impurities.  $H_1$  induces tunneling between the dots as desired but also induces a slight potential asymmetry, which might occur if the electrode was placed slightly off-center.  $H_2$  produces the desired energy level shift but also increases tunneling slightly.

The first step towards identifying the Hamiltonians  $H_0$ ,  $H_1$  and  $H_2$  involves finding the rotation frequencies  $\|\mathbf{d}_0\|$  as well as  $\|\mathbf{d}_{0+1}^{(\ell)}\|$ ,  $\|\mathbf{d}_{0+2}^{(\ell)}\|$  and the angles  $\theta_0$ ,  $\theta_{0+1}^{(\ell)}$ ,  $\theta_{0+2}^{(\ell)}$  for several gate voltages  $f_1^{(\ell)}$  and  $f_2^{(\ell)}$ . We do this by applying each gate voltage for various periods of time  $t_j$  and finding  $z(t_j) = \langle \sigma_z(t_j) \rangle$  (Fig. 3). An estimate of the rotation frequency  $\omega$  is obtained by taking the discrete Fourier transform (DFT) of  $z(t_j) - \frac{1}{J} \sum_{j=1}^J z(t_j)$  and identifying its maximum. We then estimate the time  $t_* = \frac{\pi}{\omega}$  when  $z(\alpha_t)$  is expected to assume its first minimum, acquire (circa 150) additional data points for  $t \in [0.85t_*, 1.15t_*]$  and determine the minimum  $z_{min}$  by

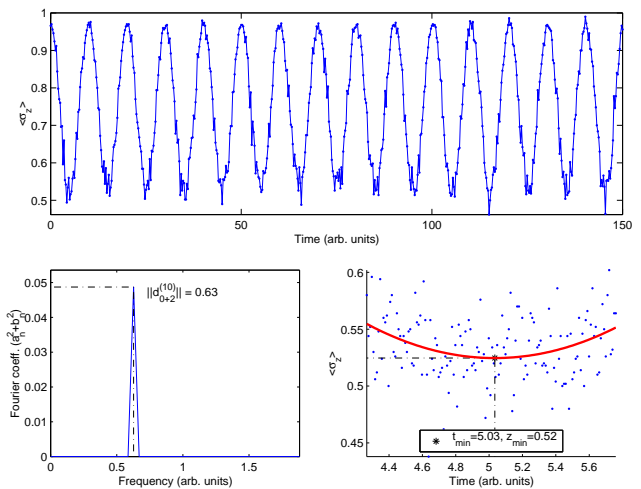


FIG. 3: Identification of  $\|\mathbf{d}\|$  and  $\theta$  for  $\mathbf{d} = \mathbf{d}_0 + f_2^{(10)} \mathbf{d}_2$ . Shown is simulated data for  $\mathbf{d}_{0+2}^{(10)}$  for  $f_2^{(10)} = 0.5$ . The top graph is used to estimate the rotation frequency using the DFT, the bottom left plot shows the Fourier transform, and the bottom right plot the magnification of the region of interest as well as the parabola that provides the best least-squares fit to the data.

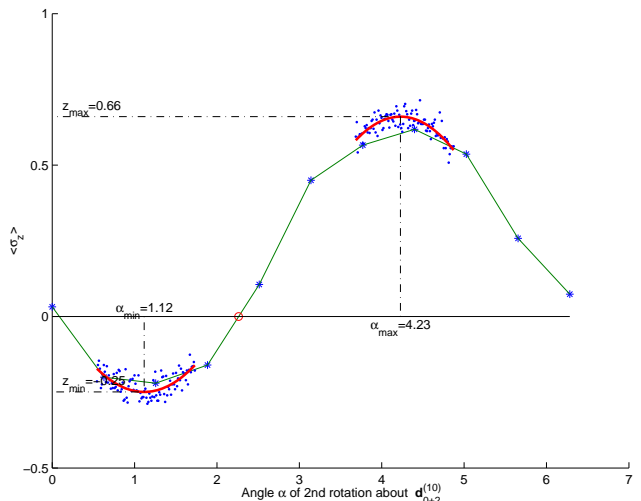


FIG. 4: Identification of  $\phi$  for  $\mathbf{d} = \mathbf{d}_0 + f_2^{(10)} \mathbf{d}_2$ . The points  $*$ , are a coarse sampling of the curve from which the first axis crossing can be estimated (red circle). This then gives estimates of the turning points  $\alpha_{min}^{est}$  and  $\alpha_{max}^{est}$  which can be refined by re-sampling (dots) in their vicinity and fitting a parabola (red curves). From this we determine the vertices  $(\alpha_{min}, z_{min})$  and  $(\alpha_{max}, z_{max})$ .

fitting a *parabola* to these data points;  $\theta = \frac{1}{2} \cos^{-1}(z_{min})$ . This proved to be considerably more accurate for noisy data than fitting a function of the form Eq.(8) to the data points and reading off the frequency and minimum from this curve directly.

Next we determine the angles  $\phi_{0+m}^{(\ell)}$  relative to the reference axis, chosen to be  $\mathbf{d}_0$  here. In all of the

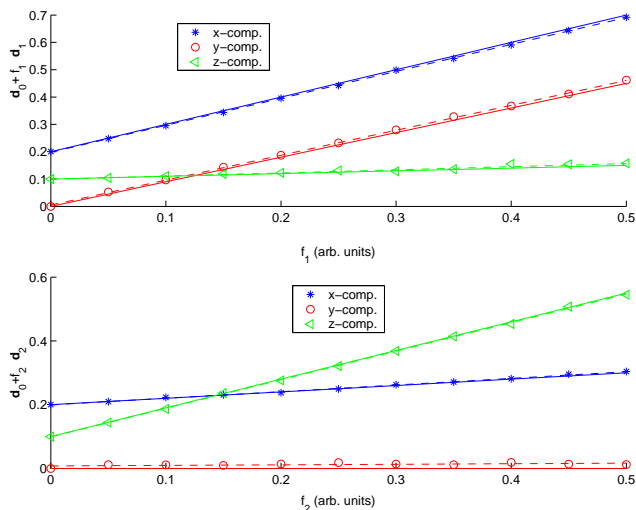


FIG. 5: Identification of the components of  $\mathbf{d}_0$  and  $\mathbf{d}_m$ . Typical simulated experimental run for the system defined by Eq.(11) and the estimated components of  $\mathbf{d}$  for different field settings. Shown are the best straight line fit (dashed lines) and the actual values (solid line). Note the excellent agreement between the actual values and the best fit obtained. A typical run of the program yielded:  $\mathbf{d}_0 = (0.1987, 0.0064, 0.0992)^T$ ,  $\mathbf{d}_1 = (0.9859, 0.9122, 0.1149)^T$ ,  $\mathbf{d}_2 = (0.2081, 0.0170, 0.8957)^T$ , i.e., the Hilbert-Schmidt norm errors  $\|\mathbf{d}_m^{est} - \mathbf{d}_m^{act}\|$  were less than 3% (0.0066, 0.0238 and 0.0193 for  $m = 0, 1, 2$  respectively).

following experiments the system is initialized in state  $\mathbf{s}_1 = (\cos \beta, \sin \beta, 0)^T$  by applying a suitable rotation

about the reference axis. In our case the state  $\mathbf{s}_0$  is rotated to  $\mathbf{s}_1$  by letting it evolve freely for  $\approx 8.1379$  time units yielding  $\beta \approx -1.0489$ . We then apply each field  $f_m^{(\ell)}$  for various times to achieve rotations by various angles  $\alpha$  (Fig. 4). This yields the parameters  $\gamma = \frac{1}{2}(z_{max} - z_{min})$  and  $\delta = \pi - \frac{1}{2}(\alpha_{min} + \alpha_{max})$  in Eq.(9) from which we can obtain  $\phi$ , e.g., by setting  $D = \gamma \cos \delta$  and  $\phi = -\beta - \sin^{-1}(D/\sin(\theta))$  where  $\theta$  is the vertical tilt angle of the rotation axis determined in the previous step.

Finally, having determined all the relevant parameters of the rotation axes, we convert the data to Cartesian coordinates, and plot the  $x$ ,  $y$  and  $z$  components of  $\mathbf{d}_{0+m}^{(\ell)}$  for each field  $f_m$  as a function of  $f_m^{(\ell)}$  (Fig. 5). From the straight line fitting, we can then estimate the Hamiltonians.

In conclusion, we have presented a stepwise procedure to determine the dynamical response of a Hamiltonian 2-level quantum system to control fields when we only have access to measurement in a single fixed basis. This overcomes a weakness in the assumptions of QPT and thus enables us to bootstrap the procedure to estimate parameters for systems consisting of arrays of qubits. Numerical results indicate that the procedure is fairly robust for Hamiltonians of physical interest. Extensions of the procedure higher-dimensional or dissipative systems may be possible.

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- [11] If all axes have  $\theta \notin [\frac{\pi}{4}, \frac{3\pi}{4}]$  then all we can do is map the initial state  $\mathbf{s}_0$  to the state closest to the equatorial plane by a  $\frac{\pi}{2}$  rotation about the most horizontal axis and proceed in a similar manner as above. However, the resulting expressions will be more complicated, and the accuracy of  $\phi$  will diminish when  $\mathbf{s}_1$  is close to  $\mathbf{s}_0$ , but such a system would be a poor candidate for a qubit.