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RATCHET LIMITS FOR A CRACK IN A WELDED PIPE SUBJECTED TO A CYCLIC TEMPERATURE LOAD AND A CONSTANT MECHANICAL LOAD

Tianbai Li

Department of Mechanical Engineering
University of Strathclyde
Glasgow, Scotland, UK

Haofeng Chen

Department of Mechanical Engineering
University of Strathclyde
Glasgow, Scotland, UK

Weihang Chen

Department of Mechanical Engineering
University of Strathclyde
Glasgow, Scotland, UK

James Ure

Department of Mechanical Engineering
University of Strathclyde
Glasgow, Scotland, UK

ABSTRACT

This paper presents the ratchet limit analysis of a pipe with a symmetric crack in a mismatched weld by using the extended Linear Matching Method (LMM). Two loading conditions are considered: i) a cyclic temperature load and a constant internal pressure; and ii) a cyclic temperature load and a constant axial tension. Individual effects of i) the geometry of the Weld Metal (WM), ii) the size of the crack, iii) the location of the crack and iv) the yield stress of WM on the ratchet limits, maximum temperature ranges to avoid ratchetting and limit loads are investigated. Influence functions of the yield stress of WM on the maximum temperature ranges and limit loads are generated. The results confirm the applicability of the extended LMM to the cracked welded pipe.

Keywords: crack, ratchet limit, limit load, welded pipe, maximum temperature range

INTRODUCTION

The circumferential butt welded pipes are widely used in nuclear power plants and usually subjected to complex varying thermal and mechanical loads [1-2]. Under such loads, the pipes may fail either from the accumulated plastic deformations during the increasing load cycles or from the reverse plastic deformations. The former is known as ratchetting, which leads structures to incremental collapse; the latter is named plastic shakedown, which gives rise to local low cycle fatigue. For a pipe with a crack in the weld, the elastic stress singularity at the crack tip violates the elastic shakedown condition, hence the non-existence of a finite shakedown limit. Therefore the ability to calculate the ratchet limit of the cracked pipe is particularly desirable. The obtained ratchet limit may then be used to calculate the ratchetting reference stress to predict material deformation and rupture [3].

Ratchetting analysis of loaded structures has been investigated by many researchers in past decades [2-20]. The complexity of ratchetting means that analytical solutions are rare, and thus incremental Finite Element Analysis (FEA) is widely used. Incremental FEA can only show if ratchetting occurs, and therefore many calculations are required to generate the Bree-like diagram [4].

In order to overcome the difficulties of the step-by-step elasto-plastic FEA, a number of direct methods based upon the Koiter's [5] kinematic and/or the Melan's [6] static theorems have been developed including: i) the nonlinear superposition method [7]; ii) mathematical programming methods [8-9]; iii) the Generalized Local Stress Strain (GLOSS) r-node method [10]; iv) the Elastic Compensation Method (ECM) [11, 12]; and v) the Linear Matching Method (LMM) [13-20]. The LMM is distinguished from other simplified methods by ensuring that equilibrium and compatibility are satisfied at each stage. The LMM has been shown to give accurate shakedown analysis to complex geometries and load histories [13, 14]. The LMM has also been extended to evaluate ratchet limits [15-18] for defect-free components subjected to cyclic load conditions from two-load extremes [15-17] to multi-load extremes [18]. However, the application of the latest LMM ratchet limit method [18] to structures with a discontinuity in the geometry and material has not yet been undertaken.

In this paper, the method is used to address ratchet limits of a circumferentially welded pipe with a circumferential crack in the weld subjected to a varying temperature load and a constant i) internal pressure or ii) axial tension. The remainder of this paper comprises five parts. In section 2, the LMM ratchet limit method is briefly described. Section 3 presents the pipe geometry and material properties. This is followed by the FE model of the pipe. The ratchet limit analysis is presented in Section 5. In this section, the effects of strength of the WM,

location and size of the crack, width of the WM, and finally the coefficient of thermal expansion of the WM on the ratchet limit are discussed.

LINEAR MATCHING METHOD

Consider a body of volume, V , with a surface area S . The body is subjected to varying mechanical loads, $P^v(x_i, t)$, over a fraction of the surface area, S_p , and varying thermal loads $\theta^v(x_i, t)$. A zero displacement rate condition is applied over the remainder of the surface area, S_u such that $\dot{u}_i = 0$. Over a time cycle $0 \leq t \leq \Delta t$, these loads are decomposed into constant and cyclic components such that

$$P^v(x_i, t) = \lambda \bar{P}(x_i) + P(x_i, t), \quad \theta^v(x_i, t) = \lambda \bar{\theta}(x_i) + \theta(x_i, t) \quad (1)$$

where λ is a load multiplier. \bar{P} and $\bar{\theta}$ are the constant mechanical and thermal load distribution respectively. P and θ are the cyclic mechanical and thermal load respectively. The corresponding linear elastic stress history $\hat{\sigma}_{ij}$ is then given as

$$\hat{\sigma}_{ij}(x_k, t) = \lambda \bar{\sigma}_{ij}(x_k) + \hat{\sigma}_{ij}^p(x_k, t) + \hat{\sigma}_{ij}^\theta(x_k, t) \quad (2)$$

where $\bar{\sigma}_{ij}(x_k)$ is the elastic stress due to \bar{P} and $\bar{\theta}$. $\hat{\sigma}_{ij}^p(x_k, t)$ and $\hat{\sigma}_{ij}^\theta(x_k, t)$ are the elastic stress histories corresponding to $P(x_k, t)$ and $\theta(x_k, t)$, respectively. The cyclic stress history $\sigma_{ij}(x_k, t)$ over the time cycle is given by

$$\sigma_{ij}(x_k, t) = \hat{\sigma}_{ij}(x_k, t) + \bar{\rho}_{ij}(x_k) + \rho_{ij}^r(x_k, t) \quad (3)$$

where $\bar{\rho}_{ij}(x_k)$ is a constant residual stress and corresponds to $\lambda \bar{\sigma}_{ij}(x_k)$. $\rho_{ij}^r(x_k, t)$ is a changing residual stress corresponding to $\hat{\sigma}_{ij}^p$ and $\hat{\sigma}_{ij}^\theta$ during a cycle and satisfies:

$$\rho_{ij}^r(x_k, 0) = \rho_{ij}^r(x_k, \Delta t) = \bar{\rho}_{ij}^0(x_k) \quad (4)$$

where $\bar{\rho}_{ij}^0(x_k)$ is the constant element of ρ_{ij}^r

Consider an energy function

$$I(\dot{\epsilon}_{ij}^c, \lambda) = \int_V \int_0^{\Delta t} (\sigma_{ij}^c - \sigma_{ij}) \dot{\epsilon}_{ij}^c dt dV \quad (5)$$

where $\dot{\epsilon}_{ij}^c$ is a kinematically admissible strain rate. σ_{ij}^c represents a stress at yield corresponding to $\dot{\epsilon}_{ij}^c$.

The determination of the ratchet limit is implemented by a two-stage nonlinear minimisation procedure: i) a changing residual stress ρ_{ij}^r is computed by an incremental minimisation of the energy function I and satisfies Eq. (4), with the application of the cyclic load; and ii) a global minimisation of the upper bound shakedown theorem is performed to evaluate the additional constant load, which leads the load state to the ratchet limit.

Consider a body subjected to a cyclic load involving multi-load extremes. It is assumed that plastic strains only occur at

the extremes corresponding to the time instants t_k ($k=1, \dots, K$). The instants t_k represents a sequence of time points in the cyclic load history such that $\Delta \epsilon_{ij}^c = \sum_{k=1}^K \Delta \epsilon_{ij}^p(t_k)$, where $\Delta \epsilon_{ij}^p(t_k)$ is the plastic strain increment at t_k . Hence we have the function

$$I(\dot{\epsilon}_{ij}^c, \lambda) = \sum_{k=1}^K I_k = \int_V \sum_{k=1}^K (\sigma_{ij}^k - \hat{\sigma}_{ij}(t_k) - \rho_{ij}^r(t_k)) \Delta \epsilon_{ij}^k dV \quad (6)$$

where

$$\rho_{ij}^r(t_k) = \bar{\rho}_{ij}^0 + \sum_{m=1}^k \Delta \rho_{ij}(t_m) \quad (7)$$

$$\Delta \epsilon_{ij}^T(t_k) = C_{ijmn}(\bar{\mu}_k) \Delta \rho_{mn}(t_k) + \Delta \epsilon_{ij}^p(t_k) \quad (8)$$

$$\Delta \epsilon_{ij}^p(t_k) = (\hat{\sigma}_{ij}^p(t_k) + \hat{\sigma}_{ij}^\theta(t_k) + \rho_{ij}^r(t_k))' / (2\bar{\mu}_k) \quad (9)$$

where $\Delta \epsilon_{ij}^T$ is compatible and $\Delta \rho_{ij}$ satisfies equilibrium. An upper 'dash' refers to deviatoric components. $\bar{\mu}_k$ is an iterative shear modulus and determined by the linear matching condition [15,16]

$$\bar{\mu}_k = \frac{2\sigma_y}{3\bar{\epsilon}(\Delta \epsilon_{ij}^p(t_k))} \quad (10)$$

where σ_y is the yield stress and $\bar{\epsilon}(\Delta \epsilon_{ij}^p(t_k))$ is the effective plastic strain increment.

The changing residual stress is computed by the minimisation of the I via the iterations among Eqs. (7-10). We denote $\Delta \rho_{ij}^n(t_k)$ as an evaluated changing residual stress at k^{th} load instance after n^{th} iteration, where $k=1, \dots, K$ and $n=1, \dots, N$. At n^{th} iteration, $\Delta \rho_{ij}^n(t_k)$ is computed for all K load instances. The converged solution occurs if the summation of all changing residual stresses at N^{th} iteration vanishes, i.e. $\sum_{k=1}^K \Delta \rho_{ij}^N(t_k) = 0$. Hence the constant residual stress $\bar{\rho}_{ij}^0$ can also be determined by

$$\bar{\rho}_{ij}^0 = \sum_{k=1}^K \sum_{n=1}^N \Delta \rho_{ij}^n(t_k) \quad (11)$$

The ratchet limit can be determined by the minimisation of the upper bound shakedown theorem [15], with the elastic solution augmented by the changing residual stress $\rho_{ij}^r(t_k)$. The theorem gives

$$\int_V \sum_{k=1}^K \sigma_{ij}(t_k) \Delta \epsilon_{ij}(t_k) dV = \int_V \sum_{k=1}^K \sigma_{ij}^c(t_k) \Delta \epsilon_{ij}(t_k) dV \quad (12)$$

Where σ_{ij} is given in Eq. (3). For the application of the von Mises yield criterion, we have

$$\int_V \sum_{k=1}^K \sigma_{ij}^c(t_k) \Delta \epsilon_{ij}(t_k) dV = \int_V \sum_{k=1}^K \sigma_y \bar{\epsilon}(\Delta \epsilon_{ij}(t_k)) dV \quad (13)$$

Thus, an upper bound ratchet limit multiplier is given by solving Eq. (12) with consideration of Eqs. (2), (3) and (13).

$$\lambda = \frac{\int \sum_{k=1}^K \sigma_y \bar{\varepsilon}(\Delta \varepsilon_{ij}(t_k)) dV - \int \sum_{k=1}^K (\sigma_{ij}^p(t_k) + \sigma_{ij}^0(t_k) + \rho_{ij}^r(t_k)) \Delta \varepsilon_{ij}(t_k) dV}{\int \sum_{k=1}^K \bar{\sigma}_{ij} \Delta \varepsilon_{ij}(t_k) dV} \quad (14)$$

where $\bar{\varepsilon}(\Delta \varepsilon_{ij}(t_k)) = \sqrt{\frac{2}{3} \Delta \varepsilon_{ij} \Delta \varepsilon_{ij}}$ is the effective plastic strain increment at t_k . This multiplier λ gives the capacity of the body subjected to cyclic loads P and θ to withstand constant loads \bar{P} and $\bar{\theta}$ before ratchetting occurs. On the basis of this formulation, the LMM produces a sequence of monotonically reducing upper bounds, which converges to the least upper bound ratchet limit for the chosen class of displacement fields. In the following sections, a symmetric cracked welded pipe is analysed in detail using the proposed method.

PIPE GEOMETRY AND MATERIAL PROPERTIES

Consider a circumferentially welded pipe, with a circumferential symmetric inner/central/outer surface crack in the weld (Fig. 1). The inhomogeneous pipe includes two different material domains - Parent Material (PM) and Weld Metal (WM). Each material is isotropic, elastic perfectly plastic and satisfies the von Mises yield criterion. The initial residual stress in the pipe due to the welding process is considered to be ignored due to post weld heat treatment. The length L , inner radius R_i , wall thickness w , crack length a and weld width H are shown in Fig. 1 and Table 1. The material properties including the yield stress σ_y , Young's modulus E , Poisson's ratio ν , conductivity k and coefficient of thermal expansion α adopted in this paper for the baseline calculation are given in Table 2, where WM and PM have same values of E , k and ν .

LOADING CONDITIONS AND FINITE ELEMENT MODELLING

In this analysis, the pipe is subjected to two loading conditions: i) $\Delta\theta + p$, a cyclic temperature $\Delta\theta$ and a constant internal pressure p (with closed end conditions) (Fig. 2a) or (ii) $\Delta\theta + T$, a cyclic temperature $\Delta\theta$ and a constant axial tension T (Fig. 2b).

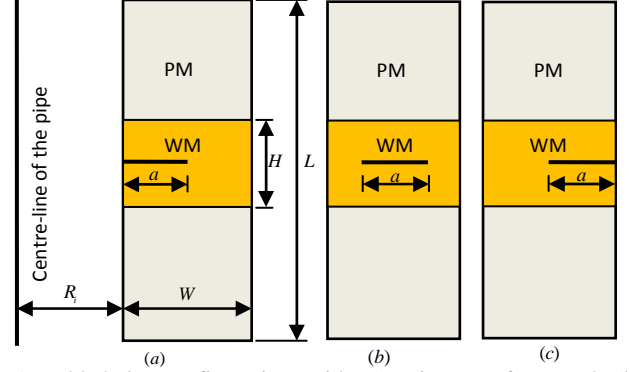


Fig.1 Welded pipe configurations with (a) an inner surface crack, (b) a central crack and (c) an outer surface crack

Table 1 Shape parameters of a welded pipe with a symmetric crack

$w(mm)$	L	R_i	a	H
40	$5w$	$7.5w$	$0.5w$	$0.5w$

Table 2 Material properties of a welded pipe

σ_y^{PM} (MPa)	σ_y^{WM} (MPa)	E (GPa)	α^{PM} ($10^{-5} \cdot C^{-1}$)	α^{WM} ($10^{-5} \cdot C^{-1}$)	k ($Wm^{-1} \cdot C^{-1}$)	ν
230	460	200	1.9	1.8	15	0.3

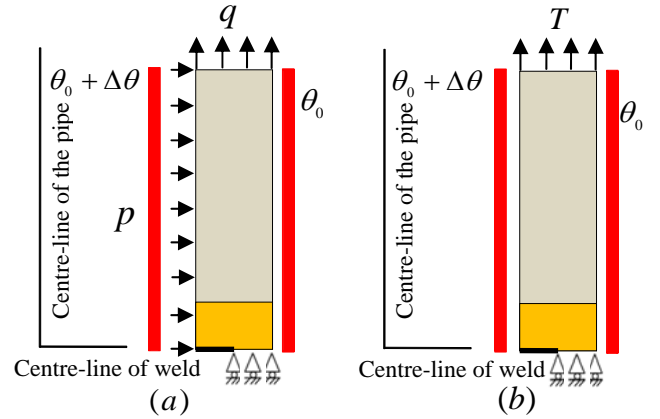


Fig. 2 Thermal and mechanical loads and boundary conditions of the cracked welded pipe: (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Fig. 2 shows the two-dimensional axisymmetric model, with a symmetry condition applied in the axial direction. The end of the pipe is constrained to remain in-plane, simulating the expansion of a long pipe. The closed end condition of the pipe is simulated by applying an equivalent axial tension $q = pR_i^2 / (2R_i w + w^2)$.

It is assumed that the ambient air temperature outside of the pipe is θ_0 , and the operating temperature of the fluid contained within the pipe fluctuates between ambient and a higher value, $\theta_0 + \Delta\theta$ (Fig. 3). Due to the dissimilar material in the pipe, the applied cyclic thermal loading may be constructed by three thermal stress extremes: i) a thermal stress field produced by a linear temperature gradient through the wall

thickness; ii) a thermal stress field due to the different thermal expansion coefficients between the PM and WM occurring at the highest uniform temperature; and iii) a zero thermal stress field simulating a uniform ambient temperature. If θ_0 is zero, the maximum effective elastic thermal stresses for these three extremes can be determined by the maximum temperature difference $\Delta\theta$. Hence the thermal load history can be characterised by $\Delta\theta$.

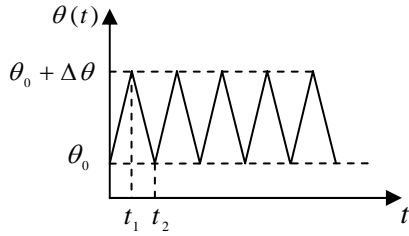


Fig. 3 The operating temperature history of the fluid contained within the welded pipe

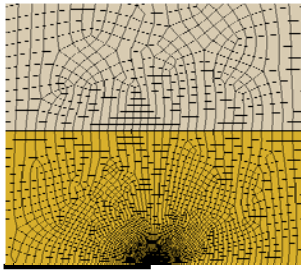


Fig. 4 Finite element mesh of the welded pipe with an inner crack $a = 0.5w$

In this paper, the Abaqus type CAX8R 8-node biquadratic axisymmetric quadrilateral elements with reduced integration are used for structural analysis and DCAX8 8-node quadratic axisymmetric heat transfer quadrilateral elements with reduced integration scheme are used for the heat transfer analysis (Fig. 4).

RESULTS AND DISCUSSIONS

In this paper, a mismatch rate r in the yield stress between the WM and the PM is introduced

$$r = \sigma_y^{WM} / \sigma_y^{PM} \quad (15)$$

Effect of crack location and yield stress of weld metal σ_y^{WM} on the ratchet limits

In this subsection, pipes with inner/central/outer surface cracks in the weld are considered. The values of yield stress of the WM σ_y^{WM} used are 115, 230 and 460MPa, respectively, and σ_y^{PM} is held constant at 230MPa (i.e. $r = 0.5, 1$ and 2).

Fig. 5 show the converged ratchet limit interaction curves of cracked welded pipes with $r = 0.5, 1, 2$ and a pure PM pipe ($r = 1$) without a crack, subjected to $\Delta\theta + p$ (Fig. 5a) or

$\Delta\theta + T$ (Fig. 5b). In this diagram, a normalised internal pressure p/p_{PM} (or axial tension T/T_{PM}) and a temperature range $\Delta\theta$ are chosen as an abscissa and an ordinate respectively. p_{PM} and T_{PM} are the limit internal pressure and limit axial tension of the pure PM pipe without a crack, respectively.

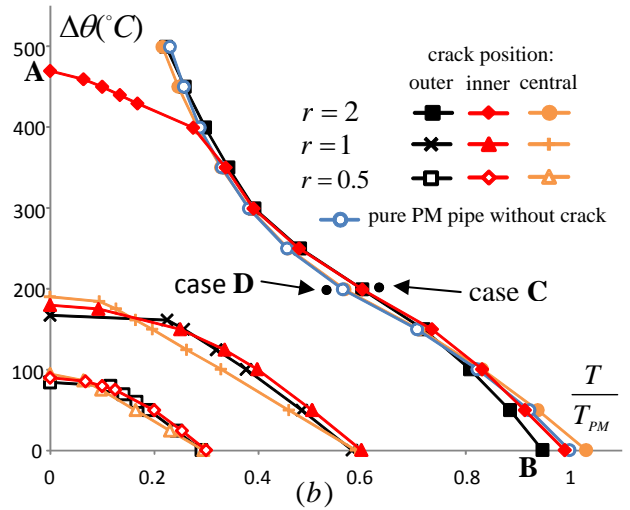
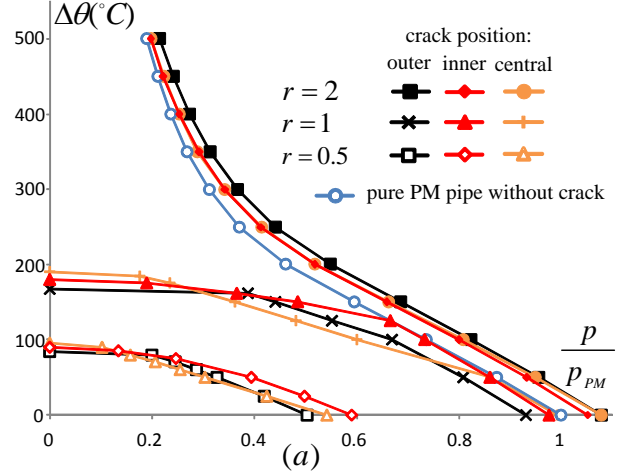


Fig. 5 Ratchet limit interaction curves of the welded pipe with the different r and the different crack locations. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$.

In the Fig. 5, it can be seen that only the ratchet limit boundaries of the pure PM pipe without a crack and the welded pipe ($r = 2$) with an inner/central/outer crack (excluding an inner crack in Fig. 5b) exhibit typical Bree-like diagrams. The ratchet limit boundaries in other cases intersects the y-axis. For example, the point A in Fig. 5b represents a maximum temperature range to avoid ratchetting for an applied cyclic thermal load and a particular form of a potential mechanical load. The point B denotes the limit load for the applied mechanical load.

Fig. 5 shows that for all r , the three different locations of the symmetric crack have little effect on the ratchet limit boundaries, except for the case of $r = 2$ and $\Delta\theta \geq 400^\circ\text{C}$ in

Fig. 5b, where the inner surface crack produces much lower ratchet limits than the central crack and outer surface crack.

It can be observed that the ratchet limit boundaries including the limit internal pressure / axial tension and the maximum temperature range to avoid ratchetting reduce with the decreasing r . It is also noted that for the case of $\Delta\theta + p$, when $r \geq 1$ and $\Delta\theta < 100^\circ\text{C}$ (Fig. 5a), the change in r has little effect on the ratchet limit boundary due to the plastic collapse occurring in the PM.

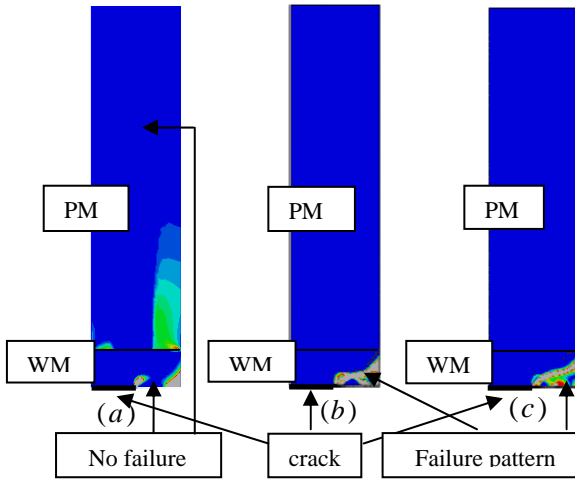


Fig. 6 The non-ratchetting/ratchetting mechanisms for the inner cracked welded pipe (Fig. 5a) subjected to a cyclic temperature range $\Delta\theta$ and a constant internal pressure ($p/p_{PM} = 0.15$), when (a) $r = 2$, $\Delta\theta = 500^\circ\text{C}$ (no ratchetting mechanism), (b) $r = 1$, $\Delta\theta = 185^\circ\text{C}$ (ratchetting mechanism in WM) and (c) $r = 0.5$, $\Delta\theta = 88^\circ\text{C}$ (ratchetting mechanism in WM)

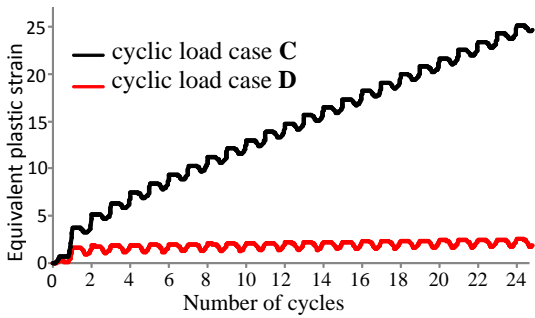


Fig. 7 Abaqus verification of the ratchet limit for the cyclic temperature of $\Delta\theta = 200^\circ\text{C}$ using detailed step by step analysis

Three typical failure modes are given in Fig. 6 which shows the non-ratchetting/ratchetting mechanisms for the inner cracked welded pipe (Fig. 5a), subjected to a cyclic temperature range $\Delta\theta$ and a constant internal pressure ($p/p_{PM} = 0.15$). When $r = 2$ and $\Delta\theta = 500^\circ\text{C}$ (Fig. 6a), no ratchetting mechanism occurs and the pipe still has a capacity to resist an additional internal pressure. When $r = 1$, $\Delta\theta = 88^\circ\text{C}$ (Fig. 6b) or $r = 0.5$, $\Delta\theta = 185^\circ\text{C}$ (Fig. 6c), a ratchetting mechanism occurs

at the weld material, and the pipe will experience incremental plastic collapse after a limited number of cycles.

It is particularly interesting that for the case of $r = 2$, after the pipe is subjected to the cyclic temperature range $\Delta\theta \geq 470^\circ\text{C}$, the pipe with an inner surface crack can withstand an internal pressure but cannot withstand an axial tension. This is because the thermal stress in the plastic zone could be reduced by the superposition of the mechanical stress caused by an internal pressure, but not by an axial tension.

Consider two load cases C and D (Fig. 5b), which are just outside and inside the predicted ratchet limit domain at temperature range $\Delta\theta = 200^\circ\text{C}$. The plastic strain histories (Fig. 7) calculated by the ABAQUS step-by-step analysis verified the accuracy of LMM ratchet limit boundary by showing that i) under the load case C, the maximum equivalent plastic strain increases with load cycles to give a strong ratchetting mechanism; and ii) under the load case D, the maximum equivalent plastic strain ceases to increase after 20 load cycles, giving a non-ratchetting mechanism.

Effect of crack size

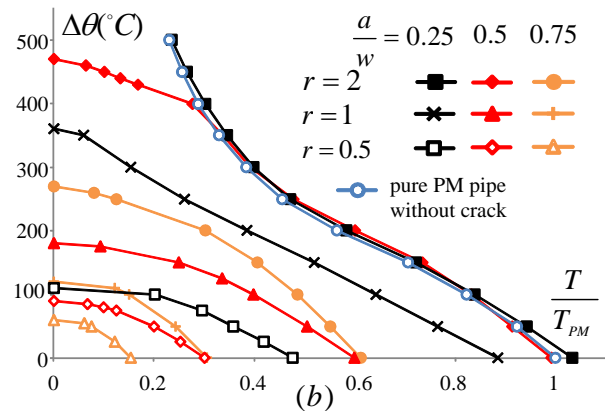
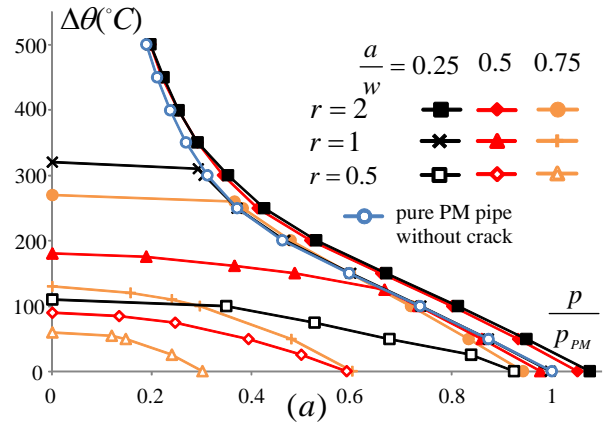


Fig. 8 Ratchet limit interaction curves of the welded pipe with the different crack sizes a and the different r . The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Three symmetric crack lengths are considered: $a = 0.25w$, $0.5w$ and $0.75w$. For each crack length, three yield stresses are considered as per the previous sections, $r = 0.5, 1$ and 2 .

Fig. 8 gives ratchet limit interaction curves of the pipe subjected to $\Delta\theta + p$ (Fig. 8a) or $\Delta\theta + T$ (Fig. 8b). It shows that i) when $r \leq 1$ (excluding the case of $r = 1$ and $a \leq 0.5w$ in Fig. 8a), the ratchet limit boundaries including the limit internal pressure / axial tension and the maximum temperature range to avoid ratchetting reduces with the increasing a ; ii) when $r = 2$ and $\Delta\theta < 300^\circ\text{C}$ (except for the case of $a = 0.75w$ in Fig. 8b), the change in a has little effect on the ratchet limit diagrams. The reason of the reduction in the limit load with the increasing a is due to the plastic collapse occurring in the WM. A larger crack length in the WM causes a smaller effective load carrying area, which leads to a lower limit internal pressure / axial tension.

Effect of weld width

In order to study the effect of weld width, values of $H = 0.25w$, $0.5w$ and w were chosen. Similarly, all limits for three different width are computed based on three different yield stresses of WM: $r = 0.5$, 1 and 2 .

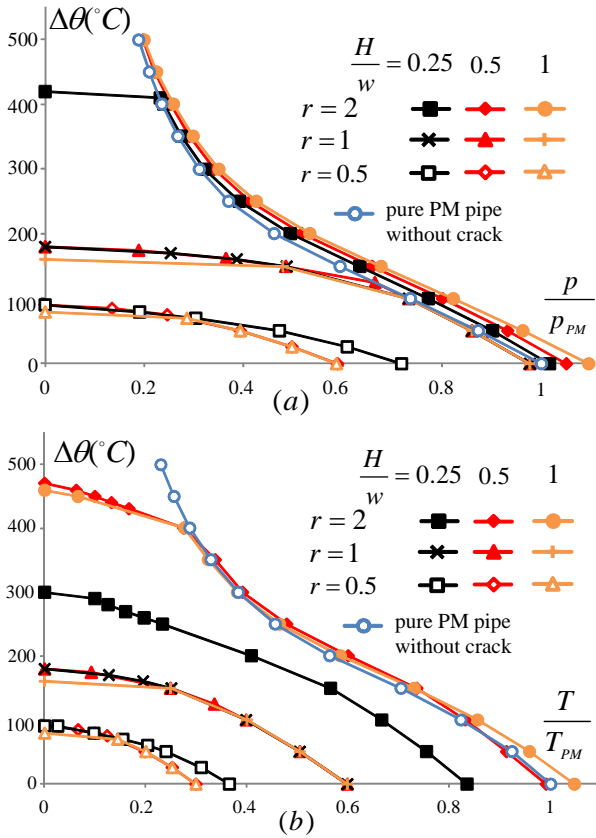


Fig. 9 Ratchet limit interaction curves of the pipe with the different thickness H of the WM and the different r . The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Fig. 9 gives ratchet limit interaction curves of the pipe subjected to $\Delta\theta + p$ (Fig. 9a) or $\Delta\theta + T$ (Fig. 9b). It shows that for all r (excluding the cases of $r = 2$ and $H = 0.25w$), the change in H has little effect on the ratchet limit diagrams.

Fig. 9b shows that when $r = 2$, the width $H = 0.25w$ gives a smaller limit tension than that of $H = 0.5w$ and w . This is because the pipe failure zone is a 45 degree inclined strip which is from the crack tip to the side boundary. Hence, the smaller width H of WM means that this 45 degree slip line must travel further through weaker parent material, which causes the lower limit tension of the pipe. The width $H = 0.25w$ also gives a smaller maximum temperature range to avoid ratchetting than that of $H = 0.5w$ and w due to the aforementioned reason.

Effect of coefficient of thermal expansion of weld metal α^{WM}

Three values of $\alpha^{WM} / \alpha^{PM} = 0.5, 0.95$ and 2 were chosen. The thermal expansion of the PM material was given a fixed value of $\alpha^{PM} = 1.8 \times 10^{-5} \text{ }^\circ\text{C}^{-1}$. All limits for the three different α^{WM} are computed based on three different yield stresses of WM: $r = 0.5, 1$ and 2 .

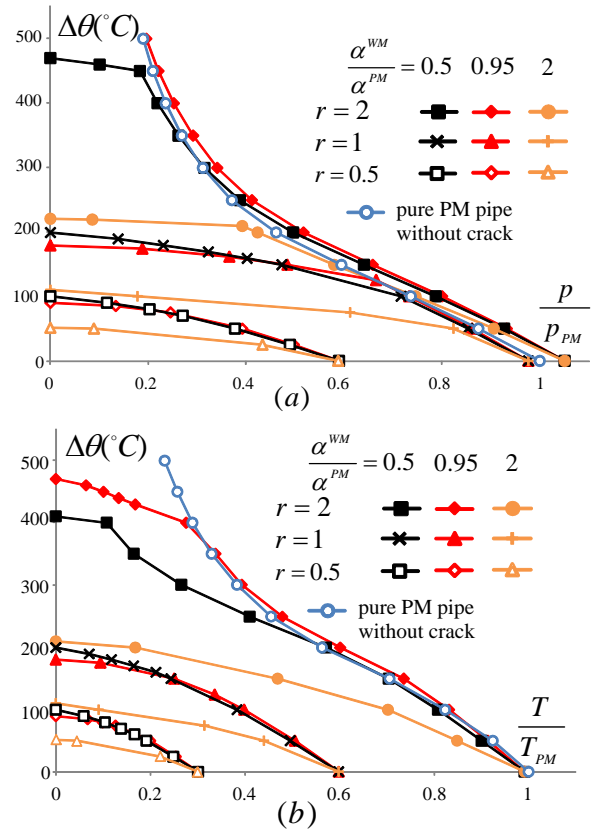


Fig. 10 Ratchet limit interaction curves of the pipe with the different thermal expansion coefficients of the WM α^{WM} and the different r , where $\alpha^{PM} = 1.9 (\times 10^{-5} \text{ }^\circ\text{C}^{-1})$. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Fig. 10 gives ratchet limit interaction curves of the pipe subjected to $\Delta\theta + p$ (Fig. 10a) or $\Delta\theta + T$ (Fig. 10b). It shows that for all r , i) the change in α^{WM} has no effect on the limit internal pressure (or limit axial tension) due to the purely mechanical nature of the load; and ii) $\alpha^{WM} / \alpha^{PM} = 2$ gives a

smaller maximum temperature range to avoid ratcheting in comparison with the cases of $\alpha^{WM} / \alpha^{PM} = 0.5$ and 0.95 . This is because a larger difference in thermal expansion coefficients between the PM and the WM leads to a larger field of high thermal stress around the interface between two materials, which may interact with the another high stress field either around the crack tip or in the parent material, thus causing failure at smaller temperature range.

Discussions

In the previous subsections, the results show that five parameters -- the yield stress of WM σ_y^{WM} , the location (inner/central/outer) and length a of the crack, the width w and the thermal expansion coefficient α^{WM} of WM have the different effects on the ratchet limits, maximum temperature ranges to avoid ratcheting, and limit loads. Among these parameters, σ_y^{WM} is the most sensitive parameter to the ratchet limit boundary, and the crack location is the least sensitive one. A further investigation of the effect of these parameters is given in the Fig. 11 and Tables 3-6.

Fig. 11 shows how the yield stress of WM affects the ratchet limit of the pipe with an inner surface crack. It suggests that the higher WM yield strength leads to a larger limit load and a larger maximum temperature range to avoid ratcheting for both loading cases. It is noted that for the case of $\Delta\theta + p$, there is a rapid increase in limit load up to $r = 0.75$, with the increases being small in comparison when $r > 0.75$ (shown in Fig. 11a). When $r > 1.5$, the maximum temperature range to avoid ratcheting steeply rises with the increasing r , shown in Fig. 11b. All trend lines are fit to the data to give the functions, shown in Eqs. (16-19).

For the pipe subjected to $\Delta\theta + p$, we have

$$\frac{p}{p_{PM}} = \begin{cases} 1.21r - 0.018 & 0.5 \leq r \leq 0.8 \\ 0.079r + 0.89 & 0.8 < r \leq 2 \end{cases} \quad (16)$$

$$\Delta\theta^p = \begin{cases} 91.42r^2 + 33.14r + 52 & 0.5 \leq r \leq 1.5 \\ 1000r - 1190 & 1.5 < r \leq 1.54 \\ -0.71r + 1.78 & 1.54 < r \leq 1.55 \\ > 500 & 1.55 < r \leq 2 \end{cases} \quad (17)$$

For the pipe subjected to $\Delta\theta + T$

$$\frac{T}{T_{PM}} = -0.16r^2 + 0.86r - 0.098 \quad 0.5 \leq r \leq 2 \quad (18)$$

$$\Delta\theta^T = 89.52r^2 + 23.33r - 60 \quad 0.5 \leq r \leq 2 \quad (19)$$

where p_{PM} and T_{PM} are the limit internal pressure and limit axial tension of the pure PM pipes without a crack, respectively. $\Delta\theta^p$ or $\Delta\theta^T$ represents the maximum temperature range to avoid ratcheting for the pipe subjected to an applied cyclic thermal load $\Delta\theta$ and a potential internal pressure p or axial tension T , respectively.

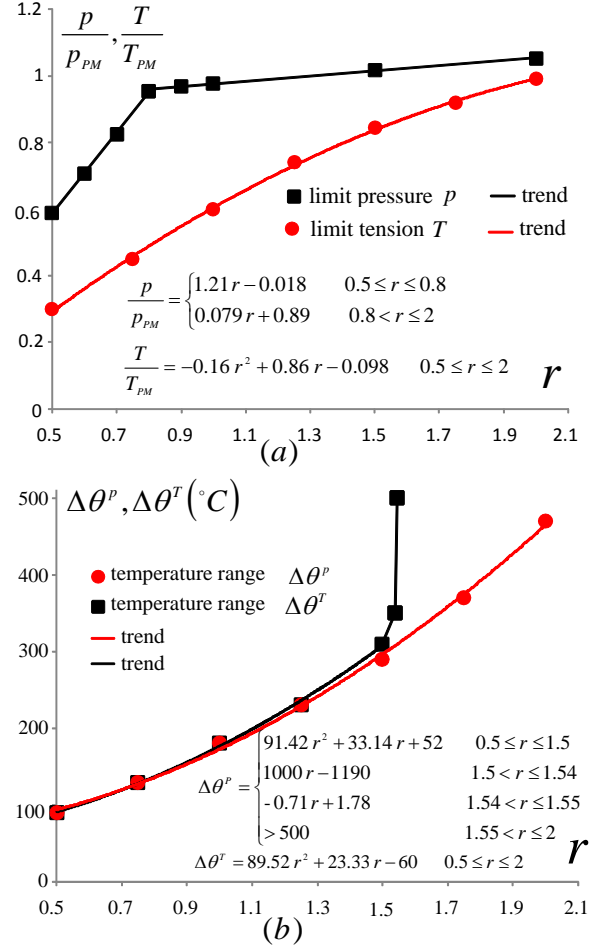


Fig. 11 The effect of the yield stress of WM σ_y^{WM} on (a) the limit loads and (b) the maximum temperature ranges of the pipe under i) $\Delta\theta + p$ or ii) $\Delta\theta + T$

Table 3 Limit load and maximum temperature range of the pipe with the different crack locations and the different r , where $a/w = 0.5$, $H/w = 0.5$ and $\alpha^{WM} / \alpha^{PM} = 0.95$. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Loading condition	crack location	Normalised limit load p/p_{PM} (T/T_{PM})			Maximum temperature range $\Delta\theta^p$ or $\Delta\theta^T$ ($^{\circ}C$)		
		$r = 0.5$	$r = 1$	$r = 2$	$r = 0.5$	$r = 1$	$r = 2$
$\Delta\theta + p$	inner	0.59	0.98	1.05	90	180	-
	outer	0.50	0.93	1.08	84	167	-
	central	0.54	0.99	1.08	95	190	-
$\Delta\theta + T$	inner	0.30	0.60	0.99	90	180	470
	outer	0.29	0.58	0.95	84	167	-
	central	0.29	0.59	1.03	95	190	-

Table 4 Limit load and maximum temperature range of the inner cracked pipe with the different crack length a and the different r , where $H/w = 0.5$ and $\alpha^{WM}/\alpha^{PM} = 0.95$. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Loading condition	crack size a/w	Normalised limit load $p/p_{PM} (T/T_{PM})$			Maximum temperature range $\Delta\theta^p$ or $\Delta\theta^T$ ($^{\circ}C$)		
		$r=0.5$	$r=1$	$r=2$	$r=0.5$	$r=1$	$r=2$
$\Delta\theta + p$	0.25	0.93	1.00	1.08	110	320	-
	0.50	0.59	0.98	1.05	90	180	-
	0.75	0.30	0.60	0.94	60	130	270
$\Delta\theta + T$	0.25	0.48	0.89	1.03	110	360	-
	0.50	0.30	0.60	0.99	90	180	470
	0.75	0.15	0.31	0.61	60	120	270

Table 5 Limit load and maximum temperature range of the inner cracked pipe with the different thickness of the WM H and the different r , where $a/w = 0.5$ and $\alpha^{WM}/\alpha^{PM} = 0.95$. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Loading condition	WM width H/w	Normalised limit load $p/p_{PM} (T/T_{PM})$			Maximum temperature range $\Delta\theta^p$ or $\Delta\theta^T$ ($^{\circ}C$)		
		$r=0.5$	$r=1$	$r=2$	$r=0.5$	$r=1$	$r=2$
$\Delta\theta + p$	0.25	0.72	0.98	1.02	90	180	420
	0.5	0.59	0.98	1.05	90	180	-
	1	0.59	0.98	1.09	80	160	-
$\Delta\theta + T$	0.25	0.37	0.60	0.84	90	180	300
	0.5	0.30	0.60	0.99	90	180	470
	1	0.30	0.60	1.05	80	160	-

Table 6 Limit load and maximum temperature range of the inner cracked pipe with the different α^{WM} and the different r , where $\alpha^{PM} = 1.9 (\times 10^{-5} \text{ }^{\circ}C^{-1})$, $a/w = 0.5$ and $H/w = 0.5$. The pipe is subjected to (a) $\Delta\theta + p$ or (b) $\Delta\theta + T$

Loading condition	α^{WM}/α^{PM}	Normalised limit load $p/p_{PM} (T/T_{PM})$			Maximum temperature range $\Delta\theta^p$ or $\Delta\theta^T$ ($^{\circ}C$)		
		$r=0.5$	$r=1$	$r=2$	$r=0.5$	$r=1$	$r=2$
$\Delta\theta + p$	0.5	0.59	0.98	1.05	100	200	470
	0.95	0.59	0.98	1.05	90	180	-
	2	0.59	0.98	1.05	52	110	220
$\Delta\theta + T$	0.5	0.30	0.60	0.99	100	200	410
	0.95	0.30	0.60	0.99	90	180	470
	2	0.30	0.60	0.99	52	110	210

The obtained results are further summarised in Tables 3-6 which show the effects of the crack location, crack length, weld width and weld thermal expansion coefficient on the limit load and maximum temperature range to avoid ratchetting, respectively. The conclusion is given in next section.

CONCLUSION

The extended Linear Matching Method (LMM) is successfully applied in this study for the ratchet limit analysis of circumferentially welded pipes containing a circumferential crack subjected to a cyclic temperature $\Delta\theta$ and a constant i) internal pressure p or ii) axial tension T . Based on the results obtained in this study, the following conclusions are given: i) When compared with a pure Parent Material (PM) pipe without a crack, the discontinuity in material (due to the Weld Metal (WM)) and in geometry (due to a crack) may lead to a significant change in the ratchet limit boundary including the maximum temperature range to avoid ratchetting and limit load; ii) Among five parameters, variation of the yield stress

σ_y^{WM} of the WM has the largest impact on the ratchet limits. The limit load and the maximum temperature range to avoid ratchetting rise with the increasing σ_y^{WM} . The relationship between them has been formulated; iii) An increase in the symmetric crack length a decreases the maximum temperature range to avoid ratchetting and limit load, but the crack location has the least effect on the ratchet limit out of the parameters considered in this work; iv) The weld width H has little effect on the limits for all r , except for the case of $r=2$ and $H=0.25w$ when the pipe is under axial tension, where the ratchet limit boundary is significantly reduced in comparison with cases of $r=2$ and $H \geq 0.5w$; v) The large difference in the coefficient of thermal expansion between the WM and the PM significantly decreases the maximum temperature ranges to avoid ratchetting, but the limit load is unaffected by any changes in α^{WM}/α^{PM} .

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