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1 **Monitoring degradation mechanisms in PTB7:PC₇₁BM photovoltaic**
2 **cells by means of impedance spectroscopy**

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12
13 **Abstract**

14 We have used impedance spectroscopy technique to monitor degradation mechanisms in
15 organic solar cells based on a blend of PTB7:PC₇₁BM. We have measured the
16 impedance of the cell on a periodical basis for almost four months, and experimental
17 data have been modelled using three different circuits. The evolution of the circuital
18 parameters gives information about the device dynamical mechanisms. We have
19 observed at high voltages a low frequency feature that is more pronounced along days
20 of measurement. This low frequency arc has been associated to charge accumulation
21 that is related to a worsening of charge extraction through the contacts. The
22 simultaneous increase of recombination and low frequency resistances at high voltages
23 (around V_{oc}) results in a decrease of the fill factor and therefore of the efficiency.

24 Keywords: Organic solar cells, impedance spectroscopy, monitoring degradation.

27 1. Introduction

28

29 During the last years, organic photovoltaic (OPV) has become a promising technology
30 in the field of renewable energy [1-3]. Among all types of OPV, bulk heterojunction
31 (BHJ) organic solar cells (OSCs) have become very popular due to the high efficiencies
32 achieved using both small molecules [4] and polymers [5]. OSCs offer advantages over
33 inorganic devices (both, silicon or III-V) such as lightweight, thinness, potential
34 flexibility, transparency, low cost and low temperature fabrication techniques such as
35 spin coating, spray coating, inkjet printing, etc. However, there are still some issues,
36 such as device stability and life time that must be solved before OPV turns into a real
37 alternative to inorganic devices [6].

38 Regarding materials, poly (3-hexylthiophene) P3HT and fullerene [6,6]-phenyl-C60
39 butyric acid methyl ester PC₆₀BM blend has been the most studied and understood
40 system, and it has achieved efficiencies up to 4 % [7]. This value has been far exceeded
41 by using a new donor material: poly[[4,8-bis[2-ethylhexyl)-hexyl)oxy]benzo[1,2-b:5-
42 b']dithiophene-2,6-diyl][3-fluoro-2-[(2-ethyl-hexyl)carbonyl]thieno[3,4-b
43 thiophenediyl]] (PTB7). Using this material blended with PC₇₁BM, a certified
44 efficiency of 9.2 % has been obtained [5]. This improvement has been achieved thanks
45 to: i) the absorption of PTB7 in the near infra-red region, ii) the proper energy level
46 alignment with the work function of most used contacts, and iii) the high carrier
47 mobility in this polymer. Besides, PTB7 is semitransparent, making it an ideal candidate
48 for building integrated PV [8]. However, one of the main drawbacks of this technology
49 is the poor device stability. Several works have been focused on this problem, in
50 particular, the penetration of the oxygen and moisture into the active layer [9-13]. The
51 fabrication of inverted poly(3,4-ethylenedioxylenethiophene):poly(styrenesulphonic
52 acid) (PEDOT:PSS) free cells, avoids the etching of indium tin oxide (ITO) [14].

53 On the other hand, Impedance Spectroscopy (IS) technique is a valuable tool for
54 obtaining information about carrier dynamics inside the device [15]. It has been used
55 extensively in organic devices such as emitters [16] and OSCs [17-19]. It consists of
56 superimposing a small voltage signal on a DC voltage. The frequency response of the
57 electrical impedance (defined as the small signal voltage over the small signal current)
58 provides information about material and device parameters such as dielectric constant,
59 built-in voltage, acceptor impurity concentration, geometrical capacitance and mobility
60 [20]. Carrier transport and recombination mechanisms can be identified in the IS spectra
61 and times related to those processes (recombination and diffusion times) can be
62 estimated [17, 20, 21]. It also provides information about the selectivity of the contacts
63 [22, 23] and allows distinguishing between effects taking place in different parts of the
64 device, such as the bulk, interfaces and electrodes [24]. In the last years this technique
65 has been occasionally applied to study degradation mechanisms in OSCs. By comparing
66 IS in fresh and aged devices, Zhao et al. determined that degradation processes take
67 place at different interfaces (P3HT/PCBM and blend/electrode) [25]. Lin et al.
68 performed a layer analysis using IS in dark conditions and obtained information about
69 the changes taking place in device layers and interfaces during the degradation process
70 [26]. By comparing IS before and after the degradation, Weerasinghe et al. conclude
71 that degradation is due to the formation of an electron barrier at the electrode interface
72 and not due to layer delamination [27]. Other works using impedance measurements
73 revealed an increase of the transport resistance in aged devices that is correlated with an
74 increase of defects that obstruct the efficient transport of carriers. Simultaneously,
75 measurements showed an improvement of the electron contact selectivity due to a better
76 covering of the cathode with fullerene molecules [28].

77 In this work we present a detailed degradation study by means of monitoring the
78 impedance spectra of a non-encapsulated inverted OSC based on a blend of
79 PTB7:PC₇₁BM on a periodical basis for almost four months. The cell structure is
80 ITO/ZnO/PTB7:PC₇₁BM/MoO₃/Ag deposited onto glass substrate. Measurements have
81 been performed in dark and under illumination at different bias voltages. Experimental
82 data have been fitted with different equivalent circuits including constant phase (CPE)
83 and Warburg elements.

84 **Experimental details**

85 ITO coated substrates were used as cathode. The ZnO layer was grown by sol-gel where
86 the precursor solution was prepared according to [29]. Spin coating was performed at
87 6000 rpm during 60 seconds followed by a thermal annealing at 200°C during 20 min in
88 air. The active layer PTB7:PC₇₁BM with a relation 1:1.5 was deposited by spin coating
89 in a glovebox system yielding a thickness of 100 nm. A thermally evaporated thin film
90 of MoO₃ (5 nm) was used as electron blocking layer (EBL). A 100 nm Ag layer was
91 evaporated as anode. Devices were not encapsulated. Inset in Figure 1a shows a cross
92 section scheme of the device.

93 The I-V characteristic was measured using an Abet Technologies Sun 3000 solar
94 simulator calibrated with a monocrystal silicon reference cell (Rera Systems).

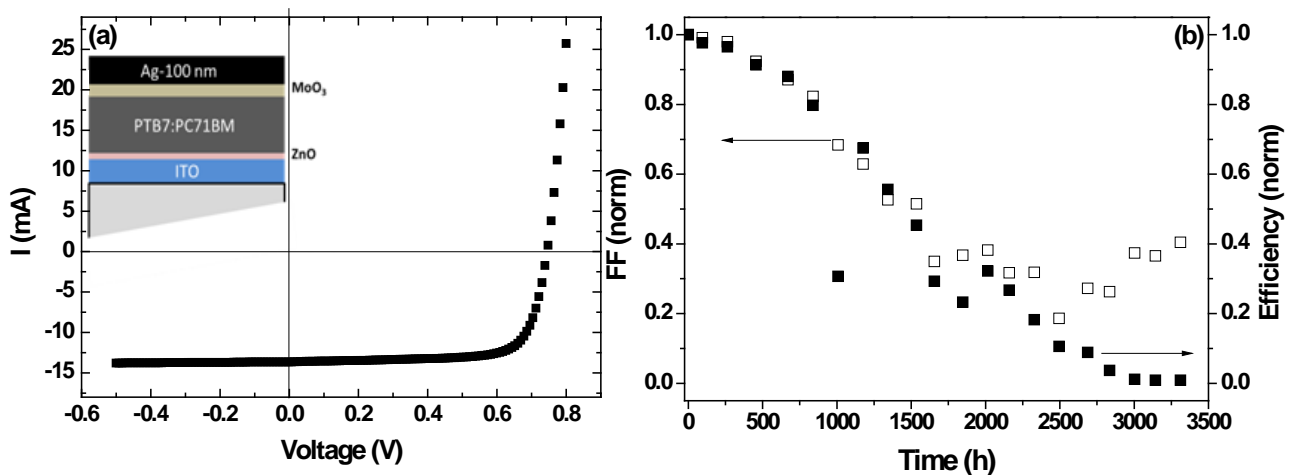
95 Impedance measurements were performed with a Solartron 1260 impedance analyzer.
96 The cell was connected to the analyzer that fed the input signal, biasing the device at
97 different DC levels and superimposing an alternating signal of sweeping frequency with
98 amplitude 100 mV. Light measurements were performed illuminating the device with a
99 conventional red LED (TLHR4400 from Vishay) since absorbance of PTB7:PC₇₁BM
100 films presents a maximum at 600 nm.

101 **2. Results and Discussion**

102

103 Figure 1(a) shows the I-V curve of a pristine device under illumination AM1.5
104 irradiation (100 mW/cm^2). Parameters of pristine solar cells are: $J_{sc} = 13.26 \text{ mA/cm}^2$,
105 $V_{oc} = 0.75 \text{ V}$, $FF = 73 \%$ and efficiency (η) = 7.27 %. Inset depicts the layer structure of
106 the inverted device where the Ag behaves as the anode contact, ITO is the cathode, ZnO
107 is used as HBL (hole blocking layer) and MoO_3 as EBL. State of the art of inverted
108 solar cells based on PTB7 with ohmic contacts for photogenerated charge collection
109 presents efficiencies of 9.2 % and long-term ambient stability when devices are
110 encapsulated in inert atmosphere [5].

111 The time evolution of the FF and the efficiency for the device are shown in Figure
112 1(b). The measured PV parameters were normalized to the corresponding initial values.
113 In between measurements the cells were stored at ambient conditions in dark, which
114 corresponds to ISOS-D-1 Shelf test at level 2, according to consensus stability testing
115 protocols for OPVs [30]. The other parameters (J_{sc} and V_{oc}) remain constant until the
116 efficiency drops to 40% of its initial value [31]. The evolution of the efficiency follows
117 that of the FF until it reaches that value.



118

119 Figure 1. (a) I-V curve under 1 sun AM1.5 illumination of a fresh cell. Inset shows the device
 120 layer structure, (b) Evolution of the normalized FF and efficiency. The parameters are
 121 normalized to the respective value at t = 0h.

122 Figure 2(a) shows the impedance Cole-Cole diagram in dark conditions of the pristine
 123 device from 1 Hz to 1 MHz, at 0.2 and -2 V with no significant injected current.
 124 Experimental data (open symbols) resemble a depressed semicircle that has been
 125 modeled with the parallel R-CPE circuit shown in figure 3, named hereafter **Model A**.
 126 Solid lines of Figure 2(a) show the fit. The depressed semicircle is usually modeled with
 127 two or three parallel RC sets, each one related to a time constant of a dynamical process
 128 inside the cell [32]. In this work, attempts to describe it using RC sets have been
 129 unfruitful, and a distributed element resumed in CPE has been used, suggesting that the
 130 involved interfaces may have great porosity [15]. R_S is modeling wires and contacts,
 131 and R_P is the parallel combination of shunt and dynamical resistances. A constant phase
 132 element (CPE) is a non-ideal capacitor that models the non-homogeneous double-layer
 133 with $Z_{CPE} = 1 / (CPE_T(j\omega)^{CPE_P})$. Since all the fits leads CPE_P values ranging from 0.9 to 1,
 134 CPE will be approximated to a capacitor with $CPE_T = C$, the capacity value. The
 135 capacitance extracted from the fit to dark measurements at negative and sufficiently low
 136 bias that no charge is injected, follows a Mott-Schottky voltage dependence, related to
 137 the depletion capacitance at the cathode contact, whose expression is given by [20]:

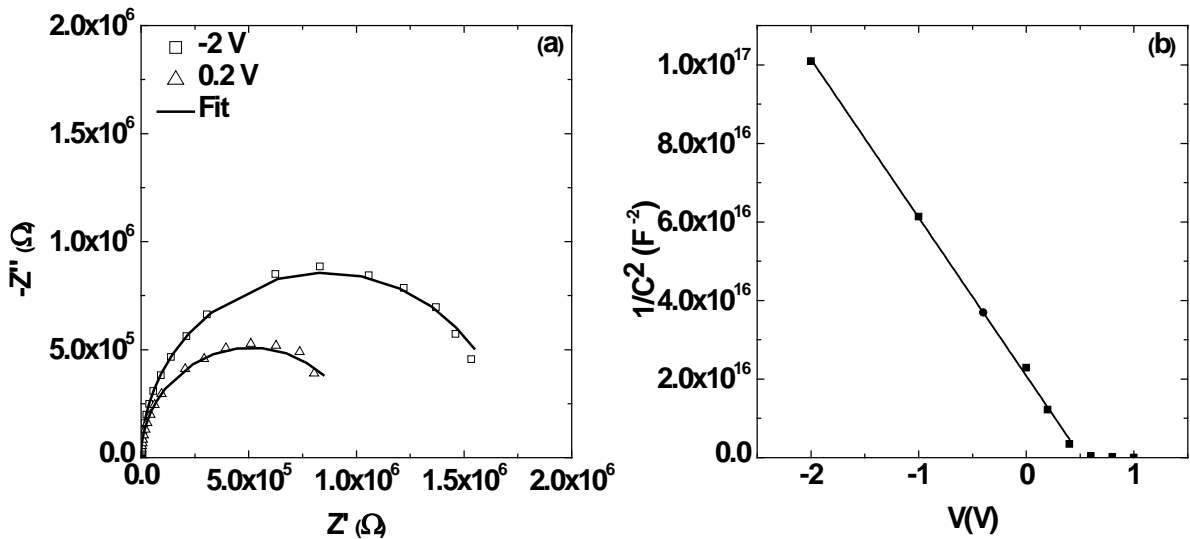
$$138 \quad C^{-2} = \frac{2(V_{bi} - V)}{A^2 e \epsilon \epsilon_0 N_A} \quad (1)$$

139 where previous $CPE_T = C$, V_{bi} is the built-in potential required for flat band conditions
 140 at the cathode interface, N_A is the acceptor impurity density, A is the area (9.6 mm^2), V
 141 is the applied voltage and ϵ and ϵ_0 are the dielectric constant and vacuum permittivity
 142 respectively.

143 The dielectric constant is obtained from the geometrical capacitance (capacitance at
 144 reverse bias) as:

$$145 \quad \varepsilon = \frac{CL}{A\varepsilon_0} \quad (2)$$

146 with L being the active layer thickness, 100 nm, leading a value of 3.6, in agreement
 147 with [33]. Figure 2(b) shows the linear regression of equation (1) to the experimental
 148 data. The acceptor impurity density $N_A = 1.07 \times 10^{17} \text{ cm}^{-3}$, and the built in potential $V_{bi} =$
 149 0.52 V, have been calculated from the slope and the intercept with the X axis of the
 150 linear fit respectively.



151
 152 Figure 2. (a) Impedance spectra under dark conditions at two voltages. Solid lines show the fit
 153 with a parallel R-CPE circuit. (b) Mott-Schottky curve using capacitance values obtained from
 154 the fit using the circuit A of figure 3, where $\text{CPE}_T = C$.

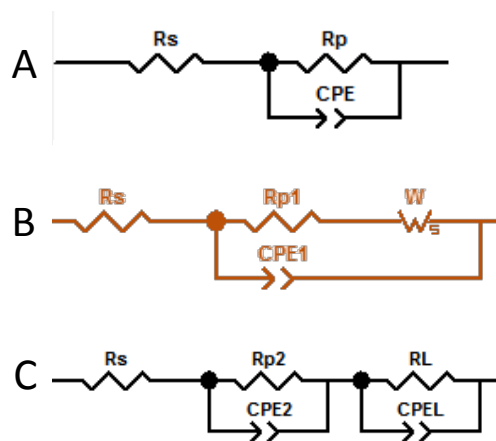
155
 156 Figure 4 depicts experimental impedance spectra under illumination at different bias
 157 voltages for fresh devices, ranging from 0 to 0.4 V in Fig. 4(a), and from 0.6 to 0.8 V in
 158 Fig. 4(b). Experimental data have been fitted using the equivalent circuits of figure 3.
 159 Model A has been used again for voltages below 0.6 V since spectra resemble one

160 semicircle as shown in figure 4(a). In this case, capacitance associated to the CPE
 161 element of model A is the chemical capacitance associated to the excess of charges in
 162 the device.

163 At voltages equal or above 0.6 V a new feature at low frequencies (right side of the
 164 Cole-Cole plot) appears. This tail has been modeled with: i) Warburg element (model B
 165 in figure 3) and ii) an extra R-CPE element (model C in figure 3). As it will be
 166 discussed later in the paper, the appearance of such a low frequency tail may be related
 167 to a charge accumulation inside the device (model C). However, the tail shape changes
 168 along time from a depressed semicircle to a line with slope under 45°. This low
 169 frequency feature time evolution can be associated to a Warburg phenomenon in which
 170 slow diffusion effects may be occurring (model B).

171 It is remarkable that both, CPE and Warburg elements, can be created from a
 172 transmission line of R-C elements, ensuring a unit repetition higher than 100. These
 173 distributed elements reproduce the spectra of the former non-ideal elements.

174 Figure 3 summarizes the three circuits used to model impedance spectra.



175
 176 Figure 3. Circuit A has been used to fit impedance measurements below 0.6 V. Circuits B and C
 177 have been used to model impedance data from 0.6 up to 1V.

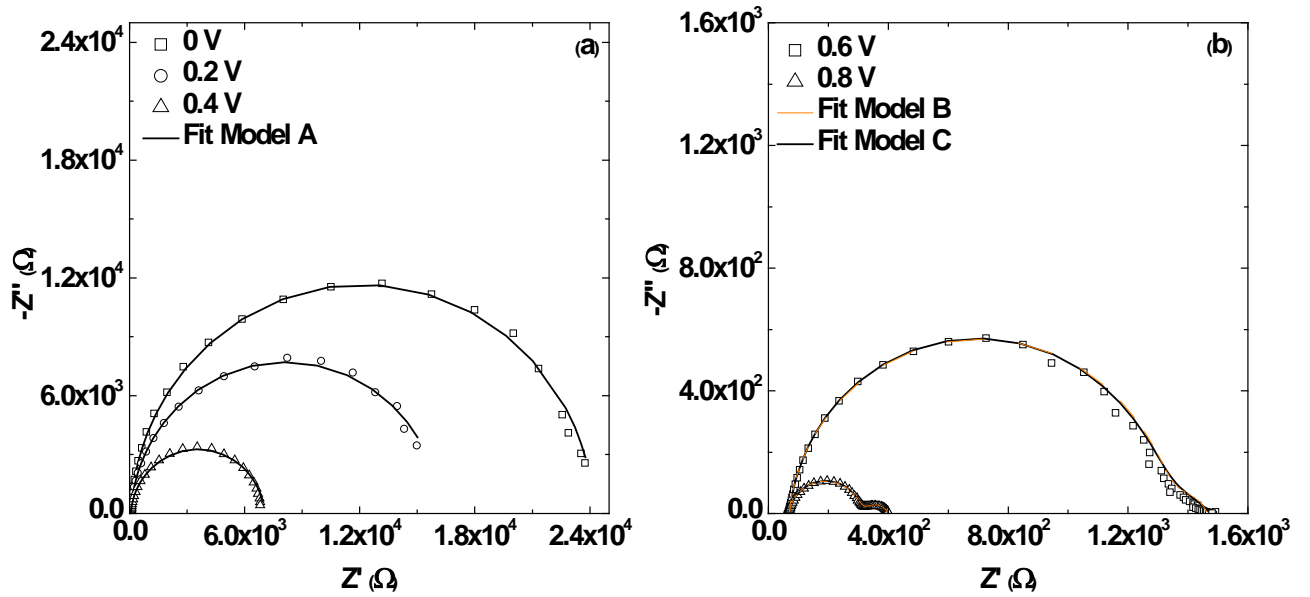
178 Model B consist of short circuit Warburg element [15] in series with the
 179 recombination resistance (here R_{p1}), all in parallel with a CPE (named here as CPE1),
 180 that reproduces the low frequency tail [31]. Warburg impedance can be defined as:

$$Z_W = W_R \frac{\tanh(j\omega W_T)^{W_P}}{(j\omega W_T)^{W_P}} \quad (3)$$

182 where W_R is the Warburg resistance, W_T is a Warburg capacitance and W_P is a constant
 183 value in our case ranging from 0.3 to 0.5. Warburg element has been often found in
 184 literature in different devices, including dye solar cells [34-35].

185 Figure 4 (b) shows that both models B and C can accurately reproduce the
 186 experimental impedance spectra overlapping in the whole frequency range. We propose
 187 that the low frequency feature, modeled either the Warburg element (model B) or the
 188 extra R_L - CPE_L (model C), can be interpreted as a charge accumulation that cannot be
 189 effectively extracted through the contacts. It is worth pointing out that IS technique does
 190 not allow to determine in which electrode the charge accumulation takes place. Previous
 191 works report on charge accumulation at the ZnO interface but only when the cell is
 192 illuminated [36, 37]. In our case, the low frequency arc in the Nyquist plot occurs at
 193 high voltages (0.6 and 0.8 V), both in dark and light conditions, suggesting that the
 194 charge accumulation is not due to photo induced carriers but to the applied electric field.
 195 On the other hand, the anode is exposed to oxygen and water since devices are inverted
 196 and not encapsulated, suggesting that both slow diffusion and charge accumulation
 197 phenomena at the anode are not discarded scenarios. In summary, the low frequency arc
 198 in the Cole-Cole increases the device resistivity, worsening charge extraction and thus
 199 generating a charge accumulation effect.

200 It is remarkable that no transport resistance associated to diffusion mechanisms is
 201 needed to model the impedance spectra at high frequencies, implying that the mobility
 202 of the blend material is such that transport is not limiting conduction



203

204 Figure 4. Impedance spectra of fresh devices under illumination at several voltages. Solid lines
 205 show the fit to the circuits of figure 3.

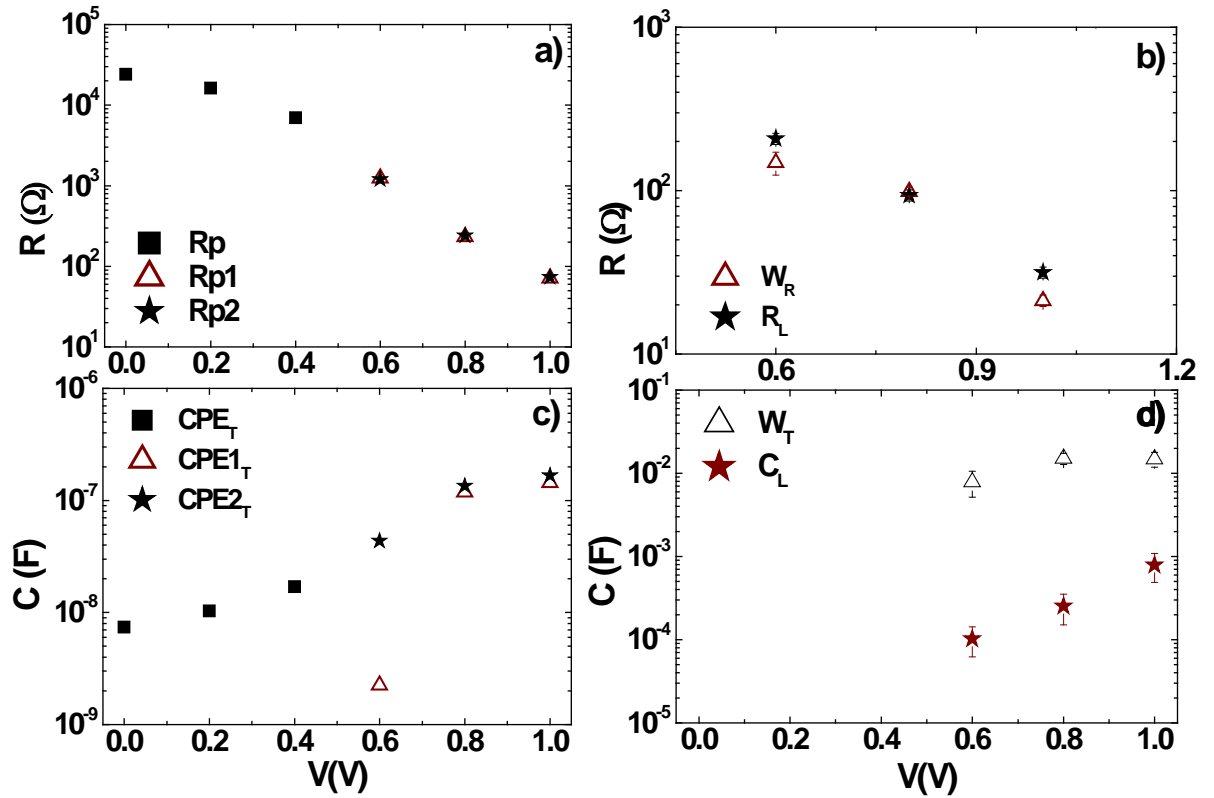
206 Figure 5 shows the parameters extracted from the previous fits at voltages ranging
 207 from 0 to 1 V. Figures 5(a) and (b) show the resistive parameters, and figures 5(c) and
 208 (d) the capacitive ones. Figure 5(a) shows that R_P , R_{P1} and R_{P2} follow the same trend
 209 with R_{P1} and R_{P2} overlapping at high voltages. These parallel resistances decrease with
 210 voltage, indicating an increase of charge recombination as expected.

211 Figure 5(c) shows the accurate match of $CPE1_T$ and $CPE2_T$ following the same trend
 212 as CPE, and increasing with voltage due to charge injection. At 0.6V the impedance
 213 spectra do not clearly show a low frequency semicircle but a tail causing a mismatch
 214 between $CPE1_T$ and $CPE2_T$. Models B and C are equivalent and lead to similar
 215 parameters when two arcs are clearly observed but differ at this transition voltage.

216 Concerning W_R and R_L shown in Figure 5(b), both parameters have similar values
 217 since they are both related to the low frequency arc diameter. Low frequency capacitors
 218 shown in Figure 5d do not present the same values since they are not equivalent from a
 219 circuitual point of view. Even though the low frequency resistances (W_R and R_L)

220 decrease with voltage, this does not mean that the charge accumulation effect decreases.
221 These parameters have to be regarded in comparison to the parallel resistances (R_{P1} and
222 R_{P2}) associated to charge recombination. In order to study the influence of charge
223 accumulation resistance in the overall cell impedance, the ratio W_R/R_{P1} has been
224 calculated obtaining 0.12 and 0.42 for 0.6 V and 0.8 V respectively. This suggests that
225 the influence of charge accumulation phenomenon at the interface increases with
226 voltage as was expected.

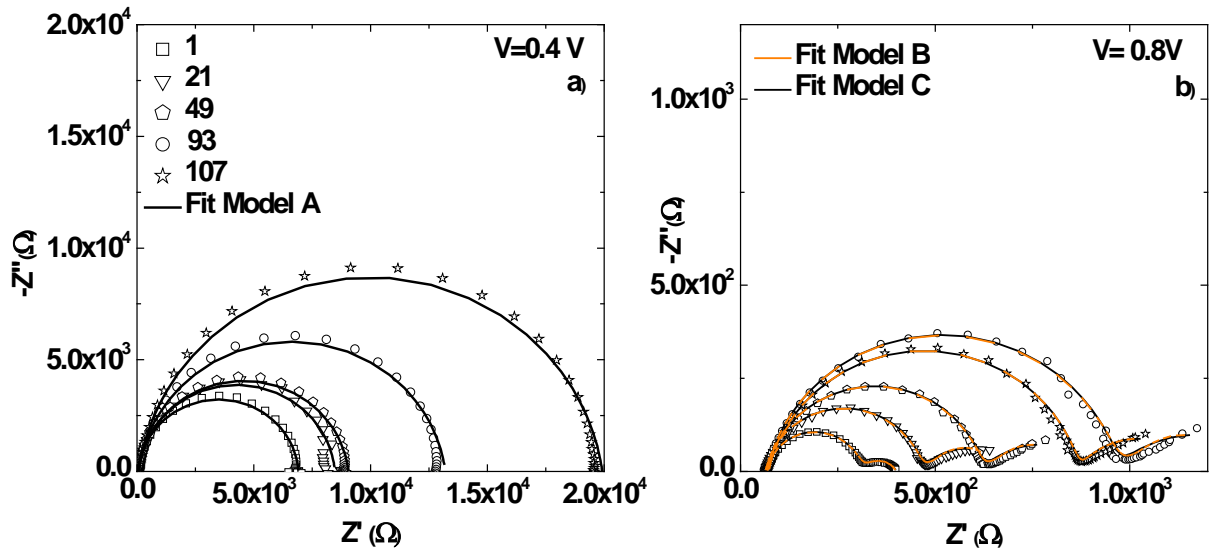
227 Although at first glance the low frequency arc may also be attributed to traps states
228 present in the organic layer, we have discarded this hypothesis since traps would
229 respond to the low frequency signal at low voltages, when traps begin to fill. However,
230 the low frequency arc only appears in the Nyquist plot at high voltages (see Figure 4b)
231 when there is a strong charge injection. In this situation, the high current flowing
232 through the device would strongly affect the trap occupancy function (trap states would
233 be filled) avoiding the small signal to activate the trapping-detrapping process and thus
234 suppressing the trap response. This dismisses trap mechanisms and supports the
235 hypothesis of charge accumulation [38].



236

237 Figure 5. Parameters obtained from the fits of figure 4 using models of figure 3. Model A, B and
 238 C parameters are plotted with squares, hollow triangles and stars respectively. (a) Parallel
 239 resistance, R_p . (b) Warburg resistance and R_L associated to low frequencies (c) CPE_T (=C)
 240 attributed to the main semicircle in the Cole-Cole plot. (d) CPE_L (= C_L) and Warburg capacitive
 241 (= W_T) parameter related to the low frequency feature. Error bars are included in figures (b) and
 242 (d), in figures (a) and (c) the error bar is within the symbol size.

243 In an attempt to check the variations of the previous parameters with time, Figure 6
 244 shows selected impedance spectra for the 107 days of tracking. Although some
 245 fluctuations can be observed, the overall trend is that the magnitude of the impedance
 246 increases due to the raise of R_p (the right intercept of the depressed semicircle with the
 247 X axis). Figure 6b shows the evolution of impedance spectra with time at 0.8V,
 248 depicting that from a circuitual point of view both models B and C can accurately
 249 reproduce the low frequency feature. In addition, Figure 6b shows an increase with time
 250 of the low frequency arc suggesting that the effect of charge accumulation is more
 251 pronounced with time. This effect is related to cell degradation, since at high voltages
 252 and low frequency, an increase of the overall resistance implies that the I-V curve
 253 flattens diminishing the slope and thus fill factor.



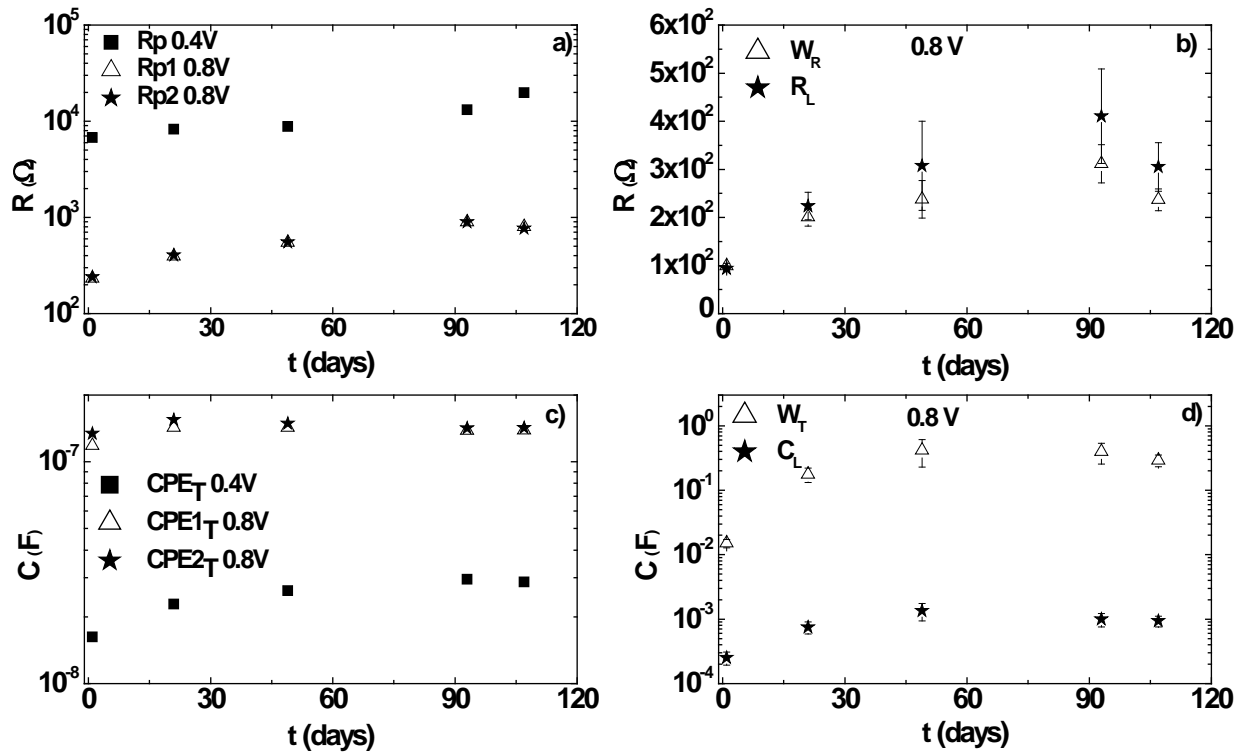
254

255 Figure 6. a) Evolution of impedance spectra for 107 days at two voltages 0.4 V and b) 0.8 V.
 256 Solid lines show the fit to models A, B and C.

257

258 Figure 7a shows that the parallel resistance at 0.4 V remains quasi-stable until the last
 259 days of measurement that slightly increases with time, suggesting that the bulk layer
 260 degrades leading eventually to permanent device failure, as has been previously
 261 observed by [26, 27].

262 Figures 7b and 7d show an increase with time of the low frequency resistance (R_L and
 263 W_R) and low frequency capacitances (W_T and C_L) respectively. Both trends indicate an
 264 enhancement in the charge accumulation, increasing the resistive effect at the contact,
 265 thus hindering charge extraction through the electrodes and ultimately contributing to
 266 device degradation. This fact is confirmed by the slight increase of the chemical
 267 capacitance shown in Figure 7c. From a circuitual point of view, the sum of R_P and R_L
 268 (or W_R), neglecting R_S , represents the inverse of the I-V slope. Thus, at 0.8 V (around
 269 V_{oc}), a simultaneous increase of R_P and W_R with time implies a decrease of such slope,
 270 and consequently a decrease in FF and thus efficiency, which is in agreement with
 271 Figure 1b.

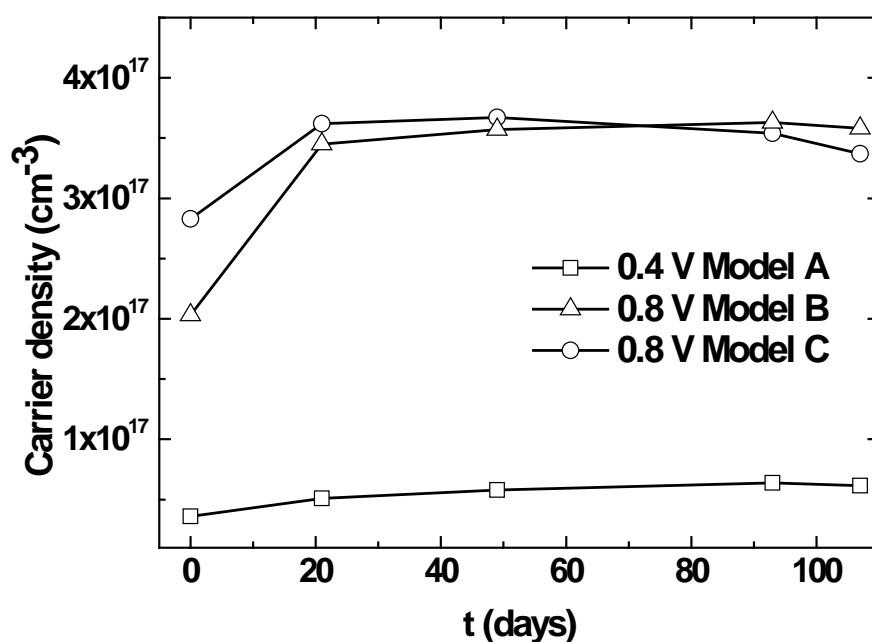


272

273 Figure 7. Evolution of parameters obtained from the fit of figure 6 for 107 days at $V = 0.4$ and
 274 0.8 V. Model A, B and C parameters are plotted with squares, hollow triangles and stars
 275 respectively. (a) Parallel resistance, R_p ; (b) Resistance associated to the low frequency feature;
 276 (c) Capacitance CPE_T ; (d) Capacitance associated to low frequencies. Error bars are included in
 277 figures (b) and (d), in figures (a) and (c) the error bar is within the symbol size.

278

279 Figure 8 shows the carrier density extracted from the integral of the chemical
 280 capacitance versus time. As mentioned before, the impedance spectra do not show a
 281 conduction limiting effect associated to charge diffusion mechanism. The increase of
 282 carrier density again ratifies the hypothesis that charges cannot be efficiently extracted
 283 through the contacts, possibly due to the charge accumulation at the electrodes. After 20
 284 days of measurement the excess of carriers within the cell saturates. Moreover, some
 285 authors have also suggested the formation of a metal-oxide layer due to corrosion of
 286 metal electrode surface that can act as a charge-transport barrier [39].



287

288 Figure 8. Carrier density extracted from the integral of chemical capacitance (CPE_T) vs time at
 289 0.4 and 0.8 V.

290 **3. Conclusions**

291

292 We have measured impedance spectra of non-encapsulated inverted organic solar cells
 293 based on PTB7:PC₇₁BM for almost four months in order to study degradation. Low
 294 voltage measurements have been successfully fitted using a classic equivalent circuit,
 295 with a contact resistance R_S in series with a parallel set of a mainly capacitive constant
 296 phase element CPE, and a carrier recombination resistance R_P . However, a new feature
 297 appears at high voltages and low frequencies that has been accurately modeled with two
 298 different equivalent circuits, one including a Warburg element and the other one using
 299 an extra R-CPE. The low frequency feature suggests charge accumulation effects at the
 300 electrodes that ultimately results in a worsening of charge extraction, due to the
 301 incorporation of oxygen and water through the anode. Moreover, the parallel resistance
 302 associated to the active blend increases with time, indicating a worsening of conduction
 303 in the bulk, and thus a cell degradation. The increase of the overall resistance (R_P+R_L)

304 with time at high voltages is in agreement with the diminishing of the I-V slope and the
305 corresponding decrease of the fill factor.

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