

HIGH PERFORMANCE ORGANIC TRANSISTORS FOR ORGANIC ELECTRONIC
APPLICATIONS

A Dissertation

by

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ABSTRACT

Thin-film transistor (TFT) devices using organic semiconducting materials have attracted widespread attentions due to their low cost, flexible form factor, and easy fabrication. However, organic materials' poor performance as compared to inorganic semiconductor such as silicon limits their applications. Specially, high-frequency operation in organic transistors has never been achieved with organic semiconducting material. One very attractive application for organic electronics is low-cost and flexible Radio Frequency Identification Tag (RFID), which requires relatively high frequency operation. Because of low mobility and high operating bias voltage, the current organic TFT is not appropriate for the most of applications including RFID.

The objective of this research is to develop the high performance organic transistor structures which are suitable for organic electronic applications. In designing, two major performance metrics of devices are focused to be improved, which are the on-current level with high on-off ratio and the cutoff frequency of the transistors. They are determined mainly by the carrier mobility, the injection of carrier at the metal/semiconductor boundary, and the passive parasitic components introduced by device geometry. In this study, three new structures are investigated, namely dual-organic layer Metal-Semiconductor Field-Effect Transistor (MESFET), depletion mode organic Metal-Oxide-Semiconductor Field-Effect Transistor (MOSFET), and organic Heterojunction Bipolar Transistor (HBT). Each of these devices is optimized to enhance the performance of the devices based on comprehensive theoretical modeling, and

validated by simulation using TCAD. The devices with channel length of longer than 4 μm exhibit a few μA of on-current and ~ 10 MHz cutoff frequency. The results obtained in this work show those novel transistor structures can overcome the weakness of conventional organic TFTs and have great potential in realizing organic circuit applications in the future.

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Contributors

This work was supervised by a dissertation committee consisting of Professor Xing Cheng [advisor], Professor Jun Zou, and Professor Weiping Shi of the Department of [Electrical and Computer Engineering] and Professor Choongho Yu of the Department of [Mechanical Engineering].

The device fabrication for Chapter 3 was collaborated with Bo Yu of the Department of [Material Science in South University of Science and Technology of China].

All other work conducted for the dissertation was completed by the student independently.

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CHAPTER I

INTRODUCTION: ORGANIC ELECTRONICS

Over the years, organic electronic and its potential applications have attracted widespread attentions in research. Organic transistors can be processed at a low temperature, and they can be fabricated with easy processing steps, such as printing, nanoimprinting, and roll to roll [1], [2]. However, organic transistors have many constraints which limit the use of organic transistor only to a very few applications. As compared to main stream silicon devices, the most critical disadvantages of organic transistors are their very poor carrier mobility and their structural feasibility since many of conventional fabrication methods are unavailable to process organic semiconducting materials, for instances, ion implantations, and etc. Although there have been so many efforts to develop novel processing techniques suitable for fabrications of organic transistors, most of them are focused on MOSFET structure. Some of already developed and widely used transistors' structures such as MESFET, depletion mode MOSFET, and HBT are more feasible to fabricate using organic semiconducting materials without very sophisticated methods because they can be stacked layer by layer as thin film shapes. Furthermore, almost infinite number of organic material choice is possible by chemical synthesizing. Consequently, devices requiring different layers, different doping profiles, or different energy band parameters can take the advantages from the stacks of thin organic films. As of these reasons, different structures of organic transistors should be thoroughly studied and strongly considered as a component of organic electronics.

Above mentioned transistor devices, MESFET, depletion mode MOSFET and HBT are originally designed in need of high performance device for extremely high speed electronic circuits even in conventional silicon technology. Therefore, the AC performance of those devices built with organic semiconductors are expected to behave much better than typical organic MOSFET transistors as well as the DC performance. It has been reported that the cut off frequency of nanometer range of channel length OTFT can be up to 10MHz with moderate carrier mobility [3], which is not high considering the short channel length of nanometer range. As stated earlier, fabricating well behaving OTFT with such short channel length is very difficult and impossible only with normal organic processing methods. On the other hand, organic MESFET, depletion mode OTFT, and Organic Heterojunction Bipolar transistor device are shown that the cut off frequencies can be up to more than 10MHz even when the channel length is a few micrometers.

As the first step of the study, short-channel and long channel TFT devices are simulated by incorporating physical models for materials, interfaces and device operations. The purpose of this simulation is to validate that the simulation has captured all essential physical models in device operations. Also, important material and physical parameters used in these models can be extracted by comparing simulation results with experimental results published in literature. After that, the OMESFET, depletion mode OTFT, and OHBT structures are simulated to demonstrate the advantages and weakness of those organic transistor devices. Finally, the modifications are made for those devices to optimize the performance of the devices and overcome the weakness of devices. The

improvements of performances are demonstrated for both of theoretical simulation results and experiments results. All the device structures are compatible and built with normal processing techniques of organic materials.

CHAPTER II

BACKGROUND PHYSICS AND MODELING

There are three main different physics explaining organic semiconductors from inorganic counterparts. Organic semiconductors are not crystalized in atomic level such as silicon. Instead, they are π -conjugated materials where the charge transport occurs by hopping from one molecule to other using trap sites of molecules. Therefore, unlike inorganic semiconductors, the carrier behavior of organic semiconductor is very different from inorganic semiconductor, which results in that the carrier mobility depends on the electric field and the carrier concentration, more complicated way than inorganic semiconductors. This hopping process is not limited only on the behavior of carrier in the bulk region of semiconductor, but also affects the behavior of carrier at the interface between electrode and semiconductor. In addition to hopping, another physics phenomena affects the carrier behavior of injection into semiconductor at the interface of metal/organic. The permanent electric dipole is formed at the metal/organic interface and the resulting potential barrier is 0.1eV~0.5eV higher than the expected one aligned by their workfunction of metal and ionization energy of organic semiconductor. To account the injection of carrier from electrode accurately, Schottky tunneling and trap assisted tunneling must be considered as well as thermionic emission over the barrier. In this chapter, these three physics are investigated thoroughly and modeled by ATLAS TCAD device simulator.

It is worth to note that the material properties of organic semiconductors, such as carrier mobility, trap density, and the shift of metal workfunction, varies greatly depending on the choice of material, the degree of chemical contamination, film morphology, and the process environment. As of this reason, instead of finding the exact values of material parameters to do fine tuning when modeling the physics, the generalized parameters were found to reproduce the behavior of device from experiments.

Carrier Mobility

In organic semiconducting materials, depending on the film, whether it is highly disordered or highly crystallized, carrier mobility is described by slightly different mechanisms. Carriers are repeatedly trapped by shallow traps, which are located near conduction and valence band, and released by thermal agitation. This kind of carrier transporting behavior is also known as multiple trap and release (MTR) [1], [4]. Another kind of carrier movement in organic semiconductor takes place through deep level traps located at middle of forbidden band. Since those traps are located in deep level, trapped carriers are not able to escape only by thermal agitation. Instead, those carriers jump to the near trap site when applied electric field is high enough [5]. Both of carrier movements take place in both of highly disordered and highly crystallized organic materials. In highly crystallized organic semiconductors, the density of deep level traps is much smaller than highly disordered organic semiconductors. Therefore,

crystallized organic semiconductors have much higher carrier mobility and more linear I-V behavior rather than quadratic I-V behavior.

To model carrier mobility in organic semiconductors accurately, the followings must be considered: 1) Low-field mobility [6], 2) Carrier concentration dependent mobility enhancement factor [4], [5], and 3) Field dependent mobility enhancement factor [7], [8]. The field independent mobility (low field mobility) can be described as

$$\mu_{eff} = \frac{n_f}{n_f + n_t} \cdot \mu_0 \quad (1)$$

Where n_f and n_t are the number of free carriers and trapped carriers. Equation (1) explains that the shallow traps close to conduction/valence band slow down the carrier mobility by continuous trapping and it can be easily modeled by replacing the constant mobility parameter. Although (1) is an approximated equation and the product of distributed trap and probability must be integrated to get a complete answer, it is good enough to model the low field mobility incorporating with shallow traps.

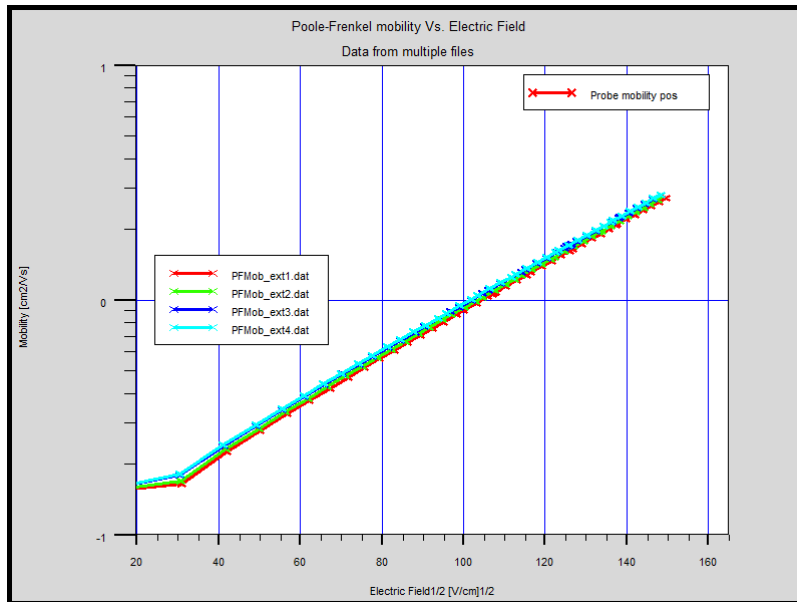
To account for the effect of high electric field, an electric field mobility enhancement factor must be combined with (1). The field enhancement factor can be written as

$$\exp\left(\frac{q}{kT} \beta \sqrt{F}\right) \quad (2)$$

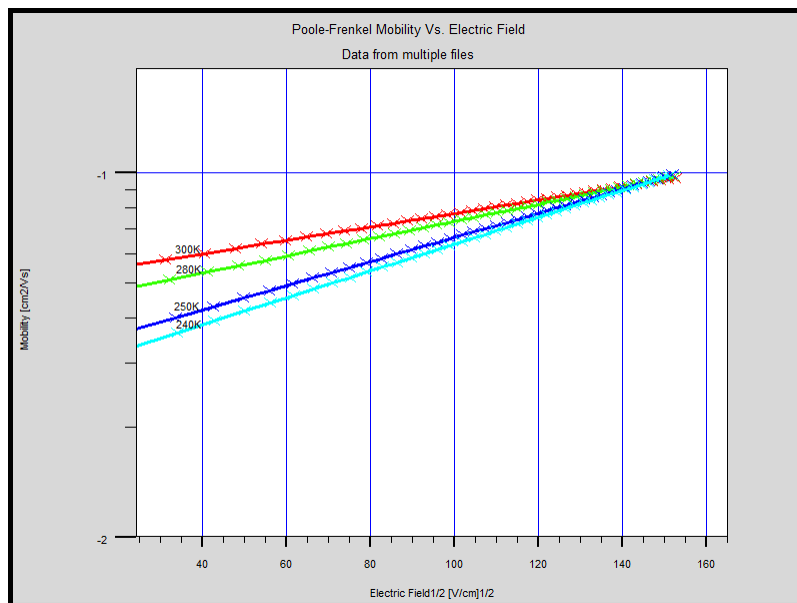
Where β is the Poole-Frenkel factor. Combining (1) and (2) gives an equation of electric field and shallow traps with the fitting parameter γ

$$\mu(T, F) = \frac{n_f}{n_f + n_t} \cdot \mu_0 \cdot \exp\left[\left(\frac{q}{kT} \beta - \gamma\right) \sqrt{F}\right] \quad (3)$$

Equation (3) is known as Poole-Frenkel mobility model [7]-[9]. It can be easily noticed that even very small change of the fitting parameter results in a huge deviation in current level because of its exponential dependency. Although using the equation reproduce the tendency of current depending on electric field, it is possible that simulation results are diverged more than several orders. Also, in our simulation study, $\sim 10^3$ of current level deviation was observed without adjusting the fitting parameter. Due to this reason, especially in preceding simulation study before building an actual device, Poole-Frenkel mobility model is poor at predicting the current-voltage behavior. Figure 1 shows that how the calculated mobility deviates greatly when the channel length of device is changed without adjusting the fitting parameters, or when the fitting parameters are changed while the device size remains same. Because of this reason, equation (3) is referred as Poole-Frenkel mobility with a limited range of electric field.



(a) Short Channel Device



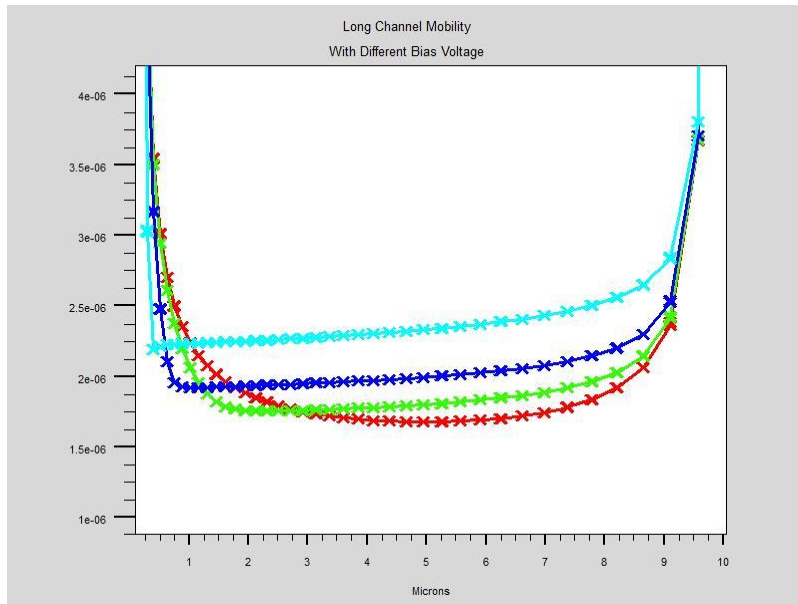
(b) Long Channel Device

Figure 1. Simulated Poole-Frenkel Mobility Model

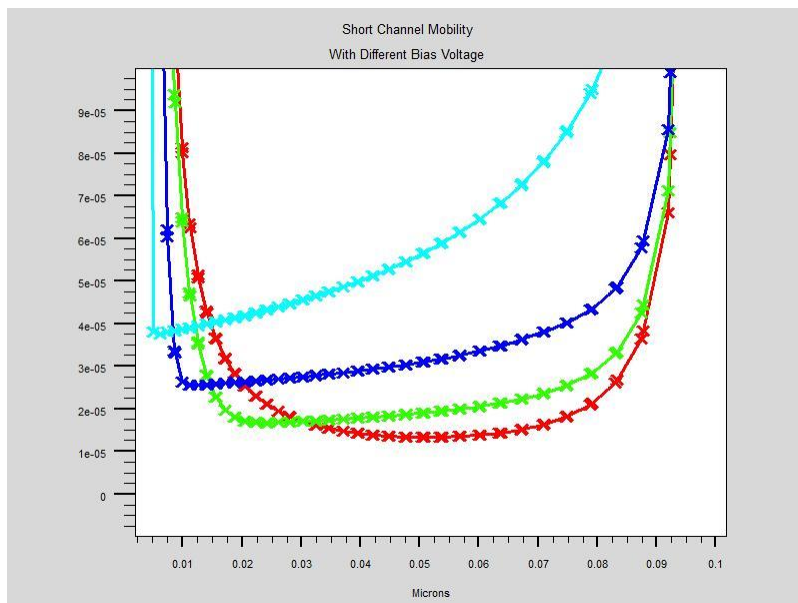
Instead, using unified Gaussian disorder Pasveer model [4] gives us simulation results excellent matched with experiment results without changing any fitting parameters and therefore it is much more feasible model to use to design a device and predict the performance of designed device. In fact, there is no fitting parameter of non-physics meaning in Pasveer mobility model such as β in Poole-Frenkel mobility model. The equation of Pasveer mobility model is a fundamentally same form with Poole-Frenkel mobility and the expression is

$$\mu(T, n, F) = \mu_0 \cdot g_1(T, n) \cdot g_2(T, F) \quad (4)$$

Comparing equation (4) to (3), (4) has another mobility enhancement term g_1 included. The term indicates that carrier mobility also depends on the carrier concentration [4]. The term of g_2 is also an exponential function of electric field with better refined range of electric field. The author of [4] claimed that Pasveer mobility model is better with the devices which have small Schottky barriers and the range of Gaussian width of densities less than $\sim 0.2\text{eV}$. In OTFT devices, the gate voltage reduces the width of Schottky barrier enough to induce the tunneling at the interface between organic and source/drain contact, the Pasveer mobility model is also applicable to OTFT devices. Furthermore, in recent studies of OTFT, as well-ordered materials are used more often rather than highly disordered ones, it is more reasonable to use the Pasveer mobility model for simulation study. The calculated carrier mobility is shown in Figure 2 in accordance with the position. The carrier mobility fits the widely known value of mobility from many literatures and experiments.



(a) Long Channel Device



Short Channel Device

Figure 2. Simulated Pasveer Mobility Model

It is also proved that the mobility modeled with Pasveer model agrees with experiments even when the size of device is changed in the later part of this chapter. The modeled values of Pasveer mobility are shown in Table 1.

In this study, both of pentacene and P3HT are used to build actual devices since the energy band parameters of those two materials are almost same. That is, devices are categorized as polymer devices or small molecule devices for simplicity. Moreover, they are the most popular organic semiconducting materials used in organic TFT devices.

Table 1. Modeled Pasveer Mobility Parameters

Fitting Parameter	Value	Variation
α	0.1nm	± 0.02
σ	0.1eV	+0.05, -0.02

Metal/Organic Interfaces

When an organic material and metal are contacted together without any surface treatment such as doping or depositing thin layer of surface modifying materials, Schottly contacts are formed instead of ohmic contact even when using metals with high

workfunctions. The shift of metal workfunction is described by several physics phenomena [10]: 1) charge transfer caused by the difference between a metal workfunction and the electron affinity and ionization energy of organic film [11], 2) chemical reaction filling states at the interface and resulting in the shift of Fermi level at the interface [12], and 3) molecule-induced modification of the metal workfunction, which is also known as pillow effect [13]. According to [10], the effect of 1) is negligible compared to 3) since pentacene/P3HT and gold are used in our study. The category of 2) affects the interface depending on the structure of TFT devices whether it is top contact or bottom contact, which is the result of fabrication sequence [12]. Our strategy of modeling the metal/ organic interface for simulation study is that setting the Schottky barrier height about 0.3~0.5eV as reported in [10] and [12] first, then performing fine tunings by adjusting Richardson constant and the effective mass of carrier to control Schottky tunneling and thermionic emission [14] at organic/metal interface. This method of approximation is not accounted for describing the interface physics best, but good enough to fit the experiment curves and validating our device design since this method still includes most of the crucial physics at organic/metal interface. The Richardson constant which controls both of tunneling and recombination currents can be described as the equation

$$A^* = \frac{4\pi m q k^2}{h^3} \quad (5)$$

Where m is the effective mass of carriers. It is assumed that the effective mass of majority carrier hole can be varied from 0.5 to 3 from depending on the type of organic

thin films, therefore the value is swept in the range to perform a fine tune to fit the results of experiments.

The one of the most critical performance bottlenecks of organic transistors is organic/metal interface due to Schottky contact formed, which is not only limiting the injection of carrier, but also preventing devices from saturating. To minimize the problem, gold is usually the best choice for P-type transistor most of the time as source and drain electrodes as the workfunction of gold is 5.1~5.4eV which is close to the valence band (HOMO level) of organic semiconductor. In case of organic MESFET, another metal/organic interface exist at gate electrode which is, on the contrary to the previous case, high Schottky barrier is desirable indeed to prevent the unwanted gate leakage current [14], [15]. Naturally, aluminum is the most popular choice for gate electrode to align the workfunction of gate as far as possible from the valence band. However, the shift of gate metal workfunction toward to valence band makes Schottky barrier at gate is smaller. Therefore, I-V characteristics at interface must be carefully modeled and fine tuning of interface parameters must be performed.

The first component of current flowing into the organic from electrode is described by thermionic emission. This current can be expressed as the equation [14]-[16]

$$J = q v_s N_{c,v} \exp\left(\frac{-\phi_b}{kT}\right) \left[\exp\left(\frac{qV}{kT}\right) - 1 \right] \quad (6)$$

Where v_s is the surface recombination velocity of carrier and ϕ_b is the barrier height of Schottky contact.

The other component of current at metal/organic interface is Schottky tunneling induced by high electric field applied between source and drain metal electrode and organic semiconductor, or gate metal and organic semiconductor [17]. To model the Schottky tunneling current in our simulation, the following equation is used.

$$J_T = \frac{A^* T_L}{k} \int_E^\infty \Gamma(E') \ln \left[\frac{1 + f_s(E')}{1 + f_m(E')} \right] dE' \quad (7)$$

Where A^* is the Richardson constant, $\Gamma(E)$ is the tunneling probability, and $f_s(E)$ and $f_m(E)$ are the distribution functions in the semiconductor and metal. In short channel devices, Schottky tunneling is the dominant current flowing in the device. Thus, without any modification of interface, the short channel organic transistors do not enter into the saturation region and the current increases by quadratic function. This is the another main reason of not fabricating short channel OTFTs besides the increased cost of building short channel devices.

To model the interface physics, the measured DC characteristics of short channel OTFT from literature were used because of the two reasons: 1) It is difficult to separate Schottky tunneling current and thermionic emission current from the total current and 2) the carrier mobility in organic semiconductor is also strongly depending on the electric field, in turn, both of Schottky tunneling component and mobility component must be combined when modeling the behavior of device. It is shown that Schottky tunneling becomes significant at around $4\mu\text{m}$ short channel length and starts becoming dominant over thermionic emission at $1\mu\text{m}$ from simulations, which depicts that the tunneling current can be modeled accurately using the DC characteristics of less than $1\mu\text{m}$ channel

length device. In other words, Schottky tunneling current is insignificant in long channel device such as demonstrated in [18]. Figure 3 and Figure 4 are the simulation results of 200nm and 70nm short OTFT, which are fabricated in [19], with Schottky tunneling model. The modeled parameters are listed in Table 2.

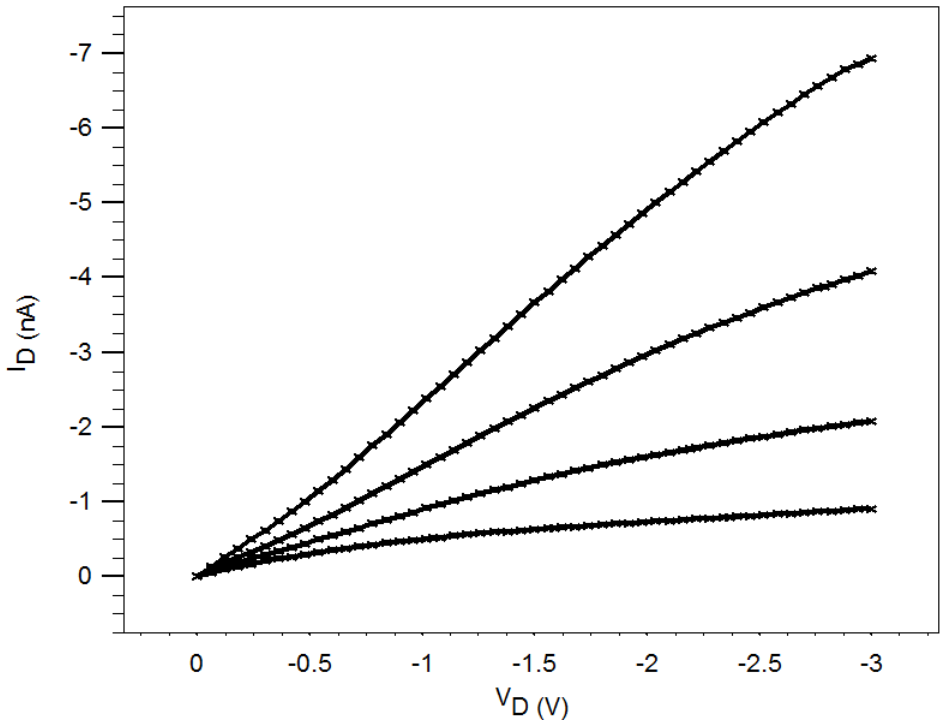


Figure 3. 200nm Short Channel OTFT in order to Model Schottky Tunneling

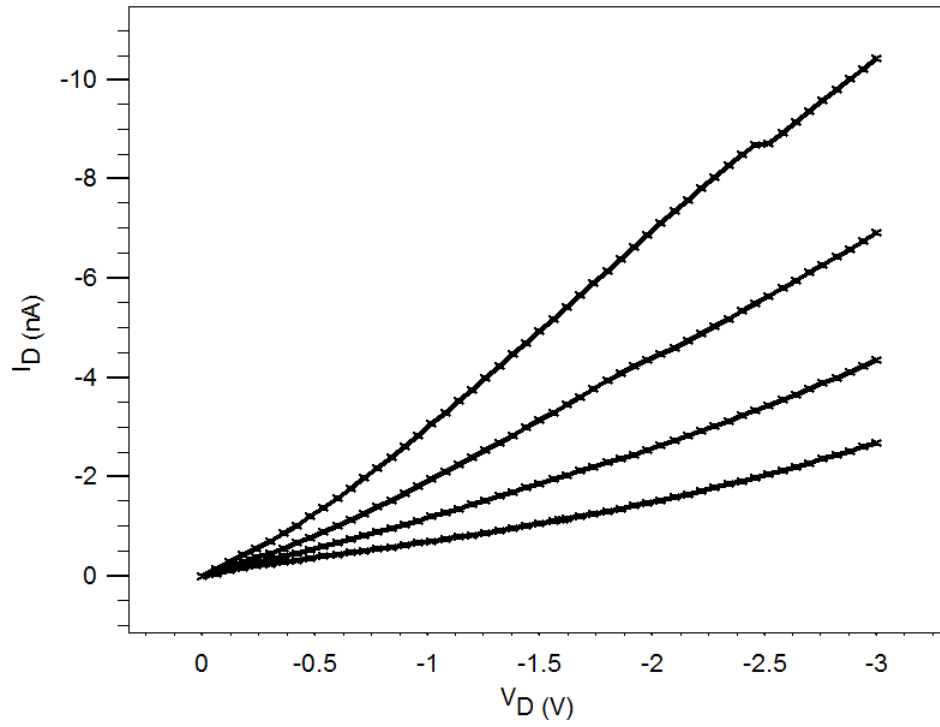


Figure 4. 70nm Short Channel OTFT in order to Model Schottky Tunneling

Table 2. Modeled Shottky Contact Parameters

Fitting Parameter	Value	Variation
Richardson Constant (A^*)	300	± 50
Effective Mass (h_e^*)	2.5	± 0.5

Organic Defects

Unlike inorganic single crystalline semiconductors such as silicon, organic semiconductor materials show that the huge variations of parameters in material properties depending on morphology, methods of deposition, surface treatment agents, and etc. That is, the density of traps is not the unique material property and can be varied under different circumstances. Also, since the behavior of carrier in existence of defects is modeled with mobility model [4], [5], [9], the main purpose of trap density model is only to reduce the number of free carriers in organic semiconductor effectively. Generally, the distribution of trap sites is described with two Gaussian distributions, the first one is located near the conduction and valence bands, and the other one is located deeply inside the forbidden band [1], [20]. Then, the number of trapped carriers is calculated by integrating multiplication of the probability of occupancy and the number of trap sites over the energy.

$$P_{D.trapped} = \int_{E_{p,trap}}^{E_c} g_D(E) F_{D,trap}(E, n, p) dE$$

To maintain the generality with unified Pasveer mobility model, the main Gaussian peak of trap sites is set to 10^{20}cm^{-3} and width is set to 0.1eV in order to keep calculated carrier mobility unaffected by the traps. Instead, only the second Gaussian peak is adjusted to fit experiment results and perform fine tuning because the deep trap sites affects the number of trapped carrier mainly and weakly interact with the carrier mobility [9]. The example of modeled trap density vs. energy is shown in figure 5.

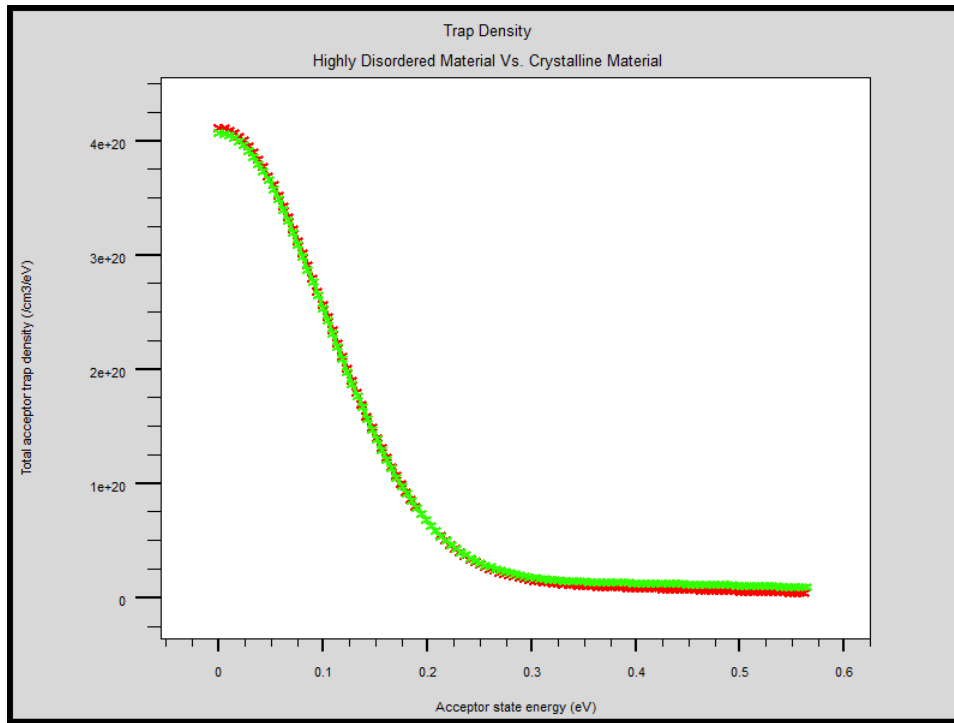


Figure 5. Modeled Trap Density of Organic Materials

As shown in figure 5, with 0.1eV of Gaussian width, the second peak of Gaussian trap density which represents the deep traps of disordered materials is relatively small number compared to main peak. And therefore, the resulting distribution of total traps can be approximated as one Gaussian distribution with different Gaussian width [21].

Other Modeling Considerations

The first three parts of this chapter describe the physics inherited in organic materials. Although those physics models are good enough to model OTFT devices and reproduce the experiments results with simulations, under the low bias condition, i.e., device is turned off or in subthreshold region, the small shift of threshold voltage or external lumped impedance is better to be included to obtain more accurate simulation results. The threshold voltage shift is usually occurred by trapped charges between thermally grown oxide and silicon substrate. For the most case in organic transistors, bottom gate feature is more commonly used to reduce the number of process steps and it is easier to fabricate. Therefore, the trapped charge at oxide interface cancels out certain amount of applied gate voltage or adds off-set voltage to gate. Figure 6 illustrates the types of trapped oxide charges [22], [23].

SiO ₂	Q_m: Mobile Charge Q_{ot}: Oxide Trapped Charge
Transition Region	Q_f: Fixed Oxide Charge
Silicon	Q_{it}: Interface Trapped Charge

Figure 6. Illustration of Oxide Charge

Amorphous SiO₂, dangling bonds at oxide interface, transition region between silicon and oxide, and sodium ion contamination while performing thermal growth introduce four types of oxide charges. Under well controlled industry environment, total amount of oxide charge is generally,

$$Q_T = Q_m + Q_{ot} + Q_f + Q_{it} \cong 10^{10} \text{ C/cm}^{-2}$$

However, under lab environment, Q_T can be increased up to $\sim 10^{12} \text{ C/cm}^{-2}$.

Another consideration of device modeling is external lumped impedance element which is caused by the self-impedance of proving point, interfacial impedance, layout design, and the resistance and inductance of pad which is connected to source and drain [24]. This is shown in Figure 7.

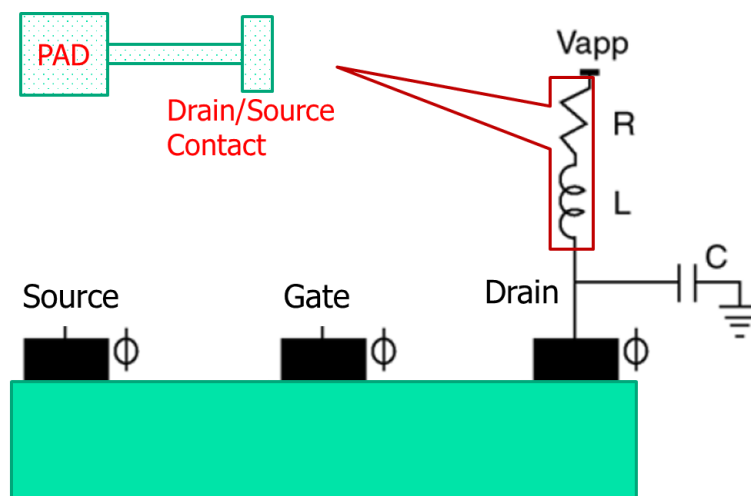


Figure 7. External Lumped Impedance Modeling

The external lumped impedance is measured from comparing the bulk resistance of organic semiconductor to the resistance of bulk organic semiconductor plus metal pads. The modeled parameters for oxide charge and external lumped impedance are listed in Table 3.

Table 3. Modeled Parameters of External Elements

Fitting Parameter	Value	Variation
Q_T	$10^{12} \text{ C/cm}^{-2}$	$\pm 20\%$
R_C	10 k Ω	-

Validation of Physics Models by Simulations of OTFT Devices

In this step, by combining all of the modeled physics above into the device structure, simulating the device and comparing the simulation results to experiment results, it is shown that modeling of each physics is valid. To make our further simulations for new designed devices confident, all the validated material parameters must be included before proceeding device design based on simulations. In validation step, experiment results shown in other papers are reproduced by simulation. The devices we simulate in this step are categorized into long channel, short channel, highly crystallized small molecule, and disordered polymer. It is assumed that the density of organic defects and constant mobility can be changed depending on organic film. Other parameters are kept as same to obtain most accurate simulation results from our own design.

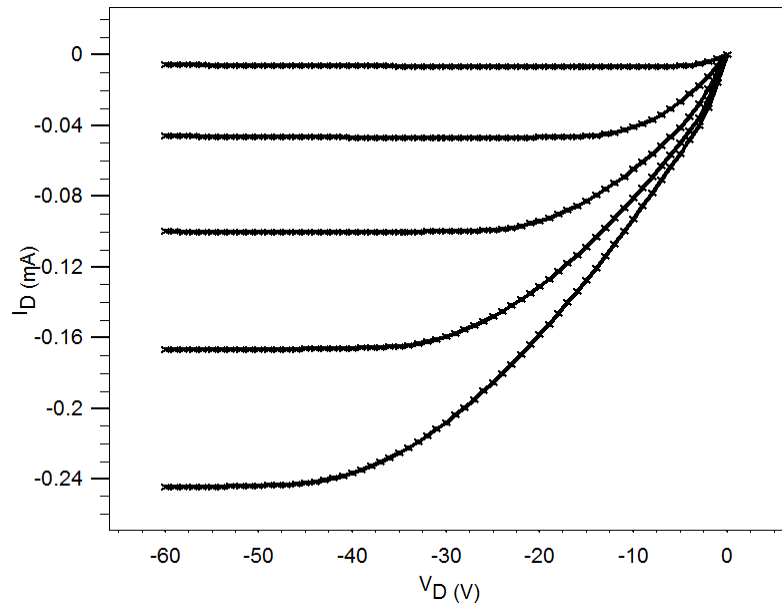
Figure 8 and Figure 9 are the case of long channel devices and highly crystallized organic semiconductor in [18]. [18] reports the average carrier mobility of these devices is $\sim 5 \text{ cm}^2/(\text{Vs})$ and the highest is up to $\sim 10 \text{ cm}^2/(\text{Vs})$. As stated previously, the constant mobility is adjusted to $0.7 \text{ cm}^2/(\text{Vs})$ to achieve $5 \text{ cm}^2/(\text{Vs})$ of the saturation mobility with Pasveer enhancement factor. The simulation results agree with the experiment results quite accurately.

The second category of verification is the case of short channel devices with highly disordered organic material. To model this case, the density of traps is increased and the width of Gaussian density. In addition to the trap density, the constant mobility parameter is substituted with $0.001 \text{ cm}^2/(\text{Vs})$. Figure 10, Figure 11, and Figure 12 are the

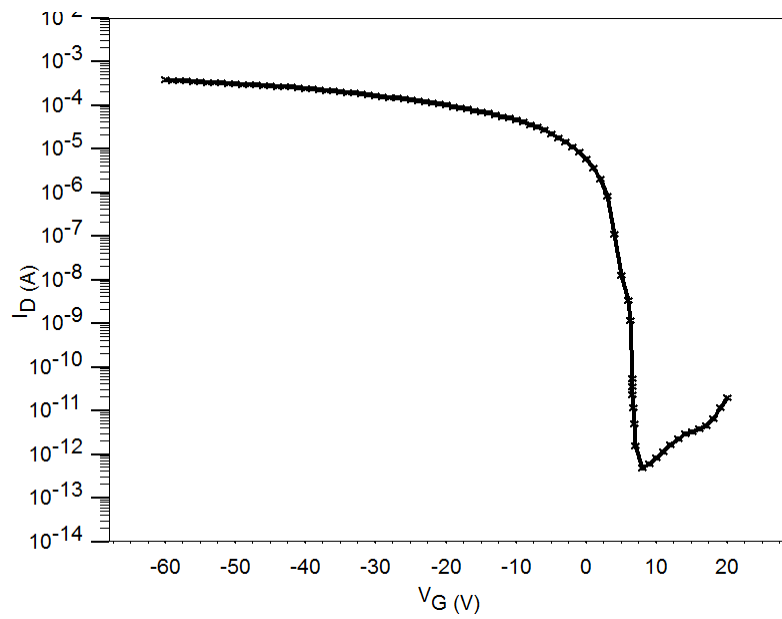
simulation results of short channel and disordered material. As the channel length becomes shorter near hundreds of nanometers, the simulation results deviate more from the experiment results reported in [19], although the current level is still in the same order and the current voltage behavior fits very well. This is possibly due to the poorly modeled short channel effect in OTFT and the lack of information how they measured device. For instance, in [19], the author claimed that the gate leakage current is about 2pA with 5nm thickness of gate oxide. This is almost impossible without using high-k dielectric even in modern silicon devices. Furthermore, in our study, the extremely short channel devices which are in the range of 100nm are not used.

In addition to the measured DC characteristics, AC simulations are also conducted for the device which has the experiment result of AC response to obtain complete device performance results. From the oscillating frequency of ring oscillator in [18], the cutoff frequency can be extracted by calculation. AC and transient response simulations are shown in Figure 13 and Figure 14.

The simulation results are summarized in Table 4 and Table 5 and the results show that these material parameters and modeled physics are valid for our device simulations.

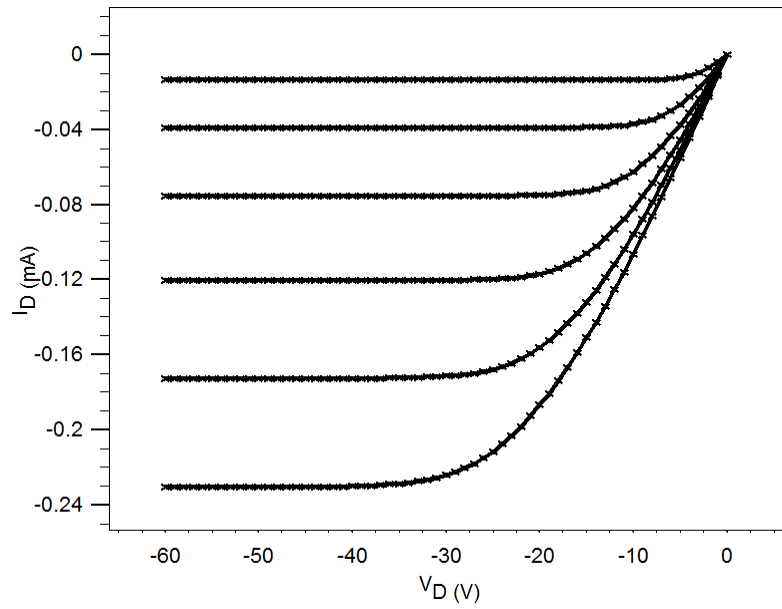


(a) Output Curves

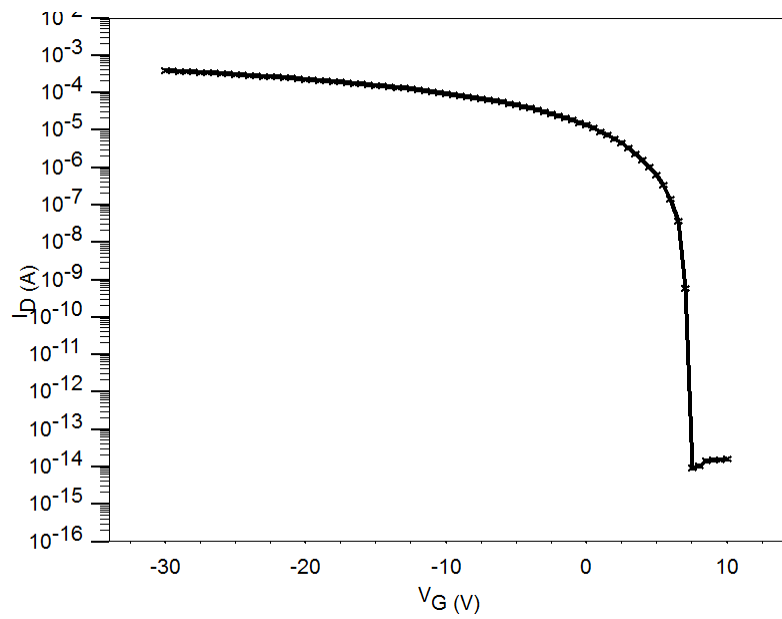


(b) Transfer Curve

Figure 8. 125 μ m Long-Channel OTFT Device DC Characteristics

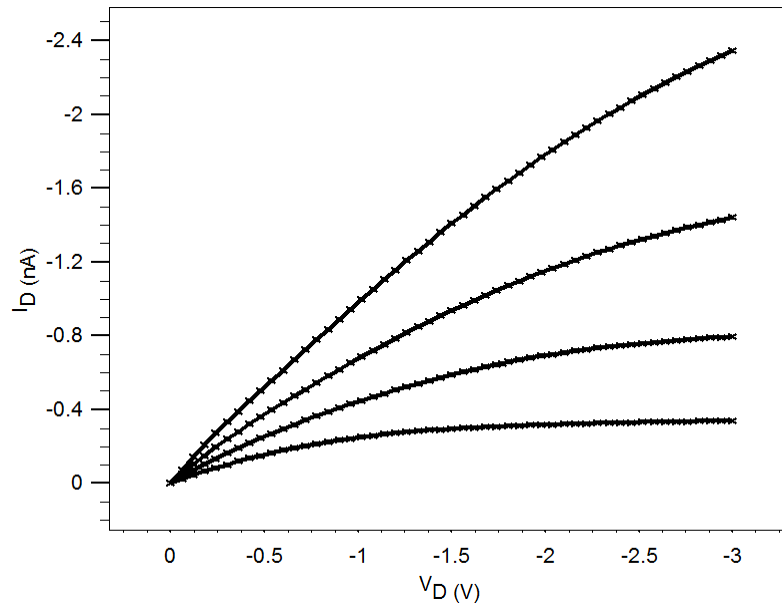


(a) Output Curves

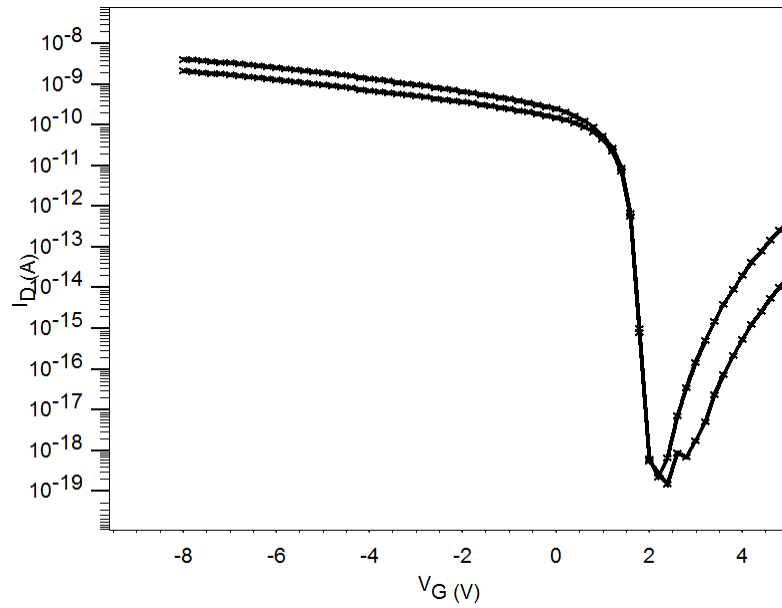


(b) Transfer Curve

Figure 9. 50 μ m Long-Channel OTFT Device DC Characteristics

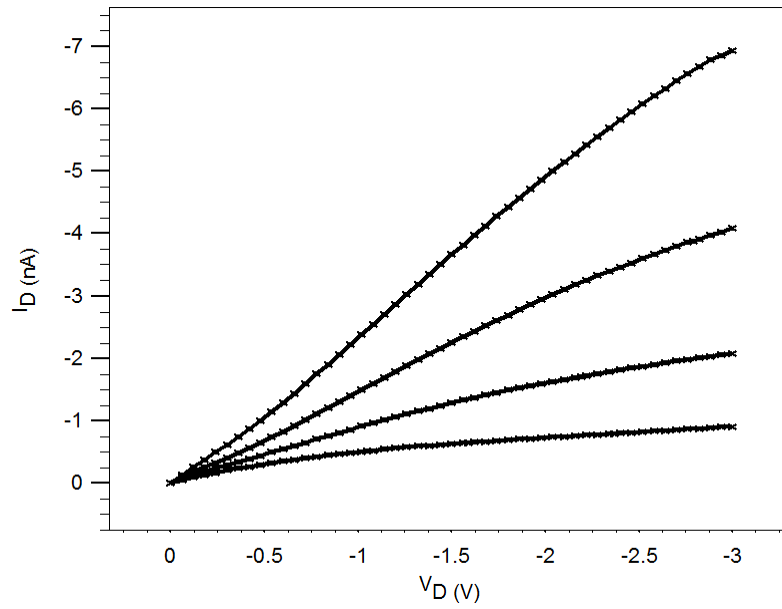


(a) Output Curves

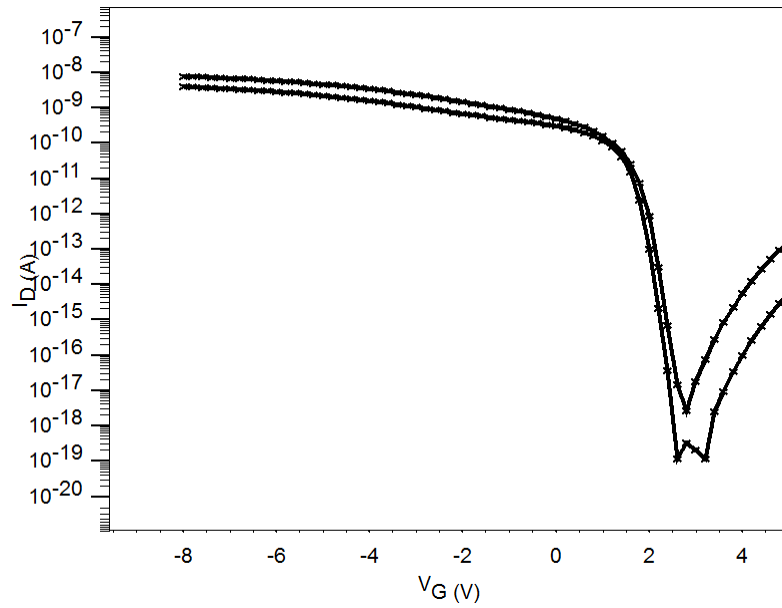


(b) Transfer Curves

Figure 10. $1\mu\text{m}$ Short-Channel OTFT Device DC Characteristics

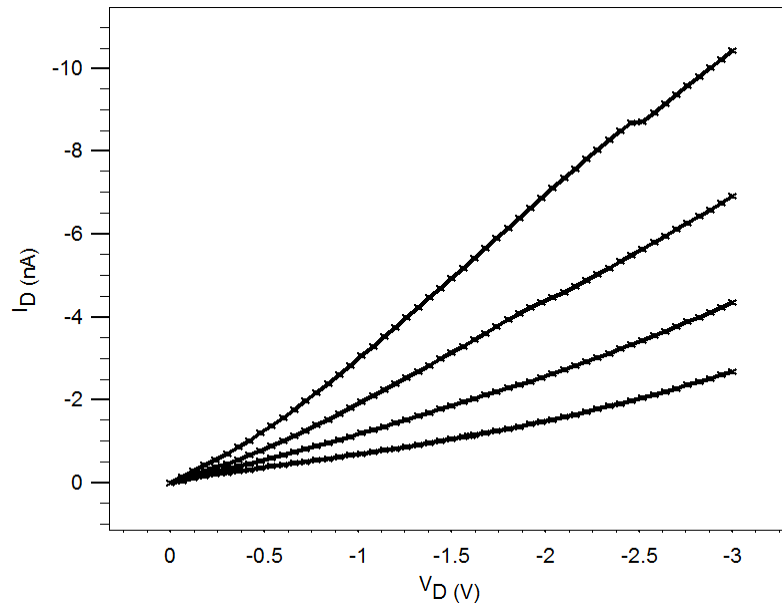


(a) Output Curves

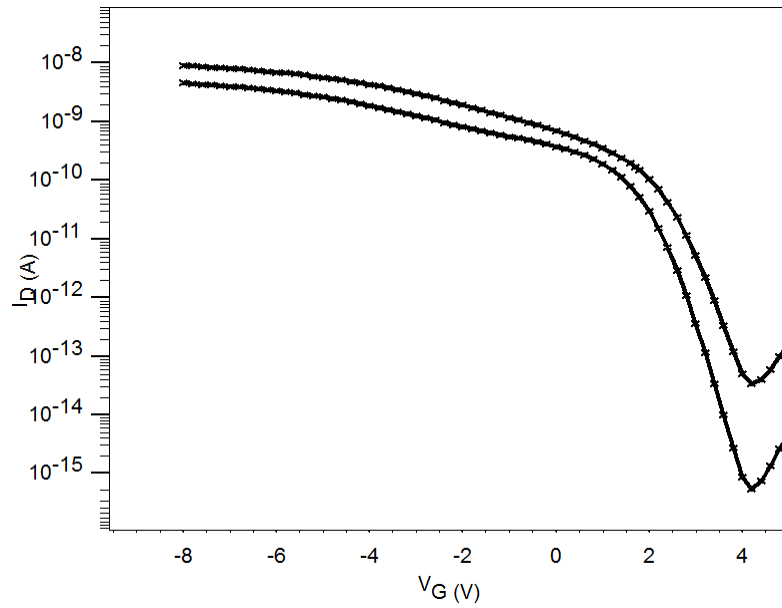


(b) Transfer Curves

Figure 11. 200nm Short-Channel OTFT Device DC Characteristics

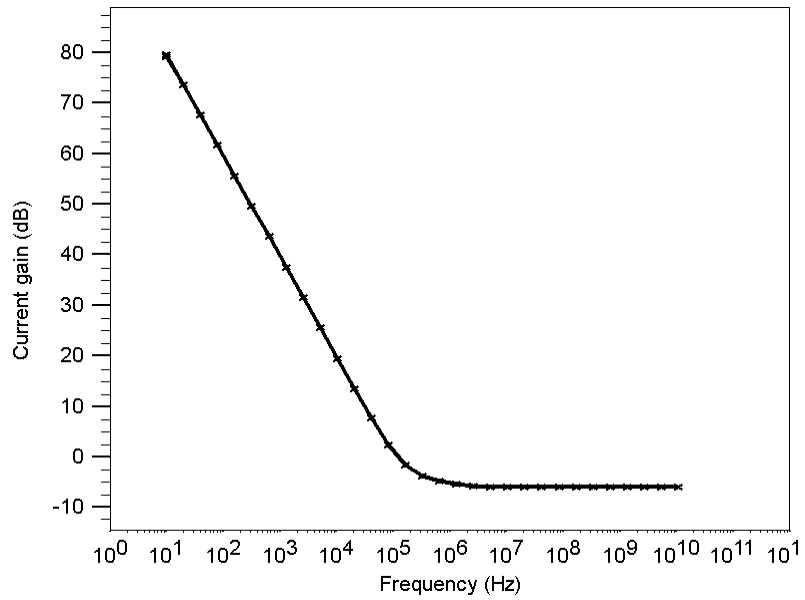


(a) Output Curves

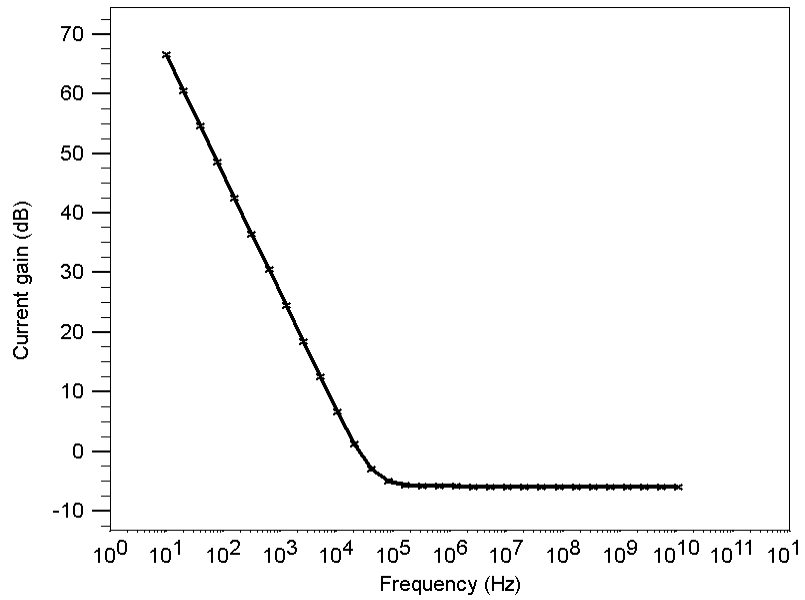


(b) Transfer Curves

Figure 12. 70nm Short-Channel OTFT Device DC Characteristics

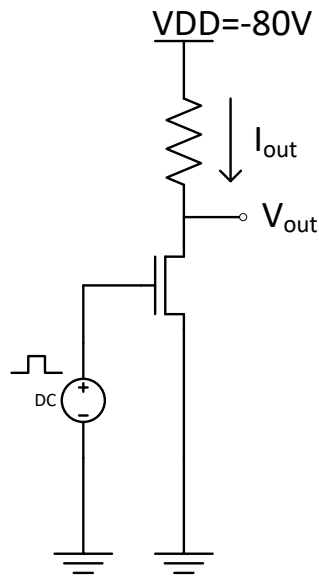


(a) Short Circuit Current Gain Vs. Frequency, 125µm Channel Length

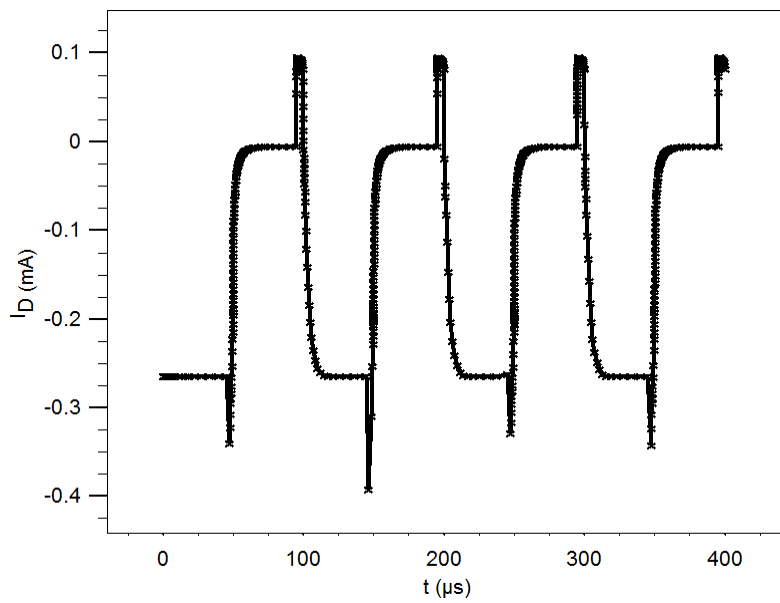


(b) Short Circuit Current Gain Vs. Frequency, 50µm Channel Length

Figure 13. AC Response of 125µm and 50µm OTFT

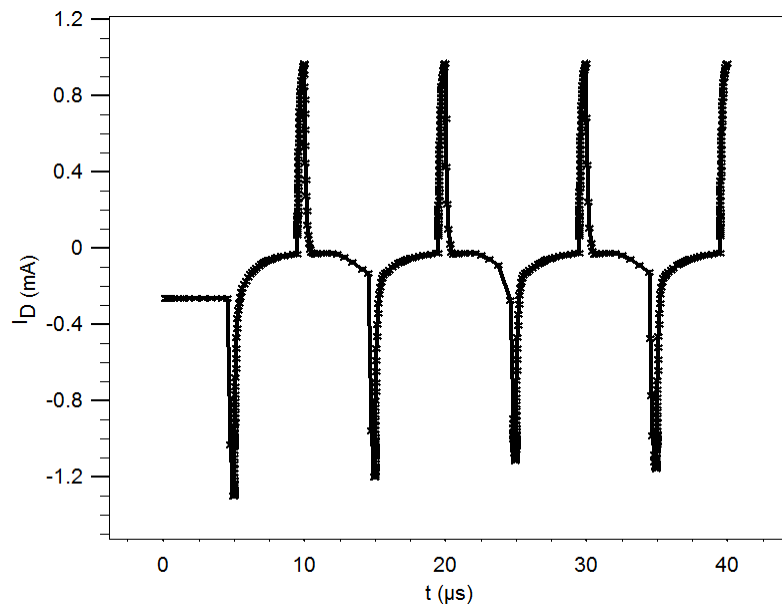


(a) PMOS Inverter to Validate Transient Response



(b) Output Signal of (a) with 10kHz Input Pulse

Figure 14. Transient Response of 50 μ m OTFT



(c) Output Signal of (a) with 100kHz Input Pulse

Figure 14. Continued

CHAPTER III

DEVICE DESIGN, SIMULATION, AND EXPERIMENT

In this chapter, based on the issues of performance bottleneck which are stated previously, three new designed organic transistors are simulated and fabricated. New designing is involved to: 1) reduce the injection barrier between metal and organic, hence improve current injection, 2) increase the carrier mobility in the organic region where the channel is formed, and 3) reduce unwanted parasitic elements. Each transistor device designed has two or more of enhancing schemes.

Organic Metal Semiconductor Field Effect Transistor(OMESFET)

Unlike MOSFET or TFT structures, the important feature of MESFET structure is that the gate insulator does not exist. In other words, there must be a potential barrier to prevent gate leakage current when gate is zero biased or slightly forward biased. It is a simply Schottky barrier to prevent the unwanted gate leakage current [14], [15].

Consequently, the certain amount of gate leakage current exists even with zero gate bias due to the behavior of carriers at gate interface. Under any bias condition of normal MESFET operation, gate is never forward biased and therefore the current induced by thermionic emission only exist. Since there is a limited choice of metals for gate electrode, the current flow into the gate by thermionic emission can be controlled weakly. Although MESFET operates with much smaller voltage range than MOSFET, the carrier mobility of organic material is very low, the operating voltage can be inevitably up to

tens of volts which can contribute tunneling current specially when the size of device small. Another reason of taking the gate current into the design consideration is that on-current of MESFET is technically same with off-current of MOSFET. That is, even the small amount of gate current is possibly significant compared to the on-current of MESFET. These drawbacks were the motivations to design and suggest the new MESFET structure.

MESFET is usually on without the gate bias voltage and is turned off when a bias voltage is applied to the gate. The depletion region under the gate must extend over the complete thickness of the semiconductor layer to turn off the device. Under zero gate bias, the semiconductor film thickness must be larger than the depletion region thickness to form a conduction path between the source and the drain electrodes. Based on the property of organic material, pentacene is weak P-type without doping, and the conducting path of the channel in MESFET is electrically neutral. In this case, the equations of depletion width and the resistance of the conduction channel are derived as [25], [26]

$$d(x) = \sqrt{\frac{2\epsilon_s [V(x) + V_{bi} - V_g]}{qN_a}} \quad (8)$$

$$dR = \frac{dx}{q\mu N_a W [t - d(x)]} \quad (9)$$

Where N_a is the acceptor concentration, t is the thickness of the channel, V_{bi} is the built-in potential of the Schottky gate contact, and W is the channel width. After substituting above equations into $dV = IdR$, the current equation is derived by integrating the following equation:

$$dV = I_d dR = I_d \frac{dx}{q\mu N_a W[t - d(x)]} \quad (10)$$

Then, the drain currents are expressed as following for saturation and triode regions [14], [15]:

$$I_d = q\mu\mu_a \frac{Wt}{L} \left(V_d - \frac{2}{3} \frac{[V_d + V_{bi} - V_g]^{3/2} - [V_{bi} - V_g]^{3/2}}{V_p^{1/2}} \right) \quad (11)$$

$$I_{d.sat} = q\mu\mu_a \frac{Wt}{L} \left(\frac{V_p}{L} + \frac{2[V_{bi} - V_g]^{3/2}}{3V_p^{1/2}} - V_{bi} + V_g \right) \quad (12)$$

In equation (11) and (12), V_p is the gate voltage that makes the channel completely depleted. The voltage is called pinch-off voltage similarly as the case of MOSFET. Note that the current boundary condition of Schottky barrier is not included in (8)-(12) and constant mobility is used instead of complete Pasveer mobility. According to (12), the rough calculation of saturation current is $\sim 0.1 \mu\text{A}$ with 100 of W to L ratio. The current will be even lowered when Schottky contact boundary condition is included in the equation. This low current cancels out the inherent advantages of MESFET device and eventually the performance of organic MESFET is not much better than organic TFT. However, our simulation study shows that the performance of organic MESFET is greatly improved with a little modification of MESFET structure. The idea of improving organic MESFET is using the doped thin layer as a conducting path of channel below depletion region formed by gate built-in potential. Figure 15 shows the both structures of normal MESFET, dual layer MESFET, and derived compact model scheme [27]. In dual layer MESFET, the acceptor concentration is increased effectively,

$$N_{A,eff} = \frac{N_A(t-d(x)) + N_{A,d}t_d}{(t-d(x)) + t_d} \quad (13)$$

Where $N_{A,d}$ is the acceptor concentration of doped layer and t_d is the thickness of channel formed in doped layer. If it is assumed that the most part of depletion region occurs in undoped layer when device is turned on, then the on-current of the device is also increased to

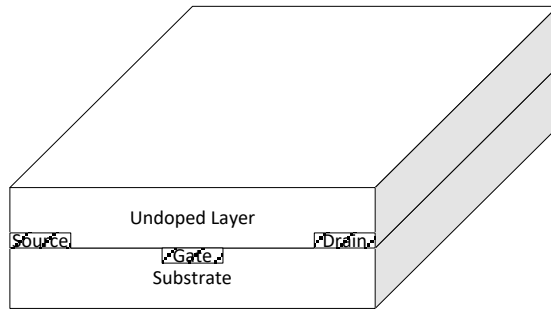
$$I_{d,DL} \cong I_d \cdot \frac{N_{A,d}}{N_A} \cdot g_1(T, n) \quad (14)$$

In equation (14), the mobility enhancement factor of carrier concentration dependency is also included. The adding the doped layer, in turn, inevitably increase the threshold voltage. The equation (15) is the expression of the threshold voltage for single layer regular MESFET device, and (16) is derived for suggested dual layer MESFET device.

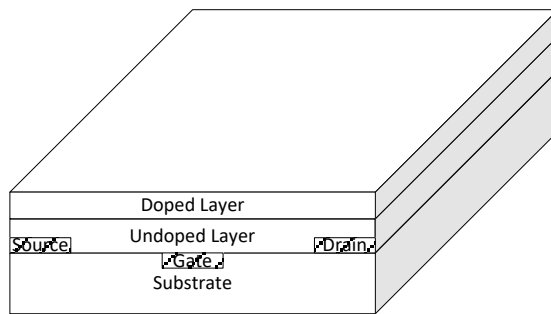
$$V_T = V_{bi} - \frac{t^2 \cdot q \cdot N_A}{2\epsilon_s} \quad (15)$$

$$V_T = V_{bi} - \frac{(t+t_d) \cdot q \cdot (N_A \cdot t + N_{A,d} \cdot t_d)}{2\epsilon_s} \quad (16)$$

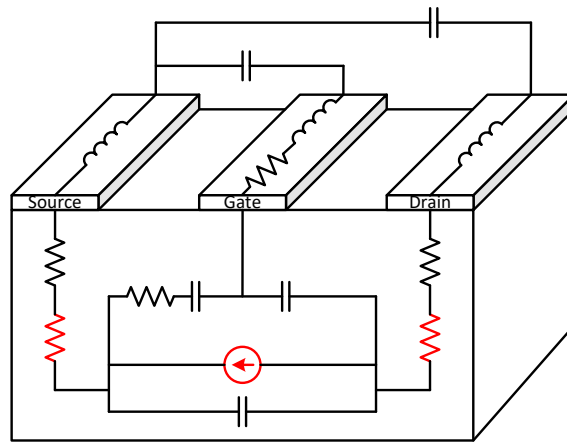
By examining the both of equations, it can be known that the threshold voltage shift can be minimized. To evaluate the complete current continuity equations and obtain solutions, Silvaco ATLAS TCAD is used for simulation study.



(a) Normal MESFET Structure



(b) Suggested Dual-Layer MESFET Structure



(c) Compact Model of MESFET

Figure 15. The Structure and Compact Model of OMESFET

The output curves are shown in Figure 16 and the transfer curves are shown in Figure 17 for both of single layer MESFET and dual-layer MESFET. As shown, dual-layer MESFET has much higher on-current than single layer MESFET. Of course, the high current level comes with the price. It trades the high current level off higher V_p , which means it needs higher voltage to completely deplete the region below gate electrode since the Fermi level moved down toward valence band in doped thin organic layer. However, optimized thickness and doping concentration of doped layer can be minimized the increment of V_p . Fig. 16 clearly indicate that the threshold voltage shifts only about $\sim 2.8V$ whereas the saturation current is increased by ~ 50 times. Even only for the aspect of DC performance, the dual-layer organic MESFET is superior to the single layer organic MESFET.

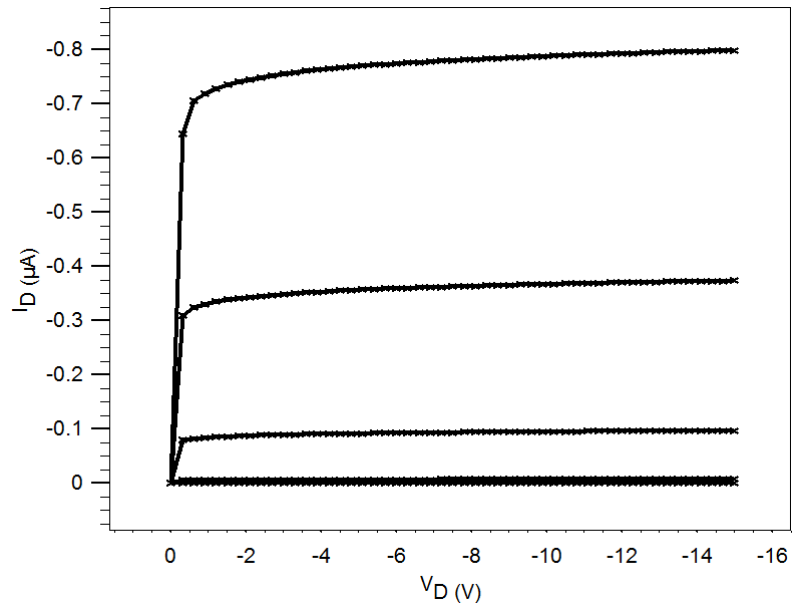
In spite of the fact that superior DC performance of device also indicate the device can operate at higher frequency, the AC performance of devices are often determined by inherited and parasitic component including such as overlap capacitance, depletion capacitance, resistance of depleted region at the end of channel, and etc. In [18], the ring oscillator was demonstrated and its oscillating frequency was only a few kHz even with remarkably high DC performance OTFTs. This evidently indicate that the structure of device is very important even when devices are the same types. In this section, it is shown that how using dual-layer structure improves the AC performance by simulations. It can be a possible candidate for low frequency range RFID tags which use 13 MHz frequency signal [20] with fully organic based devices.

To calculate the short circuit current gain of the devices, S-parameters is obtained from simulation first, and the values of S-parameters at each frequency point are substituted in the equation of

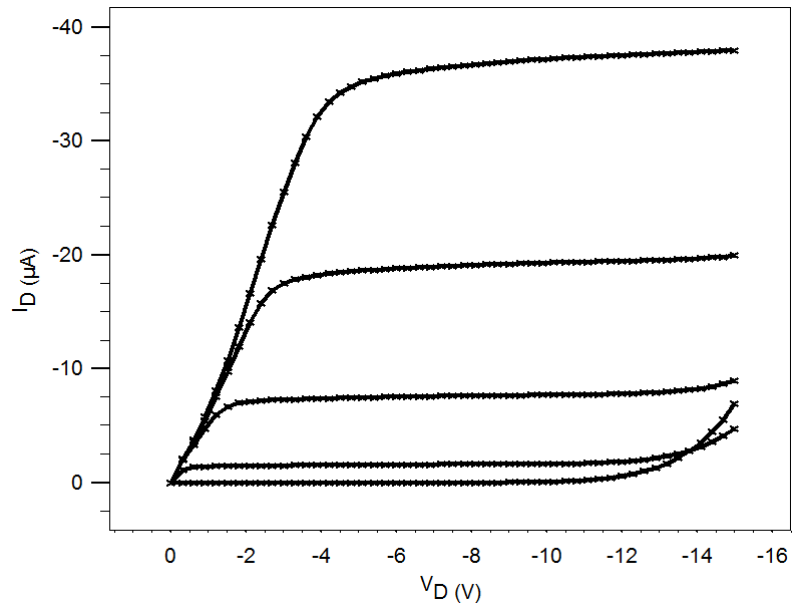
$$H_{21} = 20 \log_{10} \left| \frac{-2|S_{21}|^2}{(1 - S_{11})(1 + S_{22}) + S_{21}S_{12}} \right| \quad (17)$$

The frequency at which (17) is equal to zero is called the unity gain cutoff frequency since the magnitude of output current is same with input current. In our simulations, only common source figure, which is most commonly used, is investigated. The source electrode of the device is set as the common ground, the gate as the input, and the drain as the output. The calculated short-circuit current gains are plotted in Figure 18.

Suggested MESFET structure reaches up to 50 MHz of cutoff frequency with 10 μ m channel length. This dimension size is easily realized under any lab environment, and with any method of organic processing. It is known that the channel length of OTFT must be less 200nm and the patterned gate electrode is needed instead of using common gate for OTFT to reach around ~10MHz cut off frequency [3]. Furthermore, in order to build the OTFT device with those features, complicated processing methods, such as shadow masking, are required [3].

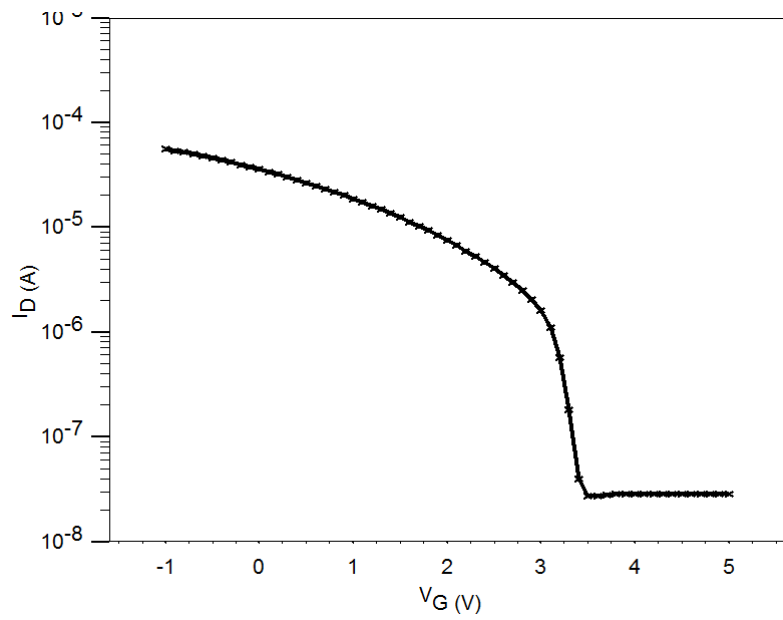


(a) Single Layer Organic MESFET

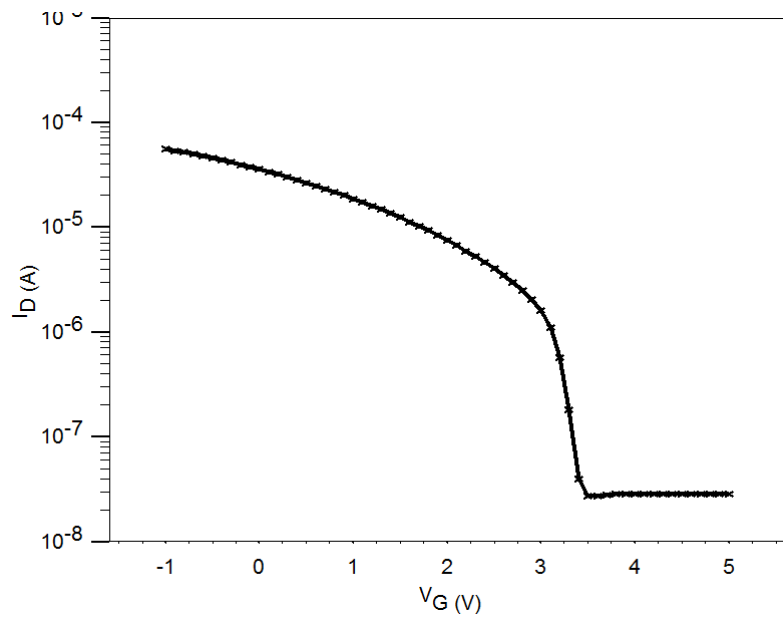


(b) Dual Layer Organic MESFET

Figure 16. Output Characteristics of Single and Dual Layer OMESFET

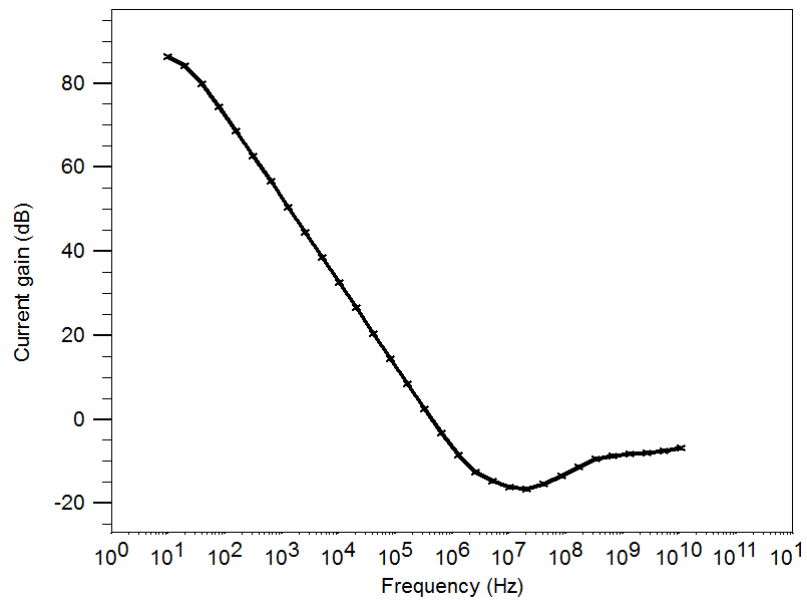


(a) Single Layer Organic MESFET

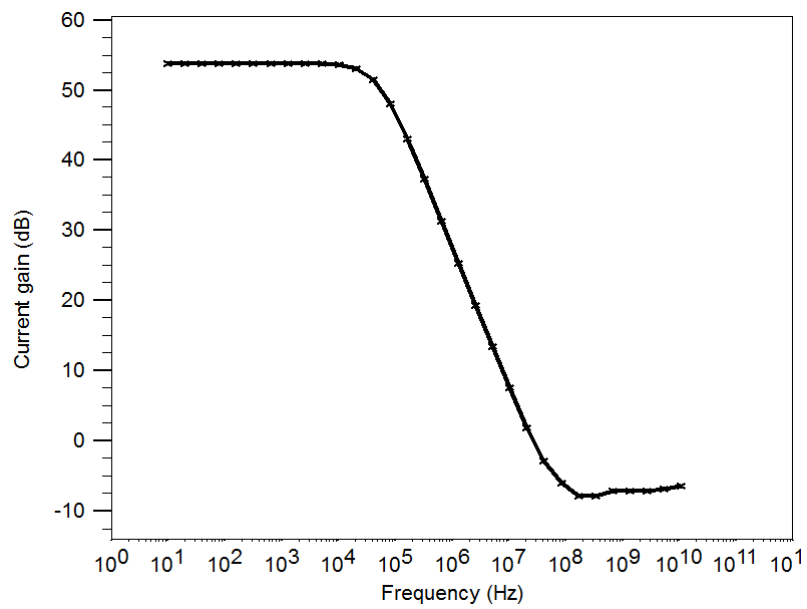


(b) Dual Layer Organic MESFET

Figure 17. Transfer Characteristics of Single and Dual Layer OMESFET



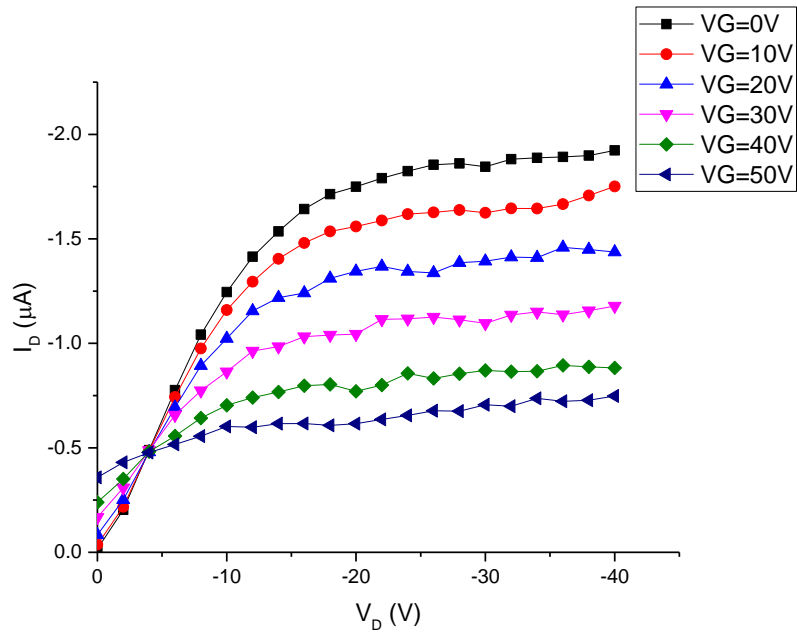
(a) Single Layer Organic MESFET



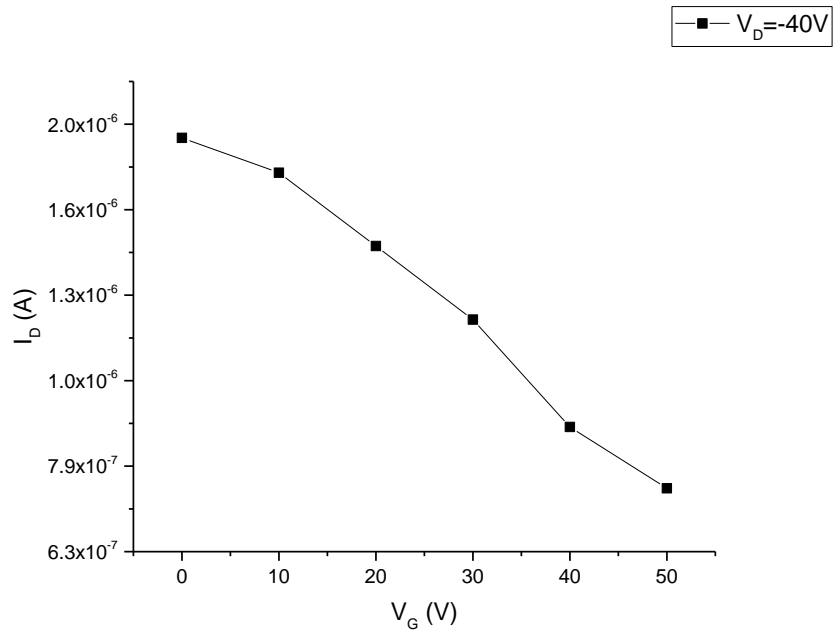
(b) Dual Layer Organic MESFET

Figure 18. AC Response of Single and Dual Layer OMESFET

Despite of outperforming characteristics of dual-layer OMESFET, the fabricated OMESFETs have degraded performance as shown in Figure 19. As gate bias voltage become larger, the greater gate leakage current flows into gate electrode instead of that the device is turned off. Since the gate leakage current is steady not quadratic over the range of drain voltage, it is expected that the leakage current is mainly due to the thermionic emission rather than Schottky tunneling. In fact, the gate leakage current could be reproduced by simulations with the increased value of gate workfunction from 4.1eV to 4.6eV and the reduced value of effective hole mass from 3 to 2. Evidently, aluminum gate metal is damaged during the process of fabrication. The re-fitting simulation results are shown in Figure 20.

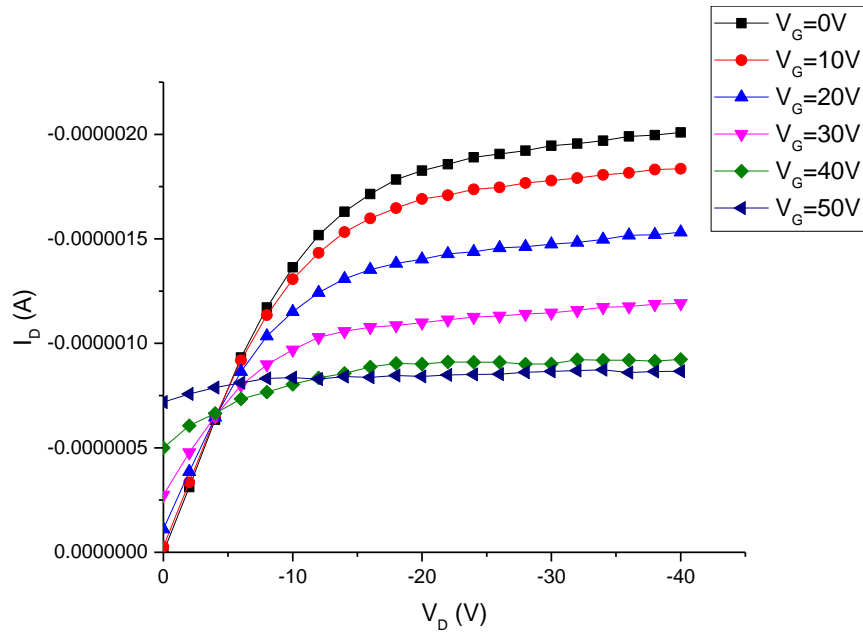


(a) Single Layer MESFET: Output Curves

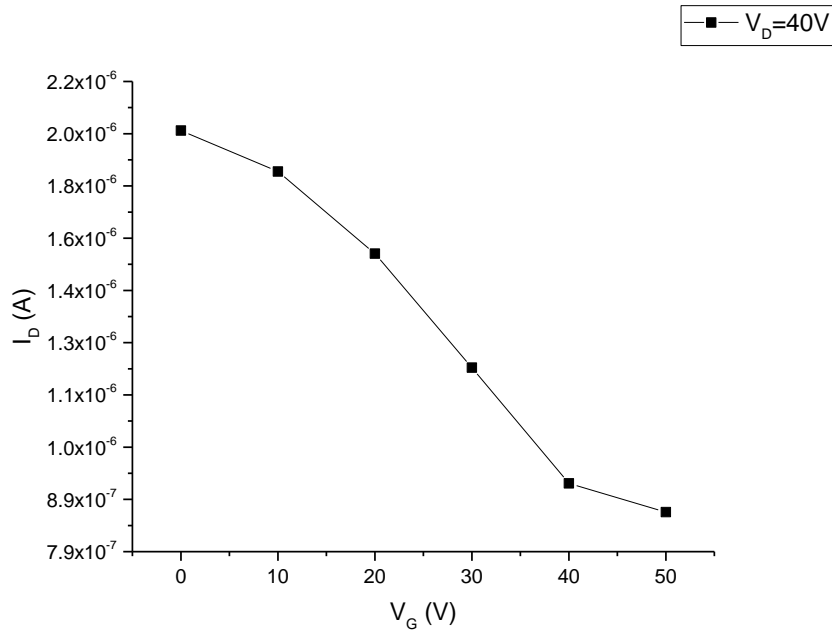


(b) Single Layer MESFET: Transfer Curve

Figure 19. DC Characteristics of OMESFET Experiment Results

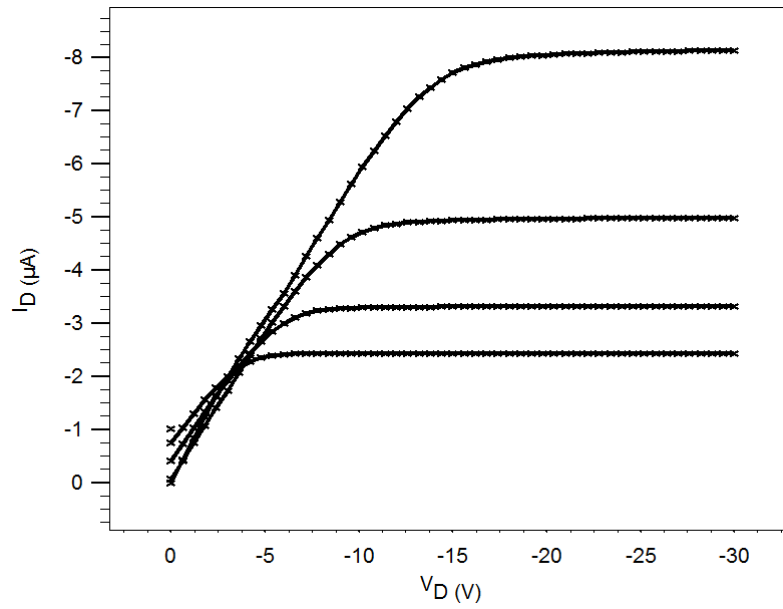


(c) Dual Layer MESFET: Output Curves

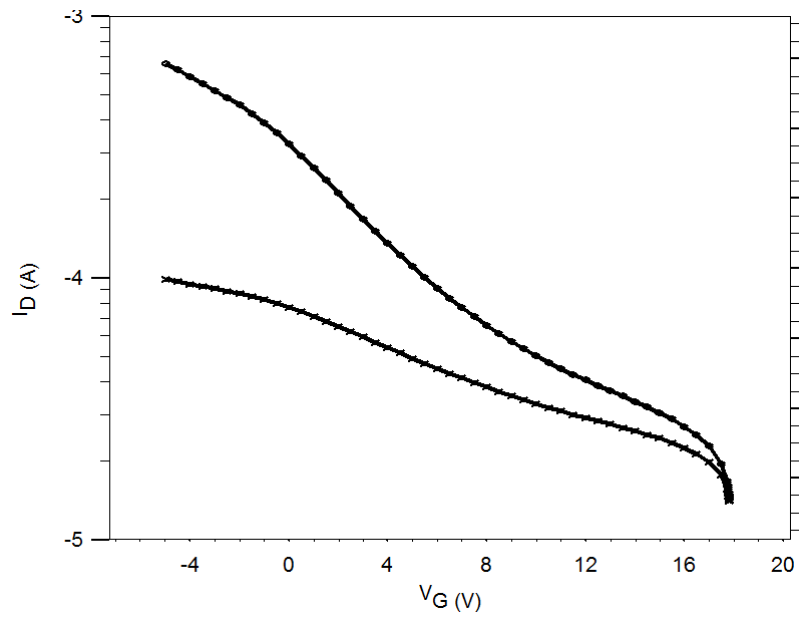


(d) Dual Layer MESFET: Transfer Curves

Figure 19. Continued

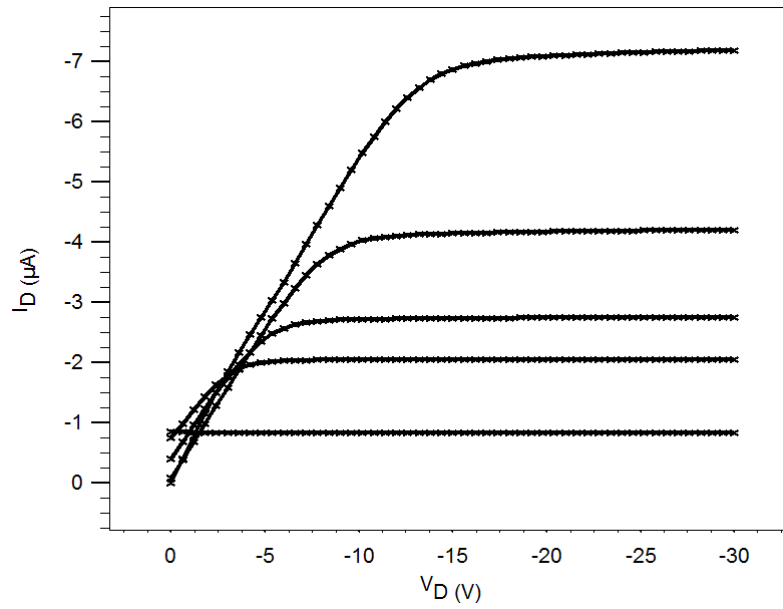


(a) Single Layer MESFET: Output Curves

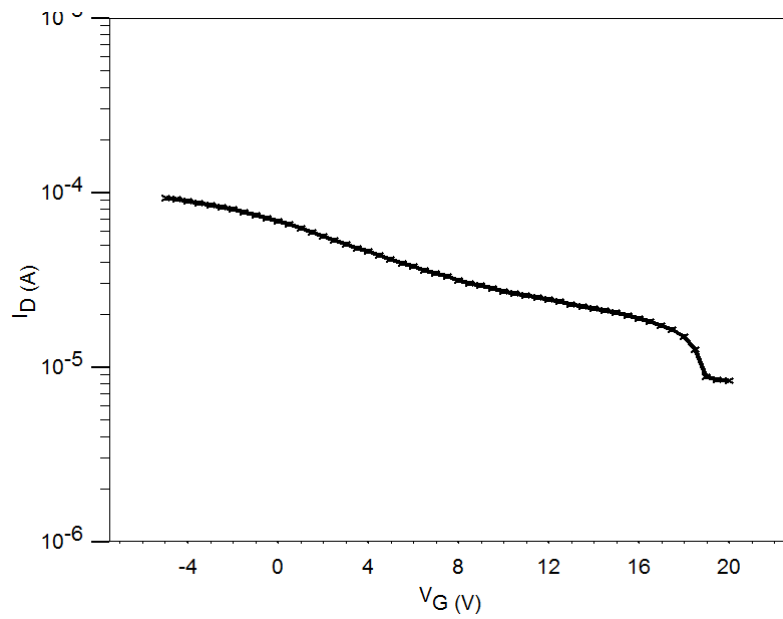


(b) Single Layer MESFET: Transfer Curves

Figure 20. The Results of Re-Fitting Simulations



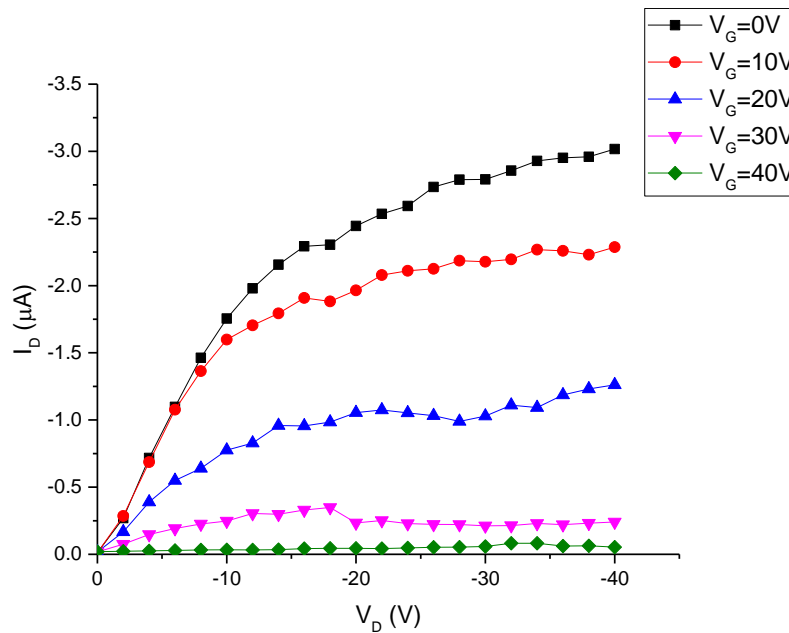
(c) Dual Layer MESFET: Output Curves



(d) Dual Layer MESFET: Transfer Curves

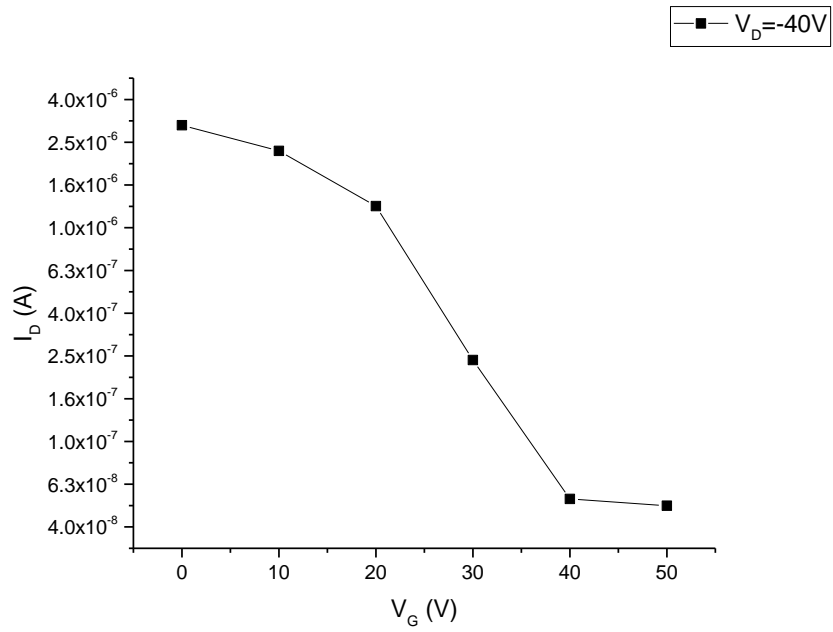
Figure 20. Continued

By increasing the thickness of aluminum gate, to minimize the effect of damaging, and after several tries with handling the device very carefully during the process, OMESFET without gate leakage current could be fabricated. In Figure 21, the DC characteristics of OMESFET indicate that off-current is still significant and it may limit the application of device only to analog circuits. The results of OMESFET simulations and experiments are summarized in Table 6.

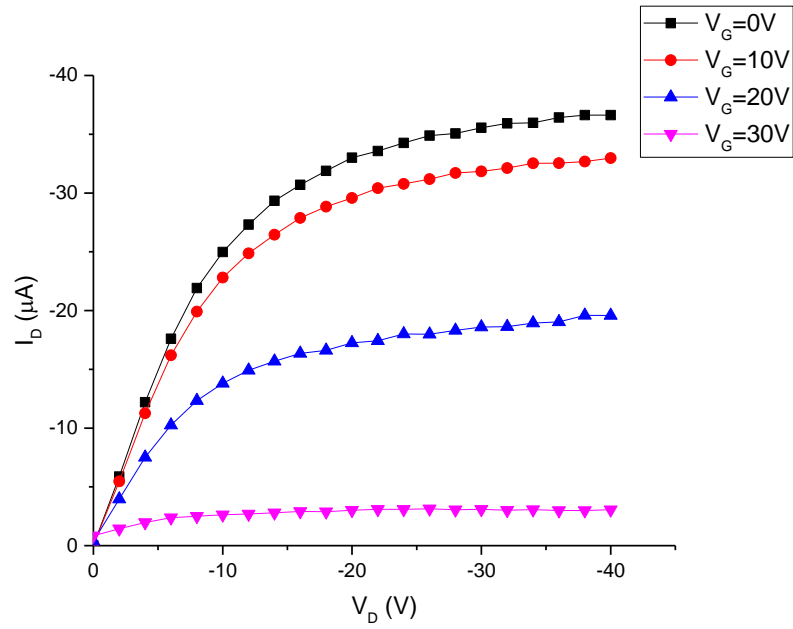


(a) Single Layer MESFET: Output Curves

Figure 21. DC Characteristics of OMESFET Experiments after Optimization

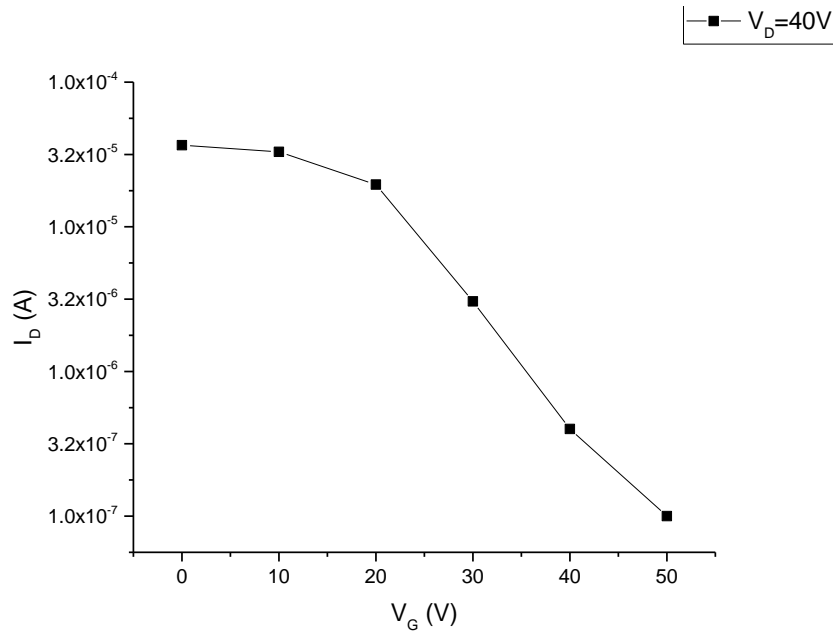


(b) Single Layer MESFET: Transfer Curve



(c) Dual Layer MESFET: Output Curves

Figure 21. Continued



(d) Dual Layer MESFET: Transfer Curve

Figure 21. Continued

Depletion Mode Organic Thin Film Transistor(OTFT)

Depletion mode MOSFET is commonly used in silicon technology due to the high speed of device, less power consumption, and smaller flicker noise performance [28], [29]. These advantages of silicon device remain intact in organic devices.

Moreover, the issues which cause the poor performance of organic transistors are resolved by doping the channel region. As stated previously, these issues are 1) high injection barrier at metal/organic interface, 2) charge trapping by organic defect sites, and 3) low carrier mobility. Adding P-type dopants in the channel region lower the

Fermi level toward valence band, hence the width of Schottky barrier becomes very narrow and charge injection is facilitated [30]-[33]. Also, the increased number of holes from dopants fill out the trap sites residing in organic layer and more free carriers exist without trapping [34], [35]. Consequently, the increased number of free carrier concentration enhances the carrier mobility by concentration dependent mobility factor, μ_0 .

As similar as OMESFET, the depletion mode OTFT is usually on without the gate bias voltage and is turned off when a positive bias voltage is applied to the gate of p-type transistor. However, unlike OMESFET, the depletion mode OTFT is possible to be biased with a negative voltage to gate electrode since organic layer is insulated by dielectric. In this way of gate biasing, even more holes are accumulated in the channel and higher current level can be reached. This possible bias conditions give more options to choose in which mode the device operates; complete accumulation mode, depletion mode, normal depletion mode, and depletion mode with surface inversion. If the device has a heavily doped and thicker channel below gate metal, then the thickness of conducting channel is greater than the maximum thickness of depletion layer. In this case, the transistor never reaches pinch-off condition, and it is hard or impossible to turn off the device. This type of devices is called Type-B depletion mode MOSFET while Type-A depletion mode MOSFET has lightly doped channel [28]. One strategy of increasing the maximum thickness of depletion layer under the channel is depositing intrinsic organic layer to form a P⁺-I junction. First, considering single layer of depletion

OTFT, the equations of depletion width and the resistance of the conduction channel are derived similarly as OMESFET,

$$d(x) = \frac{C_i[V_g + V(x) - V_{bi}]}{qN_a} \quad (18)$$

$$dR = \frac{dx}{q\mu N_a W[t - d(x)]} \quad (19)$$

Where N_a is the acceptor concentration, t is the thickness of the channel, V_{bi} is the built-in potential formed by Fermi level difference between gate electrode and organic layer, and W is the channel width. For Equation (18), the square root term disappeared from Equation (8) since the gate insulator exist in depletion mode OTFT. After substituting above equations into $dV=IdR$ again, the current equation is derived by integrating the following equation:

$$dV = I_d dR = I_d \frac{dx}{q\mu N_a W[t - d(x)]} \quad (20)$$

Then, the drain currents are expressed as following for saturation and triode regions [26]:

$$I_d = \mu C_i \frac{W}{L} \frac{n}{N_a} \left[(V_T - V_g) V_d - \frac{1}{2} V_d^2 \right] \quad (21)$$

$$I_{d.sat} = \frac{1}{2} \mu C_i \frac{W}{L} \frac{n}{N_a} (V_T - V_g)^2 \quad (22)$$

In equation (21) and (22), V_T is pinch-off or threshold voltage which makes the thickness of depletion region same as the thickness of conducting channel. For the simplicity of deriving equation, Schottky contact boundary condition of source and drain

contacts are excluded. Adding the enough dopants in the channel region make the number of free carriers n almost same with N_a . However, if the doping concentration is too high then, the pinch-off voltage V_p becomes large and device starts to behave as resistor rather than transistor. Assuming that the doping concentration is high enough only to fill out the traps of organic film, but not high enough to make the transistor as resistor, then Equation (21) and (22) become,

$$I_d = \mu g_l(T, n) C_i \frac{W}{L} \left[(V_T - V_g) V_d - \frac{I}{2} V_d^2 \right] \quad (23)$$

$$I_{d.sat} = \frac{I}{2} \mu g_l(T, n) C_i \frac{W}{L} (V_T - V_g)^2 \quad (24)$$

It indicates that the higher current level can be achieved by both of the mobility enhancement factors of carrier concentration dependency and reduced trap sites. Nevertheless, another DC performance of device is degraded because the pinch-off voltage increases, so that the device becomes difficult to be turned off even with very large gate voltage resulting in low on-off current ratio. Equation (25) gives the explanation of this.

$$V_T = \frac{t \cdot q \cdot N_A}{C_i} - V_{bi} \quad (25)$$

To minimize the increment of pinch-off voltage, only thin layer right underneath the channel is doped while the second organic layer remains intrinsic as shown in Figure 22.

Now, the effective doping concentration becomes

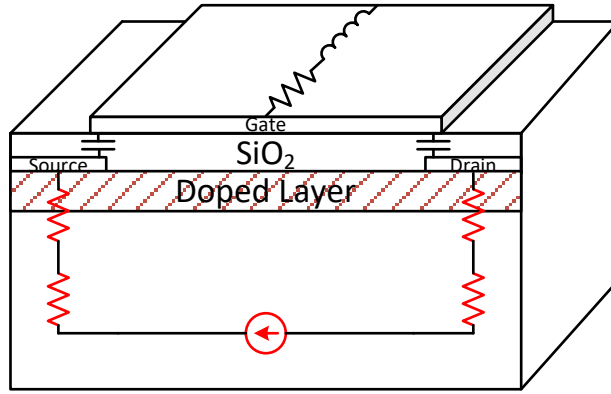


Figure 22. The Structure of Depletion Mode OTFT and Compact Model

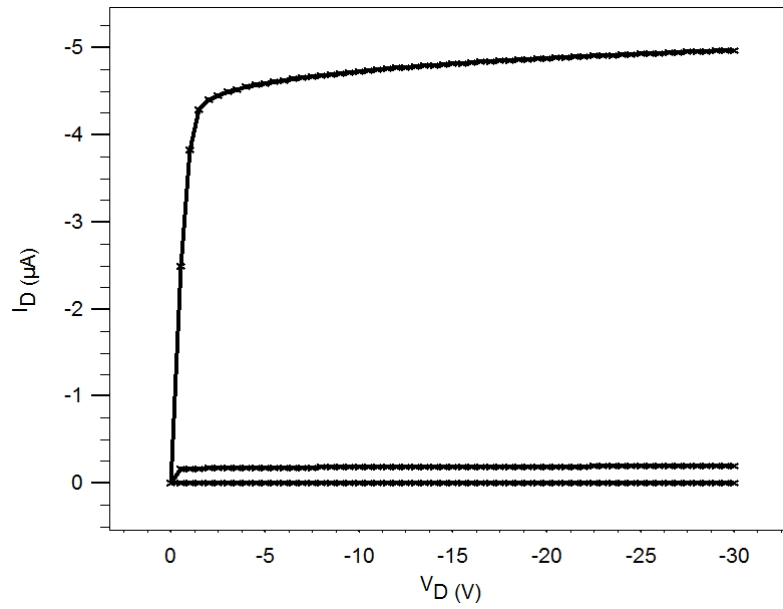
$$N_{A,eff} = \frac{N_A(t - d(x)) + N_{A,d}t_d}{(t - d(x)) + t_d} \quad (26)$$

Where $N_{A,d}$ is the acceptor concentration of doped layer and t_d is the thickness of channel formed in doped layer. Equation (26) is substitute in Equation (25) and the new equation of pinch-off voltage is

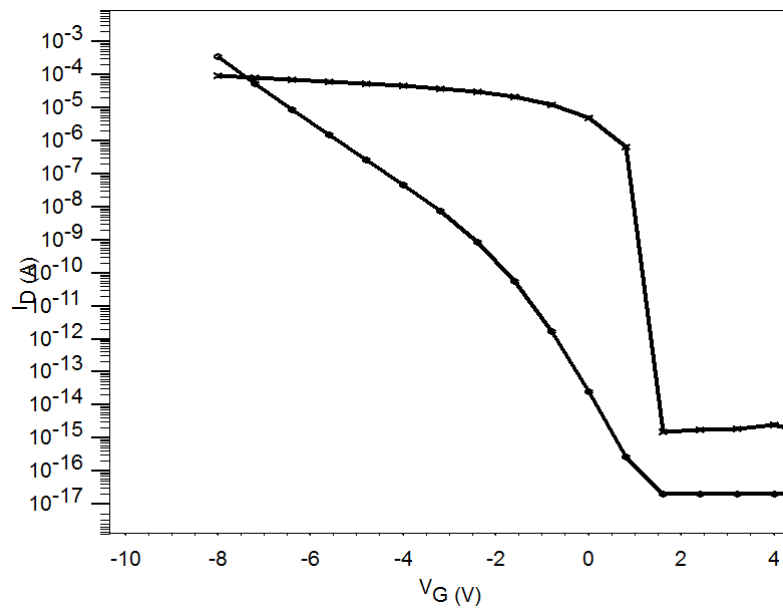
$$V_T = \frac{t \cdot q}{C_i} \frac{N_d t_1 + N_A t_2}{t} - V_{bi} \quad (27)$$

By optimizing the both of thickness and doping concentration, it can be known that the threshold voltage shift can be minimized.

The output curves, transfer curve, and AC response are shown in Figure 23-26 with different doping concentration for both of single layer depletion mode OTFT and dual layer depletion mode OTFT. As shown, dual-layer depletion mode OTFT has much higher on-current than single layer one, reaching 0.4mA.

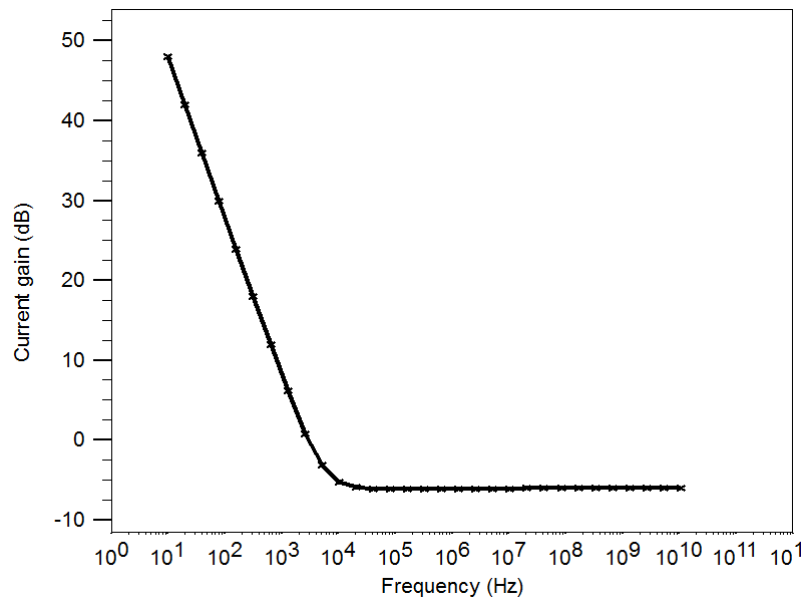


(a) Single Layer Depletion OTFT: Output Curves



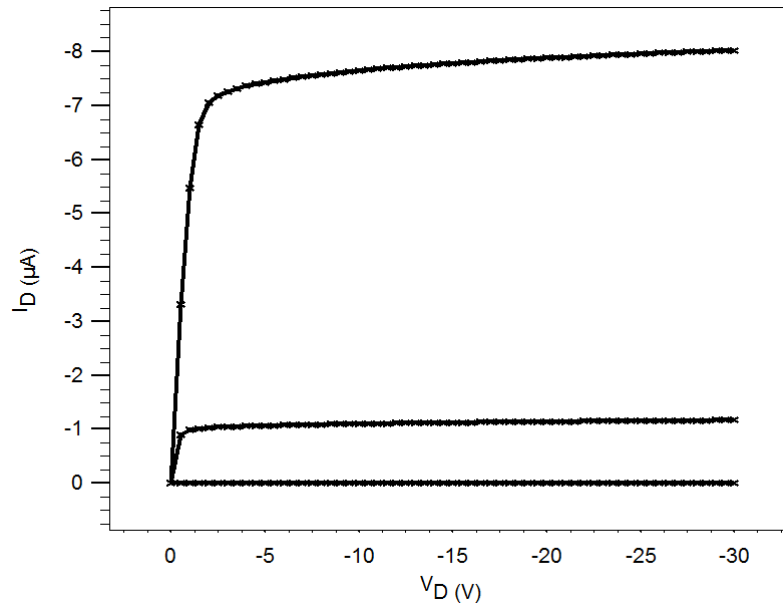
(b) Single Layer Depletion OTFT: Transfer Curves

Figure 23. Simulation Results of Intrinsic Single-Layer Depletion OTFT

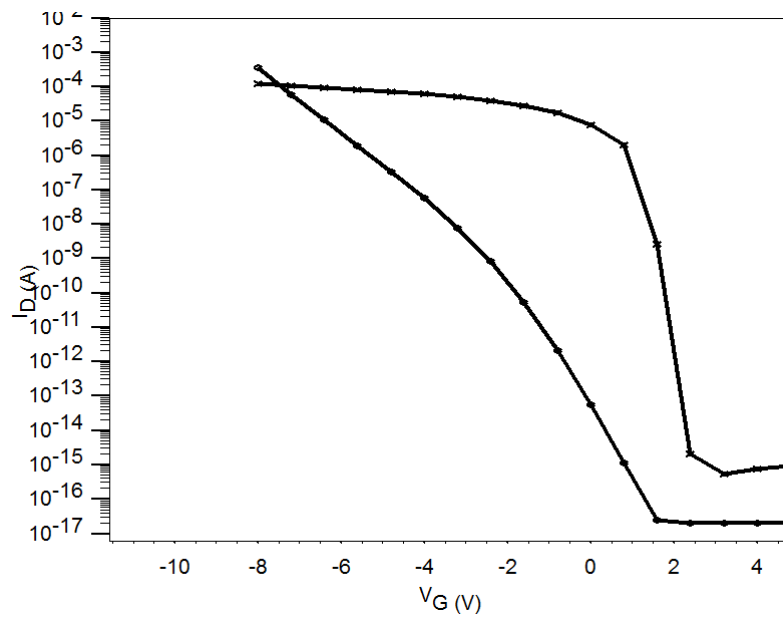


(c) Single Layer Depletion OTFT: Short Circuit Current Gain Vs. Frequency

Figure 23. Continued

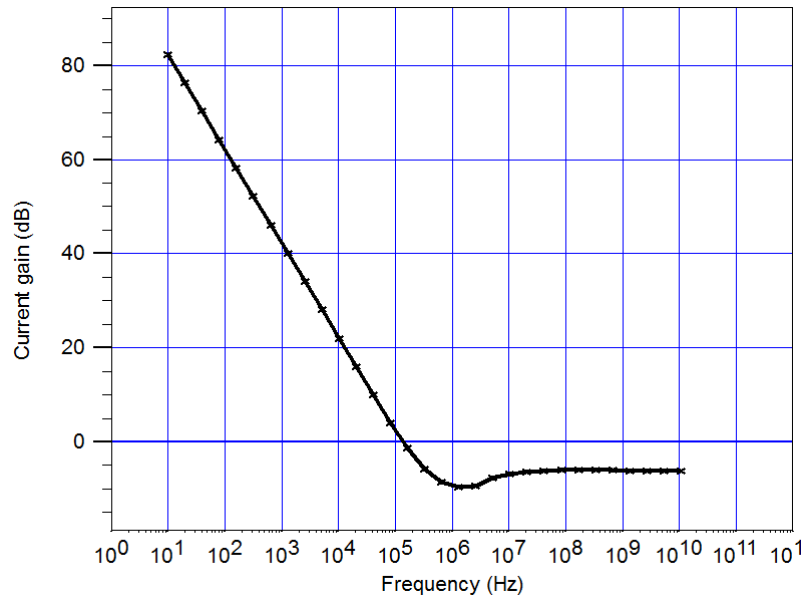


(a) Single Layer Depletion OTFT: Output Curves



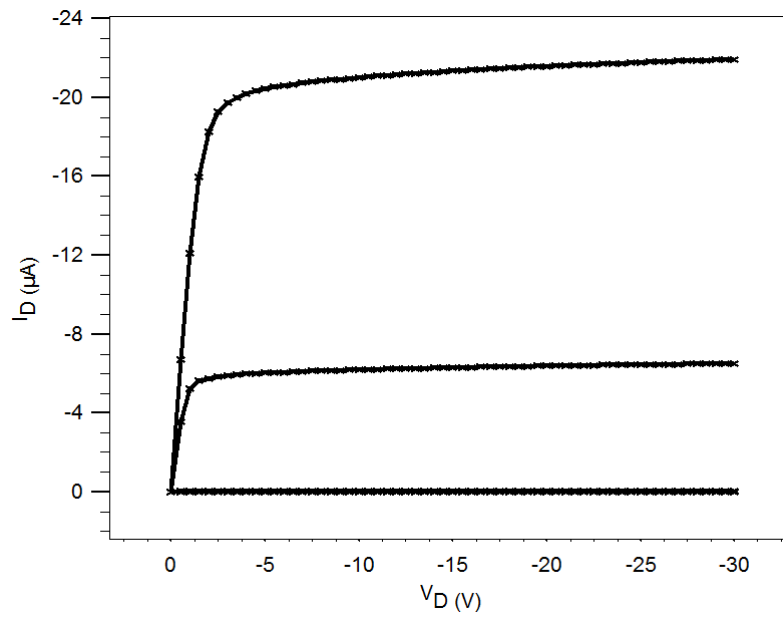
(b) Single Layer Depletion OTFT: Transfer Curves

Figure 24. Simulation Results of Light Doped Single-Layer Depletion OTFT

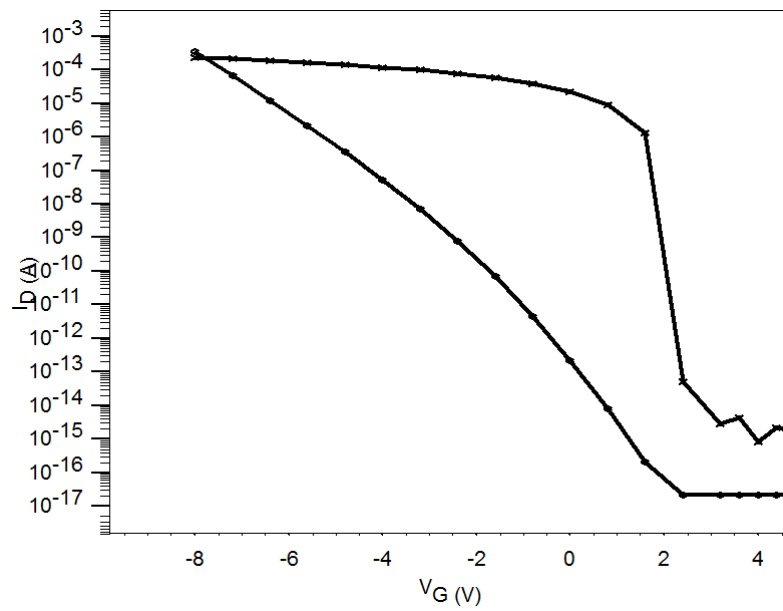


(c) Single Layer Depletion OTFT: Short Circuit Current Gain Vs. Frequency

Figure 24. Continued

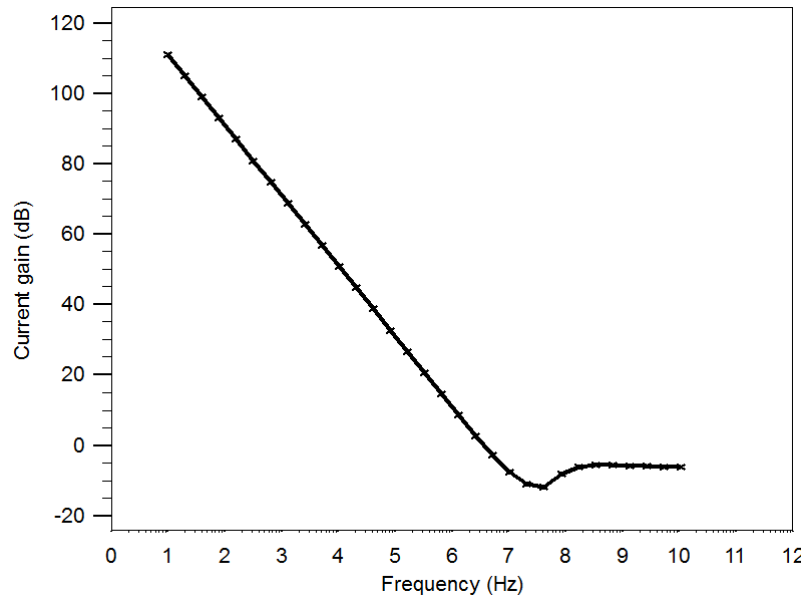


(a) Dual Layer Depletion OTFT: Output Curves



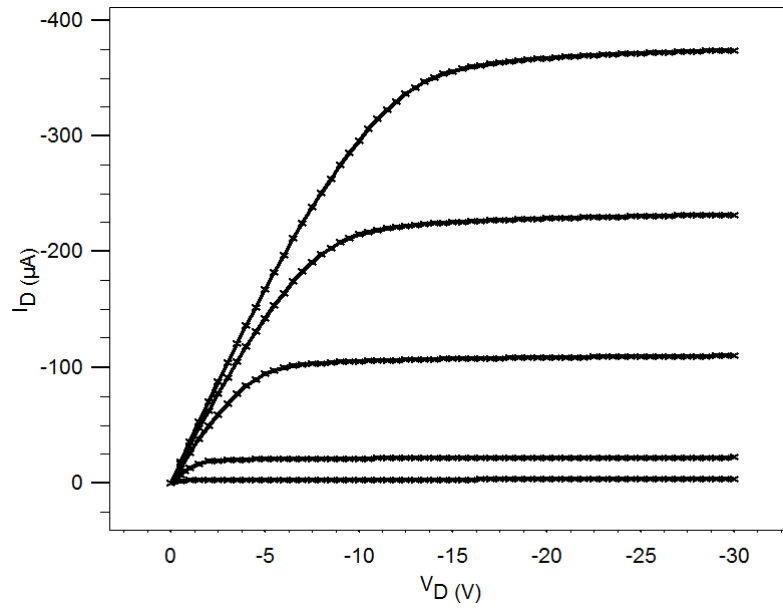
(b) Dual Layer Depletion OTFT: Transfer Curves

Figure 25. Simulation Results of 2% Weight Doped Dual-Layer Depletion OTFT

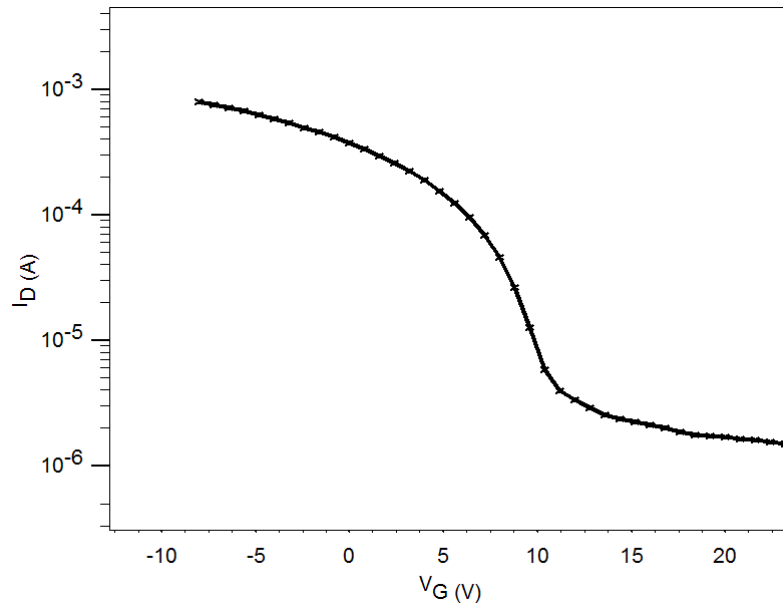


(c) Dual Layer Depletion OTFT: Short Circuit Current Gain Vs. Frequency

Figure 25. Continued

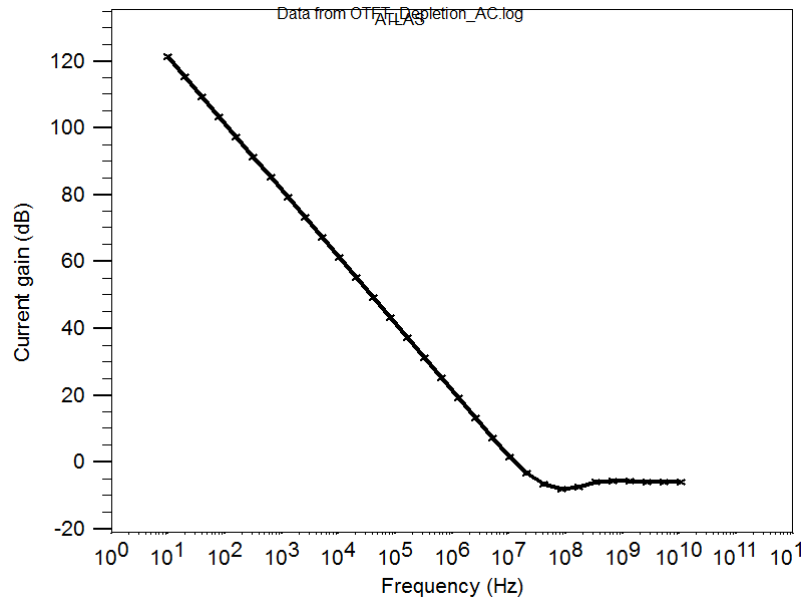


(a) Dual Layer Depletion OTFT: Output Curves



(b) Dual Layer Depletion OTFT: Transfer Curves

Figure 26. Simulation Results of 4% Weight Doped Dual-Layer Depletion OTFT



(c) Dual Layer Depletion OTFT: Short Circuit Current Gain Vs. Frequency

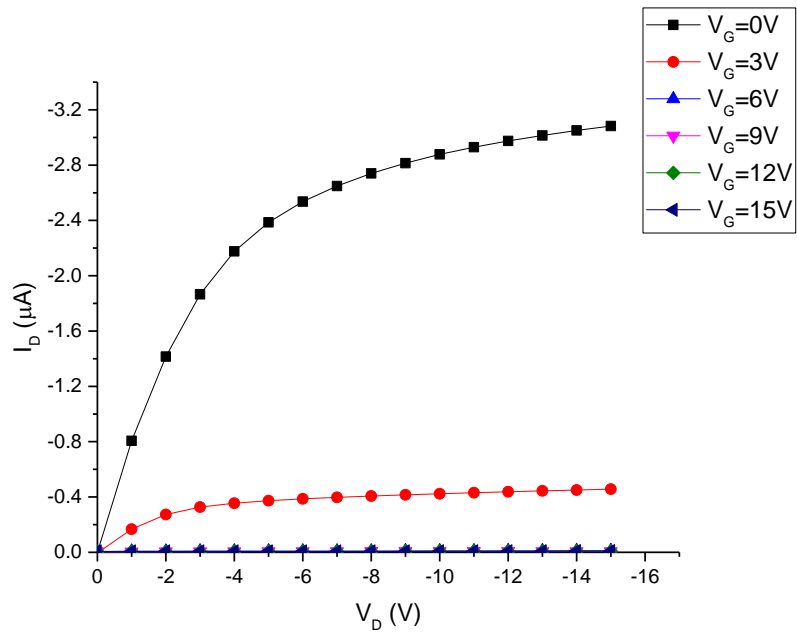
Figure 26. Continued

As shown in the Figure 26, the device cannot be pinched off with the doping concentration of $5 \times 10^{17} \text{cm}^{-3}$ and above, and therefore the off current of device is high. AC performance is remarkable even with such a long channel length of $10 \mu\text{m}$. The depletion mode OTFT can reach 10MHz of cutoff frequency. Under the assumption of that the cutoff frequency increases approximately linear by scaling the channel length, then the cutoff frequency of $1 \mu\text{m}$ of smaller channel length device is expected to have the unity gain frequency located at around 100MHz.

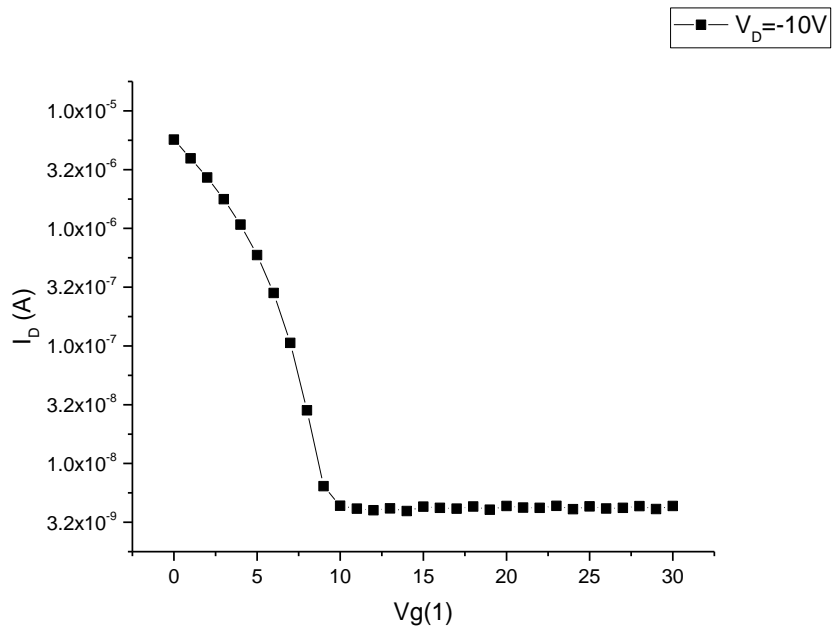
To verify the design and simulation, actual devices are fabricated and measured, and measured results are shown in Figure 27~30 in accordance with different doping

concentration and structure. It clearly indicates that depletion mode OTFT has very high on-current level, lower operation voltage, high cutoff frequency, and it can be applicable to many organic electronic applications. One down side or possible limitation is the high off current. There are several ways of solving this problem which is verified by simulations and modeling. First, adding another contact at the intrinsic layer similar as body contact of silicon MOSFET or dual gate scheme. In this way, the ability to control the conductivity of channel is improved and makes easier to turned off the device. Second method is using the N-doped layer instead of intrinsic layer. However, N-type organic material is much more unstable and much more careful passivation of device is necessary to protect N-type material. Also, both methods are required to process extra additional steps, so those device structures are not fabricated at this time.

The results of depletion mode OTFT simulations and experiments are summarized in Table 7.

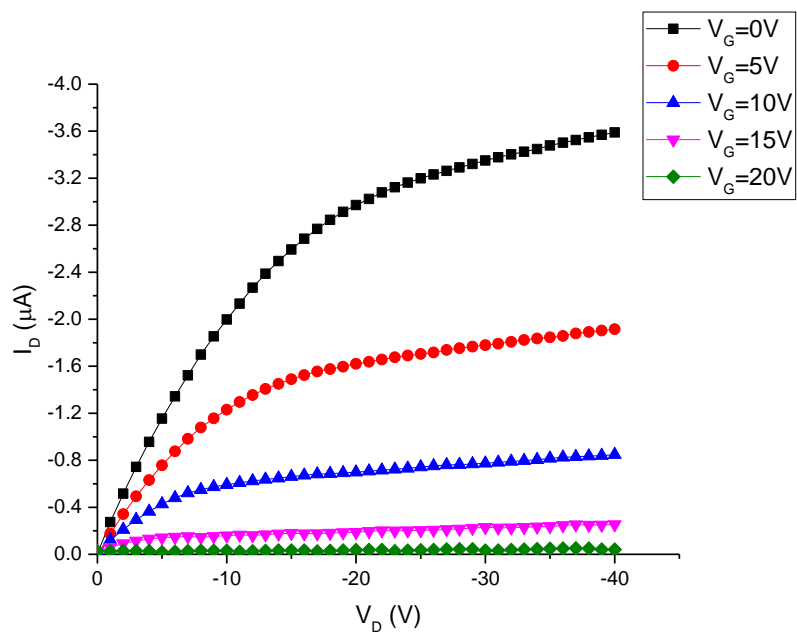


(a) Single Layer Depletion OTFT: Output Curves

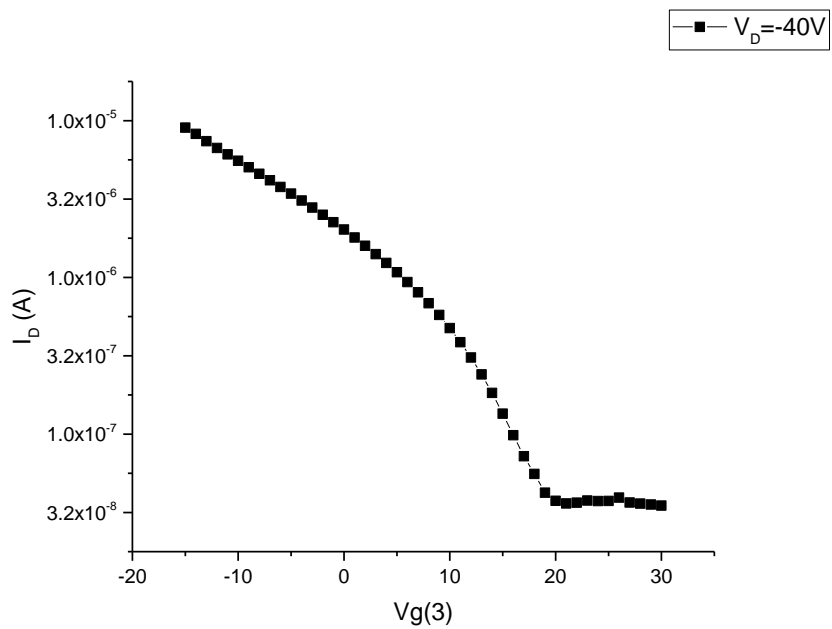


(b) Single Layer Depletion OTFT: Transfer Curves

Figure 27. Experiment Results of Intrinsic Single-Layer Depletion OTFT

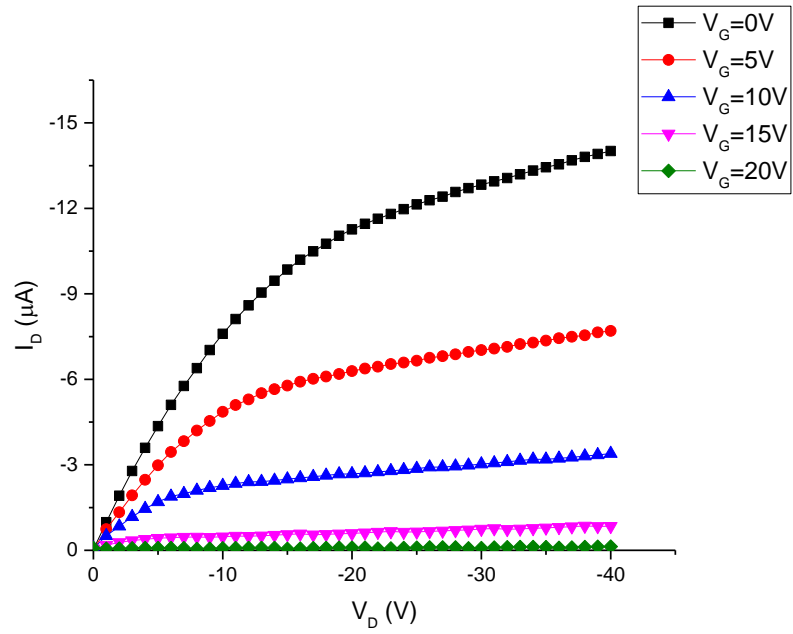


(a) Single Layer Depletion OTFT: Output Curves

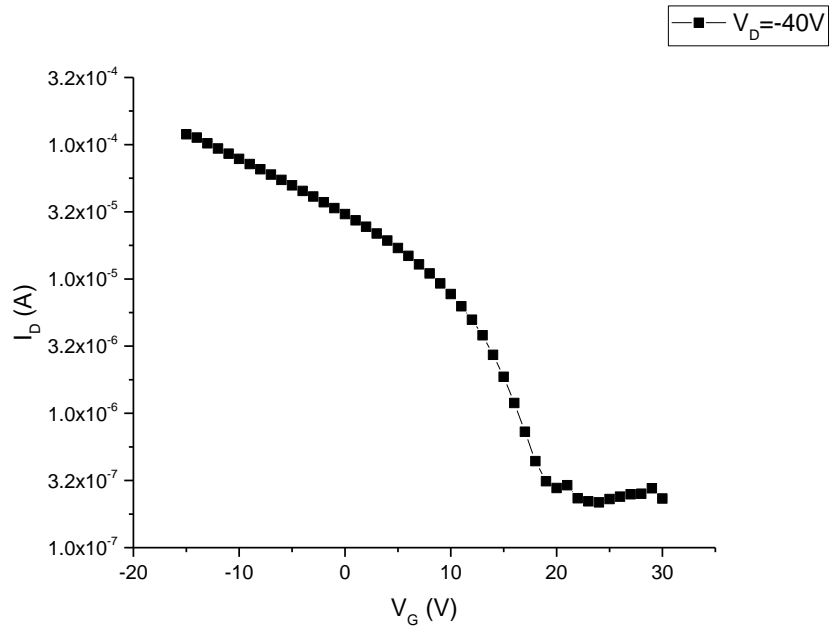


(b) Single Layer Depletion OTFT: Transfer Curves

Figure 28. Experiment Results of Light Doped Single-Layer Depletion OTFT

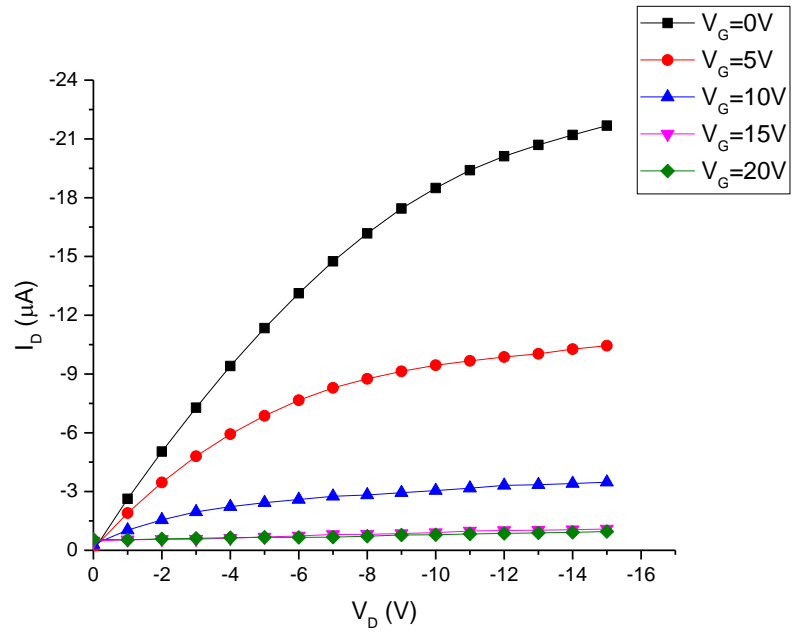


(a) Dual Layer Depletion OTFT: Output Curves

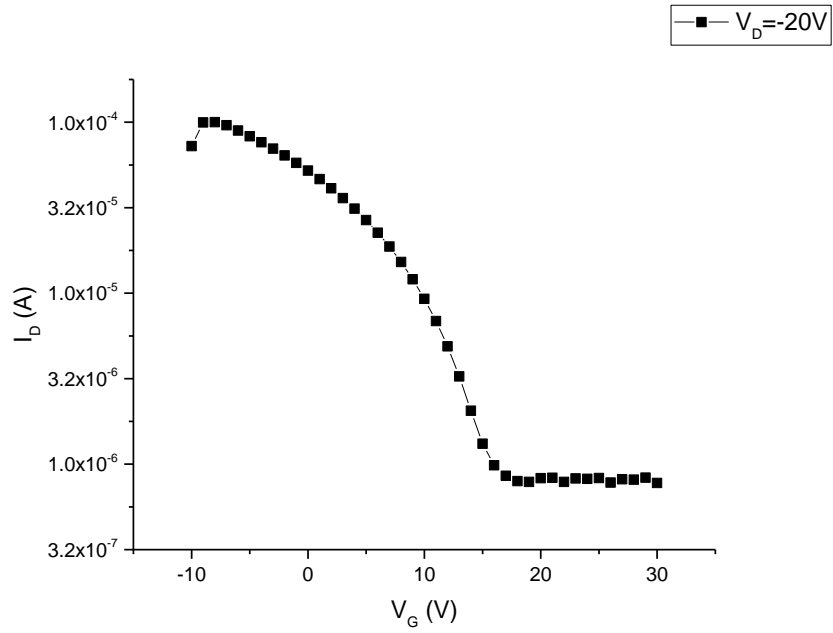


(b) Dual Layer Depletion OTFT: Transfer Curves

Figure 29. Experiment Results of 2% Weight Doped Dual-Layer Depletion OTFT



(a) Dual Layer Depletion OTFT: Output Curves



(b) Dual Layer Depletion OTFT: Transfer Curves

Figure 30. Experiment Results of 4% Weight Doped Dual-Layer Depletion OTFT

Organic Heterojunction Bipolar Transistor(OHBT)

The last device studied in this research is organic heterojunction bipolar transistor, which can actually resolve all the issues involving with organic transistor devices by very high doping concentration, minimized parasitic components and current mode mechanism rather than field effect via capacitor. The challenging parts of OHBT are organic material selection and physical etching of organic layers without causing damages. Since two different materials with different energy band, possibly three different materials in case that N-type doping is unavailable, it is better to synthesize the material chemically rather than using commercially available organic materials. Because of this reason, the attempt to fabricate OHBT device has not been made in this research. The fabrication part will remain as a future work and OHBT is only designed by TCAD after thorough investigation and study theoretically. All the material parameters are designed according to the widely known organic band parameters [36]-[37] , so that OHBT device is feasible to be fabricated. By following the designing steps illustrated in Figure 31, all the designed material parameters are listed in Table 8. Also, the designed structure is shown in Figure 32.

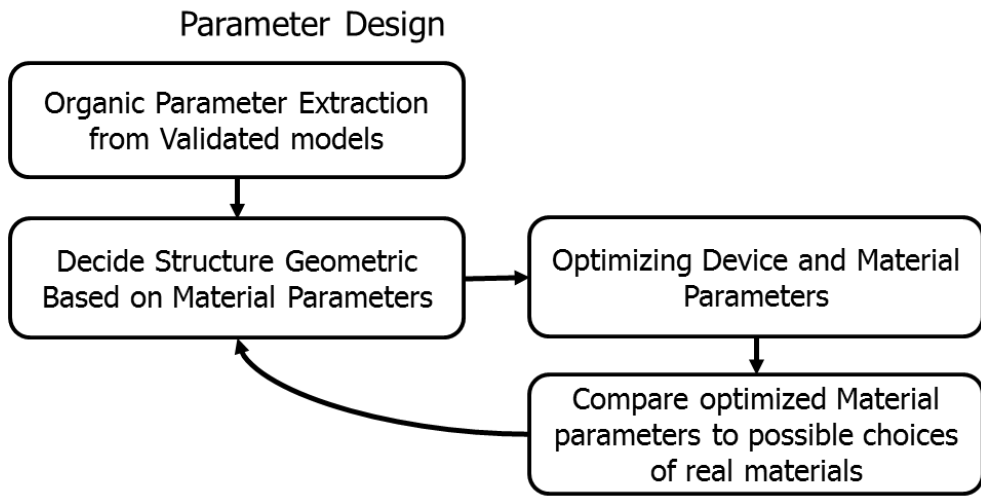


Figure 31. OHBT Designing Methods and Steps

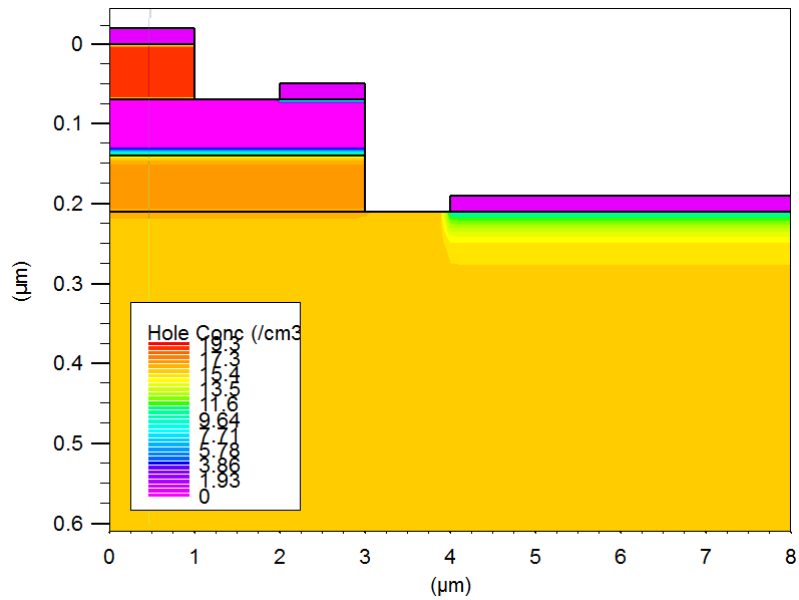
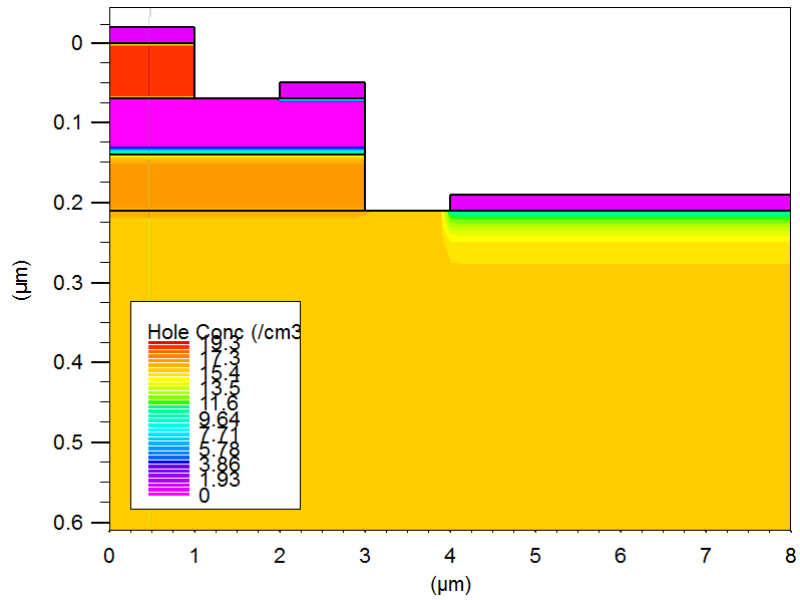
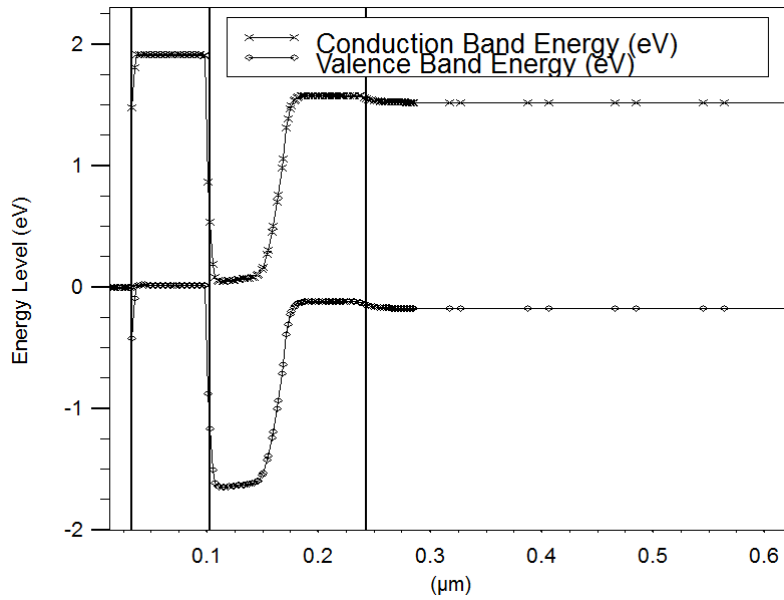


Figure 32. Design Structure of OHBT

The parameters of materials listed above are determined to ensure the operation of typical inorganic HBT device. The base/emitter heterojunction makes the potential barrier seen by base electrons in the conduction band is higher than that seen by emitter holes in the valence band. Thus, for a given base/emitter bias, the ratio of holes injected to electrons injected will be higher, and thus the gain will be higher [38], [39]. The band gap difference enables to keep a thin and highly doped base at the same time, which results in a very high cutoff frequency and high gain [40]. One different feature from inorganic HBT is that the doping concentration of sub-collector is very high. In inorganic HBT, light doped sub collector is preferred since it is desirable for all of the collected carrier to flow into the collector electrode without scattering. That is, light doped sub-collector gives carriers higher mobility. In contrast to inorganic HBT, to increase the carrier mobility in sub-collector region, high doping concentration is preferable. In fact, since the operation voltage of HBT is extremely small compared to field effect organic transistor and thus applied electric field is not high enough to increase the mobility, the only way to increase the carrier mobility is to keep carrier concentration as high as possible in organic HBT. The designed OHBT device is shown in Figure 33, and it illustrates the mechanism of operation.

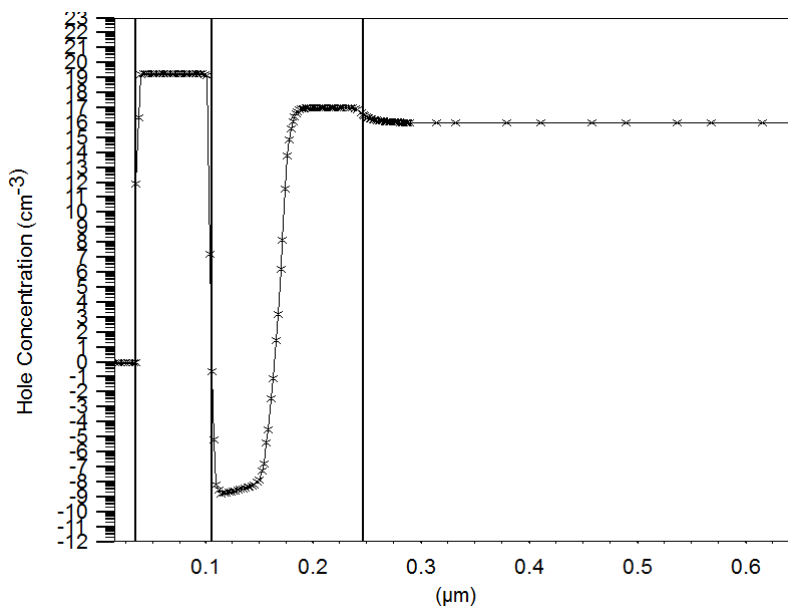


(a) Spatial Hole Concentration in the Device under Zero Bias

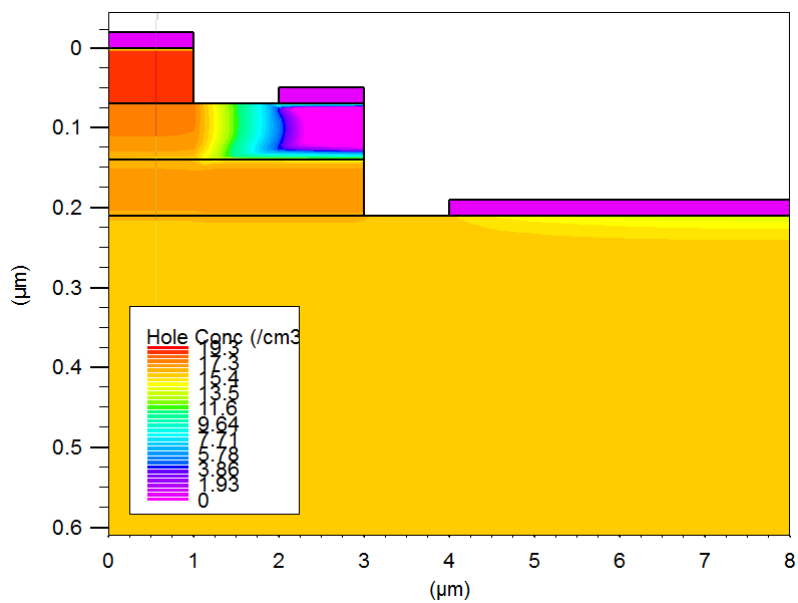


(b) Energy Band Diagram of Emitter-Base-Collector under Zero Bias

Figure 33. OHBT Energy Band under Operation: Zero and Forward Bias

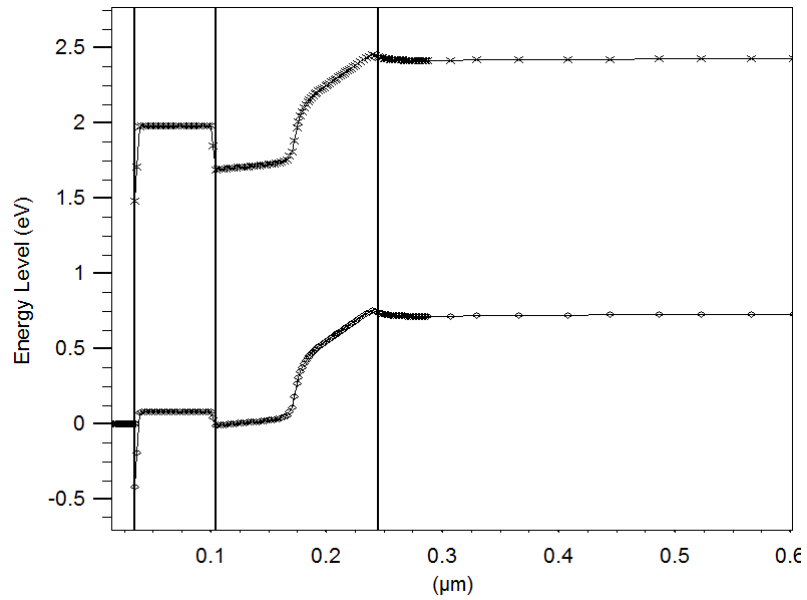


(c) Hole Concentration of Emitter-Base-Collector under Zero Bias

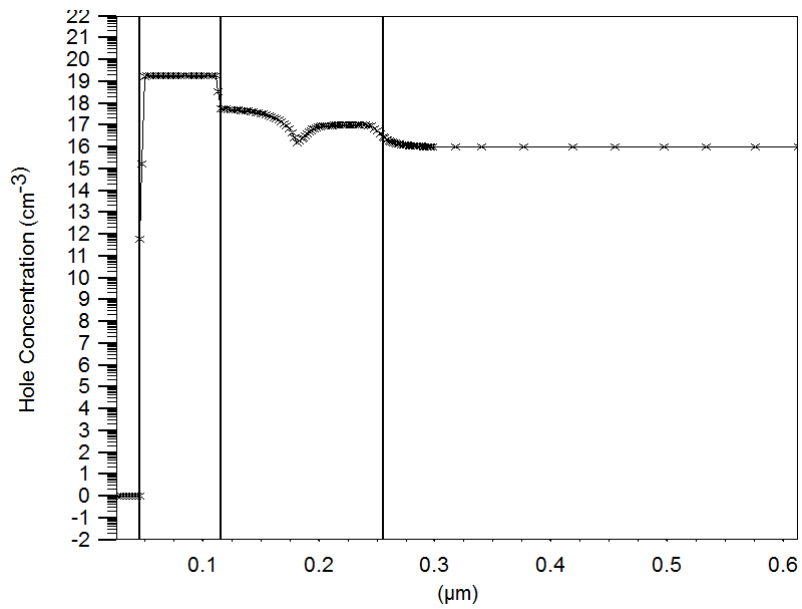


(d) Spatial Hole Concentration in the Device under Forward Bias

Figure 33. Continued



(e) Energy Band Diagram of Emitter-Base-Collector under Forward Bias



(f) Hole Concentration of Emitter-Base-Collector under Forward Bias

Figure 33. Continued

Figure 33 indicate that the hole injection barrier is 0.1eV while the electron injection barrier is 0.3eV between emitter and base junction. The thickness of emitter layer is optimized to prevent injected electrons from base reaching to the emitter electrode, and the thickness of base is kept thin enough to ensure injected holes from emitter to reach the end of base at the same time in according to the designing step shown in Figure 31. Another important feature revealed in Figure 33 is that the width of injection barrier at the interface between emitter contact and organic emitter layer is less than 10nm which is narrow enough to be considered as ohmic contact rather than Schottky contact. Therefore, higher transconductance gain and lower contact resistance are achieved in this design. To evaluate complete device performance, the compact model of OHBT is first derived as shown in Figure 34 [41], [42].

From the complete compact model of OHBT with structure in Figure 34, it can be easily understood that the parasitic elements are reduced by heavy doping. According to the equation of depletion region width (28) and the equation of cutoff frequency (29), the cutoff frequency can be calculated.

$$X_{dep} = \sqrt{\frac{2\epsilon_s}{qN} (V_{bi} - V)} \quad (28)$$

$$f_t = \frac{I}{2\pi\pi_{ec}}$$

$$\left\{ \begin{array}{l} \tau_e = \frac{I}{g_m} (C_{je} + C_{jc}) \\ \tau_c = (R_E + R_C) C_{jc} \\ \tau_B = \frac{X_B^2}{2D_n} \\ \tau_{sc} = \frac{X_C}{2v_C} \end{array} \right. \quad (29)$$

Finally, the simulation results of OHBT are shown in Figure 35 and summarized in Table 9.

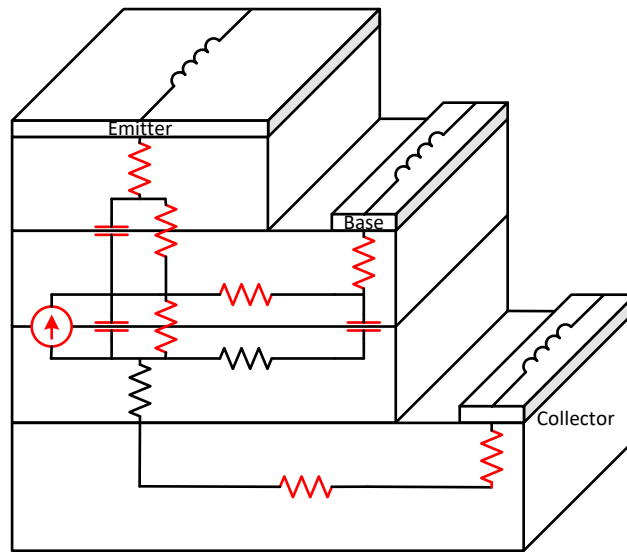
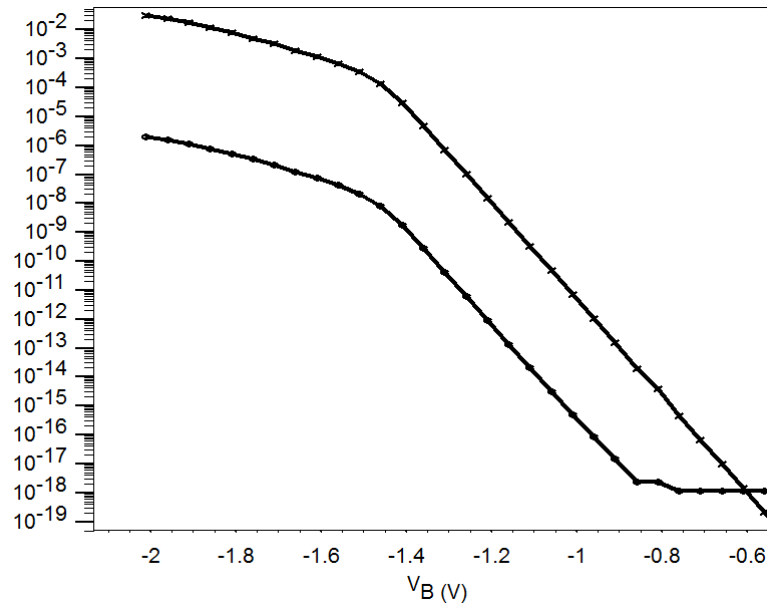
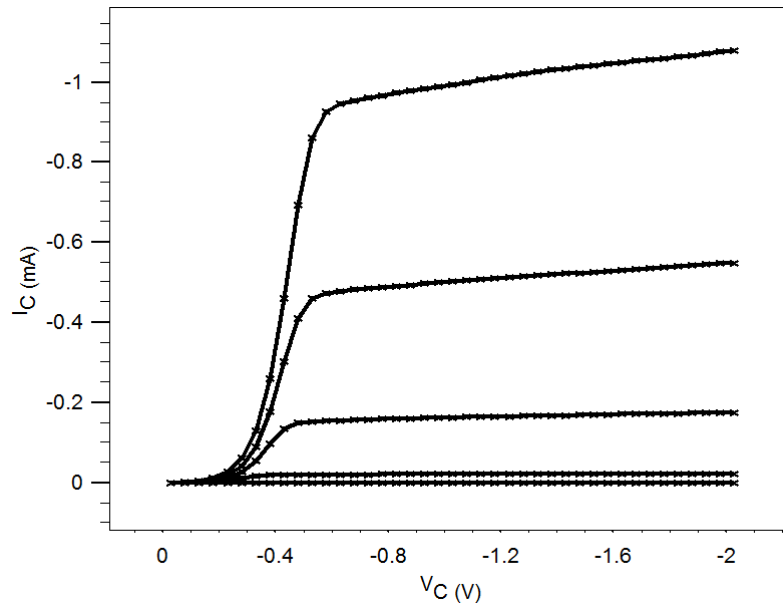


Figure 34. Compact Model of OHBT and Reduced Parasitic

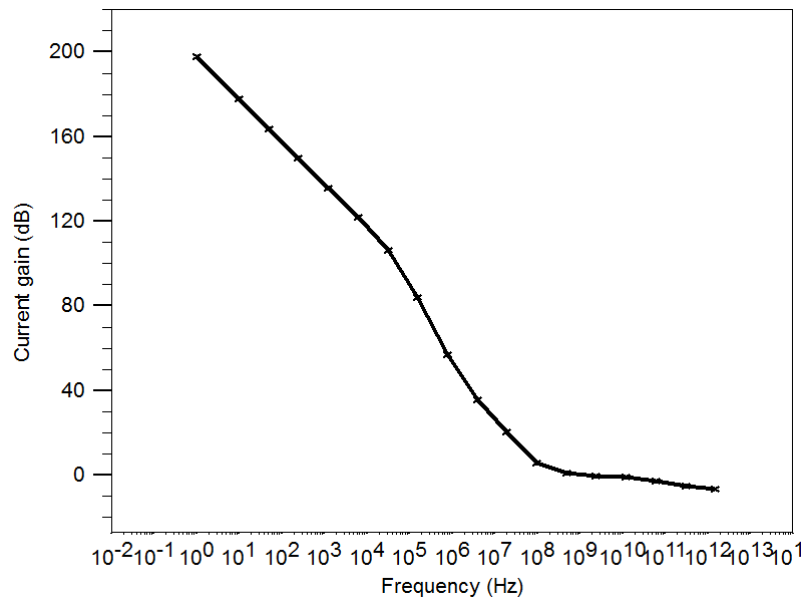


(a) DC Characteristic: Forward Gummel



(b) DC Characteristic: I_C Vs. V_C Output Curves

Figure 35. Simulation Results of OHBT



(c) AC Characteristic: Short Circuit Current Gain Vs. Frequency

Figure 35. Continued

CHAPTER IV

SUMMARY AND CONCLUSION

In this research, three different organic transistor structures are investigated with simulations and experiments. Modified organic MESFET and depletion mode OTFT devices by using the dual-layer scheme can improve the performance of devices for both of DC (higher on-current) and AC (higher operating frequency) performance as shown in simulations and experiments results. OHBT is likely have superior performance to all the currently existing organic transistor structures based on simulations. The dual-layer organic MESFET device can operate with a nominal voltage of less than 10 V and operate at a frequency up to 50 MHz, and the depletion mode OTFT device can operate with a nominal voltage of 20 V and operate at a frequency up to 10 MHz. The performance of the devices will be further improved when highly crystallized organic materials. With 10MHz or higher cutoff frequencies, those devices can be possible candidates to build low frequency range RFID tags, LCD backplane panel and many other large area electronic circuits with full organic integration. All the performances of devices are summarized in Table 10.

As for the future works, each of essential components of electronic circuit will be built with organic materials, and complete integrated circuit system will be demonstrated.

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APPENDIX A

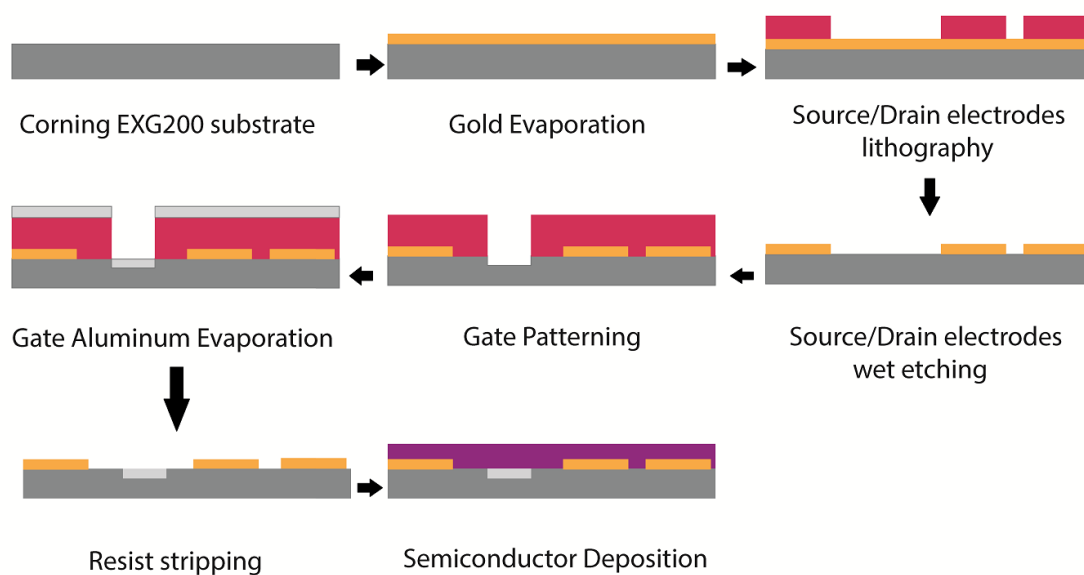
DEVICE FABRICATION

For MESFETs, 30nm of gold was deposited on Corning EXG200 glass substrate using thermal evaporation. Then, Source/drain electrodes were patterned by photolithography and wet etching. Aluminum gate electrodes were patterned by liftoff process. AZ5214 was used in its image reversal mode. After lithography, the substrate was etched in the gate area to a depth of 37nm utilizing the resist as the etch mask. 40nm of aluminum was deposited by thermal evaporation then. The resist was striped in solvent thereafter and finally the gate was patterned. The liftoff process enables burying the gate electrode in the substrate. Therefore, it allows us to accurately mimic the layout design in the simulation. After all the electrodes were successfully fabricated, both polymeric and small-molecule organic semiconductors were deposited by spin coating and thermal evaporation respectively.

Doping concentration, types of materials and semiconductor layer thickness were varied for the optimization of device performance.

For depletion mode OTFTs, heavily doped n type silicon was used as the substrate with its body as the common gate. 300nm thermal dioxide was used as the insulator dielectric for the long channel devices. For short channel devices, aluminum oxide was used instead of silicon dioxide for its high permittivity and film density to suppress the gate leakage current and short channel effects. Source/Drain electrodes were patterned with liftoff process. Electron beam lithography was conducted with

ZEP520 resist and then 3nm Cr & 30nm gold was evaporated. After resist stripping, P3HT and pentacene were deposited as the active layer. Different doping concentration and film thickness were applied to find out the optimize device performance.



APPENDIX B

LARGE TABLES

Table 4. Reproduced Simulation Results of Long Channel OTFT

Long Channel	Experiment*		Modeled by Simulation	
	$L=125\mu\text{m}$	$L=50\mu\text{m}$	$L=125\mu\text{m}$	$L=50\mu\text{m}$
Threshold Voltage V_t	~6V	~6V	~8V	~6V
Operating Voltage V_{DD}	-60V	-40V	-60V	-40V
On-Current I_{ON}	250 μA	240 μA	240 μA	240 μA
On-Off Ratio	$\sim 10^8$	$\sim 10^8$	$\sim 10^{10}$	$\sim 10^{10}$
Cutoff Frequency(Device) f_c	—	$\sim 1.2\text{kHz} \times 5 \times 20$	25kHz	80kHz
Saturation Mobility μ_n	2.5	3	1.75	2

Table 5. Reproduced Simulation Results of Short Channel OTFT

Short Channel	Experiment*			Modeled by Simulation		
	$L=1\mu\text{m}$	$L=200\text{nm}$	$L=70\text{nm}$	$L=1\mu\text{m}$	$L=200\text{nm}$	$L=70\text{nm}$
Threshold Voltage V_t	2V	3V	4V	2V	3V	4V
Operating Voltage V_{DD}	-3V	-3V	-3V	-3V	-3V	-3V
On-Current I_{ON}	2.8nA	5.5nA	26nA	2.4nA	7nA	11nA
On-Off Ratio	$\sim 10^4$	$\sim 10^4$	$\sim 10^4$	$\sim 10^{10}$	$\sim 10^{10}$	$\sim 10^5$
Cutoff Frequency(Device) f_c	-	-	-	-	-	-
Saturation Mobility μ_n	0.01	0.01	0.01	0.01	0.01	0.01

Table 6. Summarized Results and Comparison of OMESFET

	Experiment		Modeled by Simulation	
	Single Layer	Dual Layer	Single Layer	Dual Layer
Threshold Voltage V_t	~40V	~40V	~3.5V	~3.5V
Operating Voltage V_{DD}	-40V	-40V	-4V	-4V
On-Current I_{ON}	3 μ A	35 μ A	0.8 μ A	38 μ A
On-Off Ratio	~60	~320	~10 ³	~10 ³
Cutoff Frequency(Device) f_c	—	—	700kHz	20MHz
Saturation Mobility μ_n	0.075	0.1~0.3	0.02	0.2

Table 7. Summarized Results and Comparison of Depletion OTFT

	Experiment		Modeled by Simulation	
	Single Layer	Dual Layer	Single Layer	Dual Layer
Threshold Voltage V_t	~18V	~15V	~2V	~12V
Operating Voltage V_{DD}	-20V	-15V	-5V	-15V
On-Current I_{ON}	4 μ A	22 μ A	8 μ A	380 μ A
On-Off Ratio	~300	~100	~10 ¹²	~10 ³
Cutoff Frequency(Device) f_c	—	—	100kHz	10MHz
Saturation Mobility μ_h	0.013	0.3	0.038	0.5

Table 8. Material Parameters of OHBT

	Doping	Type	Bandgap	Affinity	Low-field mobility
Emitter	2×10^{19}	P-type	1.9eV	3.3eV	0.1
Base	2×10^{18}	N-type	1.7eV	3eV	0.1
Collector	1×10^{18}	P-type	1.7eV	3eV	0.1
Sub-Collector	1×10^{19}	P-type	1.7eV	3.6eV	0.1

Table 9. Summarized Results of OHBT

	Experiment	Modeled by Simulation
Threshold Voltage V_t	To be measured	~0.9V
Operating Voltage V_{DD}	—	-2V
On-Current I_{ON}	—	1mA
On-Off Ratio	—	$\sim 10^{12}$
Cutoff Frequency(Device) f_c	—	1GHz
Saturation Mobility μ_n	—	1.8

Table 10. Comparison of All Designed High Performance Organic Transistors

	Dual Layer OMESFET		Dual Layer Dep OTFT		OHBT
	Experiment	Simulation	Experiment	Simulation	Simulation
Threshold Voltage V_t	~40V	~3.5V	~15V	~12V	~0.9V
Operating Voltage V_{DD}	-40V	-4V	-15V	-15V	-2V
On-Current I_{ON}	35 μ A	38 μ A	22 μ A	380 μ A	1mA
On-Off Ratio	~320	~10 ³	~100	~10 ³	~10 ¹²
Cutoff Frequency(Device) f_c	—	20MHz	—	10MHz	1GHz
Saturation Mobility μ_n	0.1~0.3	0.2	0.3	0.5	1.8