



MacKenzie, Alasdair and Škurić, Vanja and Stickland, MT and Dempster, WM (2017) A new hybrid slurry CFD model compared with experimental results. In: 12th OpenFOAM® Workshop, 2017-07-24 - 2017-07-27, University of Exeter. ,

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12th OpenFOAM[®] Workshop, University of Exeter
24th-27th July 2017

A new hybrid slurry CFD model compared with experimental results

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Outline

- Background, context and motivation to the problem
- Development of hybrid model
- PIV experiments/validation work

Background

- Weir group produce equipment for the mining and oil and gas industries
- Erosion is a large problem
- CFD modelling is used to predict erosion = better designs
- Longer pump life, better for customer



Ball mill video



Impeller

Before



After

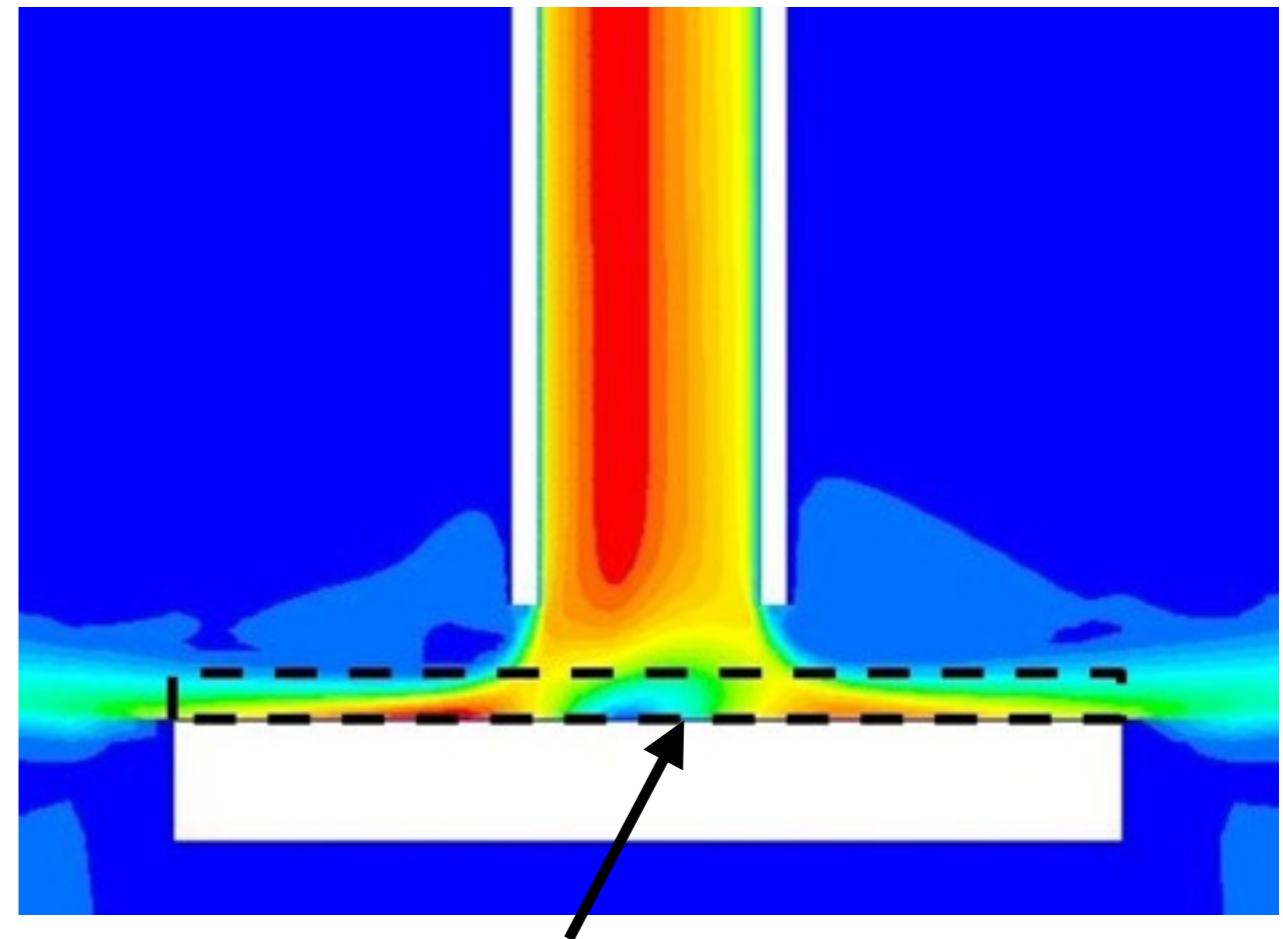


It could be as little as 2 weeks of continuous running for this to happen

Problem/Motivation

- Need particle impact data at the wall for erosion modelling
- Fluid/particulate flow simulation is computationally expensive: especially for dense slurries
- Solution to make faster: Combine with two-fluid model

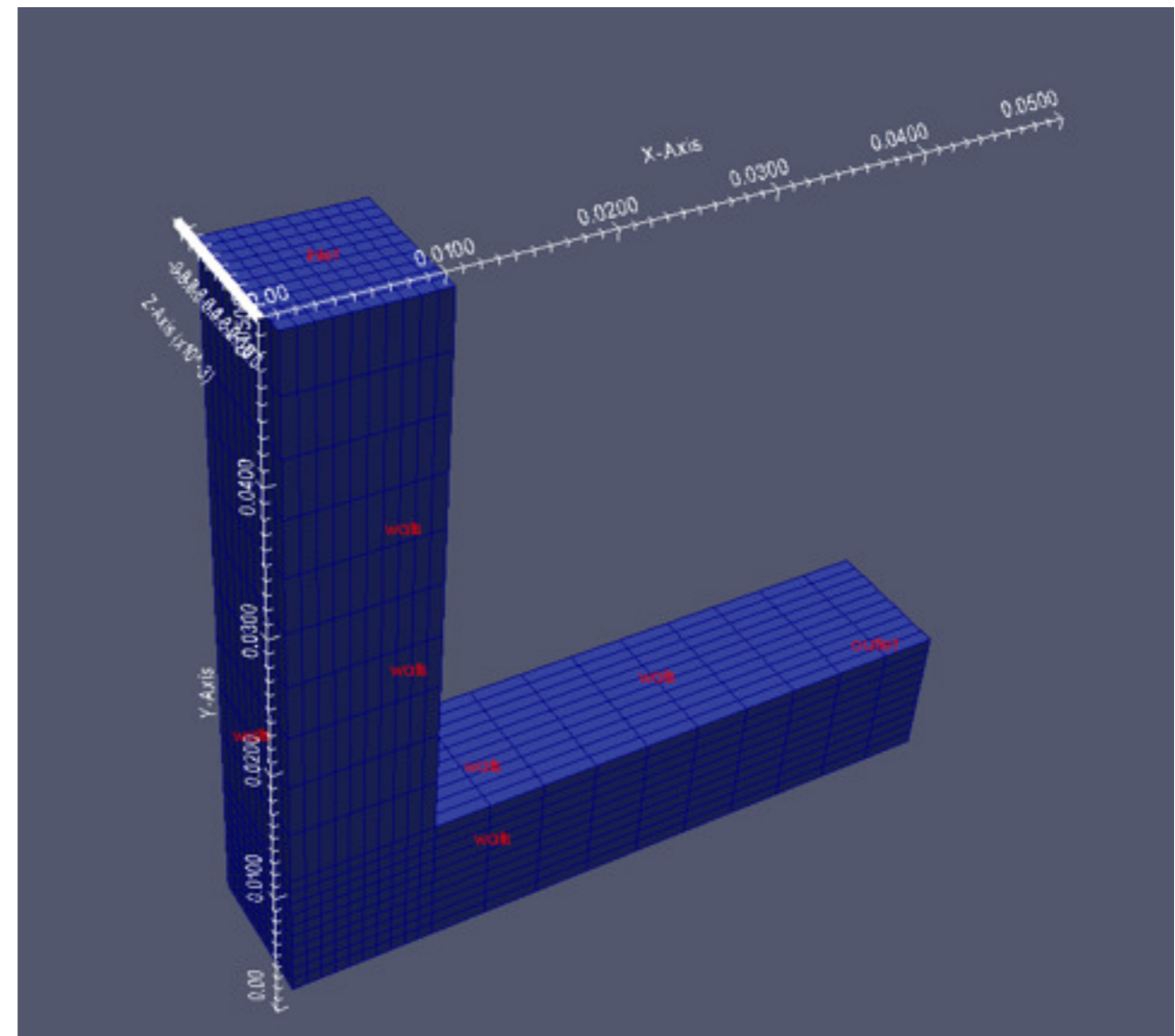
Velocity contours of submerged jet impingement test
note: old asymmetric geometry pictured



Dotted region where particles are necessary
for impact data

Geometry and Solvers

- A simple geometry was chosen for solver development
- reactingTwoPhaseEulerFoam for Euler-Euler
- DPMFoam for Euler-Lagrange
- OpenFOAM 3.0.x was used
- Tutorial available at:
http://www.tfd.chalmers.se/~hani/kurser/OS_CFD_2016/AlasdairMackenzie/tutorial1.pdf



Geometry shown with sizes in metres

Description of Solvers

reactingTwoPhaseEulerFoam

Euler-Euler

Two fluid model

Both phases treated as continuum

Incompressible model: setting in dictionary

Fast to solve

DPMFoam

Euler-Lagrange

Fluid/particle model

Transient solver for coupled transport of kinematic particle clouds

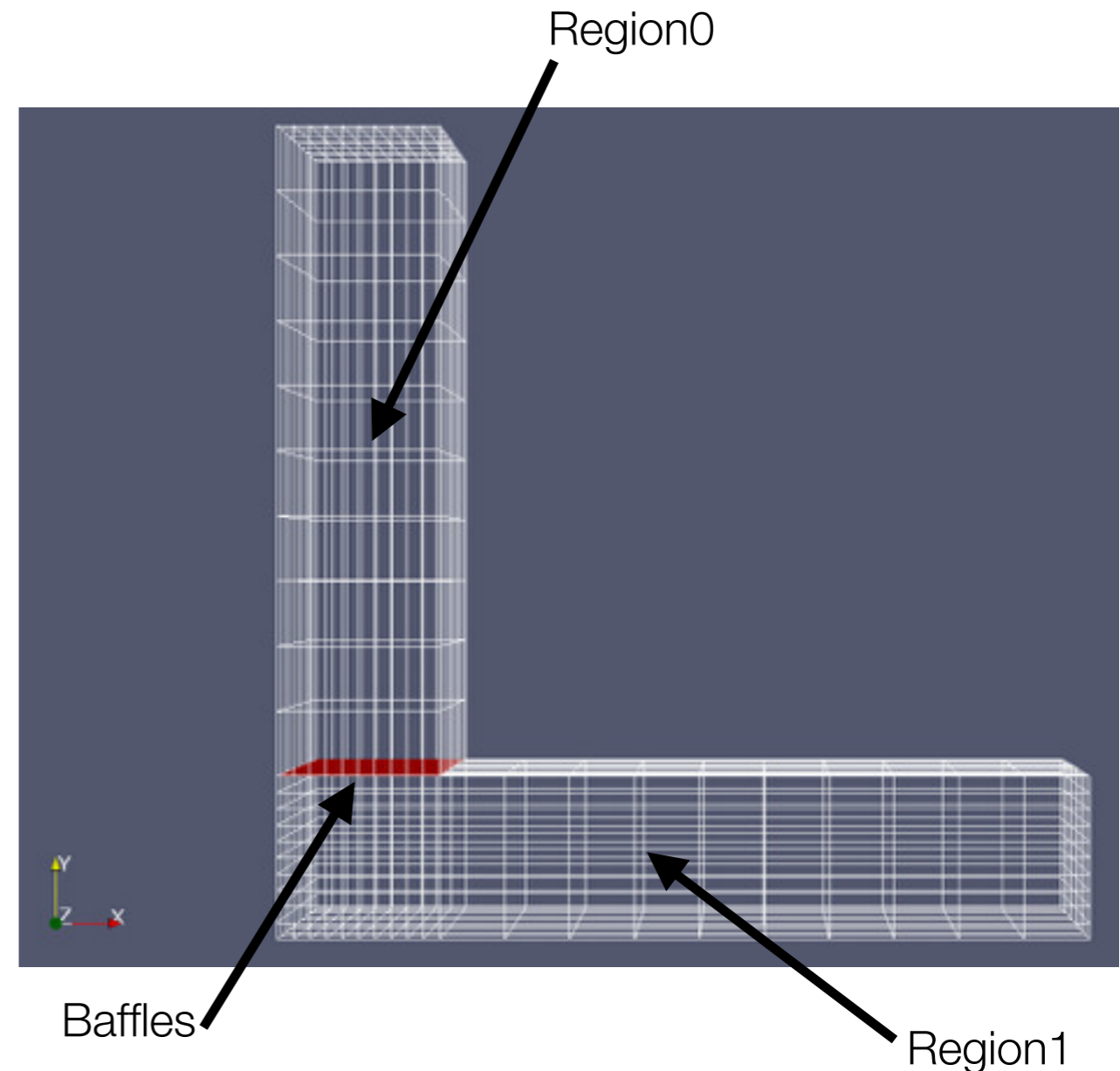
Includes the effect of volume fraction of the particles on the continuous phase

Combining the solvers

- A new solver was made based on the EE model
- To have 2 solvers running, we need 2 regions
- To go from fluid to particles, we need a transition
- An outlet/inlet is needed for particle phase, but shouldn't affect the rest of the flow
- Solution...

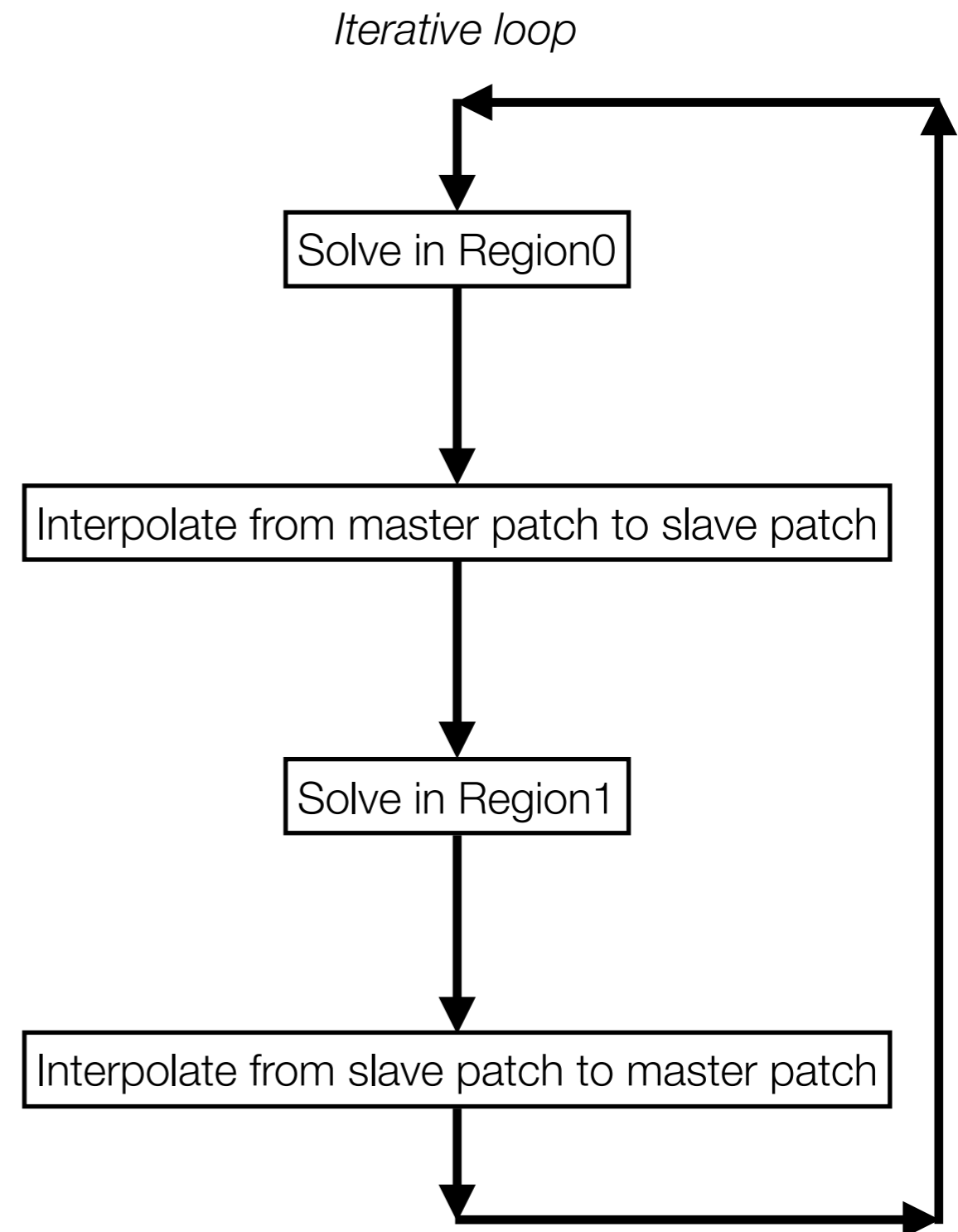
Baffles + Regions

- `createBaffles`: makes internal surface into boundary face
- *master* and *slave* patch created
- `splitMeshRegions`: Splits mesh into 2 separate regions
- BC's can now be applied to baffle patches
- `chtMultiRegionFoam`: Inspiration for solving regions sequentially



Interpolation

- patchToPatchInterpolation: transfers data between two patches
- All variables were interpolated: U1, U2, p, p_rgh, alpha1, alpha2, k, epsilon, nut, and theta
- After this was implemented, the domain ran as if it was one region, not two: the surface doesn't affect the flow
- 'back pressures' were taken into account by interpolating upstream



DPMFoam added

- Code from DPMFoam was added to new solver
- Particles injected from slave patch after back interpolation (slave to master)
- Particles are only in region1 (where erosion would take place)
- Injection values based on phase 2 from region0 by using a lookup table:
kinematicLookupTableInjection

DPMFoam injection

```
18 /* (x y z) (u v w) d rho mDot numParcels
19     where:
20     x, y, z = global cartesian co-ordinates [m]
21     u, v, w = global cartesian velocity components [m/s]
22     d       = diameter [m]
23     rho     = density [kg/m3]
24     mDot    = mass flow rate [kg/m3]
25     numParcels = number of Parcels
26     Dictionary for the KinematicLookupTableInjection */
27 (
28 (0.0005 0.01 -0.0005) (0.01417 0.01831 -0.001718) 5.5e-05 2750 0.005 -2
29 (0.0015 0.01 -0.0005) (0.06206 -0.1608 -0.001616) 5.5e-05 2750 0.005 10
30 (0.0025 0.01 -0.0005) (0.1088 -0.3422 -0.0005019) 5.5e-05 2750 0.005 19
31 (0.0035 0.01 -0.0005) (0.1497 -0.4695 -0.001312) 5.5e-05 2750 0.005 24
```

- Modified kinematicLookupTableInjection used to inject particles
- Lookup table is updated every time step
- 1 line = 1 cell
- Values for particle injection are based on new updated values so solver can deal with geometry changes etc. See Lopez' presentation for more details:

https://sourceforge.net/projects/openfoam-extend/files/OpenFOAM_Workshops/OFW10_2015_AnnArbor/Presentations/Lopez-present-OFW10-16.pdf/download

DPMFoam injection

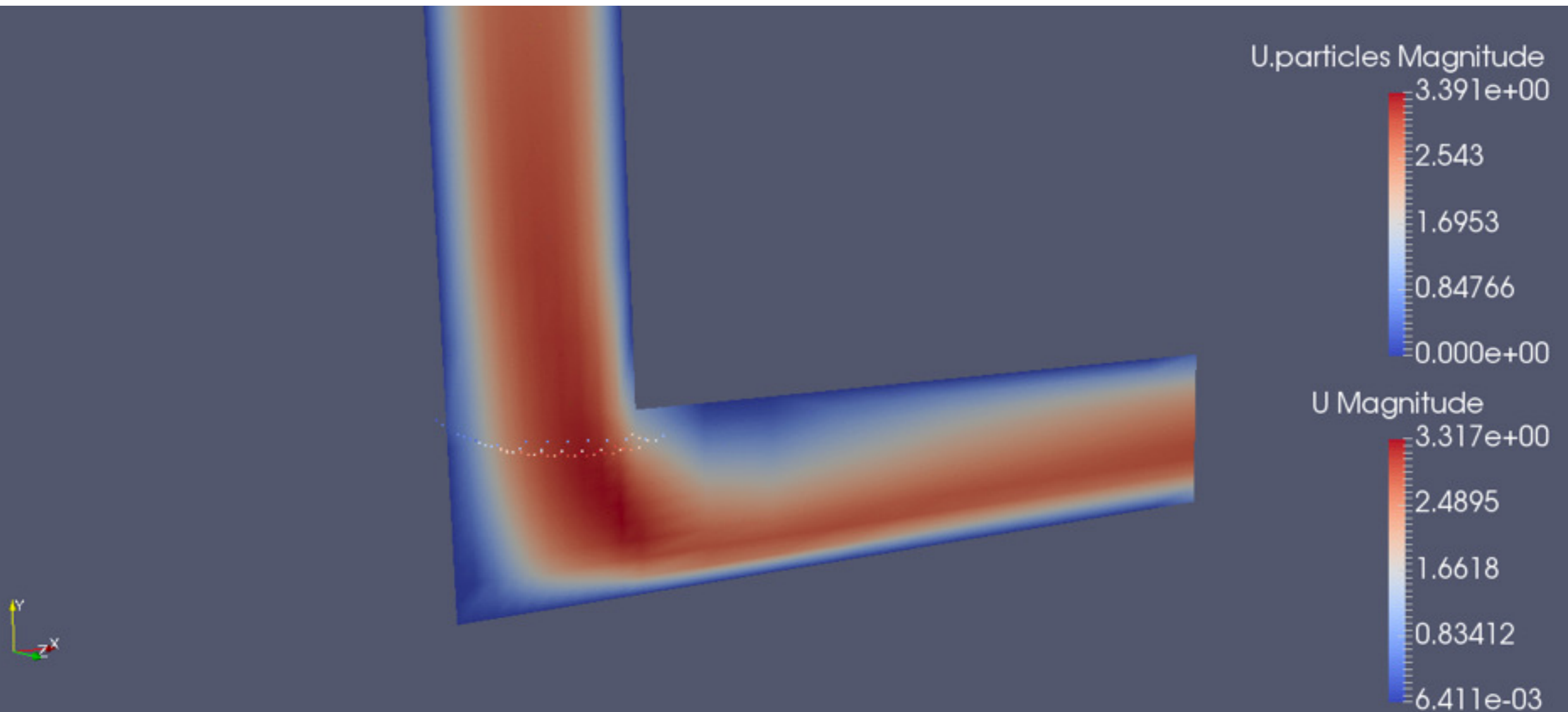
```
kinematicParcelInjectionDataIOList& injectors =
    const_cast<kinematicParcelInjectionDataIOList&>
    (
        mesh.lookupObject<kinematicParcelInjectionDataIOList>("kinematicLookupTableInjection")
    );

forAll(injectors, i)
{
    injectors[i].x() = centres[i]; //forgot to add this when in Croatia
    injectors[i].U() = U1.boundaryField()[slave][i];
    injectors[i].numParticles() = abs((alpha1.boundaryField()[master][i]*(mag(normalSlaveVector[i]))
    *uNormal[i])/((((pi)*pow3(injectors[i].d()))/6))*nParticle*(-1)*timestepsPerSecond));
}

    injectors.write();
}
```

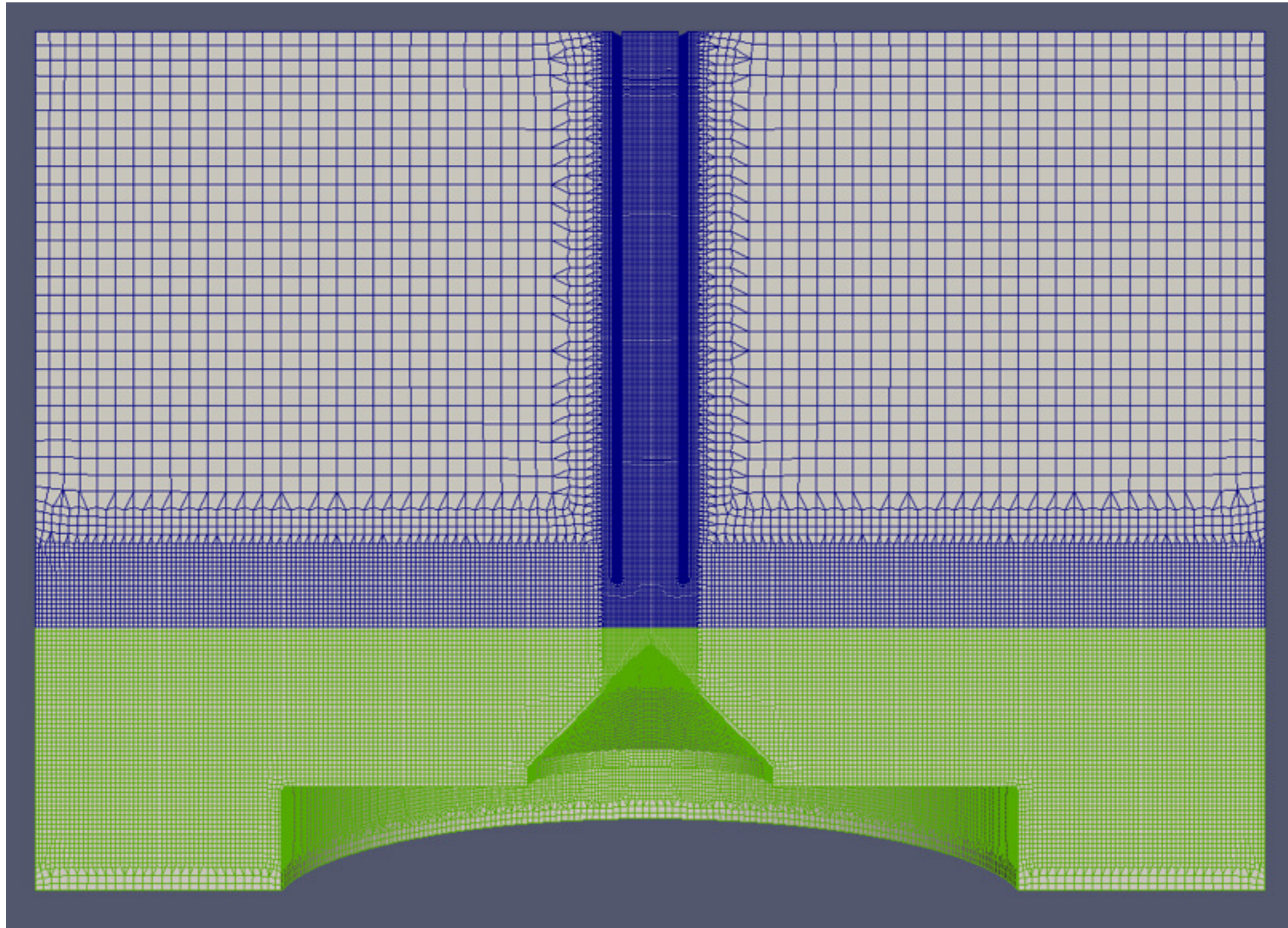
- Number of parcels to be injected is calculated from volume flow rate, number of particles/parcel and alpha distribution.
- Number of parcels/cell = (alpha particles * area of cell * normal velocity component to cell boundary face) / (volume of particle * number of particles/parcel * number of time-steps/second)

Velocity contours

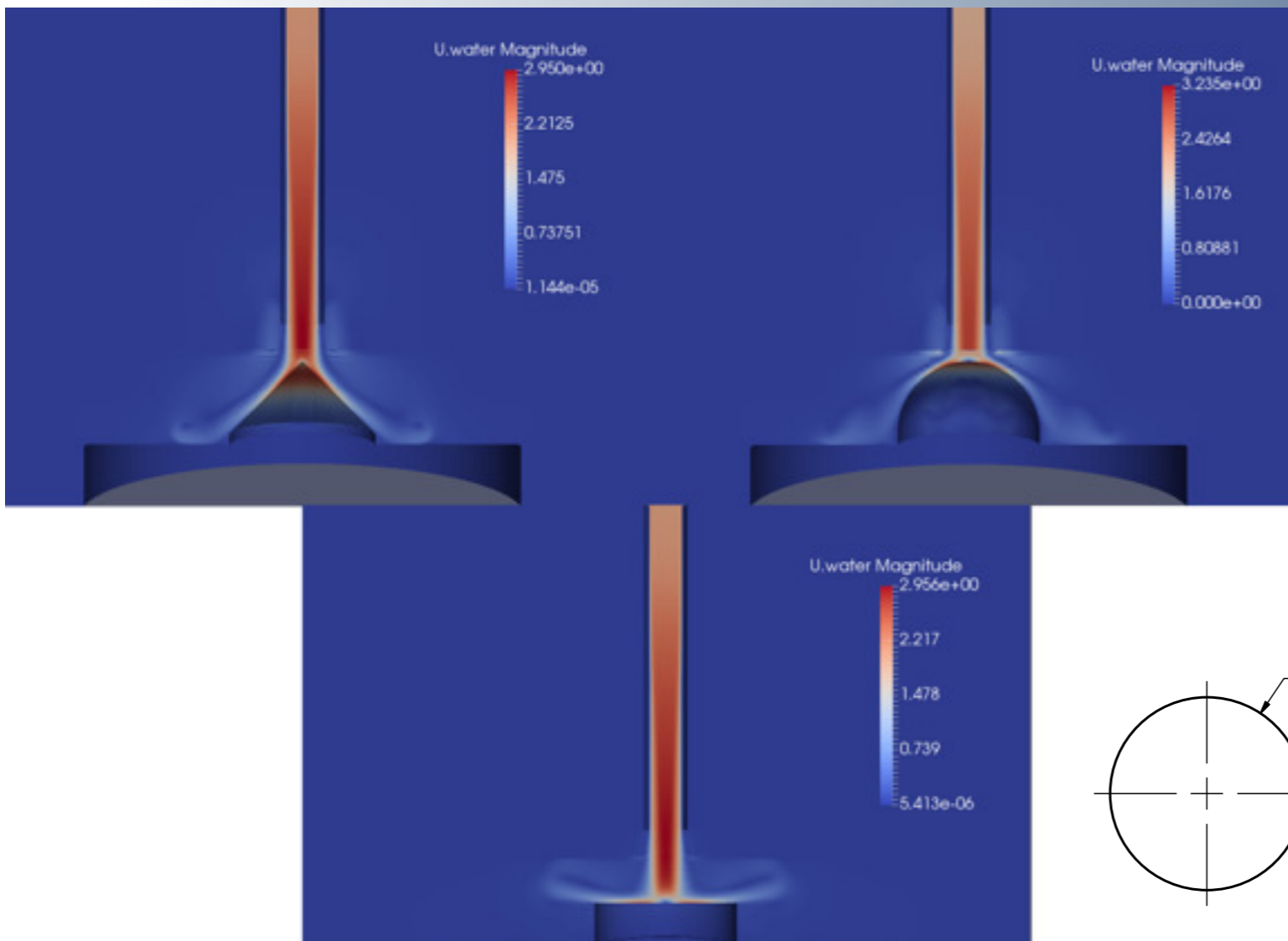


- ♦ 2D slice through Z normal. Particles injected from slave patch

Real geometry setup

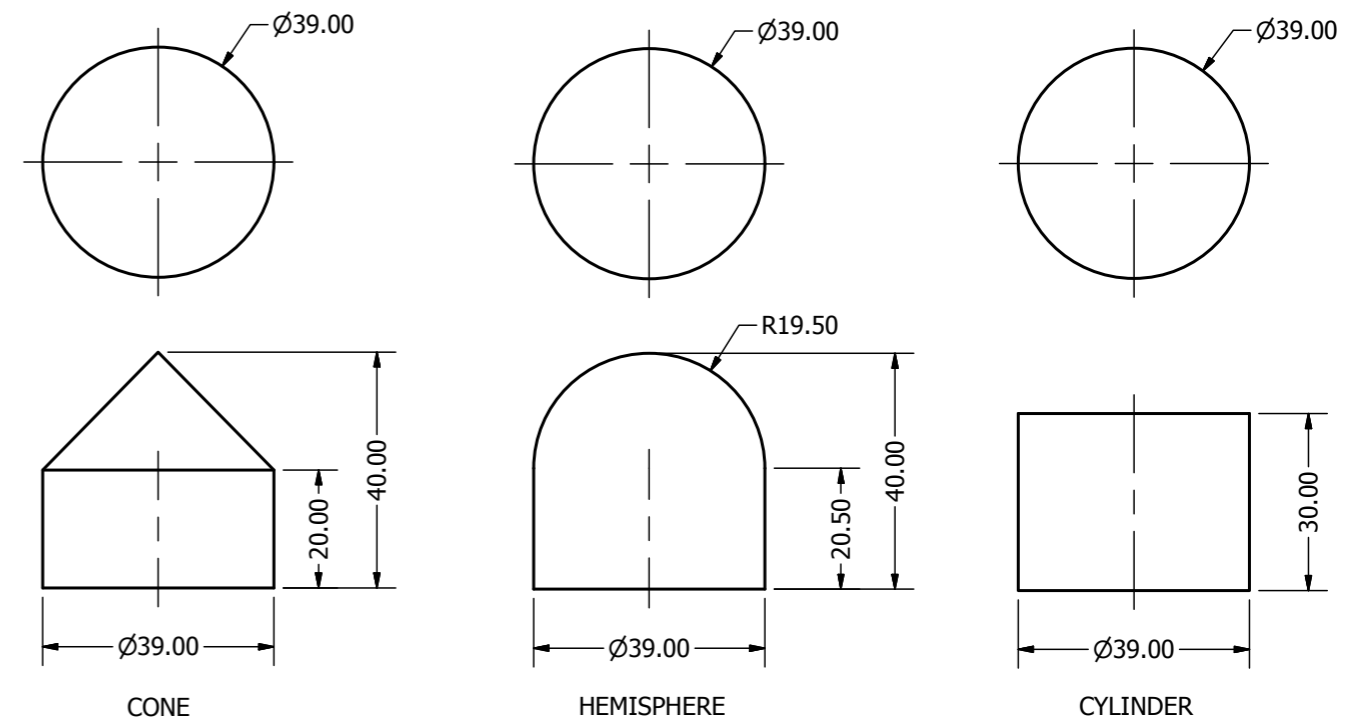


3 sample geometries



New solver was tested on the shown geometries

Particle Image Velocimetry was carried out for validation



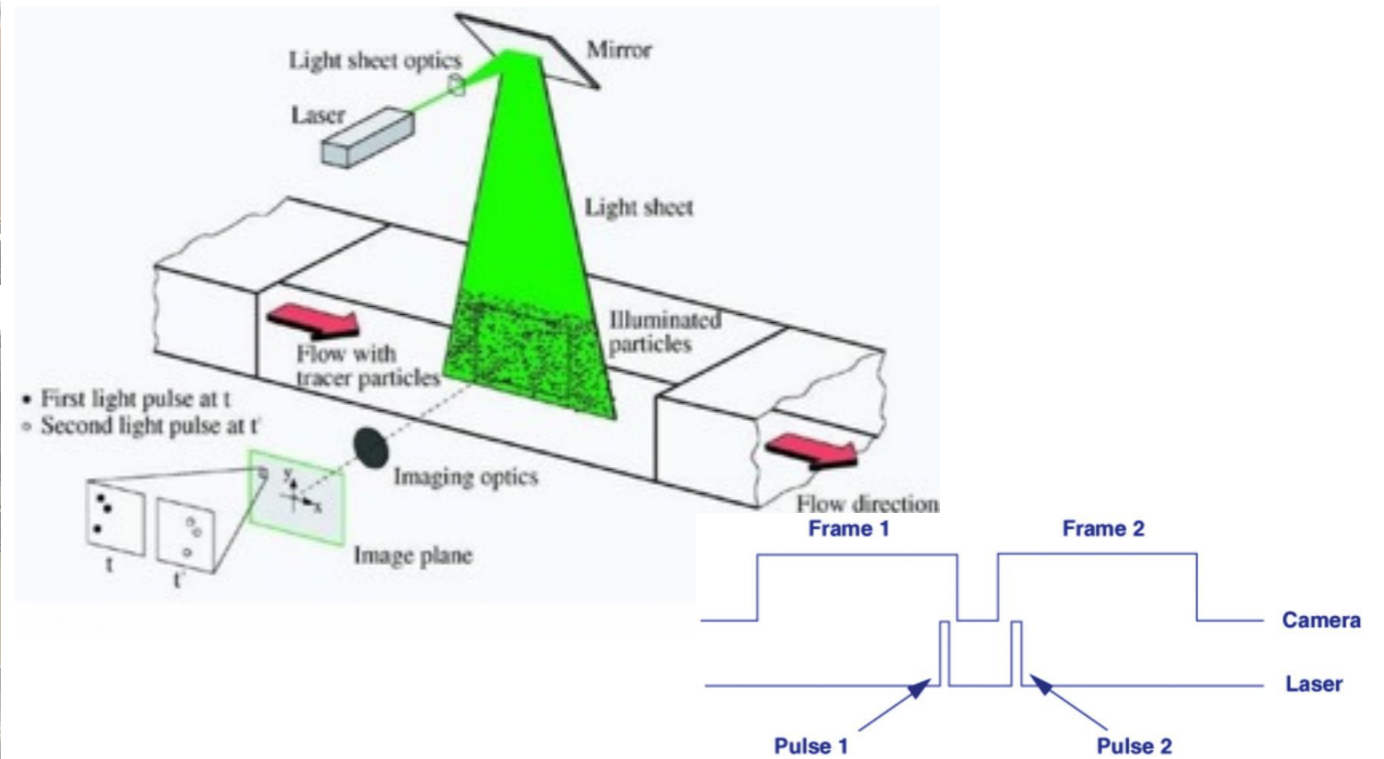
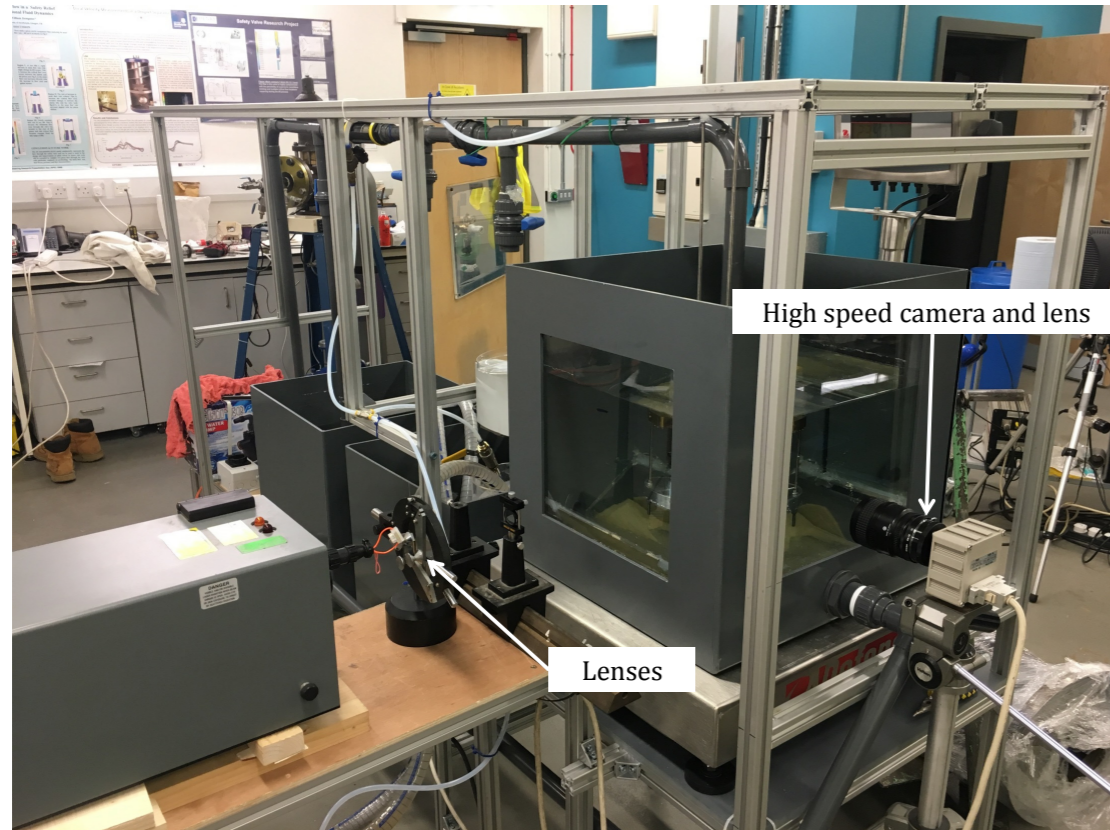
Mass flow inlet ($\sim 2\text{m/s}$)

K-Omega SST turbulence model used

Only first phase compared (**so far**)

DIMENSIONS IN MM

Experimental setup



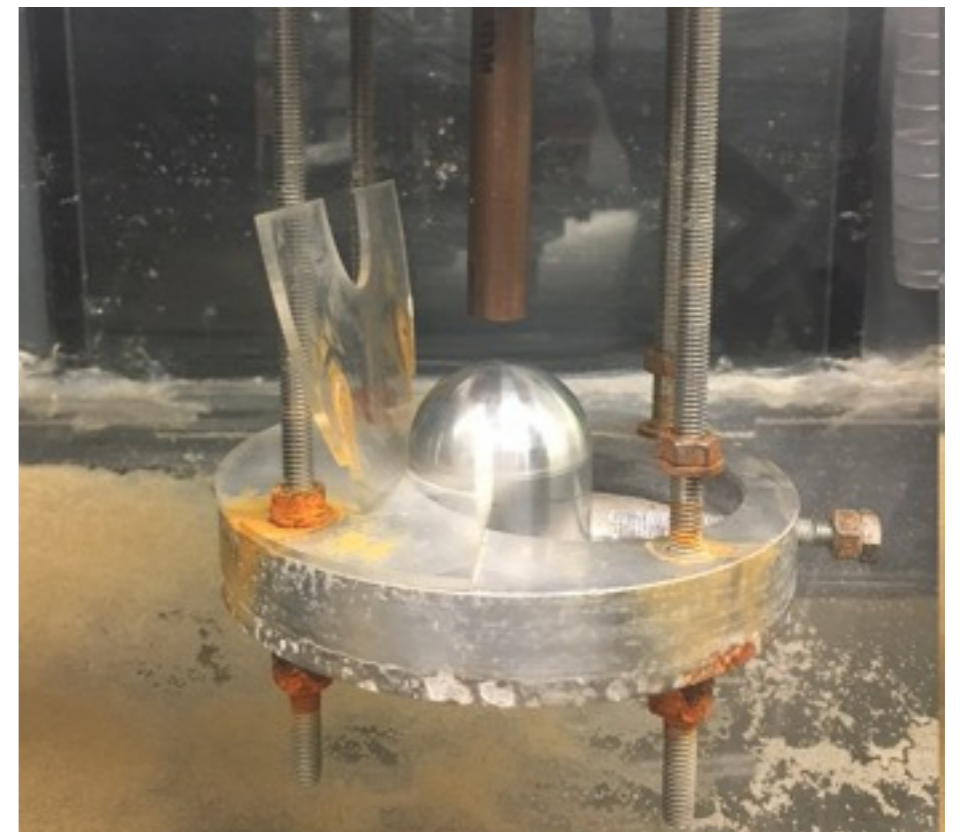
Particle Image Velocimetry

Frame straddling used by laser $\Delta T = 67 \mu s$

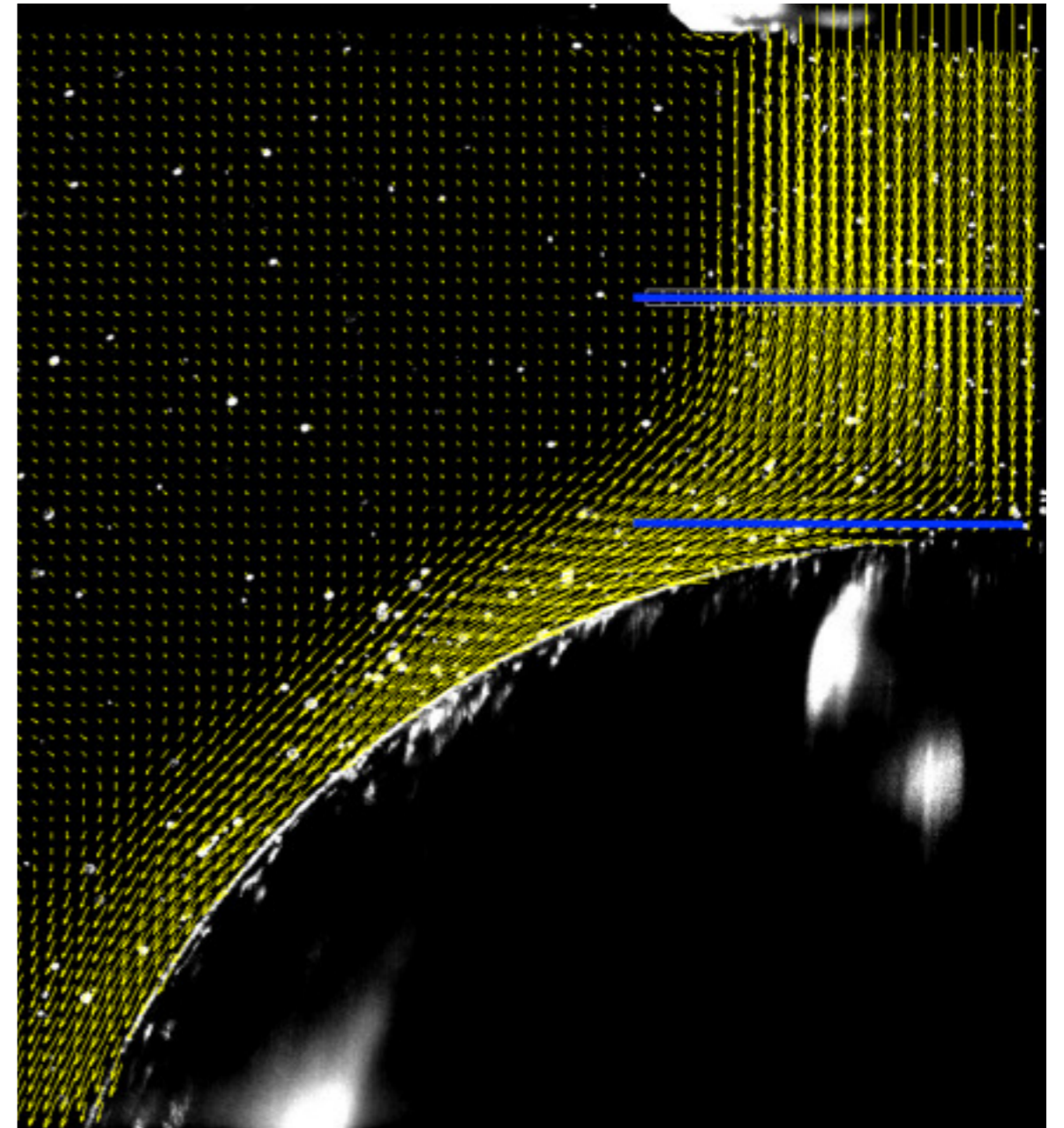
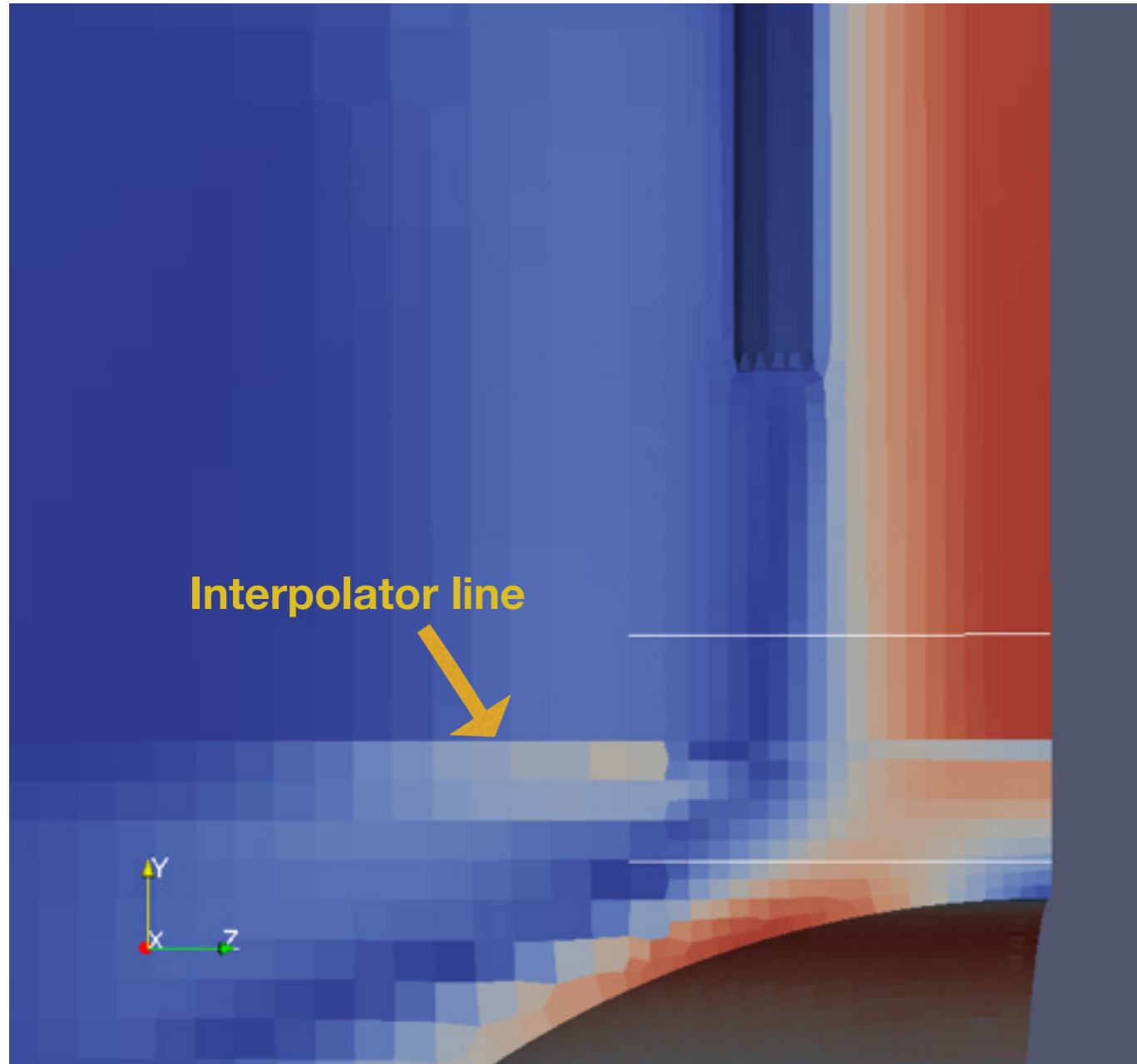
DantecDynamics laser system

250 images used, 125 image pairs

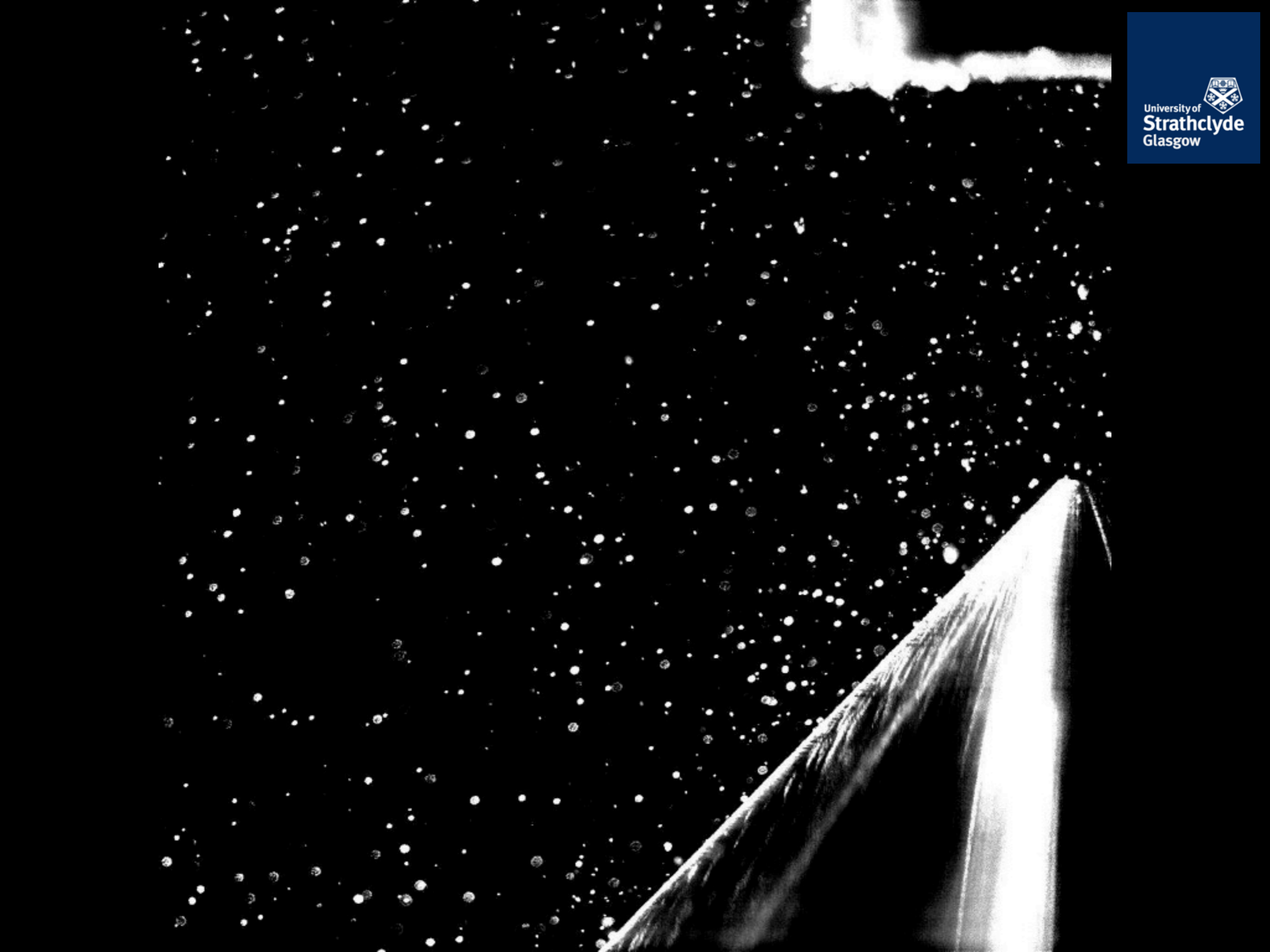
Reynolds numbers of experiments and CFD are both around 10^5 (so are comparable)



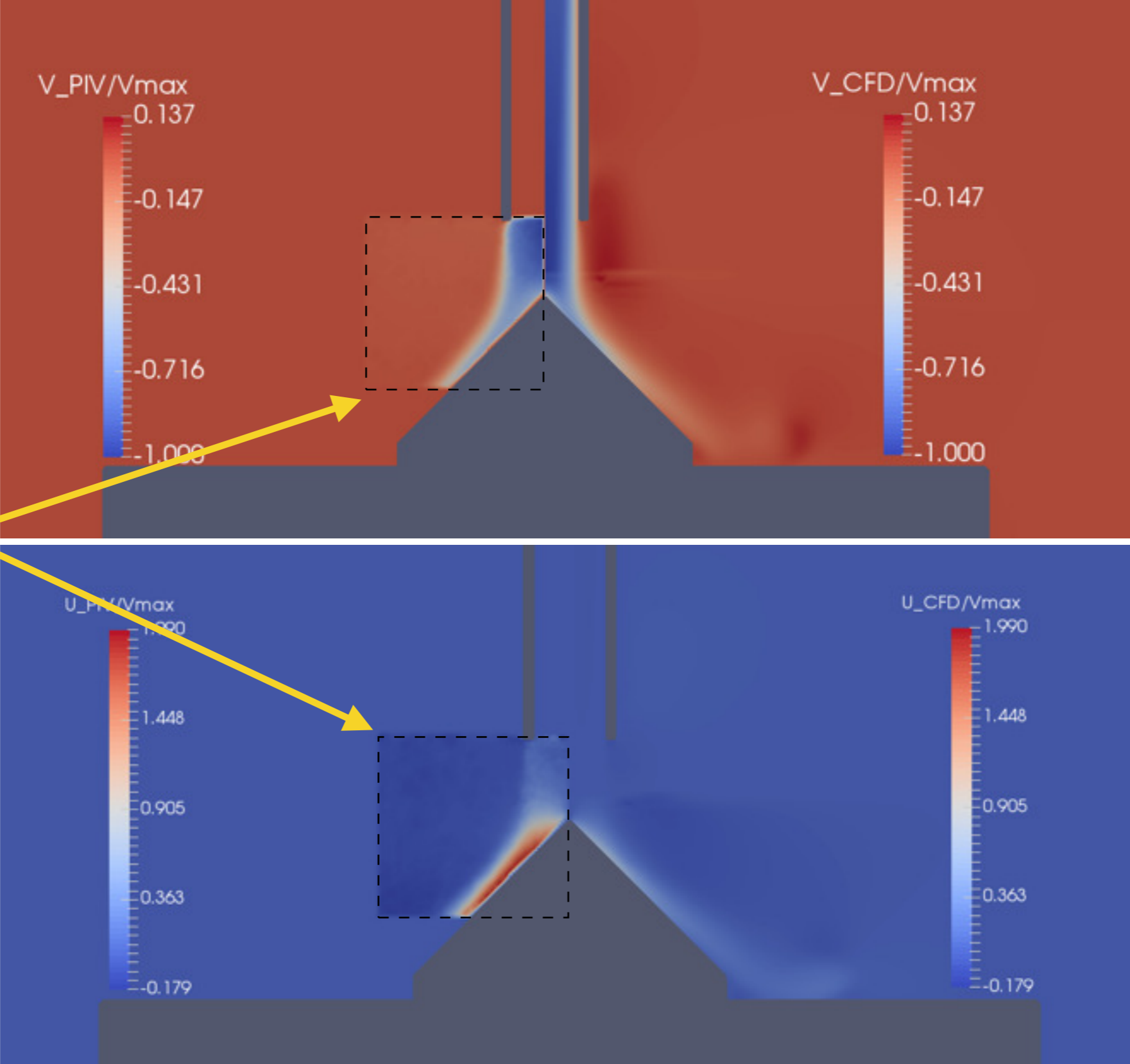
Comparison of data



Lines show where data is taken from:
top is 5mm from nozzle, bottom is 9.5/10mm from nozzle
Interpolator is in between sample lines



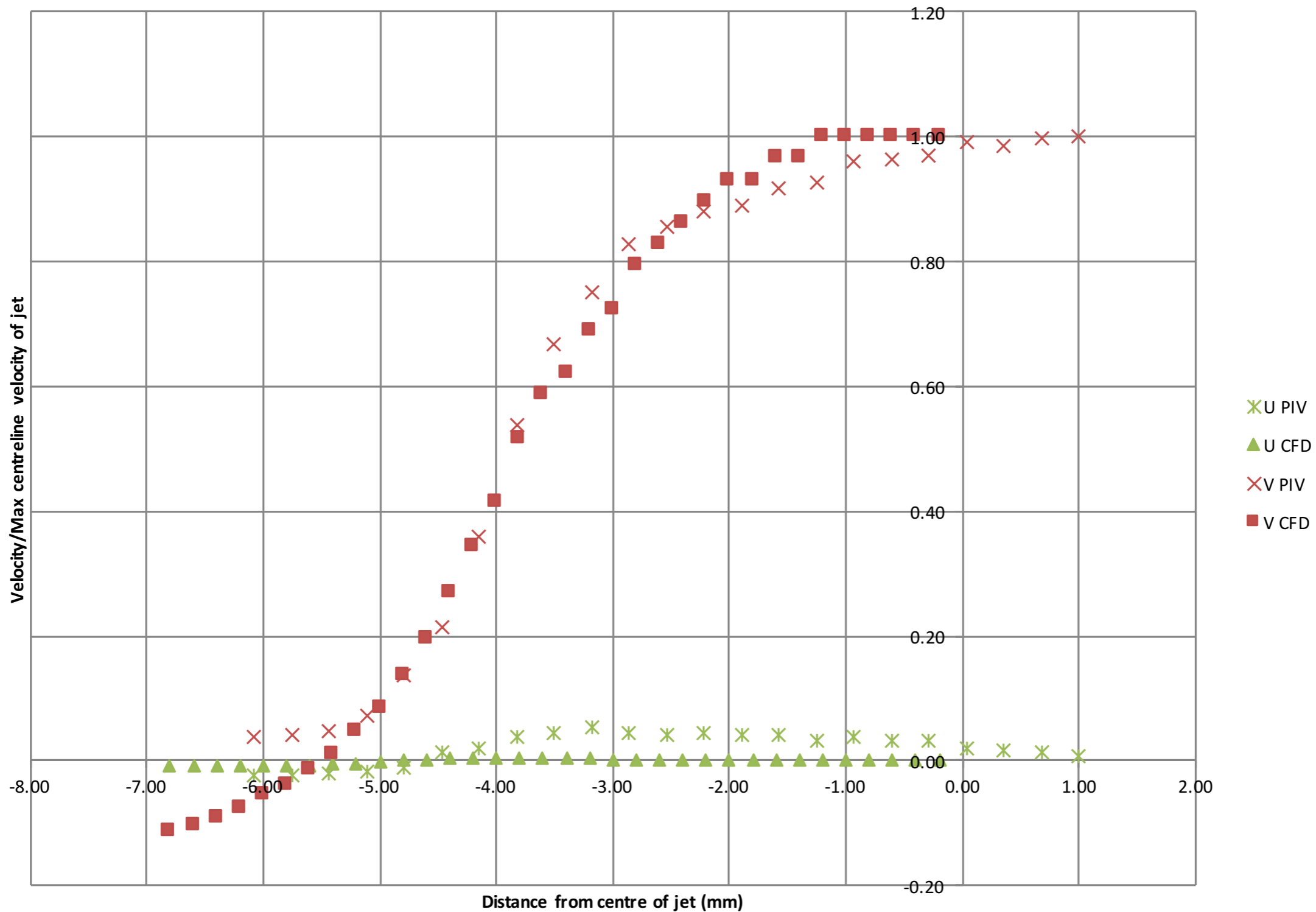
Cone velocity contours



PIV data
(same for
other slides)

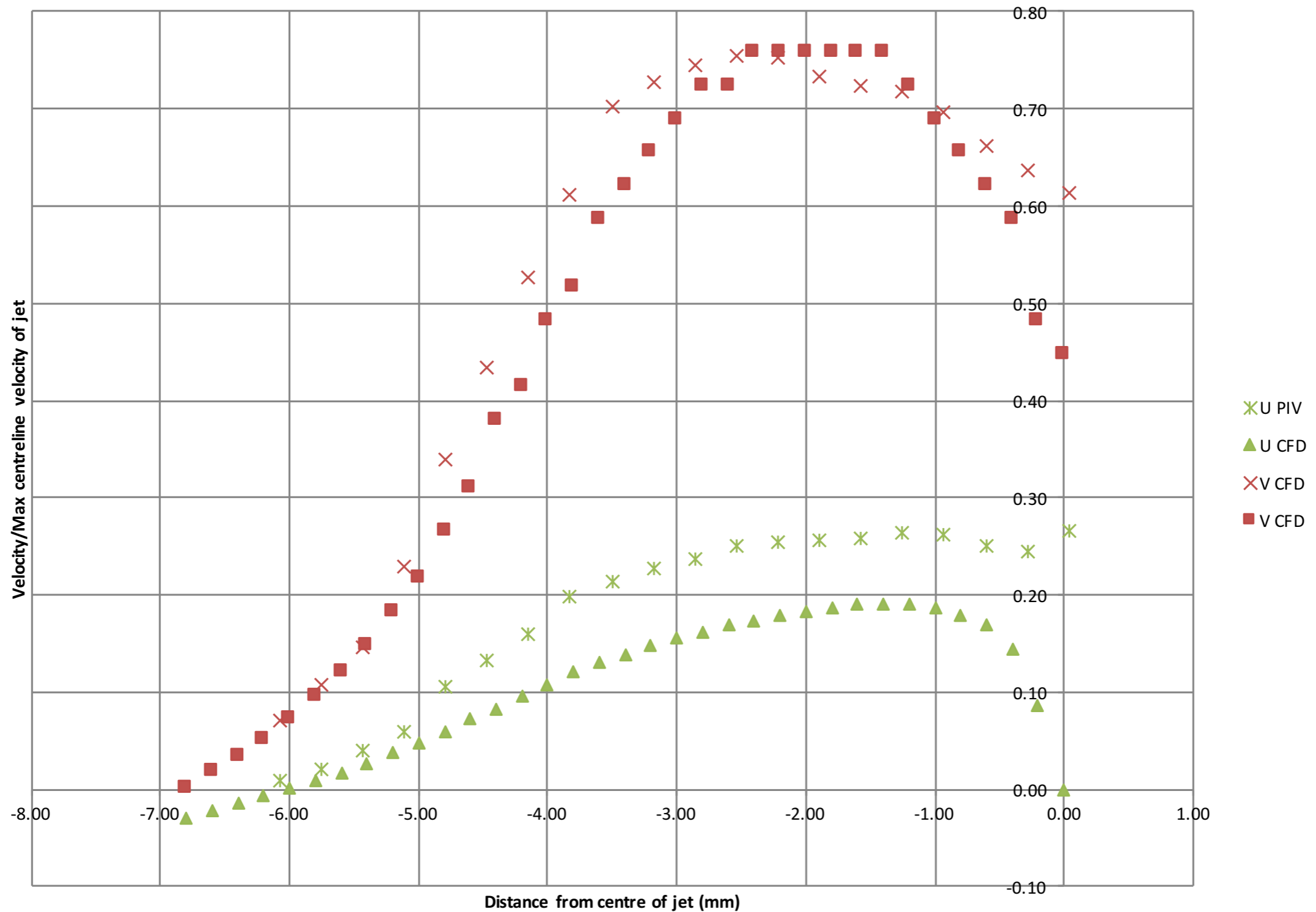
Cone

Cone- 5mm below nozzle exit: velocity profile

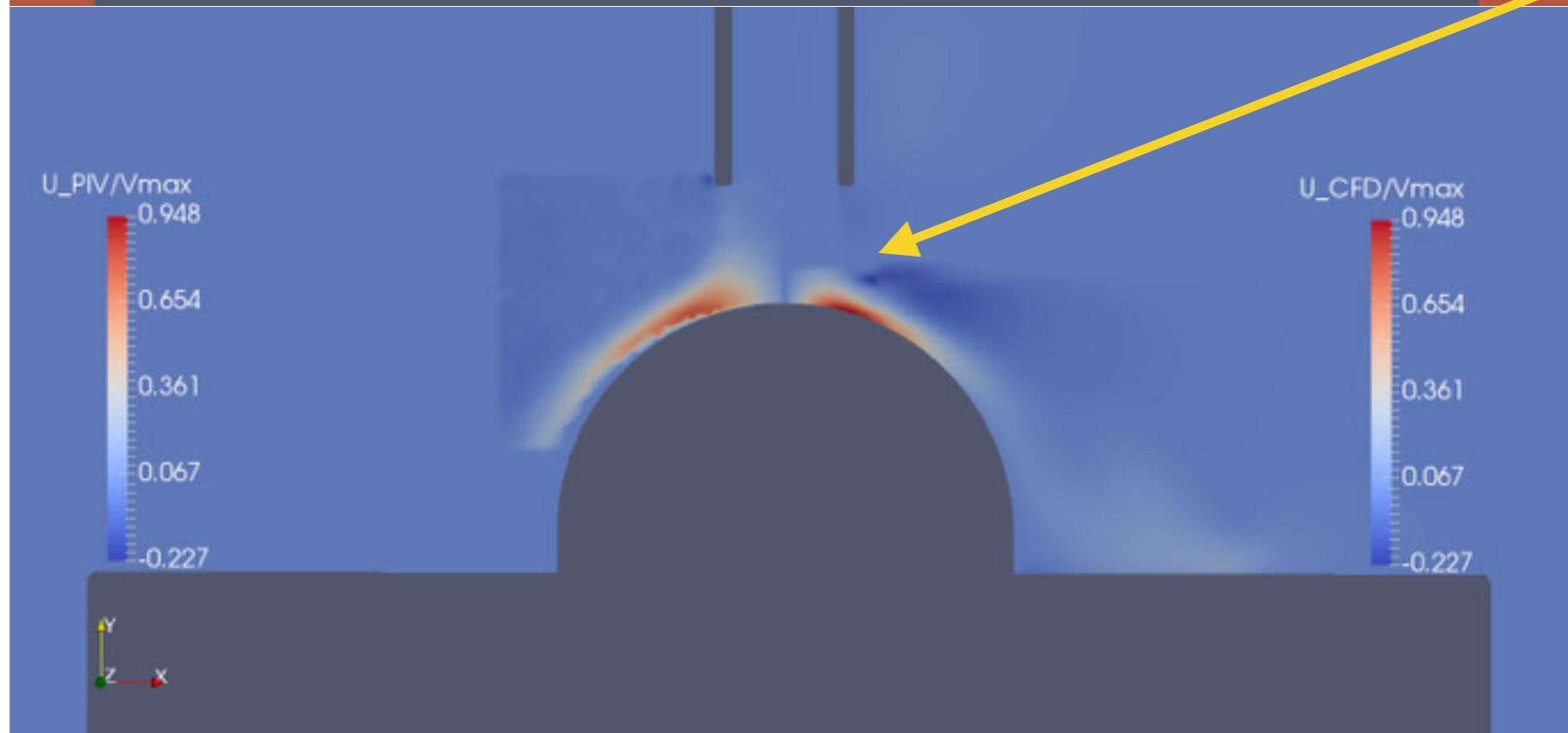
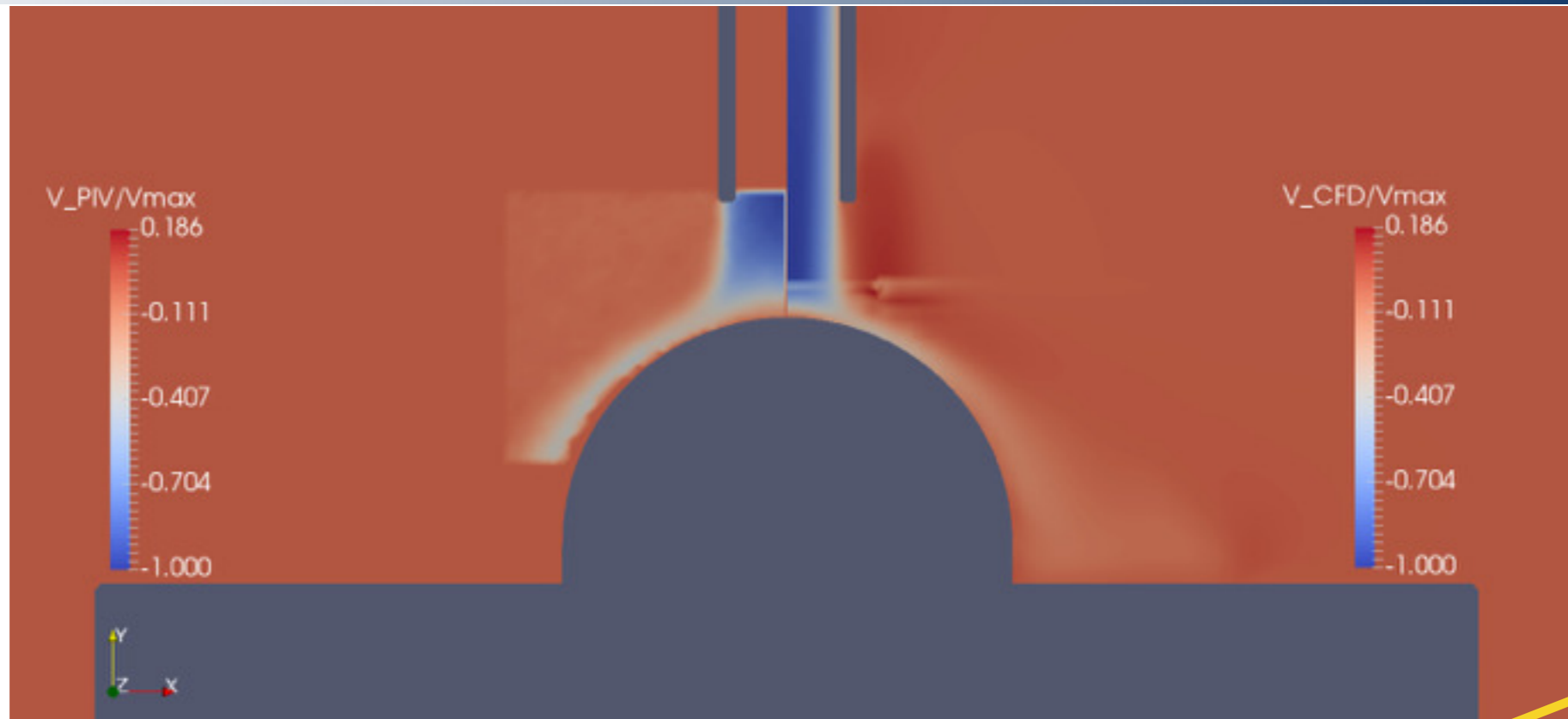


Cone

Cone- 10mm below nozzle exit: velocity profile

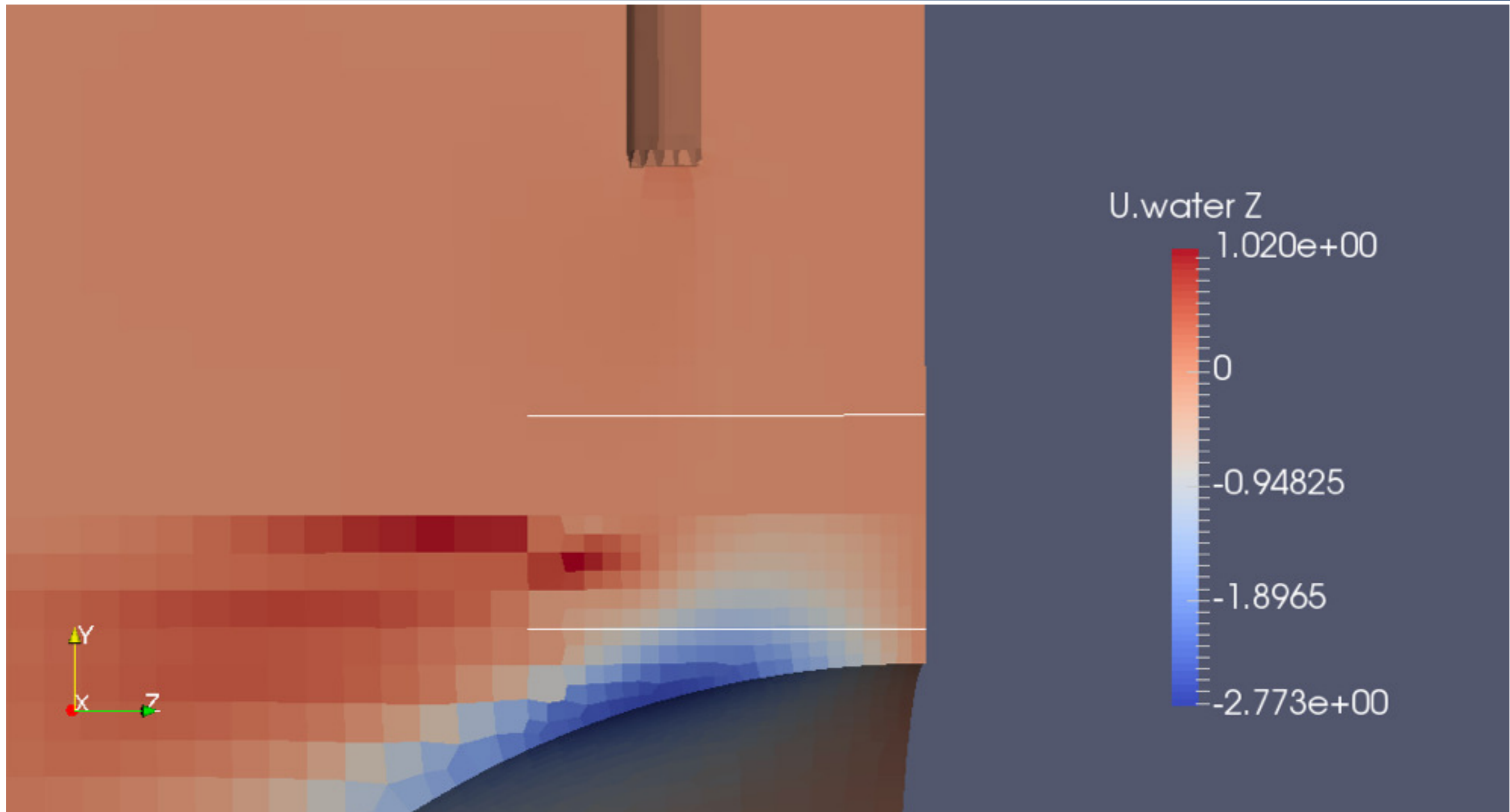


Hemisphere velocity contours



Not interpolating
'U' component
correctly upstream

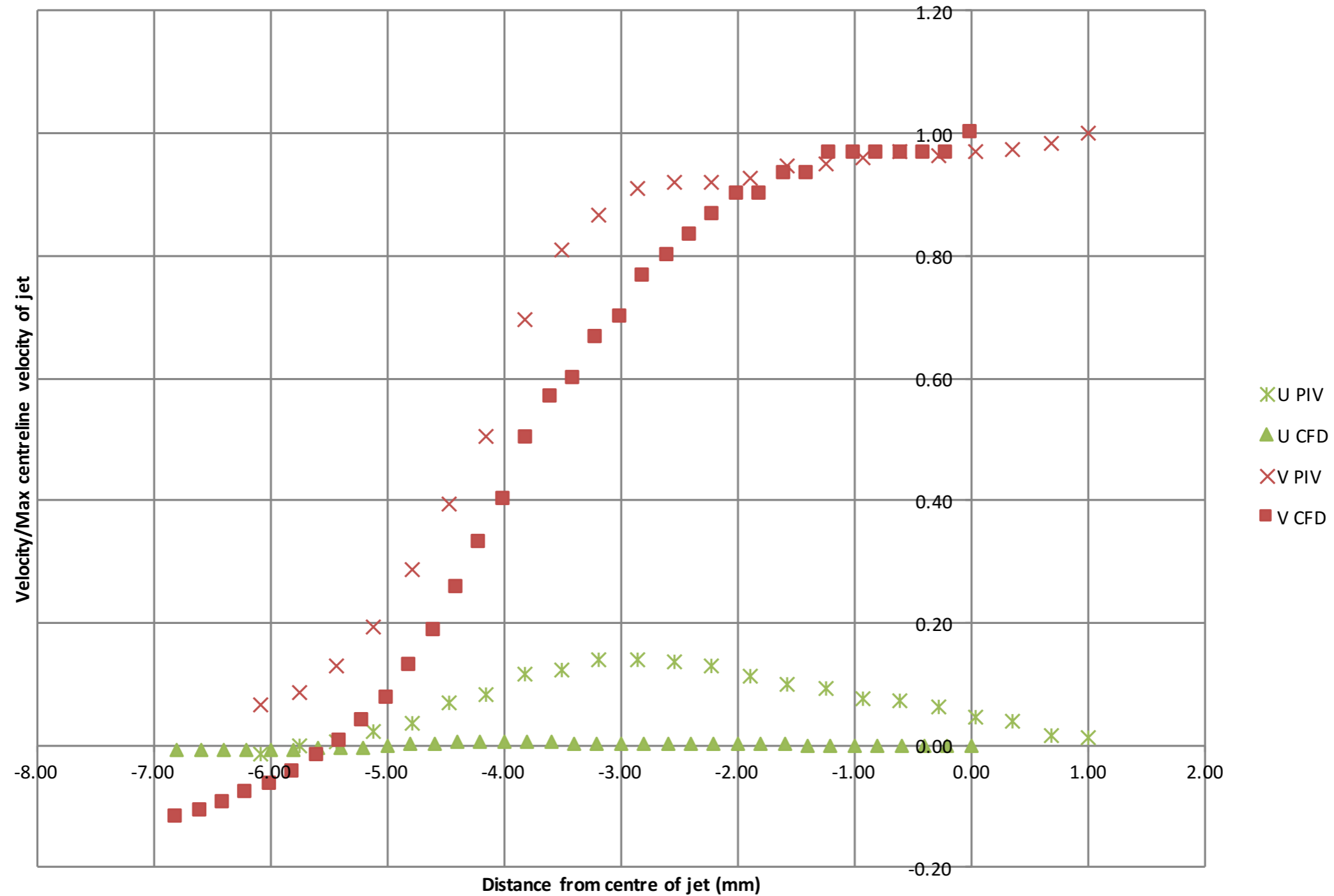
Error in Hemisphere



U.water Z is the horizontal velocity component
There is almost no UZ in region0

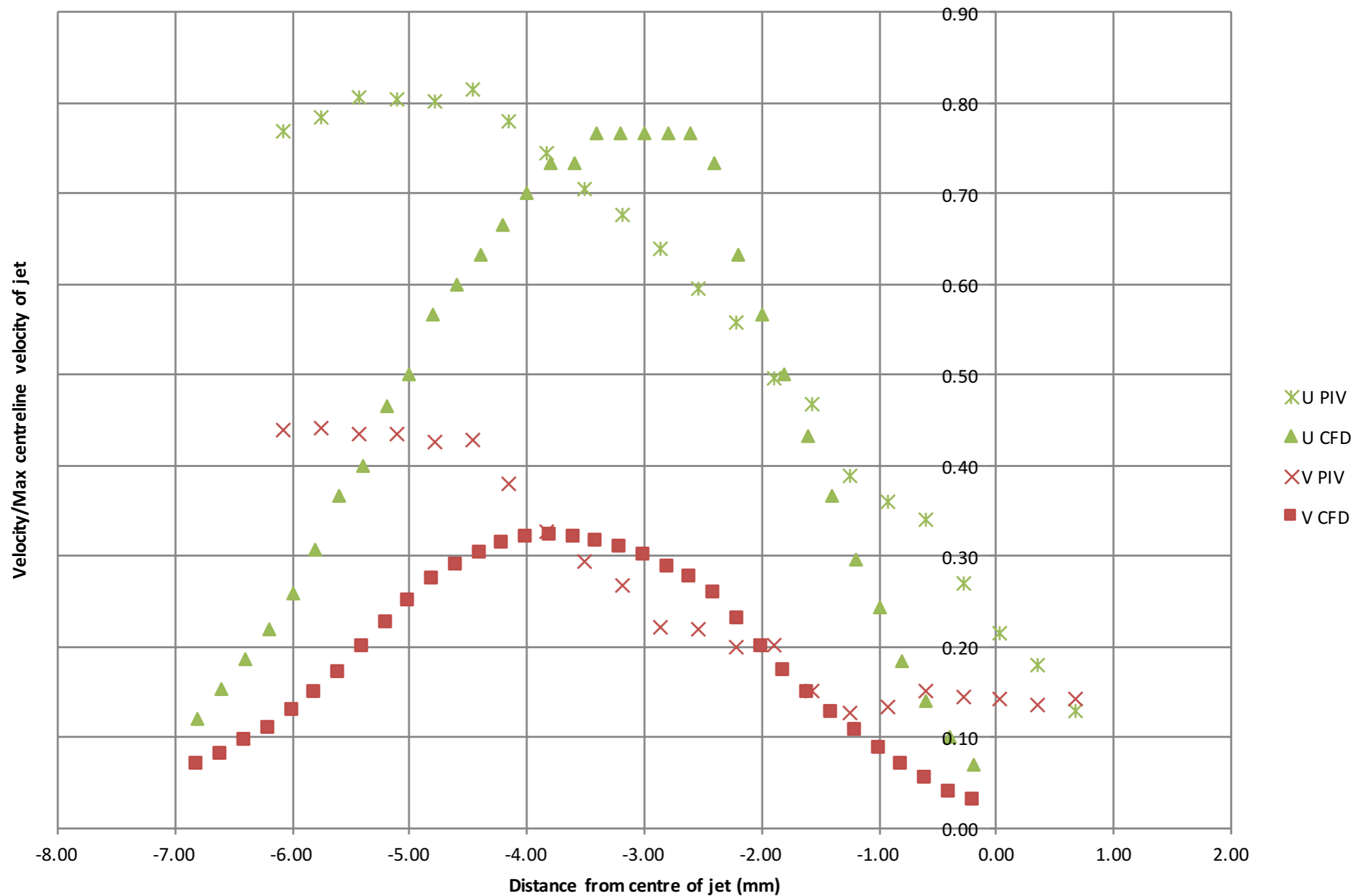
Hemisphere

5mm below nozzle exit: velocity profile

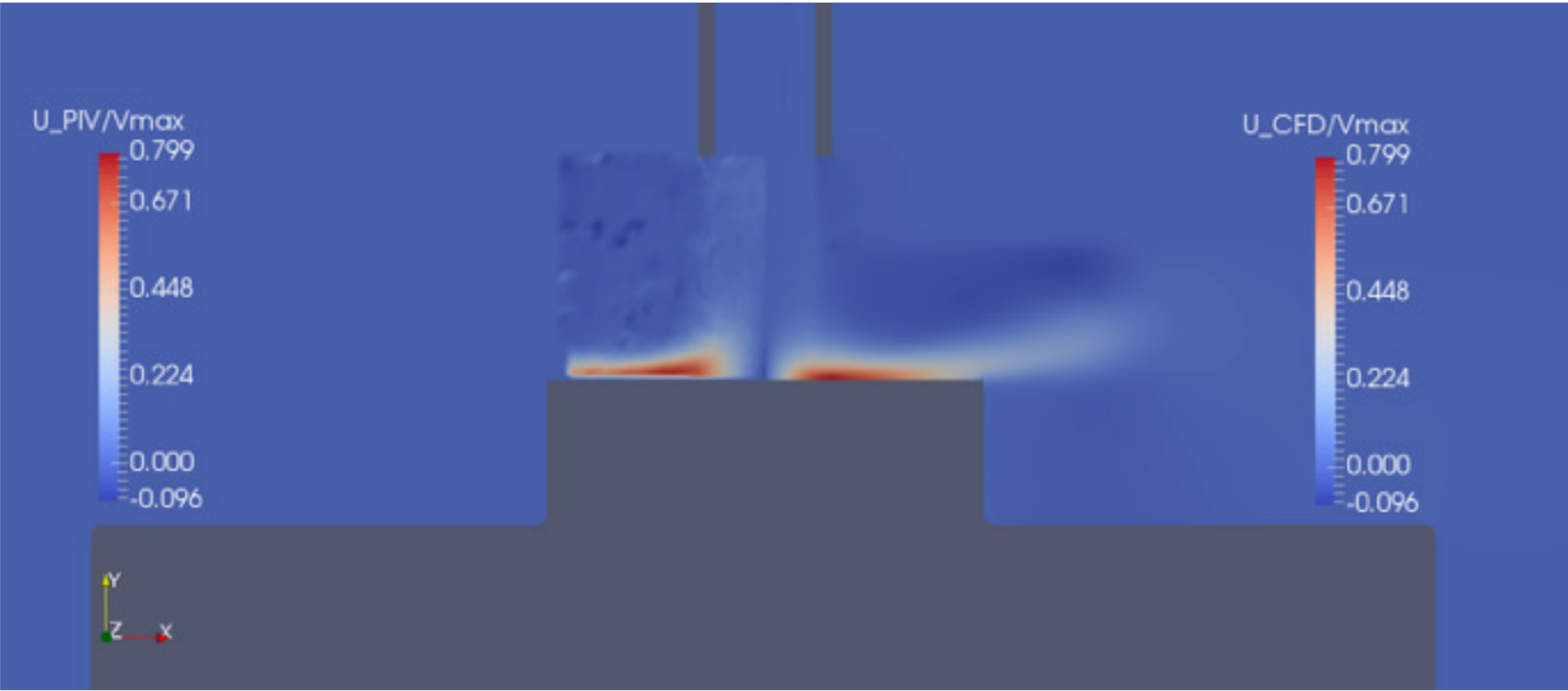


Hemisphere

9.5mm below nozzle exit: velocity profile

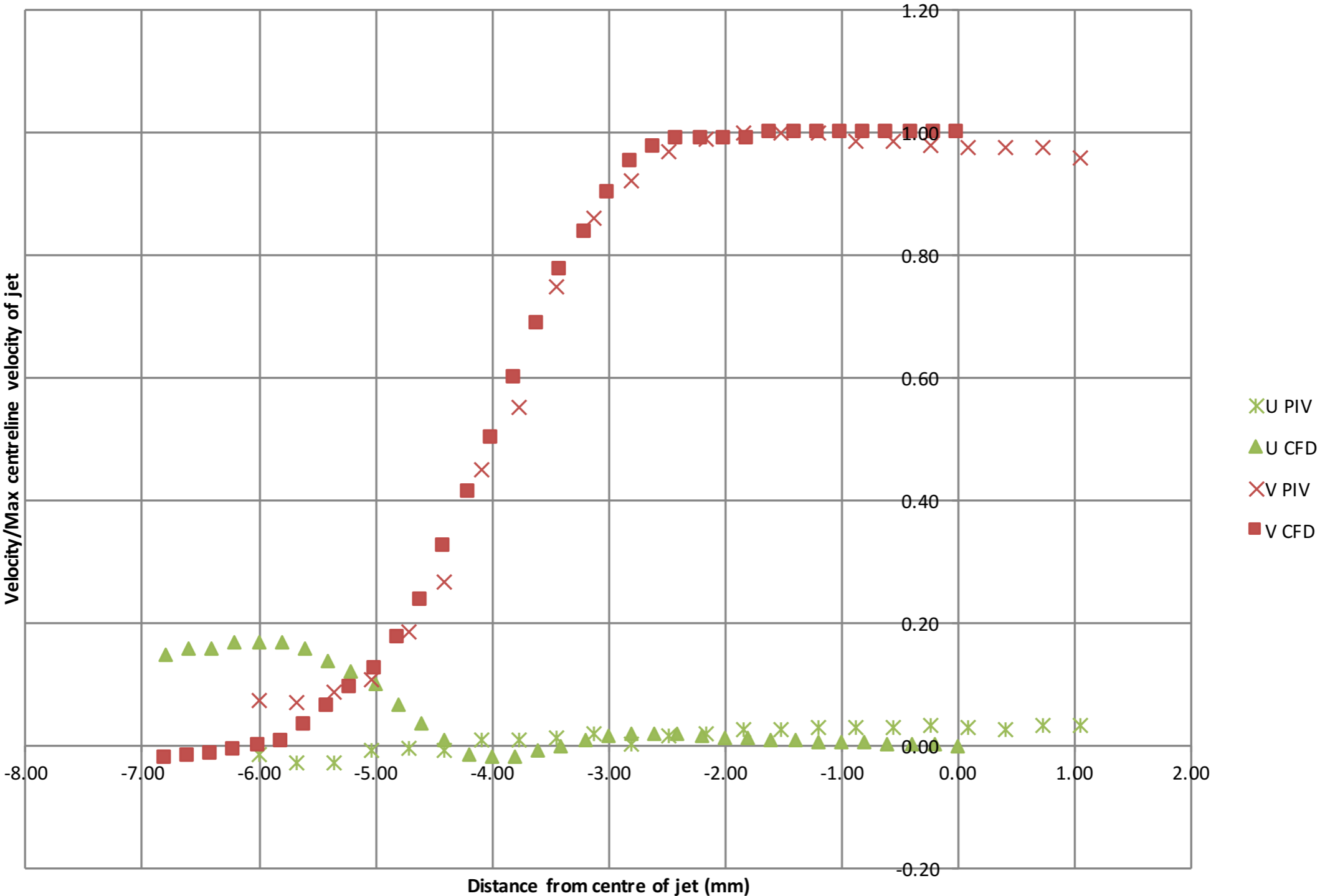


Cylinder velocity contours



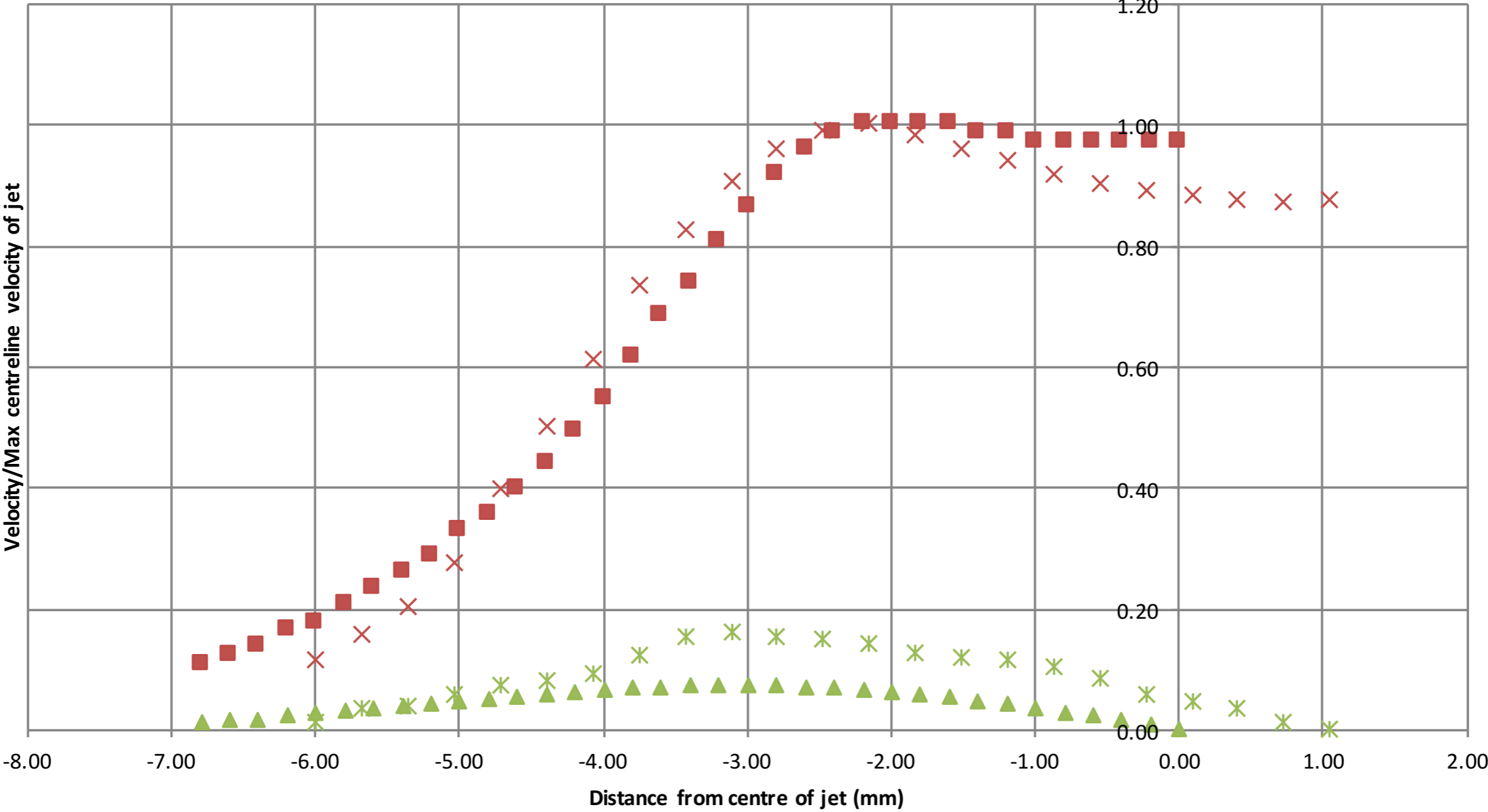
Cylinder

Cylinder- 5mm below nozzle exit: velocity profile



Cylinder

Cylinder- 5mm above sample surface: velocity profile



Future work

- Get particle injections to work properly: couple injection data with injection sites...
- Validate second/particulate phase: particle tracking experiments
- Particles back to fluid?

Conclusion

Work still in progress but...

- Fluid phase shown to work on different geometries
- Solver should dramatically reduce computational time compared to pure EL
- Particle data should still be present near walls, where required
- Enable better design of mining equipment



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Thank you

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