

On-Orbit CubeSat Performance Validation of a Multi-Mode Micropropulsion System

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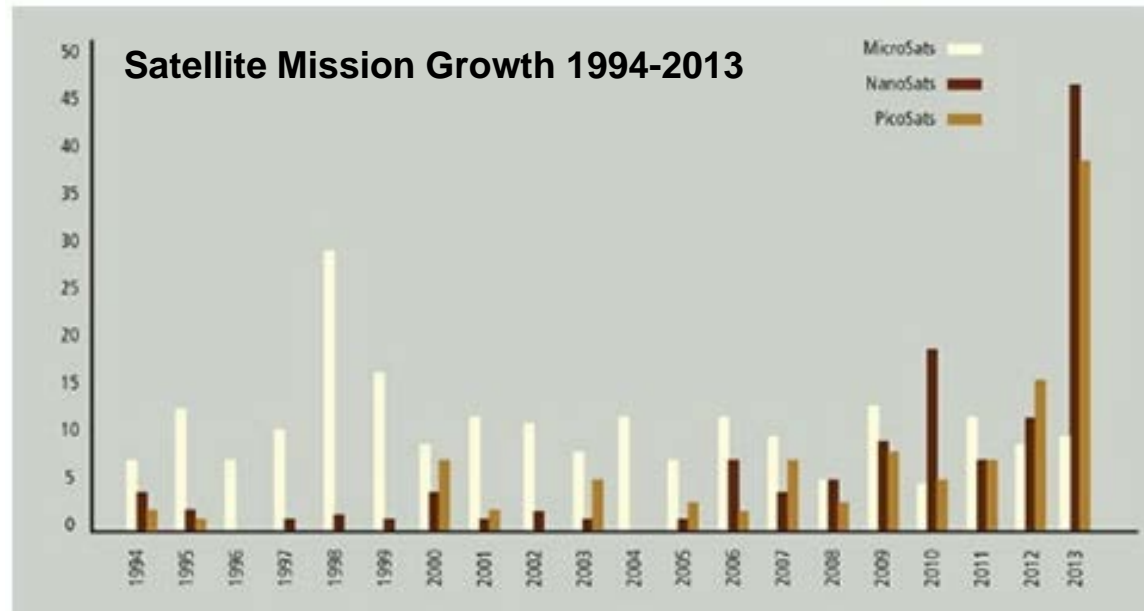
Missouri University of Science and Technology

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Mission Context

- CubeSat missions have grown exponentially, becoming the most popular form of small satellite



Gustafson, Charles L., and Siegfried W. Janson. "Think Big, Fly Small." The Aerospace Corporation. *Crosslink Magazine*, 1 Sept. 2014. Web. 07 Feb. 2017.

- In spite of this rapid growth, development of propulsion systems for small satellites has lagged behind



One Possibility: Multi-Mode Thruster



- Multi-Mode SmallSat Propulsion Mission: a technology demonstration of a single propulsion thruster operable in...
 - catalytic chemical mode
 - electrospray electric mode
- ...using the same propellant!
- Can be integrated into a CubeSat form factor

APEX CONOPS

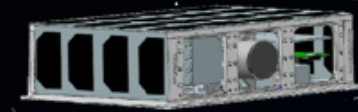
(The Advanced Propulsion Experiment)



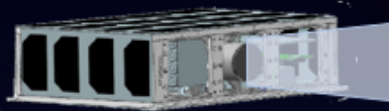
1. Launch/Separation
2. Initialization



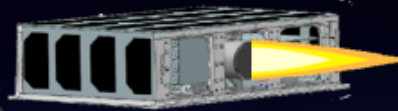
3. Detumble



**4. Cruise to Desired
Orbital Position**



5. Electrical Burn
Centered Around Argument of
Latitude of 90 degrees



6. Chemical Burn
Centered Around Argument of
Latitude of 90 degrees



7. End of Life
(Propellant Depleted)

Payload Description

- **Utilizes Non-toxic, Green Ionic Liquid Propellant**

- Can extract ions
- Energetic and capable of exothermically decomposing

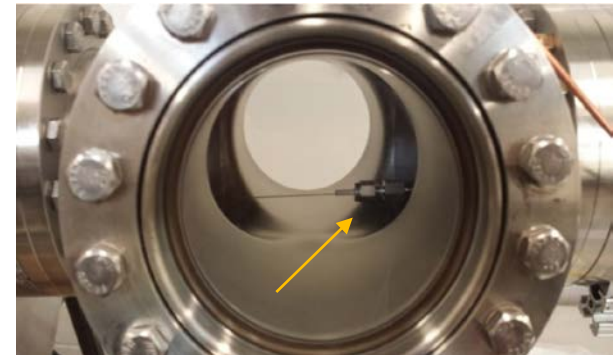
- **Chemical Mode**

- Propellant fed to thruster at high flow rate
- Combination of applied heat and catalytic microtube ignite propellant

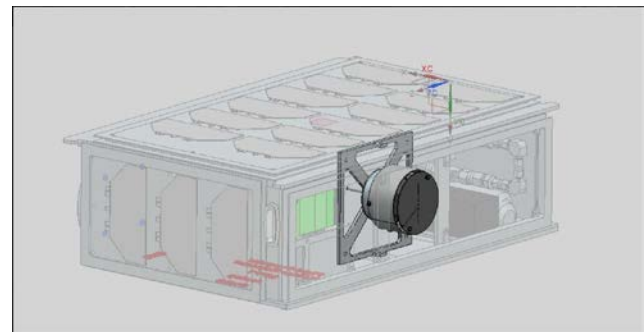
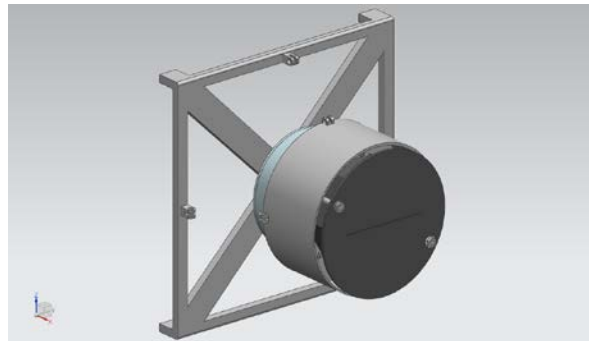
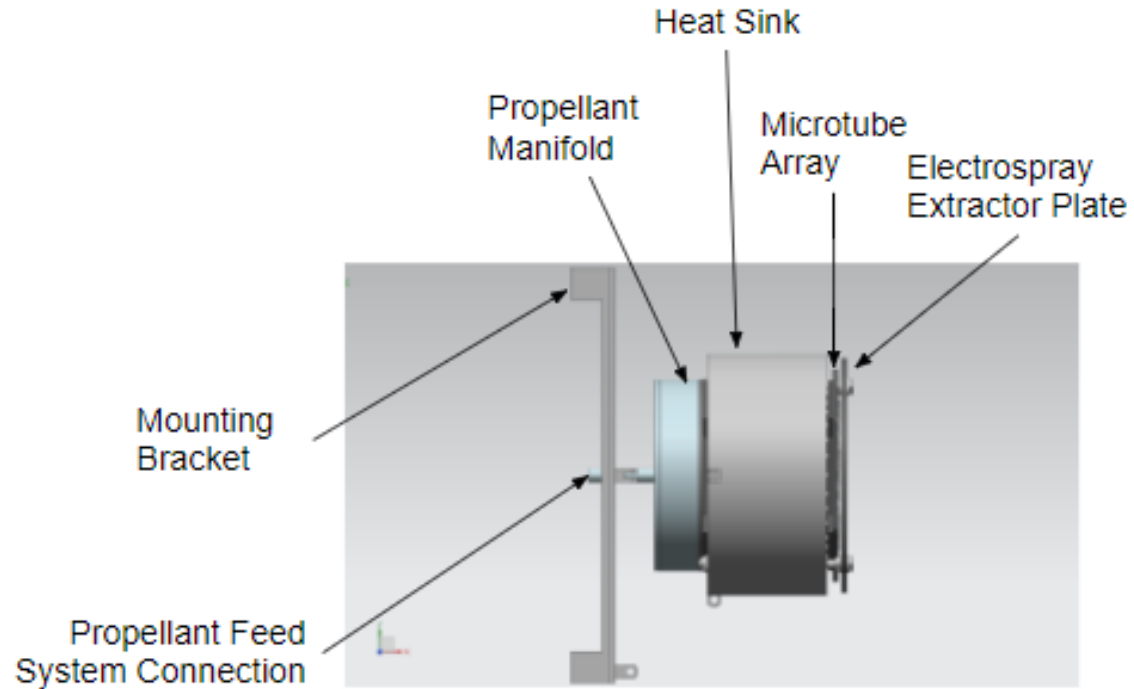
- **Electric Mode**

- Propellant fed to thruster at low flow rate
- Voltage potential applied between emitter and extractor to release ions from propellant

Preliminary testing of chemical mode with a single emitter in vacuum chamber



Payload Description



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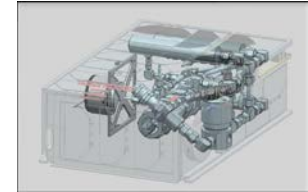
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Challenges

- Mass and Volume Constraints: 6U
- Power Constraints: Electric mode requires 3400 V in a compact circuit
- Communication: Pointing constraints
- Propulsion hardware
- Accuracy of GNC hardware
- Capabilities of thruster itself
- **Thruster Validation**
 - Thruster data downlinked for comparison with ground testing
 - Thrust measured using orbit/attitude changes



Validation Through Propulsion Engineering Data



- **Pressure**
 - Feed system pressure will be measured by pressure transducers in the feed system
 - Provides values just before the propellant storage system and thruster
 - Expected value: 200 psi
- **Temperature**
 - Thermal sensor on the propellant storage system will provide a reference temperature to compare with readings from thermocouples in the thruster itself
 - Expected combustion temperature: 1900 K (1627 degrees Celsius)
- **Voltage**
 - Thruster extractor voltage will be measured by voltage dividers on the digital circuit board at a rate of 1 Hz during electric mode burns
 - Expected value: 3.4 kV



Validating Thruster Performance with Measured Orbit Changes

- Direct thrust measurement with IMU
- Measuring attitude change
- Measuring orbit change
 - Altitude changing maneuver
 - Inclination changing maneuver
 - RAAN changing maneuver

Restrictions: Limited quantity propellant (75 cm^3)



Inertial Measurement Unit Acceleration

- IMU accuracy of 5 mG (0.049 m/s²)
 - Largest thrust detectable: 0.43 N (for a satellite mass of 8.6 kg)
- Chemical Mode
 - ~1 newton thrust
 - Acceleration can be measured
- Electric Mode
 - ~0.00025 newton thrust
 - Acceleration undetectable



Attitude Change Results

Minimum IMU detectability: 0.21 deg/s with factor of safety = 2

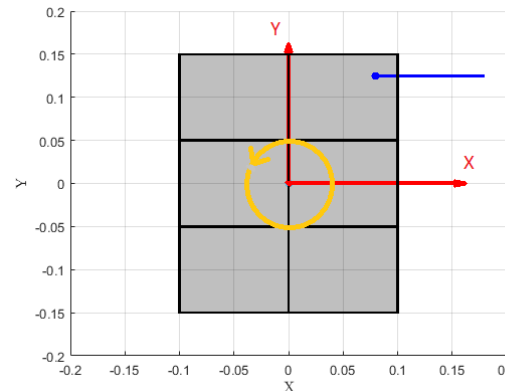
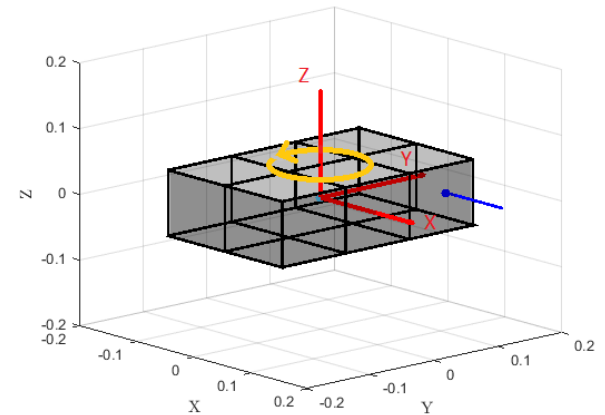
Positioning Thruster to Generate Maximum Torque:

Chemical:

- Burn Time = 1.14 sec or longer
- Change = 0.21 deg/sec

Electric:

- Burn Time = 1.06 hours or longer
- Change = 0.21 deg/sec

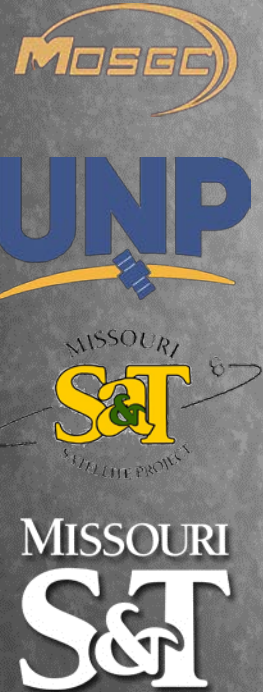
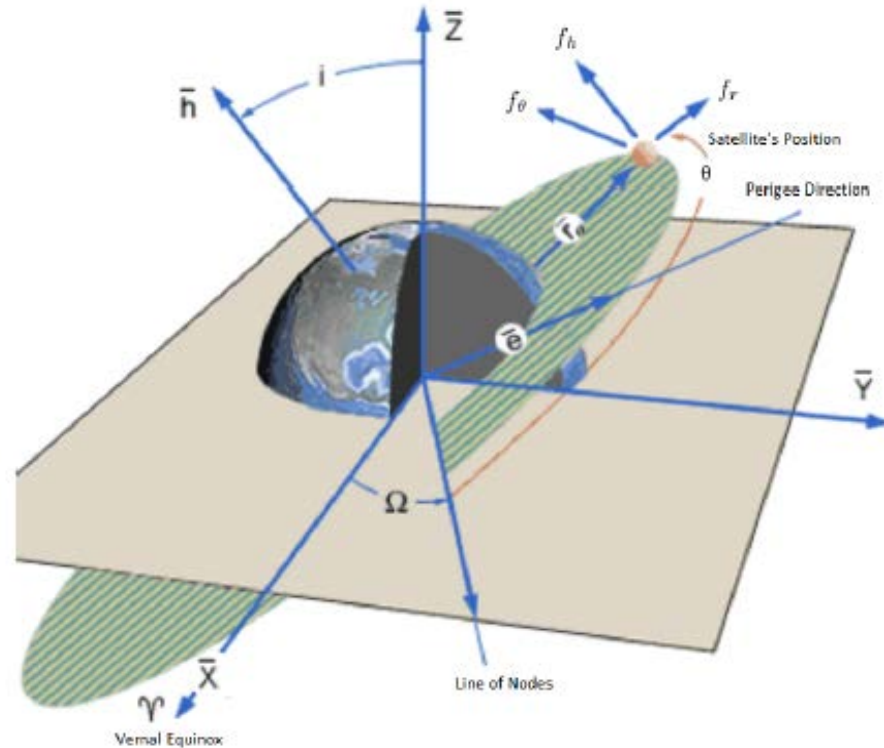


Orbit Changing Maneuver

- Key question: What orbital element gives best “bang-for-the-buck” measurability?

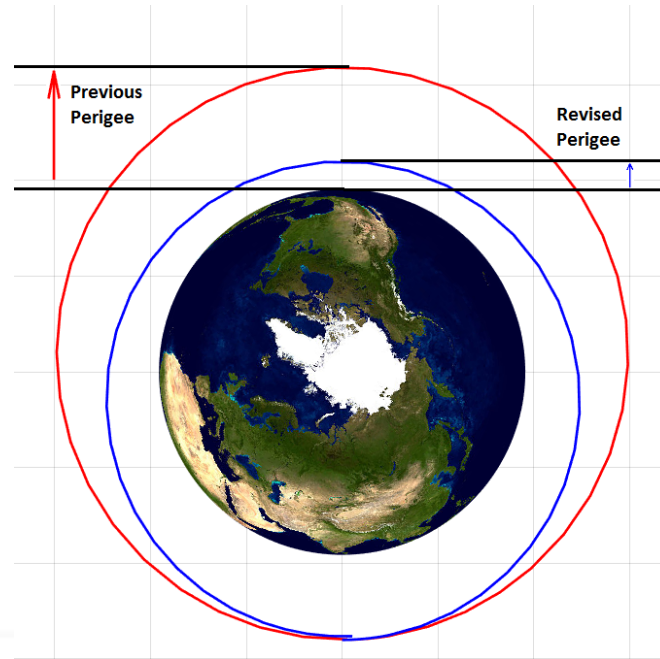
Initial Conditions:

a (km)	e	i	Ω	ω	r (km)
6753.14	0	45°	45°	90°	6753.14

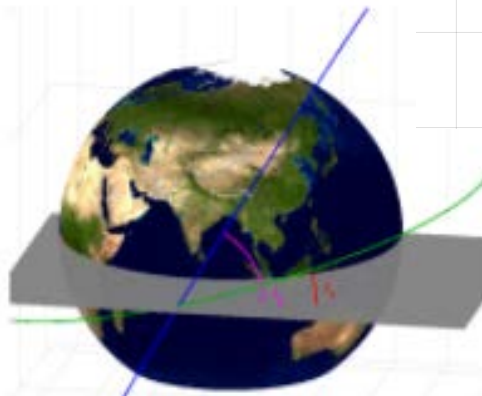


Altitude, Inclination, & RAAN Change

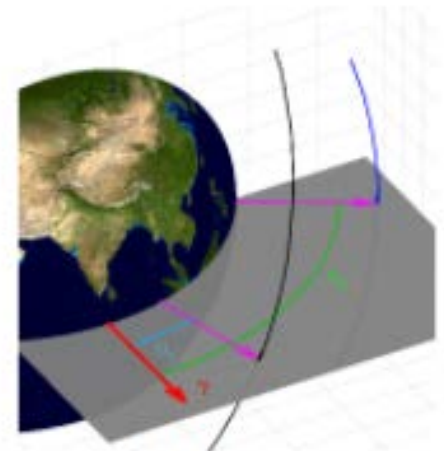
- Inclination: centered about ascending/descending nodes
- RAAN: centered about argument of latitude $\theta = \pm 90^\circ$



Periapsis Altitude
Change Diagram



Inclination Change
Diagram



RAAN Change
Diagram

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Element Sensitivity Analysis

Maneuver Type	Mode	Burn Length (sec)	Change
Periapsis Altitude	Chemical	5	2.014 km
	Electric	1000	0.106 km
Inclination	Chemical	5	0.00434°
	Electric	1000	0.00021°
RAAN	Chemical	5	0.00613°
	Electric	1000	0.00030°

- RAAN is the clear “winner”
- Now how do we measure the RAAN change and use that to quantify thruster performance?



Quantifying Thruster Performance

- Orbit determination algorithms used to determine orbital elements (RAAN change) using GPS data/measurements
- Attitude determination and control used to maintain thrust normal to orbit plane
- By integrating the Gauss Variational Equations (with constant thrust/mass) the thrust can be determined analytically



Gauss Variational Equations

$$\dot{h} = r f_{\theta}$$

$$\dot{e} = \frac{r}{h} [\sin \theta (1 + e \cos \theta) f_r + (e + 2 \cos \theta + e \cos^2 \theta) f_{\theta}]$$

$$\dot{i} = \frac{r f_h}{h} \cos \theta$$

$$\dot{\Omega} = \frac{r f_h \sin \theta}{h \sin i}$$

$$\dot{\omega} = \frac{r}{h e} [-\cos \theta (1 + e \cos \theta) f_r + \sin \theta (2 + e \cos \theta) f_{\theta}] - \frac{r f_h \sin \theta \cos i}{h \sin i}$$

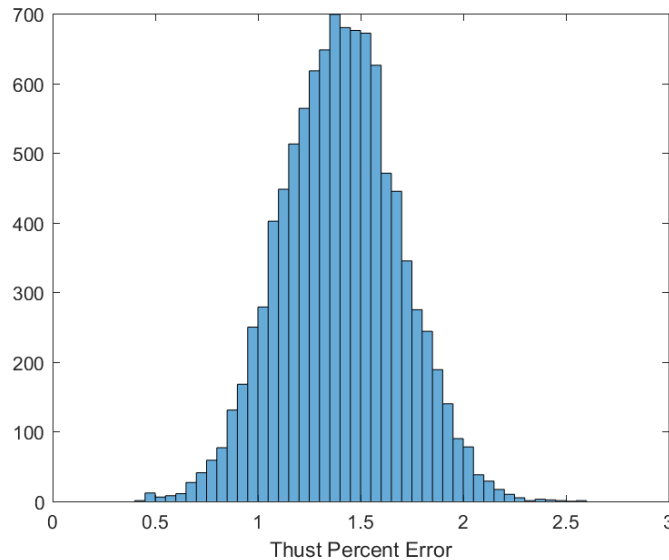
$$\dot{\theta} = \frac{h}{r^2} - \frac{r f_h \sin \theta \cos i}{h \sin i}$$



Thruster Performance Cont.

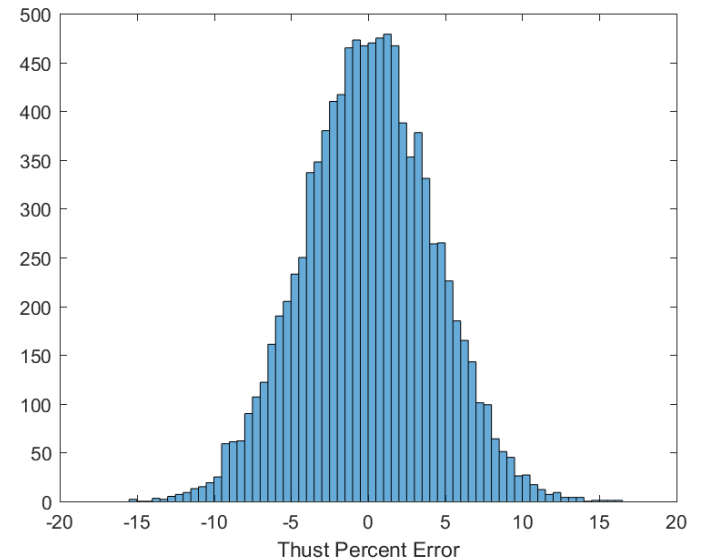
- Considering the accuracy of GPS data we are confident in being able to determine the thrust within 10% of the true value

Monte Carlo, 10000 Runs, Burn Time 5 sec



Chemical Mode (1 N thrust)

Monte Carlo, 10000 Runs, Burn Time 1500 sec



Electric Mode (0.25 mN thrust)

Ω noise: $\sigma = 12.72 \mu\text{-degrees}$



Final Remarks

- Thruster qualitatively validated with downlinked engineering data
- Thruster quantitatively validated using change in RAAN
- Considering also corroborating with change in inclination and IMU/accelerometer
- Considering expanding our paper, after receiving reviewer feedback, to apply to more general CubeSat missions

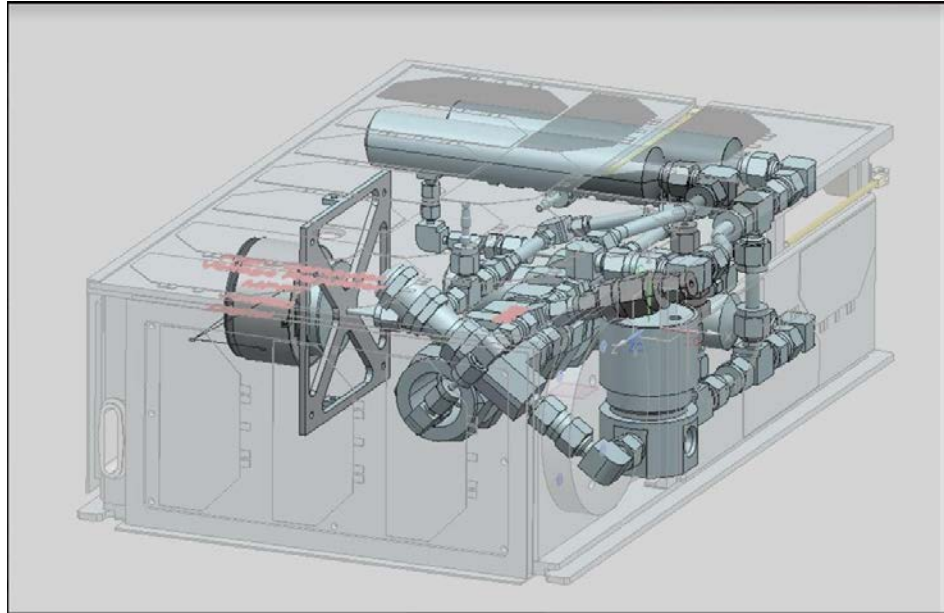


Acknowledgments

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- Alex Mundahl, Mitchell Wainwright: Missouri S&T Aerospace Plasma Lab



Questions?



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Backup Slides



Solving for Thrust

$$\dot{\Omega} = \frac{rf_h}{h \sin(i)} \sin(\theta)$$

Assuming circular orbit ($r = const$ and $\dot{\theta} = n = (\mu/a^3)^{1/2}$)

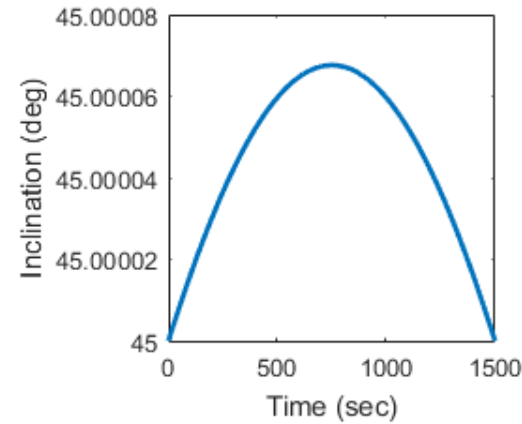
$$\int_{\Omega_i}^{\Omega_f} d\Omega = \int_0^t \frac{rf_h}{h \sin(i)} \sin(\theta) dt = \frac{rf_h}{h \sin(i)} \int_0^t \sin(\theta) dt$$

Where $i \approx const$ so $\sin(i) = const$ resulting in

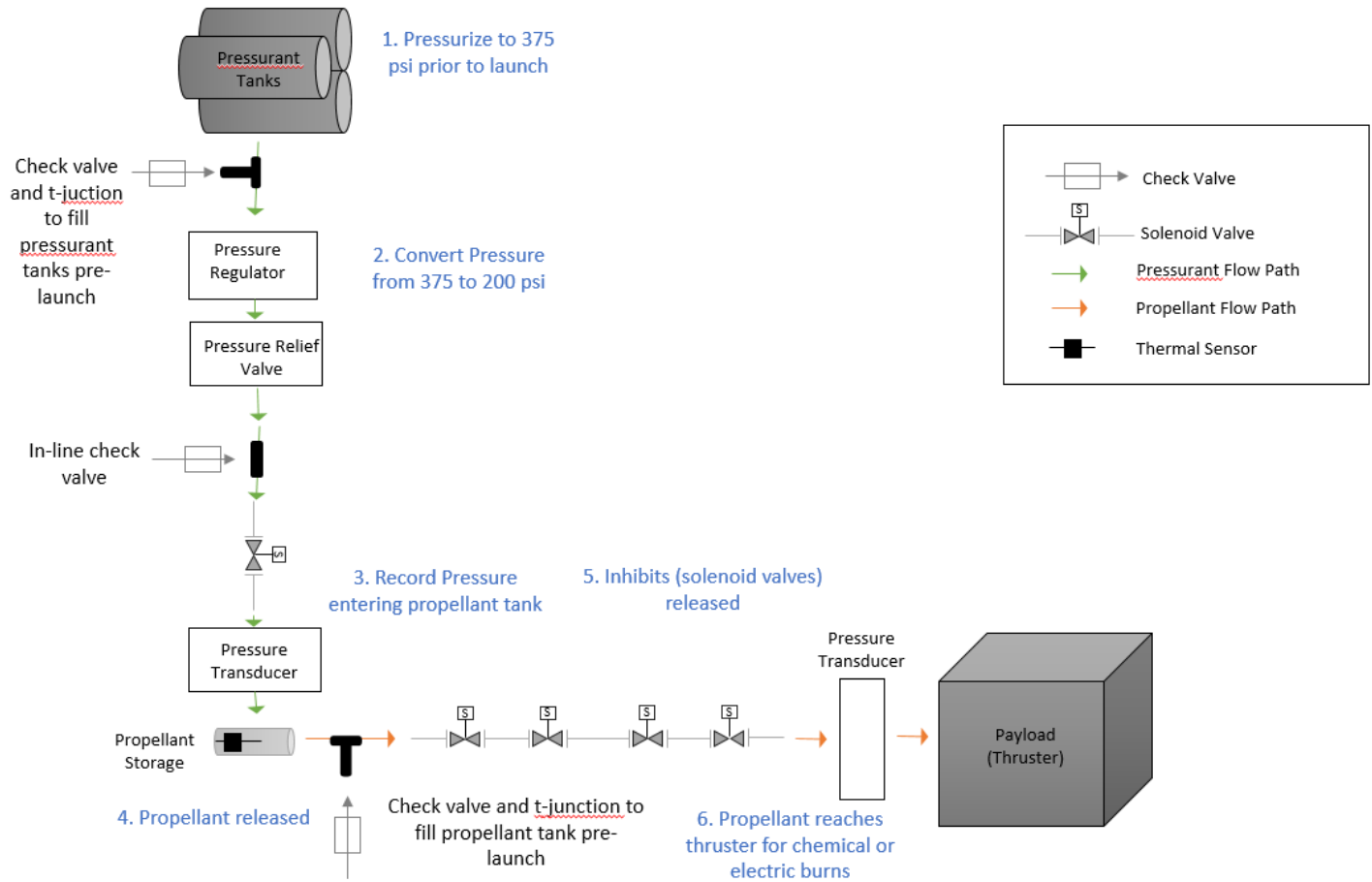
$$\Delta\Omega = \frac{rf_h}{h \sin(i) n} [\cos(\theta_i) - \cos(\theta_f)]$$

Rearranging

$$f_h = \frac{F}{m} = \frac{\Delta\Omega h \sin(i) n}{r [\cos(\theta_i) - \cos(\theta_f)]}$$

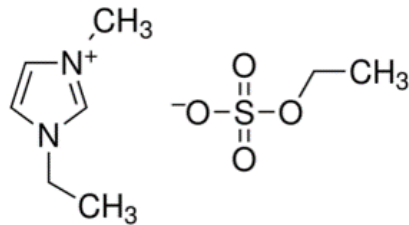


Propellant Feed System

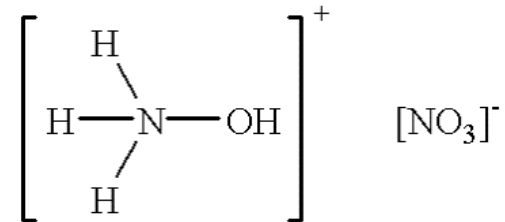


Propellant Composition

- Monopropellant Mixture: 41% Fuel 59% Oxidizer
- Fuel: 1-ethyl-3-methylimidazolium ethyl-sulfate ([Emim][EtSO₄])
- Oxidizer: Hydroxylammonium Nitrate (HAN)

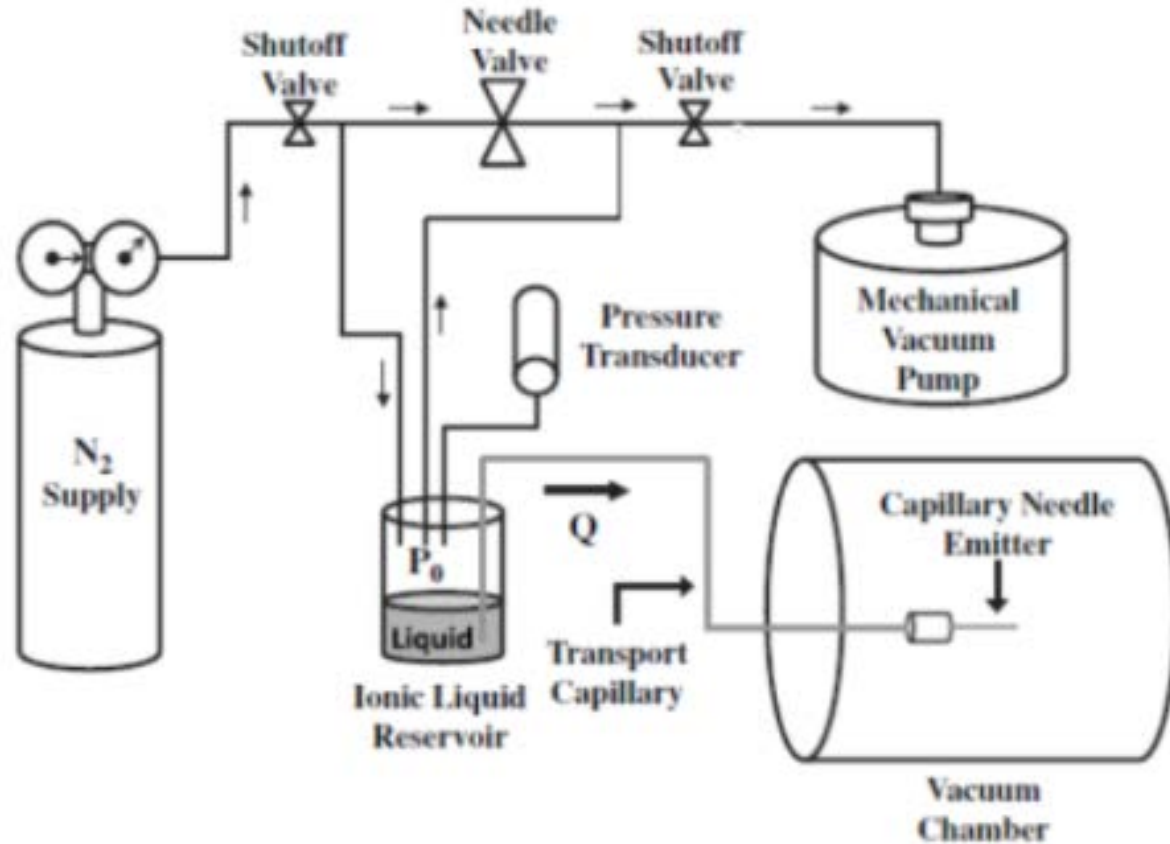


[Emim][EtSO₄]



HAN

Electrospray Mode Set Up



Plumbing and Instrumentation Diagram of the Electrospray Apparatus