

1 **Stem hydraulic capacitance decreases with drought stress: implications for modelling tree**  
2 **hydraulics in the Mediterranean oak *Quercus ilex***

3 Running title: Seasonality in stem hydraulic capacitance

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14 **Abstract**

15 Hydraulic modelling is a primary tool to predict plant performance in future drier scenarios.  
16 However, as most tree models are validated under non-stress conditions they may fail when water  
17 becomes limiting. To simulate tree hydraulic functioning under moist and dry conditions, the current  
18 version of a water flow and storage mechanistic model was further developed by implementing  
19 equations that describe variation in xylem hydraulic resistance ( $R_x$ ) and stem hydraulic capacitance  
20 ( $C_s$ ) with predawn water potential ( $\Psi_{PD}$ ). The model was applied in a Mediterranean forest  
21 experiencing intense summer drought, where six *Quercus ilex* trees were instrumented to monitor  
22 stem diameter variations and sap flow, concurrently with measurements of predawn and midday leaf  
23 water potential. Best model performance was observed when  $C_s$  was allowed to decrease with  
24 decreasing  $\Psi_{PD}$ . Hydraulic capacitance decreased from 62 to 25 kg m<sup>-3</sup> MPa<sup>-1</sup> across the growing  
25 season. In parallel, tree transpiration decreased to a greater extent than the capacitive water release  
26 and the contribution of stored water to transpiration increased from 2.0% to 5.1%. Our results  
27 demonstrate the importance of stored water and seasonality in  $C_s$  for tree hydraulic functioning, and  
28 they suggest that  $C_s$  should be considered to predict the drought-response of trees with models.

29 **Keywords:** radial stem growth, drought, hydraulic conductance, process-based modelling, holm oak,  
30 stem water storage, hydraulic function

31

## 32 **1 Introduction**

33 As soil dries and atmospheric vapor pressure deficit intensifies, xylem conduits are subjected to  
34 lower water potential and may eventually cavitate, thus limiting tree water transport. Xylem  
35 vulnerability to drought-induced cavitation has been measured in hundreds of species as the main  
36 attribute to quantify tree resistance to drought (Choat *et al.*, 2012; Sperry & Love, 2015). A growing  
37 body of evidence points, however, to a complementary factor involved in drought resistance: the  
38 radial water flow in stems to maintain tree hydraulic integrity by buffering changes in xylem water  
39 potential and limiting cavitation of xylem conduits (Goldstein *et al.*, 1998; Meinzer *et al.*, 2003;  
40 Steppe & Lemeur, 2004; Scholz *et al.*, 2007; Steppe *et al.*, 2012; McCulloh *et al.*, 2014). In this way,  
41 plant tolerance to drought does not solely rely on inherent xylem resistance to cavitation, but also on  
42 the radial capacitive release of stored water from elastic-living tissues that transiently reduces xylem  
43 tension at a given rate of flow and hence cavitation. Accordingly, a trade-off between hydraulic  
44 capacitance and structural traits involved in xylem resistance to cavitation has been observed across  
45 a wide range of woody species (Meinzer *et al.*, 2008, 2009). Nevertheless, the role of hydraulic  
46 capacitance in plant hydraulics has been traditionally overshadowed by the study of drought-induced  
47 cavitation and the vulnerability of xylem to changes in water potential (Meinzer *et al.*, 2009;  
48 McCulloh *et al.*, 2014; Epila *et al.*, 2017).

49 Hydraulic modelling is a key tool to mechanistically understand how trees cope with severe and  
50 intense drought events (Mencuccini *et al.*, 2015; Steppe *et al.*, 2015a). Mechanistic models  
51 developed for well-watered conditions commonly use static parameters to describe constant xylem  
52 hydraulic conductance (Steppe *et al.*, 2006, 2008a; Verbeeck *et al.*, 2007; Zweifel *et al.*, 2007; De  
53 Schepper & Steppe, 2010), whereas variable hydraulic conductance as a function of water potential  
54 has been successfully implemented as the soil dries out (Sperry *et al.*, 1998; Baert *et al.*, 2015;  
55 Mencuccini *et al.*, 2015). Likewise, static parameters are used to describe hydraulic capacitance (e.g.  
56 Sperry *et al.*, 1998; Steppe *et al.*, 2006; Zweifel *et al.*, 2007; Baert *et al.*, 2015); however, none of  
57 these models consider the variability in stem hydraulic capacitance, although stem water reservoirs

58 are progressively depleted under dry conditions (Scholz *et al.*, 2007, 2008; Verbeeck *et al.*, 2007;  
59 Betsch *et al.*, 2011; Kocher *et al.*, 2013; Matheny *et al.*, 2015). Accounting for the dynamic drought  
60 response of both hydraulic conductance and capacitance could improve model performance under a  
61 wide range of environmental conditions and extended time frames (Steppe *et al.*, 2008b). Model  
62 refinement via integration of tree drought responses has therefore been encouraged to advance in  
63 our mechanistic understanding of tree hydraulic functioning in future drier scenarios (Verbeeck *et al.*,  
64 2007; Baert *et al.*, 2015; Mencuccini *et al.*, 2015; Steppe *et al.*, 2015a, 2015b).

65 In this study, we aimed at modelling tree hydraulic functioning in field-grown *Quercus ilex* L. under  
66 wet to dry conditions by taking into account the dynamic nature of both xylem resistance to water  
67 transport ( $R_x$ ) and stem hydraulic capacitance ( $C_s$ ). For this purpose, process-level equations that  
68 describe the relationship of  $R_x$  and  $C_s$  with predawn water potential ( $\Psi_{PD}$ ) have been implemented in  
69 the current version of a sophisticated mechanistic model that integrates tree water transport  
70 dynamics and stem diameter variations (Steppe *et al.*, 2006, 2008a; De Swaef *et al.*, 2015). Water  
71 reservoirs are defined here as the elastic tissues subjected to reversible diel cycles of water release  
72 and refill to avoid xylem cavitation. Inelastic water release from cavitated xylem conduits under  
73 negative water potential (Tyree & Ewers, 1991; Hölttä *et al.*, 2009) is neglected because the rapid  
74 reversibility of this phenomenon remains a matter of debate (Brodersen & McElrone, 2013; Cochard  
75 & Delzon, 2013). An advantage of this approach is that measurements are not destructive, since the  
76 model is driven by sap flow and  $\Psi_{PD}$ , and calibrated against stem diameter variations and xylem  
77 water potential at midday. As these variables can be monitored with peripheral devices and by  
78 sampling a small number of leaves, the hydraulic functioning of surveyed trees can be continuously  
79 modelled and research is not restricted to discrete observations.

80 We hypothesize that including daily variations in  $R_x$  and  $C_s$  as a function of  $\Psi_{PD}$  improves model  
81 accuracy in predicting stem diameter variations and xylem water potential during the dry season.  
82 Contrarily, we predict that variability in  $R_x$  and  $C_s$  may not improve model performance during the  
83 wet season as  $R_x$  and  $C_s$  are expected to remain constant. The integrated root-to-leaf  $R_x$  was

84 modelled as function of  $\Psi_{pD}$  using a negative exponential curve (Baert *et al.*, 2015), an alternative  
85 approach to estimate the integrated root-to-leaf hydraulic conductance ( $K_x = 1/ R_x$ ) and generate  
86 vulnerability curves. Furthermore, a new equation defining the relationship between  $C_s$  and  $\Psi_{pD}$  was  
87 developed using the shape of water desorption curves and cumulative water release curves reported  
88 for several species (Zweifel *et al.*, 2000; Meinzer *et al.*, 2003, 2009; Steppe *et al.*, 2006; Barnard *et al.*,  
89 2011; McCulloh *et al.*, 2014). Both magnitude of the decrease in  $C_s$  during the dry season and  
90 contribution of stored water to the transpiration stream were evaluated. Simulated cumulative water  
91 release from internal storage pools was compared with estimates of stem water refilling at the end  
92 of the dry season after first autumn heavy rains. Likewise, the simulated vulnerability curve was  
93 compared to the vulnerability curves obtained by measurements at the organ scale in the same  
94 experimental site (Limousin *et al.*, 2010a; Martin-StPaul *et al.*, 2014).

## 95 **2 Materials and methods**

### 96 **2.1 Site description**

97 The study site is located in the Puéchabon State Forest (Montpellier, France) in a stand dominated by  
98 *Q. ilex* (43°44'29" N, 3°35'45" E, 270 m.a.s.l.). The stand has been historically subjected to periodic  
99 coppicing, with the last cut being performed in 1942. Nowadays, top canopy height is 5.5 m, stand  
100 density is 4700 stems ha<sup>-1</sup>, and most stems (> 70%) range in diameter at breast height (DBH) from 4  
101 to 10 cm. *Buxus sempervirens* L., *Phyllirea latifolia* L., *Pistacia terebinthus* L. and *Juniperus oxycedrus*  
102 L. are the main species of the understory layer. The area has a Mediterranean-type climate: annual  
103 mean temperature is 13.4 °C, annual precipitation is 907 mm, and 80% of this amount falls during  
104 winter and autumn, when temperatures are lower (Limousin *et al.*, 2009). A weather station located  
105 at the experimental site was used to monitor meteorological conditions. Air temperature, relative  
106 humidity (MP100, Rotronic, Bassersdorf, Switzerland), and rainfall (tipping bucket rain gauge  
107 ARG100, Environmental Measurements Ltd, Sunderland, UK) were measured every minute and

108 averaged every 30 minutes with a data logger (model 21X, Campbell Scientific Ltd, Shepshed, UK).  
109 More details on the experimental site are available in Rambal *et al.* (2014).

## 110 **2.2 Tree and soil measurements**

111 Six *Q. ilex* trees (see Table 1) were instrumented to continuously monitor sap flow and stem diameter  
112 variations. We selected data from the year 2009 because it was characterized by a strong and typical  
113 summer drought between mid-July and mid-September, and due to data availability on leaf water  
114 potential at predawn and midday in the instrumented trees during the summer.

115 Sap flux density ( $\text{g cm}^{-2} \text{h}^{-1}$ ) was continuously monitored with thermal dissipation probes (Granier,  
116 1985). Probe pairs were inserted at 1.2 m height with a vertical separation of 10 cm. Probes were  
117 oriented facing north to avoid direct solar heating, and were protected from rain and radiation by  
118 aluminum cover. Temperature difference between the probes was registered every 5 minutes, and  
119 averaged and recorded every 30 minutes with a data logger (model CR10X, Campbell Scientific). Sap  
120 flux density was calculated considering zero flow from the absolute maximum temperature  
121 difference over 2-day running periods. Sap flux density was upscaled to the tree level to obtain sap  
122 flow ( $F_{\text{STEM}}$ ,  $\text{g h}^{-1}$ ) by multiplying sap flux density by sapwood area. Sapwood area was estimated from  
123 an allometric relationship between tree DBH and sapwood area obtained from 18 additional trees  
124 (Limousin *et al.*, 2009). For further details about  $F_{\text{STEM}}$  measurements see Limousin *et al.* (2009).

125 Stem circumference variations were recorded using automatic band dendrometers (ELPA-98,  
126 University of Oulu, Oulu, Finland). Dendrometers were just below the thermal dissipation probes,  
127 and the outer layer of dead bark was removed prior to installation. Circumference variations were  
128 registered every 5 minutes and recorded every 30 minutes with a data logger (model CR1000;  
129 Campbell Scientific Ltd, Shepshed, UK) and transformed to stem diameter variations ( $\Delta D$ ,  $\mu\text{m}$ ). For  
130 further details about  $\Delta D$  measurements see Lempereur *et al.* (2015).

131 Leaf water potential ( $\Psi_{\text{LEAF}}$ , MPa) was measured with a pressure chamber (PMS1000, PMS  
132 Instruments, Corvallis, OR, USA) on DOYs 114, 176, 208, 234 and 310 during the 2009 growing season

133 (23 April, 24 June, 26 July, 21 August, 5 November, respectively) at predawn (before 06:00 h) and  
134 midday (14:00 h). Two leaves were sampled per tree and a third leaf was sampled if the observed  
135 difference between measurements was higher than 0.2 MPa. Samples were taken at similar tree  
136 heights and measurements were performed within 1 min after leaf excision. Leaf water potential was  
137 measured in four of the six trees instrumented for  $F_{STEM}$  and  $\Delta D$  measurements. Average  $\Psi_{LEAF}$  of  
138 these four trees was used for the two remaining trees.

139 The discrete measurements of  $\Psi_{PD}$  were interpolated on a daily basis using modelled soil water  
140 storage (SWS, mm). Daily soil water storage was modelled using the soil water balance module of the  
141 SIERRA vegetation model driven by daily values of solar radiation, minimum and maximum  
142 temperature and precipitation (Mouillot *et al.*, 2001; Ruffault *et al.*, 2013). Soil water storage and  $\Psi_{PD}$   
143 were related by a Campbell-type retention curve (Campbell, 1974). The soil water storage model was  
144 validated against measurements of SWS integrated over a rooting depth of 4.5 m and performed at  
145 approximately monthly intervals from 1998 to 2009 using a neutron moisture gauge (see Rambal *et*  
146 *al.* 2003 for further details). The relationship between modelled and measured SWS displayed a good  
147 agreement ( $R^2 = 0.92$ ;  $p < 0.0001$ ; RMSE = 16 mm;  $n = 90$ ), as well as the relationship between  
148 modelled and measured  $\Psi_{PD}$  ( $R^2 = 0.73$ ;  $p < 0.0001$ ; RMSE = 0.71 MPa;  $n = 95$ ). Despite the good fit  
149 obtained between SWS and  $\Psi_{PD}$  on an annual basis,  $\Psi_{PD}$  was underestimated by the soil water  
150 balance model during summer drought. To correct daily simulated values of  $\Psi_{PD}$  in summer,  
151 optimized parameters for each tree were selected to account for spatial heterogeneity in leaf area  
152 index, soil texture and stone fraction.

## 153 **2.3 Mechanistic tree modelling**

### 154 **2.3.1 Model description**

155 The current version of a mechanistic water flow and storage model (Steppe *et al.*, 2008a) was used to  
156 study the hydraulic functioning of *Q. ilex* trees. Briefly, the model is composed of two interconnected  
157 sub-models describing dynamics in tree water transport and stem diameter variations, in which  $F_{STEM}$

158 dynamics are intimately linked to stem  $\Delta D$  by radial water flow between the xylem and the outer  
159 tissues. Note that “stem” refers to the tree trunk, so that branches are excluded for model simplicity.  
160 The model assumes the xylem as a rigid cylinder (xylem compartment) surrounded by an elastic outer  
161 ring composed of cells of cambium, phloem and bark (storage compartment) responsible for diel  
162 shrinkage and swelling (Steppe *et al.*, 2006). Therefore, the water stored in outer elastic cells  
163 constitutes the only capacitive water source; water release from the xylem parenchyma and cavitared  
164 conduits is neglected by this model. Sap flow ( $F_{STEM}$ ) integrates the axial water flow through the xylem  
165 compartment via root water uptake ( $f_x$ ) and the radial water exchange between xylem and storage  
166 compartment ( $f_s$ ). Axial water flow ( $f_x$ ) is calculated as the water potential gradient between the roots  
167 and the stem divided by  $R_x$ , and radial water flow ( $f_s$ ) is calculated as the first derivative defining the  
168 change in water content of the storage compartment, which is influenced by the resistance to radial  
169 flow between xylem and storage compartment ( $R_s$ ,  $MPa\ h\ g^{-1}$ ). The model equations are shown in the  
170 supplementary material (Note S1). When transpiration starts, a water potential gradient between  
171 xylem and storage compartment ( $\Psi_x - \Psi_s$ ) leads to radial flow from outer cells to the xylem to fulfill  
172 the transpiration need;  $\Psi_x$  is inferred from  $\Psi_{LEAF}$  measurements (see below), whereas  $\Psi_s$  is estimated  
173 as a function of the water content and capacitance of the storage compartment (see Note S1). Water  
174 depletion in the morning results in reduction in cell turgor and reversible stem shrinkage. Conversely,  
175 water refilling in the afternoon, when atmospheric vapor pressure deficit and transpiration start to  
176 decline, results in reversible stem swelling. Water potential in the storage compartment is the  
177 algebraic sum of the osmotic potential ( $\Psi_s^O$ ) and the turgor pressure ( $\Psi_s^P$ ). Irreversible stem growth  
178 occurs when carbon requirements are met (Daudet *et al.*, 2005) and turgor pressure exceeds a  
179 threshold value for cell wall yielding ( $\Gamma$ , Lockhart 1965). For a detailed explanation of the principles of  
180 the model see Steppe *et al.* (2006, 2008a) and De Pauw *et al.* (2008).

181 To allow variation in xylem hydraulic resistance of the root-to-leaf continuum ( $R_x$ ,  $MPa\ h\ g^{-1}$ ) and  
182 stem hydraulic capacitance ( $C_s$ ,  $g\ MPa^{-1}$ ), the model was further developed by implementing two  
183 equations and their corresponding parameters:



184 The hydraulic resistance was described to vary exponentially with  $\Psi_{PD}$  (Baert *et al.*, 2015), which  
185 accounted for day to day variations in  $R_x$  with soil drying while assuming no daily refilling of cavitating  
186 xylem:

$$187 \quad R_x = r_1 e^{(\Psi_{PD}^2) r_2} \quad \text{Eqn. 1}$$

188 where  $r_1$  (MPa h g<sup>-1</sup>) and  $r_2$  (MPa<sup>-2</sup>) are the proportionality parameters influenced by plant  
189 characteristics.

190 The hydraulic capacitance of the stem was calculated as the derivative of the water release curve  
191 (Steppe *et al.*, 2006):

$$192 \quad C_s = \frac{dW}{d\Psi} \quad \text{Eqn. 2}$$

193 where  $dW$  is the variation in water content in the storage compartment (g h<sup>-1</sup>) and  $d\Psi$  the  
194 corresponding variation in  $\Psi$  (MPa h<sup>-1</sup>). In this study, the cumulative water ( $W$ ) release curve was  
195 defined by a logarithmic equation of similar shape to those previously reported (e.g. Meinzer *et al.*,  
196 2003, 2009; McCulloh *et al.*, 2014):

$$197 \quad W = -\log_{w_1}(w_2\Psi + 1) \quad \text{Eqn. 3}$$

198 where  $w_1$  and  $w_2$  are the parameters defining the shape of the water release curve. The derived form  
199 of Eqn. 3 results in an inverse equation between  $C_s$  and  $\Psi_{PD}$ :

$$200 \quad C_s = \frac{1}{(c_1 \Psi_{PD} + c_2)} \quad \text{Eqn. 4}$$

201 where  $c_1$  (g<sup>-1</sup>) and  $c_2$  (MPa g<sup>-1</sup>) are the proportionality parameters dependent on plant properties,  
202 which are related to the parameters defining the water release curve (Eqn. 3) as follows:  $w_1 = e^{c_1}$ ,

203 and  $w_2 = \frac{\ln(w_1)}{c_2}$ . Note that the purpose of this study is to evaluate seasonality in  $R_x$  and  $C_s$ .

204 Therefore,  $R_x$  and  $C_s$  in this model fluctuates on a daily basis with  $\Psi_{PD}$ , so that both are assumed  
205 constant within 24 h periods as diel variability in  $R_x$  and  $C_s$  is expected to be comparatively negligible  
206 (see Baert *et al.*, 2015).

207 Four models were calibrated for each tree: [1]  $R_x$  and  $C_s$  were assumed to be constant (the simplest  
208 framework, used for model calibration of  $R_x$  and  $C_s$ ), [2]  $R_x$  was allowed to vary and  $C_s$  was assumed  
209 to be constant (model calibration of  $r_1$ ,  $r_2$  and  $C_s$ ), [3]  $C_s$  was allowed to vary and  $R_x$  was assumed to  
210 be constant (model calibration of  $R_x$ ,  $c_1$  and  $c_2$ ), and [4] both  $R_x$  and  $C_s$  were allowed to vary (model  
211 calibration of  $r_1$ ,  $r_2$ ,  $c_1$  and  $c_2$ ). The resistance to radial flow between xylem and storage compartment  
212 ( $R_s$ ) was also calibrated in each model.

### 213 **2.3.2 Model simulation, calibration, and identifiability analyses**

214 Model simulations, calibrations and identifiability analyses were performed using the plant modelling  
215 software PhytoSim (version 2.1, Phyto-IT, Mariakerke, Belgium). Simulations were conducted with a  
216 fourth order variable step size solver of an accuracy of  $10^{-6}$  and a maximum step size of 1 h.  
217 Calibrations were done using the simplex method to minimize the weighted sum of squared errors  
218 (SSE) for  $\Delta D$  and  $\Psi_x$ . Identifiability analyses were performed to check whether the subset of model  
219 parameters to calibrate was not correlated and sensitive enough, and thus was identifiable (De Pauw  
220 *et al.*, 2008). A collinearity index (CI) above 15 indicated an unidentifiable subset of parameters.  
221 Values of non-calibrated model parameters were directly measured or assigned from literature  
222 (Table S1 in supplementary material).

223 Predawn water potential and  $F_{STEM}$  were used as model inputs, and  $\Delta D$  and  $\Psi_x$  were used for  
224 calibration purposes. The best model was selected using the final predicted error (FPE) criteria  
225 (Steppe *et al.*, 2006):

$$226 \quad FPE = \frac{SSE}{N} + \frac{2pSSE}{(N-p)N} \quad \text{Eqn. 5}$$

227 where SSE is the weighted sum of squared errors for  $\Delta D$  and  $\Psi_x$ ,  $N$  is the number of observations,  
228 and  $p$  the number of calibrated parameters. The first term of the FPE evaluates the goodness of fit  
229 between measured and simulated data, whereas the second term penalizes over-parameterized  
230 models. Thus, the smaller the FPE value, the better the model.

231 Because rain events and tree trembling resulted in irregular signals recorded by the automatic band  
232 dendrometers, data was manually inspected to select a set of days that displayed reliable diel  
233 patterns, i.e., smooth morning shrinkage and afternoon swelling. As the number of  $\Delta D$  observations  
234 after manual inspection differed among trees, FPE values also differed. To remove any effect  
235 associated to the number of observations, values of FPE were normalized relative to the simplest  
236 framework (constant  $R_x$  and  $C_s$ ) for each tree.

237 Models were calibrated under wet and dry conditions. As stem growth during the summer season is  
238 limited by soil water availability in the surveyed site (Lempereur *et al.*, 2015), wet and dry periods  
239 were defined according to growing or non-growing conditions, respectively. Periods that cover two  
240 consecutive midday  $\Psi_{LEAF}$  measurements were initially considered for model calibration: DOYs 113-  
241 177 were selected for the wet period (spring and early summer) and DOYs 207-235 for the dry period  
242 (late summer). Inaccurate simulations were initially obtained during the wet period and further  
243 attempts to improve simulations were tested. First, the stem growth curve was adjusted to a  
244 Gompertz-shaped curve (Winsor, 1932) to smooth large fluctuations registered by the band  
245 dendrometers (Fig. 1D); and second, a shorter time period around a single  $\Psi_{LEAF}$  measurement  
246 campaign (DOY 176, early summer) was additionally examined.

247 To calibrate the models, midday  $\Psi_x$  was inferred from midday  $\Psi_{LEAF}$  measurements. Under dry  
248 conditions, measurements of midday  $\Psi_{LEAF}$  could be used as a surrogate of midday  $\Psi_x$ , because of the  
249 strong stomatal limitation observed in the monitored trees (see Fig. 3 in Limousin *et al.*, 2010b)  
250 which minimized the disequilibrium in water potential between xylem and leaves (Meinzer *et al.*,  
251 2009). In contrast, substantial disequilibrium between midday  $\Psi_{LEAF}$  and midday  $\Psi_x$  might occur  
252 when water is not limiting, as has been observed in *Q. ilex* seedlings (Rodríguez-Calcerrada *et al.*,  
253 2017) and in Neotropical savanna trees (see Fig. 2 in Scholz *et al.*, 2007). Under wet conditions, the  
254 difference between midday and predawn  $\Psi_x$  ( $\Delta\Psi_x = \text{midday } \Psi_x - \text{predawn } \Psi_x$ ) was assumed as a  
255 constant fraction of  $\Delta\Psi_{LEAF}$  ( $\Delta\Psi_{LEAF} = \text{midday } \Psi_{LEAF} - \text{predawn } \Psi_{LEAF}$ ). The ratio  $\Delta\Psi_x / \Delta\Psi_{LEAF}$  was  
256 obtained from measurements performed in *Q. ilex* seedlings ( $\Delta\Psi_x / \Delta\Psi_{LEAF} = 0.342$ ; Fig. S1 in

257 supplementary material), in which leaves were covered with aluminium foil for one hour to measure  
258  $\Psi_x$ . Midday  $\Psi_x$  was therefore estimated as a function of  $\Psi_{PD}$  and  $\Delta\Psi_{LEAF}$  (midday  $\Psi_x = \Psi_{PD} + 0.342 * \Delta\Psi_{LEAF}$ ). By using this approximation of  $\Psi_x$ , we made the assumptions that leaf hydraulic resistance  
260 was a constant fraction of the tree hydraulic resistance independently of tree size (Sack *et al.*, 2003),  
261 that the water potential difference between leaves and stem depended mainly on leaf transpiration,  
262 and that the  $\Psi_x$  difference between the trunk and the branches was negligible.

#### 263 **2.4 Stem water refilling measurements**

264 Stem water refilling was estimated by integrating sap flow over intense rain events at the end of  
265 summer drought. We only considered short (< 4 hours) and heavy (> 20 mm) rainfall events occurring  
266 at night or in the late evening to ensure that recorded sap flow could be attributed to stem water  
267 refilling and not to leaf transpiration (Betsch *et al.*, 2011), and to avoid rainfall events that resulted in  
268 slow refilling extending beyond night-time. Sap flow was integrated along the rain event and  
269 following night-time hours to estimate the volume of water refilled. Stem water refilling was then  
270 divided by the corresponding shift in  $\Psi_{PD}$  measured before and after the rain event to estimate  $C_s$   
271 (Eqn. 2) and compare it with values obtained from model simulations. Available measurements of  
272  $\Psi_{PD}$  obtained less than one week before and after the rainfall event were necessary to calculate  $C_s$ .  
273 As the first heavy rain in 2009 did not meet these requirements, different years were inspected and  
274 suitable rain events were found in 2006 and 2007 to estimate  $C_s$ . TREE4 was excluded from this  
275 analysis, as it was not monitored in 2006 and 2007. However, eighteen *Q. ilex* trees located in the  
276 study site and equipped with thermal dissipation probes were additionally included.

#### 277 **2.5 Data analyses**

278 To compare model performance (i.e. normalized FPE) among the four tested models and the two  
279 surveyed periods, Tukey's multiple comparison tests were performed using the *TukeyHSD* function in  
280 the R software (version 3.2.3). The best model was then selected to obtain  $R_x$  and  $C_s$  along the  
281 gradient of  $\Psi_{PD}$  on a per-tree basis. To test whether  $F_{STEM}$  and radial water flow ( $f_s$ ) varied with  $\Psi_{PD}$ ,

282 mixed models were adjusted using the *lme* function in the nlme library, in which stem was  
283 considered as a random factor ( $n = 6$ ). As the model output for  $C_s$  refers to the whole tree,  $C_s$  was  
284 standardized per unit of storage volume. The storage volume was estimated as the product of stem  
285 height by stem basal area subtracting the xylem compartment. The integrated root-to-leaf hydraulic  
286 conductance was calculated as the inverse of the integrated root-to-leaf hydraulic resistance ( $K_x =$   
287  $1/R_x$ ,  $g\ MPa^{-1}\ h^{-1}$ ). Predawn water potential causing 50% loss of  $K_x$  ( $\Psi_{50}$ ) was obtained following Baert  
288 *et al.* (2015). To obtain the mean curve and confidence intervals of  $C_s$ , cumulative water release, and  
289 integrated root-to-leaf  $R_x$  and  $K_x$  along the gradient of  $\Psi_{PD}$ , uncertainty analyses were performed in  
290 PhytoSim using the averaged parameters among the six studied trees yielded by the best model. All  
291 values presented in the text are means  $\pm$  SE.

### 292 **3 Results**

293 Averaged among the six surveyed stems and across the whole year, daily sap flow was  $4.11 \pm 0.81$  kg  
294  $day^{-1}$  (Fig. 1C, Table 1), and mean annual diameter increment was  $0.53 \pm 0.20$  mm  $year^{-1}$  (Fig. 1D,  
295 Table 1). During spring and early summer (DOYs 113-177), average temperature was  $18.2\ ^\circ C$  and  
296 accumulated rainfall 107.2 mm. Late summer was hot and dry, with an average temperature of  $25.2$   
297  $^\circ C$  and an accumulated rainfall of 11.8 mm during the dry modelled period (DOYs 207-235). The  
298 lowest  $\Psi_{LEAF}$  was measured at the end of this period, when it reached mean values of  $-3.3$  MPa at  
299 predawn and  $-3.9$  MPa at midday (Fig. 1B).

300 Four models with constant or variable  $R_x$  and  $C_s$  were adjusted per tree and period to simulate  $\Delta D$   
301 and  $\Psi_x$  over time. A consistent pattern was observed under wet (Fig. 2A) and dry (Fig. 2B) conditions.  
302 Relative to the simplest model (constant  $R_x$  and  $C_s$ ), the normalized FPE was not reduced when  $R_x$   
303 alone was allowed to vary ( $P > 0.1$ ). In contrast, the normalized FPE was reduced ( $P < 0.001$ ) when  $C_s$   
304 was allowed to vary with  $\Psi_{PD}$ . The model with variable  $R_x$  and  $C_s$  showed the lowest normalized FPE,  
305 although its value did not differ significantly from that obtained with constant  $R_x$  and variable  $C_s$  ( $P >$   
306  $0.1$ ). Therefore, calibration of the model with a variable  $C_s$  was the main improvement required to

307 accurately simulate  $\Delta D$  and  $\Psi_x$ . Only data yielded by the best model (variable  $R_x$  and  $C_s$ ) is shown  
308 hereafter.

309 Models were calibrated under wet and dry conditions. Only TREE5 was not modelled during the wet  
310 season due to the inconsistent dendrometer signal at the time of  $\Psi_{LEAF}$  measurement. Because of  
311 concurrent stem growth, inaccurate simulations of  $\Delta D$  were initially obtained during the wet period  
312 when considering long temporal spans (DOYs 113-177; data not shown). Shorter temporal spans of 3-  
313 4 days resulted in realistic simulations of  $\Psi_x$  and  $\Delta D$  (Fig. 3A-C, FPE =  $6.04 \pm 1.90$ ). The length of the  
314 simulation period was not an issue under dry conditions when stem growth was impeded, and  
315 accurate simulations were obtained for every tree throughout the one-month simulated period (Fig.  
316 3D-F, FPE =  $7.71 \pm 2.11$ ). During the wet season, cell turgor pressure at night-time was higher than  
317 the turgor threshold for cell wall yielding ( $\Psi_s^P > \Gamma$ , Fig. 3A) leading to irreversible stem growth (Fig.  
318 3B). During the dry season, soil drying progressively reduced  $\Psi_x$ ,  $\Psi_s$  and cell osmotic potential, which  
319 explained the rather constant pattern of cell turgor pressure, which was below the turgor threshold  
320 for cell wall yielding ( $\Psi_s^P < \Gamma$ , Fig. 3D), thus impeding irreversible stem growth (Fig. 3E). Morning stem  
321 shrinkage and afternoon stem swelling (Fig. 3B, 3E) were caused by the radial water flow between  
322 xylem and storage compartments ( $f_s$ , Fig. 3C, 3F).

323 Daily  $F_{STEM}$  was directly related to  $\Psi_{PD}$  in every surveyed stem ( $P < 0.01$ , Fig. 4A). Averaged among the  
324 six stems,  $F_{STEM}$  decreased from  $7.50 \pm 0.83 \text{ kg day}^{-1}$  during the wet period ( $\Psi_{PD} = -1.0 \text{ MPa}$ ) to  $1.46 \pm$   
325  $0.81 \text{ kg day}^{-1}$  at the end of the dry period ( $\Psi_{PD} = -3.3 \text{ MPa}$ ,  $P < 0.001$ ). The decrease in daily stem  
326 water release from the storage to the xylem compartment (daily sum of negative  $f_s$ , hereafter daily  
327  $|f_s|$ , in  $\text{kg day}^{-1}$ ) with  $\Psi_{PD}$  was significant in only half of the surveyed trees ( $P < 0.05$ , Fig. 4B) and  
328 became non-significant when pooling trees across a range of  $\Psi_{PD}$  from -1.0 to -3.3 MPa ( $P = 0.15$ ).  
329 Considering the dry period only, daily  $|f_s|$  significantly decreased with  $\Psi_{PD}$  ( $P < 0.001$ ) from  $0.13 \pm$   
330  $0.03$  to  $0.10 \pm 0.03 \text{ kg day}^{-1}$  for a corresponding reduction in  $\Psi_{PD}$  of 1.3 MPa (from -2.0 to -3.3 MPa).  
331 Across the year, daily sap flow was reduced to a greater extent than daily  $|f_s|$  as the soil dried out.

332 Hence, the daily contribution of  $|f_s|$  to  $F_{STEM}$  increased with drought severity ( $P < 0.001$ ) from  $2.0 \pm$   
333  $0.9 \%$  to  $5.1 \pm 0.9 \%$  when  $\Psi_{PD}$  decreased from  $-1.0$  to  $-3.3$  MPa (Fig. 4C).

334 Stem hydraulic capacitance decreased with drought stress. Mean  $C_S$  on a storage volume basis was  
335  $61.69 \pm 6.30$  kg MPa<sup>-1</sup> m<sup>-3</sup> under wet conditions (Table 2) and reached lowest values of  $24.93 \pm 4.14$   
336 kg MPa<sup>-1</sup> m<sup>-3</sup> at the end of the summer drought (Table 3). Fig. 5A illustrates the mean cumulative  
337 release of water from storage compartments and the change in  $C_S$  at the tree level obtained in the  
338 dry period and extrapolated to a wider range of  $\Psi_{PD}$ . Hydraulic capacitance obtained from model  
339 calibration during the wet period ( $C_S = 314.51 \pm 38.83$  g MPa<sup>-1</sup> tree<sup>-1</sup>) was underestimated by the  $C_S$   
340 curve extrapolated from the dry period. Similarly, Fig. 5B displays mean  $R_x$  and  $K_x$  curves obtained in  
341 the dry period. The vulnerability curve of root-to-leaf hydraulic conductance obtained from the dry  
342 period showed a mean  $\Psi_{50}$  value of  $-2.67 \pm 0.23$  MPa (Table 3). The  $R_x$  value obtained from direct  
343 model calibration under wet conditions ( $5.01 \pm 0.45 \times 10^{-4}$  MPa h g<sup>-1</sup>, Table 2) was overestimated by  
344 the  $R_x$  curve extrapolated from summer drought.

345 Two rain events were used to independently estimate  $C_S$  from stem water refilling. In 2006, 24 mm of  
346 rainfall were registered during the night of DOY 228 to 229, whereas in 2007, a stronger rainfall of  
347 75.5 mm occurred in the night of DOY 261 to 262. The corresponding mean increase in  $\Psi_{PD}$  was 2.6  
348 and 2.9 MPa for 2006 and 2007, respectively. Stem water refilling and  $C_S$  on a tree basis were  
349 exponentially related to stem size across the 23 trees examined ( $P < 0.001$ ; Fig. 6). Average stem  
350 water refilling and  $C_S$  among the five trees monitored in both approaches were  $1134 \pm 149$  g tree<sup>-1</sup>  
351 and  $414 \pm 45$  g MPa<sup>-1</sup> tree<sup>-1</sup>, respectively.

## 352 **4 Discussion**

### 353 **4.1 The importance of a variable hydraulic capacitance in tree modelling**

354 Hydraulic capacitance is commonly measured as the slope of the initial and nearly linear portion of  
355 the curve between the cumulative water release and water potential (Meinzer *et al.*, 2003, 2008;  
356 Barnard *et al.*, 2011; McCulloh *et al.*, 2014). These estimates of  $C_S$  are therefore obtained within the

357 range of  $\Psi_x$  when plants are not subjected to drought stress. Notwithstanding,  $C_s$  varies seasonally as  
358 water storage refilling is limited by soil drying (Verbeeck *et al.*, 2007; Scholz *et al.*, 2008; Steppe *et al.*,  
359 2008b; Kocher *et al.*, 2013; Matheny *et al.*, 2015). Progressive decoupling between daily capacitive  
360 water discharge and daily water refilling leads to water reserves depletion, and accordingly, a net  
361 reduction in stem diameter is commonly observed during the dry season (Fig. 3E; Zweifel *et al.*, 2000;  
362 Lempereur *et al.*, 2015). Progressive depletion of water reservoirs should be incorporated in process-  
363 based hydraulic models by the implementation of a direct relationship between  $C_s$  and soil water  
364 availability. However, to the best of our knowledge, no mechanistic model has yet considered  
365 drought-induced variability in  $C_s$  to model tree hydraulic functioning. Furthermore, and unexpectedly,  
366 considering the variation of  $C_s$  with  $\Psi_{PD}$  was also found to result in more accurate simulations of  $\Psi_x$   
367 and  $\Delta D$  during the wet period. In contrast to previous studies using this model in which  $C_s$  was  
368 assumed constant under well-watered regimes and stable soil water content (e.g. Steppe *et al.*, 2006,  
369 2008a; De Schepper & Steppe, 2010), considering a variable  $C_s$  was here necessary to simulate the  
370 increase in turgor that yielded irreversible cell wall extension. Assuming a constant  $C_s$  in our study  
371 resulted in a progressive reduction of maximum daily turgor pressure that impeded stem growth  
372 (simulations not shown) as  $\Psi_{PD}$  slightly declined during this “wet” period (Fig. 3A). Consequently,  
373 under both wet and dry conditions, assumptions of constant  $C_s$  may partially explain why tree models  
374 fail to reproduce variations in diameter and  $\Psi_x$  in environments where soil water availability  
375 fluctuates. We suggest that to better predict and understand tree hydraulic functioning and the risk  
376 of hydraulic failure in dry regions, it is necessary to take into account the dynamic nature of  $C_s$ .

377 Because  $C_s$  is commonly measured under moist conditions, estimates of  $C_s$  on a storage volume basis  
378 in early summer ( $62 \text{ kg m}^{-3} \text{ MPa}^{-1}$ , Table 2) might be more appropriate for literature comparison.  
379 Hydraulic capacitance of *Q. ilex* at this time of year was consistent with the reported range for  
380 evergreen sclerophyll species ( $6\text{-}102 \text{ kg m}^{-3} \text{ MPa}^{-1}$ , Richards *et al.* 2014) and lower than the ones for  
381 tropical species ( $70\text{-}420 \text{ kg m}^{-3} \text{ MPa}^{-1}$ , Meinzer *et al.* 2003, 2009) and conifers ( $107\text{-}886 \text{ kg m}^{-3} \text{ MPa}^{-1}$ ,  
382 Barnard *et al.* 2011, McCulloh *et al.* 2014). Nevertheless, neglecting the xylem tissues as capacitive



383 water sources might lead to underestimation of the overall hydraulic capacitance of *Q. ilex* stems in  
384 our study (see below). Hydraulic capacitance decreased across the season from 62 to 25 kg m<sup>-3</sup> MPa<sup>-1</sup>  
385 (from DOY 176 to 235, respectively). The 60% reduction in C<sub>s</sub> illustrates the importance of  
386 implementing variable C<sub>s</sub> in mechanistic models to accurately simulate tree water status and  
387 diameter variations. Our modelling approach further allowed estimation of the daily contribution of  
388 internal water storage to total daily sap flow ( $|f_s| / F_{STEM}$ ) as a function of  $\Psi_{PD}$ . The average  $|f_s| /$   
389  $F_{STEM}$  ratio ranged between 2% in early summer and 5% at the end of summer drought when  $\Psi_{PD}$   
390 reached mean values of - 3.3 MPa (Fig. 4C). This ratio is at the lower end of observations made in  
391 other species that may reach up to 19% when only elastic tissues are considered (see Table 3 in  
392 Betsch *et al.*, 2011). The low reliance on stored water to maintain transpiration rates in *Q. ilex* might  
393 be related to the wood features of this species with relatively high wood density and small vessel size  
394 (Limousin *et al.*, 2010a). These characteristics make trees more cavitation-resistant to xylem tension,  
395 an adaptation which seems to be related to a limited capacity to reduce xylem tension via radial  
396 water release (Meinzer *et al.*, 2008, 2009; Richards *et al.*, 2014). This trade-off also explains that C<sub>s</sub> of  
397 *Q. ilex* is at the lower end of reported values (see Fig. 5 in Meinzer *et al.* 2009 for comparison).  
398 Despite low  $|f_s| / F_{STEM}$  ratios, the reliance on stored water increased with drought stress due to a  
399 more pronounced reduction in daily  $F_{STEM}$  compared to daily  $|f_s|$ . A similar pattern was also noticed  
400 in *Quercus robur* L., which used stored water primarily when subjected to drought stress (Matheny *et*  
401 *al.*, 2015). These observations suggest greater relevance of stem water reservoirs to maintain  
402 transpiration rates and tree hydraulic integrity in future drier climates (see Tyree & Ewers 1991; and  
403 Bréda *et al.* 2006).

#### 404 **4.2 Model limitations**

405 Two limitations related to the model structure and assumptions were detected during this study.  
406 First, accurate simulations of diameter variations during the wet period were restricted to time  
407 frames of 3-4 days. Beyond this short time interval, diameter simulations progressively deviated from  
408 measured values. During dry conditions, however, the length of the model period was not an issue

409 because irreversible stem growth was prevented by soil water limitation (Lempereur *et al.*, 2015).  
410 Any diameter variation during summer drought could be uniquely ascribed to radial water flow  
411 causing elastic stem shrinkage and swelling. In contrast, during the wet period when irreversible  
412 growth occurred, the carbon status of the plant is a factor involved in growth, for example via  
413 osmotic regulation of cell turgor and elongation (Lockhart, 1965; Daudet *et al.*, 2005). The lack of  
414 carbon-related equations in our water-based model describing sugar transport and/or carbon  
415 allocation to growth could explain inaccurate simulations when the modelled period extended  
416 beyond 3-4 days. Accordingly, the generally prescribed time frame for this model ranges from one  
417 day to two weeks (Steppe *et al.*, 2006, 2008b). More sophisticated models integrating water and  
418 carbon transport processes should be further developed to simulate irreversible stem growth on a  
419 seasonal basis (De Schepper & Steppe, 2010; Mencuccini *et al.*, 2015; Steppe *et al.*, 2015a).

420 Second, the model is theoretically designed to estimate  $C_s$  only for outer tissues and we ignore the  
421 amount of water released by the xylem compartment. The contribution of the xylem to whole stem  
422 diameter variations is expected to be minor (Zweifel *et al.*, 2000; Steppe & Lemeur, 2004; Steppe *et al.*,  
423 2006), and our model therefore assumes the xylem as a rigid compartment and outer tissues –  
424 namely cambium, phloem, and phelloderm – as an elastic storage compartment responsible for diel  
425 shrinkage and swelling. Nevertheless, the amount of water released for a given change in volume is  
426 higher in the xylem than in the outer tissues; about 3.5 times higher in the case of savanna trees,  
427 which results in a greater capacitance of the xylem compartment (Scholz *et al.*, 2007, 2008). Higher  
428 capacitance of the xylem can be ascribed to both elastic living parenchyma and the capacitive effect  
429 of cavitated conduits (Tyree & Ewers, 1991; Hölttä *et al.*, 2009; Richards *et al.*, 2014). Thus, water  
430 release from the xylem could be important in large trees with a high proportion of sapwood and  
431 lumen volume (Waring *et al.*, 1979; Hölttä *et al.*, 2009; Betsch *et al.*, 2011) or with large and  
432 numerous sapwood parenchyma rays such as *Q. ilex*. Models considering the capacitive effect of  
433 cavitation (Hölttä *et al.*, 2009) and the xylem as an elastic compartment with a distinct elastic bulk  
434 modulus and hydraulic capacitance (Perämäki *et al.*, 2005) would be necessary to further disentangle

435 the contribution of elastic outer tissues and xylem parenchyma, and inelastic cavitated conduits to  
436 the overall capacitive discharge of water to the transpiration stream.

#### 437 **4.3 Simulated stem water release curves, root-to-leaf vulnerability curves and model validation**

438 Simulations performed under dry conditions misestimated both  $C_S$  and  $R_X$  when extrapolated to a  
439 wider range of  $\Psi_{PD}$  during wet conditions, and values obtained for well-watered conditions were also  
440 necessary to realistically describe the  $C_S$  and  $R_X$  curves over the entire  $\Psi_{PD}$  range (Fig. 5). This  
441 observation denotes that any extrapolation beyond the surveyed range of  $\Psi_{PD}$  must be taken with  
442 caution. More frequent measurements of  $\Psi_{LEAF}$  (or  $\Psi_X$ ) would be necessary to re-calibrate model  
443 parameters at a higher temporal resolution (Steppe *et al.*, 2008b) and obtain a more accurate  
444 evolution of  $C_S$  and  $R_X$  across a wider range of  $\Psi_{PD}$ .

445 Estimates of stem water refilling following first heavy rains at the end of the drought period and the  
446 vulnerability curves obtained by measurements at the organ scale were compared to model  
447 simulations. At the end of summer drought, the modelled cumulative water release averaged 683 g  
448  $tree^{-1}$  at a  $\Psi_{PD}$  of -3.33 MPa (Fig. 5A), which is 60% of that estimated from the refilling calculations  
449 (1134 g  $tree^{-1}$  for a corresponding increase in  $\Psi_{PD}$  of 2.75 MPa, Fig. 6A). Likewise, mean  $C_S$  modelled  
450 across the range of surveyed conditions (from 103 to 314 g  $MPa^{-1} tree^{-1}$ , Fig. 5A) was lower than that  
451 estimated following heavy rains (414 g  $MPa^{-1} tree^{-1}$ , Fig. 6B). Inaccurate assumptions to estimate  
452 stem storage capacity and  $C_S$  using both approaches may account for this difference. First,  $C_S$  could  
453 be overestimated from water refilling calculations because the corresponding water potential  
454 increase was measured several days apart from the refilling event, and was therefore slightly  
455 underestimated. Besides, water refilling of branches and leaves incorrectly attributed to the stem  
456 may overestimate the actual stem storage capacity. Second,  $C_S$  might be underestimated from model  
457 simulations due to the water release from xylem tissues (Scholz *et al.*, 2008; Hölttä *et al.*, 2009)  
458 undetected by our model. Models that integrate the hydraulic capacitance of the xylem  
459 compartment, continuous *in vivo* measurements of wood water content using frequency domain

460 reflectometry (Matheny *et al.*, 2015), or destructive sampling to obtain stem moisture release curves  
461 with psychrometers (Meinzer *et al.*, 2003) might be complementary approaches to more accurately  
462 estimate the overall hydraulic capacitance of the stem. Likewise, direct measurements of  $\Psi_x$  would  
463 result in more accurate estimates of  $C_s$  than the simulated here, in which  $\Psi_x$  was inferred from  $\Psi_{LEAF}$   
464 measurements.

465 On the other hand, variation in  $R_x$  as a function of drought stress affected to a lesser extent the  
466 model performance. The simulated vulnerability curve along the root-to-leaf continuum exhibited  
467 reasonable agreement with measurements made at the organ scale at the same site. The mean  
468 simulated  $\Psi_{50}$  was -2.67 MPa (Table 3). Estimates of  $\Psi_{50}$  in excised branches and roots of *Q. ilex* trees  
469 located at the same site averaged -3.88 and -2.39 MPa, respectively, using the air injection technique  
470 after flushing native embolism (Limousin *et al.*, 2010a), and -4.7 MPa in branches using the bench  
471 drying technique (Martin-StPaul *et al.* 2014). Vulnerability to drought in the root-to-leaf continuum  
472 is determined to the greatest extent by the most vulnerable node along this hydraulic pathway (Baert  
473 *et al.*, 2015). In this particular case, roots might be the major constrain to water flow along the root-  
474 to-leaf continuum, followed by stems and branches (Tyree & Ewers, 1991; Sperry & Love, 2015).  
475 Therefore, the integrated  $\Psi_{50}$  (-2.67 MPa) might primarily reflect the hydraulic vulnerability of roots.  
476 This alternative approach to generate integrated root-to-leaf vulnerability curves might be useful to  
477 describe the hydraulic functioning of the whole tree while avoiding to separately measure multiple  
478 hydraulic resistances (Baert *et al.*, 2015), which might be controversial due to the strong variability in  
479 hydraulic conductance ascribed to methodological issues (Cochard & Delzon, 2013; Martin-StPaul *et*  
480 *al.*, 2014).

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628 **Table 1.** Diameter at breast height (DBH), tree height, accumulated diameter increment and mean  
 629 daily sap flow during 2009 for the six monitored *Quercus ilex* trees.

	DBH	Height	Annual diameter increment	Mean sap flow
	(cm)	(m)	(mm year <sup>-1</sup> )	(kg day <sup>-1</sup> )
TREE1	9.55	5.3	0.25	2.55
TREE2	11.05	5.0	0.16	3.00
TREE3	10.70	5.0	0.51	5.87
TREE4	13.20	5.6	1.21	7.32
TREE5	10.05	5.2	-0.10	2.90
TREE6	12.25	4.5	1.15	3.00

630 Tree DBH measured at the beginning of the 2009 growing season

631

632 **Table 2.** Hydraulic resistance to radial flow between the xylem and the storage compartment ( $R_s$ ),  
633 hydraulic resistance of the root-to-leaf segment ( $R_x$ ), and stem hydraulic capacitance ( $C_s$ ) obtained  
634 from the mechanistic water flow and storage model describing the hydraulic functioning of *Quercus*  
635 *ilex* trees during the wet season when stem growth occurred.

	$R_s$	$R_x$	$C_s$
	(MPa h g <sup>-1</sup> )	(MPa h g <sup>-1</sup> )	(kg MPa <sup>-1</sup> m <sup>-3</sup> )
	10 <sup>-2</sup>	10 <sup>-4</sup>	
TREE1	0.97	4.59 [4.59 - 4.59]	64.02 [54.66 – 72.22]
TREE2	1.41	5.72 [5.72 -5.72]	50.06 [45.03 – 54.79]
TREE3	0.93	4.59 [4.59 -4.59]	86.07 [73.33 – 98.28]
TREE4	0.53	3.65 [3.62 -3.69]	61.38 [54.98 – 66.94]
TREE5 <sup>1</sup>	NA	NA	NA
TREE6	1.15	6.49 [6.38 – 6.62]	46.91 [41.67 – 52.69]
mean	1.00	5.01	61.69
(SE)	(0.13)	(0.45)	(6.30)

636  $R_s$  was assumed constant whereas  $R_x$  and  $C_s$  were allowed to vary with predawn water potential (Eqn.  
637 1 and Eqn. 4, respectively). The modelled period lasted 3-4 days and included DOY176, when leaf  
638 water potential was measured. Mean values of  $R_x$  and  $C_s$  on a storage volume basis are shown;  
639 minimum and maximum values for this period are indicated in square brackets.

640 <sup>1</sup> TREE5 was not modelled due to an inconsistent dendrometer signal.

641 **Table 3.** Calibrated parameters used in the mechanistic water flow and storage model describing the  
 642 hydraulic functioning of *Quercus ilex* trees during summer drought when stem growth was impeded.  
 643 The hydraulic resistance ( $R_x$ ) and hydraulic capacitance ( $C_s$ ) were allowed to vary with predawn water  
 644 potential ( $\Psi_{PD}$ ). Estimates of  $C_s$  and the  $\Psi_{50}$  from the vulnerability curve were obtained from model  
 645 simulations.

	Calibrated parameters <sup>1</sup>					$C_s$ <sup>2</sup>		$\Psi_{50}$ <sup>3</sup>
	$R_s$	$c_1$	$c_2$	$r_1$	$r_2$	DOY208	DOY234	
	(MPa h g <sup>-1</sup> )	(g <sup>-1</sup> )	(MPa g <sup>-1</sup> )	(MPa h g <sup>-1</sup> )	(MPa <sup>-2</sup> )	(kg MPa <sup>-1</sup> m <sup>-3</sup> )		(MPa)
	10 <sup>-2</sup>	10 <sup>-3</sup>	10 <sup>-3</sup>	10 <sup>-3</sup>	10 <sup>-1</sup>			
TREE1	1.95	-3.07	2.68	0.99	1.29	26.52	18.48	-2.32
TREE2	1.73	-2.54	2.01	1.68	0.67	28.91	19.84	-3.21
TREE3	2.30	-2.33	2.78	1.26	1.53	31.75	23.34	-2.13
TREE4	0.53	-0.73	1.11	0.77	0.91	56.30	45.30	-2.76
TREE5	1.31	-2.99	1.20	3.15	1.55	37.43	22.66	-2.12
TREE6	1.88	-2.28	2.34	3.67	0.58	28.04	19.96	-3.46
mean	1.62	-2.32	2.02	1.92	1.09	34.82	24.93	-2.67
(SE)	(0.25)	(0.35)	(0.29)	(0.49)	(0.17)	(4.57)	(4.14)	(0.23)

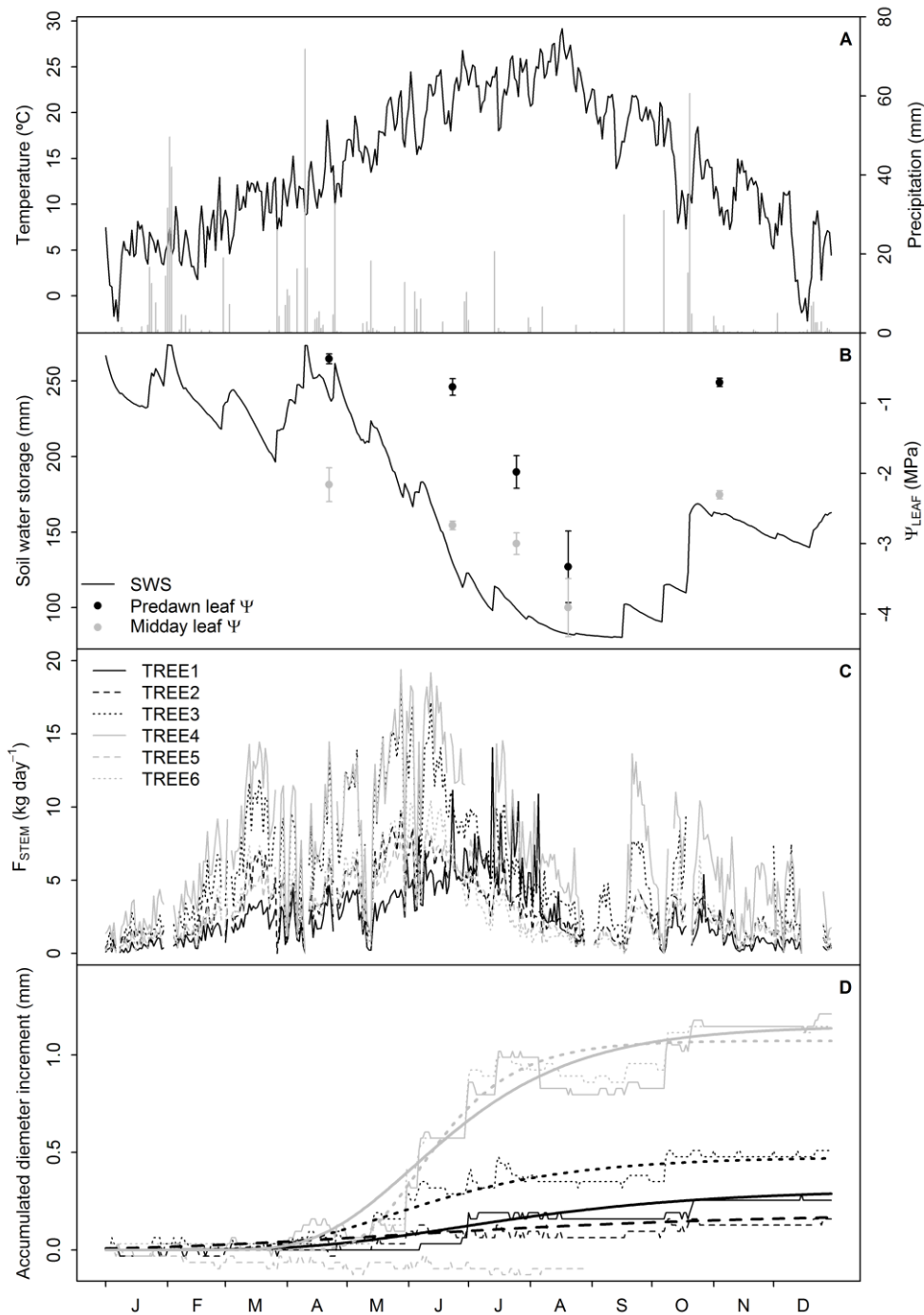
646 <sup>1</sup> Five parameters were calibrated: the proportionality parameters  $c_1$  and  $c_2$  defining  $C_s$  (Eqn. 4), the  
 647 proportionality parameters  $r_1$  and  $r_2$  defining  $R_x$  (Eqn. 1), and the radial hydraulic resistance between  
 648 the xylem and the storage compartment ( $R_s$ ).

649 <sup>2</sup>  $C_s$  was estimated for two dates when  $\Psi_{PD}$  was measured (DOYs 208 and 234) and calculated on a  
 650 storage volume basis.

651 <sup>3</sup>  $\Psi_{50}$  is the  $\Psi_{PD}$  causing 50% loss of maximum hydraulic conductance along the integrated  
 652 root-to-leaf continuum.

653

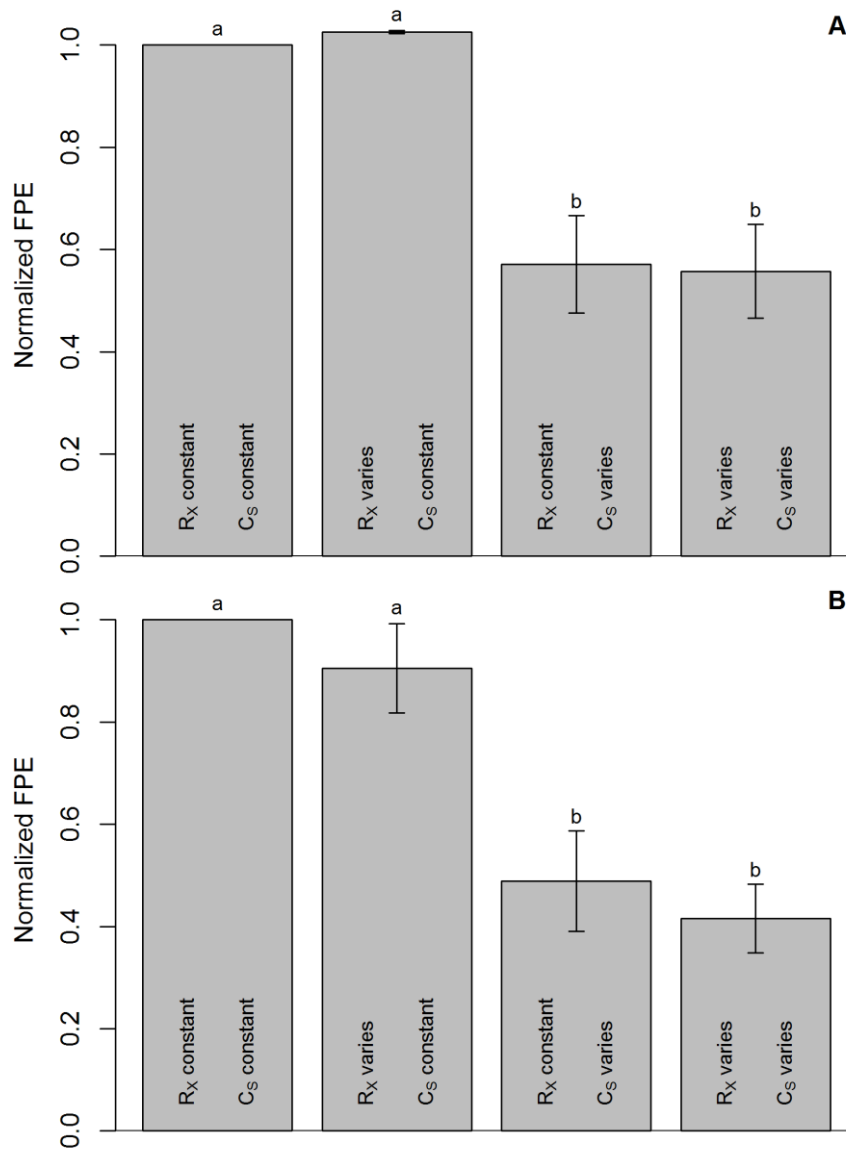
654 **Figure 1.** Daily air temperature and precipitation (A), soil water storage and predawn and midday leaf  
 655 water potential (means  $\pm$  SE; B), daily sap flow (C), and daily stem diameter variations (D) during the  
 656 year 2009. Ecophysiological measurements were performed on six *Quercus ilex* trees of the  
 657 experimental site.



658

659 Curves of accumulated diameter increment were smoothed according to the Gompertz's equation  
 660 (dashed lines). Diel variations in diameter are not shown for clarity.

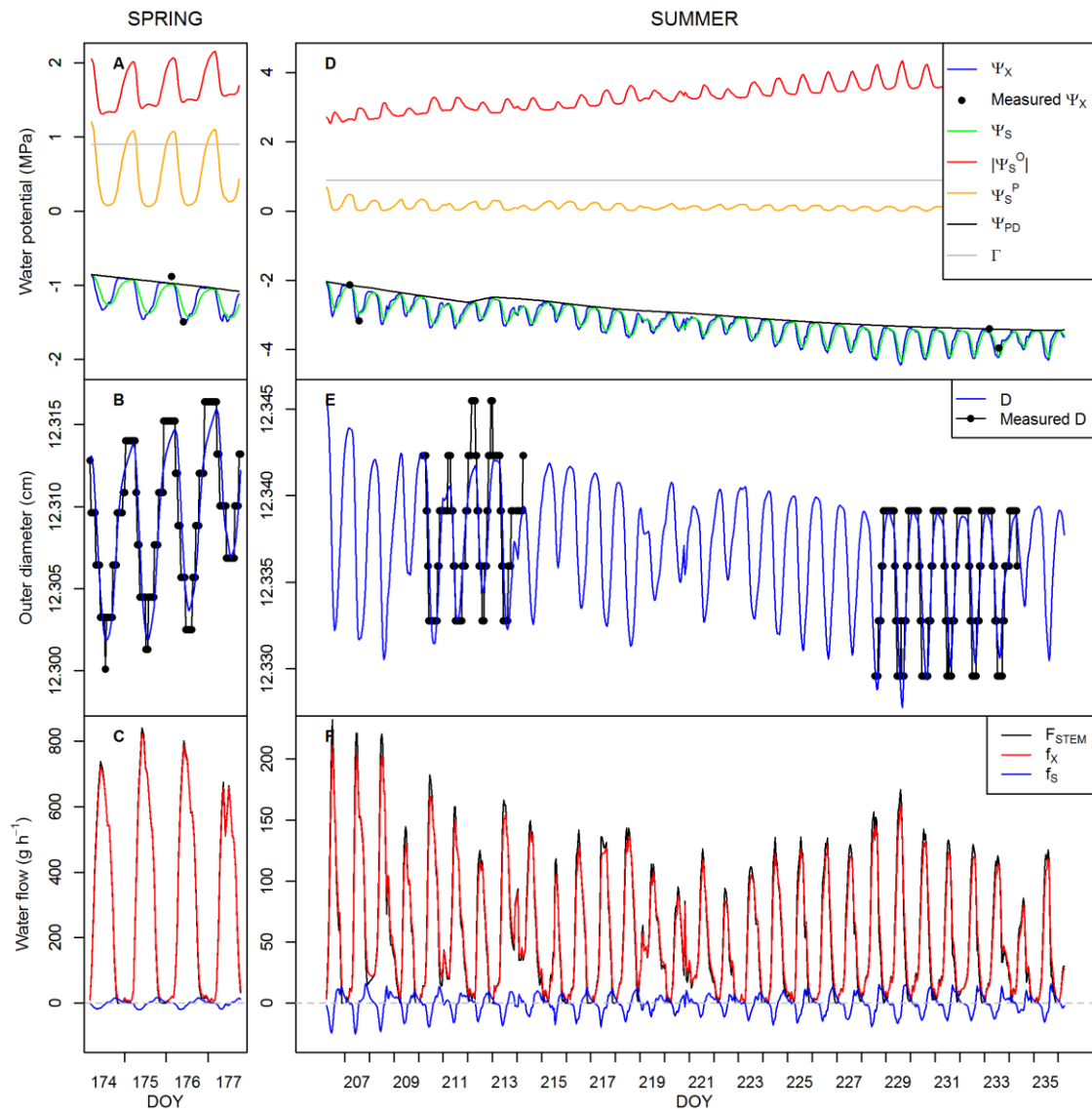
661 **Figure 2.** Normalized final prediction error (FPE) of four tested models with constant or variable  
 662 hydraulic resistance ( $R_x$ ) and capacitance ( $C_s$ ) to compare model performance. Models were used to  
 663 simulate hydraulic functioning of *Quercus ilex* trees under wet (A) and dry (B) conditions.



664

665 The FPE evaluates the accuracy of simulated diameter variations ( $\Delta D$ ) and xylem water potential ( $\Psi_x$ )  
 666 and penalizes over-parameterized models. Low FPE values indicate better model performance.  
 667 Values of FPE were normalized relative to the model with constant  $R_x$  and  $C_s$  to remove inter-stem  
 668 variability associated to the number of observations. Normalized FPE was averaged among six trees.  
 669 Different letters show significant differences ( $P < 0.05$ ).

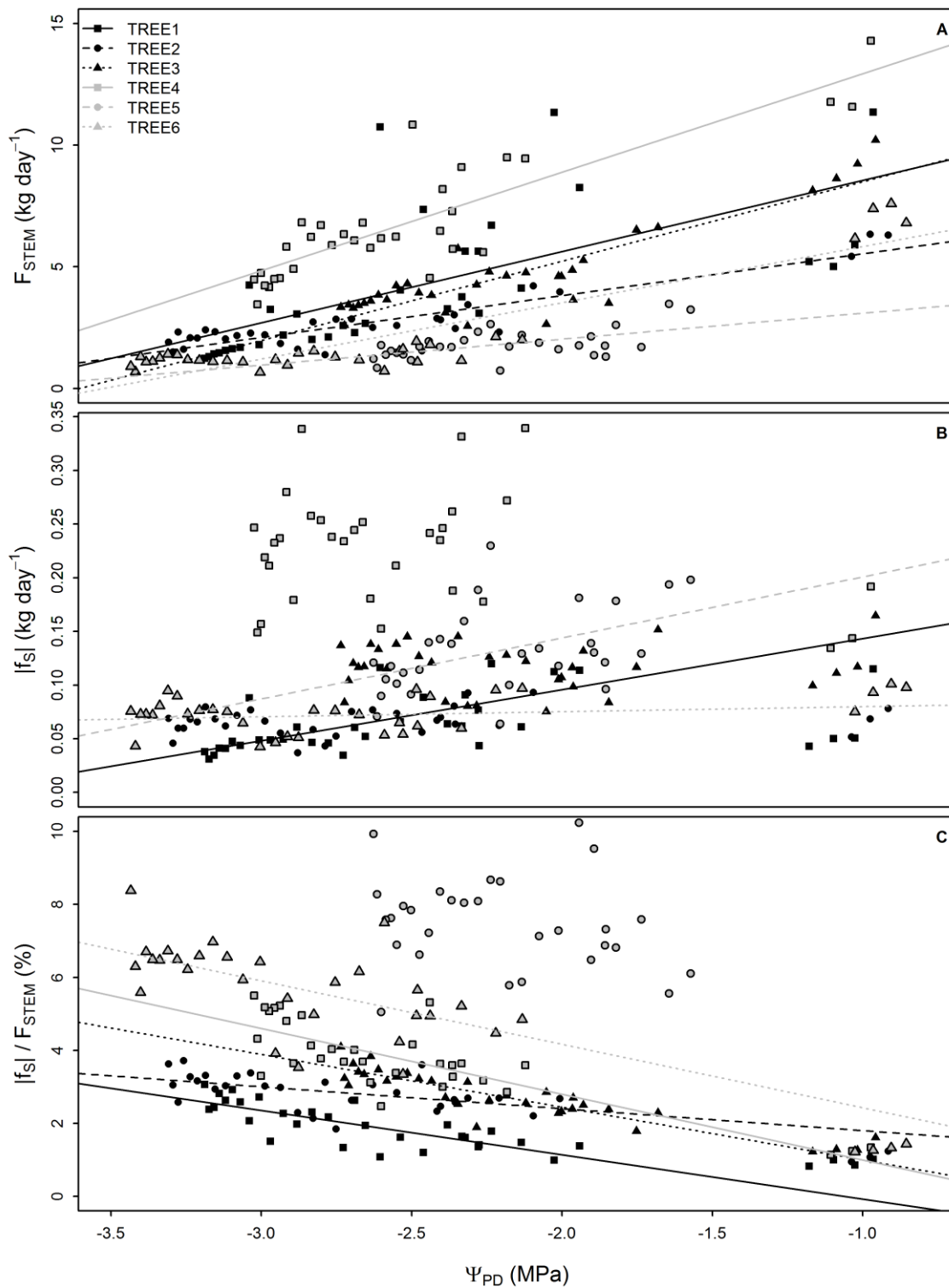
670 **Figure 3.** Measured and simulated water potentials (A, D), diameter variations (B, E) and water flows  
 671 (C, F) in *Quercus ilex* trees during the wet (A-C) and the dry (D-F) season. Predawn water potential  
 672 ( $\Psi_{PD}$ ) and sap flow ( $F_{STEM}$ ) (continuous black lines) were used as model inputs, whereas diameter  
 673 variations and xylem water potential ( $\Psi_x$ ) (black dots) were used for calibration purposes.



675 This figure displays an example of model simulation for a single tree (TREE6) when the hydraulic  
 676 resistance and hydraulic capacitance were allowed to vary with predawn water potential (best model  
 677 obtained). Under well-watered conditions, cell turgor ( $\Psi_s^P$ ) at night-time exceeded the critical value  
 678 for wall-yielding ( $\Gamma$ ) (A) resulting in irreversible stem growth (B). During summer drought,  $\Psi_s^P$  never  
 679 exceeded  $\Gamma$  (D) and irreversible stem growth was impeded (E). The storage compartment supplied  
 680 water to the xylem to fulfill transpiration requirements during the morning (negative  $f_s$ ) and was  
 681 refilled during the afternoon (positive  $f_s$ ) (C, F). Radial water exchange caused diel patterns of stem  
 682 shrinkage and swelling. Note different scales for the same variables in wet and dry periods. Note that  
 683 absolute values of osmotic water potential ( $\Psi_s^O$ ) are displayed for clarity.



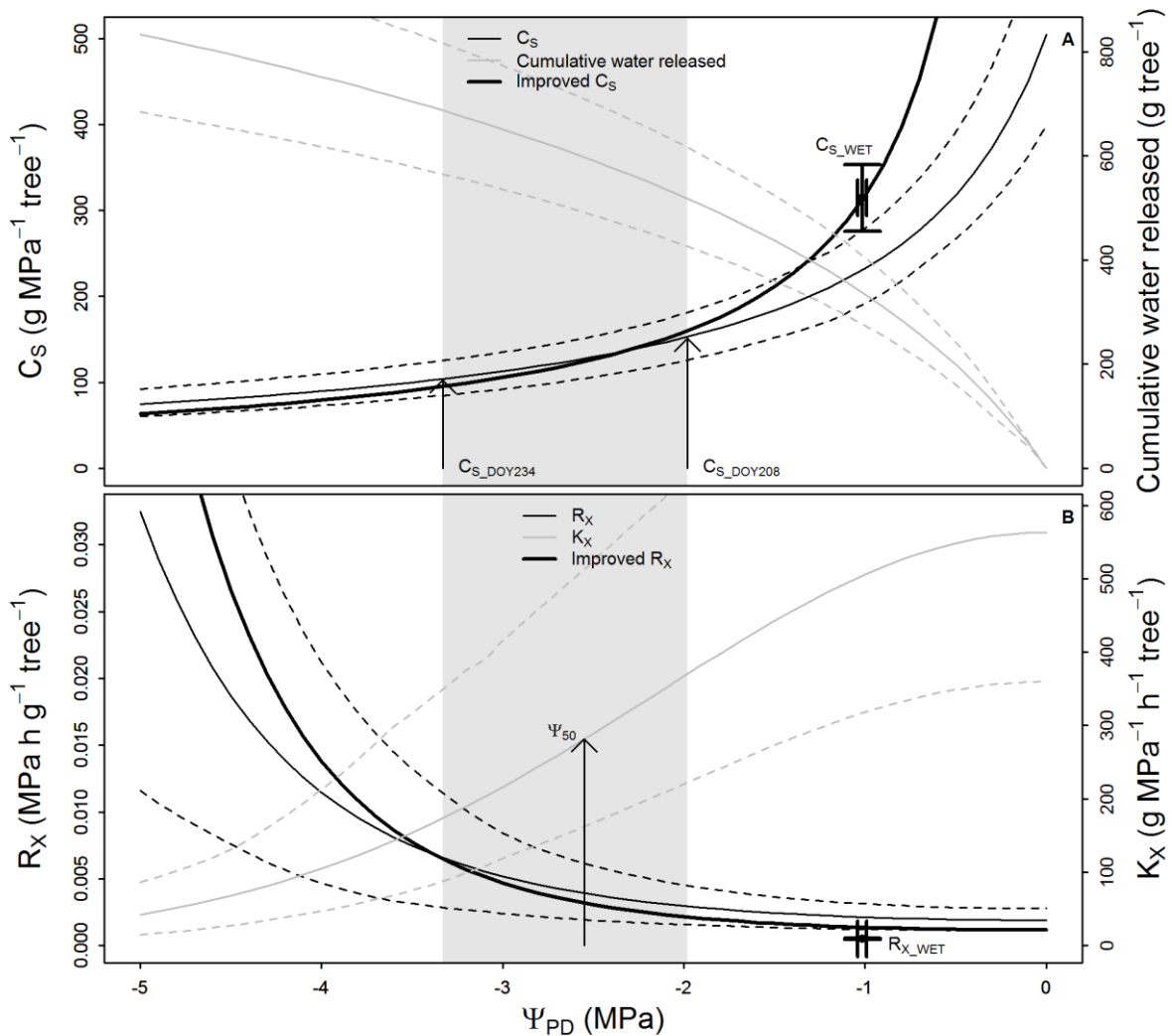
684 **Figure 4.** Variation in daily sap flow (A;  $F_{STEM}$ ), daily stem water release (B;  $|f_s|$ ), and the contribution  
 685 of  $|f_s|$  to  $F_{STEM}$  (C) in *Quercus ilex* trees along a gradient of predawn water potential ( $\Psi_{PD}$ ).



686

687 Data from model simulations in early summer (wet period) and summer drought (dry period) are  
 688 pooled. Only significant regressions are depicted ( $P < 0.05$ ).

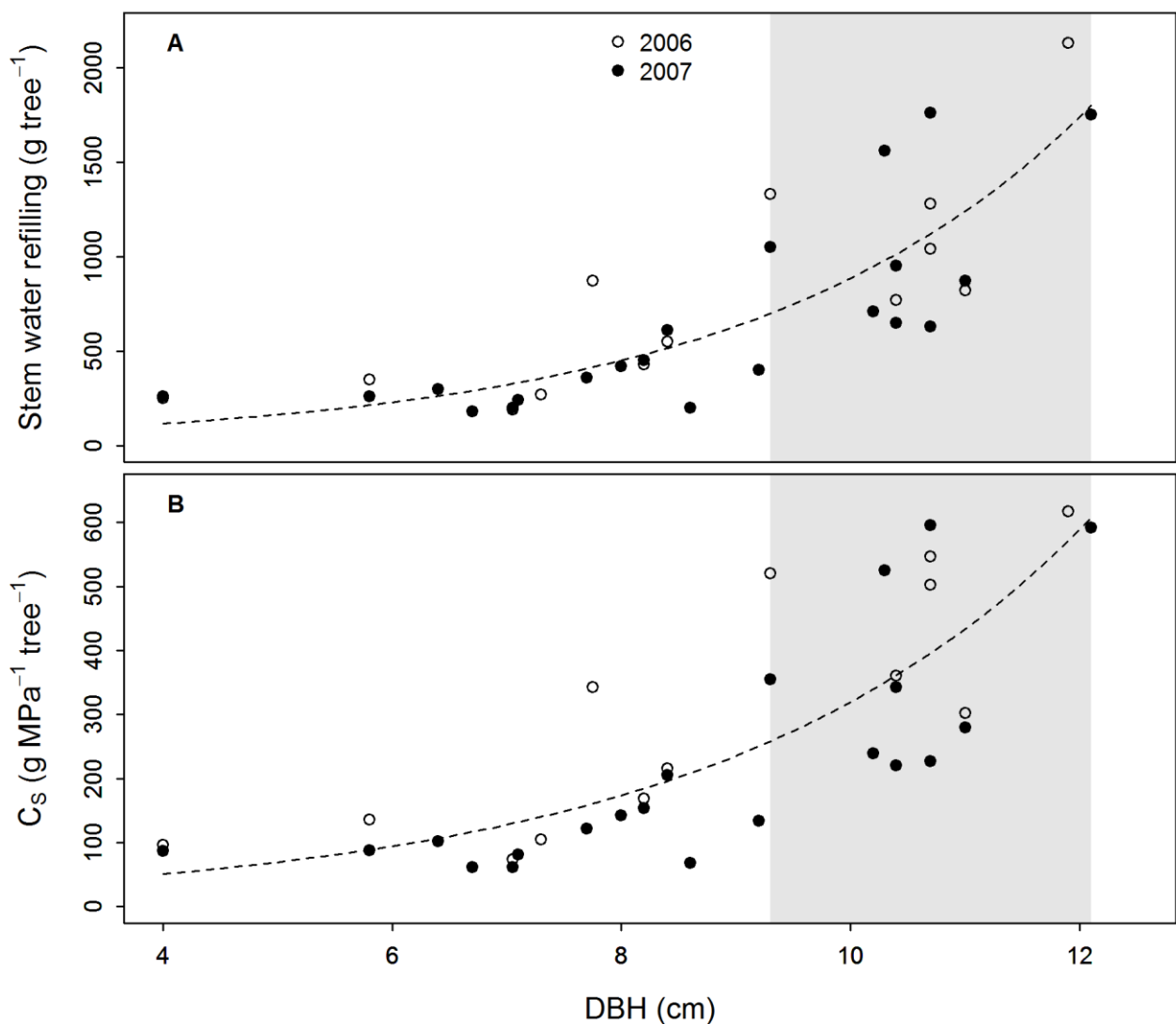
689 **Figure 5.** Hydraulic capacitance ( $C_S$ ) and cumulative water released at the tree level (A), and hydraulic  
 690 resistance ( $R_X$ ) and conductance ( $K_X$ ) in the root-to-leaf continuum (B) along a gradient of predawn  
 691 water potential ( $\Psi_{PD}$ ).



692

693 Calibrated parameters obtained from six *Quercus ilex* trees during the dry period (Table 3) were used  
 694 to estimate the mean (continuous line) and 95<sup>th</sup> and 5<sup>th</sup> percentile (dashed lines) curves of each  
 695 variable. The calibrated parameters were obtained from a mechanistic model in which  $R_X$  (Eqn. 1)  
 696 and  $C_S$  (Eqn. 4) were allowed to vary with  $\Psi_{PD}$ . Shaded areas indicate the modelled dry period, when  
 697 average  $\Psi_{PD}$  ranged between -1.98 and -3.33 MPa. The curves of  $C_S$  and  $R_X$  adjusted for long-term  
 698 (one-month) simulations of the dry period (in black) were improved by including values of the short-  
 699 term (3-4 days) calibrations of the wet period (in red).

700 **Figure 6.** Stem water refilling (A) and hydraulic capacitance ( $C_s$ ) (B) at the tree level estimated after  
 701 the first heavy rain following the dry season. Two rain events registered in 2006 and 2007 (open and  
 702 closed circles, respectively) met the minimum requirements to estimate stem storage capacity. Stem  
 703 water refilling and  $C_s$  were estimated for a total of 23 *Quercus ilex* trees ranging in diameter at breast  
 704 height (DBH) from 4 to 12.1 cm. Stem water refilling and  $C_s$  were exponentially related to tree DBH  
 705 (Stem water refilling =  $30.27 \times e^{(0.34 \times \text{DBH})}$ ;  $C_s = 15.05 \times e^{(0.31 \times \text{DBH})}$ ;  $P < 0.001$ ). Shaded areas indicate the  
 706 range in DBH of trees additionally surveyed for modelling.



707