



Computational Fluid Dynamic design of steam cracking reactors: extrusion method for simulation of dynamic coke layer growth

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Coke reduction methods

- Feed additives
- Metal surface technologies
- 3D reactor technology



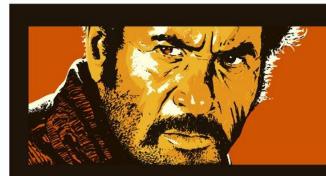
3D reactor technology | The Good, the Bad & the Ugly



Enhanced heat transfer & mixing → Less cokes?

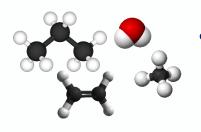
Increased pressure drop Lower olefin selectivity?





Long term performance and stability?

Where are we?



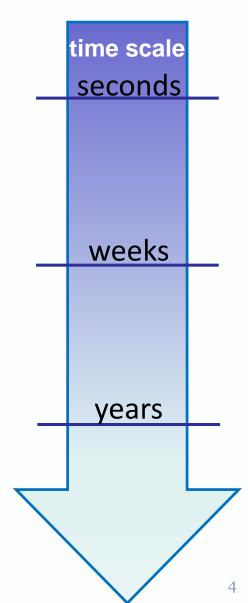
- Short term performance
 - Reactor residence time
 - Product yields, selectivities



- Intermediate term performance
 - Reactor run length
 - Coking rate, pressure drop, TMT



- Long term performance
 - Reactor stability & lifetime
 - Deterioration of reactor material

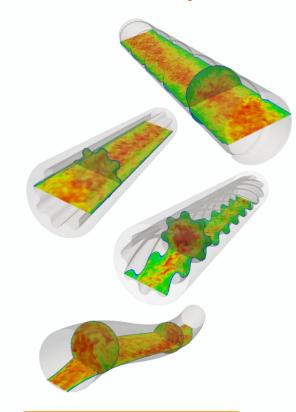


1D Reactor performance

Does the improved coking rate outweigh the loss of selectivity?

In a 1D world...

1D Simulation	Bare	Straight fins	Rifled	MERT	SFT
ΔP/ΔP _{Bare}	1.00	1.22	1.67	2.17	1.26
U/U _{Bare}	1.00	1.21	1.58	1.50	1.19
T _{gas/cokes} [K]	1079.4	1066.4	1050.2	1054.5	1066.9
Rel. r _{coke}	-	-4.8%	-34.9%	-43.1%	-24.1%
Rel. yield C ₂ H ₄	-	-0.27%	-0.83%	-1.47%	-0.32%
Rel. yield C ₃ H ₆	-	+0.03%	+0.08%	+0.13%	+0.03%



~ seconds

~ 1000 CPU hours

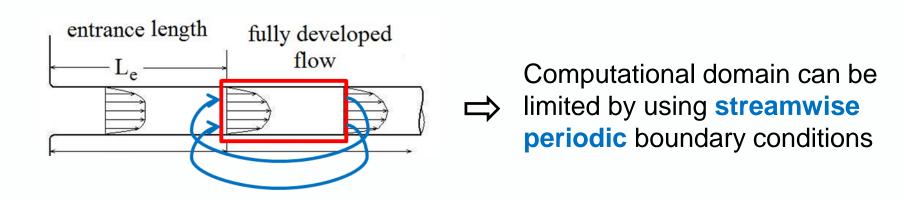
3D CFD simulations are computationally very expensive

Spatial vs. streamwise periodic

Full-scale reactor simulation



Trick: streamwise periodicity



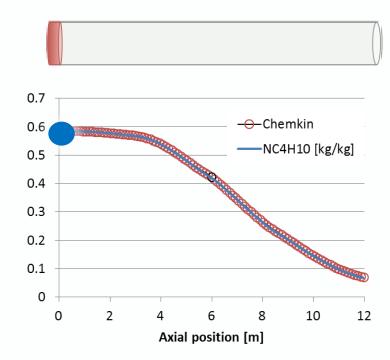
Periodic reactive simulations

- Assume velocity fully-developed over the short computational volume
- Use transient velocity field to evaluate species and enthalpy radial mixing
- Translate transient results back to the true steady-state by reconstructing the position from the bulk velocity:

Transformation: Time → Position

$$\Delta z = U_{bulk} \, \Delta t = \frac{\int_{\partial V} \rho u_z dA}{\int_{\partial V} \rho dA} \, \Delta t$$

Speedup factors of 200+



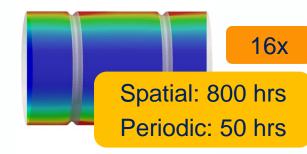
Periodic reactive | 3D Product yields

250x

Spatial: 10 hrs

Periodic: 0.04 hrs

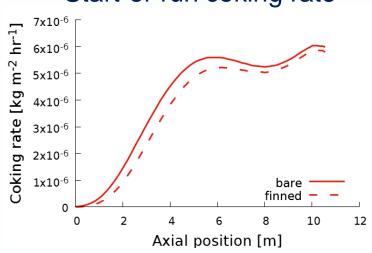




	Bare tube	Finned tube	Ribbed tube
COT [K]	1152.6	1151.6	1155.2
TMT [K]	1230.6	1222.7	1177.2
ΔP [Pa]	27682	29061	110001
Conversion	74.96%	74.99%	76.18%
CH4	13.96%	14.04%	14.54%
C2H2	1.64%	1.69%	1.55%
C2H4	27.60%	27.87%	27.74%
C2H6	1.23%	1.27%	1.32%
C3H6	22.91%	22.50%	23.52%
1,3-C4H6	2.91%	2.97%	2.88%

Coke formation | The Ugly

Start-of-run coking rate



Evaluation of 3D reactor technologies requires tracking coke layer growth

NO streamwise periodicity

NO limitation of computational domain

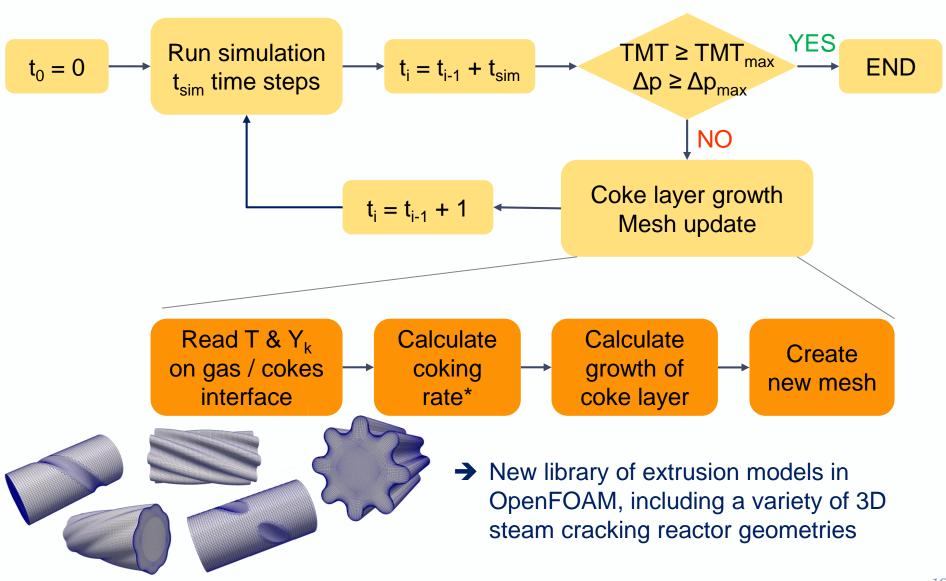
NO fast periodic simulation approach



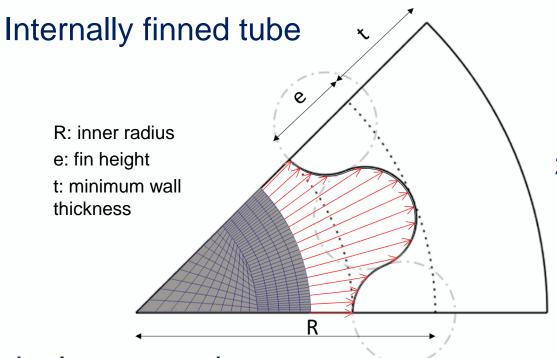


Tracking coke formation requires simulation of the entire geometry and is **computationally very expensive**

Dynamic modeling of coke formation

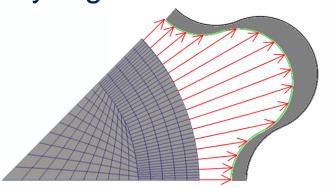


Extrusion of 3D reactor geometries



- 1. Start from core cylindrical geometry
- 2. Extrusion to 3D surface

Coke layer growth



Extrusion of gas and cokes region from core cylinder wall to specified surface geometry, while taking into account calculated coke layer thickness

Test case | Millisecond propane cracker

Feedstock 118.5 kg/h propane

Propane conversion 80% (± 0.05%)

Steam dilution 0.326 kg/kg

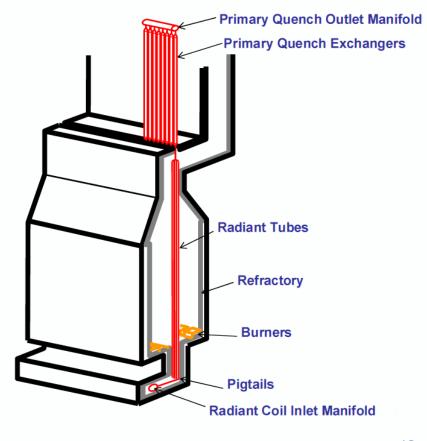
• CIT 903.7 °C

COP 170 kPa

Two geometries were simulated

- Same reactor volume
- Same axial length
- Same minimal wall thickness



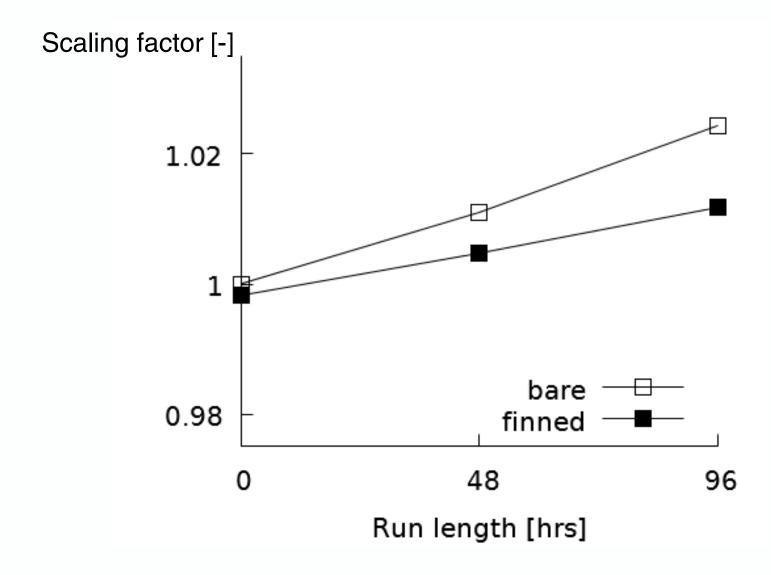


Run length simulation

Two mesh updates, each corresponding to 48 hours of coke layer growth Heat flux updated to keep propane conversion constant 10 Axial position [m] Increasing run length 96h SOR 2

Heat flux [W m⁻²]

Heat flux correction



CFD model | Setup



Turbulence modeling

• RANS: $k-\omega$ SST model (Menter, 2001)

Numerical setup

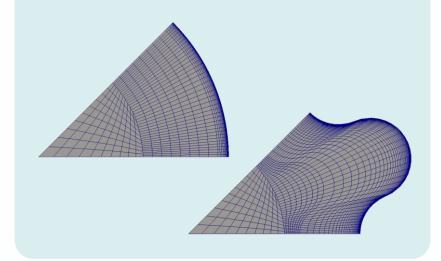
- Steady-state
- SIMPLE algorithm
- 2nd order central differencing spatial discretization scheme

Chemistry model

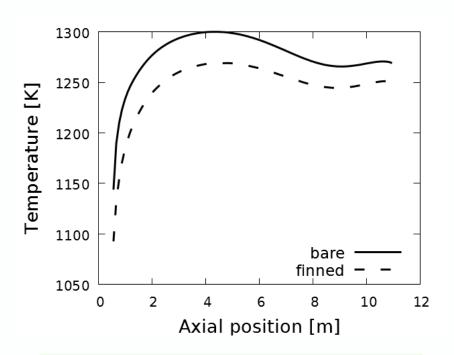
- Full single-event microkinetic CRACKSIM model reduced to core for propane cracking:
 - 151 reactions
 - o 29 species (13 radicals)

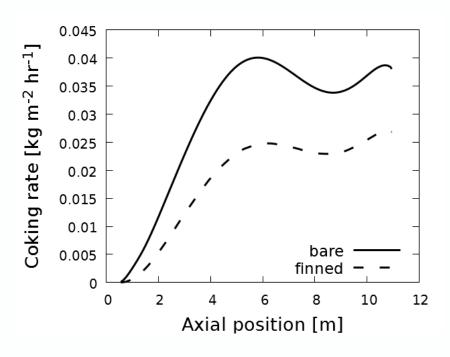
Meshing

- Structured grids for improved grid spacing control and cell orthogonality
- 1/8th of the tube's cross section
- Near wall grid resolution satisfying y⁺ < 1



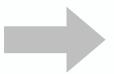
SOR Performance





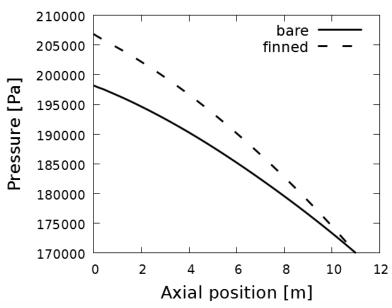
Max. TMT finned: 30 K lower

Max. coking rate: 32.5% lower



Increased run length?

Product selectivities



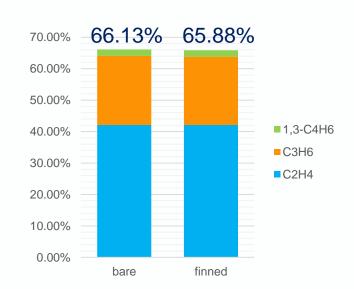
Minor effect on *total* olefin selectivity

Radial mixing effects cannot be predicted based on 1D simulations only

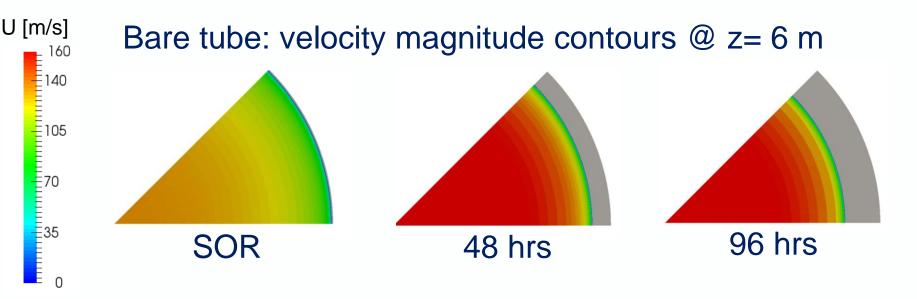
Reactor pressure drop 30% higher



Lower olefin selectivity?

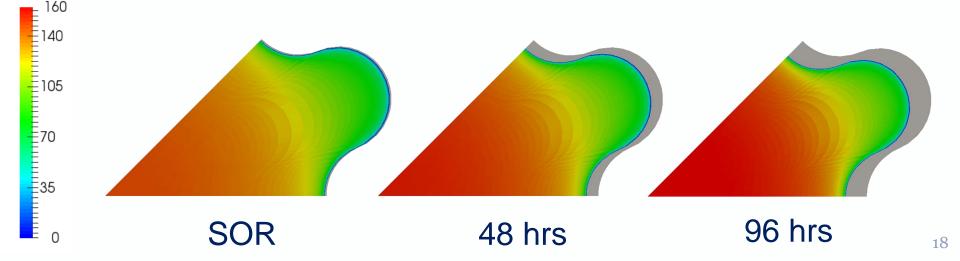


Coke layer growth



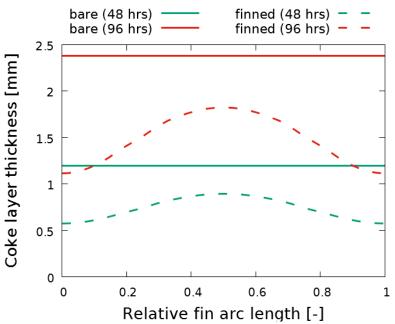
Finned tube: velocity magnitude contours @ z= 6 m

U [m/s]



Coke layer growth





Large difference in coke layer thickness BUT greater internal surface area



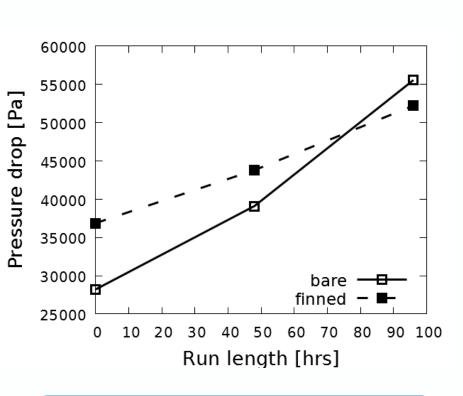
Small difference in effective coke volume

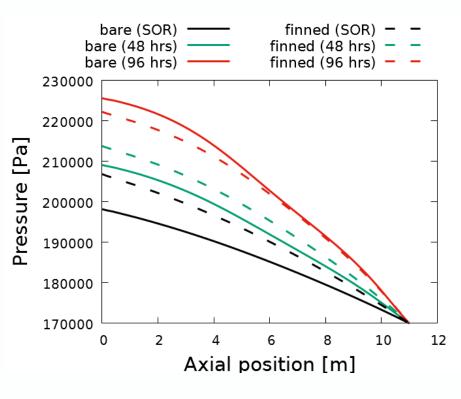
Coke volume at $z = 6 \text{ m} [\text{cm}^3 \text{ m}^{-1}]$

	Bare	Finned
48 hrs	12.98	11.84
96 hrs	23.59	23.24

Total coke volume for finned tube still smaller than for bare tube

Pressure drop





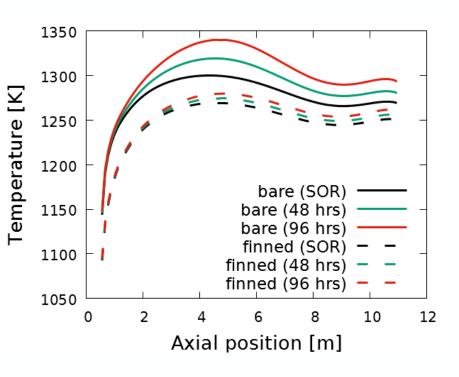
Cross-sectional flow area decreases

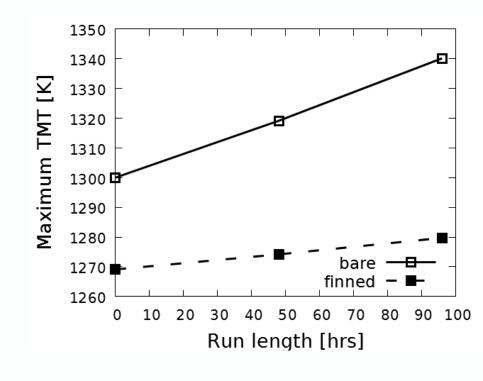


Pressure drop increases

Pressure drop increase for bare tube almost 2x faster than for finned tube

Tube metal temperature





Thermal resistance coke layer



Max. TMT increases

TMT increase for bare tube 4x faster than for finned tube

Conclusions & future work

- 3D computational fluid dynamic simulations allow optimization of industrial steam cracking reactors
- New method to perform yield & run length simulations of industrial steam crackers was developed
 - Combination with streamwise periodic simulations not possible
- Proof-of-concept reactive simulation of industrial propane cracker: bare vs. finned tubes
 - Strongly non-uniform formation of cokes in fins
 - Pressure drop increases faster in bare tube
 - TMT increases faster in bare tube
- Advantages of other 3D geometries (e.g. MERT) over finned tubes to be evaluated

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Thank you for your attention!

