

Bridges in modelling and simulation of steam cracking: from fossil to renewable feedstock and from molecule to furnace

Kevin M. Van Geem and Guy B. Marin

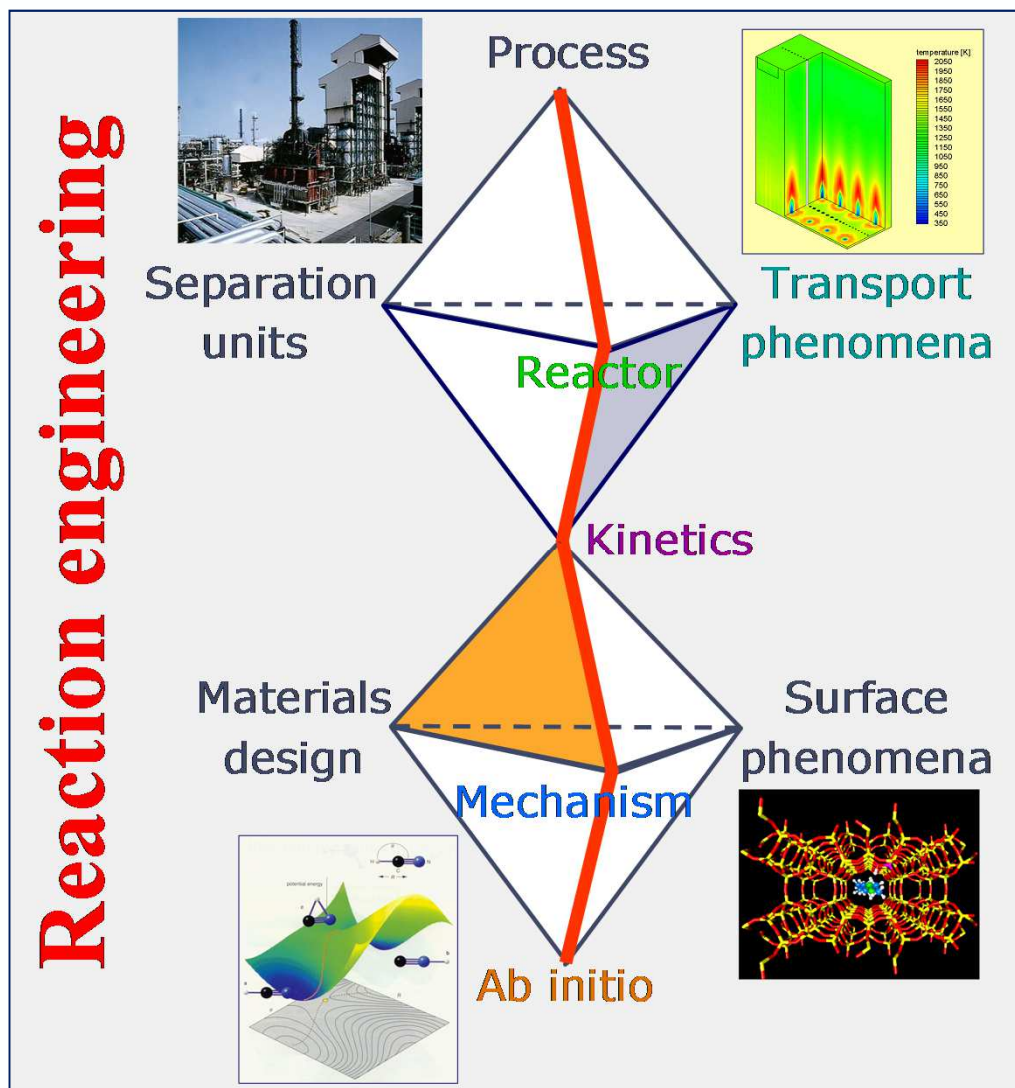
Laboratory for Chemical Technology, Ghent University

<http://www.lct.UGent.be>

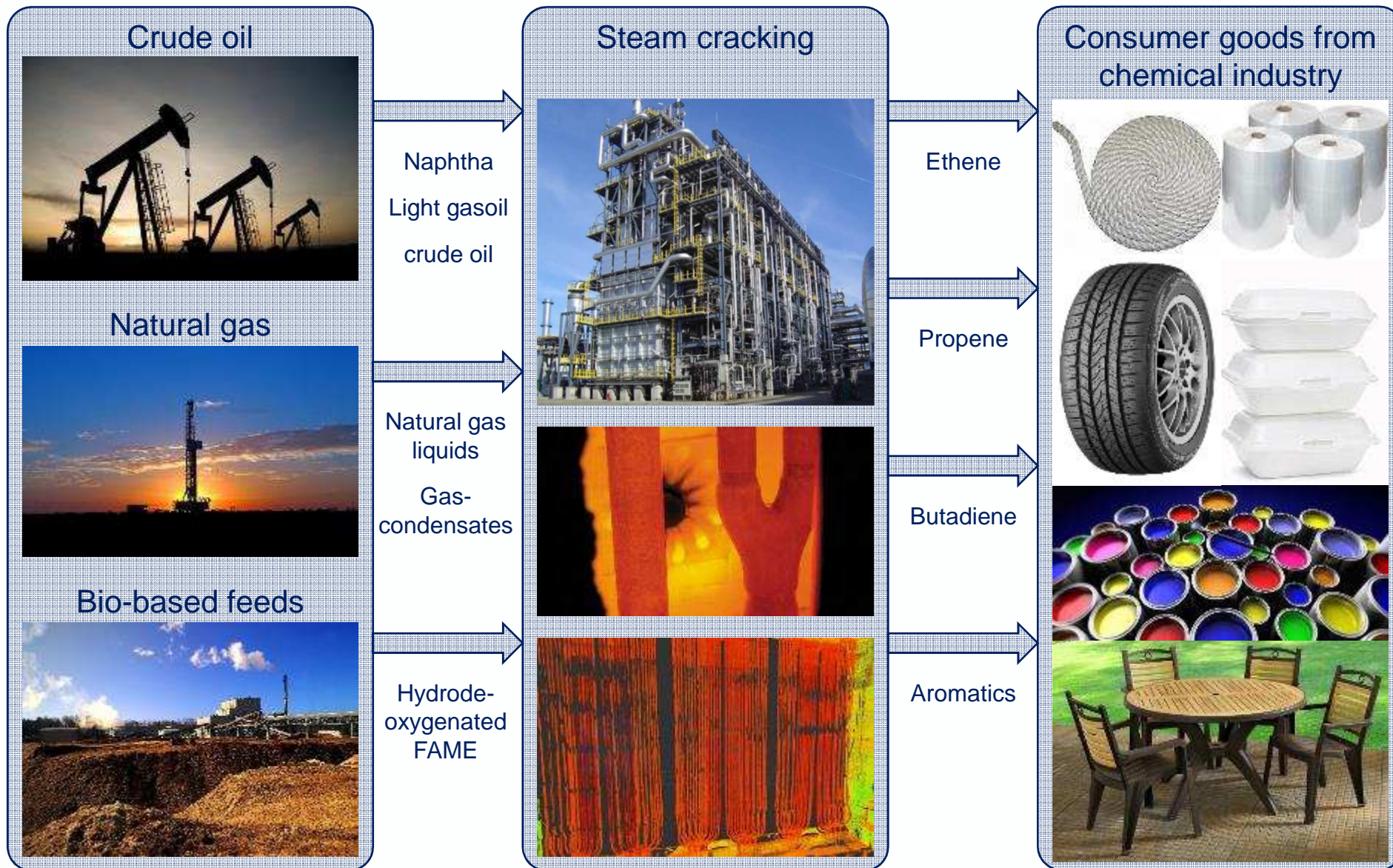


66th Canadian Chemical Engineering Conference “Sustainability & Prosperity”
October 16-19 (2016) Québec City (Canada)

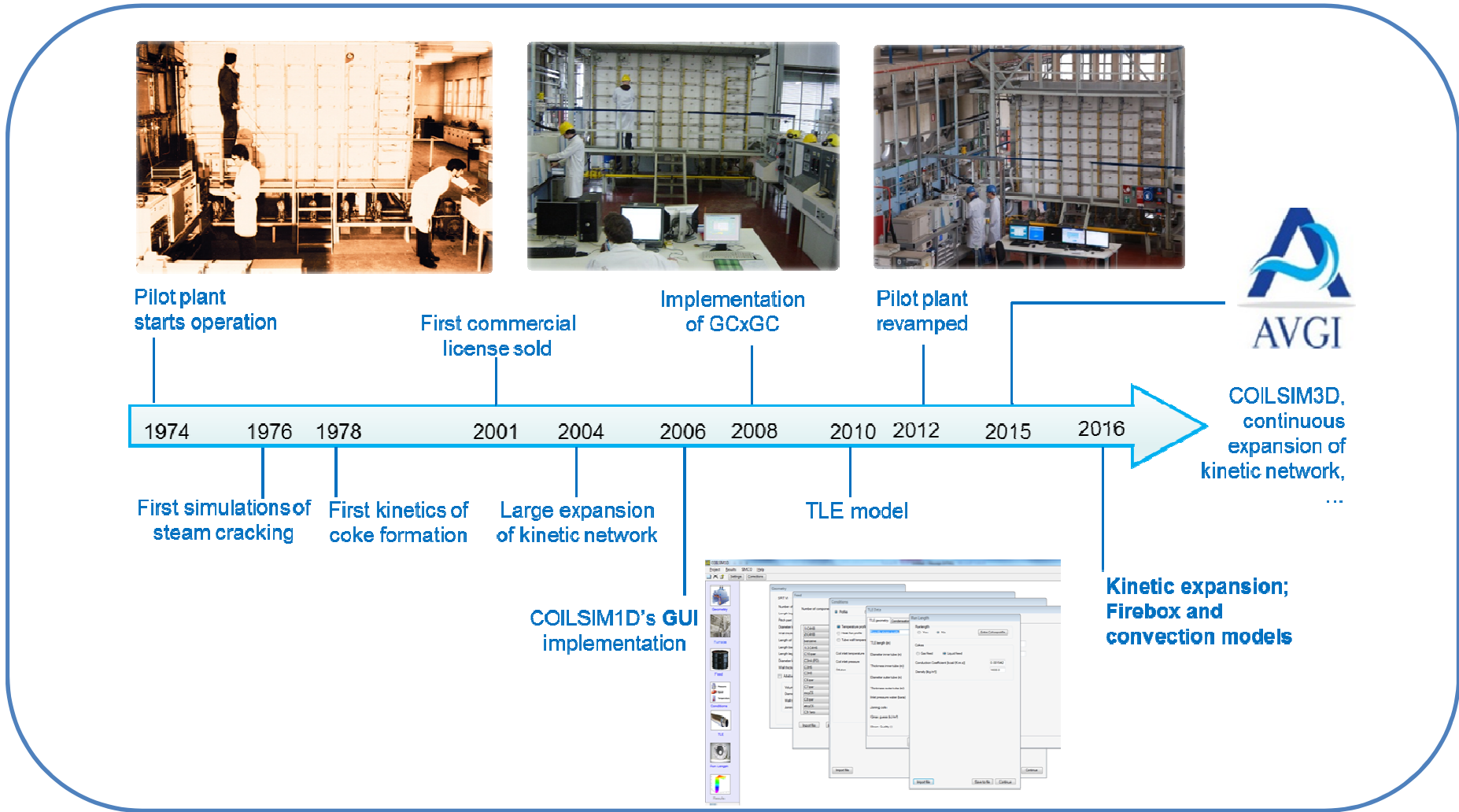
From molecule to industrial plant



Steam cracking: from fossil to renewables

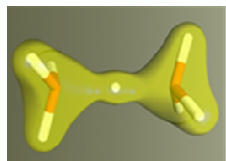
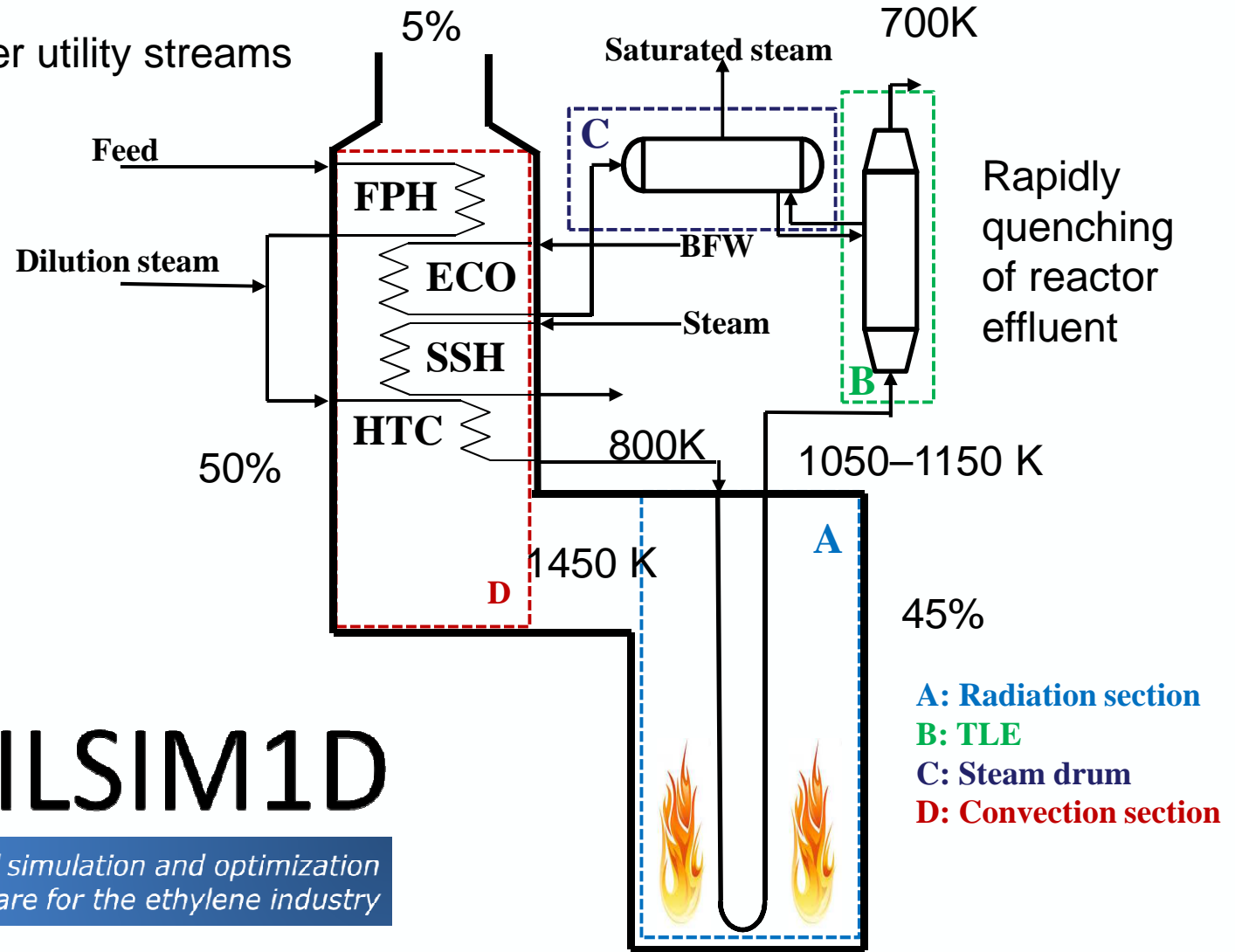


Steam cracking: Ghent University history



Steam cracking: hot section

Preheat feed and other utility streams

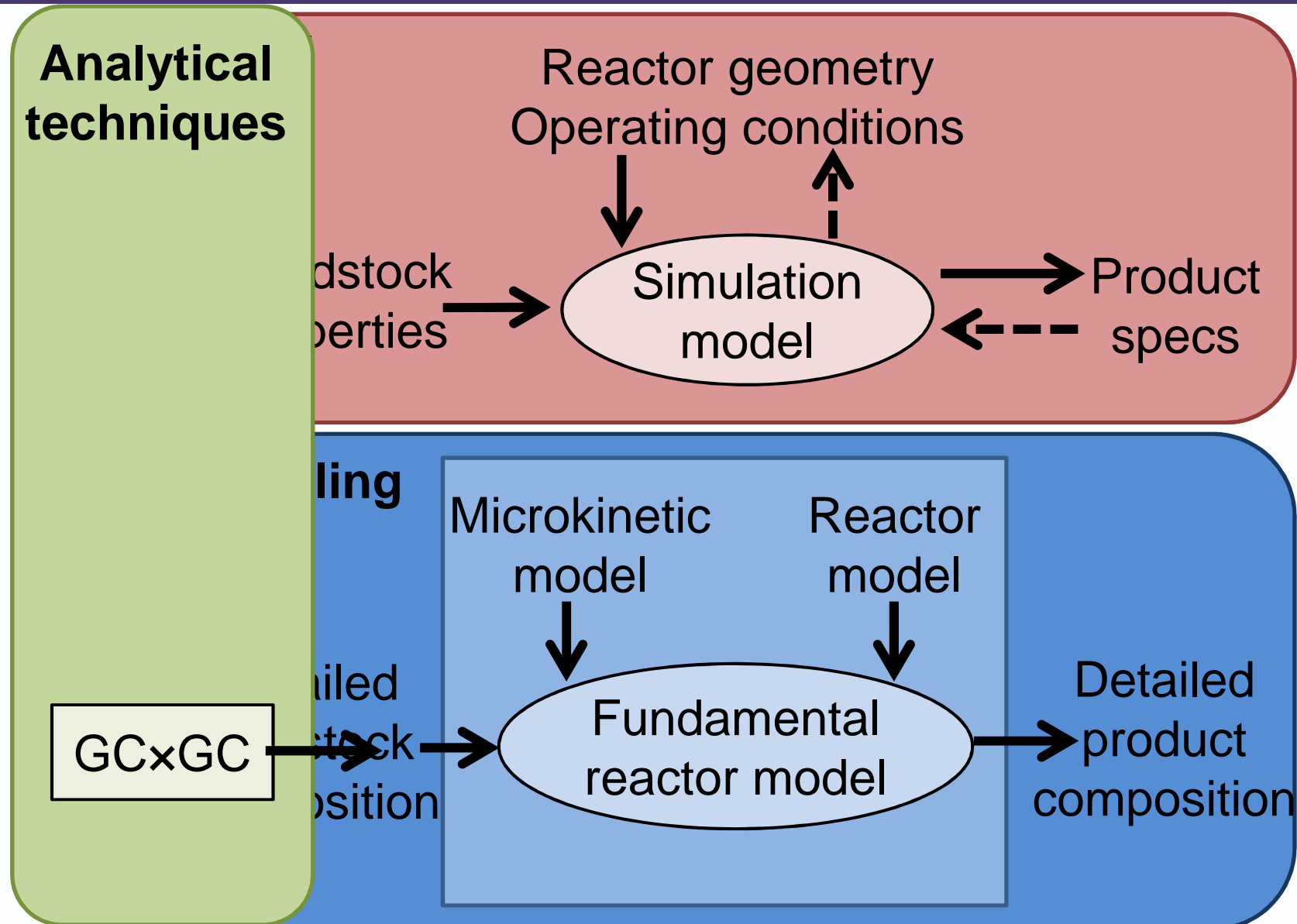


COILSIM1D

The advanced simulation and optimization software for the ethylene industry

Endothermic process 1050–1150 K

Reaction and reactor model



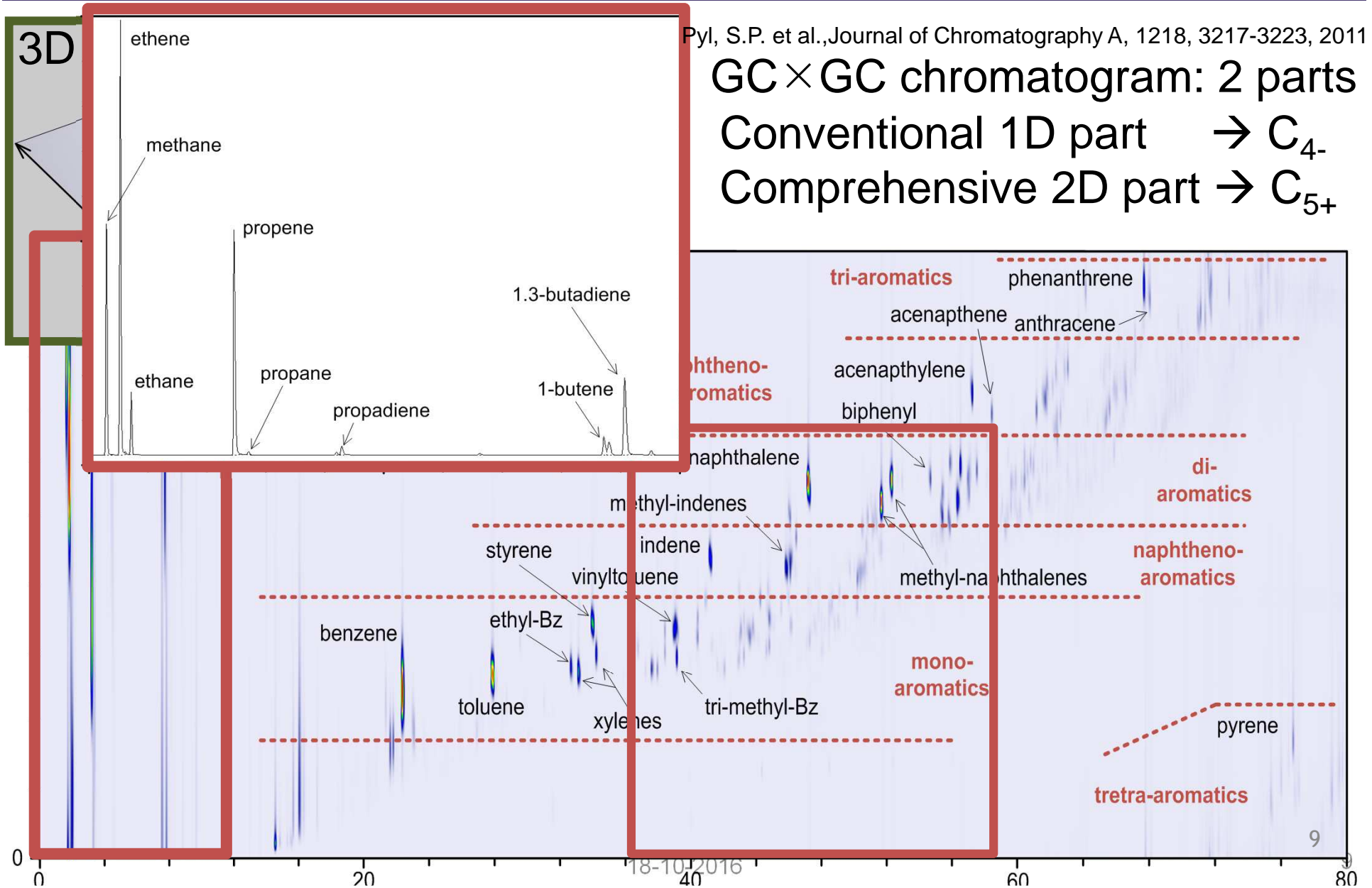
Outline

- Introduction
- Feedstock
- Kinetics
- Reactor
- Process
- Conclusions

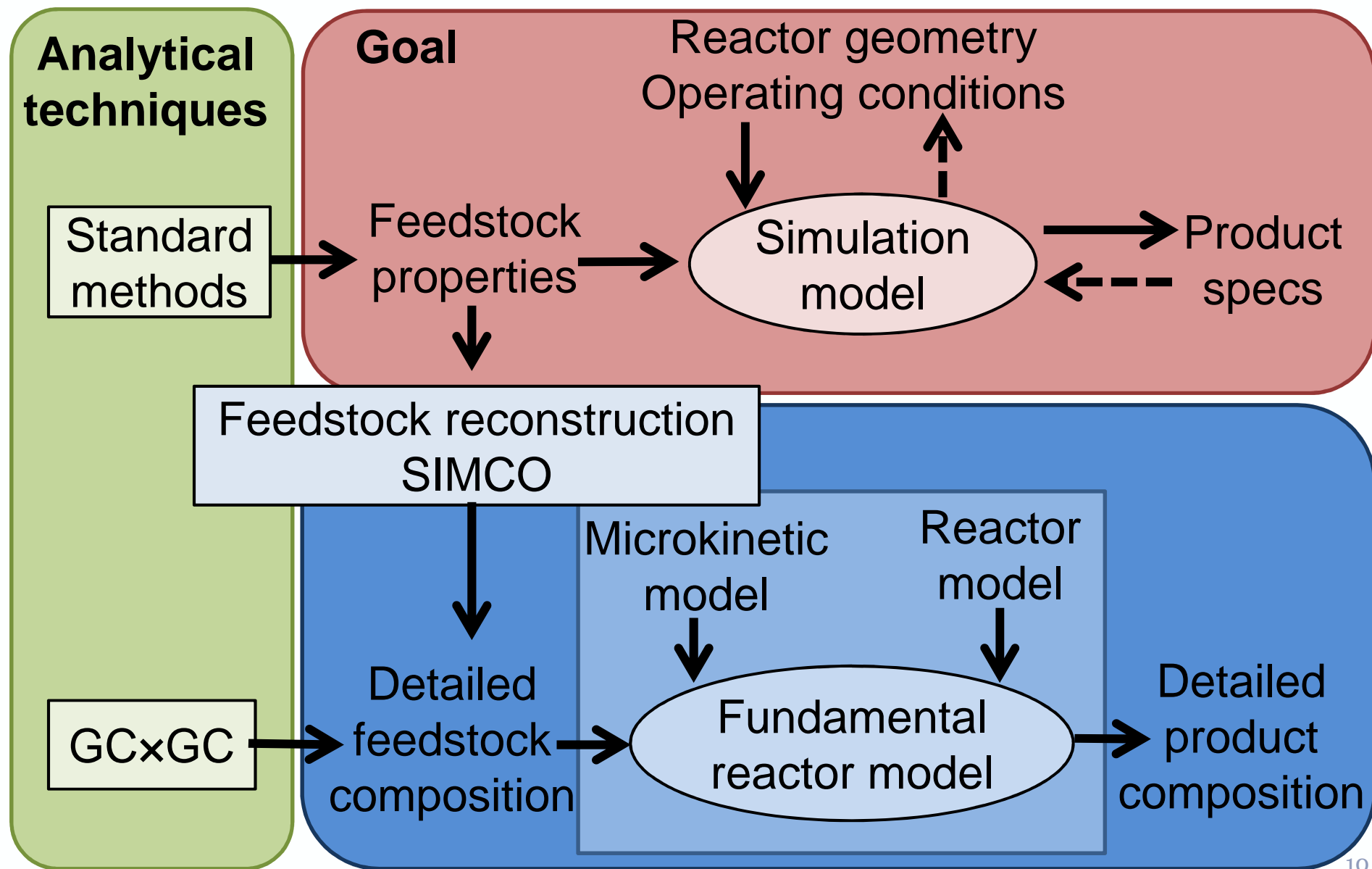
Outline

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On-line GCxGC



SIMCO: ANN or Shannon entropy



Maximization of Shannon Entropy

Feedstock properties

- Average molecular weight
- Elemental composition
- Specific density
- Global PINA analysis
- Boiling point data (e.g. D2887 simdist)
- Aromatic Sulfur

Shannon entropy reconstruction maximization



Detailed composition

- Species identity
- Mole or mass fractions

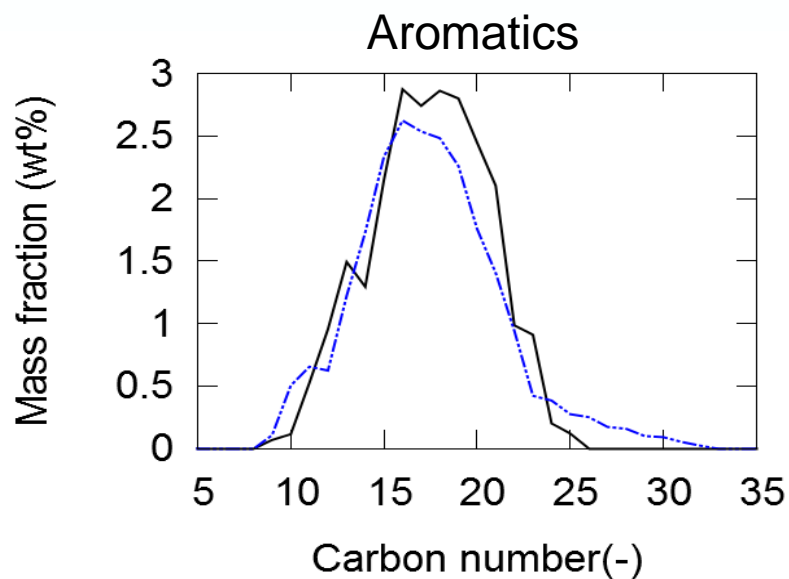
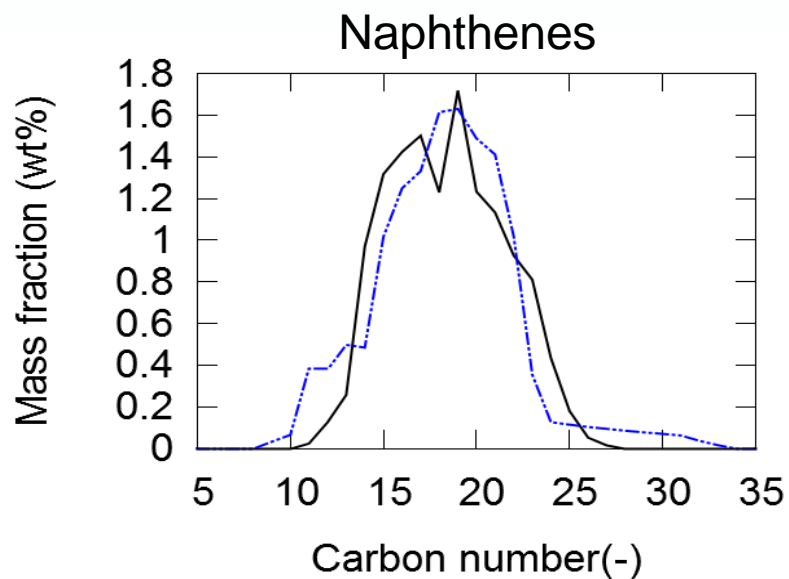
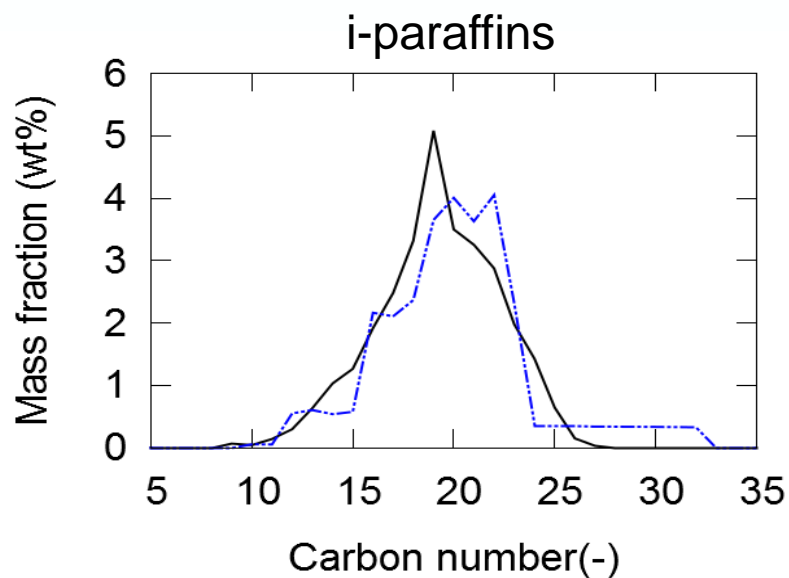
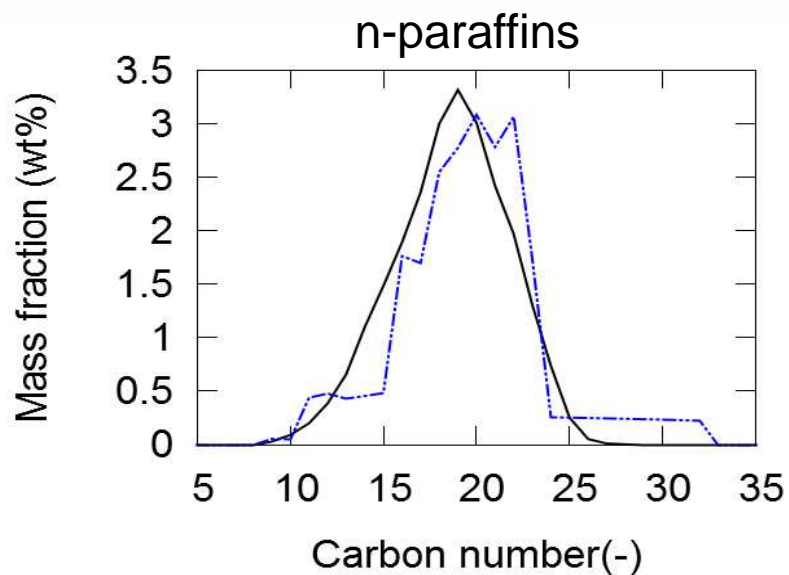


$$\text{MAX } S(y_i) = - \sum_{i=1}^{N_M} y_i \ln(y_i) \quad \text{with} \quad \sum_{i=1}^{N_M} y_i = 1$$

± 20 properties Constraints from mixing rules (example): More than 100 unknown

$$\frac{1}{d_{\text{exp}}} = \sum_{i=1}^{N_M} \frac{y_i M_{w_i}}{d_i \sum y_i M_{w_i}} \quad \text{mole fractions} \quad M_{w_{\text{exp}}} = \sum_{i=1}^{N_M} y_i M_{w_i}$$

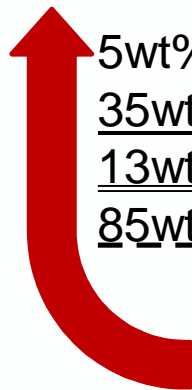
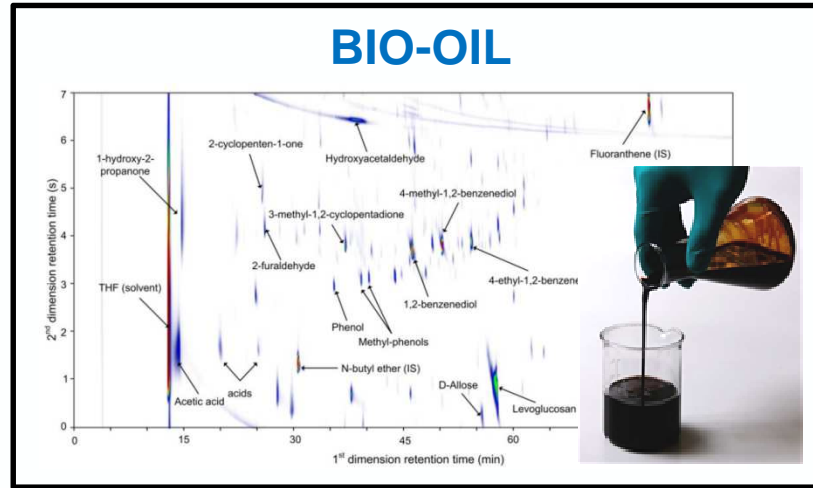
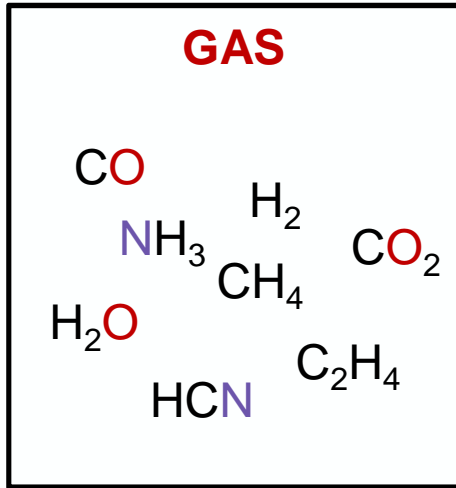
SIMCO results: Hydrocarbons



Outline

- Introduction
- Feedstock: renewables
- Kinetics
- Reactor
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- Conclusions

Thermochemical conversion of biomass

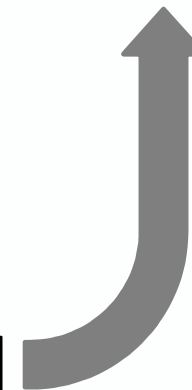


5wt%
35wt%
13wt%
85wt%

Torrefaction
Slow pyrolysis
Fast pyrolysis
Gasification



20wt%
30wt%
75wt%
5wt%

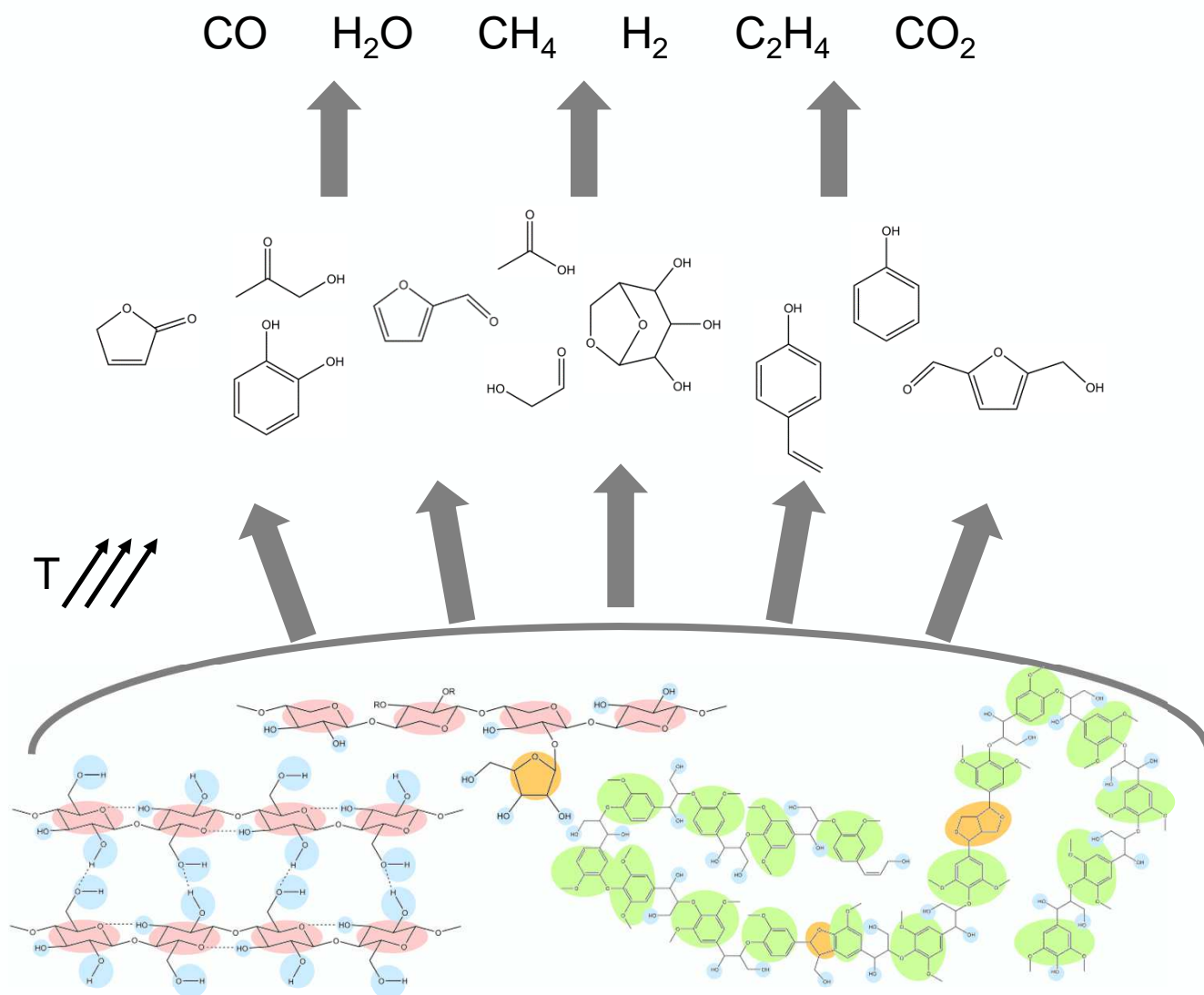


75wt%
35wt%
12wt%
10wt%



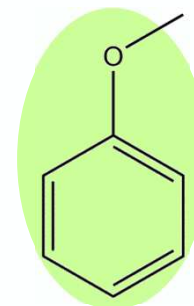
LIGNOCELLULOSIC BIOMASS

Model components for biomass pyrolysis



Study molecules with structural moieties found in biomass

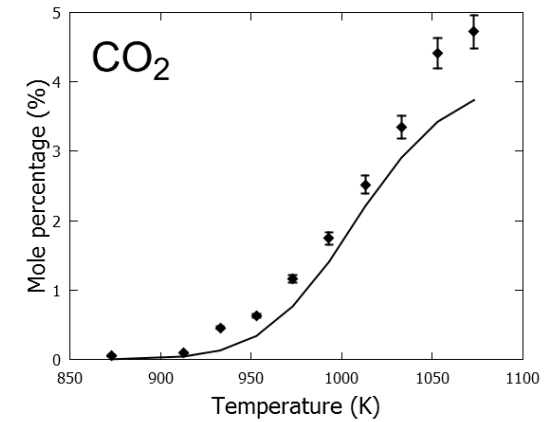
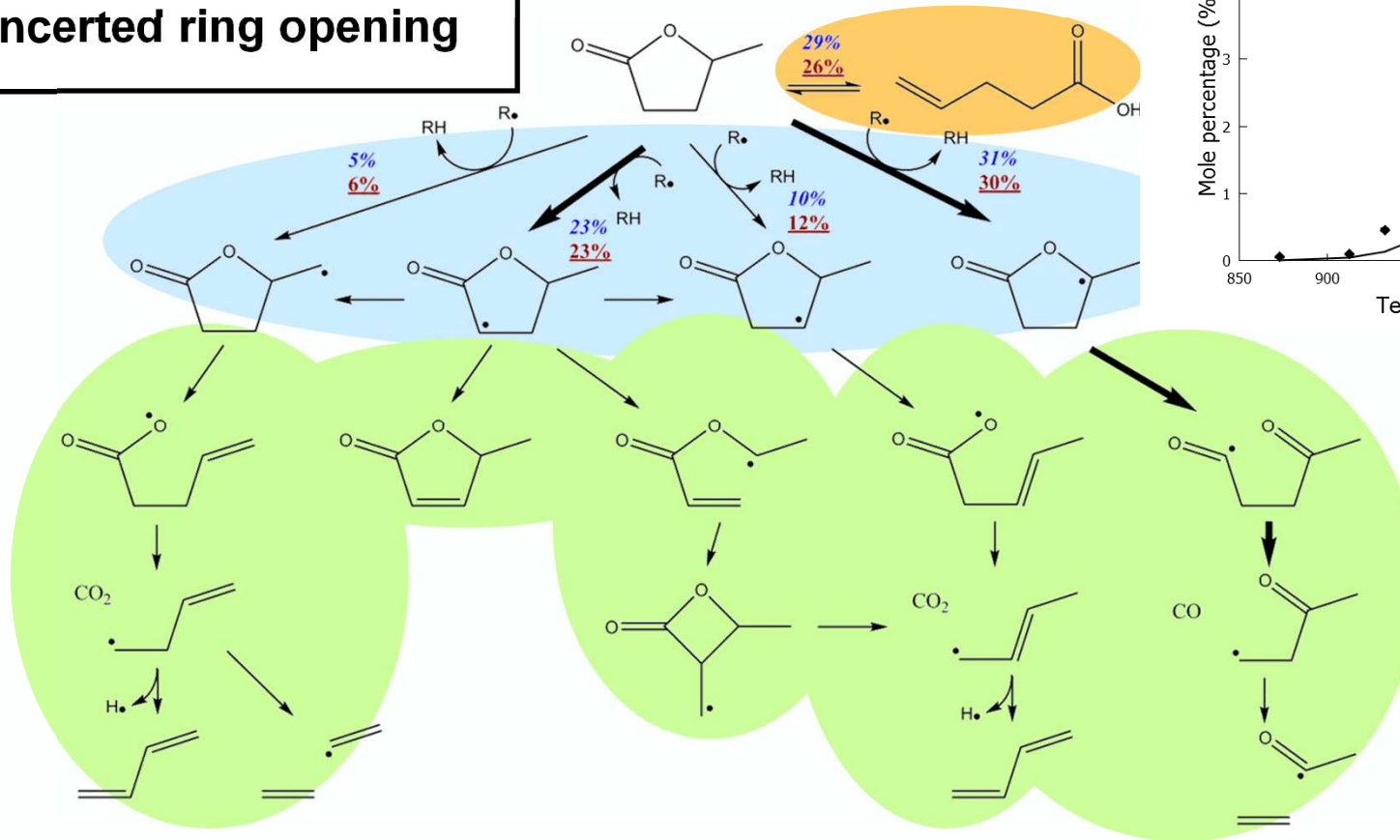
For example:



Reaction families

- 1) Scission
- 2) Hydrogen abstraction
- 3) β -scission/addition
- 4) Concerted ring opening

Gamma-Valerolactone (GVL) pyrolysis



De Bruycker, R. et al., *Combustion and Flame*, 164, 183-200, 2016

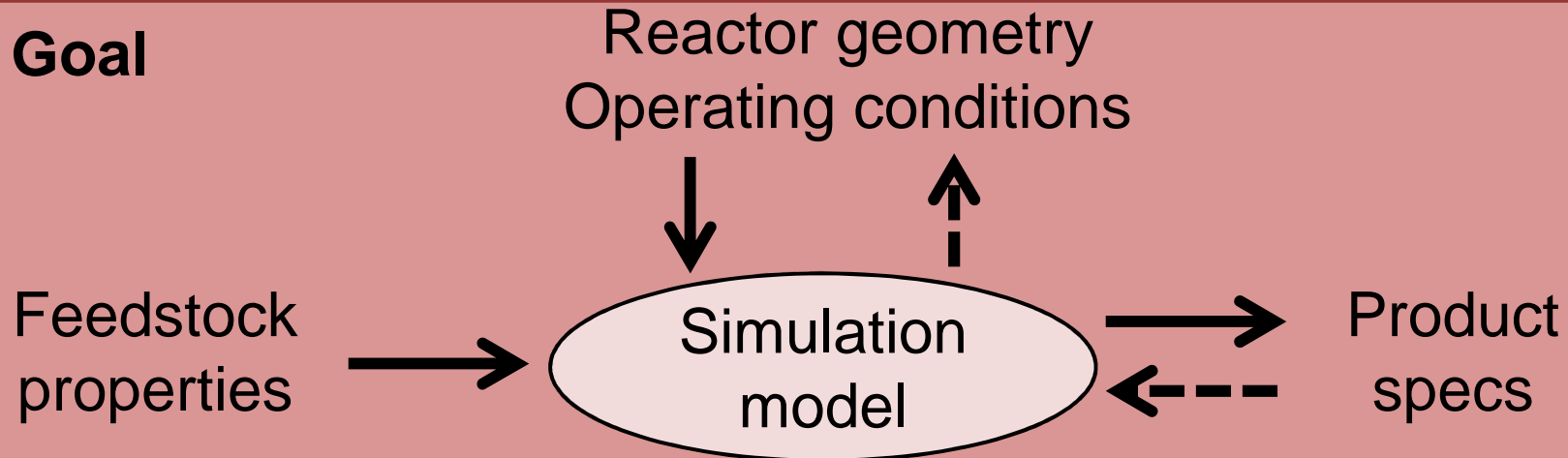
De Bruycker, R. et al., *Proceedings of the Combustion Institute*, 35, 515-523, 2015

Outline

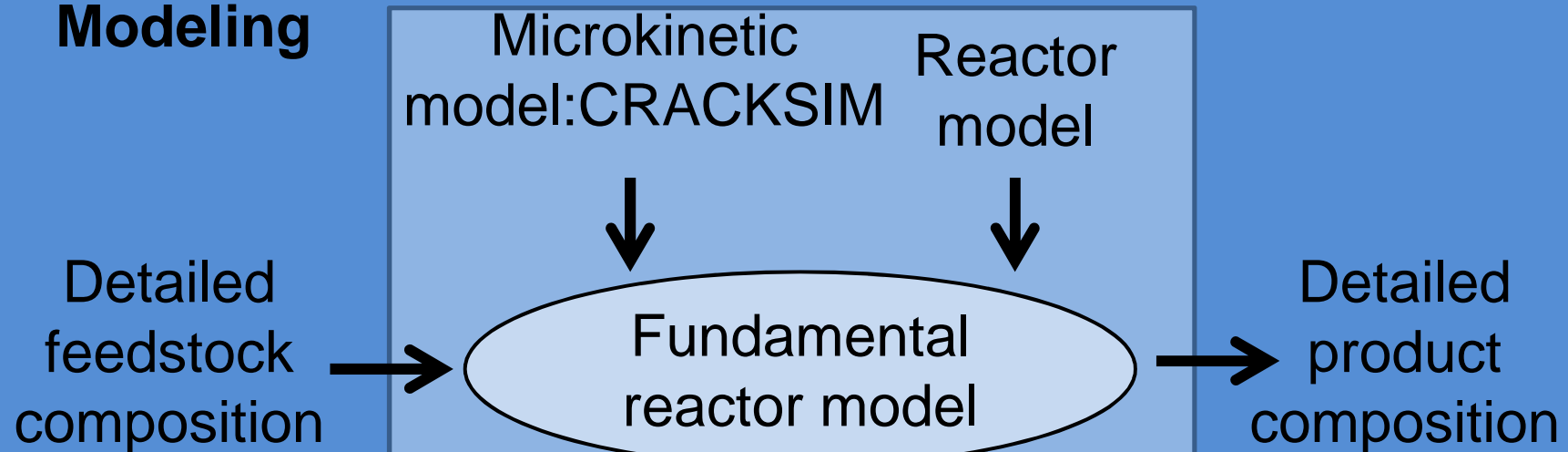
- Introduction
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- Kinetics
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CRACKSIM: steam cracking kinetics

Goal



Modeling

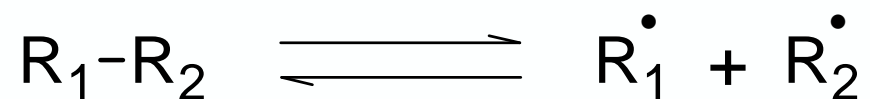


Outline

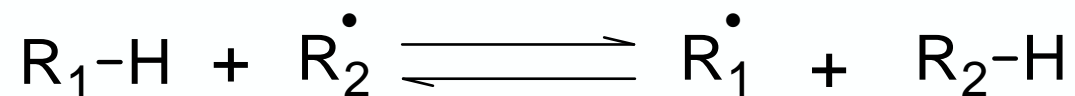
- Introduction
- Feedstock
- Kinetics: reaction network
- Reactor
- Process
- Conclusions

Families of elementary reactions

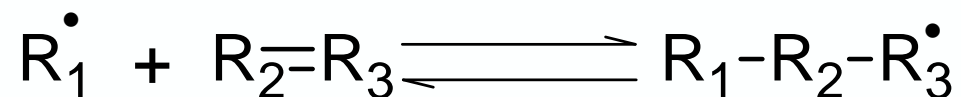
Bond dissociation and radical recombination



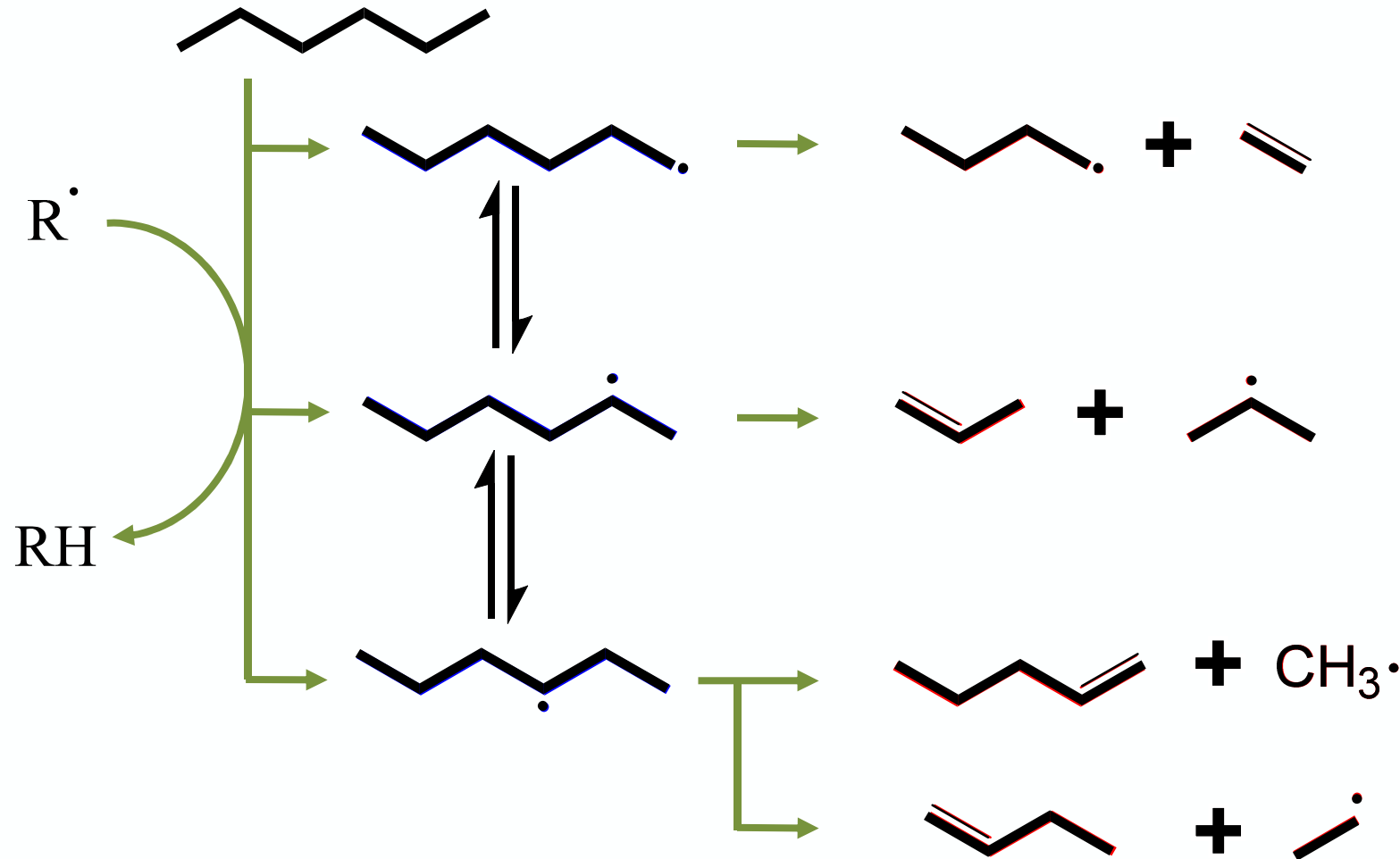
Hydrogen abstraction (inter- and intramolecular)



Radical addition and β -scission (inter- and intramolecular)



Decomposition scheme: n-hexane



β species

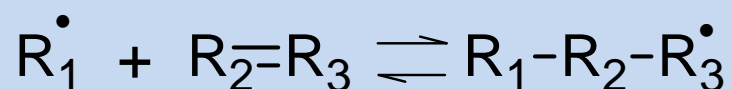
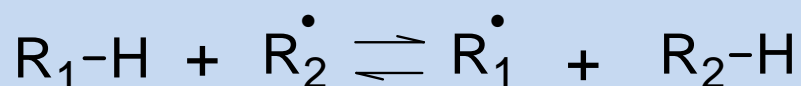
PSSA to μ radicals

μ and β networks: CRACKSIM

CRACKSIM

β network

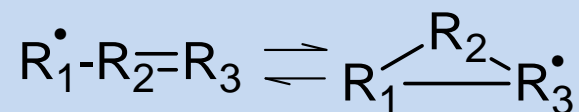
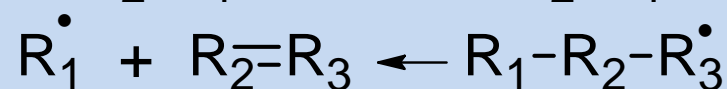
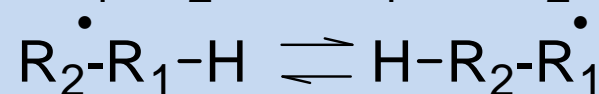
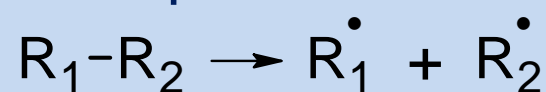
Bi- and monomolecular reactions for β radicals



1324 reversible reactions
51 molecules
43 radicals

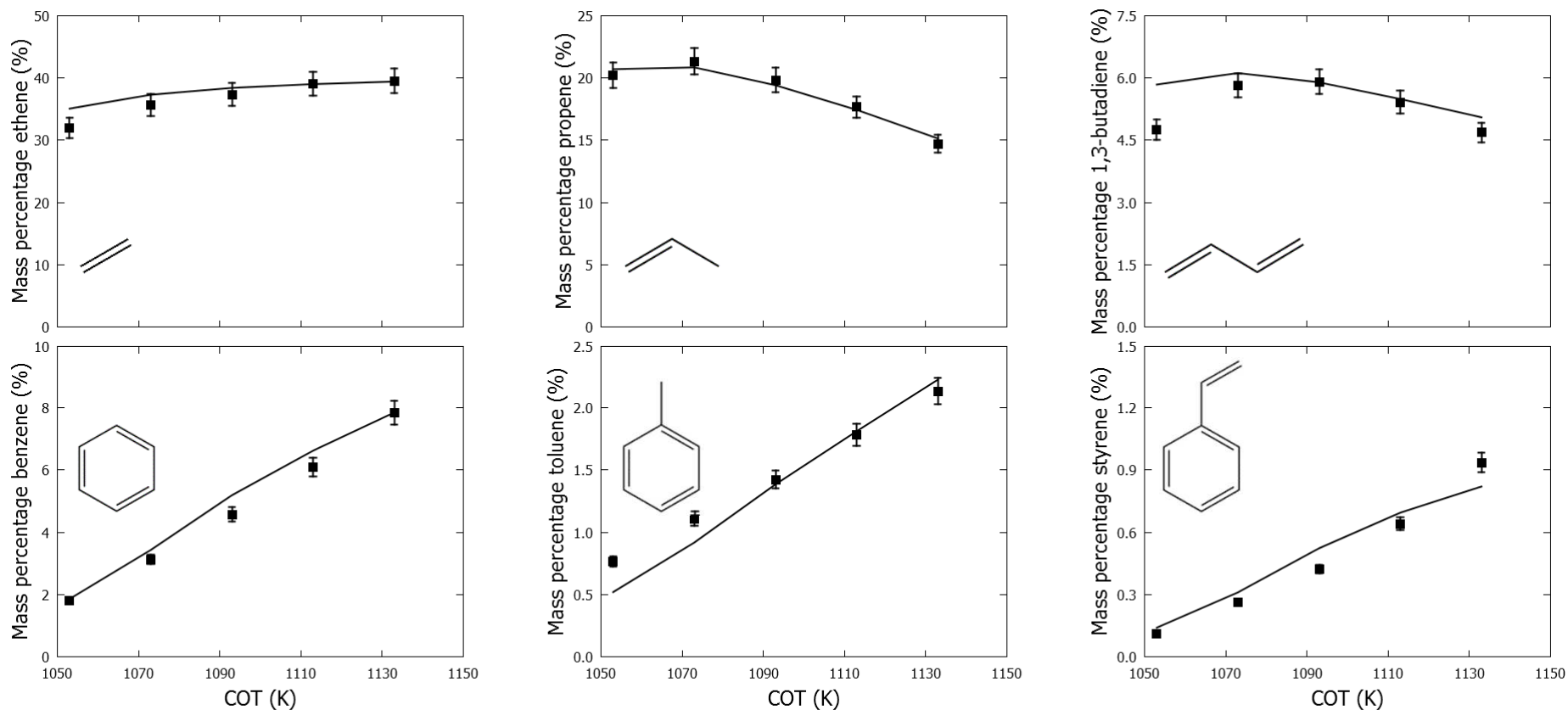
μ network

Monomolecular reactions for μ radicals



13584 schemes
676 molecules

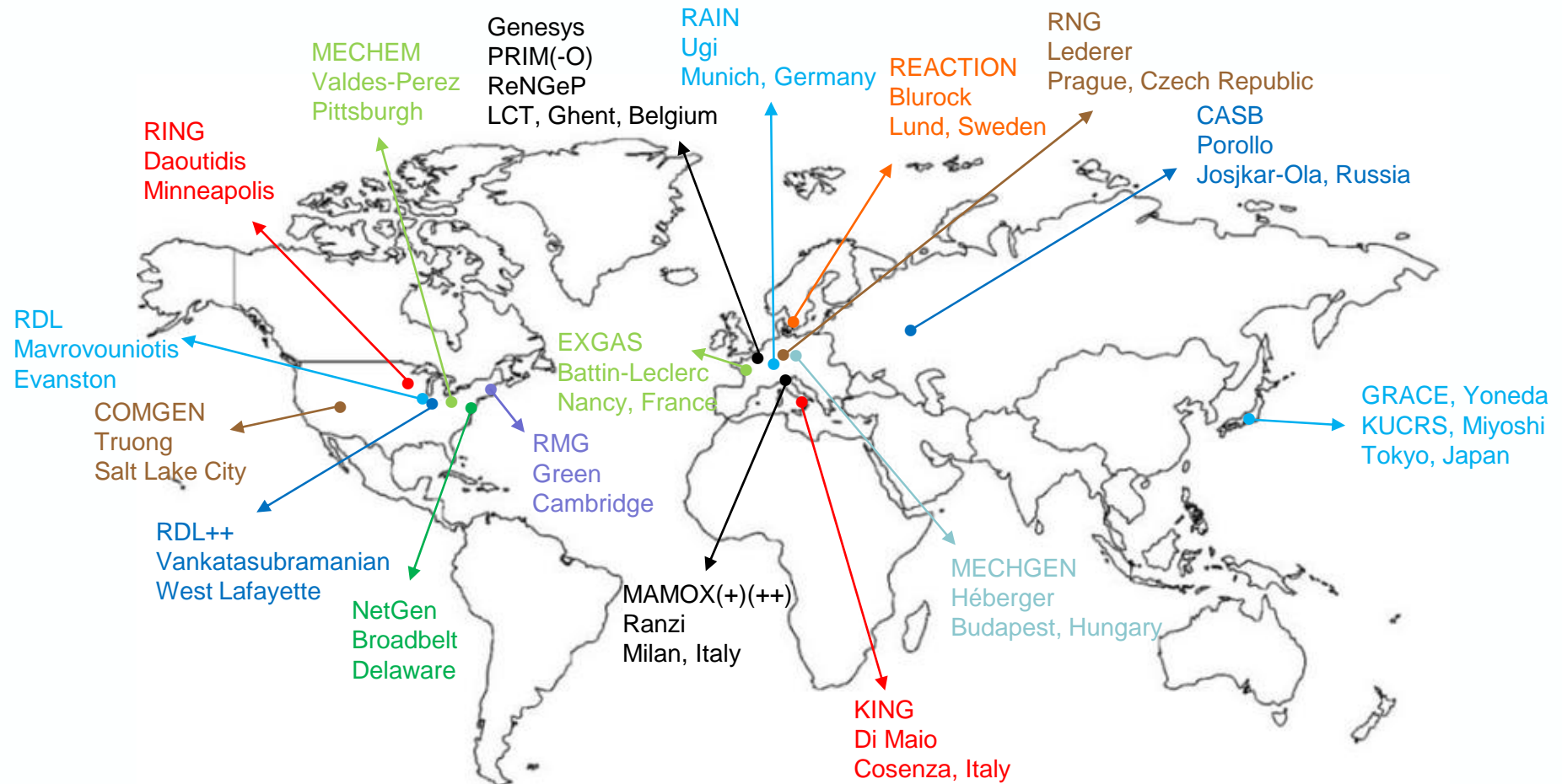
Validation



- **Experimental yields during steam cracking of bio-derived hydrocarbons**
 Feedstock composition: $MW_{\text{average}} = 230\text{g/mol}$ 51wt% normal alkanes – 49wt% branched alkanes
 $F_{\text{HC},0} = 0.04\text{ g/s}$, $F_{\text{H}_2\text{O},0} = 0.02\text{ g/s}$, $P = 0.17\text{ MPa}$

— calculated

Network generators



A new program for kinetic model construction

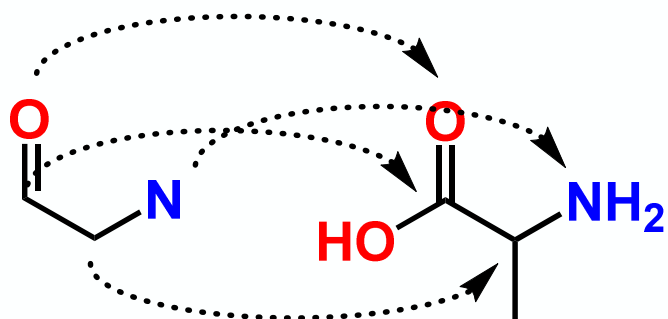
GENESYS - GENERation [of reacting] SYStems

Genesys: Kinetic model construction using chemo-informatics
Vandewiele, N.M.; Van Geem, K.M.; Reyniers, M.-F.; Marin, G.B.
Chemical Engineering Journal, 207-208, 526-538, 2012

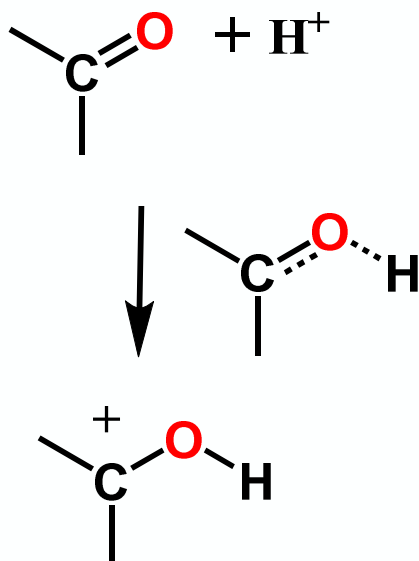
Van de Vijver, R. et al. International Journal of Chemical Kinetics, 47 (4), 199-231, 2015

Graph theory yields powerful algorithms

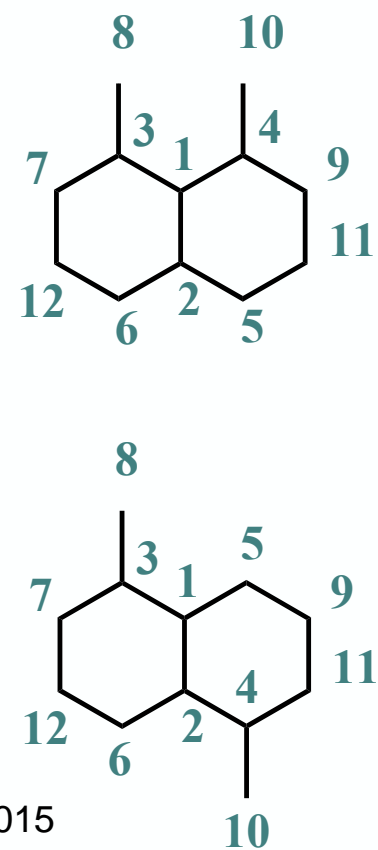
Pattern Recognition



Reactant -> product



Molecule Identifiers



"Kinetics of Chemical Reactions : Decoding Complexity"

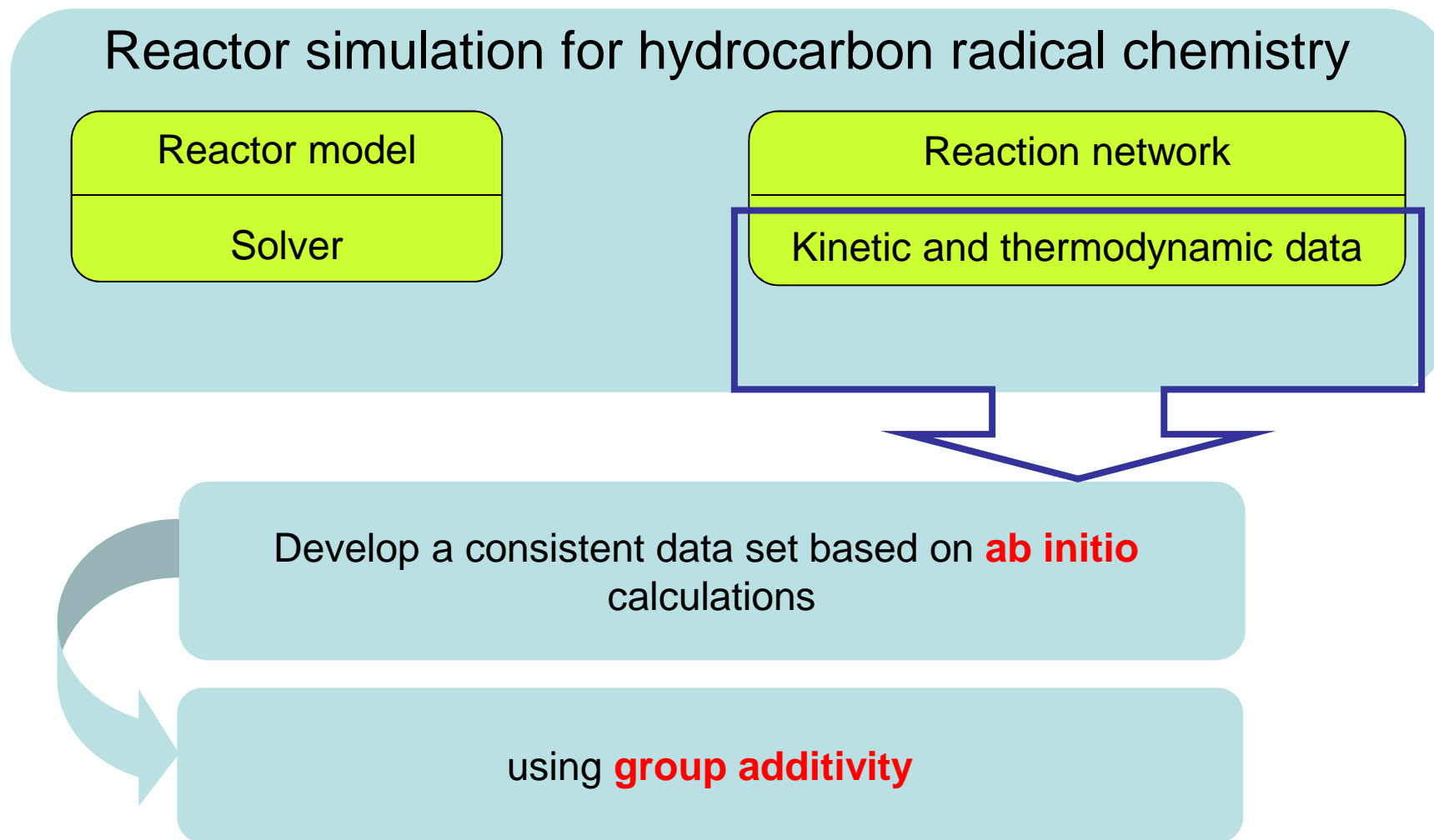
G.B. Marin and G.S. Yablonsky, Wiley-VCH Verlag, 446 pages, 2011

Vandewiele, N.M. et al., Journal of Computational Chemistry, 36 (3), 181-192, 2015

Outline

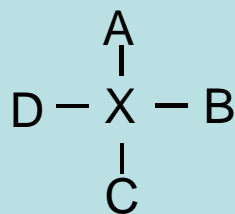
- Introduction
- Feedstock
- Kinetics: ab initio
- Reactor
- Process
- Conclusions

Objective: data base



Benson's group additive method

Benson group



Notation: X-(A)(B)(C)(D)

X: Central atom

Valence ≥ 2

{ C, C_d, O, CO, CCO, C•, C_d• }

A, B, C, D: Ligand

{ H, C, C_d, O, CO, CCO, C•, C_d•, O•, CO•, CCO• }

Group additivity for thermochemistry

$$f = \sum_i GAV_f(\text{group}_i) + \sum_j NNI_j$$



Group additive values
(**GAV**)



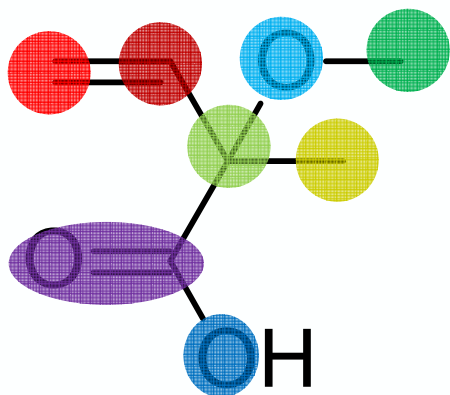
Corrections for non-nearest-neighbor interactions (**NNI**)

- ✓ hydrogen bonds
- ✓ gauche interactions
- ✓ other interactions

$$f = \Delta_f H^\circ, S_{\text{int}}^\circ, C_p^\circ \quad S_{\text{int}}^\circ = S^\circ + R \ln\left(\frac{\sigma}{n_{\text{opt}}}\right)$$

From small to large species with group additivity

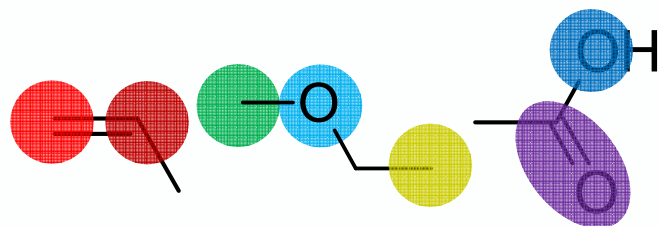
2-methoxy-2-methylbut-3-enoic acid



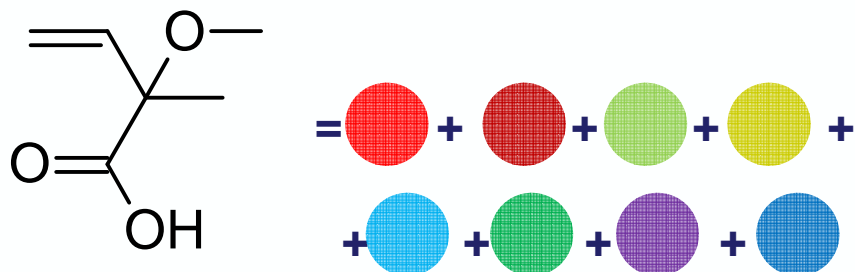
Atoms in large molecules

Group additivity

Atoms in small molecules with similar surroundings



Additivity



additive groups

- $C_d-(H)_2$
- $C_d-(C)(H)$
- $C-(C)(C_d)(O)(CO)$
- $O-(C)_2$
- $C-(O)(H)_3$
- $C-(C)(H)_3$
- $CO-(C)(O)$
- $O-(CO)(H)$

Outline

- Introduction
- Feedstock
- Kinetics: thermo first
- Reactor
- Processes
- Conclusions

Thermo e.g. for oxygenates: GAV data base

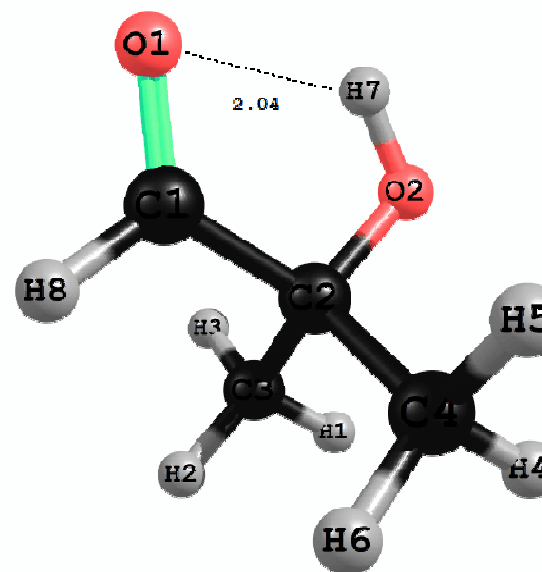
Database of thermodynamic data, $\Delta_f H^\circ$, S° and C_p° (300 K-1500 K)

- 450 oxygenate compounds
- CBS-QB3 methodology
- 1D-HR approximation for all internal rotors



- 157 GAVs using Benson's GA method
- 26 NNI corrections (mainly hydrogen bonds)
- 77 HBIs for the thermochemistry of radicals

2-hydroxy-2-methyl-propanal



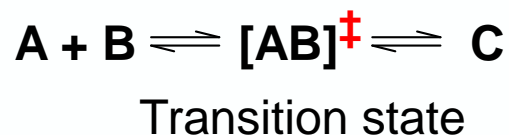
NNI8 Hbr_H-O-C-CO

Outline

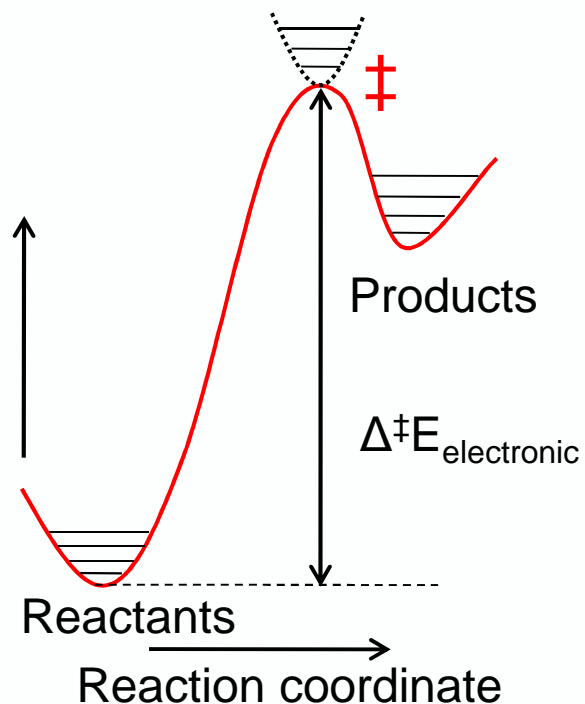
- Introduction
- Feedstock
- Kinetics: rate coefficients
- Reactor
- Process
- Conclusions

Kinetics: computational approach

Conventional Transition State Theory (high pressure limit)



$$k_\infty(T) = \kappa(T) \frac{k_B T}{h} \frac{q_\ddagger}{q_A q_B} V_m e^{-\frac{\Delta E_0}{RT}}$$



Electronic barrier ΔE_0

The CBS-QB3 ab initio method is used.

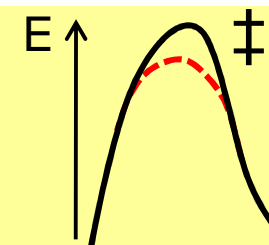
Partition functions q

- Ideal gas approximation
- Hindered Rotor (1D-HR)



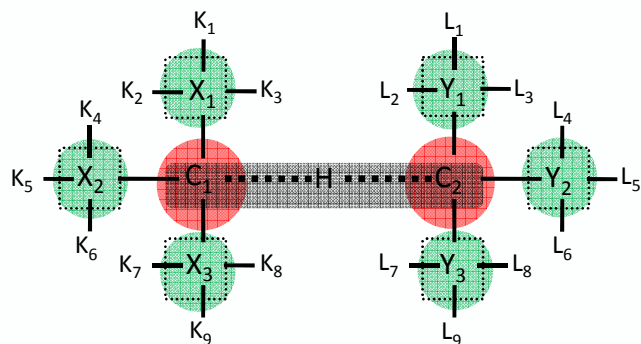
Tunneling coefficient κ

- Eckart



Group additivity for kinetics: data base of ΔGAV^o

Transition state for hydrogen abstraction



Arrhenius equation

$$k = Ae^{-\frac{E_a}{RT}}$$

$$k = \kappa_{Eckart} n_e k_{GA} = \kappa n_e \tilde{A} e^{-\frac{E_a}{RT}}$$

Number of single events

$$n_e = \frac{n_{opt,\ddagger}}{\prod_j n_{opt,j}} \frac{\prod_j \sigma_j}{\sigma_{\ddagger}}$$

Group additivity for Arrhenius parameters

$$E_a(T) = E_{a,ref}(T) + \underbrace{\sum_{i=1}^2 \Delta GAV_{E_a}^o(C_i)}_{\text{Primary}} + \underbrace{\sum_{i=1}^3 \Delta GAV_{E_a}^o(X_i)}_{\text{Secondary}} + \underbrace{\sum_{i=1}^3 \Delta GAV_{E_a}^o(Y_i)}_{\text{Tertiary}} + \Delta E_{E_a,res}^o$$

$$\log \tilde{A}(T) = \log \tilde{A}_{ref}(T) + \underbrace{\sum_{i=1}^2 \Delta GAV_{\log \tilde{A}}^o(C_i)}_{\text{Primary}} + \underbrace{\sum_{i=1}^3 \Delta GAV_{\log \tilde{A}}^o(X_i)}_{\text{Secondary}} + \underbrace{\sum_{i=1}^3 \Delta GAV_{\log \tilde{A}}^o(Y_i)}_{\text{Tertiary}} + \Delta \log \tilde{A}_{res}^o$$

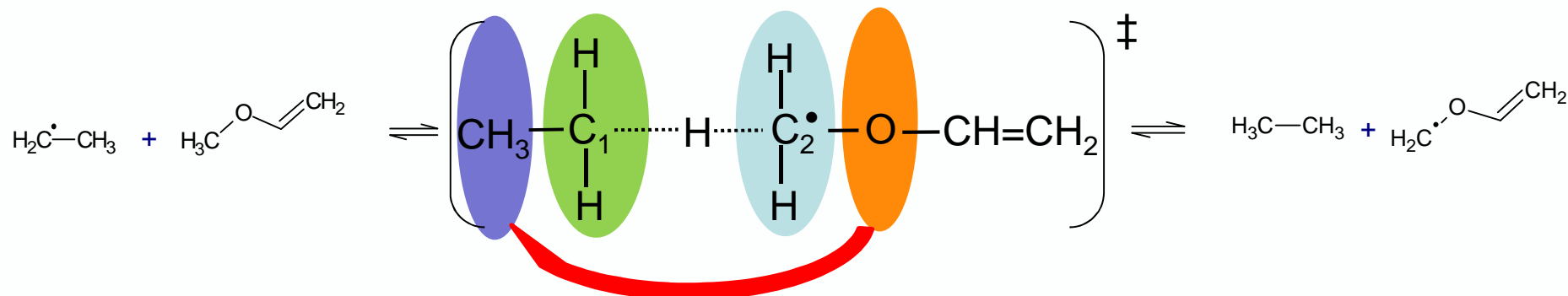
Proposed by Saeys et al. for activation energies (*AIChE J.* **2004**, 50 (2), 426-444.)

Extended by Sabbe et al. for pre-exponential factors (*Phys. Chem. Chem. Phys.* **2010**, 12, 1278-1298)

Kinetics: data base of ΔGAV°

Hydrogen abstraction (*ethyl* + *ethenyl methylether*)

Paraskevas, P. et al., Journal of Physical Chemistry A, 119 (27), 6961-6980, 2015

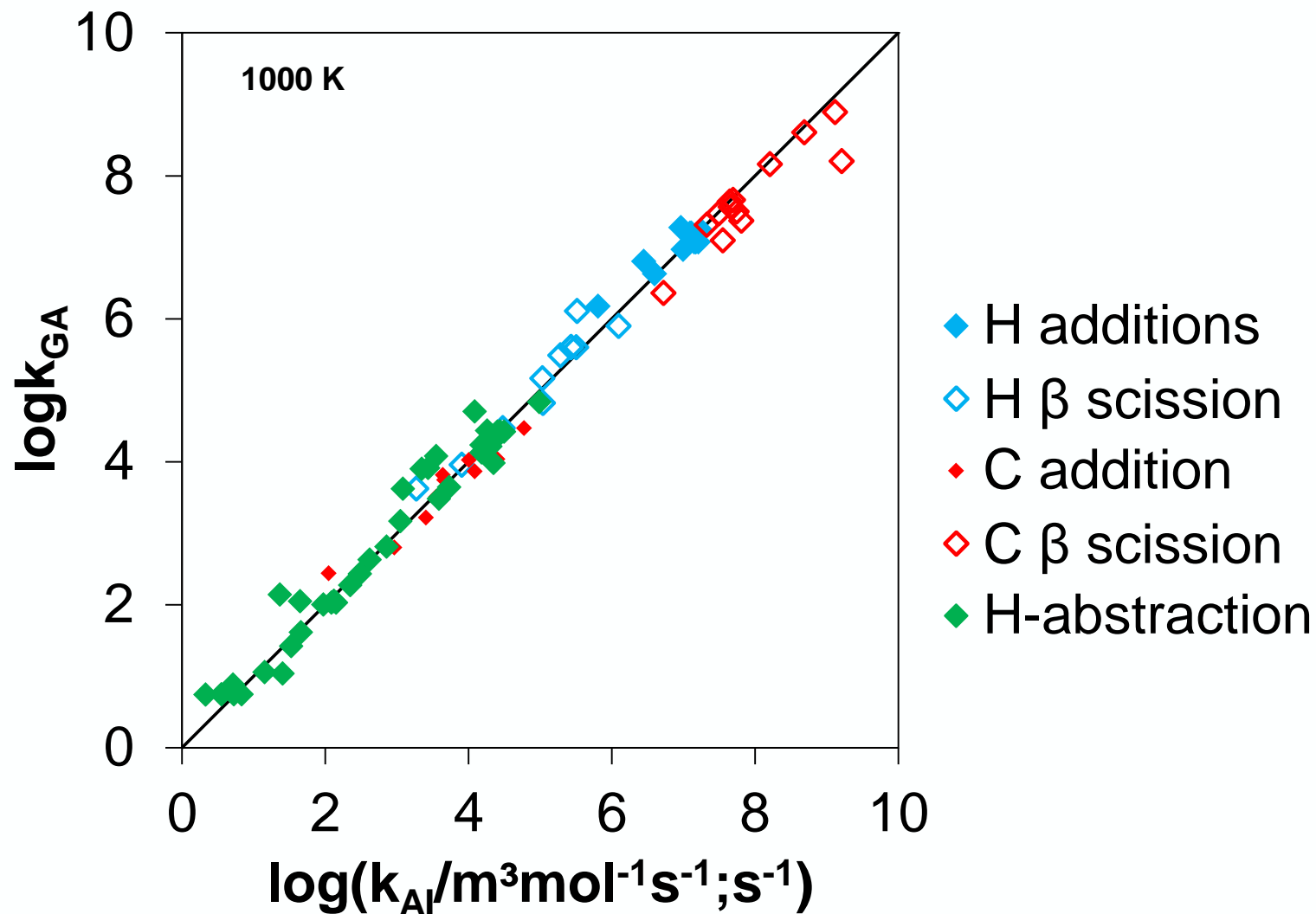


$$E_a(T) = E_{a,\text{ref}}(T) + \Delta GAV_{E_a}^\circ(C_1) + \Delta GAV_{E_a}^\circ(C_2) + \Delta GAV_{E_a}^\circ(X_1) + \Delta GAV_{E_a}^\circ(Y_1) + \Delta E_{a,\text{res}}$$

$\text{CH}_3 + \text{CH}_4$	$\text{C}_1\text{-(C)(H)}_2$	$\text{C}_2\text{-(O)(H)}_2$	$\text{C-(C}_1\text{)(H)}_3$	$\text{O-(C}_2\text{)(C}_d\text{)}$	\int_{H}^0
69.7 kJmol ⁻¹	+4.7 kJmol ⁻¹	-18.2 kJmol ⁻¹	+0 kJmol ⁻¹	+6.8 kJmol ⁻¹	-0.4 kJmol ⁻¹
$E_{a,\text{GA}} = 62.6 \text{ kJmol}^{-1}$			$E_{a,\text{ab initio}} = 62.0 \text{ kJmol}^{-1}$		

$\text{CH}_3 + \text{CH}_4$	$\text{C}_1\text{-(C)(H)}_2$	$\text{C}_2\text{-(O)(H)}_2$	$\text{C-(C}_1\text{)(H)}_3$	$\text{O-(C}_2\text{)(C}_d\text{)}$	\int_{H}^0
5.268	-0.866	-0.512	+0	+0.480	-0.053
$\log(A_{\text{GA}}/\text{m}^3 \text{ mol}^{-1} \text{ s}^{-1}) = 5.095$			$\log A_{\text{ab initio}} = 5.203$		

Kinetics: validation of group additivity



Sabbe et al. *ChemPhysChem* **2008**, 9 (1), 124-140

Sabbe et al. *ChemPhysChem*, **2010**, 11(1), 195-210

Sabbe et al. *PhysChemChemPhys*, **2010**, 12 (6), 1278-1298

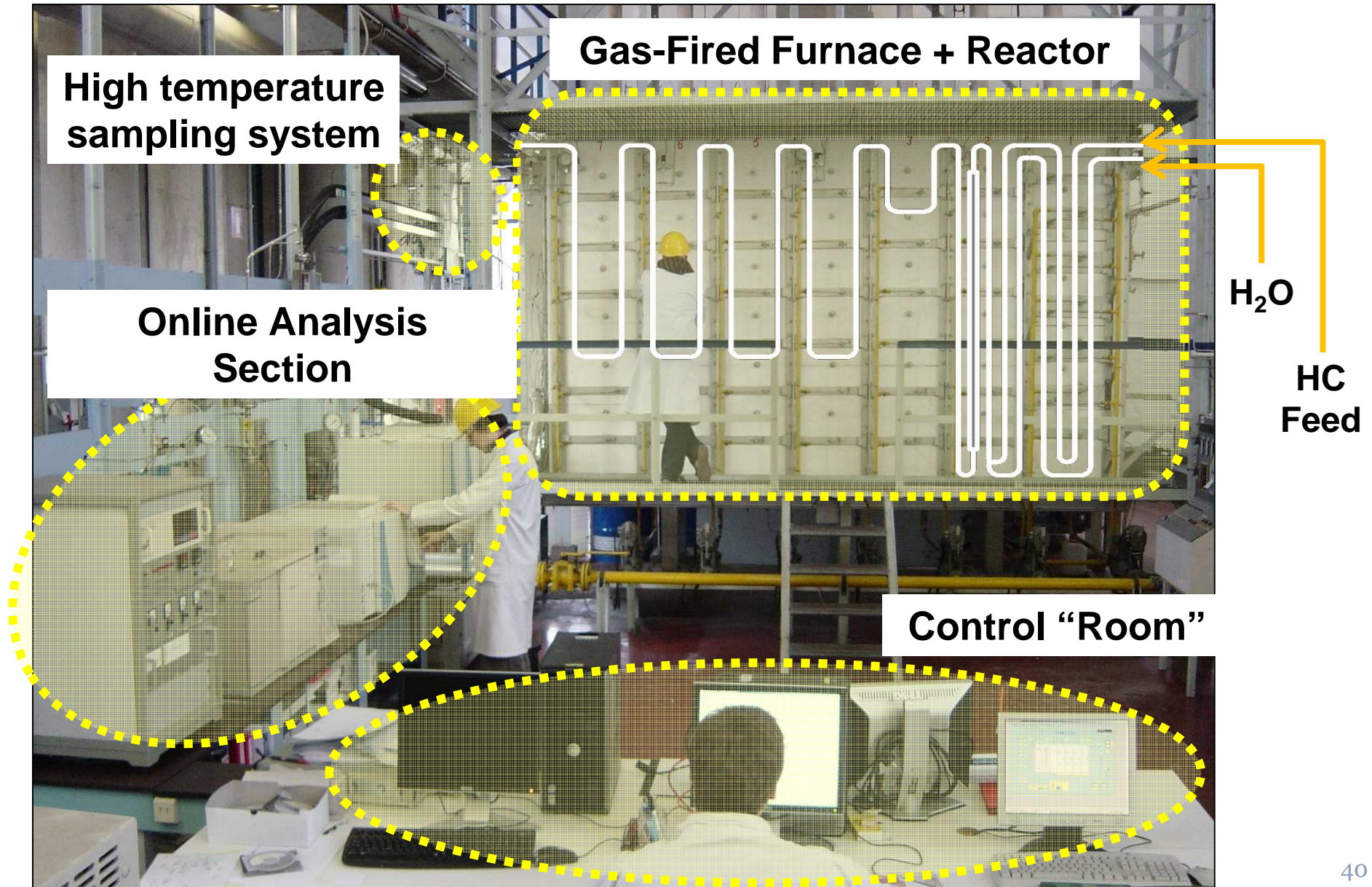
Outline

- Introduction
- Feedstock
- Kinetics
- **Reactor**
- Process
- Conclusions

Outline

- Introduction
- Feedstock
- Kinetics
- Reactor : pilot scale
- Process
- Conclusions

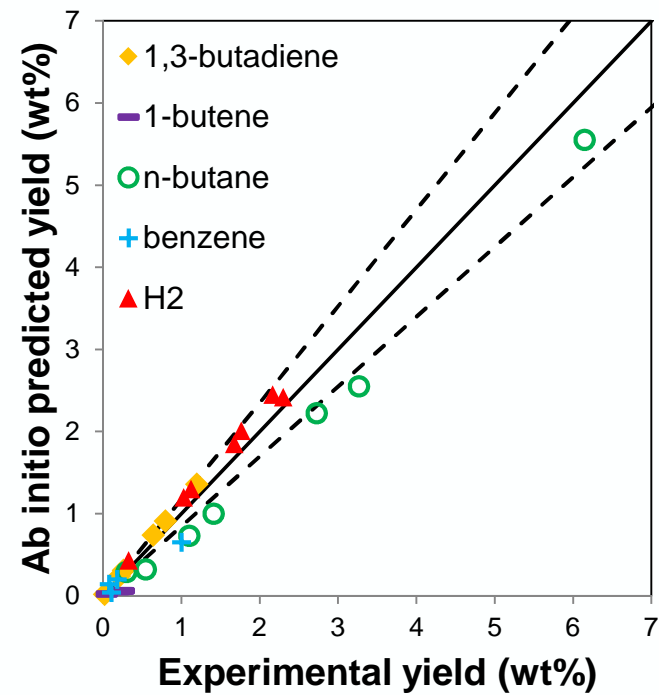
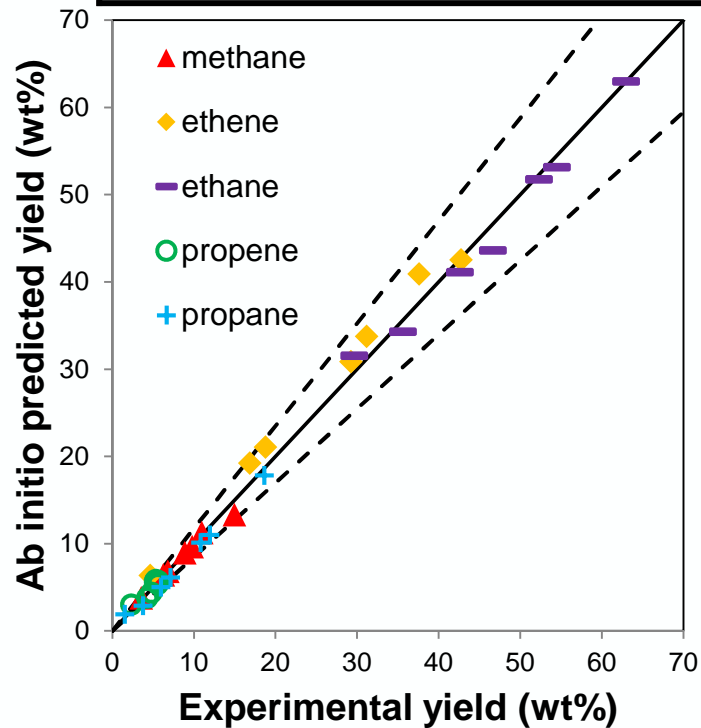
Steam Cracking Pilot Plant



Pilot results: $C_1/C_2/C_3/C_4$

Process conditions	
Feed	3 wt% C_1 67 wt% C_2 22 wt% C_3 8 wt% C_4
COT	1005-1119 K
COP	0.152-0.157 MPa
Steam dilution	0 kg/kg

without a single adjusted parameter






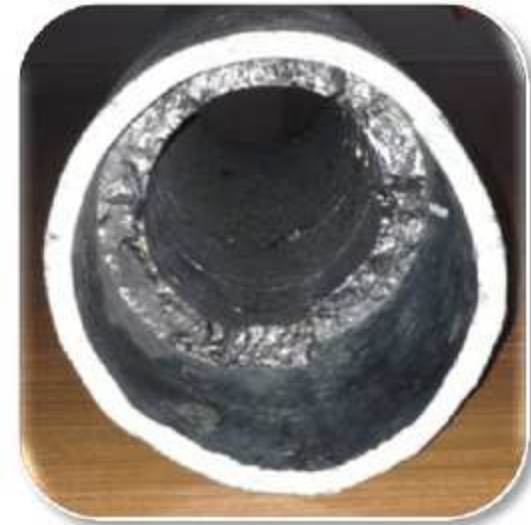
Outline

- Introduction
- Feedstock
- Kinetics
- **Reactor: 3D alternatives**
- Process
- Conclusions

Coke formation

Deposition of a carbon layer on the reactor surface

-  Thermal efficiency
-  Product selectivity
-  Decoking procedures



[Muñoz, 2013]

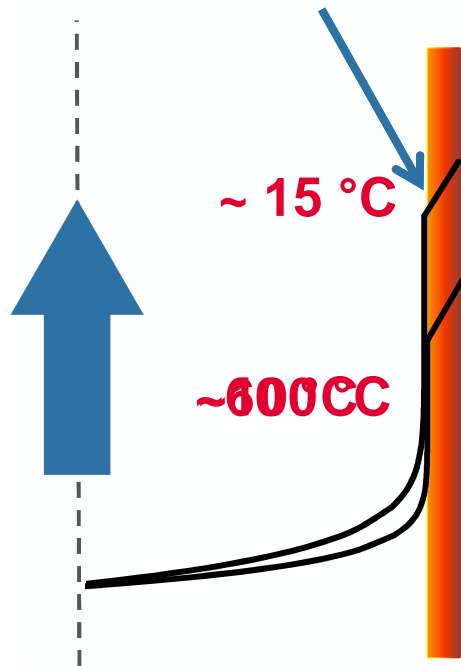
Estimated annual cost to industry: \$ 2 billion

Mitigation by

- Feed additives
- Metallurgy & surface technology
- 3D reactor technology

Coke formation: 3D reactor technologies

Cokes formed here
 $T \uparrow \rightarrow$ coking rate $\uparrow\uparrow$

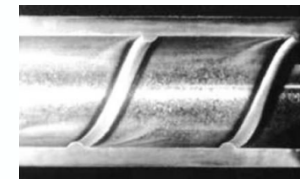


Reduce convective heat resistance

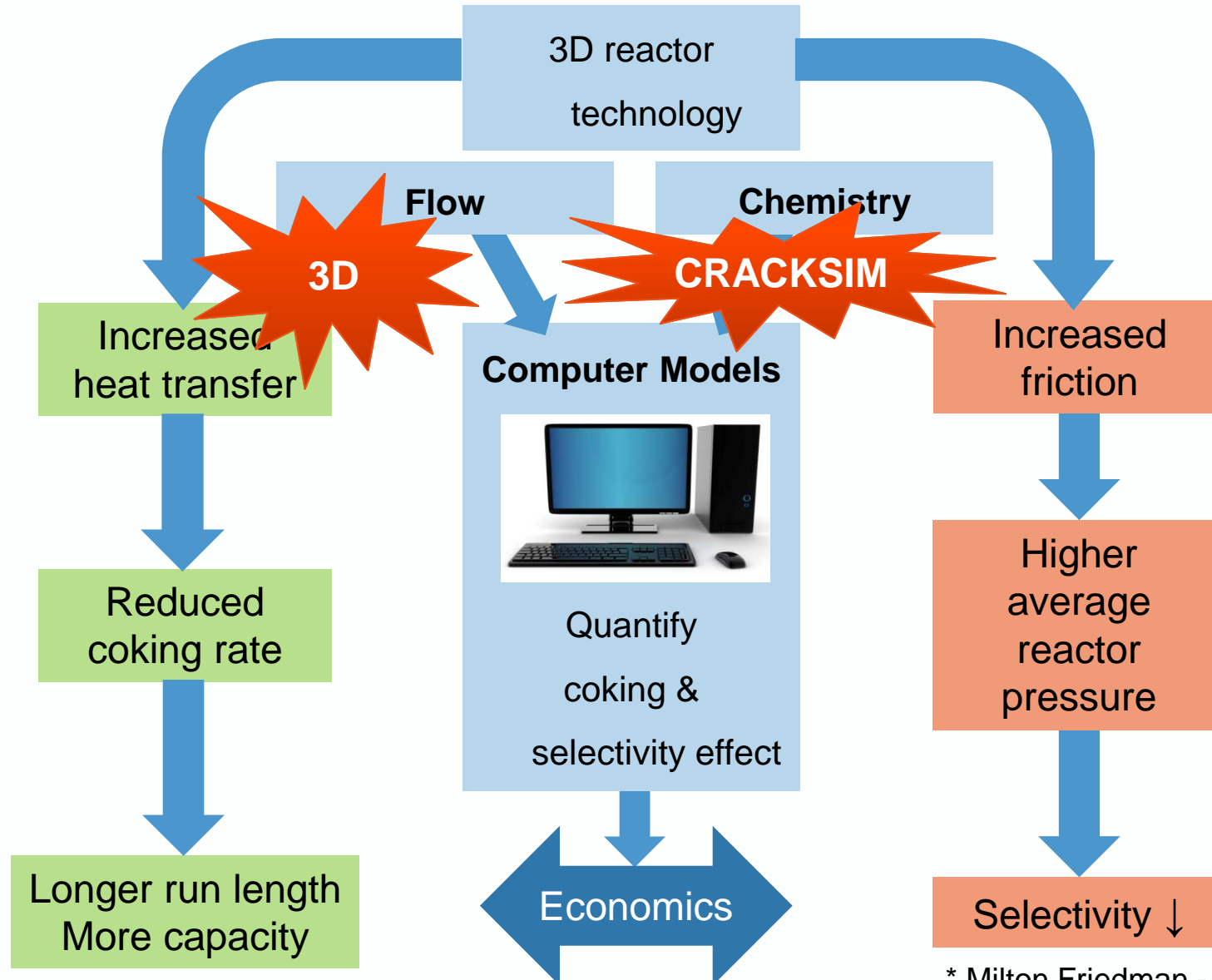
Increase surface area



Better mixing



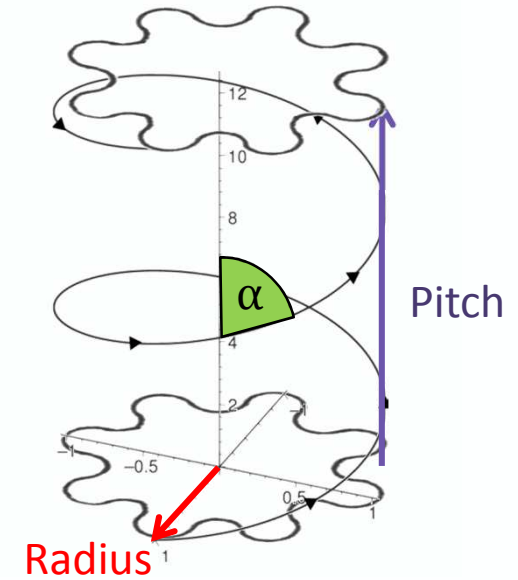
"There ain't no such thing as a free lunch"



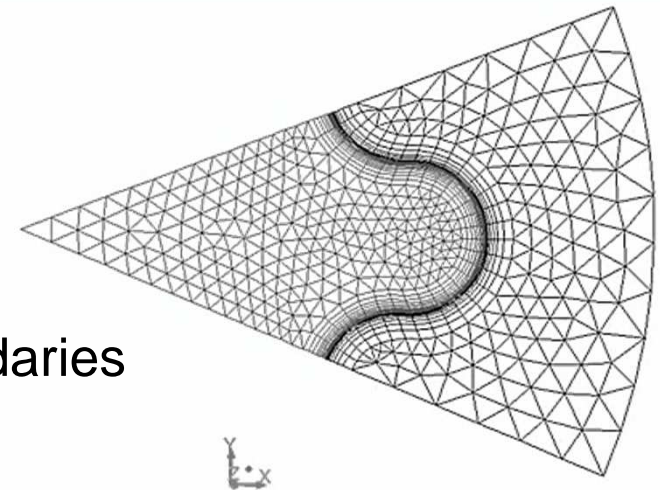
Helicoidal finned tubes



Radiant coils in Borealis Furnace, KBR



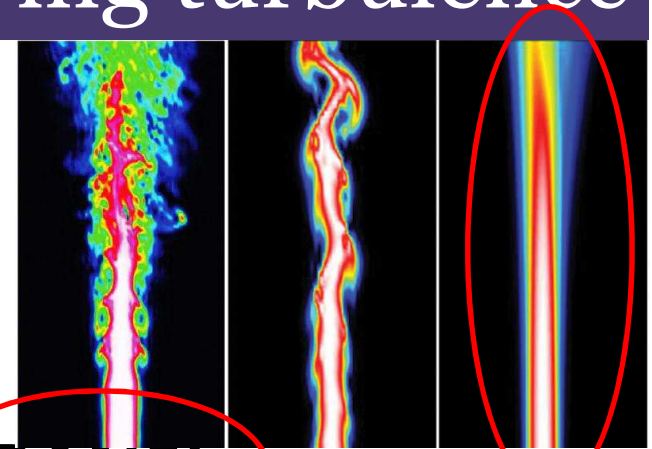
Computational domain: 1 fin with periodic boundaries



Outline

- Introduction
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- **Reactor : CFD models**
- Process
- Conclusions

Resolving turbulence



Reynolds-Averaged Navier-Stokes (RANS)

Single model for all scales, additional equations to provide closures

Large Eddy Simulation (LES)

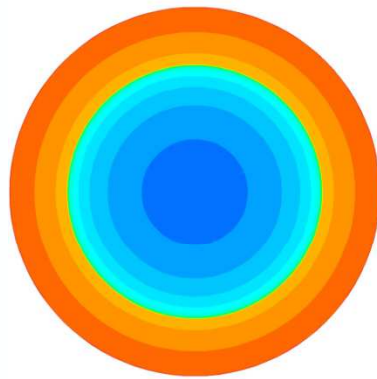
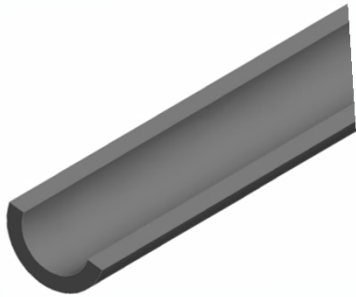
Resolve relevant energy containing scales, model the smaller energy dissipating eddies

Direct Numerical Solution (DNS)

Fully resolve all time and length scales

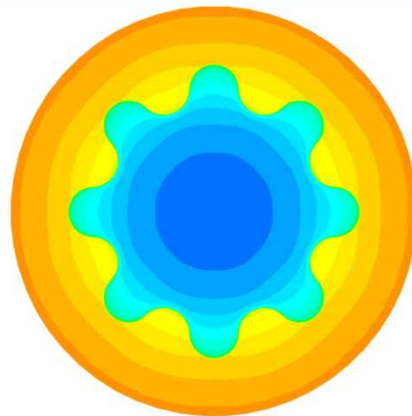
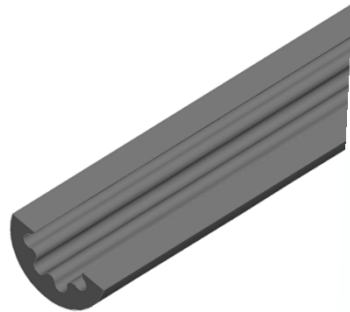
Radial temperature profiles

Bare



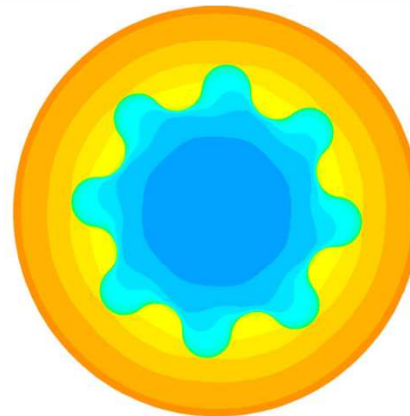
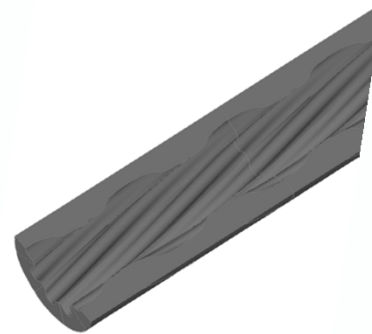
1170

Straight



1203

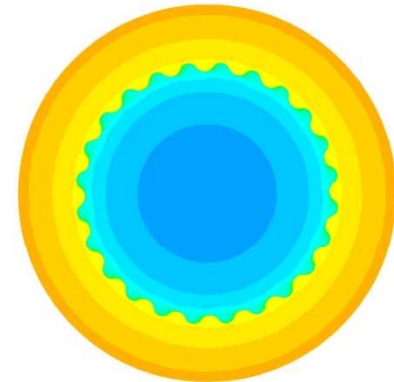
Helix



1268

SmallFins

Optimized

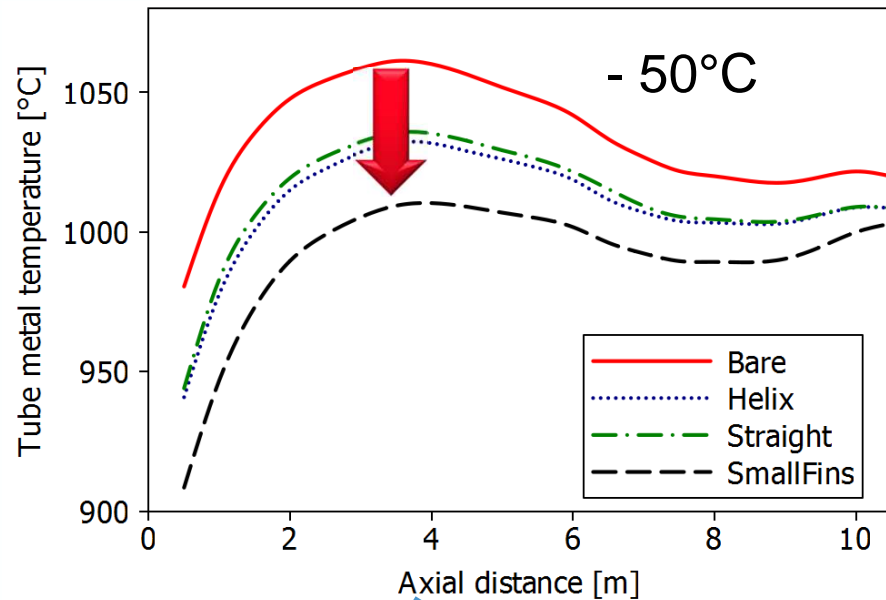


1300

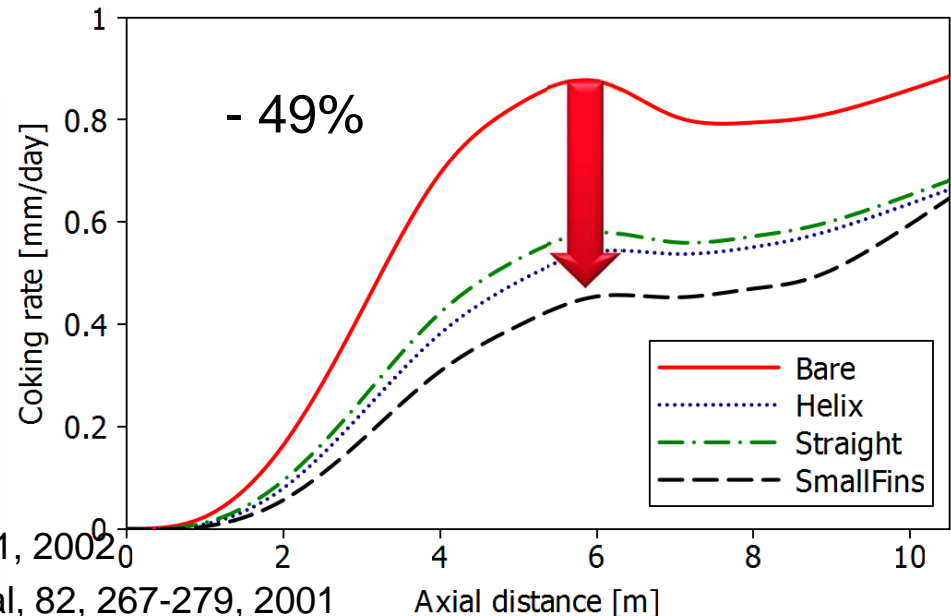
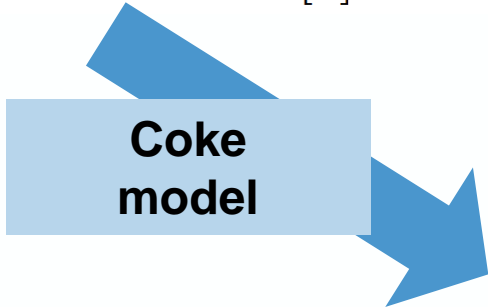


More uniform gas temperature
Lower metal temperature

Axial wall temperature and coking profile



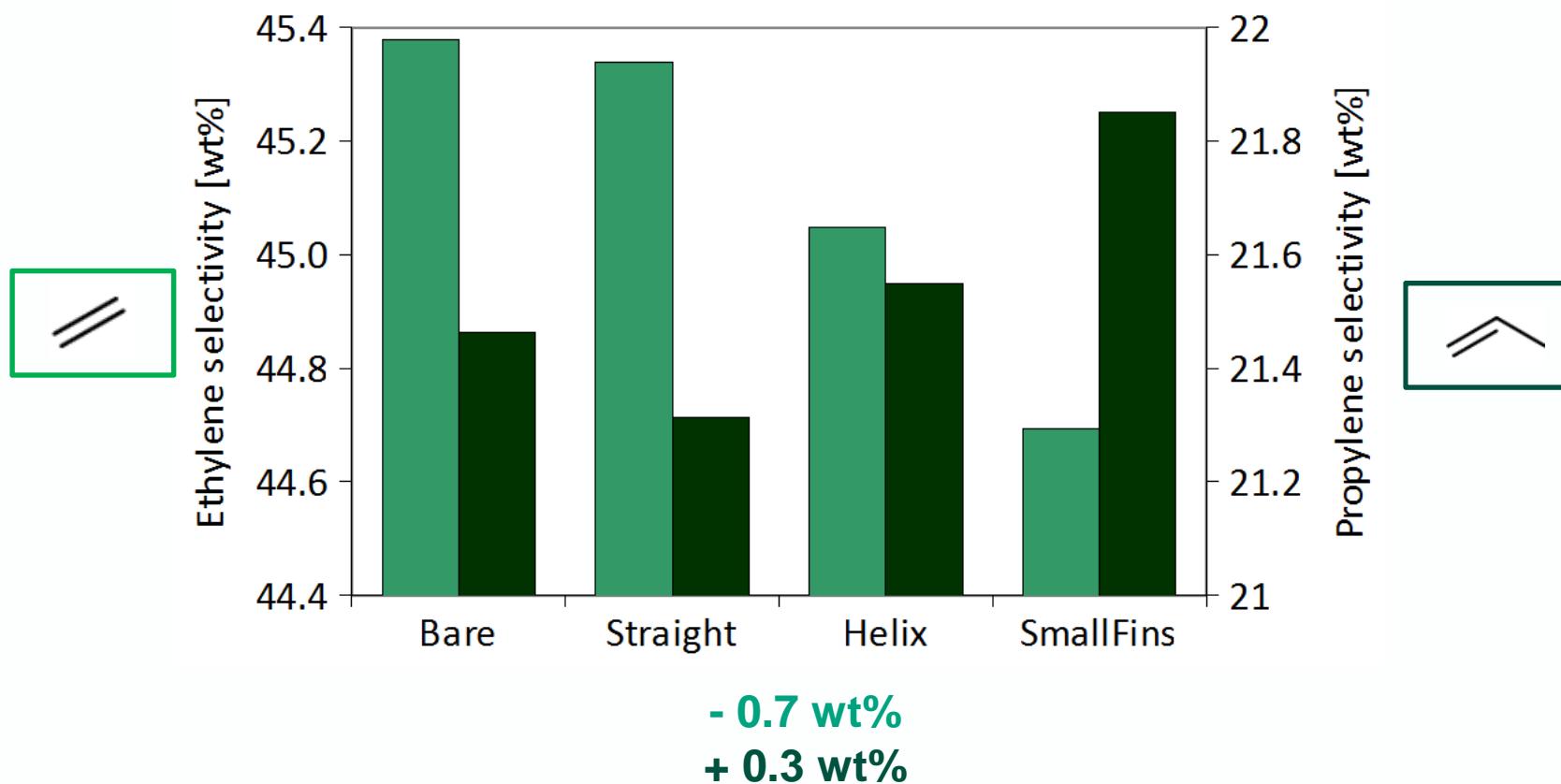
Cracking reaction model
26 components
13 radical species
212 elementary reactions



S. Wauters and G.B. Marin, IEC Research, 41, 2379-2391, 2002

S. Wauters and G.B. Marin; Chemical Engineering Journal, 82, 267-279, 2001

Effect on start of run yields

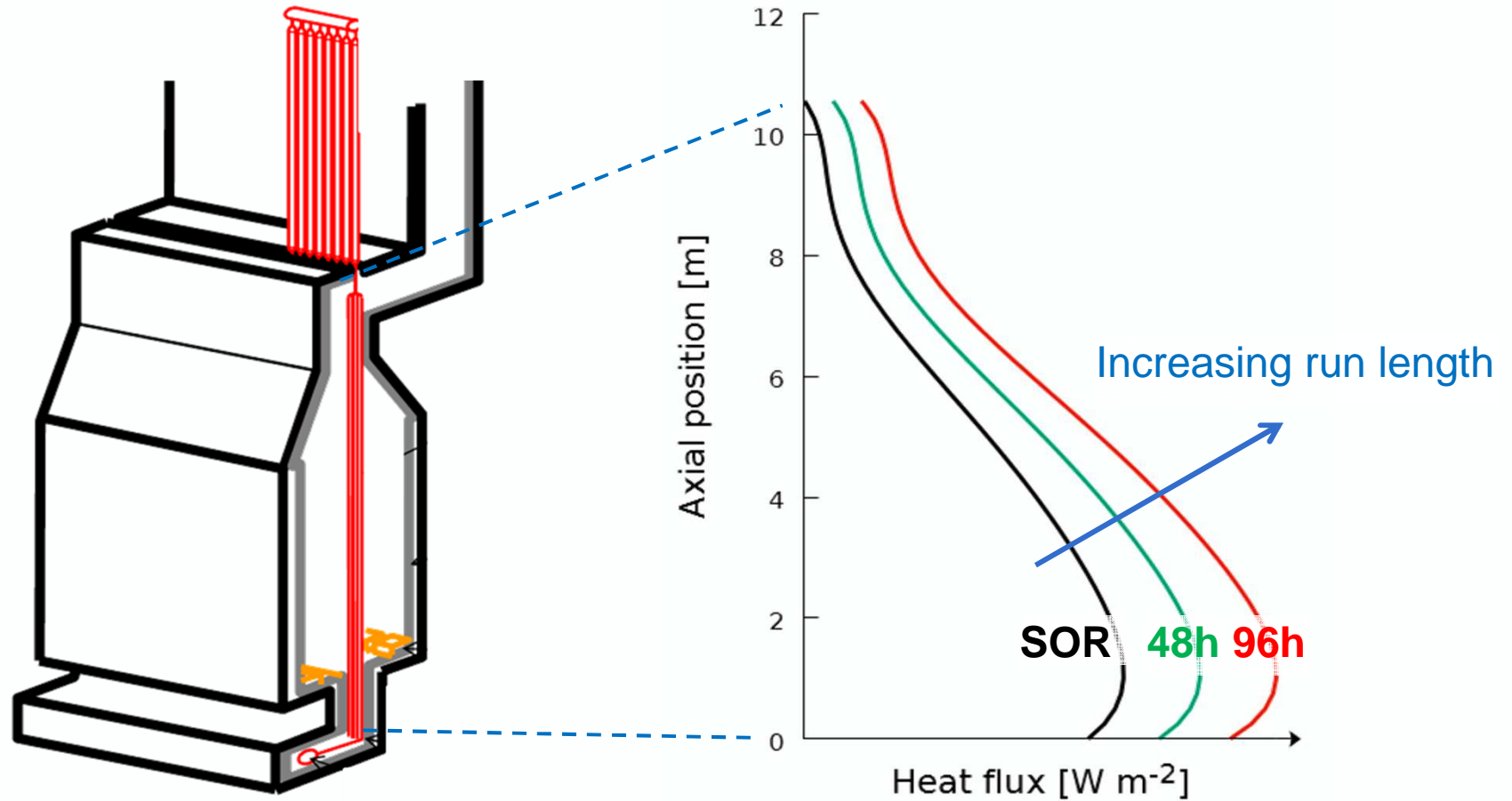


Radical reaction model
26 components
13 radical species
212 elementary reactions

Outline

- Introduction
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- Reactor: "run length"
- Process
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Run length simulation

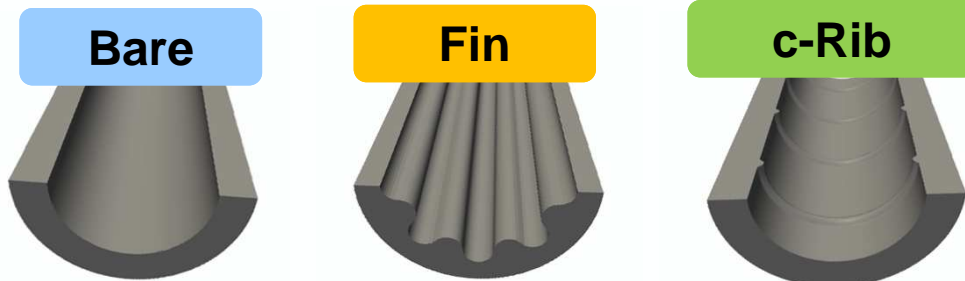
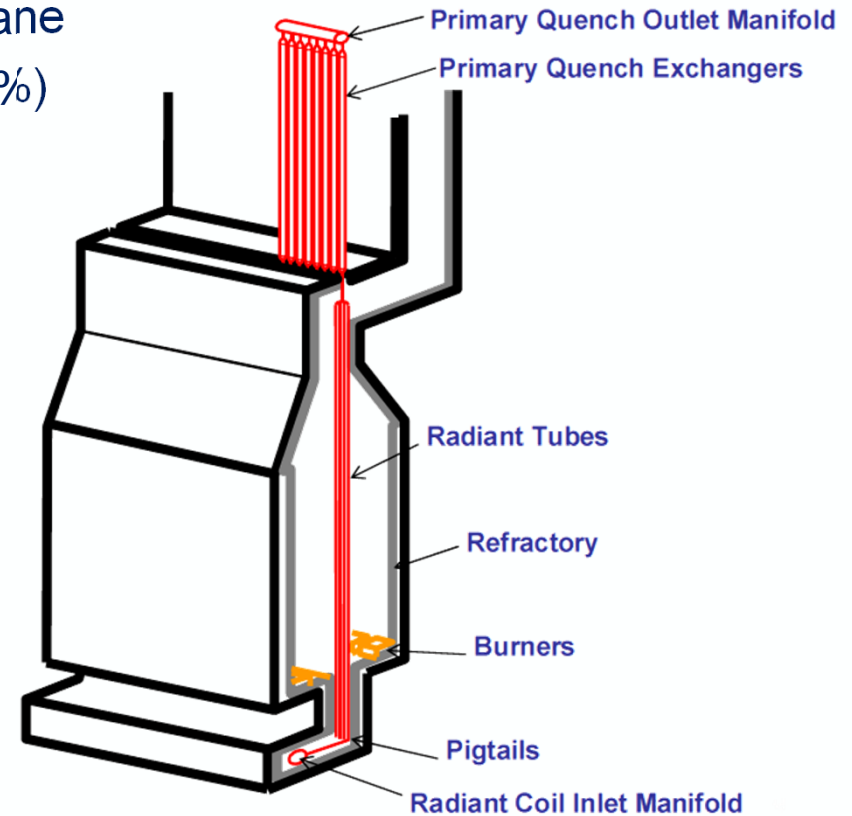


Millisecond propane cracker

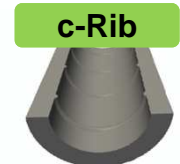
- Feedstock 118.5 kg/h propane
- Propane conversion 80.15 % ($\pm 0.05\%$)
- Steam dilution 0.326 kg/kg
- CIT 903.7 °C
- COP 170 kPa

Different geometries simulated

- Same reactor volume
- Same axial length
- Same minimal wall thickness

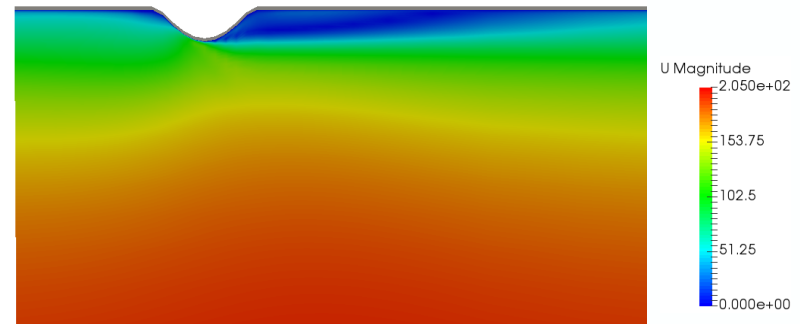
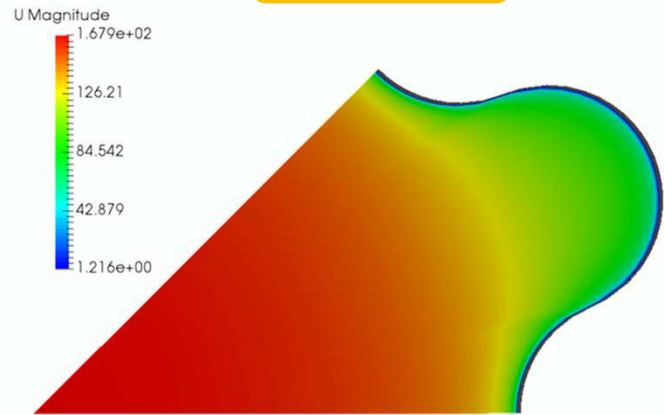


Non-uniform coke layer growth



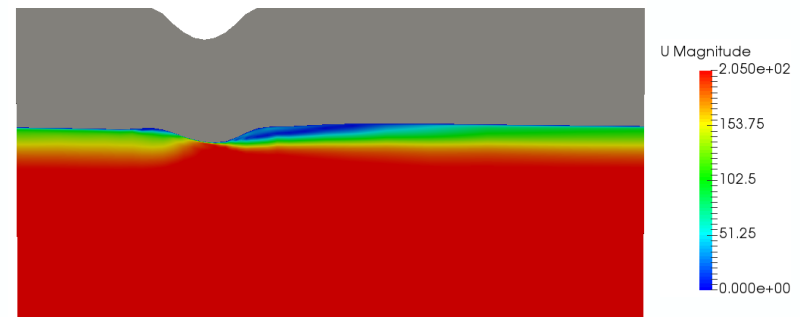
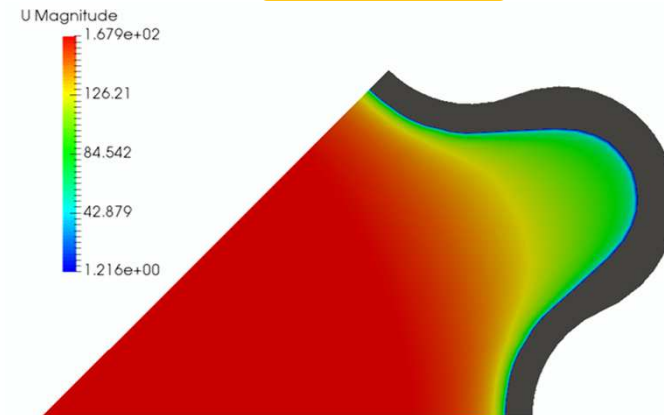
SOR (0 hrs)

SOR

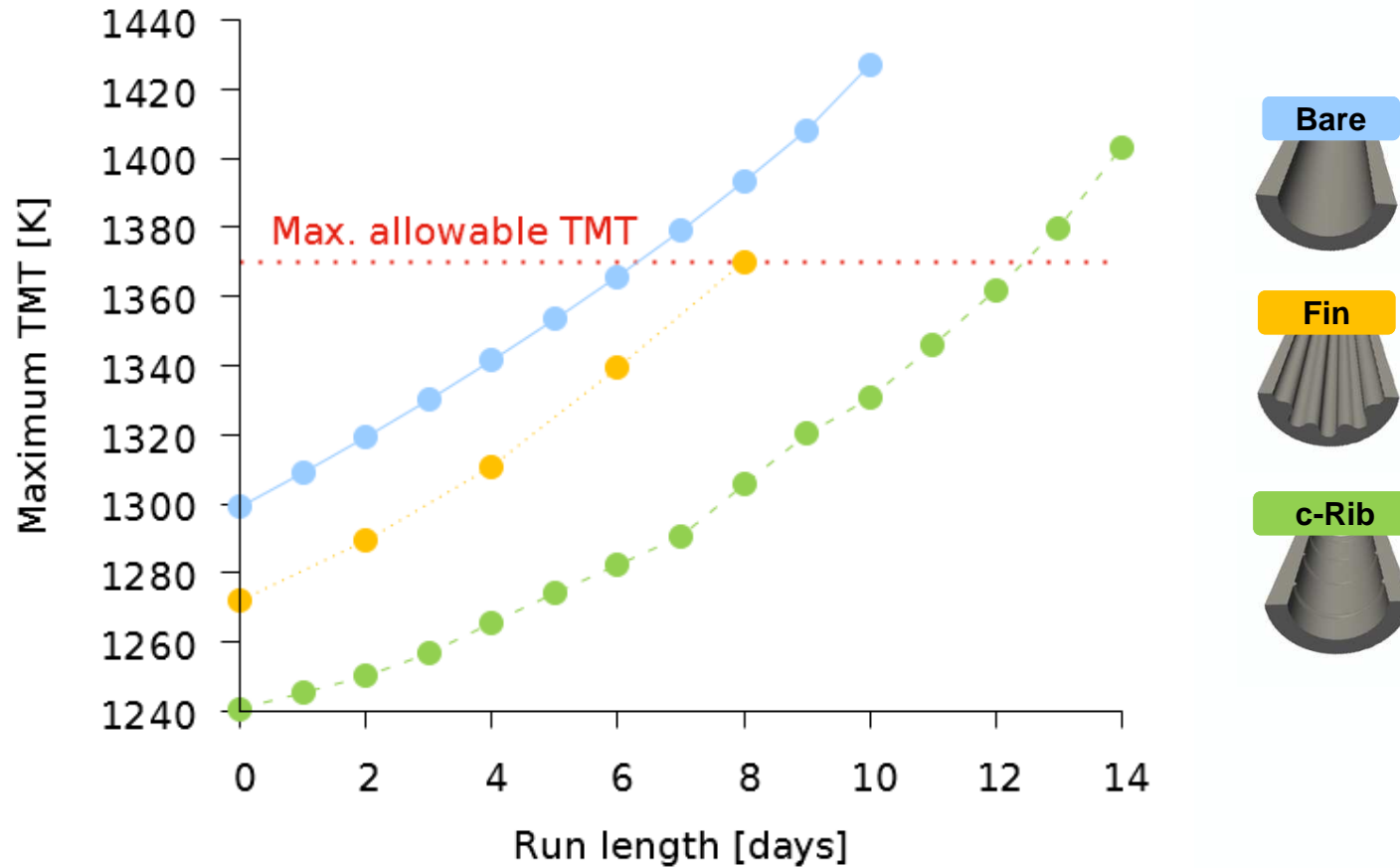


48 hrs

10 days



Tube Metal Temperature

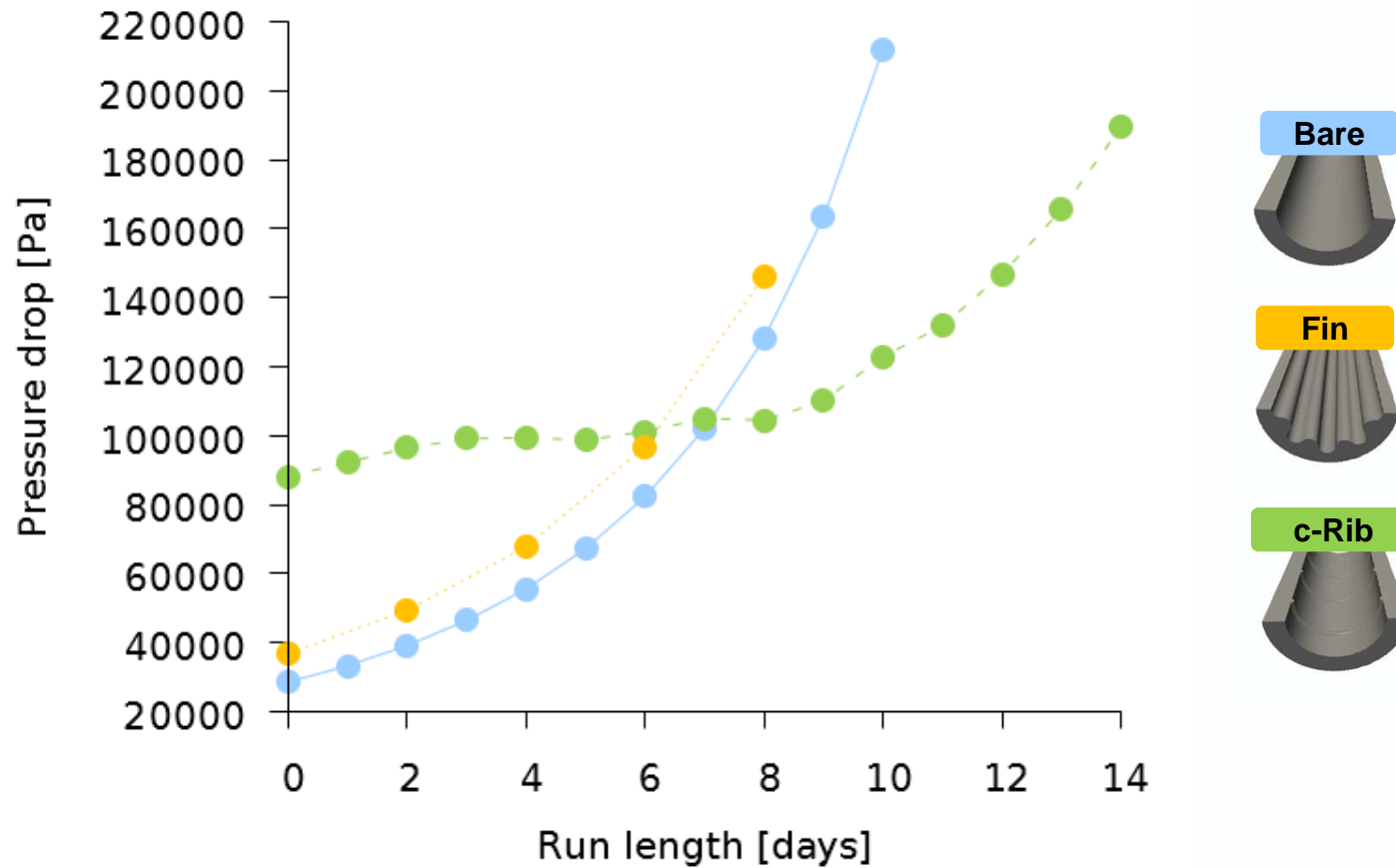


Thermal resistance coke layer

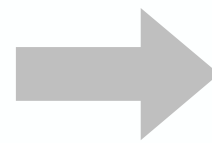


Max. TMT increases

Pressure drop



Cross-sectional flow area decreases due to coke



Pressure drop increases

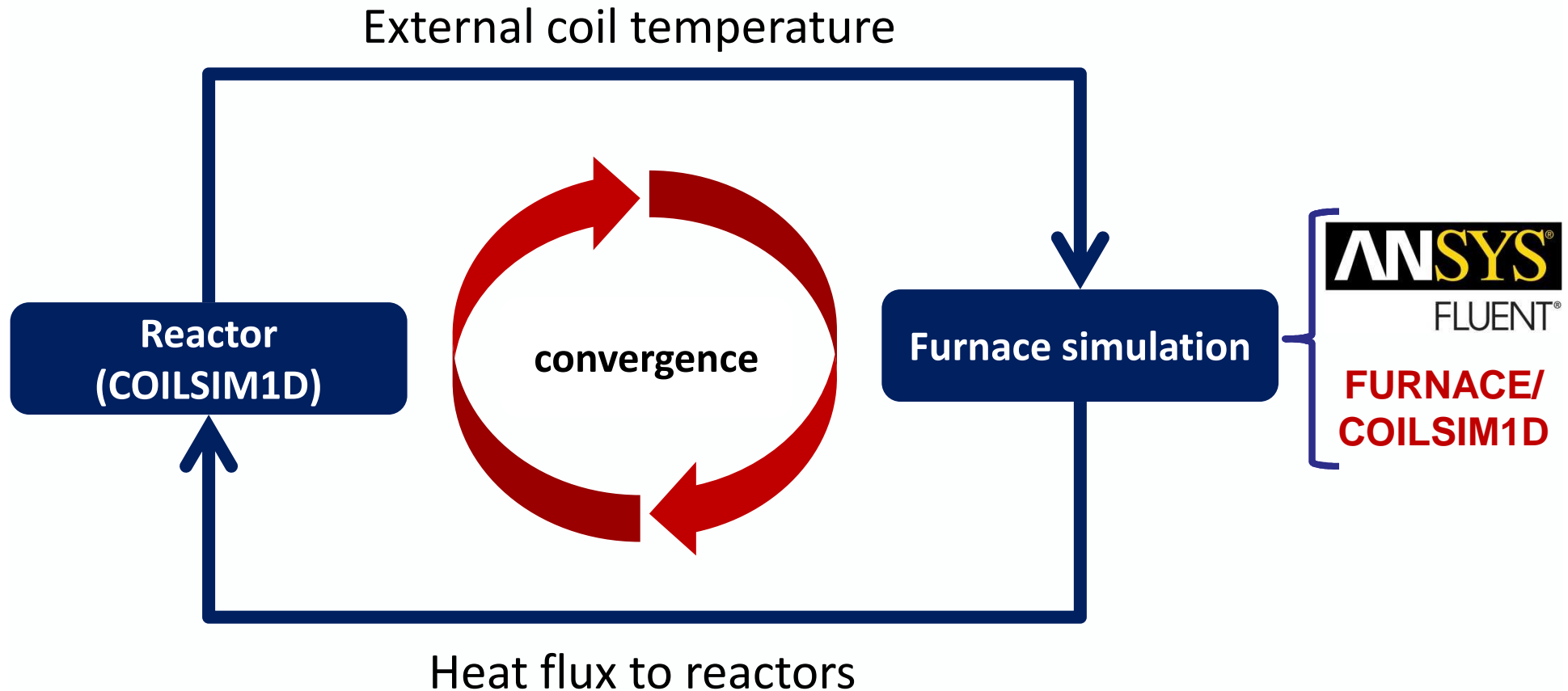
Outline

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- Reactor
- **Process**
- Conclusions

Outline

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- Reactor
- **Process: fire box**
- Conclusions

Coupled reactor-furnace simulation



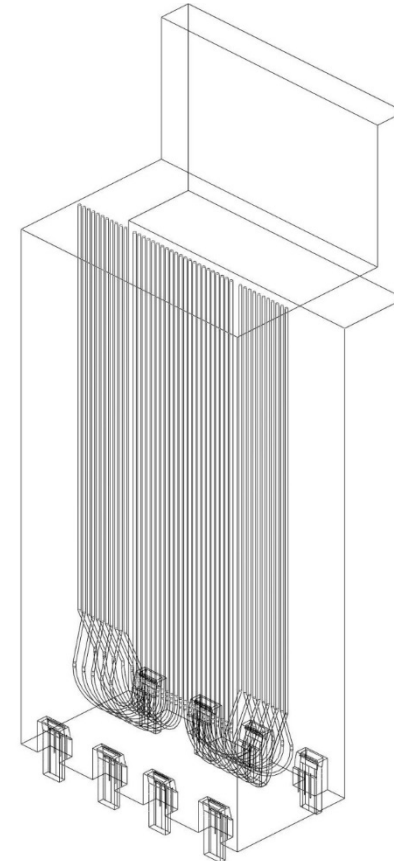
Full furnace simulation

Ultra Selective Conversion (USC)

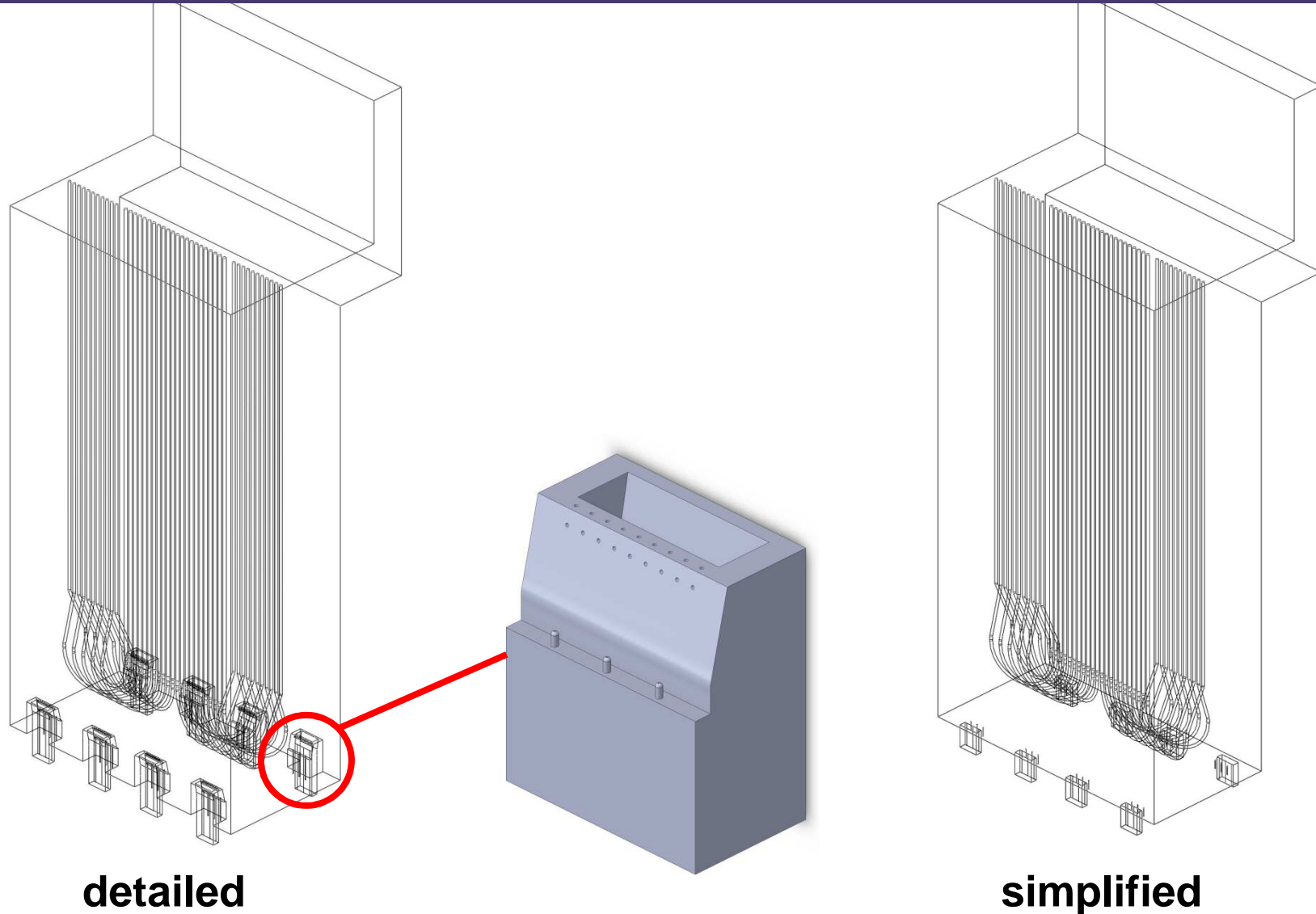
- 100% floor burner
- Fuel composition mol%: CH₄(89%)-H₂(11%)
- U coil
- Feedstock: Naphtha

Coupled modeling

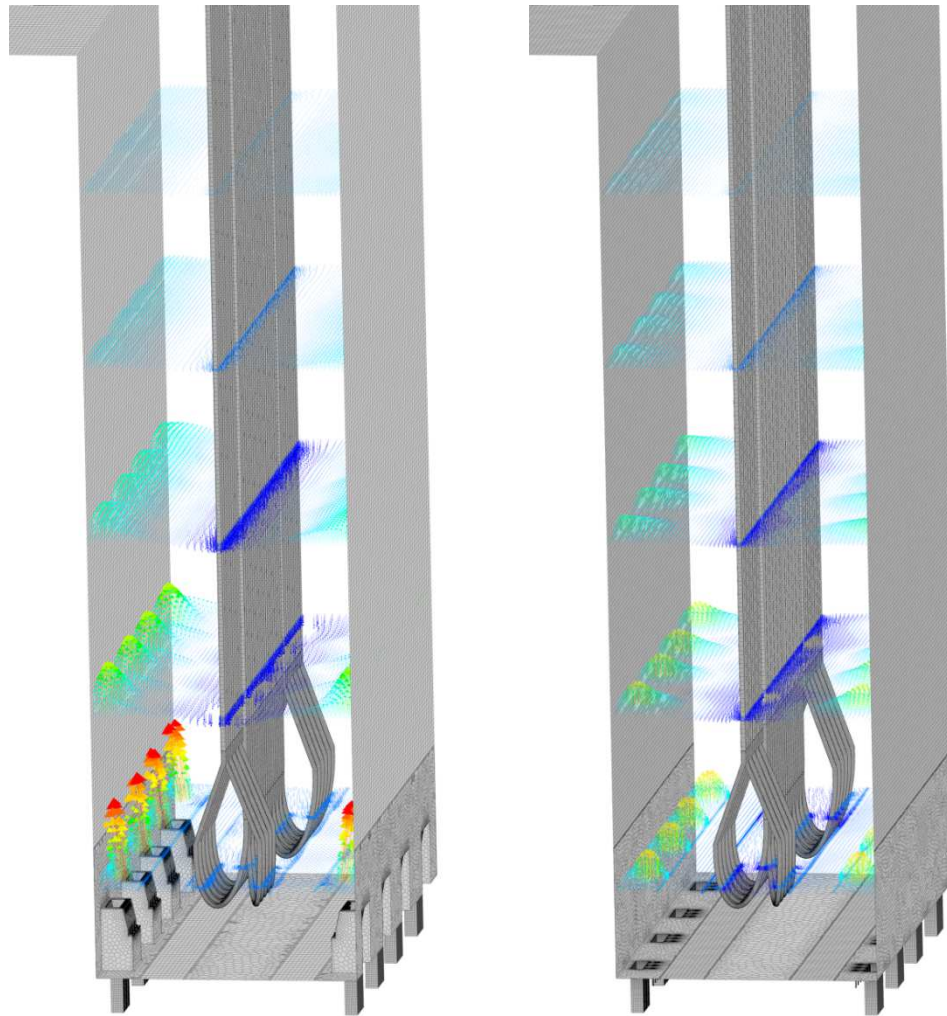
- 3D CFD furnace model
- **1D reactor model (COILSIM1D)**
- Detailed cracking kinetics (CRACKSIM)



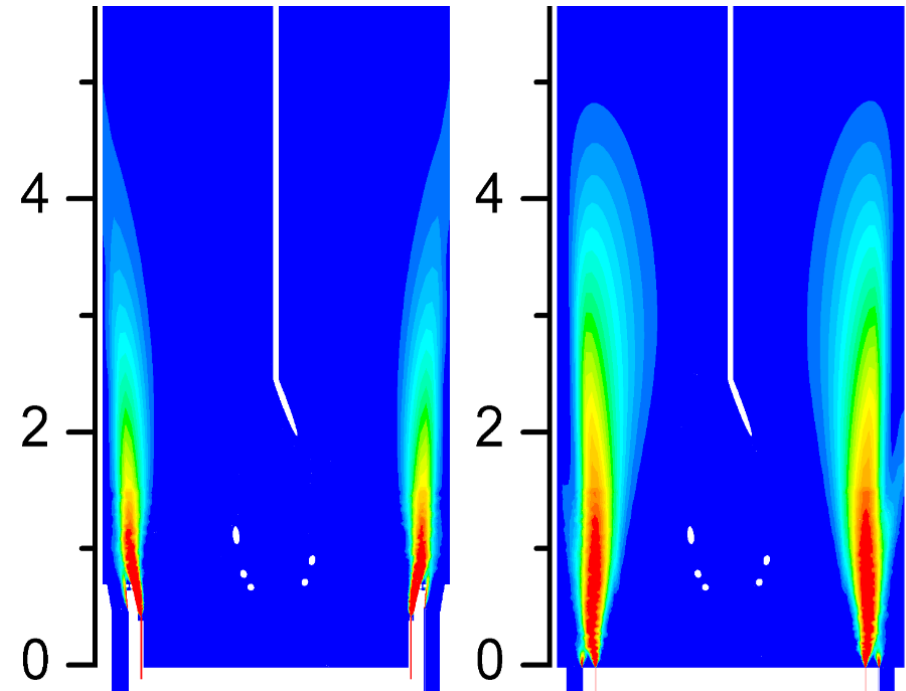
Detailed : long flame burners



Flue gas: velocity and concentration fields



Methane mole fraction



detailed

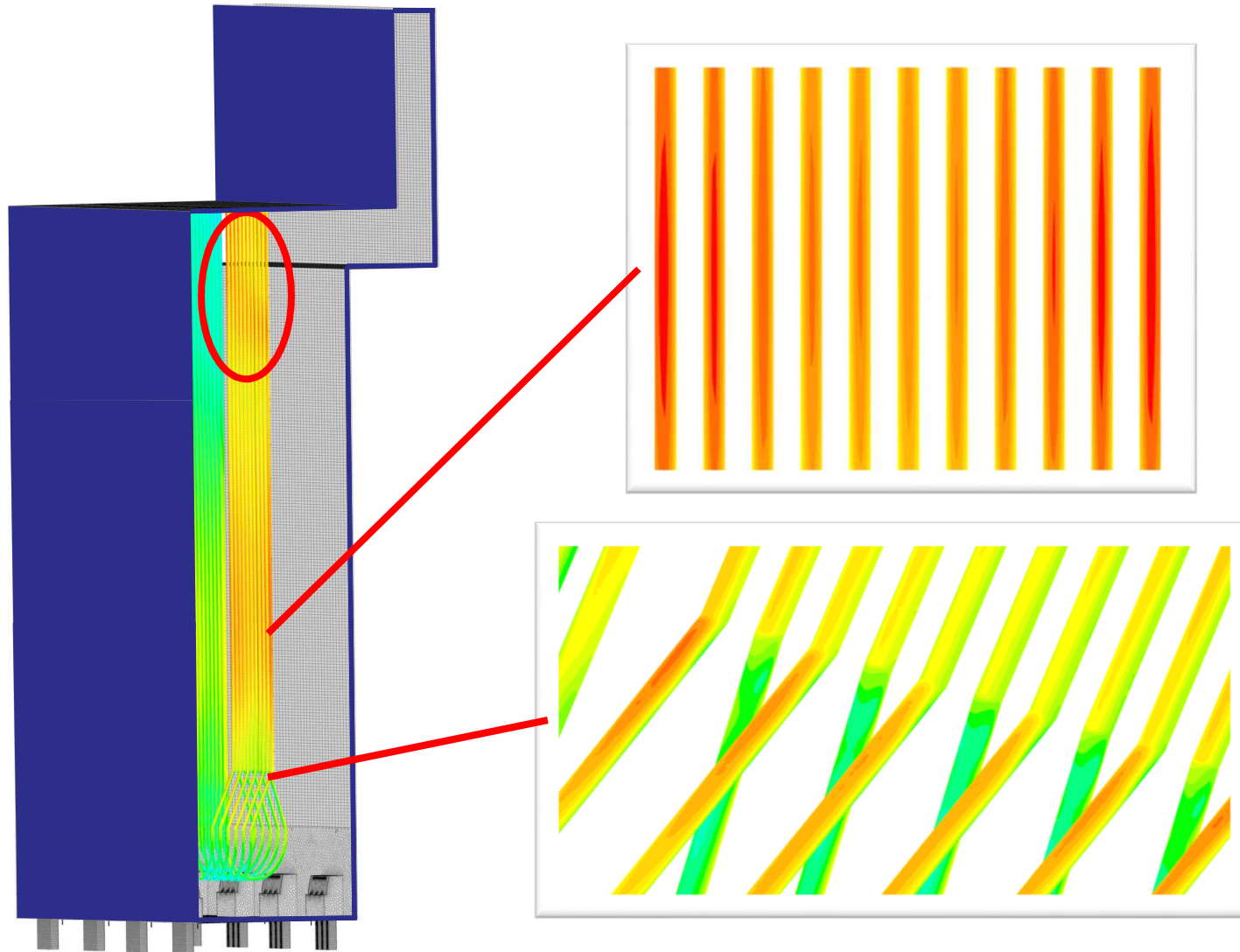
simplified



Detailed case

- Stronger turbulence
- Faster reaction

Tube wall temperature field: local hot spots

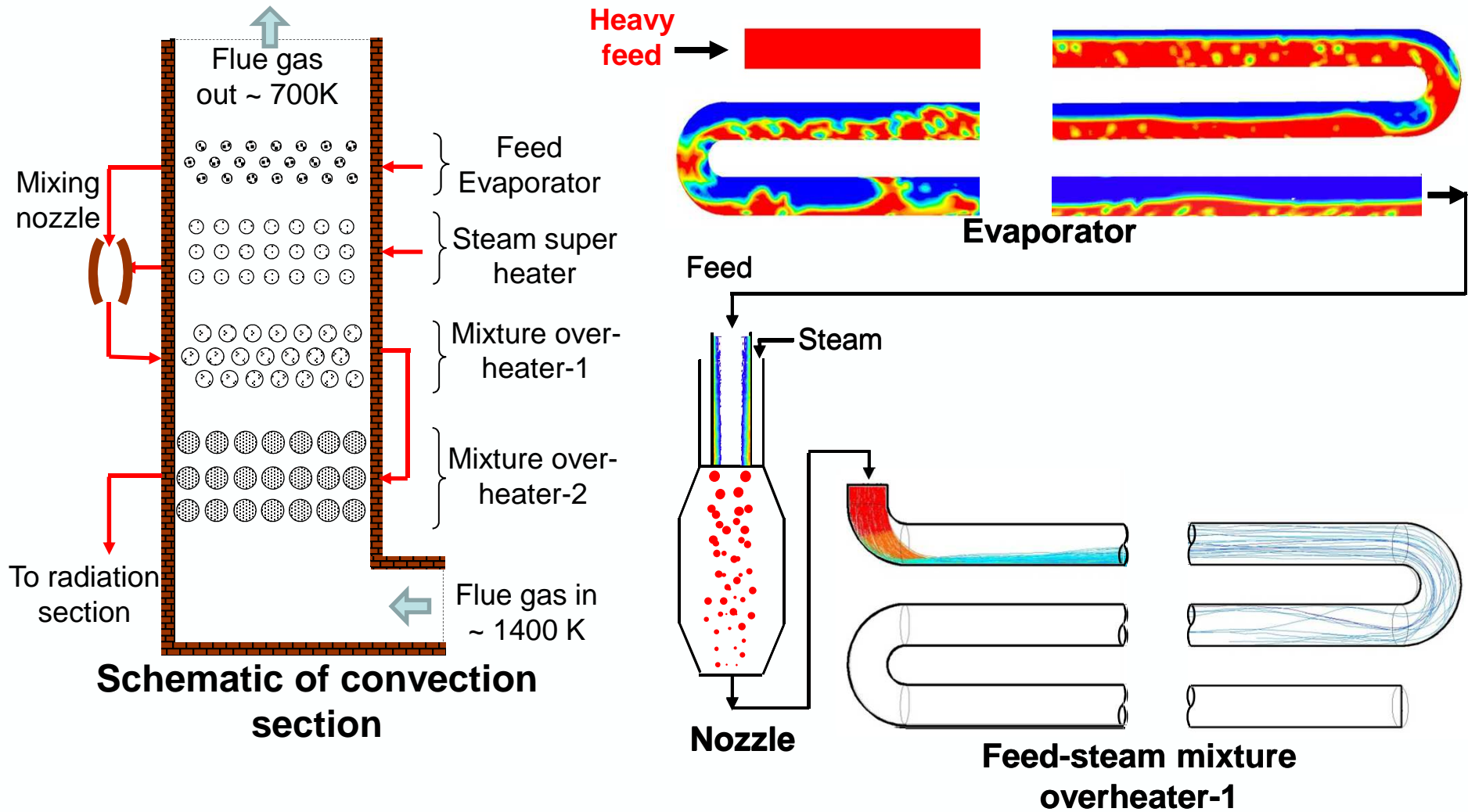


This information is key for control

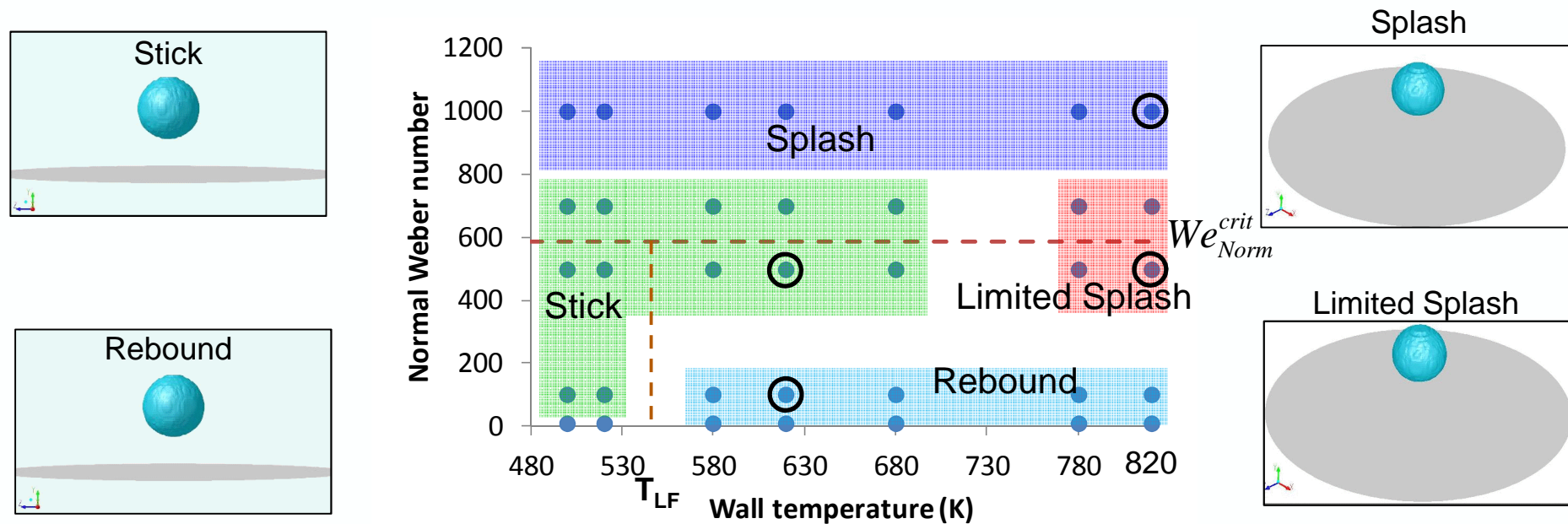
Outline

- Introduction
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- Reactor
- **Process: convection section**
- Conclusions

Steam cracker convection section



Gas condensate: multicomponent mixture

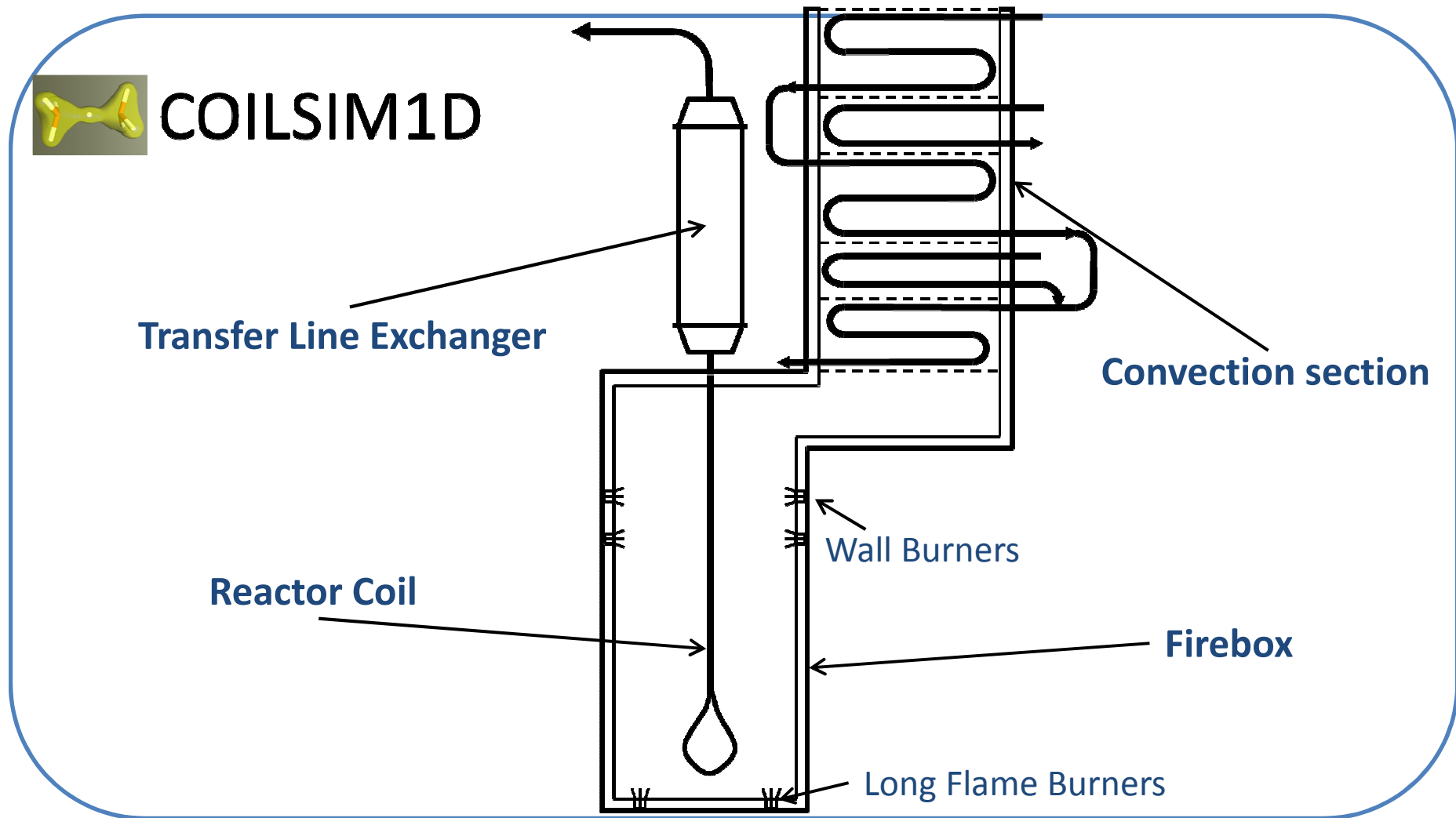


- Wider stick regime as compared to that in single component droplet regime map
- For splash and limited splash, the no. of daughter droplets formed is greater than predicted by correlations available in literature

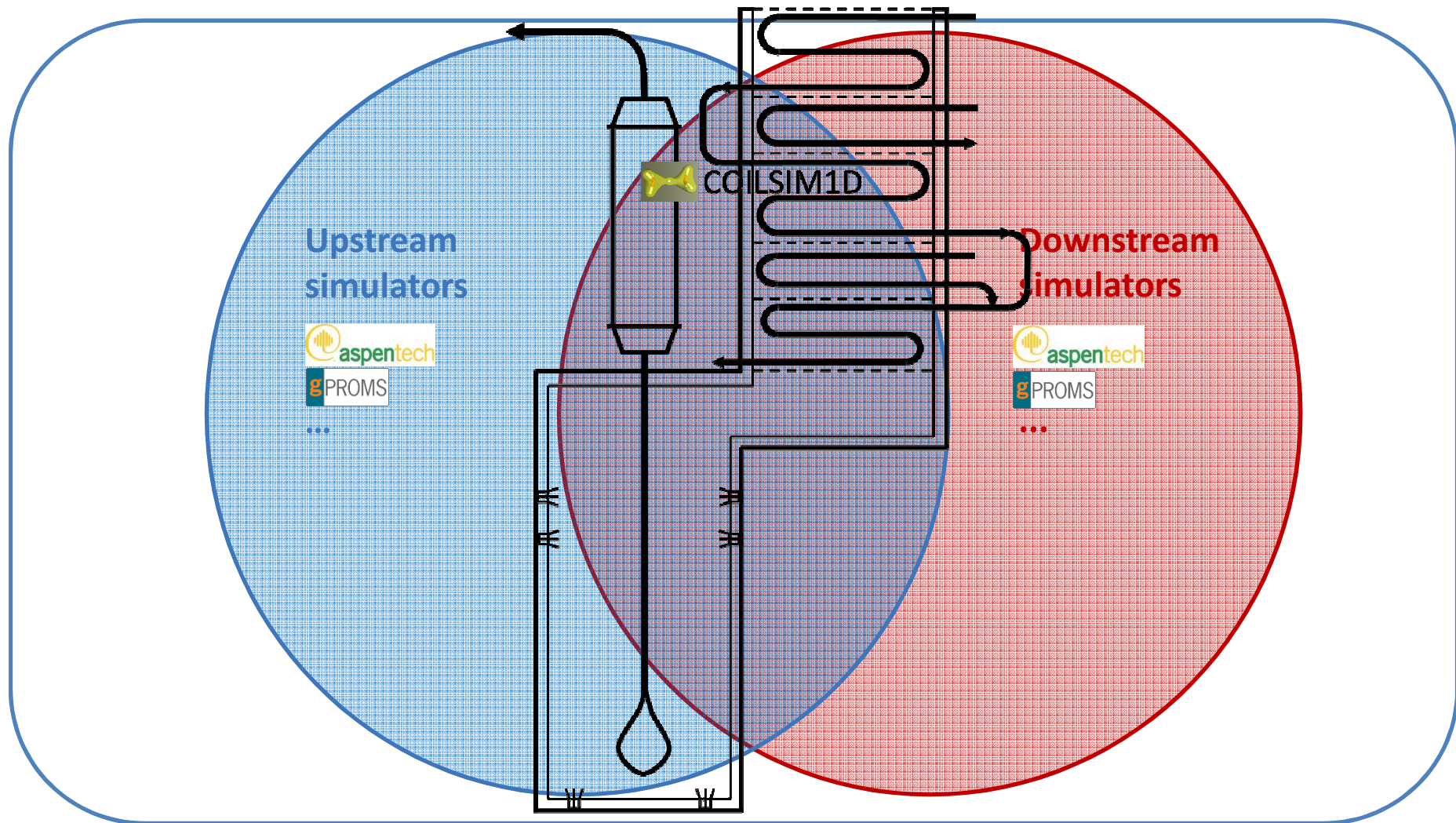
Outline

- Introduction
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- Kinetics
- Reactor
- **Process: hot section**
- Conclusions

The COILSIM1D package



The COILSIM1D package

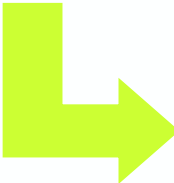


Outline

- Introduction
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Conclusions

- Shannon Entropy maximization to reconstruct feedstocks in terms required for a microkinetic model
- Consistent data set for thermochemistry and kinetics of hydrocarbon and oxygenates radical chemistry
- Ab initio simulation of steam cracking of $C_2/C_3/C_4$ and oxygenates
- Compatibility of renewable feedstocks with existing plants
- Emergence of 3D reactor technologies based on CFD
- Integration of reactor/convection section/furnace



integration of computational chemistry methods with engineering tools at larger time and length scales and experimental validation provides a powerful tool for the optimization and/or design of industrial units

Acknowledgments



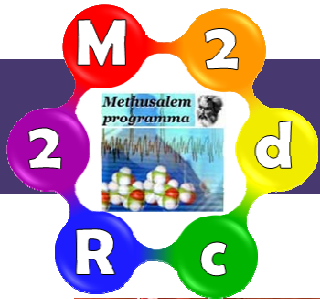
The Long Term Structural Methusalem Funding



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People



Glossary

- SFT: Swirl Flow Tube, a tube with a helicoidal centerline. The helix amplitude is smaller than or equal to the tube radius.
- Swirl flow: a whirling or eddying flow of fluid.
- Swirl number: ratio of tangential over axial momentum transfer
- Wall shear stress: component of stress parallel with the wall. It is the product of the viscosity and the derivative of axial velocity with respect to the radial coordinate.