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Probing Earth's conductivity structure beneath oceans by scalar geomagnetic data: autonomous surface vehicle solution

Alexey Kuvshinov^{1*}, Jürgen Matzka², Benny Poedjono³, Friedemann Samrock¹, Nils Olsen⁴ and Sudhir Pai⁵

Abstract

The electric conductivity distribution of the Earth's crust and upper mantle provides a key to unraveling its structure. Information can be obtained from vector data time series of the natural variations of the magnetic and electric field in a directional stable reference frame. Applying this method, known as magnetotellurics, to oceanic regions is challenging since only vector instruments placed at the sea bottom can provide such data. Here, we discuss a concept of marine induction surveying which is based on sea-surface scalar magnetic field measurements from a modern position-keeping platform. The concept exploits scalar magnetic responses that relate variations of the scalar magnetic field at the survey sites with variations of the horizontal magnetic field at a reference site. A 3-D model study offshore Oahu Island (Hawaii) demonstrates that these responses are sensitive to the conductivity structure beneath the ocean. We conclude that the sensitivity, depending on the bathymetry gradient, is typically largest near the coast offshore. We show that such sea-surface marine induction surveys can be performed with the Wave Glider, an easy-to-deploy, autonomous, energy-harvesting floating platform with position-keeping capability.

Keywords: Marine EM, Wave Glider, Scalar magnetic field variations

Introduction

Magnetotellurics (MT) is an electromagnetic induction method to infer the electric conductivity structure of the subsurface from the measurement of time series of the natural variations of the magnetic and electric field at the surface (Chave and Jones 2012). Knowledge of the conductivity structure is of interest for recovering the structure of the Earth's crust and mantle (Khan and Shankland 2012) and for estimating the influence of induced electric currents in the oceans and mantle on geomagnetic observations on ground and from satellite (Kuvshinov 2008). More and more MT studies are conducted offshore (Baba et al. 2010; Naif et al. 2013; Key et al. 2013) to fill the substantial gap in our knowledge about Earth's electric conductivity structure in the vast oceanic regions. Due to the requirement for a fixed or known sensor orientation

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were deployed in two configurations: one anchored to the seafloor; the second free-floating. Here, we explore an application of the scalar response concept using modern position-keeping platform in the form of an autonomous surface vehicle (ASV) not tethered to the seafloor.

The paper is organized as follows. "Scalar responses" section outlines the derivation of scalar responses. "3-D model study" section presents the results of a 3-D model study which demonstrates the sensitivity of the responses to conductivity structures beneath the ocean. The modeled region is Oahu Island (of the Hawaii Islands chain) and surroundings. The Honolulu geomagnetic observatory operated by US Geological Survey (USGS) was chosen as a reference site. Based on the results of this model study, three suitable offshore sites near Oahu Island were identified and scalar measurements were performed in May-August 2013 using the unmanned, autonomous, wave and solar powered "Wave Glider" ASV. This platform was developed and operated by Liquid Robotics Oil and Gas/Schlumberger and was equipped for our field experiment with a towed Overhauser scalar magnetometer. "Scalar field measurements using the Wave Glider platform" section provides information about the platform, "Data processing" discusses the data processing, and "Observed versus predicted responses" section presents a comparison of the predicted responses with those estimated from the data. "Conclusions and discussion" section contains conclusions and discussion. The paper also includes two appendices in which alternative "scalar" responses are introduced.

Scalar responses

This section sketches the derivation and explanation of scalar responses and closely follows the line of reasoning and nomenclature used by Avdeev et al. (1994).

Deriving the scalar responses one relies on two assumptions: (a) The source of the time-varying magnetic field is a vertically incidenting plane wave; (b) the magnitude of magnetic field variations, $\mathbf{B}(\mathbf{r}, t)$, is much smaller than the magnitude of the static ambient (main) magnetic field, $\mathbf{B}_0(\mathbf{r})$, i.e.,

$$|\mathbf{B}(\mathbf{r},t)| \ll |\mathbf{B}_0(\mathbf{r})|. \tag{1}$$

The latter assumption allows to represent time variations of the scalar field, $F(\mathbf{r}, t)$, in the following form

$$F(\mathbf{r},t) = |\mathbf{B}_0(\mathbf{r}) + \mathbf{B}(\mathbf{r},t)| - |\mathbf{B}_0(\mathbf{r})| \approx \mathbf{p}(\mathbf{r}) \cdot \mathbf{B}(\mathbf{r},t), (2)$$

where **p** stands for the normalized static main field (or in other words for the unit vector in the direction of the main field)

$$\mathbf{p}(\mathbf{r}) = \frac{\mathbf{B}_0(\mathbf{r})}{|\mathbf{B}_0(\mathbf{r})|}.$$
(3)

Transforming Eq. (2) into the frequency domain we have

$$F(\mathbf{r},\omega) \approx \mathbf{p}(\mathbf{r}) \cdot \mathbf{B}(\mathbf{r},\omega). \tag{4}$$

Note that in the latter equation the condition $\mathbf{p} \cdot \mathbf{B} = 0$ leads to the "amphidrome" phenomenon F = 0, discussed in detail by Hitchman et al. (1998) and Lilley et al. (1999). It happens when the direction of the time-varying field is largely perpendicular to the main field direction.

Further, the plane wave assumption allows us to write an equation (Berdichevsky and Dmitriev 2008) which relates the vertical component B_z with the horizontal component $\mathbf{B}_H = (B_x B_y)$ at the survey site **r** via the socalled tipper **T**

$$B_z(\mathbf{r}) = \mathbf{T}(\mathbf{r}) \cdot \mathbf{B}_H(\mathbf{r}), \quad \mathbf{T} = (T_{zx} \ T_{zy}), \tag{5}$$

where the *x*- and *y*-directions are defined as the directions to magnetic North and magnetic East, respectively, with *z* being vertically downwards.

One can also write another equation that relates horizontal components at a survey site with horizontal components at a reference site \mathbf{r}_b via the so-called inter-site horizontal magnetic tensor \underline{M}

$$\mathbf{B}_{H}(\mathbf{r}) = \underline{\underline{M}}(\mathbf{r}, \mathbf{r}_{b}) \mathbf{B}_{H}(\mathbf{r}_{b}), \quad \underline{\underline{M}} = \begin{pmatrix} M_{xx} & M_{xy} \\ M_{yx} & M_{yy} \end{pmatrix}.$$
(6)

Note that hereinafter the dependence of all quantities (except **p**) on frequency is implied but omitted. By substituting Eq. (6) in Eq. (5), and then substituting the resulting equation and Eq. (6) in Eq. (4) we obtain an equation which relates variations of the scalar magnetic field at the survey site with variations of the horizontal magnetic field at the reference site

$$F(\mathbf{r}) = \mathbf{S}(\mathbf{r}, \mathbf{r}_b) \cdot \mathbf{B}_H(\mathbf{r}_b), \quad \mathbf{S} = (S_{fx} \ S_{fy}), \tag{7}$$

where (inter-site) responses, S_{fx} and S_{fy} , which we will call "scalar magnetic responses," are a combination of components of tipper **T**, elements of the horizontal magnetic tensor *M* and components of the normalized main field **p**

$$S_{fx} = M_{xx}p_x + M_{yx}p_y + (T_{zx}M_{xx} + T_{zy}M_{yx})p_z, \quad (8)$$

$$S_{fy} = M_{xy}p_x + M_{yy}p_y + (T_{zx}M_{xy} + T_{zy}M_{yy})p_z.$$
 (9)

Five comments are relevant at this point.

 Since the scalar magnetic responses are a combination of components of tippers and horizontal magnetic tensor, they cannot contain any useful information about the Earth's interior in regions characterized by a 1-D conductivity distribution for both survey and reference site. Indeed, in 1-D conductivity models the tipper is zero and the horizontal magnetic tensor is just the unit matrix. Luckily in our survey setup one always has a 3-D environment due to the contrast between ocean and land (recall that a reference site is located onshore).

• If the survey site **r** is in a 1-D conductivity environment, then $T_{zx} = T_{zy} = 0$ (due to the vertically incidenting plane wave excitation), and thus, Eqs. (8)–(9) are reduced to

$$S_{fx} = M_{xx}p_x + M_{yx}p_y,\tag{10}$$

$$S_{fy} = M_{xy}p_x + M_{yy}p_y. \tag{11}$$

Note that Eqs. (10)–(11) are also valid near the dip equator, due to the fact that $p_z = 0$ there.

In polar regions (where *p_z* ≫ *p_x*, *p_y*) Eqs. (8)–(9) are reduced to

$$S_{fx} = \left(T_{zx}M_{xx} + T_{zy}M_{yx}\right)p_z,\tag{12}$$

$$S_{fy} = (T_{zx}M_{xy} + T_{zy}M_{yy})p_z.$$
 (13)

- Since the unit vector **p** generally varies insignificantly within the area of most MT surveys, one can assume that $\mathbf{p}(\mathbf{r}) \equiv \mathbf{p}(\mathbf{r}_c)$, where \mathbf{r}_c is some point (e.g., the center) of the survey area.
- If the horizontal electric field, \mathbf{E}_H is measured at a reference site, then alternative scalar responses can be obtained, which relate variations of the scalar magnetic field at a survey site with variations of the horizontal electric field at a reference site. More details about these responses are presented in Appendix 1.

3-D model study

We performed a 3-D model study in order to estimate the sensitivity of scalar responses to conductivity structures beneath the ocean. The target region was Oahu Island, Hawaii, and surroundings. The modeling was performed in the period range between 4 min and 3 h using the X3D code (Avdeev et al. 1997a, 2002). The code is based on the contracting integral equation technique (Pankratov et al. 1995) and proved to be an accurate and efficient tool for 3-D EM modeling in a wide range of applications, including MT, induction logging, airborne, ground controlledsource and motionally induced EM (Avdeev et al. 1997a, b, 1998, 2002; Pankratov et al. 1998, 2004; Pulkkinen and Engels 2005; Avdeev and Avdeeva 2009; Kalscheuer et al. 2012; Samrock and Kuvshinov 2013). The conductivity model we adopted consists of eight anomalous layers (three layers account for topography and five for bathymetry) on top of a one-dimensional (1-D) conductivity section. Bathymetry and topography data have been taken from the ETOPO1 Global Relief Model database (Amante and Eakins 2009). The left plot of Fig. 1 presents the map of bathymetry and topography in the region. The 3-D conductivity distribution within the eight anomalous



Fig. 1 *Lett* Bathymetry of Hawaii with Oahu Island and the Hoholdid geomagnetic observatory (*black diamond*) in the centre. *Red dots* show the three sites where the scalar magnetic field was measured. *Right* Mantle 1-D conductivity profiles used in our 3-D model study. The *blue curve* stands for the global 1-D conductivity section (GLO) obtained from satellite magnetic data (Kuvshinov and Olsen 2006). The *red curve* depicts a regional 1-D conductivity section (PHS) beneath the Philippine Sea recovered from sea-bottom MT data (Baba et al. 2010)

layers is derived under the assumption of a seawater conductivity of $\sigma_{sea} = 3.2$ S/m and a land conductivity of $\sigma_{\text{land}} = 10^{-2}$ S/m. The original, one arc-minute, data of bathymetry and topography used for estimating conductivity distributions in these layers were interpolated to a regular Cartesian grid with a horizontal cell size of $1 \text{ km} \times 1 \text{ km}$. The total horizontal size of the model was 356 km \times 356 km. The sensitivity of scalar responses to conductivity variations beneath ocean was investigated with respect to two different 1-D conductivity sections. These sections are shown in the right plot of Fig. 1. The first 1-D section, labeled as GLO, is a global conductivity section that has been inferred from satellite magnetic data (Kuvshinov and Olsen 2006) and that was modified to have a realistic low conductivity in the upper 100 km as these depths are not resolvable by satellite magnetic data. The second 1-D section, denoted as PHS, is a regional 1-D model (for the Philippine Sea), which has been recovered from sea-floor MT data (Baba et al. 2010). Note that we performed extensive model studies to justify the parameters describing the model (cell and mesh sizes, number of anomalous layers, values for seawater and land conductivities). These studies revealed that the effects from varying seawater and land conductivities are smaller than the effect from varying the 1-D section.

Figure 2 exemplifies surface maps of tipper, horizontal magnetic tensor and scalar magnetic response at the period of 1300 s for the region around Oahu Island, Hawaii. The left and right plots show the magnitudes of the real and imaginary parts of the corresponding responses, respectively, which, in case of the scalar responses, are defined as

$$\Re S = \sqrt{\left(\Re S_{fx}\right)^2 + \left(\Re S_{fy}\right)^2, \Im S} = \sqrt{\left(\Im S_{fx}\right)^2 + \left(\Im S_{fy}\right)^2}.$$
(14)

Similarly, we define $\Re T$, $\Im T$, $\Re M_x$, $\Im M_x$, $\Re M_y$ and $\Im M_y$. Note that Honolulu magnetic observatory (IAGA code HON) was chosen as the reference site. Also note that here the global (GLO) 1-D conductivity profile was used as underlying 1-D section. Finally, we remark that the normalized static magnetic field **p** was calculated using a recent update of the CHAOS model (Olsen et al. 2014).

Figure 2 shows the anomalous behavior in both the real and imaginary parts of all responses in the regions where lateral contrasts of conductivity (here controlled by bathymetry) exist (the so-called coast or ocean effect discussed in numerous papers (Lilley et al. 1979; Lilley 2005; Kuvshinov and Utada 2010). The horizontal magnetic tensor \underline{M} and scalar magnetic response **S** reveal anomalous behavior offshore, whereas the most prominent anomalies of tipper **T** are confined to the coast. In general, it is seen that the scalar magnetic response **S** is indeed a combination of components of tipper and horizontal magnetic tensor.

It is also interesting to note that \mathbf{T} (and thus total-field fluctuations) are suppressed on the north side of Oahu. This pattern is a nice example of magnetic amphidrome conditions, mentioned in "Scalar responses" section.

To quantify the sensitivity of scalar magnetic responses to subsurface conductivity we also compute the responses using a different, regional (PHS) 1-D conductivity profile. The maps in Fig. 3 present the difference between scalar magnetic responses computed for the two 1-D sections. Here, the difference (in the real part) stands for the quantity

$$d\Re S = \sqrt{\left(\Re S_{fx}^G - \Re S_{fx}^P\right)^2 + \left(\Re S_{fy}^G - \Re S_{fy}^P\right)^2}, \quad (15)$$

where superscripts "G" and "P" denote results obtained in the model with global (GLO) and regional (PHS) 1-D conductivity profiles, respectively. Similarly, we define the difference in the imaginary part. The results are presented for the two periods 1300 s (top) and 10,000 s (bottom). The difference is most prominent near the northwest and the southeast (offshore) tips of Oahu Island and reaches 50% of the responses themselves at a period of 1300 s (cf. the bottom plots in Fig. 2).

Final model experiment comprises computation of the responses using 1-D section which coincides with PHS profile down to depth of 14 km (the depth where GLO and PHS profiles meet; cf. right plot of 1) and follows GLO profile below 14 km. The maps of difference between the

responses computed for this and GLO sections (see Additional file 1) suggest that the scalar responses are most sensitive to the upper (crustal) layers of the 1-D section.

Scalar field measurements using the Wave Glider platform

From the model study we identified three regions around Oahu island where the largest sensitivity of scalar responses, as quantified by Eq. (15), to subsurface conductivity were detected. The actual location of the sites is shown in Fig. 1 by red dots. The coordinates of the sites, hereinafter denoted as M1, M2 and M3 sites, are (21.0835°N, 158.0000°W), (21.2420°N, 157.6290°W) and (21.5540°N, 158.3821°W), respectively.

To measure the scalar magnetic field variations at these locations, the Wave Glider observation platform was used. The Wave Glider autonomous surface vehicle (ASV) was invented and developed by Liquid Robotics Inc. It is a two-part vehicle and comprises a surface component (the "float"; shown in the left plot of Fig. 4) and a submerged component (the "sub"; shown in the right plot of Fig. 4) connected by an umbilical tether. The ASVs propulsion system is passive and mechanical; it converts energy from wave motion into thrust. Solar panels mounted on the platform are used to charge batteries which provide power to the control system, radios and payload. Other components of the vehicle are a satellite communication system, navigation control, solar charging system, batteries and different instrument payloads. In our experiment the Wave Glider was equipped with a towed scalar magnetometer model "Explorer" by Marine Magnetics, www.marinemagnetics.com. The control and communication with the vehicle is provided via a satellite system. The ASV can be programmed to travel directly from one location to another, follow a specific route, or can be fixed at one position (within ± 200 m or so) for a long time (from days to weeks). In our marine survey, continuous measurements at fixed positions were conducted for 3.8, 2.9 and 8 days at the sites M1, M2 and M3, respectively. The scalar magnetic field measurements were performed in May-August of 2013, and synchronous measurements of the horizontal magnetic field from Honolulu magnetic observatory were used as reference site data.

Data processing

We discuss the processing scheme on the example of data collected at the M1 site. Green and blue curves in Fig. 5 show variations of scalar magnetic field at M1 and reference (Honolulu observatory) site, respectively. Evidently the offset is due to the static internal field difference between two sites. The pronounced high-frequency oscillations (of 20 nT amplitude in average) at survey







site appeared to be due to ± 200 m meandering of Wave Glider position (shown in Fig. 6) in the presence of strong gradients of crustal field which are observed in this region.

To suppress undesirable oscillations in the data we elaborated the following correction scheme.

• First, we subtract the CHAOS predictions of scalar static magnetic field from the data at both survey and reference site. We denote the resulting signals as $F_s(\mathbf{r}(t), t)$ and $F_b(\mathbf{r}_b, t)$, respectively. The dependence of \mathbf{r} on time t in F_s reflects the fact that Wave Glider slightly changes its position. This step removes the

observed offset between survey and reference measurements.

- Second, we subtract the $F_b(\mathbf{r}_b, t)$ from $F_s(\mathbf{r}(t), t)$. The resulting part of the signal, denoted as $\delta F_s(\mathbf{r}(t))$, should only contain observed oscillations at the survey site which are associated with fluctuations of the Wave Glider position. This is true under the assumption that time variations of the scalar magnetic field due to external source (of ionospheric or/and magnetospheric origin) are approximately the same at survey and reference site.
- Third, we approximate δ*F_s* by a bilinear function in horizontal position *x*, *y*:









$$\delta F_s(\mathbf{r}(t)) \approx Ax(t) + By(t) + Cx(t)y(t) + D, \qquad (16)$$

and determine the coefficients A, B, C and D by least squares fitting. Here, we introduce local two-dimensional (*OXY*) Cartesian coordinate system where the origin of coordinates coincides with the location of the reference site.

• Finally, once the coefficients *A*, *B*, *C* and *D* are determined, we obtain corrected data, *F_c*(**r**, *t*), at survey site as

$$F_{c}(\mathbf{r},t) = F_{s}(x(t), y(t), t) - (Ax(t) + By(t) + Cx(t)y(t) + D).$$
(17)

Red curve in Fig. 5 shows the corrected time series at M1 site obtained by implementing the above scheme. It is

seen from the figure that the correction scheme indeed suppresses high-frequency oscillations at survey site caused by small changes in position of the measuring platform.

Observed versus predicted responses

The six plots in Fig. 7 show the comparison of predicted and observed scalar magnetic responses. Left and right plots present the x- and y-components of the responses, respectively, with black and red colors showing real and imaginary parts. The observed responses were estimated using a data processing tool (Püthe and Kuvshinov 2014) based on a robust section-averaging approach with a jackknife estimator of the uncertainties.



It is seen from the figure that overall the predictions (squares—for GLO model, and triangles—for PHS model) are in encouraging agreement with the observations (open circles with error bars) at all sites, in both components, and in real as well as imaginary parts. Even the predicted reversal of the real and imaginary parts of S_{fy} at M2 site is similar to the observations. The remaining discrepancy is most probably due to inaccuracy of the underlying 3-D conductivity model, and partly due to inaccuracy in the estimated (observed) responses, due to the limited time length of observations.

Conclusions and discussion

In this paper we discuss a concept of marine induction surveying which is based on sea-surface scalar magnetic field measurements from a position-keeping platform. The concept exploits scalar magnetic responses that relate variations of the scalar magnetic field at the survey sites with variations of the horizontal magnetic field at a reference site. We demonstrate-based on a realistic 3-D model study-that the scalar magnetic responses are sensitive to the conductivity structures beneath the ocean. We conclude that the sensitivity, depending on the horizontal gradient of bathymetry, is typically largest near the coast offshore. We show that such sea-surface marine induction surveys can be performed with the Wave Glider observation platform. We believe that this type of survey represents an attractive complement to traditional marine MT studies based on sea-bottom vector measurements. We also would like to remark here that in contrast to sea-bottom observations, which require special design of the instruments, one can use standard instruments for the scalar survey.

Performing 3-D models studies we ultimately tested whether the observations are able to distinguish between two 1-D models that strongly differ down to 300 km depth. The topic for further work could include answering the following questions: (a) What are the prospects of distinguishing between profiles which differ less? (b) Whether one can resolve 3-D inhomogeneities beneath oceans with this technique? (c) What is an optimal resolution of the model to account properly for the ocean effect? (d) Is it possible to improve the quality of the observed responses?

As for survey concept itself, we are also aware of some drawbacks. First, since the scalar magnetic responses are a combination of components of tipper and horizontal magnetic tensor, they cannot contain any useful information about the Earth's interior in regions characterized by a 1-D conductivity distribution. Indeed, assuming a vertically incidenting plane wave source and a 1-D conductivity, the tipper is zero and the horizontal magnetic tensor is just the unit matrix. Luckily in our survey setup one always has a 3-D environment due to the contrast between ocean and land (recall that a reference site is located onshore), and variable bathymetry.

Second, an estimation of the scalar magnetic responses requires measurements of the horizontal magnetic field components at a reference site. This means that the concept will only work in oceanic regions sufficiently close to a reference station (less than a few hundred kilometers to satisfy the source vertically incidenting plane wave approximation for both locations).

Third, the highly conducting ocean acts as an effective shield, which prevents the electromagnetic field at shorter periods to penetrate into the Earth; the deeper the ocean the stronger this shielding. Consequently, the shallower the ocean, the better the performance of the sea-surface scalar survey.

Lastly, one can speculate that on the sea surface the magnetic signals from waves and swells could affect the scalar response estimation. However, these motionally induced signals have much higher frequencies (Lilley et al. 2004) compared to the signals we are interested in.

In this paper we explore the applicability of the Wave Glider platform to measure signals originating from plane wave sources. Another option could be the use of the platform for measuring the solar-quiet (Sq) daily variations of the magnetic scalar field in remote oceanic regions otherwise not covered by observations. In this scenario, scalar measurements are analyzed together with simultaneous data from a global net of geomagnetic observatories by means of estimating and interpreting local-to-global responses, similar to those introduced in Püthe et al. (2014). Note that for this type of survey there is no need for reference site observations. One alert, however, is that there are bands of latitude (between dips $I = 20^{\circ}$ and $I = 30^{\circ}$, and between dips $I = -20^{\circ}$ and $I = -30^{\circ}$) where the scalar Sq signal is substantially suppressed because the Sq field direction is largely perpendicular to the main field direction (cf. the note after Eq. 4).

In contrast to sea-bottom MT observations, which include electric field measurements, our observations are purely magnetic, at least at the survey sites. As shown in Appendix 1, another type of responses could be constructed which relate variations of the scalar magnetic field at the survey sites with variations of the horizontal electric field at a reference site. However, in this case the galvanic distortion problem (cf. Jiracek 1990) could complicate the interpretation.

Finally, we would like to note a promising extension of the concept which involves-along with surface scalar measurements-simultaneous scalar magnetic field measurements performed at depth in the water or at sea bottom directly below the sea-surface measurements. This observation scheme is sketched in Appendix 2, and it allows for deriving alternative scalar responses which relate variations of the vertical gradient of the scalar magnetic field at a survey site to horizontal magnetic (or/ and electric) field variations at a reference site. As shown in Appendix 2, these responses is a combination of components of the tipper and elements of the inter-site impedance tensor provided the horizontal magnetic field at a reference site is invoked, or a combination of components of the tipper and elements of the horizontal electric tensor if the horizontal electric field at a reference site is used. This type of survey is more difficult to conduct, but has the advantage of leading to responses that contain information about the electric field at the survey site.

Additional file

Additional file 1: Figure S1. Difference between scalar magnetic responses for the two 1-D sections GLO and PHS + GLO at two periods—1300 (top) and 10000 (bottom) sec. PHS + GLO section coincides with PHS profile down to depth of 14 km (the depth where GLO and PHS profiles meet; cf. right plot of Figure 1 of the main text) and follows GLO profile below 14 km. Left and right plots show the magnitude of the real and imaginary part of the corresponding difference, respectively. Note that different scales are used for the plots.

Abbreviations

MT: magnetotelluric; ASV: autonomous surface vehicle; USGS: United States Geological Survey.

Authors' contributions

AK and JM initiated the study and wrote the draft, BP and SP conducted the Wave Glider survey, AK and FS performed the model study, and AK and NiO processed the data. All authors read and approved the final manuscript.

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Competing interests

The authors declare that they have no competing interests.

Appendix 1: Scalar mixed responses

Let us introduce the inter-site admittance \underline{Y} which relates variations of the horizontal magnetic field at a survey site with variations of the horizontal electric field at a reference site

$$\mathbf{B}_{H}(\mathbf{r}) = \underline{\underline{Y}}(\mathbf{r}, \mathbf{r}_{b}) \mathbf{E}_{H}(\mathbf{r}_{b}), \quad \underline{\underline{Y}} = \begin{pmatrix} Y_{xx} & Y_{xy} \\ Y_{yx} & Y_{yy} \end{pmatrix}, \quad (18)$$

where $\mathbf{E}_H = (E_x E_y)$. Similarly, as it was done in "Scalar responses" section, by substituting Eq. (18) in Eq. (5), and then substituting the resulting equation and Eq. (18) in Eq. (4) we obtain the desired relation

$$F(\mathbf{r}) = \mathbf{A}(\mathbf{r}, \mathbf{r}_b) \cdot \mathbf{E}_H(\mathbf{r}_b), \quad \mathbf{A} = (A_{fx} A_{fy}), \quad (19)$$

where the responses, A_{fx} and A_{fy} , which we will call "scalar mixed responses," are a combination of components of tipper **T**, elements of the admittance tensor \underline{Y} and components of the normalized main field **p**

$$A_{fx} = Y_{xx}p_x + Y_{yx}p_y + (T_{zx}Y_{xx} + T_{zy}Y_{yx})p_z, \quad (20)$$

$$A_{fy} = Y_{xy}p_x + Y_{yy}p_y + (T_{zx}Y_{xy} + T_{zy}Y_{yy})p_z.$$
 (21)

The first four statements in bullets in "Scalar responses" section on the scalar magnetic responses are also valid for these scalar mixed responses.

Appendix 2: Scalar gradient responses

Let us assume that variations of the scalar magnetic field are simultaneously measured at sea surface and directly below at a certain depth in the ocean. Also let us assume that the period of the variations is long enough to write

$$B_z^+ - B_z^- = 0, (22)$$

$$\mathbf{n} \times (\mathbf{B}_H^+ - \mathbf{B}_H^-) = \mu_0 S \mathbf{E}_H.$$
(23)

Here, superscripts "+" and "-" stand for sea surface and at depth, respectively, μ_0 is the magnetic permeability of free space, **n** is an upward unit vector, $S = \sigma d$ is the conductance, where σ is (assumed to be known) conductivity of seawater, and d is depth. Then, using Eq. (22), we can write the vertical gradient of the scalar magnetic field as

$$\Delta F = F^+ - F^- = \mathbf{p} \cdot (\mathbf{B}^+ - \mathbf{B}^-) = \mathbf{p}_H \cdot (\mathbf{B}_H^+ - \mathbf{B}_H^-),$$
(24)

or expressed via electric field (cf. Eq. 23) as

$$\Delta F = -\mu_0 S \mathbf{p}_H \cdot (\mathbf{n} \times \mathbf{E}_H). \tag{25}$$

Here, $\mathbf{p}_H = (p_x p_y)$. Substituting the inter-site impedance relation

$$\mathbf{E}_{H}(\mathbf{r}) = \underline{\underline{Z}}(\mathbf{r}, \mathbf{r}_{b}) \mathbf{B}_{H}(\mathbf{r}_{b}), \quad \underline{\underline{Z}} = \begin{pmatrix} \tilde{Z}_{xx} & \tilde{Z}_{xy} \\ \tilde{Z}_{yx} & \tilde{Z}_{yy} \end{pmatrix}, \quad (26)$$

in Eq. (25) we obtain responses that relate variations of the vertical gradient of the scalar magnetic field at a survey site with variations of the horizontal magnetic field at a reference site by

$$\Delta F(\mathbf{r}) = \mathbf{V}(\mathbf{r}, \mathbf{r}_b) \cdot \mathbf{B}_H(\mathbf{r}_b), \quad \mathbf{V} = (V_{gx} \ V_{gy}), \quad (27)$$

where the responses V_{gx} and V_{gy} , which we will call "scalar gradient magnetic responses," are a combination of elements of inter-site impedance, conductance and normalized horizontal magnetic field

$$V_{gx} = \mu_0 S \left(\tilde{Z}_{xx} p_y - \tilde{Z}_{yx} p_x \right), \tag{28}$$

$$V_{gy} = \mu_0 S \left(\tilde{Z}_{xy} p_y - \tilde{Z}_{yy} p_x \right).$$
⁽²⁹⁾

If the horizontal electric field is measured at a reference site, then alternative scalar gradient responses can be introduced that relate variations of the vertical gradient of the scalar magnetic field at a survey site with variations of the horizontal electric field at a reference site

$$\Delta F(\mathbf{r}) = \mathbf{U}(\mathbf{r}, \mathbf{r}_b) \cdot \mathbf{E}_H(\mathbf{r}_b), \quad \mathbf{U} = (U_{gx} \ U_{gy}), \quad (30)$$

where the responses, U_{gx} and U_{gy} , which we will call "scalar gradient electric responses," are a combination of elements of horizontal electric (telluric) tensor, conductance and normalized horizontal static field

$$U_{gx} = \mu_0 S (L_{xx} p_y - L_{yx} p_x), \qquad (31)$$

$$U_{gy} = \mu_0 S (L_{xy} p_y - L_{yy} p_x). \tag{32}$$

Note that in order to obtain the latter equations we used the following relation

$$\mathbf{E}_{H}(\mathbf{r}) = \underline{\underline{L}}(\mathbf{r}, \mathbf{r}_{b}) \mathbf{E}_{H}(\mathbf{r}_{b}), \quad \underline{\underline{L}} = \begin{pmatrix} L_{xx} & L_{xy} \\ L_{yx} & L_{yy} \end{pmatrix}.$$
(33)

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