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Scandium-doped zinc cadmium oxide as a new stable n-type oxide thermoelectric material†

L. Han,* D. V. Christensen, A. Bhowmik, S. B. Simonsen, L. T. Hung, E. Abdellahi, Y. Z. Chen, N. V. Nong, S. Linderoth and N. Pryds*

Scandium-doped zinc cadmium oxide (Sc-doped ZnCdO) is proposed as a new n-type oxide thermoelectric material. The material is sintered in air to maintain the oxygen stoichiometry and avoid instability issues. The successful alloying of CdO with ZnO at a molar ratio of 1 : 9 significantly reduced the thermal conductivity by up to 7-fold at room temperature. By carefully selecting the Sc-dopant concentrations, a high power factor of $7.1 \times 10^{-4} \text{ W m}^{-1} \text{ K}^{-2}$ at 1173 K could be obtained. Therefore, the highest $ZT \sim 0.3$ at 1173 K was achieved for the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.01}\text{O}_{1.015}$ sample, and it has so far one of the highest ZT values among those reported for ZnO based thermoelectric materials over the temperature range, e.g., its ZT value at 300 K, which is 0.012, is over 1 order of magnitude higher than that of the state-of-the-art nanostructured Al-doped ZnO, which is 0.0013. It suggests that this material is a good candidate for improving the overall conversion efficiencies in oxide thermoelectric modules. Meanwhile, Sc-doped ZnCdO is robust in air at high temperatures, whereas other n-type materials, such as Al-doped ZnO, will experience rapid degradation of their electrical conductivity and ZT .

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Introduction

Thermoelectric (TE) technology is a promising energy-conversion technology. TEs directly convert heat into electricity without any moving parts. Such a reliable and maintenance-free technology has already been used as a crucial long-life power source for space needs since the 1950s.¹ In civil use, TEs offer a promising solution for waste heat recovery.² Several classes of thermoelectric materials are being investigated for renewable power generation applications including tellurides,^{3,4} half-Heuslers,^{5,6} silicides,^{7,8} and oxides.⁹ The integration of TE generators can improve the overall energy efficiency of many systems, such as automobiles, fossil fuel power stations, and solar panels. For industrial processes, including those involving petroleum production, steel manufacturing, and transportation, exploitable high temperature (above 800 K) waste heat is abundant. Thus, TE systems consisting of materials with decent TE properties that are stable at high temperatures are needed. Here thermoelectric materials based on oxides are promising candidates because of their potential high-temperature chemical stability, abundant resources, and low-cost processing.⁹

The current state-of-the-art oxide TE materials are p-type calcium cobaltates,^{10,11} n-type strontium titanates (STO),^{12,13} n-type aluminum-doped zinc oxide (AZO),^{14,15} and n-type calcium manganates (CMO).^{16–19} Promising ZT values of 0.61 at 1118 K and reliable thermal stability have been achieved for p-type calcium cobaltates.¹¹ However, the current n-type candidate oxides still suffer from either relatively low ZT or poor stability.⁹ ZnO based TE materials experience severe degradation of their electrical conductivity during operation in air above 600 K because of the decrease in the donor concentrations.²⁰ STOs have also been reported to be unstable in air above 670 K because the Ti^{3+} in STO is unstable and is readily oxidized to Ti^{4+} , thus, the ZT will decrease strongly in air above 670 K.⁹ CMO is a good candidate high-temperature material, but its ZT value is still much lower than those of the best n-type oxide materials.^{21,22} Therefore, better n-type oxide candidate materials are needed for the construction of oxide TE modules with sufficiently high energy-conversion efficiencies.

The integration of nanostructuring into ZnO-based TEs has emerged as a popular topic since 2010.^{23–26} The AZO nanocomposites sintered using nano-precursors have achieved an ultra-low thermal conductivity of $2.8 \text{ W m}^{-1} \text{ K}^{-1}$ at room temperature.²⁴ Although nanostructuring has been demonstrated to be useful for reducing the thermal conductivity of AZO, strong degradation of the electrical conductivity was also observed.²⁶ As a result, the nanostructuring of AZO was only useful for achieving a high peak ZT at high temperature, but near room temperature, ZT is usually lower than that of bulk samples because of lower electrical conductivity.^{24,25} In contrast,

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† Electronic supplementary information (ESI) available: Calculated results from Rietveld refinements of XRD spectra, parameters used for the Callaway model, calculated phonon density of states by DFT calculation, and supplement TE properties. See DOI: 10.1039/c6ta03126a



band-gap engineering methods, such as alloying, have also been intensively utilized to optimize TE materials.^{27–30}

The ternary compound ZnCdO, which was synthesized by alloying ZnO with CdO, has already been investigated for its electronic structure, phase stability and optical properties.^{31–33} However, the TE properties of ZnCdO have never been reported before. By experimentally screening the external carrier donor dopants, we selected Sc as the adequate dopant and developed scandium doped zinc cadmium oxide as a new n-type oxide compound for high temperature TE application. This material not only has superior *ZT* values to the conventional AZO, but more importantly it also has much better long-term stability in air at high temperatures, where the current state-of-the-art AZO is not suitable.

Experimental

Preparation of samples

Doped zinc cadmium oxide ($\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_y\text{O}_{1+1.5y}$) was obtained by conventional solid-state-reaction (SSR) methods from the starting powders of ZnO, CdO, and Sc_2O_3 . The powders were mixed at different molar ratios by ball milling using ceramic balls for 24 h. The resulting mixtures were then uniaxially pressed with a Φ 20-mm stainless steel die at 65 MPa for 60 s, followed by isostatic pressing at 5 GPa for 60 s. The compressed pellets were sintered in a chamber furnace with a heating and cooling rate of 1 K min^{-1} at $850 \text{ }^\circ\text{C}$ for 24 h in air and then at $1300 \text{ }^\circ\text{C}$ for 5 h in air to maintain the oxygen stoichiometry. The sintered materials reached relative densities above 98%. The sintered bulk materials were then cut into desired configurations and dimensions with a diamond cutter and subjected to TE characterization. The TE anisotropy of the samples was ignored because of the minor TE anisotropic nature of hexagonal ZnO and the randomized grain orientations in this study.³⁴

Characterization

The electrical conductivity (σ) and Seebeck coefficient (S) were measured simultaneously using a ULVAC-RIKO ZEM-3 under 0.1 bar of helium from room temperature to 1173 K. A homemade rig was used for the measurement of electrical conductivity (σ) using the four probe method in air from room temperature up to 1073 K. Hall measurements were carried out at room temperature using the van der Pauw method with a superconducting magnet (measured up to 2 T). The thermal conductivity (κ) was determined from the thermal diffusivity (α), the mass density (D_m) and the specific heat capacity (C_p) according to the equation $\kappa = \alpha D_m C_p$. The thermal diffusivity was obtained by the laser flash method (Netzsch LFA-457, Germany), the mass densities of the samples were measured by Archimedes' method using water with a surfactant, and the specific heat capacities were estimated using the Dulong–Petit law. The errors in the measurements of σ , S , and κ are $\pm 5\%$, $\pm 5\%$, and $\pm 7\%$, respectively. X-ray diffraction (XRD) measurements were collected using a Bruker D8 diffractometer (Bruker, Germany) with Cu-K α radiation. A scanning electron microscope (SEM, Supra; Carl Zeiss, Inc., Germany) was used to

observe the microstructures of the samples. Transmission electron microscopy (TEM) imaging and dark field scanning transmission electron microscopy (STEM) were performed in combination with electron-dispersive spectroscopy (EDS) by using a JEM 3000F equipped with a field emission gun (FEG) operated at 300 kV, a high annular angle dark field (HAADF) STEM detector, and an Oxford Instruments EDS detector with an ultra-thin window. The HAADF STEM analysis was performed with a nominal probe size of 1 nm.

Results and discussion

Structural properties

Sc-doped ZnCdO samples with various amounts of Cd were investigated using XRD. For $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples, the main crystalline structure of this material appears to be similar to the wurtzite structure of pure ZnO belonging to the $P6_3mc$ space group, as shown in Fig. 1. For samples with $x = 0.125$ and 0.15, the secondary phase can be observed by the peaks marked with ‘*’ in Fig. 1a. These peaks are identical to those of pure CdO. Thus, once the molar ratio of CdO and ZnO exceeds 1 : 9, the excess CdO phase cannot be fully incorporated into ZnO under the current sintering conditions. When the ratio is below 1 : 9, CdO can be thoroughly incorporated into the wurtzite ZnO phase, as previously observed by Venkatachala-pathy *et al.*³³ As the Cd concentration increases, the main peaks shift slightly to the left (Fig. 1a), and the unit cell volumes increase accordingly (Fig. 1b). This is because the ionic radius of Cd^{2+} (0.078 nm, 4-fold coordination) is larger than that of Zn^{2+} (0.06 nm, 4-fold coordination). The Cd substitution at Zn sites will expand the unit cell volume. For samples with $x = 0, 0.05$ and 0.1, the Sc_2O_3 phase belonging to the $I2_13$ space group is indicated by a weak peak marked with ‘○’ in Fig. 1a, suggesting that Sc substitutions were located mainly at the Cd sites instead of the Zn sites. Table S1 in the ESI† gives the detailed parameters obtained from Rietveld refinement of the XRD patterns.

The XRD patterns of $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0$ to 0.04) samples are presented in Fig. 2a and show that the main crystalline structure is still wurtzite ($P6_3mc$ space group). For $y = 0.02, 0.03$ and 0.04, the secondary Sc_2O_3 phase that belongs to the $I2_13$ space group is indicated by weak peaks marked with

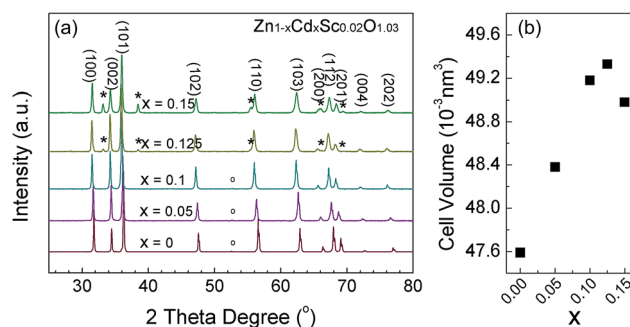


Fig. 1 (a) The XRD patterns of $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples. (b) Refined unit cell volume of the primary phase plotted as a function of Cd composition.



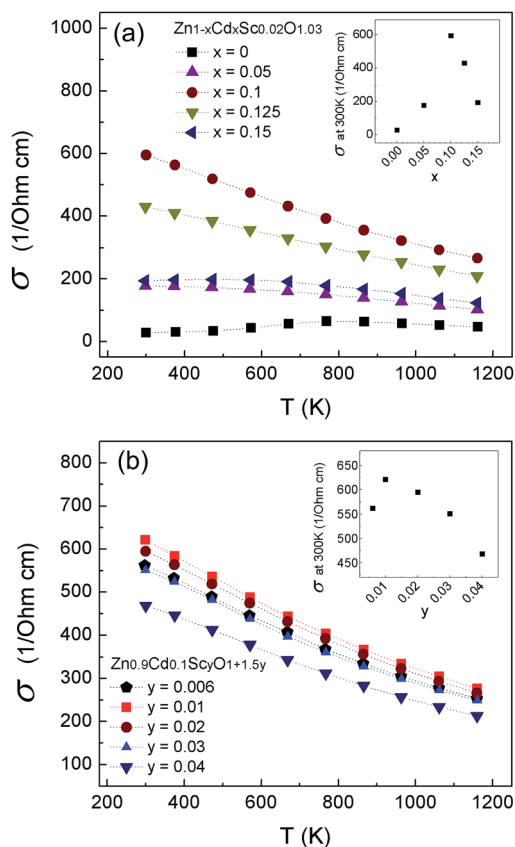


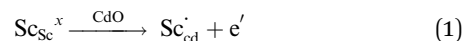
Fig. 5 Temperature dependence of the electrical conductivity σ for (a) $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples and (b) $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples.

is consistent with the XRD results. Sc is not likely to be homogeneously distributed. Instead, Sc segregates into separate particles (Fig. 4b), which is consistent with the observation of the I_{213} secondary phase from XRD spectra. However, Sc concentrations in the other areas are very low, indicating a low Sc solubility in CdO or ZnO.

Thermoelectric properties

The electrical conductivities (σ) of the $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples are shown in Fig. 5a. The $\text{ZnSc}_{0.02}\text{O}_{1.03}$ sample exhibited the lowest conductivity with mixed

conduction characteristics. As the Cd concentration increased, the corresponding σ values also increased. This is because according to XRD results, CdO addition provides substitution sites for Sc, so that the process expressed by



provides free carriers to the system, thereby increasing the conductivity. The highest conductivity was observed for the sample with $x = 0.1$, which exhibited metallic conduction behaviour. Further increasing the Cd content resulted in a decrease in σ (inset of Fig. 5a). This may be explained by the phase separation of CdO and the deterioration of the carrier mobility by increased grain boundary scattering and defect scattering. Such explanations were verified by the hall measurement results which are shown in Table 1 and will be discussed later. The influences of the Sc concentration on the electrical conductivity (σ) for the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples are shown in Fig. 5b. All the samples in this group show metallic conductivity. When $y = 0.01$, the conductivity is highest, which is comparable to that of the best Al doped ZnO bulk materials.³⁵ As y increased beyond 0.01 , the conductivity decreased (inset of Fig. 5b). This may be explained by the precipitation of the I_{213} secondary phase and the increased grain boundary scatterings.

Fig. 6 shows the temperature dependence of the samples' Seebeck coefficients (S). Their negative S values indicated n-type conduction. Additionally, the monolithically increasing absolute S values with increasing temperature suggested the thermal excitation of electrons and the negligible contribution from bipolar conduction. Fig. 6a shows that the $\text{ZnSc}_{0.02}\text{O}_{1.03}$ sample had the highest $|S|$ because it had the lowest carrier concentration n (Table 1). The addition of Cd severely lowered the $|S|$ by significantly increasing n . However, increasing the effective mass m^*/m_e had a positive effect, preventing $|S|$ from becoming too low. When $x = 0.1$, $|S|$ is still much higher than that of our previous AZO sample²⁶ which has a similar n . Fig. 7b shows the temperature dependence of the Seebeck coefficients, S , of the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples. The $|S|$ values for all samples were found to be very similar. The $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ sample had a slightly higher $|S|$ value than the other compositions. The inset of Fig. 7b shows the plot of S at room temperature vs. y for the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$.

Table 1 Electrical transport properties at room temperature

Sample		σ ($1/\Omega \text{ cm}^{-1}$)	S ($\mu\text{V K}^{-1}$)	n (10^{19} cm^{-3})	μ ($\text{cm}^2 \text{ V}^{-1} \text{ s}^{-1}$)	D.O.S. effective mass (m^*/m_e)
$\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$	$x = 0$	28.1	-194	0.24	71.6	0.19
	$x = 0.05$	177	-60.1	3.52	31.4	0.33
	$x = 0.1$	595	-70.6	5.61	66.2	0.53
	$x = 0.125$	429	-72.5	5.99	44.8	0.56
	$x = 0.15$	193	-58.1	5.48	22.1	0.42
$\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$	$y = 0.01$	621	-73.9	5.84	67	0.57
	$y = 0.02$	595	-70.6	5.61	66.2	0.53
	$y = 0.03$	552	-76.5	6.02	57.2	0.59
	$y = 0.04$	469	-84.1	4.71	62	0.56



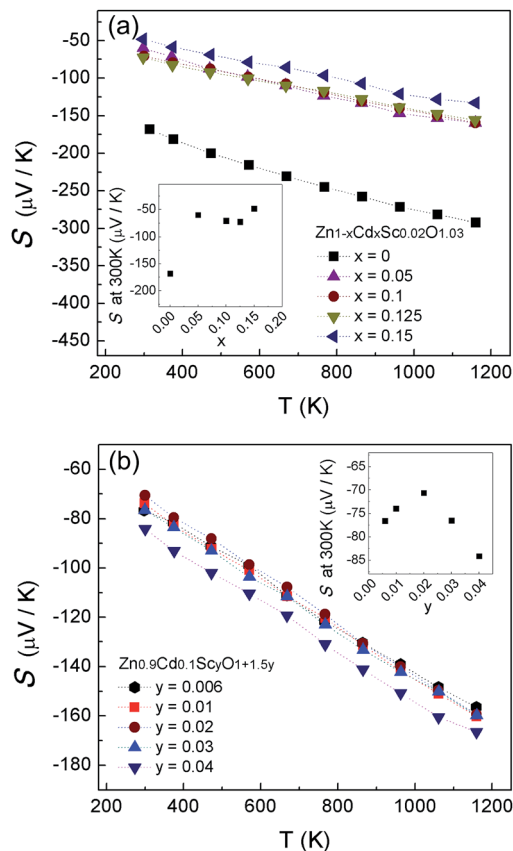


Fig. 6 Temperature dependence of the Seebeck coefficient S for (a) $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples and (b) $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples.

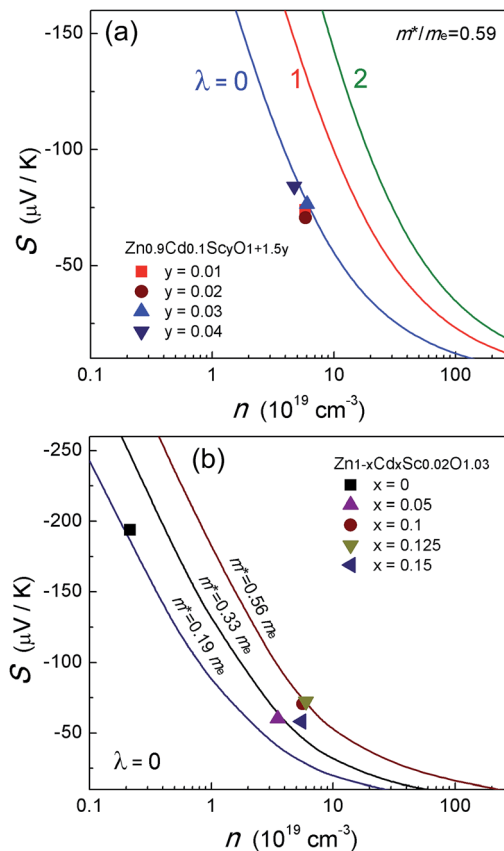


Fig. 7 Room temperature Seebeck coefficient S plotted as a function of carrier concentration n for (a) $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.01$ to 0.04) samples, and (b) $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples. The solid colored lines represent the calculated values based on (a) scattering mechanisms with $m^*/m_e = 0.59$ and (b) effective mass with $\lambda = 0$.

A room-temperature Hall measurement was conducted to determine the carrier concentration (n), and the results are presented in Table 1 together with the results for other electrical transport properties. The effective mass (m^*/m_e) was obtained according to the Pisarenko relation, as discussed previously.²⁶ The addition of Cd increased n to the order of 10^{19} cm^{-3} without severely decreasing μ . For $x = 0.1$, μ was maintained at $66.2 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$, which is comparable or higher than the value obtained for the AZO samples.^{24–26} In contrast, m^*/m_e was notably increased by increasing Cd from 0.19 for $\text{ZnSc}_{0.02}\text{O}_{1.03}$ to 0.53 for $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$, and the latter's value exceeded that of $\text{ZnAl}_{0.02}\text{O}_{1.03}$ (~ 0.4).²⁶ However, the addition of excessive Cd, e.g., $x = 0.15$, resulted in a reverse effect, lowering the n , μ , and m^*/m_e values, which is not desirable. Changing the Sc concentration from 0.01 to 0.04 had a much smaller effect on the transport properties than changing the Cd content. n and μ were found to be relatively stable with only minor fluctuations. Using the n and m^*/m_e values shown in Table 1, a simple parabolic band model¹ can be applied to describe the carrier density and Seebeck coefficient:

$$F_\lambda(\xi) = \int_0^\infty \frac{x^\lambda dx}{1 + \exp(x - \xi)} \quad (2)$$

$$S = -\frac{k_B}{q} \left[\frac{(2 + \lambda)F_{\lambda+1}}{(1 + \lambda)F_\lambda} - \xi \right] \quad (3)$$

$$n = 4\pi \left(\frac{2m^*k_B T}{h^2} \right)^{3/2} F_{1/2} \quad (4)$$

where $F_\lambda(\xi)$ is the Fermi integral and ξ is the reduced electrochemical potential. λ is a scattering parameter which takes the value 0 for acoustic phonon scattering, 1 for optical phonon scattering, and 2 for ionized impurity scattering.¹ Fig. 7 shows S as a function of n at room temperature. In Fig. 7a, the S values for $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.01$ to 0.04) samples correspond very well to $\lambda = 0$, indicating that acoustic phonon scattering is the dominant scattering mechanism. In Fig. 7b, the three lines correspond to the three different m^* values obtained assuming that acoustic phonon scattering is the dominant scattering mechanism. A clear increase of m^* with increasing x can be observed. Given that their μ values are comparable, according to the band theory,²⁷ it is reasonable to suggest that the increase of m^* arises from the convergence of the conduction bands in $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0.05$ to 0.15). However, further investigations are needed to confirm this hypothesis.



Fig. 8 shows the power factor ($S^2\sigma$) of the samples. For the $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples shown in Fig. 8a, the highest $S^2\sigma$ values were obtained for $x = 0.1$ because of the well-maintained μ and adequately increased n and m^* . Further increasing x decreased $S^2\sigma$. For the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples, the change in $S^2\sigma$ with changing y was not as pronounced as that with changing x . Among the tested values, the highest power factor of $\sim 7.1 \times 10^{-4} \text{ W m}^{-1} \text{ K}^{-2}$ at 1173 K was achieved for $y = 0.01$; this value is comparable to that of the conventional AZO.²⁶

Fig. 9a shows the total thermal conductivity as a function of temperature for the $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples. For $x = 0$, $\text{ZnSc}_{0.02}\text{O}_{1.03}$ shows a high thermal conductivity similar to those of pure ZnO and AZO.³⁵ The addition of Cd effectively reduced the thermal conductivity by alloy scattering. The $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ sample showed 7-fold lower thermal conductivity than the $\text{ZnSc}_{0.02}\text{O}_{1.03}$ sample. The decrease in the thermal conductivity with increasing Cd concentration continued to a minimum of $\sim 2.5 \text{ W m}^{-1} \text{ K}^{-1}$ at 1173 K ($x = 0.125$). Further increasing the Cd content had a reverse effect on the thermal conductivity values, presumably because of phase separation. The small κ values obtained for the $\text{Zn}_{0.875}\text{Cd}_{0.125}\text{Sc}_{0.02}\text{O}_{1.03}$ sample are comparable to or even smaller than those previously reported for the AZO nanocomposites (κ values between 2 and $3.5 \text{ W m}^{-1} \text{ K}^{-1}$ at 1173 K).²⁴⁻²⁶ The lattice

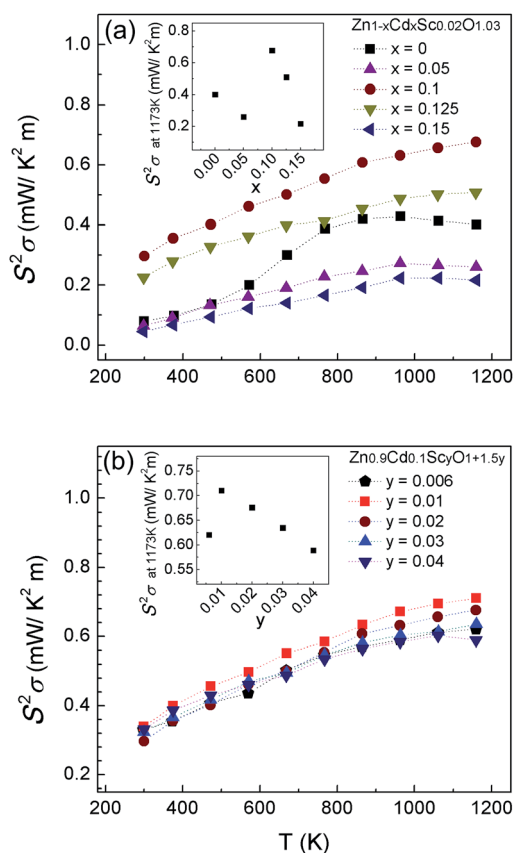


Fig. 8 Temperature dependence of the power factor $S^2\sigma$ for (a) $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples, and (b) $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples.

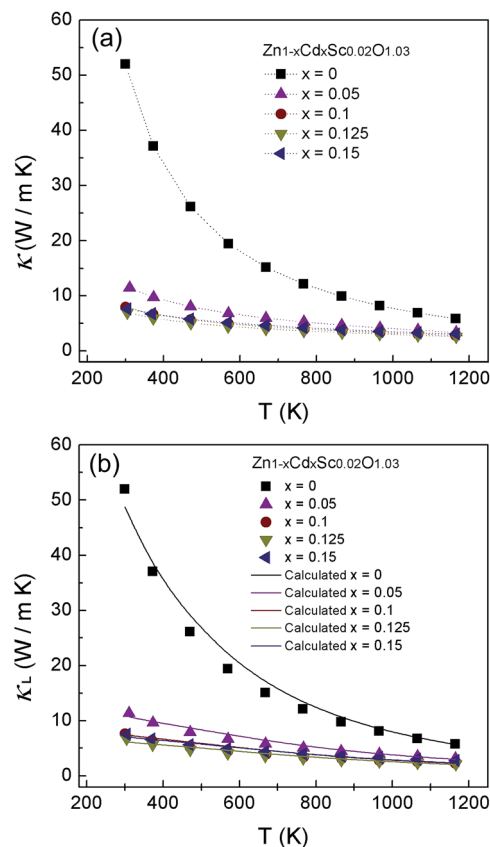


Fig. 9 Temperature dependence of (a) the total thermal conductivity κ and (b) the lattice thermal conductivity κ_L for $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples. The solid lines in (b) represent values calculated using a Debye–Callaway model.

contribution κ_L to the total κ was estimated using a reduced Lorenz number of $1.8 \times 10^{-8} \text{ W}\Omega\text{K}^{-2}$. The extracted κ_L values are shown in Fig. 9b. The values of κ_L are somewhat similar to the values of κ , indicating that the lattice component dominates the thermal conductivity for all the samples. The Debye–Callaway model³⁶⁻³⁹ was used to calculate the lattice thermal conductivity as follows:

$$\kappa_L = \frac{k_B}{2\pi^2\nu} \left(\frac{k_B T}{\hbar} \right)^3 \times \left\{ \int_0^{\theta/T} \frac{\tau_c x^4 e^x}{(e^x - 1)^2} dx + \frac{\left[\int_0^{\theta/T} \frac{\tau_c}{\tau_N} \frac{x^4 e^x}{(e^x - 1)^2} dx \right]^2}{\int_0^{\theta/T} \frac{1}{\tau_N} \left(1 - \frac{\tau_c}{\tau_N} \right) \frac{\tau_c x^4 e^x}{(e^x - 1)^2} dx} \right\} \quad (5)$$

where k_B is the Boltzmann constant, ν is the speed of sound, \hbar is the reduced Planck's constant, x is the normalized frequency $\hbar\omega/k_B T$, T is the absolute temperature, and θ is the Debye temperature. τ_c is the combined relaxation time calculated using Mathieson's rule as follows:

$$\tau_c^{-1} = \tau_{\text{pad}}^{-1} + \tau_N^{-1} + \tau_B^{-1} \quad (6)$$



where τ_c is composed of alloy point defect scattering τ_{pad} , normal phonon–phonon scattering τ_N , and boundary scattering τ_B . The relaxation time for these scattering mechanisms is calculated from the following relations:

$$\tau_{\text{pad}}^{-1} = A\omega^4 = \alpha T^4 x^4 \quad (7)$$

$$\tau_N^{-1} = BT^3 \omega^2 = \beta T^5 x^2 \quad (8)$$

$$\tau_B^{-1} = v/L \quad (9)$$

where A , B , α and β are the scattering strength-related parameters, ω is the phonon frequency, and L is the average grain size values. The parameters used for the calculations are listed in Table S3 in the ESI.† The calculated results are shown as solid lines in Fig. 9b. The calculations indicated that the reduction of the thermal conductivity was mainly caused by point defect scattering or alloy scattering, indicating that adding CdO results in oxide alloys with ZnO. The grain size also influences the reduction of the thermal conductivity, but its influence is quite small compared to that of alloy scattering.

Fig. 10a shows the thermal conductivity as a function of temperature for the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples. Varying the Sc concentration in this range exerted a small effect on the thermal conductivity. All samples in this

group have comparable thermal conductivities. As the Sc concentration increased, the thermal conductivity slightly decreased, and the lowest κ value was obtained for $y = 0.04$. The lattice contribution κ_L to the total κ was estimated and is shown in Fig. 11b. The values of κ_L remain similar to the values of the total conductivity. The calculated values are shown as solid lines in the figure.

To elucidate the mechanism of the alloy scattering based reduction of lattice thermal conductivity, the phonon mean free path (MFP) was plotted against the normalized phonon frequency ($\hbar\omega/k_B T$) according to the Debye–Callaway model, as shown in Fig. 10. At 300 K, most of the phonon spectrum, especially in the lower-frequency region, was reduced significantly as x increased from 0 to 0.1, providing a good explanation for the 7-fold-smaller thermal conductivity obtained for the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ sample compared to that of the $\text{ZnSc}_{0.02}\text{O}_{1.03}$ sample (Fig. 11a). At 1173 K, the effect of alloy scattering remains quite pronounced because of the depression of the phonon spectrum in the intermediate- and high-frequency regions (Fig. 11b). Additionally, density functional theory (DFT) calculations of phonon density of states (DOS) spectra were performed for these samples. A clear red shift relative to ZnO and the occurrence of low-energy phonons were observed for $\text{Zn}_{0.875}\text{Cd}_{0.125}\text{O}$. These results revealed the signature of phonon glass formed by alloying Cd into ZnO (Fig. S1 in the ESI†).

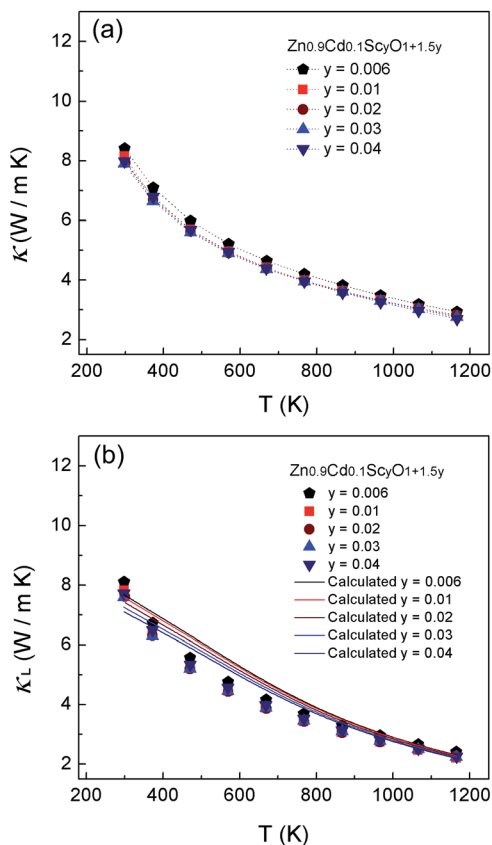


Fig. 10 Temperature dependence of (a) the total thermal conductivity κ and (b) the lattice thermal conductivity κ_L for $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples. The solid lines in (b) represent values calculated using a Debye–Callaway model.

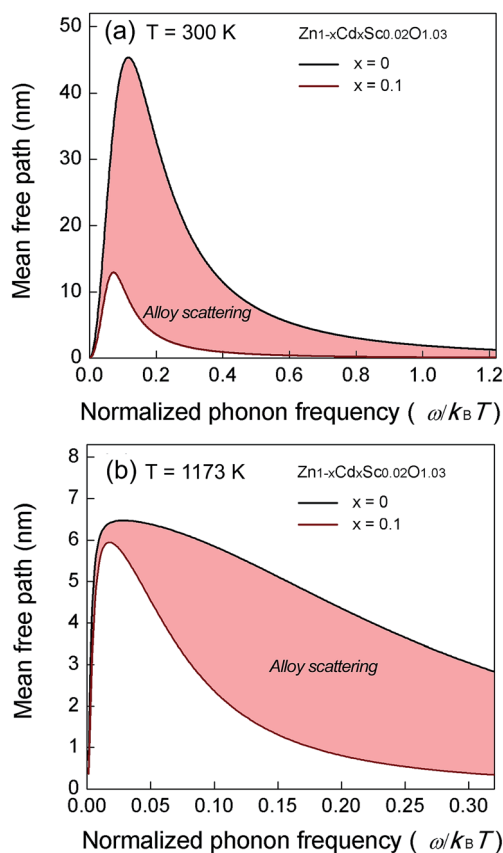


Fig. 11 The phonon MFP vs. normalized phonon frequency ($\hbar\omega/k_B T$) at (a) 300 K and (b) 1173 K according to the Debye–Callaway model.



The values for the ZT figure of merit are shown in Fig. 12. When $x = 0$, the peak ZT value at 1173 K for the $\text{ZnSc}_{0.02}\text{O}_{1.03}$ sample is only 0.075, even lower than that previously obtained for the AZO;⁴⁰ when $x = 0.1$, the peak ZT value at 1173 K for $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ was increased to 0.28, corresponding to an improvement by a factor of 2.73. Further increasing the Cd concentration only decreased the obtained ZT values. Clearly, adding Cd significantly influences the ZT . In Fig. 12b, the ZT values for $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples are quite similar. Despite the error bar for the ZT values ($\sim 30\%$), $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ achieved the highest peak ZT value: 0.3 at 1173 K. Comparing the ZT of $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ to our previous results for AZO^{26,40} and the state-of-the-art AZO from literature results^{24,25,35,41} shows that $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.01}\text{O}$ has one of the highest currently known ZT values over a range of temperatures among ZnO based TE materials, *e.g.*, its ZT value of 0.012 at 300 K is over 1 order of magnitude higher than that (0.0013) obtained for the state-of-the-art nanostructured AZO.^{24,25} Thus, this material is a good candidate for improving the overall conversion efficiencies in oxide TE modules.

Engineering power factor and figure of merit ZT

An engineering power factor $(\text{PF})_{\text{eng}}$ and a dimensionless engineering figure of merit $(ZT)_{\text{eng}}$ were defined by Ren *et al.* as

$$(ZT)_{\text{eng}} = Z_{\text{eng}}\Delta T = \frac{\left(\int_{T_c}^{T_H} S(T)dT\right)^2 \int_{T_c}^{T_H} \sigma(T)dT}{\int_{T_c}^{T_H} \kappa(T)dT} \Delta T$$

$$= \frac{(\text{PF})_{\text{eng}}}{\int_{T_c}^{T_H} \kappa(T)dT} \Delta T,$$

where T_H is the hot side temperature, T_c is the cold side temperature, and ΔT is the temperature difference between the cold and hot sides. The as-defined $(\text{PF})_{\text{eng}}$ and $(ZT)_{\text{eng}}$ can reliably predict the output power and practical conversion efficiency, respectively, thereby preventing the reporting of unrealistic efficiency values using average ZT values and complex numerical simulations. Therefore, the $(\text{PF})_{\text{eng}}$ and $(ZT)_{\text{eng}}$ for the new $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ material were calculated and compared with those for the other state-of-the-art AZO samples, as shown in Fig. 13. $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ shows the highest $(\text{PF})_{\text{eng}}$ because of its superior electrical transport properties relative to the AZO, although the bulk AZO⁴⁰ shows a higher peak PF at 1173 K than the new materials. Compared to the other AZO nanocomposites, this improvement was even more substantial. When $T_H = 1173$ K, the $(\text{PF})_{\text{eng}}$ of $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ was ~ 0.5 $\text{W m}^{-1} \text{K}^{-1}$, whereas that of the AZO nanocomposite was ~ 0.05 – 0.15 $\text{W m}^{-1} \text{K}^{-1}$. Fig. 13b shows the $(ZT)_{\text{eng}}$ of these samples as a function of T_H . The AZO nanocomposite exhibited higher $(ZT)_{\text{eng}}$ than the AZO bulk samples. When $T_H = 1173$ K, the $(ZT)_{\text{eng}}$ of the AZO nanocomposite was higher than that of the AZO bulk by a factor of ~ 2 , whereas the new $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.1}\text{O}_{1.15}$ showed ~ 10 times-higher $(ZT)_{\text{eng}}$ than the AZO bulk, suggesting that the new material has a significantly enhanced practical conversion efficiency compared to the conventional AZO materials.

High temperature stability in air

One of the most striking advantages of this newly developed material is its stability in air. For a long time, ZnO based materials, such as AZO, have suffered from electrical conductivity degradation in air at high temperatures. Such degradation is related to the elimination of intrinsic electron donor defects within ZnO, such as oxygen vacancies V_{O} , zinc interstitials, Zn_i , and zinc antisites, Zn_o . The formation of these point defects follows these general reaction equations:⁴³

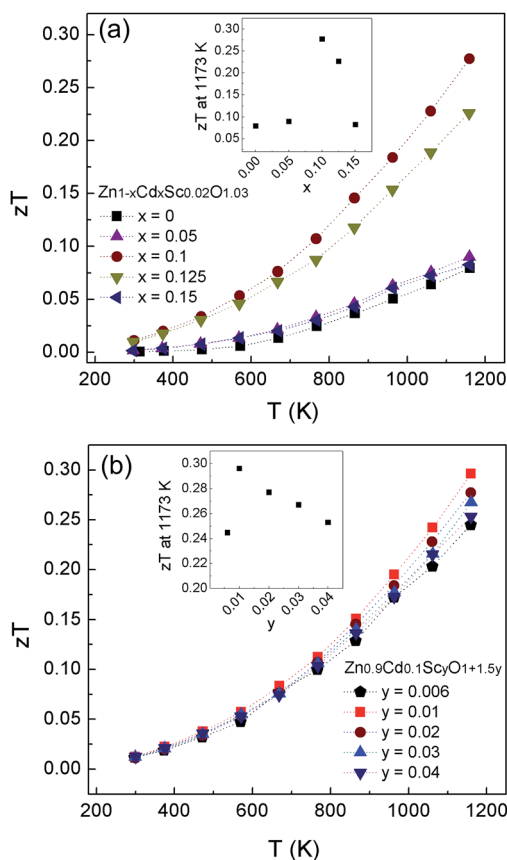
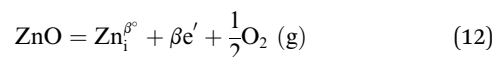
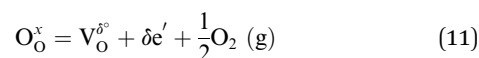


Fig. 12 Temperature dependence of the figure of merit ZT for (a) $\text{Zn}_{1-x}\text{Cd}_x\text{Sc}_{0.02}\text{O}_{1.03}$ ($x = 0$ to 0.15) samples and (b) $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_y\text{O}_{1+1.5y}$ ($y = 0.006$ to 0.04) samples.



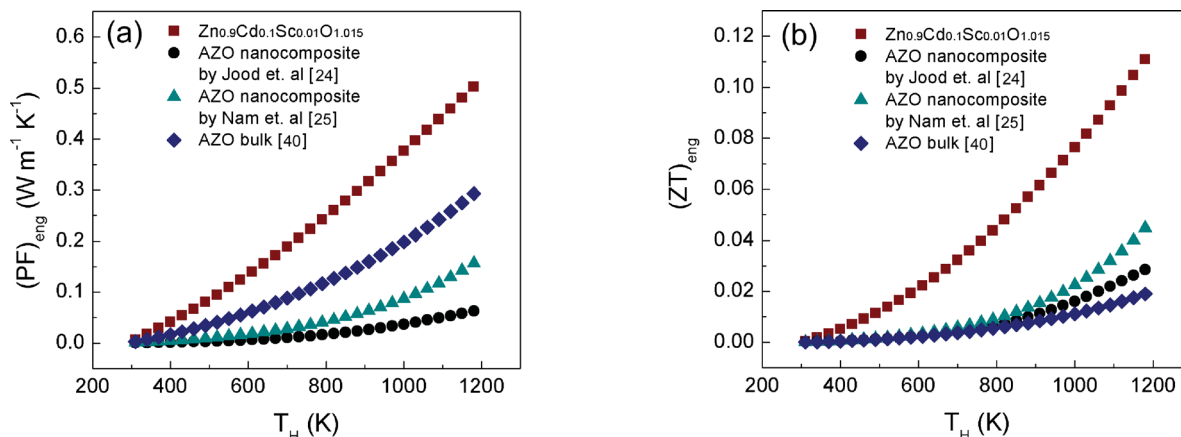
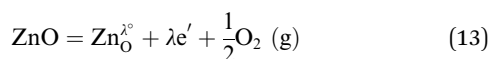


Fig. 13 Comparison of $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.01}\text{O}_{1.015}$ with other AZO materials reported in the literature^{24,25,40} in terms of (a) the engineering power factor $(\text{PF})_{\text{eng}}$ and (b) the engineering figure of merit $(\text{ZT})_{\text{eng}}$, as a function of hot side temperature T_{H} . The cold side temperature T_{C} is 300 K.



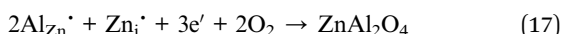
where δ , β , $\lambda = 1$ or 2 , and the equilibrium constants of reactions (11)–(13) can be obtained using the mass action law, as expressed by the following equations:

$$K_{(V_{\text{O}}^{\delta})}^{\text{f}} = [V_{\text{O}}^{\delta}] [e']^{\delta} P_{\text{O}_2}^{1/2} \quad (14)$$

$$K_{(\text{Zn}_{\text{i}}^{\beta})}^{\text{f}} = [\text{Zn}_{\text{i}}^{\beta}] [e']^{\beta} P_{\text{O}_2}^{1/2} \quad (15)$$

$$K_{(\text{Zn}_{\text{O}}^{\delta})}^{\text{f}} = [(\text{Zn}_{\text{O}}^{\delta})] [e']^{\lambda} P_{\text{O}_2}^{1/2} \quad (16)$$

where P_{O_2} represents the partial pressure of oxygen in the system. From these equations we can see that the probabilities of forming oxygen vacancies, zinc interstitials, and zinc antisite defects are all related to the partial pressure of oxygen in the system. The charge carrier concentrations are also directly related to these reactions. Moreover, the dopant impurities, for example, $\text{Al}_{\text{Zn}}^{\cdot}$, $\text{Zn}_{\text{i}}^{\cdot}$, also undergo a reaction with oxygen by:



in which ZnAl_2O_4 is a non-conducting spinel phase,⁴⁰ the same as ZnGa_2O_4 in Ga-doped ZnO. According to previous investigations,⁴⁴ Zn antisites and Zn interstitials are the main source of free electrons in doped ZnO. However, when heated at an elevated temperature with excessive oxygen, Zn antisites and Zn interstitials undergo chemical reactions and form insulating secondary phases such as ZnAl_2O_4 and ZnGa_2O_4 . Therefore the Ga and Al-doped ZnO work usually at a semi-stable state with defects, for example, sintered in nitrogen. After curing with oxygen at high temperature, their carrier density would dramatically decrease and therefore they are not suitable for high temperature thermoelectrics in air.

In contrast, the new material bypasses the problem by introducing Cd and Sc dopants, a majority of the donors are from the Sc replacing Cd, $\text{Sc}_{\text{Cd}}^{\cdot}$, and there are no irreversible chemical reactions that will lead to the formation of insulating

phases, as previously discussed in eqn (1). To verify its stability, an *in situ* measurement of the electrical conductivity σ in air was performed for the new $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ and the conventional $\text{Zn}_{0.98}\text{Al}_{0.02}\text{O}_{1.03}$ samples from our previous work⁴⁰ to compare their thermal stability, as shown in Fig. 14. Both samples were treated with two heating and cooling cycles up to 1073 K in air over approximately 48 hours. $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ showed stable σ compared to $\text{Zn}_{0.98}\text{Al}_{0.02}\text{O}_{1.03}$, whereas the latter's σ decreased by more than 1 order of magnitude after the cycles, consistent with the observations of Schäuble *et al.*⁴⁵

The TE long-term stability was also tested by annealing the samples in air at 1073 K for 72 h in a muffle furnace with the TE properties of $\text{ZnAl}_{0.2}\text{O}_{1.03}$ and $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ measured before and after the annealing. The figure of merit ZT before and after annealing is shown in Fig. 15. A slight degradation of $ZT \sim 5\%$ occurred in the $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ sample after 72 h of annealing in air despite the errors, whereas the $\text{Zn}_{0.98}\text{Al}_{0.02}\text{O}_{1.03}$ sample showed extremely large degradation (up to $\sim 90\%$). Changes in the electrical transport properties constituted the major reason for the change in the ZT , because the change in the lattice thermal conductivity was negligible.

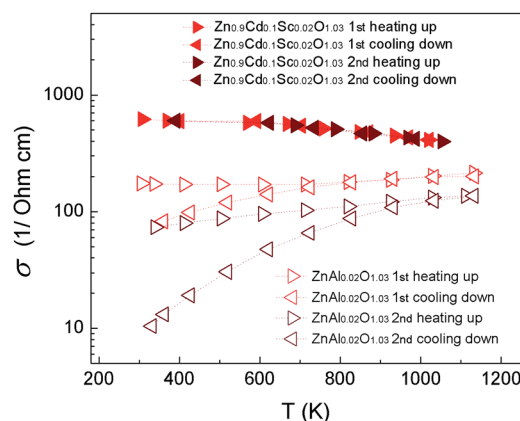


Fig. 14 Electrical conductivity σ of $\text{Zn}_{0.9}\text{Cd}_{0.1}\text{Sc}_{0.02}\text{O}_{1.03}$ and $\text{Zn}_{0.98}\text{Al}_{0.02}\text{O}_{1.03}$ samples⁴⁰ during heating and cooling cycles in air.



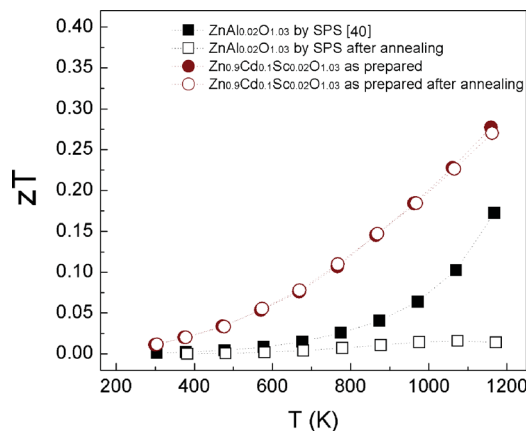


Fig. 15 Temperature dependence of the figure-of-merit ZT for $Zn_{0.9}Cd_{0.1}Sc_{0.02}O_{1.03}$ and $Zn_{0.98}Al_{0.02}O_{1.03}$ samples⁴⁰ before and after annealing for 72 h at 1073 K in air.

The TE properties of the samples, both before and after the annealing, are concluded in Fig. S2 in the ESI†. The degradation of $ZnAl_{0.02}O_{1.03}$ is mainly attributable to the elimination of donor defects such as zinc interstitials and oxygen vacancies, and can be simply observed by the changes in the samples' colour. In Fig. 16a and c, the $ZnAl_{0.02}O_{1.03}$ sample appeared dark after SPS in a vacuum, but after annealing in air at 1073 K for 72 h, the segment turned light yellow, indicating a significant change in its electrical properties. In contrast, in Fig. 16b and d, the $Zn_{0.9}Cd_{0.1}Sc_{0.02}O_{1.03}$ sample sintered in air retained its dark greenish colour after annealing in air at 1073 K for 72 h. Nevertheless, the stability of the material under working conditions in a large temperature gradient (>500 K) in air should be further investigated.

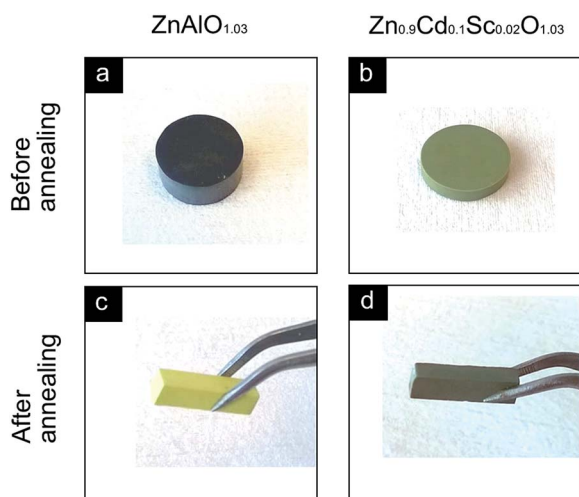


Fig. 16 Photographs of (a) a bulk pellet of $ZnAl_{0.02}O_{1.03}$ sintered by spark plasma sintering in a vacuum, (b) a bulk pellet of $Zn_{0.9}Cd_{0.1}Sc_{0.02}O_{1.03}$ sintered in air, (c) a cuboid segment of $ZnAl_{0.02}O_{1.03}$ after annealing in air at 1073 K for 72 h, (d) a cuboid segment of $Zn_{0.9}Cd_{0.1}Sc_{0.02}O_{1.03}$ after annealing in air at 1073 K for 72 h.

Conclusions

The TE properties of newly developed Sc-doped $ZnCdO$ materials were systematically investigated. The $Zn_{0.9}Cd_{0.1}Sc_{0.01}O_{1.03}$ sample showed the highest ZT (~ 0.3 at 1173 K and ~ 0.24 at 1073 K) and a good engineering ZT that was significantly higher than those of the nanostructured AZO materials. These superior ZT values can be attributed to the alloying of CdO with ZnO , which significantly reduced the lattice thermal conductivity. Meanwhile, the alloying of CdO increased the DOS effective mass without decreasing the carrier mobility. After tuning the carrier concentration, a large power factor of $\sim 7.1 \times 10^{-4} \text{ W m}^{-1} \text{ K}^{-1}$ was obtained. Meanwhile, Sc-doped $ZnCdO$ is robust in air at high temperatures up to 1073 K for 72 h, and its TE performance is retained after heating and cooling cycles in air. In contrast, other ZnO based TE materials, such as AZO, experience rapid degradation of their TE performances. Overall, the Sc-doped $ZnCdO$ material represents a new and promising n-type material with superior properties for high-temperature TE applications.

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