1 Chondrites as samples of differentiated planetesimals

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1 ABSTRACT

2 Chondritic meteorites are unmelted and variably metamorphosed aggregates of the earliest solids of the solar system. The variety of metamorphic textures in 3 chondrites motivated the "onion shell" model in which chondrites originated at 4 5 varying depths within a parent body heated primarily by the short-lived radioisotope ²⁶Al, with the highest metamorphic grade originating nearest the 6 center. Allende and a few other chondrites possess a unidirectional magnetization 7 8 that can be best explained by a core dynamo on their parent body, indicating 9 internal melting and differentiation. Here we show that a parent body that accreted 10 to >~200 km in radius by ~1.5 Ma after the formation of calcium-aluminum-rich 11 inclusions (CAIs) would have a differentiated interior, and ongoing accretion would 12 add a solid undifferentiated crust overlying a differentiated interior, consistent with formational and evolutionary constraints inferred for the CV parent body. This 13 14 body could have produced a magnetic field lasting more than 10 Ma. This 15 hypothesis represents a new model for the origin of some chondrites, presenting 16 them as the unprocessed crusts of internally differentiated early planetesimals. Such 17 bodies may exist in the asteroid belt today; the shapes and masses of the two largest 18 asteroids, 1 Ceres and 2 Pallas, can be consistent with differentiated interiors, 19 conceivably with small iron cores with hydrated silicate or ice-silicate mantles, 20 covered with undifferentiated crusts.

21 Key words: chondrite; planetesimal; magma ocean; differentiation; Allende

1. INTRODUCTION

2	The antiquity and abundance of CAIs in CV chondrites have long suggested an early
3	parent body accretion age. New Pb-Pb and Al-Mg ages of chondrules in CVs indicate
4	they may be among the oldest known in any chondrite class, with ages ranging from ~ 0
5	to ~3 Ma after CAIs (Amelin and Krot 2007, Connelly et al. 2008, Hutcheon et al. 2009)
6	(Fig. 1). The time of accretion of a body controls the amount of initial ²⁶ Al, which was
7	likely uniformly distributed in the inner protoplanetary disk (Jacobsen et al. 2008).
8	Bodies that accreted to more than ~ 20 km radius before ~ 1.5 Ma after the formation of
9	CAIs likely contained sufficient ²⁶ Al to melt internally from radiogenic heating (Hevey
10	and Sanders 2006, Merk et al. 2002, Sahijpal et al. 2007, Urey 1955). These early-
11	accreting bodies would have melted from the interior outward, resulting in an interior
12	magma ocean under a solid, conductive, undifferentiated shell (Ghosh and McSween Jr.
13	1998, Hevey and Sanders 2006, McCoy et al. 2006, Merk et al. 2002, Sahijpal et al. 2007,
14	Schölling and Breuer 2009). This shell would consist of the same chondritic material that
15	made up the bulk accreting body before melting began; further, and critically, ongoing
16	accretion would add undifferentiated material to the crust, and this material may even
17	have bulk compositions distinct from the differentiated interior.
18	Allende and a few other chondrites possess a unidirectional magnetization (Blum et
19	al. 1989, Wasilewski 1981, Weiss et al. 2010). Funaki and Wasilewski (1999) suggested a

20 liquid metallic core dynamo origin for magnetism on the CV parent body. Weiss et al.

21 (2010) described how unidirectional magnetization in Allende is consistent with a field

22 lasting >10 Ma. The variety of metamorphic textures in chondrites originally motivated

23 the "onion shell" model in which chondrites originated at varying depths within a parent

body heated primarily by the short-lived radioisotope ²⁶Al, with the highest metamorphic 1 grade originating nearest the center (Miyamoto et al. 1981, Taylor et al. 1987). Now, the 2 3 metamorphic, magnetic, and exposure age data collectively indicate a new model for the CV chondrite parent body in which interior melting is incomplete and a magma ocean 4 5 remains capped by an undifferentiated chondritic shell. This conductive lid insulates the 6 internal magma ocean, slowing its cooling and solidification by orders of magnitude 7 while still allowing sufficient heat flux out of the core to produce a dynamo with 8 intensities consistent with magnetization in Allende [see analysis in (Weiss et al. 2008)]. 9 Materials in the undifferentiated lid experienced varying metamorphic conditions. 10 Chondritic meteorite samples, including Allende, provide motivation for this study. 11 We seek to define the accretion age and size that would allow internal differentiation of a 12 body consistent with Allende originating in the unmelted crust. A chondritic surface, a 13 silicate or ice-silicate mantle and crust, and an iron core should characterize such a body. 14 Further, we will investigate the implications of internally differentiated bodies, including 15 their possible existence in the asteroid belt today. This study is designed to test the 16 feasibility of internal differentiation with a retained primitive crust, and the feasibility of 17 generating a long-lived magnetic core dynamo on such a body. 18

19

2. MODELS AND METHODS

To calculate heat fluxes, the possibility of a core dynamo, and temperature gradients in the unmelted crust, we assume instantaneous accretion and solve the heat conduction in a sphere with initial ²⁶Al evenly distributed (Hevey and Sanders 2006). The body is heated homogeneously but radiates energy into space, producing a hot interior and chilled crust. If the interior exceeds its solidus temperature sufficiently, the resulting interior
 magma ocean would advect heat to the base of the crust, where heat transfer continues
 through the far slower process of conduction.

4 Although new models and observations indicate rapid accretion (Johansen et al. 5 2007), the accretion of planetesimals early in solar system history was certainly not 6 instantaneous, as discussed in Ghosh et al. (2003), Merk et al. (2002), and Sahijpal et al. (2007). A hypothetical parent body with 300-km radius receives $\sim 10^{25}$ J in kinetic energy 7 during incremental accretion, sufficient to heat the body homogeneously by only 10 to 8 20°C (see SD). Thus the first-order temperature driver prior to 2 Ma after CAIs was ²⁶Al 9 heating. The complexity and stochastic nature of boundary conditions, sizes and rates of 10 11 impactors, and energy partitioning during incremental accretion also means that 12 incremental model results are necessarily non-unique. Incremental accretion models are 13 likely therefore to require a Monte Carlo approach. Because our intention is to 14 demonstrate the feasibility of partial differentiation rather to model it explicitly, we 15 conclude that instantaneous accretion is a reasonable simplification for calculating core 16 heat flux.

Incremental accretion, though it may not influence the heating of the body, does partially control cooling. A thickening conductive undifferentiated lid added to an initially partially melted planetesimal will slow its heat flux into space and therefore lessen the driving mechanism for a magnetic core dynamo. A simple model of incremental accretion is considered in comparison to the instantaneous models; this model is described below.

23 **2.1 Heating and heat transfer**

1	The initial ²⁶ Al content of CV chondrites is a controlling parameter in these
2	calculations. Kunihiro et al. (2004) find that there is insufficient radiogenic aluminum in
3	CO chondrites to cause more than minimal melting even with the help of radiogenic 60 Fe,
4	and also argue that the CV parent body was unlikely to have melted. However, their
5	conclusion for CV chondrites is based on an initial ²⁶ Al content identical to that of CO
6	chondrites and instantaneous accretion. Here we find that the potentially older age of CV
7	chondrules (the youngest being up to 1 Ma older than those in CO chondrites) combined
8	with non-instantaneous accretion mean the CV body could have melted. See Table 1 for
9	model parameters including bulk aluminum content.

Following Hevey and Sanders (2006) we assume instantaneous accretion and solve
 the heat conduction in a sphere with initial ²⁶Al evenly distributed:

12
$$\rho C_{P} \frac{\partial T}{\partial t} = \frac{1}{r^{2}} \frac{\partial}{\partial r} \left(kr^{2} \frac{\partial T}{\partial r} \right) + A_{0}(r, t), \qquad (1)$$

13 where ρ is density, C_p is the heat capacity of the chondrite, *T* is temperature, *t* is time, *r* is 14 radius, *k* is thermal conductivity, and A_0 is the radiogenic heat source per volume per 15 time. The temperature profile in these planetesimal models is initially calculated using an 16 analytic solution as given by Carslaw and Jäger (1946) and Hevey and Sanders (2006): 17

$$18 T = T_0 + \frac{\kappa A_0}{\kappa \lambda} e^{-\lambda t} \left[\frac{R \sin\left(r\left(\frac{\lambda}{\kappa}\right)^{\frac{1}{2}}\right)}{r \sin\left(r\left(\frac{\lambda}{\kappa}\right)^{\frac{1}{2}}\right)} - 1 \right] + \frac{2R^3 A_0}{r \pi^3 K} \sum_{n=1}^{\infty} \frac{-1^n}{n\left(n^2 - \frac{\lambda R^2}{\kappa \pi^2}\right)} \sin\left(\frac{n \pi r}{R}\right) e^{-\frac{\kappa n^2 \pi^2 t}{R^2}}$$
(2)

1 where the variables are as defined in Table 1, and *t* is the time elapsed since accretion. 2 The power from ²⁶Al, A_0 in W m⁻³, is obtained by multiplying the decay energy of 3 aluminum, converted to J kg⁻¹, with the aluminum content of chondrites, the ²⁶Al decay 4 constant, the material density, and the initial ²⁶Al/²⁷Al ratio, and similarly for the other 5 radioactive nuclides considered (see Supplementary Data, SD). To obtain the initial 6 power for later accretion times, the initial A_0 is multiplied by $e^{-\lambda t}$, where *t* is here the 7 instantaneous time of accretion.

8 The accreted chondritic material is assumed to begin to melt at 1,200°C and reach its 9 liquidus at 1,600°C at the low but non-zero pressures of the planetesimal interiors (in a 10 Vesta-sized body the pressure at the bottom of a mantle magma ocean will be 1 kb or less, 11 and over that pressure range the solidus will change by less than 20°C and the adiabat by 12 less than 4°C). These temperatures are based on experimental melting of Allende bulk 13 compositions (Agee et al. 1995) taking into consideration the absence of the iron metal 14 component (removed to the core) and the loss of some volatiles. Melting is calculated 15 using the following simplified expression for melt production per degree above the 16 solidus:

17
$$f = \Delta T \frac{df}{dT} = \Delta T \frac{C_P}{H_f} = (0.002)\Delta T$$
 [fraction by weight], (3)

18 where C_p and H_f are the heat capacity and heat of fusion of the silicates, and ΔT is the 19 temperature excess of the melt source beyond its solidus (Hess, 1992). The coefficient 20 0.002 therefore has units of K^{-1} and the resulting *f* is a nondimensional weight fraction. Latent heat of melting is similarly applied to the temperature of the melting material.
 The total temperature change for complete melting in this simple linear melting scheme,
 using values from Table 1, is

4
$$\Delta T = \frac{H_f}{C_p} \approx 500K.$$
 (4)

5 The latent heat temperature change is applied to the melting material at each time step of 6 the model until complete melting is achieved. The model tolerates temperatures in the 7 magma ocean above the liquidus temperature, and conductive heat loss through the lid 8 continues. High temperatures lead to melting and thus thinning of the lid.

9 We calculate thermal profiles using equation 2 at intervals of 1,000 years until the 10 body has melted 10% by volume (so much radiogenic heat is created in these bodies that 11 the degree of melting is 100%, and volume here refers to a fraction of the total 12 planetesimal volume). After this point, the internal magma ocean is treated as a 13 homogeneous adiabatic fluid, and conduction of heat through the unmelted crust limits 14 the heat flux available to drive the core dynamo.

These calculations are done using a finite difference formulation of the heat conduction equation in spherical coordinates for the conductive lid, which is defined as the material at temperatures below 1,400°C based on an assumption that melting above 50% will produce a convecting fluid no longer constrained by a solid network of residual crystals. In this simulation all material in the conductive lid is assumed to be porous, unmelted chondritic material. Although the temperature profiles indicate areas of partial melt and sintering, these are not treated in the calculations. At each step the heating contributions of ²³⁵U, ²³⁸U, ²³²Th, ⁴⁰K, and ²⁶Al are added,
 assuming chondritic concentrations, to each element in the conductive lid and to the bulk
 magma ocean beneath. Concentrations, heat production, and calculation schema for U,
 Th, and K are from Turcotte and Schubert (2002); Al values and references are listed in
 Table 1. Heating from ²⁶Al is given by

6
$$H(t) = H_0 C_0 e^{-\lambda t} [W \text{ kg}^{-1}],$$
 (5)

7 where H_0 is heating rate of ²⁶Al, C_0 is the fraction of ²⁶Al in the bulk material, and λ is 8 the decay constant for ²⁶Al. For values and references see Table 1.

9 Radiogenic heat is added to the crust in proportion to the silicate portion of the bulk
10 chondrite, subtracting volume for pore space, assumed to be 25%, and for metal fraction,
11 and to the magma ocean, which is assumed to be 100% bulk silicate.

Heat is conducted upward from the magma ocean to the surface through the conductive lid using the following expression for temperature controlled by heat conduction in a sphere:

15
$$T_{r}^{t} = T_{r}^{t-dt} + \kappa dt \left(\frac{1}{r} dr \left(T_{r+dr}^{t-dt} - T_{r-dr}^{t-dt} \right) + \frac{1}{dr^{2}} \left(T_{r+dr}^{t-dt} - 2T_{r}^{t-dt} + T_{r-dr}^{t-dt} \right) \right) + dt \frac{H}{C_{p}}, \tag{6}$$

where *dt* is a Courant time step determined by thermal diffusivity, and *dr* is the radial length of an element in the finite difference grid that does not exceed 1 km. At each time step the temperature at the bottom of the conductive lid is examined, and if the bottom of the lid has melted, the radius of the bottom of the grid is adjusted upward and the grid points redefined; latent heat is also considered at each melting step. If more melting has occurred then the appropriate volume is added to the core, at the current temperature of the magma ocean.

1	Although iron-nickel metal melts at temperatures below primitive silicate melting
2	temperatures, the metal liquid may be unable to segregate into a core until the silicates
3	are partially molten. Previous studies differ on whether core segregation occurs near
4	950°C, at the iron alloy eutectic, or in the range 1,170 to 1,570°C, between the solidus
5	and liquidus of the silicate portion [see Sahijpal et al. (2007) and references therein].
6	Here we assume metallic core formation occurs instantaneously when the bulk chondritic
7	material reaches its model solidus, 1,200°C. At the point that the body has reached 10%
8	melting by volume, the core is assumed to be at thermal equilibrium with the small
9	internal magma ocean from which it just segregated (for a 100-km radius body, at 10
10	vol% melting the internal convecting magma ocean reaches a radius of about 46 km, and
11	if the body began with 20 vol% metals the core has a radius of 30 km).
12	The core is assumed to contain no U, Th, K, or Al; all these elements are compatible
13	with the silicate magma ocean and not with the metallic core material. Thus the core,
14	initially at thermal equilibrium with the overlying magma ocean, has a thermal history
15	entirely driven first by the radiogenic heating of the overlying magma ocean (during
16	which the core is heated by the magma ocean, and heat flux is therefore into rather than
17	out of the core), and then by secular cooling of the body (during which the core cools and
18	heat moves back into the magma ocean).
10	

19 To calculate these changes, at each time step heat flux through the core-mantle20 boundary is calculated as

21
$$F_{core} = \kappa_{core} \rho_{core} \frac{dT}{dr} \quad [J \text{ m}^{-2} \text{ s}^{-1}],$$
(7)

22 and the resulting temperature change in the core is given as

1
$$\Delta T_{core} = \frac{3dtF_{core}}{\rho_{core}C_{P,core}r_{core}}$$
 [K], (8)

2 which is a simplification in this geometry of the general statement

3
$$\Delta T = \frac{dt F_{core} A_{core_surface}}{V_{core} \rho_{core} C_{P,core}}.$$
 (9)

4 The corresponding temperature change in the magma ocean is given as

5
$$\Delta T_{MO} = \frac{3dt F_{core} r_{MO,top}^2}{\rho_{MO} C_{P,MO} \left(r_{MO,top}^3 - r_{core}^3 \right)} [K],$$
(10)

6

7 where $r_{MO,top}$ is the radius at the top of the internal magma ocean, equivalent to the radius 8 at the bottom of the conductive lid. Next, the heat flux out of the magma ocean and into 9 the conductive lid is calculated using an equivalent statement to equation 6, and the 10 corresponding additional temperature change in the magma ocean is calculated using an 11 equivalent statement to equation 9.

12 The physics and chemistry of cooling an internal magma ocean on a small body are 13 not well understood. Mineral phases solidifying from the magma ocean will be dense in 14 comparison to the magma ocean, with the exception of plagioclase feldspar. The time 15 required for mineral grains to either sink or float out of the convecting magma ocean is, 16 however, possibly longer than the time of solidification of the body (Elkins Tanton et al. 17 2008). We therefore assume for simplicity that the conductive lid does not significantly 18 thicken from beneath while the internal magma ocean is still convecting, as that would 19 require material to adhere to its bottom and leave the convecting magma ocean. Rather, 20 the magma ocean continues to convect and cool and fractionate under the existing

thinnest conductive lid. Convection is assumed to be inhibited at temperatures below
 1,000°C by a high crystal fraction in liquids evolved through some degree of fractional
 solidification. No latent heat of solidification is applied during cooling.

4 For the simple incremental accretion model shown here, the initial assumptions are 5 the same: A radius of instantaneous accretion is chosen and heating calculated until 10% 6 of the planetesimal's volume is melted. The calculations are then passed to the convective code, with conduction occurring through the unmelted lid. Shells of cold undifferentiated 7 8 material are added to the outside of the planetesimal in increments of equal radius until a 9 final radius is acquired, in a simple approximation of the addition of new material to the 10 outside of the planetesimal. Thus, heat flux is inhibited through the growing lid. The new 11 material added to the exterior is assumed to have the same radioactive element 12 composition as the initial material.

13 **2.1 Calculating internal structure in asteroids**. To address whether examples of 14 differentiated parent bodies of the kind we propose are conceivably preserved in the 15 asteroid belt today, we consider the simple case of a rotating, hydrostatic figure 16 composed of a core and mantle, each of uniform density (Fig. SD2). For such a body it is 17 possible to relate shape, gravitational moments and internal structure. We invoke the formalism of Dermott (1979), who derived a relationship between the moment of inertia 18 factor (C/Ma^2) and the internal density structure for a planetary body with this 19 20 configuration

$$\frac{C}{Ma^2} = \frac{2}{5} \left[\frac{\rho_m}{\langle \rho \rangle} + \left(1 - \frac{\rho_m}{\langle \rho \rangle} \left(\frac{r_c}{R} \right)^2 \right) \right],\tag{11}$$

1 where *M*, *R* and $\langle \rho \rangle$ represent the mass, radius and mean density of the body, *C* is the 2 moment about the polar axis, *a* is the semi-major equatorial axis, r_c is the core radius, and 3 ρ_m and ρ_c are the mantle and core densities. Introducing an expression for the mean 4 density

$$\left\langle \rho \right\rangle = \frac{\left(\frac{4}{3}\right)\pi \left[\rho_c r_c^3 + \rho_m \left(R^3 - r_c^3\right)\right]}{\left(\frac{4}{3}\right)\pi R^3} \tag{12}$$

6 allows the mantle and core densities to be expressed as

$$\rho_m = \left\langle \rho \right\rangle \left[\frac{\frac{5}{2} \frac{C}{Ma^2} - \left(\frac{r_c}{R}\right)^2}{1 - \left(\frac{r_c}{R}\right)^2} \right], \tag{13}$$

8 and

7

13

5

9
$$\rho_c = \frac{\left\langle \rho \right\rangle - \rho_m \left[1 - \left(\frac{r_c}{R}\right)^3 \right]}{\left(\frac{r_c}{R}\right)^3}.$$
(14)

The consistency of internal structures with the hydrostatic assumption can also be
tested using an expression between hydrostatic flattening and moment of inertia factor
(Jeffreys 1959)

$$f_{hyd} = \frac{q}{1 + \left(\frac{25}{4}\right) \left[1 - \left(\frac{3}{2}\right) \frac{C}{Ma^2}\right]}$$
(15)

1 where

2

$$q = \frac{\omega^2 a^3}{GM},\tag{16}$$

3 and ω is the rotational angular velocity and G is the universal constant of gravitation. 4 On the basis of observations of shape, mass and surface composition inferred from 5 infrared spectra, we consider asteroids 1 Ceres and 2 Pallas as the likeliest candidates 6 among the largest asteroids for the proposed parent body and we investigate models of 7 their interior structures using the expressions above. Fig. SD3 plots expression (15) 8 combined with axial measurements in Table SD2, and verifies the validity of the 9 hydrostatic shape of both bodies within the bounds of measurement error. 10 These simple calculations are intended to demonstrate the plausibility of the present-11 day existence of a differentiated CV chondrite parent body. Additional observations will 12 be required to test more rigorously whether either or both of these bodies (or others) 13 satisfy all required criteria. 14 15 3. RESULTS 16 If accreted before ~1.5 Ma after CAIs, the planetesimal melts from its interior 17 through radiogenic heat. In the largest body considered here, 500 km radius, an internal 18 magma ocean is still generated if the body accretes by 1.6 Ma after CAIs, but for smaller

19 bodies and at any later accretion times there is insufficient heat to produce an internal

20 magma ocean (Figure 2). This precise ending point of melting is dependent upon initial

21 parameters that might not be well constrained, including initial ²⁶Al content of the parent

22 body and thermal diffusivity of the variably porous and sintered conductive lid.

1	Calculation of core heat flux is a necessary first step to determining the possibility of
2	a core dynamo. Here the rapid heat transfer of convection in a liquid internal magma
3	ocean maximizes core heat flux. The magma ocean rapidly heats beyond the temperature
4	of the non-radioactive core, so initial heat flux across the core-mantle boundary transfers
5	heat into the core, rather than out. All bodies considered here reach their peak magma
6	ocean temperatures within 5 Ma after CAI formation (Figures 3, 4). Shortly after
7	radiogenic heating peaks and the body begins secular cooling heat flux from the core
8	becomes positive, compatible with creating a core dynamo.
9	All bodies considered here have sufficient size to produce a core dynamo. Bodies
10	larger than ~100 to 150 km radius will produce a core dynamo lasting longer than 10 Ma,
11	and those larger than \sim 300 to 350 km radius will produce a core dynamo lasting longer
12	than 50 Ma (Figure 3). The volume fraction of metal in the bulk material determines the
13	size of the core, but over the range of metal fractions considered here (0.05 to 0.2), core
14	heat flux and thus magnetic dynamo are not greatly affected (Figure 4).
15	As shown by Hevey and Sanders (2006), these early-accreting planetesimals melt
16	extensively and retain only a very thin crust. In the instantaneous accretion convective
17	models used here the crust is artificially limited to a thickness no less than 2% of the
18	body's radius (Figure 5). Only in bodies accreting later than ~1.3 Ma are thicker crusts
19	naturally retained on the bodies; radiogenic heating is lower and so less of the
20	planetesimal's shell melts. The thermal gradient within the stable undifferentiated crust,
21	from liquid silicate temperatures at its bottom boundary to space equilibrium blackbody
22	temperatures at its surface (Hevey and Sanders 2006, Sahijpal et al. 2007), would
23	produce regions of varying metamorphic grade.

1 The simple incremental accretion models, in which the initially instantaneous core 2 then receives increments of cold material to its surface over an additional 1 to 2 Myr, 3 would also produce core dynamos. The thickening cold crust inhibits heat flux out of the body and so lessens core heat flux but also lengthens the period of internal convection 4 5 (Figure 3). Determining the combinations of rate of accretion and final body size that 6 allow or disallow magnetic dynamos is beyond the scope of this project, but these initial 7 studies indicate that dynamos can be lengthened by adding insulating crust, and that very 8 thick added crusts would inhibit dynamos.

9 Asteroid 1 Ceres displays a hydrostatically relaxed shape from which its internal 10 structure has previously been modelled (Castillo-Rogez and McCord 2010, Thomas et al. 11 2005). And a recent analysis of the shape of 2 Pallas (Schmidt et al. 2009) finds a close 12 fit of the shape to a hydrostatically relaxed spheroid. Given current knowledge of shape, 13 Ceres is most consistent with a differentiated interior, as previously noted (Thomas et al. 14 2005), but both undifferentiated and differentiated interiors are permissible for Pallas. An assumed iron core of $\rho_c \sim 7800 \text{ kg m}^{-3}$ in 1 Ceres constrains the core to radius to 15 0.22< $r_c/R < 0.5$ and limits mantle density to $1000 < \rho_m < 1950 \text{ kg m}^{-3}$ (Figure 6). For 16 Pallas, assumption of an iron core, again with density ρ_c -7800 kg m⁻³ yields a range of 17 fractional core size of $0.3 < r_c/R < 0.6$ and constrains the mantle density to $1000 < \rho_m <$ 18 2300 kg m⁻³ (Figure 6). A mantle density of 1,000 kg m⁻³ implies pure water ice, while 19 20 higher values likely indicate mixed ices and silicates.

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- 22

4. DISCUSSION

23 4.1 Core dynamos on planetesimals

These core dynamo calculations have several caveats. Heat flux through the
undifferentiated crust may be enhanced by fluid flow (Young et al. 2003) or slowed by a
porous low-conductivity crust (Haack et al. 1990). If a body 250 km or more in radius
accretes as late as ~2.0 Ma after CAIs, its internal temperature reaches ~1,000°C and it
may form a core, but its silicate mantle will not melt more than a small fraction;
compositional convection in the core would then likely be necessary for dynamo
generation (Nimmo 2009). Therefore, ~2.0 Ma is the latest limit on accretion that will
allow a core dynamo using the parameters chosen in these models. The upper time limit
is sensitive to choice of heat capacity, final body radius, ²⁶ Al and ⁶⁰ Fe content, and
thermal boundary conditions and has uncertainties of $\sim \pm 1$ Ma.
Throughout most of the parameter space explored here bodies would create dynamos
lasting tens of millions of years (Figure 2). Our code halts calculation when the magma
ocean is assumed to end convection, but even conductive heat flux may be sufficient to
drive dynamos in some cases. Sufficient heat flux for a core dynamo is a pervasive and
robust outcome in these models. Although convection is a necessary but not sufficient
criterion for dynamo action, it appears feasible that planetesimals also had other
properties (core size, core convective velocity, spin rate) suitable for dynamo generation
(Weiss et al. 2008, Weiss et al. 2010).
4.2 The growing crust of a planetesimal
The body must retain or acquire a sufficiently thick crust to both create radial source

21 zones for each chondrite type and to be stable against foundering. Metasomatism of

22 Allende likely began within 1 Ma after CAI formation (Hohenberg et al. 2004,

23 Pravdivtseva et al. 2003), as water was mobilized within the planetesimal. The presence

of talc and the absence of serpentine indicate peak temperatures of ~300-350°C (Brearley
1997, Krot et al. 1995), while organic thermometry and presolar gases in nanodiamonds
place an upper limit of <~600 °C (Cody et al. 2008).

Figure 7 contains a compendium of data constraining the timing of events on the CV parent body and on other early-accreting bodies. Although all the isotopic systems included in this table do not have equivalent precision and accuracy, in aggregate they provide a sufficiently clear timeline to guide the modelling efforts presented in this paper. Specifically, the CV parent body contains chondrules not younger than about 3 Ma after first CAIs. The majority, and perhaps all, CAIs and chondrules in the CV parent body are older than these limits.

11 Metamorphism of chondrite parent bodies appears to stretch for tens of millions of 12 years, though peak temperatures for the CV parent body were reached at 5 to 10 Ma after 13 CAIs, based on I-Xe chronometry for Allende (Swindle 1998). These ages are within 14 error of the 5-10 Ma ages Mn/Cr ages for CV fayalites, although no Mn/Cr ages have 15 actually been reported for Allende itself (Nyquist et al. 2009). These chronometric 16 systems are subject to uncertainties associated with the initial abundances of the parent 17 nuclides, their closure temperatures, and the homogeneity of their spatial distribution in 18 the solar system.

These constraints require that the planetesimal have a reasonably thick crust while simultaneously producing a core dynamo. Instantaneous accretion models that consider convective heat transfer produce crusts that are too thin to be stable against eruption and impact foundering, and which have thermal profiles too steep to produce a sufficiently large volume consistent with Allende's constraints. These thin crusts are also too old;
 younger chondrules in Allende require ongoing accretion.

Planetesimals would be expected to continue accreting mass after the processes
proposed here are underway. Thus, colder material with younger chondrules would be
added after the majority of the body is accreted, and these younger chondrules would be
preferentially placed in near-surface material such as that hypothesized for the Allende
source. This initially cold crust will also yield significant metamorphosing but not
melting regions consistent with Allende's thermal constraints, over a body still producing
a core dynamo (Figure 2).

10 The fraction of ice in the planetesimal also affects the energy required to heat and 11 melt the silicate fraction of the body (Gilmour and Middleton 2009). Both accretionary 12 and radiogenic heat can be applied to melting (and possibly to evaporating) water before 13 silicate melting begins. Further, accretion of some icy material with the rocky chondritic 14 material would significantly enhance crustal formation through the cooling effect of 15 latent heat of melting. The accretion and differentiation of planetesimals that include both 16 ice and rock is pertinent for not just production of chondrites, but also possibly for 17 production of Pallas and Ceres.

18

4.3 Densities of solids and liquids and likelihood of eruption

Magma is unlikely to rise through the undifferentiated lid of the planetesimal.
Basaltic or picritic magmas would cool and solidify as they rise into the cool crust,
limiting their radius of maximum rise. Additionally, buoyancy alone is unlikely to drive
silicate eruption in small bodies with cool crusts. Because of the porous nature of
unheated chondrites, molten Allende liquids are in many cases denser than the

1 undifferentiated planetesimal lid (Figure 8). On Earth, Mars, and the Moon, gravity 2 forces buoyant magmas to erupt, while denser magmas may be erupted through volatile 3 pressure. Wilson and Keil (1997) predict fire-fountaining lava eruptions on Vesta driven by volatiles in magmas, but in our models we predict that the magmas will be largely dry. 4 5 On early-forming planetesimals gradual heating would drive off volatiles before silicate 6 melting begins [this is in contrast to Earth, where volatiles are either introduced to the 7 silicate solids and trigger melting by their presence (Sisson and Grove 1993) or they exist 8 in equilibrium with near-solidus silicates]. We therefore conclude that only from the 9 hottest bodies with the thinnest crusts will basaltic magmas erupt, or in cases where 10 volatiles were not driven off before magma genesis, will basaltic magmas erupt. The 11 conductive transfer and convection modelled here accounts for the effects of melting 12 from below. 13 We postulate that the picritic to basaltic silicate magma ocean liquids in the interior 14 magma oceans of these planetesimals will not fully infiltrate and cover the 15 undifferentiated crust of these bodies. Crustal stability in this case relies on three 16 processes: buoyancy of the crust, slow erosion from its bottom, and thickness sufficient 17 to prevent impacts from breaching the crust. 18 Because of the porous nature of unheated chondrites, molten Allende liquids (red 19 line in Fig. 8) are in many cases denser than the undifferentiated, unsintered, planetesimal 20 lid (grey range in Fig. 8) but close to the density of sintered material. In Fig. 8, the 21 Allende liquid densities are calculated from experimental compositions given in Agee et 22 al. (1995), using partial molar volumes and techniques from Kress and Carmichael (1991) 23 and Lange and Carmichael (1987); also see previous applications of this technique in

Elkins-Tanton et al. (2003). All measurements and calculations are done at 1 bar and
 room temperature. Here, as on the Moon, magmas would require a significant impact
 basin to erupt onto the surface through the more buoyant crust.

On such a small body viscous traction of the convecting magma ocean liquids on the
bottom of the lid will be minimal; not only do magma ocean liquids have low viscosity,
but also the small gravitational fields make convective velocities commensurately small.
Erosion of the bottom of the crust through liquid convection is therefore negligible.

8 Finally, the crust must be thick enough to prevent the majority of impacts from 9 breaching it. The small gravity fields of planetesimals prevent very great impact crater 10 depths. Taylor et al. (1987) estimate that the maximum excavation depth expected on a 11 planetesimal with 500 km diameter is 20 km. Although simple heat transfer in our models 12 produces a thin crust, later accreting material is expected to produce a far thicker crust. 13 We therefore suggest that the average impact will disrupt but not breach the crust and that 14 in most cases impacts will not allow magma to erupt. We conclude that undifferentiated 15 chondritic crusts may successfully persist through the internal magma ocean stage, 16 particularly when the bodies accreted throughout and after the window available for 17 internal heating.

18 **4.4 Source regions for meteorite types in an internally differentiated**

19 planetesimal

At temperatures above ~430°C (Yomogida and Matsui 1984) the porous chondritic material would sinter into a denser and stronger solid. At about the same temperatures, fluids may be released from the *in situ* chondritic materials. Hydrous, briney, sulfidic, or carbon-rich fluids will be able to rise efficiently through the chondritic crust at Darcy

1 velocities of meters to kilometers per year (Haack et al. 1990, Young et al. 2003). These 2 fluids may to quickly escape into space (Young et al. 2003). Even in the case where a 3 frozen ice crust slows escape, periodic impacts will disrupt this surface and aid escape. Hydrous fluids are therefore not expected to pervasively or homogeneously metasomatize 4 the entire planetesimal crust. We note further that briney fluids are insufficient to create a 5 6 core dynamo: circulating saltwater of composition like Earth's seawater has electrical 7 conductivity more than four orders of magnitude less than iron-liquid metal [see 8 discussion in Schubert et al. (1996)]. 9 The added cooler material accreting to the top of the crust will experience varying degrees of thermal and fluid metamorphism, depending on its depth and time of 10 11 accretion. Some late-accreting material will be added after the main pulse of heating and 12 metasomatism, and so will not experience the same intensity of metamorphism. The 13 stochastic nature of crustal additions implies that metamorphic grade and cooling rate 14 may not be correlated in samples from the crust. 15 These models indicate that dynamos will operate on these bodies for tens of millions 16 of years, allowing a range of accreted crustal conditions to pertain. Only the deepest parts 17 of the crust will be infiltrated by silicate magmas. These events appear to correspond well 18 with the metasomatic and metamorphic events experienced by the CV chondrites, and 19 help to explain why CV chondrites almost never contain fragments of volcanic rock. 20 The least metamorphosed, brecciated, and reduced CV chondrites containing a 21 solar wind component, such as Vigarano and Mokoia, may have originated nearest the 22 surface. Beneath were the Bali-type oxidized CV chondrites, and at greater depth, the 23 Allende-type oxidized CV chondrites (Fig. 1). Rocks like the metachondrite NWA 3133

may have originated at greatest depth in the undifferentiated crust, while the few higher
petrologic-grade clasts found in Mokoia (Krot et al. 1998) may be rare samples of the
highly thermally metamorphosed lower crust (Fig. 1). Irons like Bocaiuva (Irving et al.
2004) may have come from the core-mantle boundary region of this same body (Fig. 1).
Further, Greenwood et al. (2010) argue that CK and CV chondrites may have formed on
the same parent body, with CK chondrites simply being more highly metamorphosed, and
therefore, deeper samples.

8

4.5 The existence of internally differentiated planetesimals today

9 Because of the limited lifetime of ²⁶Al and the longer apparent period over which 10 chondrite parent bodies were forming, many parent bodies likely heated without 11 significant melting. Bodies that formed before ~1 Ma likely melted sufficiently to 12 produce only a fragile crust, and may have developed into bodies with igneous surfaces 13 like Vesta, while those accreting more slowly would have obtained an internal magma 14 ocean and a thicker, metamorphosed but unmelted crust.

15 The shapes and masses of the two largest asteroids, 1 Ceres and 2 Pallas, can be 16 consistent with differentiated interiors, conceivably with small iron cores with hydrated 17 silicate or ice-silicate mantles. The range of mantle density permits ice-silicate 18 compositions, though in this scenario for 1 Ceres the mantle is ice-rich (perhaps >50 wt%) 19 if there is no porosity, possibly not compatible with large-scale melting). The 20 corresponding range of mantle density for 2 Pallas permits more silicate-rich 21 compositions than Ceres. 22 Thus the asteroid melt may contain several examples of early-accreting bodies that

23 are internally differentiated. Unlike Vesta, Ceres and Pallas may retain their primitive

1 crusts over a differentiated interior. This is the central concept of this paper: That early 2 radiogenic of planetesimals can create partially differentiated bodies with undifferentiated 3 crusts, and that these bodies may have experienced magnetic core dynamos, varying degrees of crustal metamorphism or magmatic intrusion, and that some partially 4 5 differentiated bodies may have persisted to the current day. 6 7 **5. CONCLUSIONS** 8 Planetesimals that largely accreted before ~1.5 Ma after CAIs are likely to 9 differentiate internally through radiogenic heating (Ghosh and McSween Jr. 1998, Hevey

and Sanders 2006, Sahijpal et al. 2007, Urey 1955). Most of these bodies are capable of 11 producing a core dynamo. The earliest-accreting bodies are likely to obtain igneous crusts 12 through foundering of their thin lids, but bodies that continue to accrete past ~ 1.5 Ma are 13 likely to have an undifferentiated crust not covered by basalt.

14 Bodies that are internally differentiated in the manner described here, therefore, may 15 well exist undetected in the asteroid belt. Other asteroids may have lost their hydrostatic 16 shapes through later impacts, and their surfaces may never have been covered with 17 erupted basalt; surfaces of these bodies may have remained chondritic throughout this 18 process. Such surfaces will therefore be composed of irregular, space-weathered 19 primitive material, perhaps with highly altered or even differentiated material at the 20 bottoms of the largest craters and in crater ejecta. This scenario can help explain the mismatch between the enormous diversity (> 130) of parent bodies represented by 21 22 achondrites and the paucity (< 10) of basalt-covered asteroids.

23

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7	

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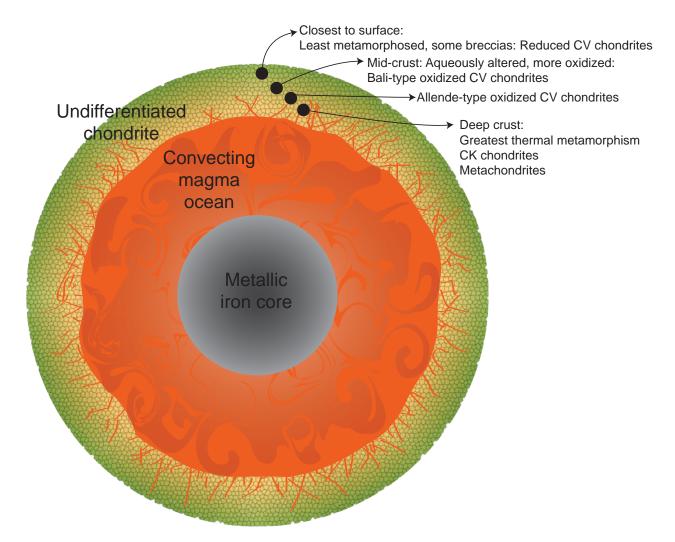
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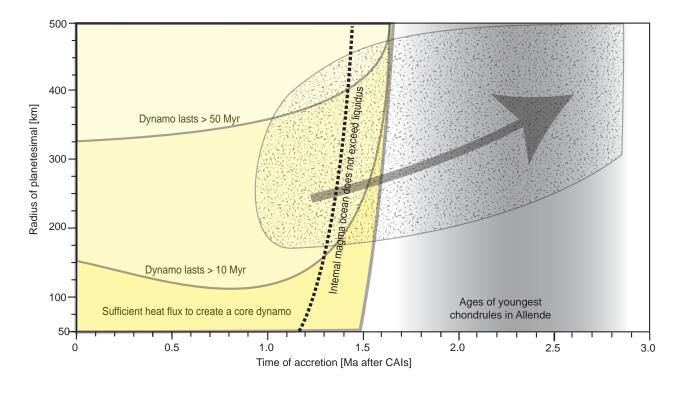
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FIGURES

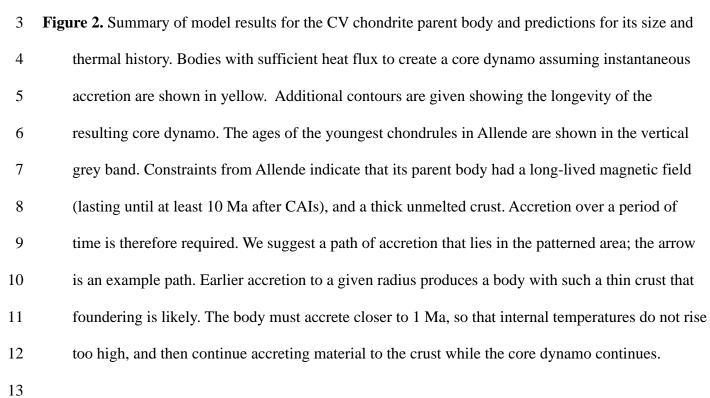


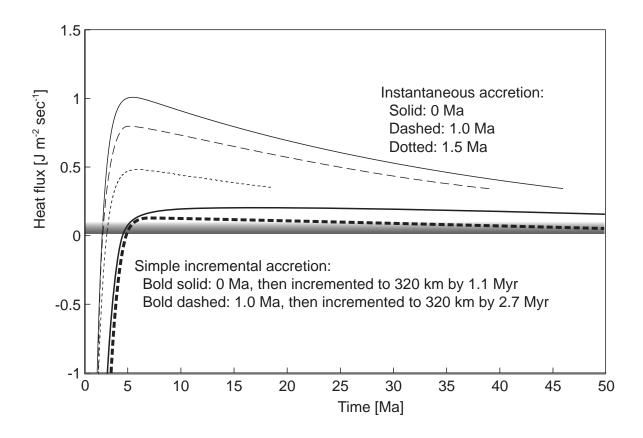
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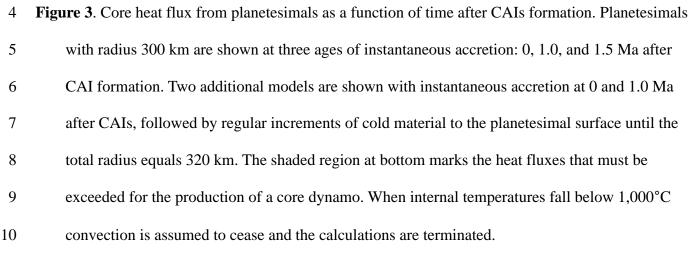
- 3 Figure 1. Schematic diagram of proposed structure for the CV parent body, including an iron core,
- 4 internal magma ocean, and undifferentiated chondritic crust with varying levels of metamorphism
- 5 and metasomatism.
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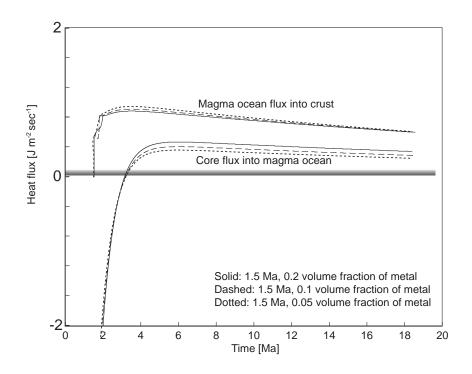




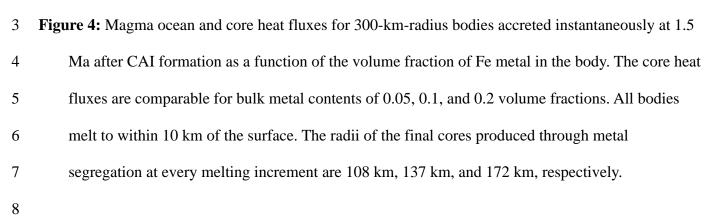


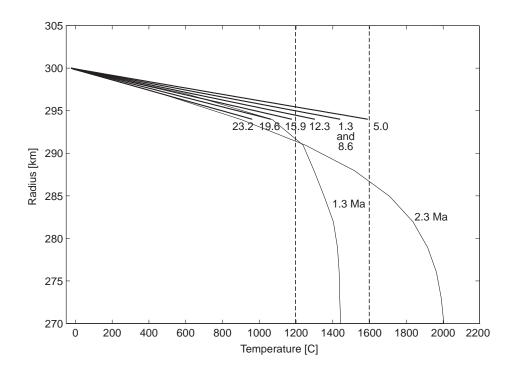






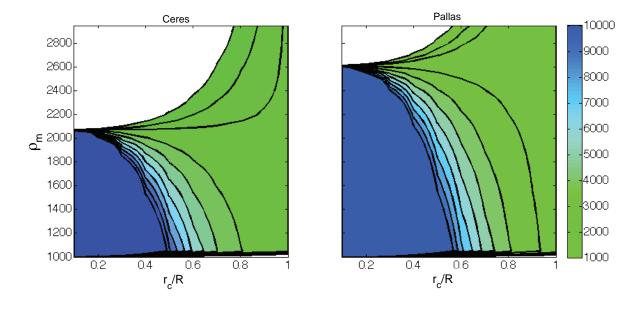






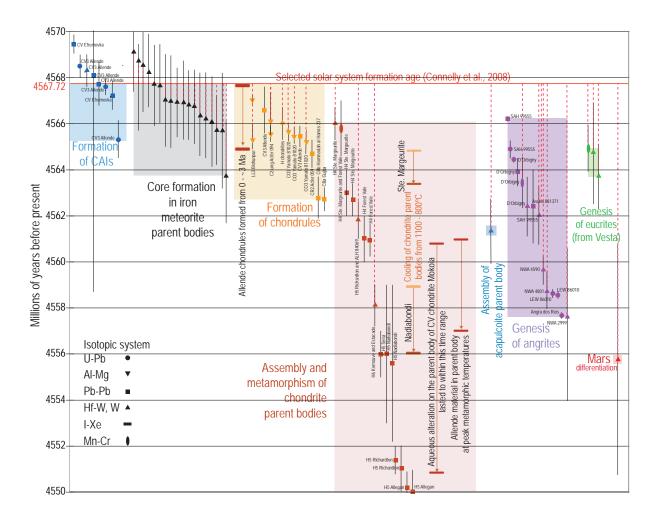


4 Figure 5: Temperature profiles for a body with radius 300 km that accreted instantaneously at 1.0 Ma 5 after CAI formation. Dashed lines: solidus and liquidus. Two thin lines, from Equation 2: 6 temperature profile at 1.3 Ma, passed to the convective code, and a later profile at 2.3 Ma, 7 included for comparison. Bold lines: profiles from the conductive lid overlying a homogeneously 8 mixed internal magma ocean at the temperature of the bottom of the lid, at 1.3, 5.0, 8.6 12.3, 15.9, 9 19.6, and 23.2 Ma. The temperatures at the bottom three nodes of the conductive lid at 5.0 Ma 10 exceed our stated lid temperature of 1400°C, but the lid is constrained in the code to be no thinner 11 than 2% of the planetesimal radius, or in this case, 6 km. The 6 km limit was reached immediately 12 at 1.3 Ma and retained afterward. Note that the solution to equation (2) at 2.3 Ma gives a lid under 13 1400°C that is ~10 km thick, rather than the ~6 km thickness from this code; allowing the interior 14 to be convectively well-mixed removes the curving boundary layer.

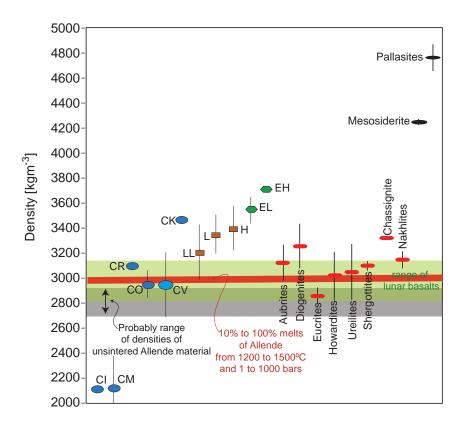


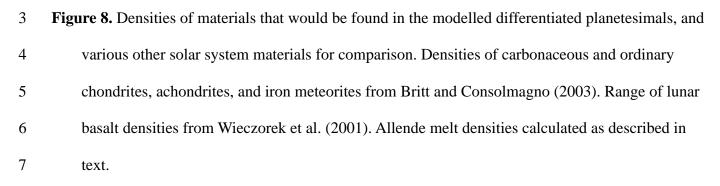


4 Figure 6. Contours of core density (ρ_c) for core radius/planetary radius (*r_c/R*) and mantle density (ρ_m)
5 for 1 Ceres (left) and 2 Pallas (right). Core densities in the range of iron metal but as light as pure
6 silicate are consistent with observations. Both bodies have mantle densities consistent with an ice
7 and silicate mixture.



1 2 Figure 7. Age constraints on meteorite and parent body evolution. Red dashed lines indicate ages 3 calculated relative to the selected age of oldest CAI. The early ages of CV chondrite chondrules and CV meteorite evidence for relatively protracted thermal metamorphism indicate an early 4 accretion age for the CV parent body. All dates and references in Table SD1. 5





1 TABLES

2 Table 1: Parameters used in models.

Variable	Symbol	Value(s)	Units	Ref.
Initial and surface				(Woolum and Casser
temperature	To	250	К	1999)
		50,000, 100,000,		
		200,000, 300,000,		
Planetesimal radius	r	400,000, 500,000	m	
			Ma after	
Age of instantaneous			CAI	
accretion		0, 1, 1.5	formation	
Metal in bulk starting material			Volume	
(for core formation)		0.05, 0.1, 0.2	fraction	
````				(Britt and
Density of conductive lid	$ ho_{_LID}$	2,900	kg m ⁻³	Consolmagno 2003)
Density of planetesimal	. –		5	5
magma ocean	$ ho_{-MO}$	3,000	kg m-3	
Density of iron core	$\rho_{-CORE}$	8,000	kg m ⁻³	
Thermal diffusivity of crust	Р_00КЕ К	8×10 ⁻⁷	m ² S ⁻¹	(Opeil et al. 2010)
mermai dinusivity or crust	ĸ	0.410	111- 3	(Monaghan and
Thermal diffusivity of core	к	6×10⁻⁵	m ² s ⁻¹	Quested 2001)
Thermal conductivity of	ĸ	0.410	111- 3	
conductive lid	K	1 5	W m-1 K-1	(Opoil at al. 2010)
	K _{LID} K	1.5 2.1	W m ⁻¹ K ⁻¹ W m ⁻¹ K ⁻¹	(Opeil et al. 2010)
Thermal conductivity	ĸ	Z. I	W III'' K''	(Fabriahnaya 1000
				(Fabrichnaya 1999,
11	0	000	11.11/1	Ghosh and McSweer
Heat capacity of silicates	Ср	800	J kg ⁻¹ K ⁻¹	Jr. 1999)
	0	050		(Bartels and Grove
Heat capacity of iron core	$C_{P_CORE}$	850	J kg-1 K-1	1991)
				(Ghosh and
Heat of fusion of silicates	Hf	400,000	J kg ⁻¹	McSween Jr. 1998)
Heating production of ²⁶ Al				(Castillo-Rogez et al.
decay	$H_0$	0.355	W kg ²⁶ Al ⁻¹	2009)
Aluminum content of CV				(Lodders and Fegley
chondrites	X _{AI}	1.8	wt%	1998)
				(Lee et al. 1976,
				MacPherson et al.
Initial ²⁶ AI/ ²⁷ AI ratio	²⁶ Al ₀	5×10 ⁻⁵		1995)
Fraction of ²⁶ Al in bulk				
Fraction of ²⁶ Al in bulk material	$C_0$	²⁶ Al ₀ X _{Al}		
	$C_0$	²⁶ AI ₀ X _{AI}		(Castillo-Rogez et al