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6-28-2017

Lightweight Absorption and Barrier Systems Comprising N-Layer Microperforates

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Kim, Nicholas N. and Bolton, J Stuart, "Lightweight Absorption and Barrier Systems Comprising N-Layer Microperforates" (2017). *Publications of the Ray W. Herrick Laboratories*. Paper 152. http://docs.lib.purdue.edu/herrick/152

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LIGHTWEIGHT ABSORPTION AND BARRIER SYSTEMS COMPRISING *N*-LAYER MICROPERFORATED PANELS



Paper 4pEA3 - 173rd meeting of The Acoustic Society of America

Boston MA



The Effect of Flexibility on the Acoustical Performance of Microperforated Materials

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WITH THANKS TO: Jinho Song (Otis Elevator), Taewook Yoo (3M/EAR), Ryan Schultz (Sandia) and Yangfan Liu (Purdue)



ASA Fall meeting, Kansas City, 10/22/12

Joint ASA/ASJ meeting Honolulu December 2016



Computational Investigation of Microperforated Materials: End Corrections, Thermal Effects and Fluid-Structure Interaction

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INTRODUCTION

- Traditional Uses of MPP's
 - Absorptive surface treatments



Deutsche Museum of History Berlin

INTRODUCTION



Great Ape House – National Zoo Washington DC

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OBJECTIVES

• Proposed Alternative Uses

(i) Functional Absorbers

 \rightarrow Lightweight, multi-layer, highly dissipative systems

OBJECTIVE







OBJECTIVES

• Proposed Alternative Uses

(ii) Absorbing barriers

 \rightarrow Lightweight, multi-layer, repositionable highly dissipative barrier

OBJECTIVE







INTRODUCTION

• Microperforated material

- Thin film with 100 microns scale holes
- Clean, light \rightarrow one alternative to fibrous sound absorbing materials







- Viscous Dissipation
 - In hole
 - Within shearing fluid exterior to the hole
- Objective
 - Multilayer panels to control sound level in speech interference range (500 Hz to 4 KHz)

INTRODUCTION



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PROCEDURE

- Procedure
 - ✓ MPP's modeled as flexible
 - ✓ Locally reacting
 - ✓ Bounded properties
 - ✓ Arbitrary number of layers up to 10
 - ✓ Arbitrary spacing of layers
 - ✓ Genetic Algorithm used to optimize properties over the Speech Inteference Range (500 Hz to 4 kHz)

PROCEDURE

 \checkmark Objective function depends on application



MULTI-LAYER OF MICROPERFORATED PANELS



Assumptions

- Hole in the MPP are cylindrical and sharp edged
- Flexural stiffness of the panel can be ignored
- Only locally reacting case considered
- Infinite panels

MLMP

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TRANSFER MATRIX METHOD



• Transfer Matrix

$[P_1]_{-}$	[<i>T</i> ₁₁	T_{12}]	$[P_2]$
$[U_1]^-$	$ T_{21} $	T_{22}	$[U_2]$

• Reflection Coefficient

$$R = \frac{T_{11} + T_{11} \cos \theta / (\rho c) - T_{21} (\rho c) / \cos \theta - T_{22}}{T_{11} + T_{11} \cos \theta / (\rho c) + T_{21} (\rho c) / \cos \theta + T_{22}}$$

• Transmission Coefficient

$$\tau = \frac{2e^{jk\cos\theta L}}{T_{11} + T_{11}\cos\theta/(\rho c) + T_{21}(\rho c)/\cos\theta + T_{22}}$$

• Dissipation Coefficient

$$\alpha_d = 1 - |R|^2 - |\tau|^2$$

TMM



TRANSFER MATRIX METHOD

- Random Incidence
 - Absorption Coefficient

$$\overline{\alpha} = \frac{\int_0^{\pi/2} \alpha(\theta) \sin(\theta) \cos(\theta) \, d\theta}{\int_0^{\pi/2} \sin(\theta) \cos(\theta) \, d\theta}$$

• Dissipation Coefficient

$$\overline{\alpha}_{d} = \frac{\int_{0}^{\pi/2} \alpha_{d}(\theta) \sin(\theta) \cos(\theta) d\theta}{\int_{0}^{\pi/2} \sin(\theta) \cos(\theta) d\theta}$$

• Transmission Loss

$$\overline{\tau} = \frac{\int_0^{\pi/2} |\tau(\theta)|^2 \sin(\theta) \cos(\theta) \, d\theta}{\int_0^{\pi/2} \sin(\theta) \cos(\theta) \, d\theta} \qquad TL = 10 \log_{10} \frac{1}{\overline{\tau}}$$

TMM

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TRANSFER MATRIX METHOD



MICROPERFORATED PANEL

• Guo et al. Model

$$R = \left(Re \left\{ \frac{j\omega t}{\sigma c} \left[1 - \frac{2}{k\sqrt{-j}} \frac{J_1(k\sqrt{-j})}{J_0(k\sqrt{-j})} \right]^{-1} \right\} + \frac{\alpha 2R_s}{\sigma \rho c} \right) \times \rho c$$

Symbol	
t	Time [sec]
σ	Surface Porosity
d	MPP hole diameter [m]

$$k = \left(\frac{\omega \rho_0}{4\eta} \right) R_s = \frac{\sqrt{2\omega \rho_0 \eta}}{2} \qquad \alpha = 4 \quad \text{when sharp end}$$

- Previous work
 - adjusted α by CFD calculation

$$\alpha = (16.9\frac{t}{d} + 152.8)f^{-0.5}$$

• Note that this equation was formulated in specific range of hole diameter, thickness of the panel, and porosity



MICROPERFORATED PANEL

• Continuity and Force equilibrium – fully coupled

$$v_y = (1 - \sigma)v_s + \sigma v_f$$

$$P_1 - P_2 + (v_f - v_s)R\frac{\sigma^2}{1 - \sigma} = j\omega m v_s$$

$$P_1 - P_2 + (v_f - v_s)R\sigma = \rho h_p j\omega v_f$$



where
$$h_p = t + 2\delta$$
 , $\delta = 8d/3\pi$

Fully coupled transfer impedance of MPP*

 \rightarrow m: Panel Mass [kg/m²]

MPP

$$Z_{MPP} = \frac{R\sigma(1-\sigma)(j\omega m - j\omega\rho(t+2\delta)) + j\omega\rho(t+2\delta)(j\omega m(1-\sigma) + R\sigma)}{\sigma(1-\sigma)(R+j\omega m) + (1-\sigma)^2\rho(t+2\delta)j\omega + \sigma^2 R}$$

* Taewook Yoo, Ph.D Thesis, Purdue University (2008)



OPTIMIZATION ALGORITHM



• GA [GENETIC ALGORITHM]



Initial population (initial point) generated at random.

Replication is the process of choosing the best individuals to participate in the production of offspring.

Crossover is to reconstruct points by mixing from the pool. Each solution is split in two by the crossover point, which is chosen at random.

Mutation is a random change of some individuals.

OBJECTIVE



OPTIMIZATION



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Constraints

	Minimum	Maximum
N	2	10
Thickness of MPP: <i>t</i> [mm]	0.2	0.8
MPP hole diameter: <i>d</i> [mm]	0.1	0.3
Surface porosity: σ	0.01	0.2
Panel mass: <i>m</i> [kg/m ²]	0.1	0.8
Panel separation: <i>l</i> [m]	0.001	0.2
Total mass: M [kg/m ²]		3
Total depth: L [m]		0.5

Varied in optimization process

OPTIMIZATION

PROCEDURE

• Genetic Algorithm was used for optimization: function for optimization is not differentiable and also is not continuous at some points

FUNCTIONAL ABSORBER



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RESULTS



- Used for dissipating energy
- Both directions were considered
- Maximize dissipation coefficient, $\overline{\alpha}_d$

PROCEDURE

• Optimization for Dissipation Coefficient

Result by number of panel (error function: $\Sigma(1-\overline{\alpha}_d)$)



Result by number of panels ($\overline{\alpha}_d$)



PROCEDURE

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• Optimization for Dissipation coefficient

Parameters for 9 panels

	<i>t</i> Thickness [mm]	<i>d</i> Diameter [mm]	σ Porosity	<i>m</i> Mass per unit area [kg/m²]	/ Distance to next panel [m]
Panel 1	0.3411	0.2831	0.0635	0.6974	0.0368
Panel 2	0.7350	0.1191	0.0614	0.1181	0.0401
Panel 3	0.7531	0.1000	0.0648	0.2289	0.0372
Panel 4	0.6777	0.1000	0.0240	0.7085	0.0053
Panel 5	0.7493	0.3000	0.0438	0.7308	0.0368
Panel 6	0.7960	0.1000	0.0437	0.1880	0.0176
Panel 7	0.4441	0.3000	0.0125	0.1115	0.0395
Panel 8	0.7960	0.1610	0.1219	0.1051	0.0286
Panel 9	0.7493	0.3000	0.0725	0.1000	-

$M = 2.9883 \text{ kg/m}^2$, L = 0.2479 m

RESULTS

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- Optimization for Dissipation coefficient
 - Finite size wall alter performance (L = 0.25 m, M = 3 kg/m*m)





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- Suspended multilayer systems can dissipate almost all incident acoustic energy
- Finite size will impact performance

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TION 📡 OBJECTIVE 🃡 PROCEDURI

MIZATION 💙 RESULTS

ABSORPTIVE BARRIER (I): Maximize TL



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RESULTS



- Use for blocking noise propagating from one side to other
- One direction was considered
- Maximizing transmission loss
- Remove the valley point (eliminate minima in TL, which does not guarantee high peak TL)

PROCEDURE

• Optimization for Transmission Loss

Error 1/TL 20 30 v 2 Number of panel

Result by number of panel (error function: $\Sigma(1/TL)$)

Result by number of panels





• Optimization for Transmission Loss

Parameters for 6 panels

	<i>t</i> Thickness [mm]	d Diameter [mm]	σ Porosity	<i>m</i> Mass per unit area [kg/m²]	<i>I</i> Distance to next panel [m]
Panel 1	0.8000	0.3000	0.0725	0.3755	0.2000
Panel 2	0.7494	0.1000	0.0100	0.7000	0.2000
Panel 3	0.8000	0.1000	0.0101	0.7295	0.0363
Panel 4	0.8000	0.3000	0.2000	0.7014	0.0020
Panel 5	0.8000	0.3000	0.1375	0.1332	0.0049
Panel 6	0. 7646	0.1000	0.0100	0.3500	-

M = 2.9896 kg/m², *L* = 0.4475 m

RESULTS

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RANDOM INCIDENCE CASE

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• Comparison of optimized set and mass law set (Number of panels: 6)

Mass Law: $m = 3 \text{ kg/m}^2$

- Performance of multilayer system is better than mass law
 - Has further advantage of being absorptive on incident side, so does not increase level on source side

RESULTS

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OBJECTIVE

PROCEDURE



• Comparison of optimized set for $\overline{\alpha}_d$ and for *TL* (*N* = 6)



OBJECTIVE

PROCEDURE

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RESULTS

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BARRIER TREATMENT



ABSORPTIVE BARRIER (II): TL and absorption

- Optimization for Partition
 - Result by number of panels (error function: $\Sigma(1-\alpha_d-0.8T)$)



PROCEDURE

BORA

ТО

- Optimization for Partition
 - Result by number of panels



PROCEDURE

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RESULTS



• Optimization for Partition

• Parameters for 8 panels

	Thickness	Diameter	Porosity	Mass per unit area	Distance to next panel
	[mm]	[mm]		[kg/m²]	[m]
Panel 1	0.800	0.300	0.113	0.100	0.030
Panel 2	0.800	0.300	0.105	0.140	0.023
Panel 3	0.800	0.300	0.183	0.382	0.017
Panel 4	0.800	0.176	0.042	0.100	0.024
Panel 5	0.780	0.300	0.076	0.112	0.004
Panel 6	0.234	0.193	0.015	0.631	0.031
Panel 7	0.800	0.100	0.035	0.644	0.136
Panel 8	0.800	0.100	0.010	0.618	-

PROCEDURE

• Comparison optimized result for a functional absorber and for a partition



OBJECTIVE

PROCEDURE

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RESULTS

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• Comparison optimized result for a functional absorber and for a partition



PROCEDURE

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RESULTS

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CONCLUSIONS

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- Optimization model for a functional absorber and a barrier cases were introduced
- Optimization result for multi-layer panels covers much broader frequency range than single panel
- Future work:
 - To decide number of segments, design optimization model for an extended reacting case
 - To decide size of the system, effects edge scattering and constraint when optimizing the system
- For presentations search for "Herrick e-Pubs"