

11-2016

Localized Heating Near a Rigid Spherical Inclusion in a Viscoelastic Binder Material Under Compressional Plane Wave Excitation

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Mares, Jesus O.; Woods, Daniel C.; Baker, Caroline E.; Son, Steven F.; Rhoads, Jeffrey F.; Bolton, J Stuart; and Gonzalez, Marcial, "Localized Heating Near a Rigid Spherical Inclusion in a Viscoelastic Binder Material Under Compressional Plane Wave Excitation" (2016). *Publications of the Ray W. Herrick Laboratories*. Paper 139. <http://docs.lib.purdue.edu/herrick/139>

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November 14, 2016

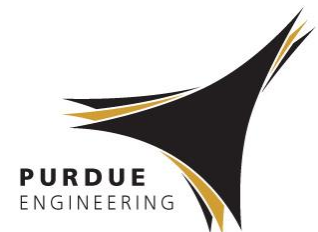
ASME 2016 International Mechanical Engineering Congress and Exposition (IMECE 2016)

Localized Heating due to Stress Concentrations Induced in a Lossy Elastic Medium via the Scattering of Compressional Waves by a Rigid Spherical Inclusion

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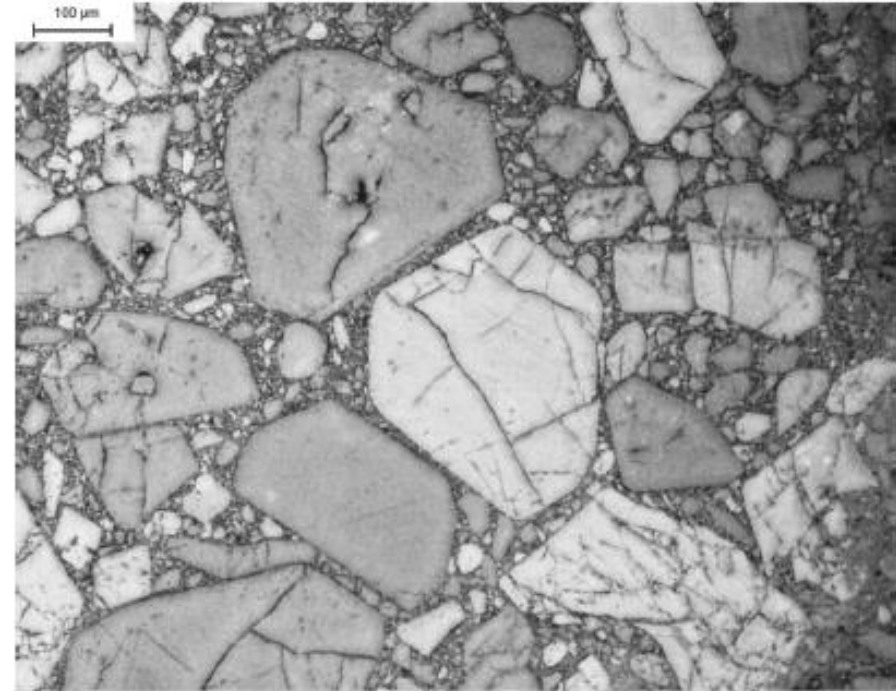
AFOSR Grant No. FA9550-15-1-0102
Program Officers: Dr. Jennifer Jordan
Dr. Martin Schmidt





Energetic materials in a binder

- Common use of energetic crystals involves embedding them in a binder
- Behaviors of interest include mechanical interactions between crystals, mechanical behavior of the binder and crystals separately, and interactions between the binder and crystals.
- Loading conditions include impact and periodic excitation
- Periodic excitation involves high strain-rate behaviors, even if overall strain rate is low
- Complex structure makes coupled mechanisms difficult to isolate

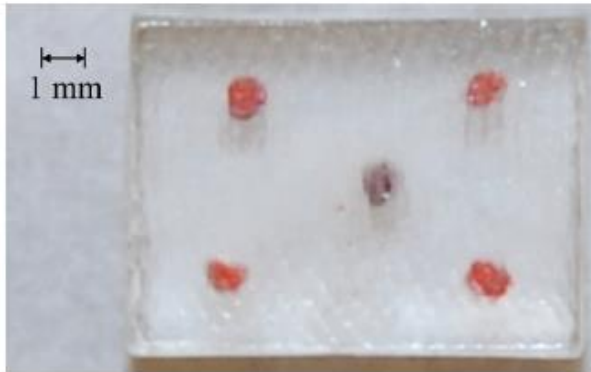


Micrograph of PBX 9501 (HMX in estane based binder)
Berghout, et. al., 2002, Combustion of damaged PBX explosive

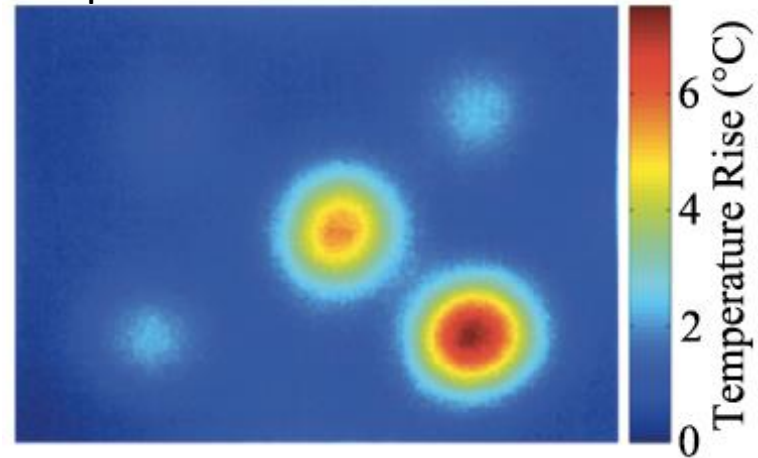


Experimental Motivation

750-800 μm AP crystals to undergo excitation



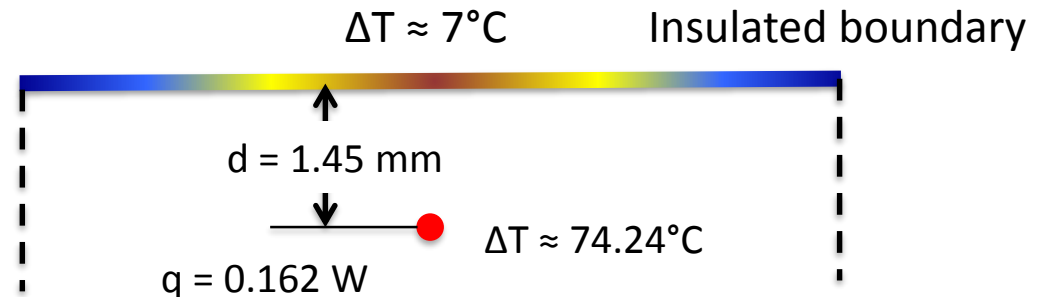
Surface temperature rise of 750-800 μm AP particles after 2 s excitation



Mares, et. al., *Journal of Applied Physics* 116, 204902 (2014); doi: 10.1063/1.4902848



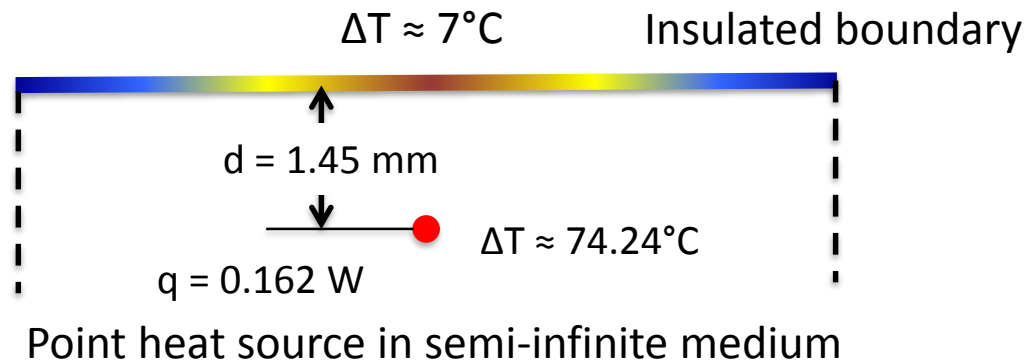
Single-crystal sample under ultrasonic excitation (image adapted from Miller et al., J. Appl. Phys., 2016)



Point heat source in semi-infinite medium



Experimental Crystal Heating Rates



- Analytical approximation using semi-infinite medium solution for heat source magnitude q and depth d (varies due to morphology)
- Particle surface temperature is found by applying the same solution with given q at the particle radius
- 37°C/s for 750-950 μm HMX in Sylgard[®] at 215 kHz
- 125°C/s for 400-500 μm AP in Sylgard[®] at 215 kHz



Ideal problem setup

Assumptions:

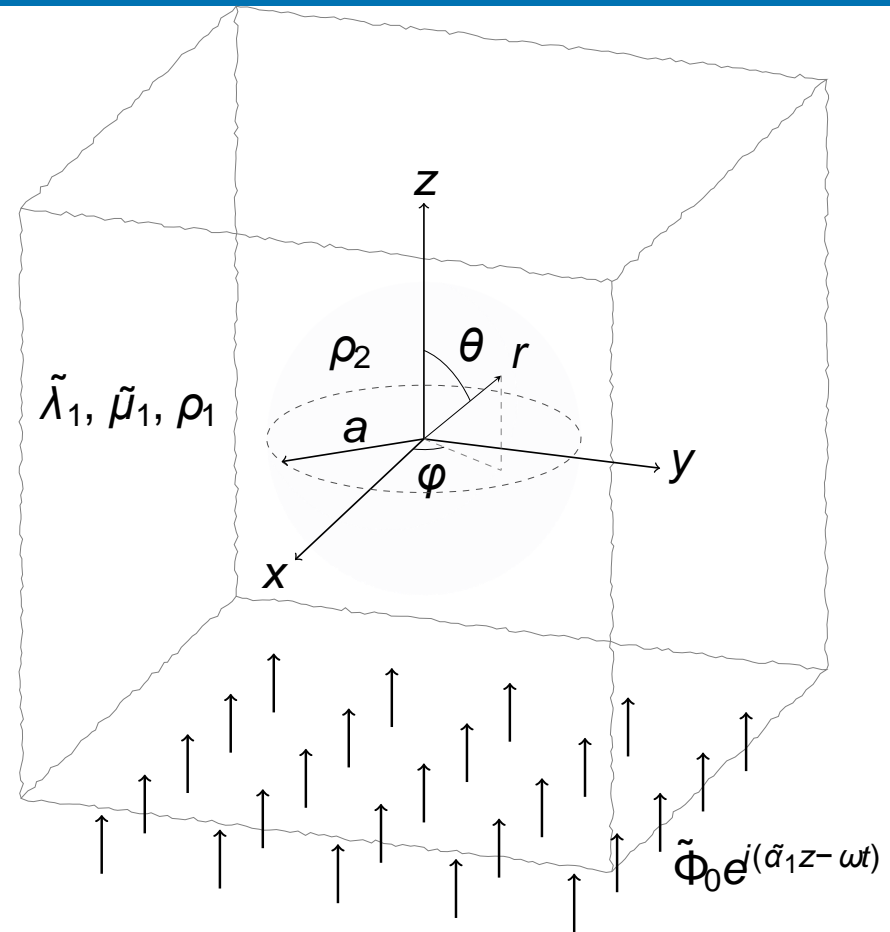
- Rigid spherical particle (no intrinsic heating)
- Linear viscoelastic binder
- Planar incident wave
- Perfect bonding between binder and particle (no particle/binder friction)
- Thermal stresses negligible
- Temperature-independent parameters

Boundary conditions:

- Displacement of binder = displacement of particle at boundary
- Newton's second law: stresses integrated over particle surface produce acceleration

Numerical Solution parameters:

- 1- μm wave amplitude
- 500- μm HMX particle
- Sylgard binder
- 500-kHz excitation frequency



Simplified diagram of single-particle embedded in a viscoelastic binder

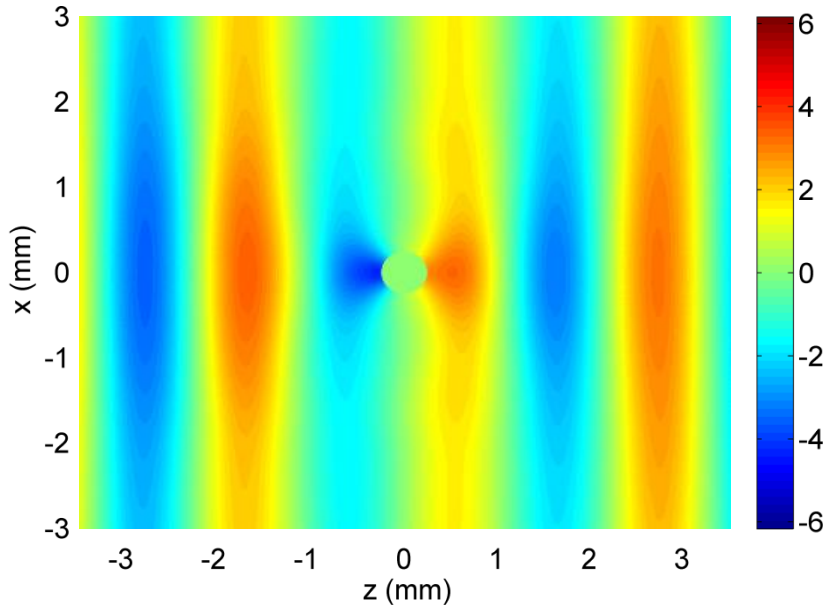


Stress Solution

- Solved by Pao and Mao in 1963 for linear elastic binder
- Expanded to lossy viscoelastic binder by Gaunard and Uberall in 1978
- Solved for lossy inclusion by Hinders, et. al. in 1994
- Solved with FE simulation by Chervinko in 2007

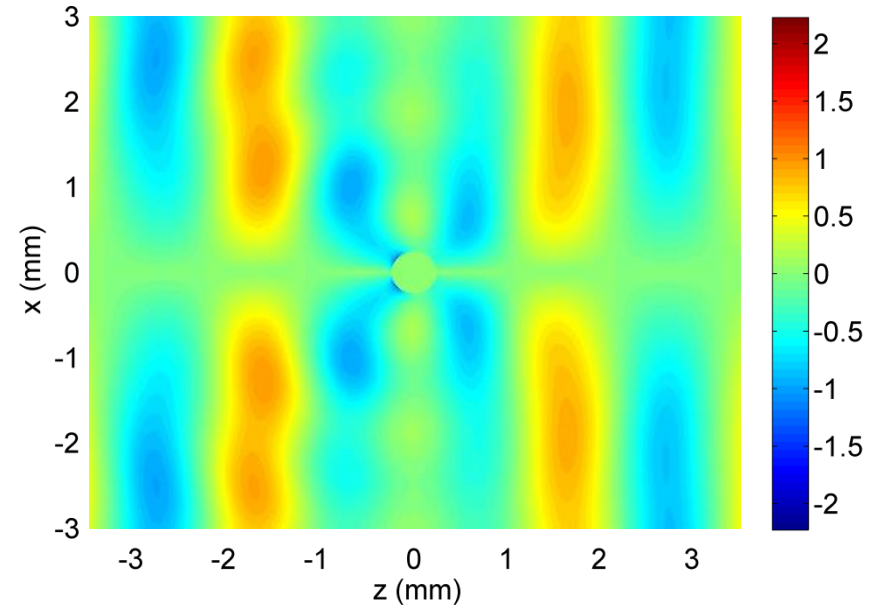
Real component of
radial stress:

$$\Re(\tilde{\sigma}_{rr})$$



Real component of
shear stress:

$$\Re(\tilde{\sigma}_{r\theta})$$



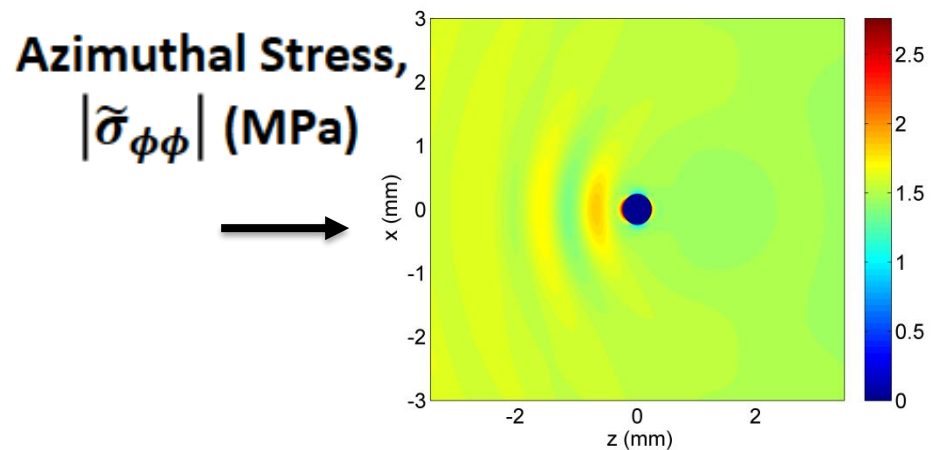
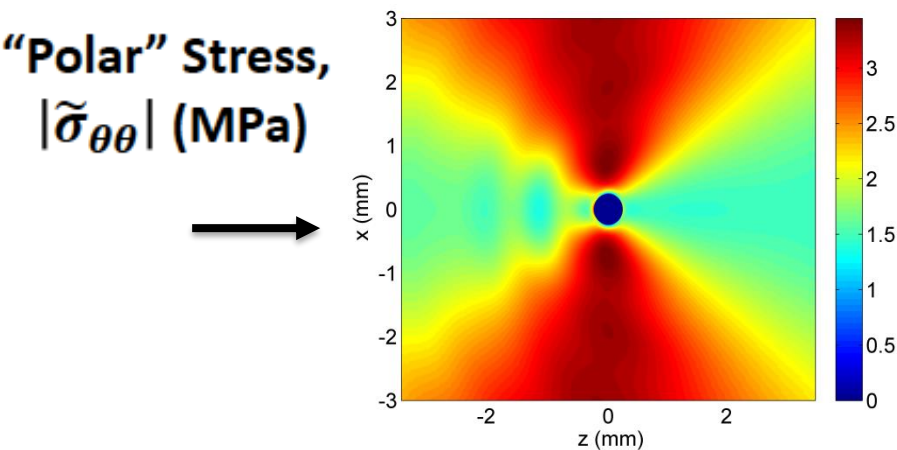
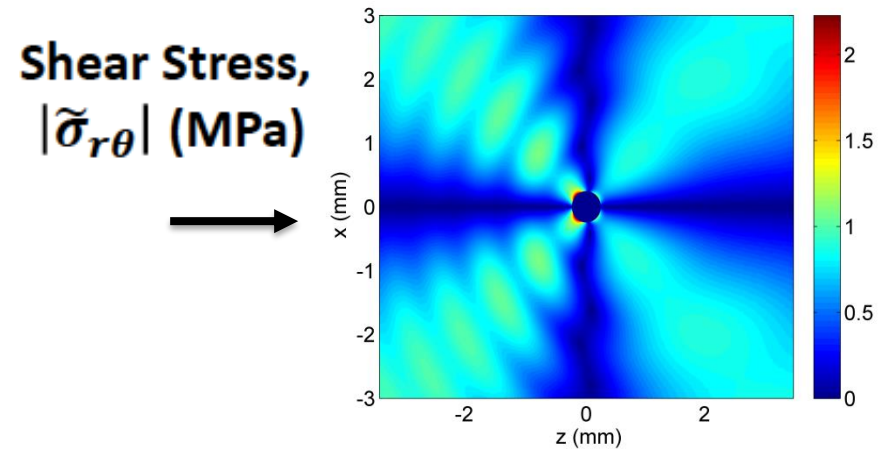
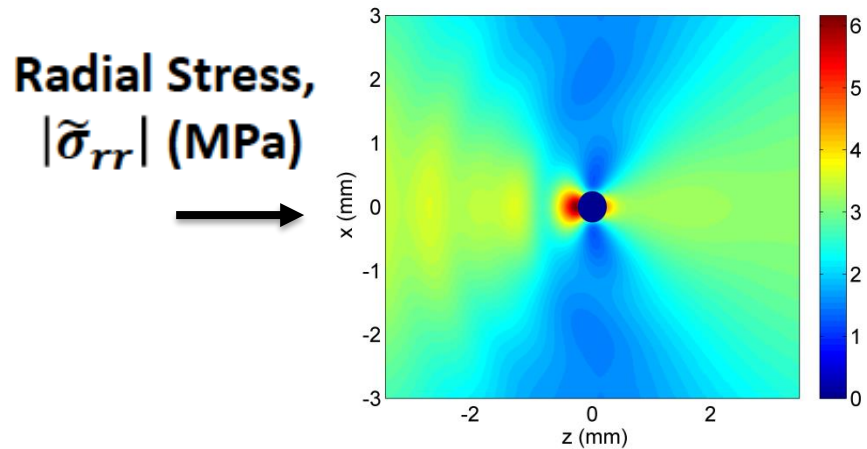
1- μm , 500-kHz harmonic plane wave excitation using Gaunard and Uberall expressions



Periodic Excitation of a Single Spherical Particle



- 1- μm , 500-kHz harmonic plane wave excitation
- 500- μm diameter HMX crystal in Sylgard

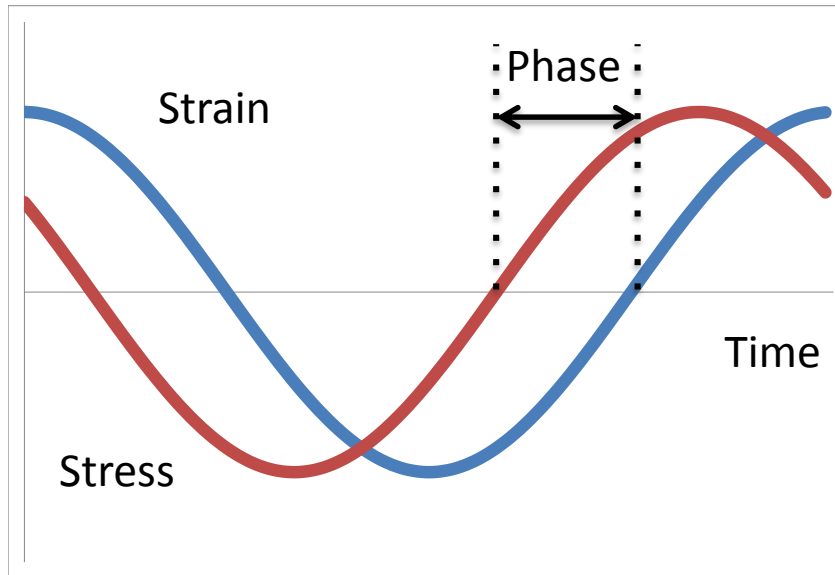




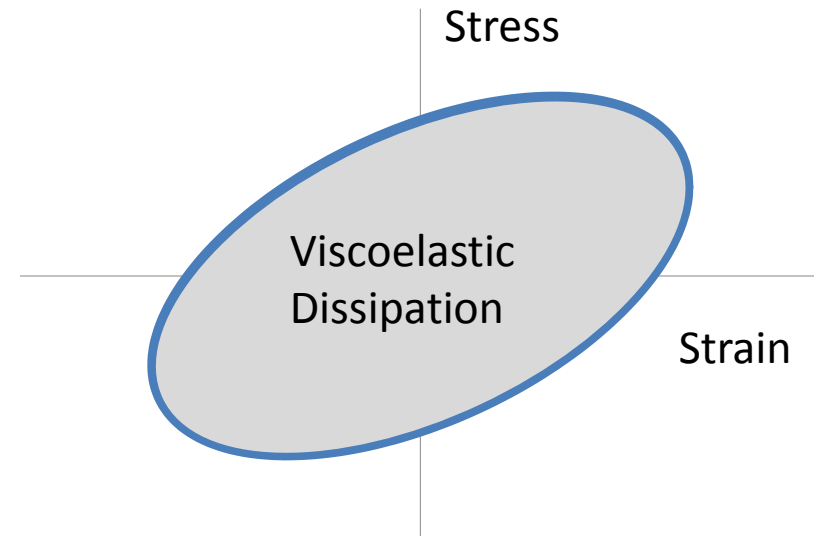
Viscoelastic Heating Model

- Based on losses in strain energy density per cycle of applied harmonic stress (hysteretic damping)

Single cycle of viscoelastic stress and strain



Phase plot of single cycle



Time-averaged heat generation (W/m³):

$$q = \frac{\omega}{2\pi} \int_{t_0}^{t_0+2\pi/\omega} \left(\sigma_{rr} \frac{\partial \epsilon_{rr}}{\partial t} + \sigma_{\theta\theta} \frac{\partial \epsilon_{\theta\theta}}{\partial t} + \sigma_{\phi\phi} \frac{\partial \epsilon_{\phi\phi}}{\partial t} + 2\sigma_{r\theta} \frac{\partial \epsilon_{r\theta}}{\partial t} + 2\sigma_{r\phi} \frac{\partial \epsilon_{r\phi}}{\partial t} + 2\sigma_{\theta\phi} \frac{\partial \epsilon_{\theta\phi}}{\partial t} \right) dt$$



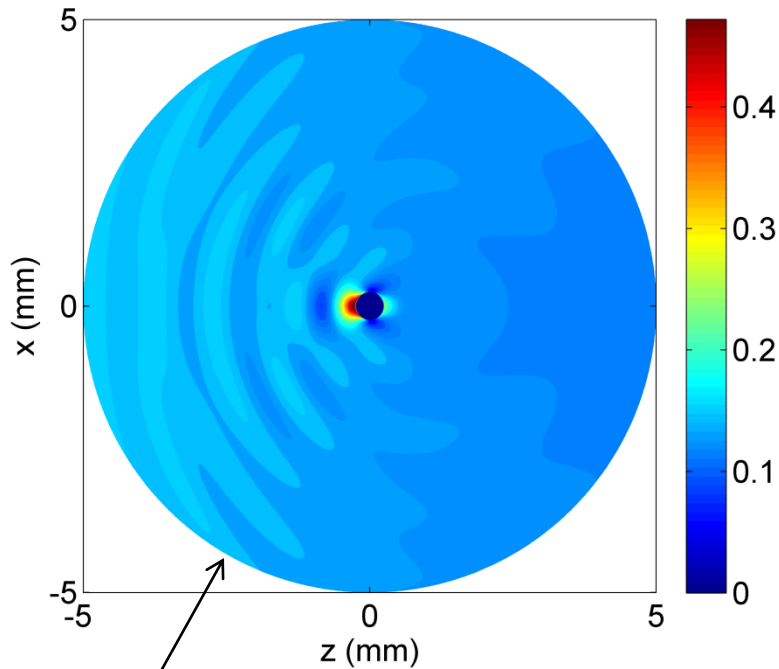
Heat Generation in HMX-Sylgard System



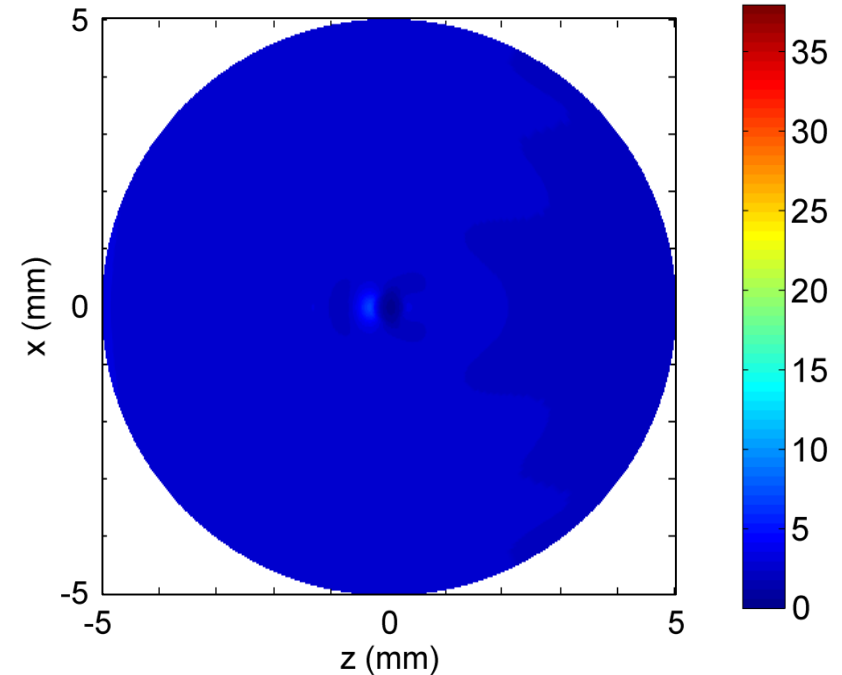
Fourier's law of conduction:

$$r_m c_{p,m} = k_m \left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin q} \frac{\partial}{\partial q} \left(\sin q \frac{\partial T}{\partial q} \right) \right] + q_m$$

**Time-averaged Heat Generation
(W/mm³)**



**Temperature Increases (°C)
from 0.05 to 0.5 s**



For the temperature solution, a free convective surface condition was applied at a large outer radius

1-μm, 500-kHz harmonic plane wave excitation

Animation shows 0.05 s increments, with one frame shown per second

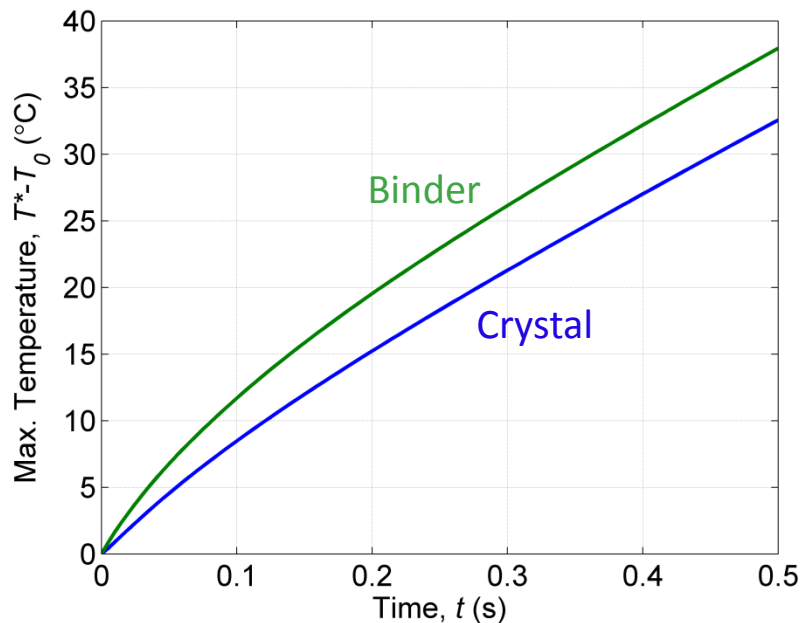


Temperature Increase in HMX-Sylgard System

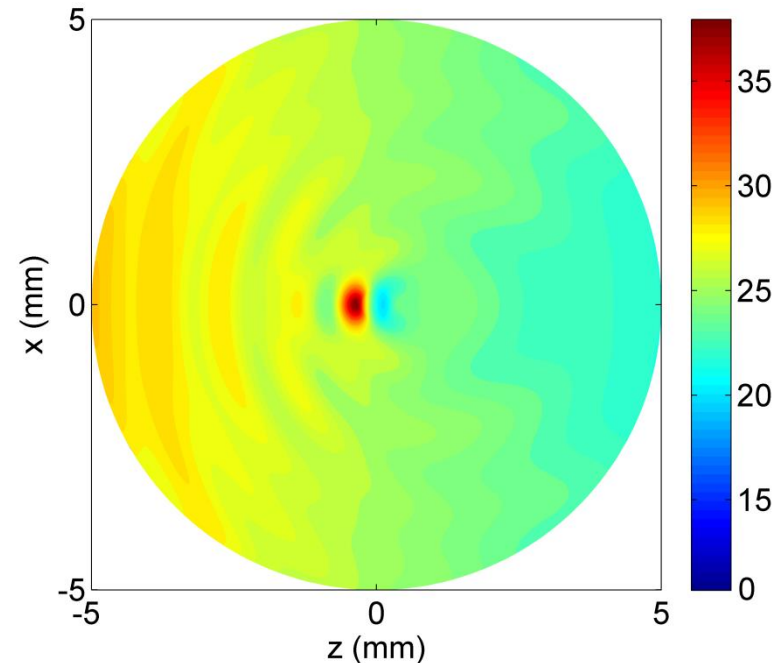


- **1- μm** , 500-kHz harmonic plane wave excitation

Transient Max. Temperature Increase of Crystal and Binder



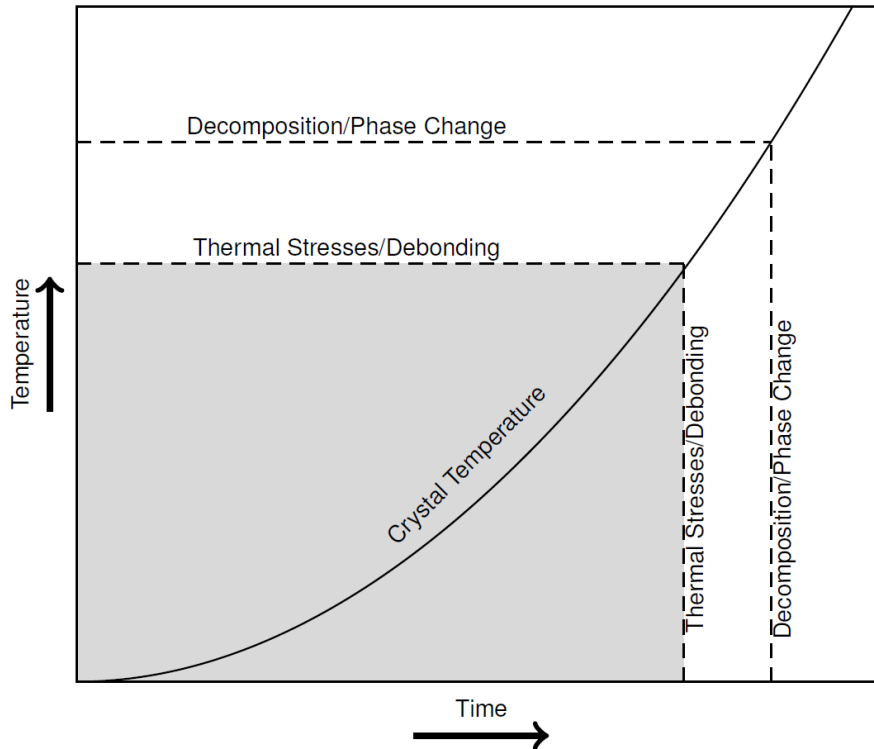
Temperature Distribution ($^{\circ}\text{C}$) at $t = 0.5$ s



Compares well to Mares, et. al. (2014) in which heating rate were estimated to be between 37 to 125 $^{\circ}\text{C}/\text{s}$ depending on shape, size, and identity of inclusion

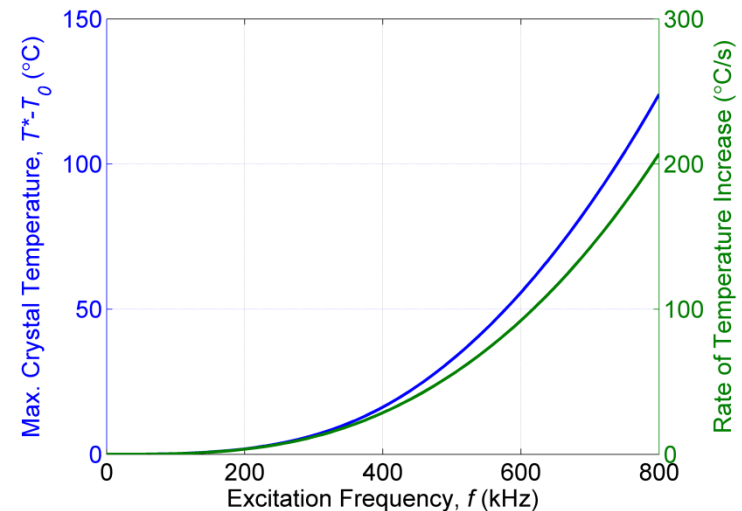
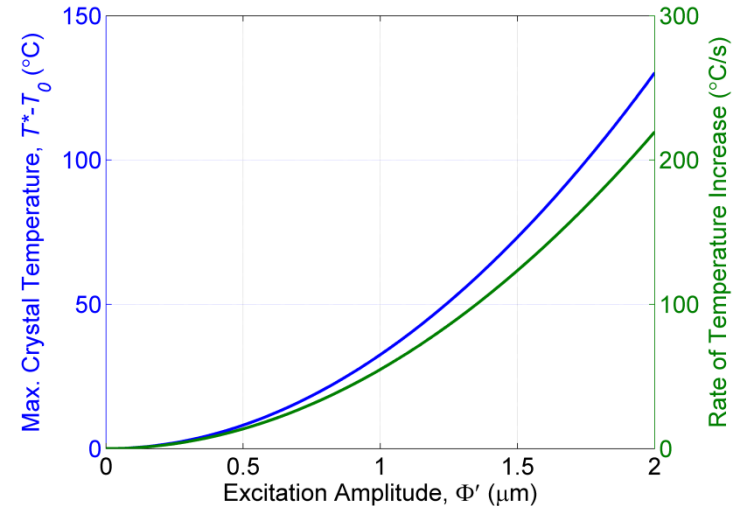


Future Modeling Efforts



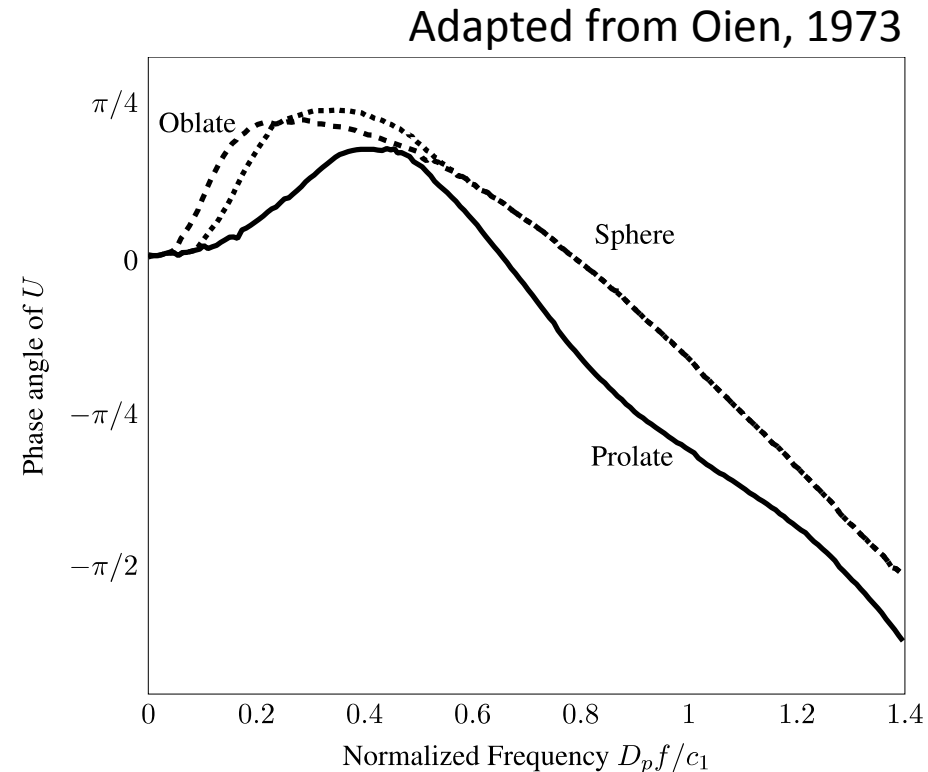
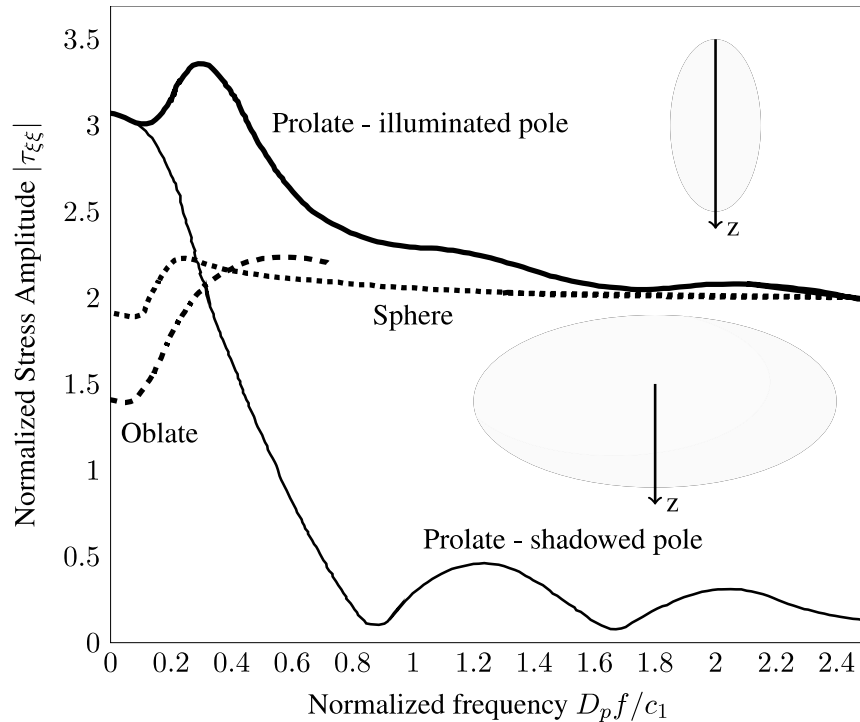
Mares et al., J. Appl. Mech., 2016 (Submitted).

- Effect of temperature-dependent parameters
- Non-linear viscoelasticity
- Thermal stress effects
- Debonding effects
- Effect of binder and particle properties





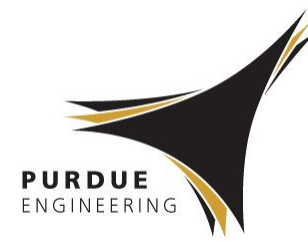
Future modeling efforts: Particle morphology



- Particle size and shape have a significant effect on stress amplitudes
- Relationship between frequency and particle size affects phase also
- Denser particle has larger vibrational amplitude



AFOSR Grant No. FA9550-15-1-0102
Program Officers: Dr. Jennifer Jordan
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Questions?

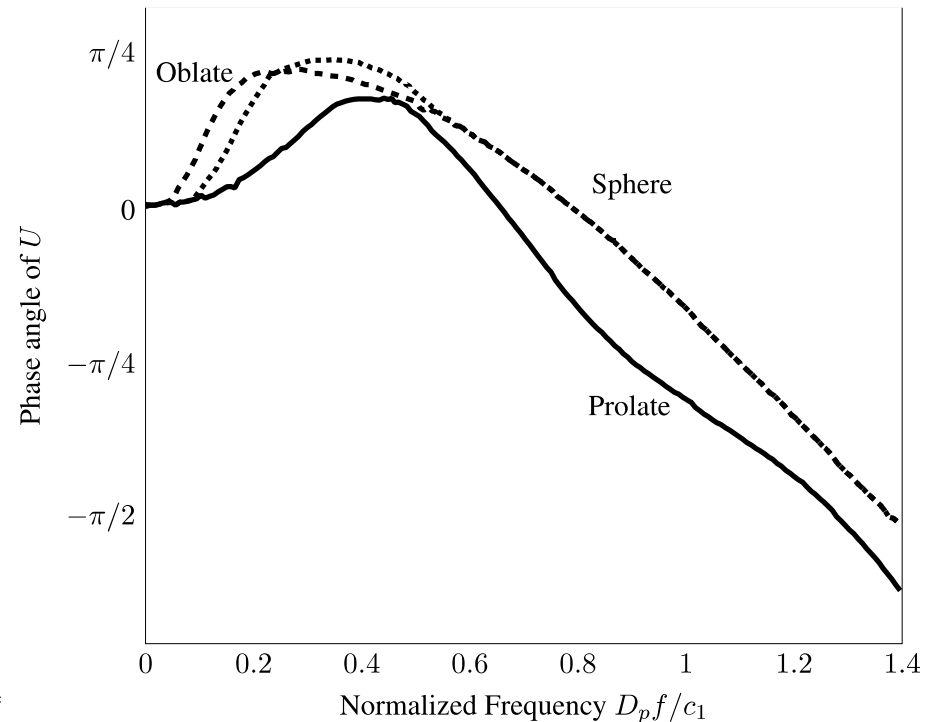
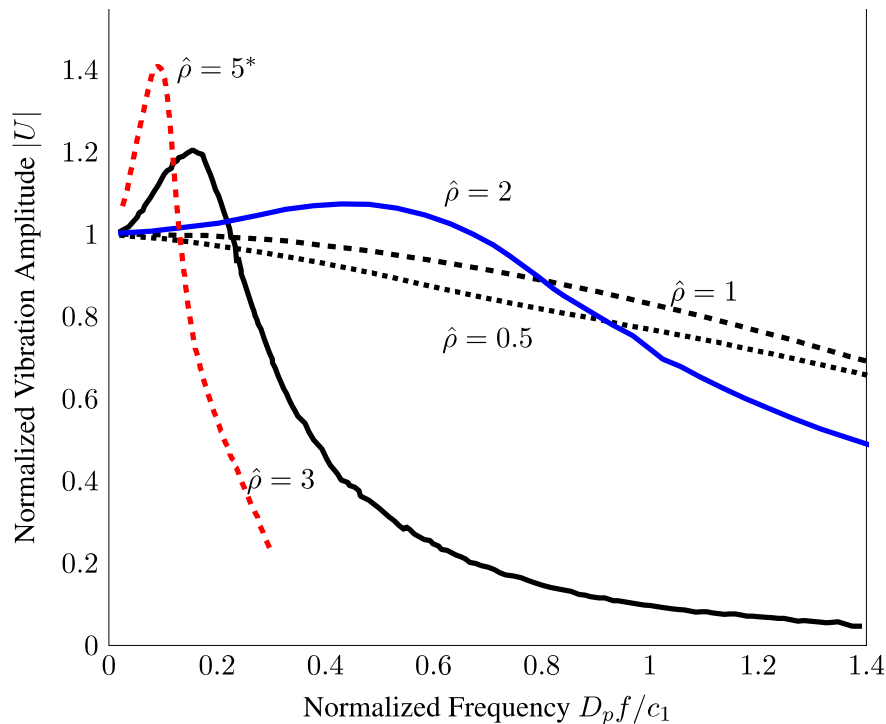


System dynamics

Particle motion described by Newton's second law:

$$\frac{4\pi a^3}{3} \rho \ddot{U} = \iint (\sigma_{rr} \cos\theta - \sigma_{r\theta} \sin\theta) a^2 \sin\theta d\theta d\varphi \Big|_{r=a}$$

Particle density affects vibration amplitude





Thermal Analysis Boundary Conditions



$$k_2 \frac{\partial T}{\partial r}(0, \theta, t) = -k_2 \frac{\partial T}{\partial r}(0, \theta + \pi, t),$$

$$T(a^-, \theta, t) = T(a^+, \theta, t),$$

$$k_2 \frac{\partial T}{\partial r}(a^-, \theta, t) = k_1 \frac{\partial T}{\partial r}(a^+, \theta, t),$$

$$k_1 \frac{\partial T}{\partial r}(R, \theta, t) = U_0 [T_0 - T(R, \theta, t)],$$

$$k_m \frac{\partial T}{\partial \theta}(r, 0, t) = 0,$$

$$k_m \frac{\partial T}{\partial \theta}(r, \pi, t) = 0,$$