

Characterizing Broadband Seismic Noise in Central London

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ABSTRACT

Recordings made at five broadband seismometers, deployed in central London during the summer of 2015, reveal the wideband nature (periods, T , of between 0.01 and 100 s) of anthropogenic noise in a busy urban environment. Temporal variations of power spectral density measurements suggest transportation sources generate the majority of the noise wavefield across the entire wideband, except at the secondary microseismic peak ($2 < T < 6$ s). The effect of road traffic is greatest at short periods ($T < 0.4$ s) where acceleration noise powers are ~ 20 dB larger than the New High Noise Model; at $T = 0.1$ s daytime root-mean-square acceleration amplitudes are 1000 times higher in central London than at an observatory station in Eskdalemuir, Scotland. Overground railways generate observable signals both at short periods ($T < 0.3$ s), which are recorded in close proximity to the tracks, and at very long periods ($T > 20$ s) which are recorded across the city. We record a unique set of signals 30 m above a subway (London Underground) tunnel interpreted as a short-period dynamic component, a quasi-static response to the train moving underneath the instrument, and a very long period ($T > 30$ s) response to air movement around the tunnel network. A low-velocity clay and sand overburden tens of metres thick is shown to amplify the horizontal component wavefield at $T \sim 1$ s, consistent with properties of the London subsurface derived from engineering investigations. We provide tabulated median power spectral density values for all stations, to facilitate comparison with any future urban seismic deployments.

Keywords: Noise, Urban, Subway, London

1 INTRODUCTION

2 Over the past 65 years there has been an increasing trend for people to live in large cities (United
3 Nations, 2014). Since 1990 the number of people living in cities with over 10 million inhabitants
4 ('megacities') has risen from 153 million to 453 million. Such environments are vibrationally noisy,
5 given the large volumes and dense concentrations of transportation networks and machinery. Urban
6 ground vibrations are of interest to a number of communities including, among others, engineering
7 seismologists (e.g., Fäh et al., 1997; Panou et al., 2005), seismic network operators (e.g., Thomas
8 et al., 2013), personnel detection specialists (Peck, 2008), and volcanic hazard assessors (e.g., Boese
9 et al., 2015). Therefore it is of interest to characterize noise level amplitudes in urban areas and to
10 identify the dominant sources. Here we report measurements of broadband noise across a network of
11 five broadband seismometers deployed in central London, UK, during the summer of 2015 (Figure
12 1). We provide an analysis of urban noise in a megacity in the early 21st century, and take care to
13 provide absolute noise power amplitudes such that they can be compared against measurements in other
14 metropolitan areas or any future noise surveys within London.

15 London, UK, is a city with a population of 10.9 million (United Nations, 2014), that has grown
16 around the River Thames approximately 60km inland from its exit into the North Sea. Reflecting
17 its almost 2000 year history, the city has a diverse range of urban environments and transportation
18 networks (Figure 1). The city is served by an extensive subway system (the London Underground)
19 and several mainline surface railway terminal stations. Road traffic density is high; in 2014 over 420
20 million miles of motor vehicle journeys were estimated to have been undertaken on major roads in
21 central London (Westminster & City of London, <http://www.dft.gov.uk/traffic-counts>, accessed April
22 2016).

23 London is situated on a broad syncline, referred to as the London Basin, and the subsurface has
24 been well studied due to the numerous geotechnical and hydrogeological investigations that have been
25 undertaken to support the construction of infrastructure (e.g., Royse et al., 2012). Beneath central
26 London, Paleozoic basement (predominantly sandstones) lies ≥ 350 m below the surface, with ~ 250 m
27 of Cretaceous sandstones, clays and chalks lying unconformably above (e.g., Sumbler, 1996). The chalk

28 has a thickness of ≤ 200 m and is mostly saturated, providing a major aquifer for the city's population.
29 Above the chalk sit Paleogene clay and sand deposits with thicknesses of many tens of metres. These
30 have greatly influenced the subsurface engineering beneath the city, especially the construction of the
31 London Underground which has exploited the advantageous tunnelling properties of the London clay
32 (e.g., Ellison et al., 2004; Royse et al., 2012). The geological sequence is topped in places, in particular
33 close to the river Thames and its tributaries, by Quaternary alluvium and river gravel deposits. In terms
34 of seismic response, it is expected that the upper tens of metres (clays, sands, gravels) will have low
35 wavespeeds compared to the chalk beneath (e.g., Bourbié et al., 1987).

36 The observations detailed in this paper highlight the absolute noise amplitudes and temporal noise
37 variations associated with a number of sources, including road traffic and the subway. We show that
38 the wideband noise field for periods between 0.01 and 100 s is controlled by anthropogenic sources,
39 except at the microseism peak. Our observations focus on vertical component noise amplitudes, in
40 order to minimise the effects of seismic wavefield amplification in weak sediments (e.g., Lermo and
41 Chávez-García, 1993). As predicted by a model derived from engineering investigation data, horizontal-
42 to-vertical component spectral ratios at each station show that site effects in London are dominated by
43 the upper tens of metres of sediments which exhibit very low (< 400 m/s) shear wavespeeds.

44 **METHODS**

45 Five three-component broadband seismometers were deployed within buildings in central London
46 between mid-July and early-September 2015. The deployments varied between two and six weeks in
47 length, depending upon access to the host facility. Instrument details and deployment dates are given in
48 Table 1. Within each building the seismometer was deployed on a concrete floor in the lowest level
49 of the building; three were in basements and two were at ground level. Care was taken to minimize
50 proximity to air-conditioning units and areas of heavy footfall, and the seismometers were encased in
51 foam to reduce thermal effects at long periods. Sampling rates were set at 200 samples per second
52 (sps), except IMP which was set at 100 sps.

53 Pre-processing of all data involved removing the manufacturer supplied instrument response, to
54 produce velocity seismograms. Where necessary for the analysis these traces were differentiated

55 to provide acceleration seismograms, or integrated to provide displacement seismograms. Prior to
56 integration a high-pass filter that suppressed periods >200 s was applied in order to reduce artifacts
57 associated with deconvolving near-zero instrument response levels.

58 To assess ambient seismic noise power levels across central London, Probability Density Functions
59 (PDFs) of Power Spectral Density (PSD) estimates were constructed using the methodology of McNa-
60 mara and Buland (2004). In summary, this method takes all data recorded on a seismometer component
61 and generates PSD estimates for each half-hour data segment using an averaged windowed Fourier
62 Transform method. The use of half-hour segments is our one variation from the method of McNamara
63 and Buland (2004) who use one-hour segments; the shorter windows allow us to provide better time
64 resolution. The PSD estimates are subsequently smoothed over one-octave bands at $1/8$ octave intervals.
65 These smoothed PSD estimates are used throughout this paper to identify temporal variations in noise
66 power at particular periods.

67 PSD estimates for each $1/8$ octave interval across all half-hour data segments were accumulated into
68 1 dB wide power bins, from which the PDF as a function of noise power for each frequency interval
69 was calculated (e.g., Figure 2). This processing technique has the advantage of not requiring data
70 preprocessing to identify quiet periods (as for example, in Peterson, 1993); for urban noise studies,
71 restricting the study to only quiet periods would significantly reduce our ability to identify temporal
72 variations in noise levels.

73 Half-hour smoothed PSD estimates for the three components of motion were also used to calculate
74 horizontal-to-vertical spectral ratios (HVSRs) at each station. The horizontal spectrum is taken to be
75 the geometric mean of the measured north and east components. Our calculations closely follow the
76 methodology of McNamara et al. (2015), but due to the short time period of data collection (two weeks
77 at the shortest deployment) we took the median HVSR value at each frequency from all half-hour
78 HVSRs to represent the average station HVSR (rather than the median of daily averages). The narrow
79 spread of HVSR values across all half-hour records in the period range of interest, as shown in the
80 results in Figure 6, suggests this is justified.

81 The following conventions are used throughout the paper. For comparison with McNamara and
82 Buland (2004) and Peterson (1993) we report noise power levels in units of decibels (dB) with respect

83 to $1 \text{ (m}^2/\text{s}^4)/\text{Hz}$, i.e., acceleration power. For example, a difference of 10 dB is equivalent to one order
84 of magnitude change in power, or a factor of 3.16 in root-mean-square (RMS) acceleration amplitude,
85 while a difference of 20 dB is equivalent to two orders of magnitude change in power and one order of
86 magnitude change in RMS amplitude (see, for example, Box 12.1 of Aki and Richards, 2002, for a short
87 explanation of decibel scales). All times in this paper are reported as Coordinated Universal Time (UT),
88 however it should be noted that the UK observes daylight saving hours during summer months (British
89 Summer Time, or BST) which is one hour ahead of UT, i.e., $\text{BST} = \text{UT} + 1$. A final convention is that
90 we refer to the London Underground as a subway, as this term is more widely used in the literature.
91 However, Londoners wouldn't recognize this description; in the city it is simply referred to as "the
92 Tube".

93 **OBSERVATIONS ACROSS LONDON**

94 The calculated vertical component noise power PDFs indicate, unsurprisingly, that seismic noise levels
95 in London are high with respect to observatory seismometer installations (Figures 2 and 3). In particular,
96 at periods, T , less than 0.8 s, the noise acceleration power levels increase rapidly to values up to 20 dB
97 higher (a factor of ten increase in RMS amplitude) than those of the New High Noise Model (NHNM;
98 Peterson, 1993).

99 At periods $T < 0.1$ s noise power levels are controlled by local sources. For example, at SJP
100 the subway beneath it generates a broadband (0.01 to 0.1 s) signal peaked at $T \sim 0.02$ s. The high
101 acceleration powers at $T = 0.04$ s exhibit an almost 20 dB reduction during the brief 4.6 hour weekday
102 night-time period when subway trains do not run (Figures 2 and 4a,c). Similar diurnal effects are
103 observed at LFS, located 60 m from one of London's main overground railway routes. The signal is
104 broadband (0.015 to 0.3 s), with a longer peak noise period (0.15 s) than that observed for the subway at
105 SJP. In contrast to rail traffic noise, at IMP the noise at $T = 0.04$ s is dominated by a source, likely to be
106 an air conditioning unit, that turns on at 06:00 and shuts down at 23:00 UT generating a 19 dB power
107 variation (Figure 4b,d).

108 At slightly longer periods ($0.1 < T < 0.4$ s) the noise spectra exhibit the same elevated levels (above
109 the NHNM) until a rapid reduction in noise power of approximately 30 dB between $T = 0.4$ s and

110 $T = 1.5$ s result in the noise spectra at all stations falling below the NHNM. This suggests that at these
111 periods anthropogenic noise sources generate less power, with natural noise sources starting to dominate.
112 This is consistent with the cessation of diurnal variations at longer periods ($1.5 < T < 20$ s). These
113 results are comparable to recordings from Bucharest, Romania, where Groos and Ritter (2009) found
114 that both man-made and natural sources contributed significantly to noise in the range $1 < T < 1.7$ s,
115 while at longer periods natural sources had larger amplitudes.

116 The secondary microseismic peak is observed at $2 < T < 6$ s (see diffuse noise in Figure 4a,b). At all
117 stations, apart from SJP where broadband subway noise dominates (Figures 3 and 4a,c), the amplitude
118 of the microseism is comparable, with a median level of ~ -123 dB during the deployment period. At
119 periods greater than the microseism peak ($T > 6$ s) there is, like at very short periods, larger inter-station
120 variability. The quieter stations (IMP, ALB and LFS) exhibit noise levels which fall within the global
121 population of observatory noise measurements (Peterson, 1993). At periods > 10 s these three stations
122 exhibit clear diurnal variations; at $T = 50$ s these variations are ~ 10 dB at ALB and IMP and almost
123 20 dB at LFS (see Figure S3, available in the electronic supplement to this article). The two noisiest
124 stations at $T > 6$ s (OWB and SJP) are those that are located closest to heavy transportation routes:
125 OWB was deployed in a basement beneath street level and close to a busy road, SJP was deployed
126 ~ 30 m above a subway line. The interpretation of the long-period vibrations at SJP is the focus of
127 section: London Underground Effects.

128 Occasionally it is the temporary absence of a persistent noise source that allows the vibrations
129 generated by the source to be quantified. One such event that occurred during the deployment was
130 the complete shutdown of the subway system between 2015-08-05 20:30 UT and 2015-08-07 04:00
131 UT due to industrial strike action. Of the three stations deployed on that date (OWB, SJP and IMP),
132 two stations (SJP, OWB) exhibited clear noise power reductions in response to the shutdown. At SJP,
133 where the station is located almost directly above the subway tunnels, clear reductions are observed
134 at $T < 0.04$ s and $T > 4$ s, but not around $T = 0.4$ s (Figure 4a,c). At the very short periods ($T = 0.04$ s)
135 the power reduction is ~ 10 dB, accounting for 55% of the regular daytime power increase. At OWB
136 a 3 dB reduction in daytime power at $T = 0.04$ s was observed compared to the regular 5 dB daytime
137 power increase, suggesting that the subway located at a distance of ~ 100 m from OWB accounts for

138 60% of the noise power at these very short periods. The shutdown generated no observable effects for
139 $T > 0.1$ s at OWB. No noise power decreases caused by the subway shutdown were observed at IMP,
140 which is located at a distance of ~ 600 m from the nearest subway line (Figure 4b,d). For conciseness,
141 only results for SJP and IMP were included in Figure 4. Interested readers will find graphical results
142 for all stations in the electronic supplement to this article (Figure S2).

143 The observation that $T = 0.4$ s noise power at SJP is not reduced by the subway shutdown suggests
144 that at this period the noise spectrum is dominated by another source (Figure 4c). Spectral variations
145 across the 0.4 to 1.5 s passband are similar across all five stations (Figure 3), suggestive of a common
146 city-wide generation mechanism. The most likely candidate is road traffic noise. The observation that
147 variations at $T = 0.4$ s are diurnal at both SJP and IMP (Figures 4e and f), with maxima at approximately
148 the time of the morning rush-hour (07:30 UT, 08:30 BST) and similar absolute amplitude variations
149 (between -103 and -91 dB) suggest a ubiquitous anthropogenic source. The temporal gradients in noise
150 power levels at $T = 0.4$ s are consistent with gradual changes in traffic volume, rather than the abrupt
151 changes in power observed for example when air-conditioning units are turned on or off (Figure 4d at
152 $T = 0.04$ s) or when trains start or stop travelling around the subway (Figure 4c at $T = 0.04$ and 4 s). The
153 observation that the daytime power at $T = 0.4$ s is reduced by greater than 2 dB at weekends compared to
154 weekdays, with Sundays exhibiting the largest reductions, is consistent with less traffic flow in London
155 during the weekends. Moreover, during the weekend of 2015-08-01 and 2015-08-02, a large cycling
156 event caused the closure of many city centre streets close to OWB and SJP during daytime periods. An
157 increased reduction in noise at these stations compared to other weekends for $0.04 < T < 0.6$ (Figure
158 4a) indicates this passband is sensitive to road traffic noise.

159 In order to understand the increase in noise power due to urban sources, it is instructive to compare
160 the noise levels measured within London with those at permanent stations in the UK. We chose to
161 compare to two stations (Figure 1 and 3 inset). The first, BKN, is located on a concrete block in a
162 purpose built seismic vault above clay and gravel deposits of unknown thickness. BKN is in an area of
163 elevated daytime road traffic and within 10 m of offices and laboratories. The second, EKB, is located
164 in an underground purpose built seismic vault excavated to sit on unweathered Silurian sedimentary
165 bedrock within a quiet rural location (Truscott, 1964).

166 The noise power spectra for the London and rural stations only converge at the secondary microseis-
167 mic peak ($2 < T < 10$ s), providing additional evidence that even in cities ocean-swell generated noise
168 dominates at these periods. Significant differences between the urban (London) and rural stations are
169 observed at short periods ($T < 1$ s). The median daytime power level at EKB is between 51 and 58 dB
170 lower than in London at $T = 0.4$ s, increasing to between 56 and 65 dB at $T = 0.1$ s. At these periods
171 EKB is approximately a factor of 1000 quieter than central London in terms of RMS amplitude. At
172 BKN the median daytime noise levels at $T = 0.4$ s are only between 7 and 14 dB lower than in London,
173 reflecting both the greater volumes of daytime traffic around BKN compared to EKB and the soft rock
174 geology beneath the station leading to higher noise and signal amplitudes (e.g., Su et al., 1992). At
175 night the difference in noise levels at $T = 0.4$ s between London and EKB reduces slightly to ~ 48 dB
176 due to reduced traffic noise in London, while the difference between London and BKN increases to
177 20 dB due to a larger reduction in traffic noise in the rural area around BKN. At periods > 10 s the
178 rural and urban noise power levels again diverge, leading to order of magnitude differences in RMS
179 amplitudes.

180 For the five central London stations, tabulated values for the 5th percentile, median, and 95th
181 percentile noise PDFs, as a function of period (e.g., Figure 2), are provided as Table S1 (and graphically
182 in Figure S1) available in the electronic supplement to this article, to facilitate comparisons with future
183 urban seismic deployments.

184 **LONDON UNDERGROUND EFFECTS**

185 The evidence from the day of strike action suggests the influence of the London Underground (subway)
186 on the seismic noise field does not extend more than a couple of hundred metres from the tunnel
187 network in central London. However, recordings at station SJP indicate that train generated broadband
188 vibrations dominate close to the subway tunnels (Figures 4 and 5). SJP was located almost directly
189 above the two Jubilee Line subway tunnels within a room that, through a series of passageways and
190 shafts, was connected to the tunnel network. The exact position of the seismometer relative to the
191 subway tunnels isn't known, but in the vicinity of SJP the Eastbound/Westbound tunnels are located
192 approximately 25 m/35 m below the ground surface respectively (Willis, 1997).

193 The velocity seismogram of a subway train passing beneath SJP exhibits an approximately 13 s
194 long envelope, dominated by power at between $T = 0.012$ and 0.05 s (Figure 5a). Vertical peak particle
195 velocity (PPV) measurements for the first trains each day (always Eastbound) have a mean value of
196 4.2×10^{-5} m/s with a standard deviation of 0.7×10^{-5} m/s. PPV values generated by known Westbound
197 trains are approximately 60% of the amplitude of those generated by Eastbound trains (the direction of
198 travel for a subset of trains was confirmed by one author, DNG, who spent 40 minutes trainspotting on
199 the Westbound platform of Westminster station). These values are comparable to previous vibration
200 measurements taken above 28 m deep Bakerloo line tunnels; Degrande et al. (2006) found surface
201 vertical PPV values of $\sim 1 \times 10^{-4}$ m/s directly above the tunnels, dropping to $\sim 5 \times 10^{-5}$ m/s at a
202 horizontal distance of 10 to 20 m.

203 Taking advantage of the broadband seismometer response, we are able to identify long-period
204 subway generated phenomena in our data. When integrated to displacement, the vertical seismogram
205 reveals a smooth downward then upward motion lasting approximately 9 s (Figure 5a). For the first
206 Eastbound train each day the vertical downward displacement has a mean value of 5.9×10^{-6} m and a
207 standard deviation of 0.4×10^{-6} m. Values for Westbound trains are remarkably similar. We hypothesize
208 that this is the quasi-static response of the seismometer to the passage of the train beneath it (see Yang
209 and Hung, 2008, for modelling of such a phenomena). The weight of the train displaces the tunnel
210 downwards resulting in the downward motion of the seismometer above it; the tunnel rebounds once
211 the train has passed. Horizontal motions (not shown here) also exhibit a smooth displacement pulse,
212 with motion directed approximately to the North-East of the station before rebounding. Although the
213 horizontal amplitudes are over an order of magnitude larger than the vertical component ($> 1 \times 10^{-4}$ m)
214 the signal-to-noise ratio is poor due to significant long-period noise on the horizontal components.

215 The quasi-static displacements are superimposed on larger-amplitude, background oscillations with
216 dominant periods of ~ 100 s (Figure 5b). As these oscillations do not occur on Sundays (when the train
217 services start later) or the day of the strike, we conclude they are associated with the movement of
218 trains in the subway network. The initial phases of this oscillation are highly correlated across different
219 days (i.e., at 04:30), although at later times this correlation degrades. Considering the first train of the
220 day in detail (Figure 5c) reveals that the quasi-static response occurs at the same phase point of the

221 long-period oscillation each day (i.e., on the upward displacement, before the maximum), providing
222 further evidence that this oscillation is linked to the start-up of the trains in the Eastbound tunnel. We
223 hypothesize that this signal is the response of the seismometer to air-motion around the tunnel system,
224 generated by moving trains displacing the air (the piston effect). For example, Lin et al. (2008) show
225 results for an experimental study in the Taipai, Taiwan, subway system with air velocity variations
226 having dominant periods of between ~ 60 and 200 s as trains moved through the network.

227 In our investigation the room in which SJP was installed was connected via a series of passageways
228 to the tunnel network. Therefore, we suggest the long-period response is caused by air pressure changes
229 around the seismometer rather than the piston effect displacing the walls of the tunnel. The piston effect
230 mechanism is consistent with the inter-day correlation degradation as time progresses from 04:30 to
231 05:30 (Figure 5b). Initially the piston effect is generated by the first train through the network producing
232 similar waveforms (the response of the tunnel and seismometer system to a single train passing). Small
233 time-shifts (Figure 5c) reflect the slightly different times that train operations start each day (up to
234 90 s variability over the 15 days of recording). At later times the air piston signal is a superposition of
235 signals generated by a number of West and Eastbound trains. Because of small changes in train transit
236 times beneath SJP, the interference of the signals generates different seismic waveforms each day.

237 **SEISMIC EVIDENCE FOR A LOW-VELOCITY OVERBURDEN**

238 The observed seismic noise amplitudes are controlled by both the noise source amplitudes and the
239 subsurface seismic propagation conditions. As described in the introduction, the upper tens of metres
240 of the geological profile beneath central London are predominantly clays and sands.

241 We utilize the horizontal-to-vertical spectral ratio (HVSr) method (see Methodology section) in
242 order to probe the subsurface structure using the noise data. Clear HVSr peaks are identified at
243 approximately 1 Hz (Figure 6b and c) which we interpret as the primary sediment layer response
244 frequency (e.g., Nakamura, 1989). These peaks are well defined across all time periods (Figure 6b),
245 and are not significantly broadened at times of higher noise amplitudes.

246 To guide our investigations, and for the purposes of seismic propagation modelling (not shown), the
247 British Geological Survey constructed a highly simplified 3D four-layer model for the central London

248 subsurface. The layers are identified as: (1) overburden, which incorporates all superficial and bedrock
 249 lithologies above the chalk, (2) unsaturated chalk, (3) saturated chalk, where the distinction between
 250 unsaturated and saturated is derived from observed groundwater levels across the Greater London
 251 area (Environment Agency, 2015) and (4) bedrock, consisting of all lithologies beneath the chalk to a
 252 nominal depth of 5000m below Ordnance Datum. Using geotechnical parameters measured during
 253 extensive ground investigations throughout London, depth-dependent seismic velocities (V_p, V_s) and
 254 material densities (ρ) were attributed to each layer (e.g., Figure 6a and Table 2). The model identifies a
 255 sharp seismic transition between Paleogene sediments in the overburden (subscript o), and the chalk
 256 (c); shear wave impedance contrasts ($\rho_o V_{s,o} / \rho_c V_{s,c}$) for the profiles beneath the five seismometers are
 257 estimated as 0.27 ± 0.01 .

258 The generation mechanism for HVSR peaks is not fully understood, with the relative contributions
 259 of vertically incident SH waves and the ellipticity of the fundamental Rayleigh wave still keenly
 260 debated (e.g., Nakamura, 2000; Fäh et al., 2001). However, numerous studies (e.g., Ibs-von Seht
 261 and Wohlenberg, 1999) show that HVSR spectral peaks are consistent with the shear wave resonance
 262 frequency, f_{est} (Hz), of a single sediment layer estimated as,

$$f_{\text{est}} = \frac{V_{s,o}}{4H_o}, \quad (1)$$

263 where $V_{s,o}$ is the mean shear-wave speed in the overburden (m/s) and H_o is the overburden thickness
 264 (m) taken in our study to be the depth to the chalk. Although probing the physical mechanism for
 265 the HVSR technique is beyond the scope of this paper, we note the similarity of Equation 1 to the
 266 theoretical relationship between vertical P wave resonance in low-velocity sediments and the Rayleigh
 267 wave spectral amplitude peak (Hudson and Douglas, 1975), suggesting an analogous relationship may
 268 exist for the SH wavefield.

269 Despite the simplifying assumption of a single-velocity overburden layer, the f_{est} values are
 270 consistent with the measured peak frequencies (f_{measured}) of ~ 1 Hz (Table 2) although f_{est} consistently
 271 underestimates f_{measured} by between 7 and 25%. We note that some of the inter-station variability
 272 is captured by the model. For example, the larger sediment thickness at IMP leads to a lower f_{est}

273 prediction compared to the other stations, which is clearly seen in the data (Figure 6c). As a check that
274 the methodology is not generating spurious 1 Hz peaks, the HSVR at the hard rock seismic vault EKB
275 was also calculated. As anticipated, the results show no sediment layer resonance (Figure 6c).

276 The good correspondence between observed and predicted HVSR peaks indicate that the very low
277 median shear wavespeeds in the overburden (~ 250 m/s), estimated from engineering investigations,
278 correctly reflect the subsurface wavespeed structure. Previous work suggests that HVSR peaks are
279 generated by a large amplification of the horizontal wavefield by the low-velocity overburden, compared
280 to the low or negligible amplification of the vertical wavefield (e.g., Lermo and Chávez-García, 1993).
281 In the case of central London the method is highly sensitive to the large impedance contrast between
282 the low velocity sands and clays and the higher velocity chalk. The implication is that comparison of
283 vertical noise power spectra between urban areas is likely to provide information regarding the sources
284 of noise, whereas comparison of horizontal spectra will contain both source and site information. In
285 the case of London, the low-velocity overburden appears to amplify horizontal noise power at ~ 1 s
286 (predominantly road traffic noise) by a factor of 4 (approximately 6 dB) compared to the vertical noise
287 power.

288 **DISCUSSION**

289 The observation that central London is subject to high amplitude seismic noise when compared to
290 observatory grade stations is not surprising, yet comparison with other urban areas is difficult. While a
291 number of other cities have been subject to seismic noise investigations (e.g., Fäh et al., 1997; Groos
292 and Ritter, 2009; Riahi and Gerstoft, 2015), there are few reports of standardized power spectral
293 density estimates. An exception to this is a study of noise at a single site in Auckland, New Zealand
294 (Boese et al., 2015), a coastal city with a population of approximately 1.4 million (2013 figures,
295 <http://www.stats.govt.nz>, accessed April 2016). Boese et al. (2015) show that median surface daytime
296 noise values in the 0.1 to 0.4 s passband fall between -110 and -120 dB, approximately 20 dB (a factor
297 of 10 in RMS amplitude) less than the values reported across London and more comparable with those
298 seen at the semi-rural UK station BKN (Figure 3). However, Boese et al. (2015) show that at the
299 noisiest times there is a distinct shift towards noise values of between -90 and -110 dB in the 0.1 to 0.2 s

300 passband, which are within the range of noise values observed in central London. Because these high
301 noise values are prevalent at times of high road use (1:30 to 3:30pm local time), Boese et al. (2015)
302 suggest that heavy traffic is the source. Other differences between the urban noise spectra can also
303 be observed; reflecting Auckland's position close to shallow coastal waters, the microseismic noise is
304 approximately 10dB greater than observed in London.

305 The sources of noise across the central London network are closely linked to transportation networks:
306 road, rail and subway. The spectral signatures of each transportation type agree well with previous
307 studies (Table 3).

308 Road traffic noise appears to dominate recordings between 0.1 and ~ 1.5 s in central London, with
309 remarkably similar spectral content across all stations (Figure 3). This is in contrast to a study of traffic
310 generated noise in Long Beach, California, which showed an increase in longer period (0.25 s) noise at
311 stations closer to an interstate highway compared to stations close to local roads (Chang et al., 2016).
312 A likely reason for this difference is that in contrast to the fast moving heavy goods vehicles on the
313 US interstate, throughout central London traffic density is high, and traffic speeds are low, leading to
314 a more homogeneous distribution of traffic sources. Indeed, at $T=0.4$ s the noise levels at OWB and
315 SJP are very similar (Figure 3c and d) even during periods when the subway is running almost directly
316 beneath SJP, indicating the dominance of road traffic noise at these periods.

317 The observations of three types of signal (dynamic, quasi-static and air-piston) associated with the
318 passage of subway trains beneath station SJP highlights the complicated nature of the wavefield close
319 to moving sources. The use of broadband seismometers is key to revealing the long-period wavefield
320 associated with mass movement (the quasi-static response) and air motion (the long-period oscillations).
321 We do not attempt to model the subway generated quasi-static displacement amplitudes. Although
322 such modelling has been undertaken previously (e.g., Yang and Hung, 2008), at SJP any model will be
323 poorly constrained as a result of uncertainties including the position of the tunnels with respect to the
324 seismometer, the properties of the geological overburden, and the distribution of the moving load.

325 Non-transportation sources will also contribute to the seismic noise spectra. Groos and Ritter (2009)
326 observed increased short-period (0.02 to 0.04 s) noise close to areas of heavy industry in Bucharest,
327 Romania, suggesting that machinery noise can dominate at very short periods. Due to the lack of heavy

328 industry in central London we do not observe such features, although it is suspected that air-conditioning
329 units generated the short-period signal ($T=0.04$ s) at IMP (Figure 4d).

330 Strong wind has also been shown to generate seismic noise in urban environments (e.g., Groos and
331 Ritter, 2009; Boese et al., 2015). In Bucharest, seismic power increases could be correlated with periods
332 of strong wind in a period range of 0.8 to 1.7 s, a transitional zone between man-made signals at shorter
333 periods and microseismic noise at longer periods (Groos and Ritter, 2009). In London strong diurnal
334 noise associated with transportation sources is observable up to periods of $T=1.5$ s, and the influence
335 of the microseism is apparent at $T>2$ s (Figures 3 and 4). This leads to a narrowband transition zone
336 between the two that, unlike in Bucharest, does not exhibit a significant reduction in noise power.
337 Therefore we suggest any significant wind generated noise signature in the London dataset is masked
338 by stronger sources (see Figure S4, available in the electronic supplement, for a comparison of noise
339 timeseries with wind speed data collected 12 km east of Westminster at London City airport).

340 The increased, and diurnally varying, noise amplitudes for $T > 20$ s at stations ALB, LFS, and IMP
341 are unexplained. Groos and Ritter (2009) suggested that such long-period motions could be caused
342 by tilting of high-rise buildings under wind load (e.g., Breuer et al., 2008), however this is unlikely to
343 generate the strong observed diurnal effects. In contrast, Sheen et al. (2009), show convincing evidence
344 that diurnally varying noise in the 20 to 100 s passband recorded in both South Korea and the US can
345 be attributed to vibrations generated by nearby trains (both overground and subway). This is consistent
346 with the diurnal noise variations at $T > 20$ s for stations ALB, LFS, and IMP, and the observation that
347 the diurnal power variations are 10 dB greater at LFS which is situated ~ 60 m from a major set of
348 overground trainlines. Moreover, no reduction in power at these periods was observed at IMP during
349 the subway strike, suggesting these variations are predominantly due to the overground railway in
350 London.

351 Given the sparse nature of the deployed network, the amplitude decay of seismic waves with in-
352 creasing distance from the transportation networks is poorly constrained. During the subway shutdown,
353 stations within 100 m of the tunnels experienced a $\sim 60\%$ reduction in daytime noise at $T=0.04$ s while
354 at 600 m from a tunnel the shutdown had no effect at the same period. Future studies focusing on
355 measureable vibration decay away from subways such as the London Underground may benefit from

356 focusing upon ranges between 100 and 500 m from the tunnels.

357 In addition to the high density of potential seismic noise sources in central London, the elevated
358 noise amplitudes could also be a result of site effects. HVSR results confirm that the upper tens of
359 metres beneath the stations is composed of low average ($V_s \sim 250$ m/s) wavespeed material (Figure 6).
360 Although the sedimentary overburden will effect the propagation of the noise wavefield, a quantitative
361 prediction of amplification based on the HVSR results isn't appropriate. Throughout this paper we
362 have focused, for the sake of brevity, on vertical component power spectra which are not expected to be
363 significantly influenced by near-surface sedimentary structure (e.g., Lermo and Chávez-García, 1993;
364 Field and Jacob, 1995). In addition, soft sediments are expected to exhibit high seismic attenuation
365 further complicating the prediction of noise wavefield amplification. At present the seismic attenuation
366 structure is poorly constrained for the materials underlying London. Despite considerable differences
367 in subsurface geology, the maximum vertical noise amplitudes observed in Auckland, New Zealand
368 (Boese et al., 2015), and London are very similar. This suggests that the high noise amplitudes are
369 predominantly a source effect.

370 CONCLUSIONS

371 Using recordings from five broadband seismometers in central London, we have shown that the
372 broadband urban noise spectrum ($T = 0.01$ to 100 s) is primarily generated by transportation sources.

373 Road traffic noise is ubiquitous across central London between $T = 0.1$ and 1.5 s, and generates
374 daytime RMS acceleration amplitudes at $T = 0.1$ s that are ~ 1000 higher than those measured at a
375 quiet hardrock observatory at Eskdalemuir, Scotland. Diurnal variations in noise at $T = 0.4$ s follow
376 the temporal pattern expected for road traffic, with nighttime values 12dB less than those in the
377 morning rush-hour (equivalent to an RMS acceleration amplitude reduction of a factor of four at night).
378 Overground rail transportation exhibit clear short period signals, peaked at ~ 0.15 s, in the vicinity of
379 the railway network. Railways also contribute to the very long period (> 20 s) noise wavefield. As
380 expected for these longer wavelength phenomena they are observed throughout central London.

381 The dynamic response to the movement of trains within the subway (the London Underground)
382 was recorded across a wide passband ($0.012 < T < 0.05$ s) at stations within 100m of the tunnels. At a

383 distance of 600 m no subway generated signals were observed. Observations made during an industrial
384 strike allow us to estimate that within 100 m of a subway tunnel, the trains generate approximately
385 60% of the noise power at very short periods ($T = 0.04$ s). At a station located ~ 30 m above a subway
386 tunnel, quasi-static effects associated with each train passing beneath the station were observed; the
387 seismometer was deflected downwards by 6×10^{-6} m before rebounding. In addition, due to the
388 deployment of the seismometer within a room connected via shafts and passageways to the subway
389 tunnels, we recorded the response to long period (> 30 s) air motions throughout the tunnel network
390 generated by the air piston effect.

391 A low-velocity ($V_s < 400$ m/s) overburden beneath London, tens of metres thick, and comprising
392 clays and sands, amplifies the horizontal noise wavefield at periods of approximately 1 s. To minimise
393 such site effects in future comparisons of urban noise levels it will be important to compare vertical
394 noise power values.

395 The observations show that broadband measurements are key to analyzing the full spectrum of
396 anthropogenic vibration noise. We have provided tabulated power spectral density values, available
397 in the electronic supplement to this article, for periods between 0.014 and 70 s, which will facilitate
398 comparison with future urban seismic deployments. As urban areas grow, and transportation networks
399 evolve, it will be of interest to observe how urban seismic noise changes.

400 **DATA AND RESOURCES**

401 Seismic data used in this study were collected using a temporary network of AWE and Imperial College
402 sensors, and cannot be released to the public. Analysis was facilitated by using the Obspy Python Pack-
403 age (Beyreuther et al., 2010). Plots were made using the matplotlib package (<http://matplotlib.org>), with
404 mapping data from OpenStreetMap, which is available under the Open Database License (specifically,
405 the ESRI shapefile download function at <http://www.bbbike.org/>)

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411 REFERENCES

- 412 Aki, K. and Richards, P. G. (2002). *Quantitative Seismology*. University Science Books, Sausalito,
413 California, 2nd edition. pp. 700.
- 414 Behm, M., Leahy, G. M., and Snieder, R. (2014). Retrieval of local surface wave velocities from traffic
415 noise - an example from the La Barge basin (Wyoming). *Geophys. Prosp.*, 62(2):223–243.
- 416 Beyreuther, M., Barsch, R., Krischer, L., Megies, T., Behr, Y., and Wassermann, J. (2010). ObsPy: A
417 Python toolbox for seismology. *Seism. Res. Lett.*, 81(3):530–533.
- 418 Boese, C., Wotherspoon, L., Alvarez, M., and Malin, P. (2015). Analysis of anthropogenic and natural
419 noise from multilevel borehole seismometers in an urban environment, Auckland, New Zealand.
420 *Bull. Seism. Soc. Am.*, 105(1):285–299.
- 421 Bourbié, T., Coussy, O., and Zinszner, B. (1987). *Acoustics of Porous Media*. Gulf Publishing Company,
422 Houston, TX.
- 423 Breuer, P., Chmielewski, T., Górski, P., Konopka, E., and Tarczyński, L. (2008). The Stuttgart TV Tower
424 - displacement of the top caused by the effects of sun and wind. *Eng. Struct.*, 30(10):2771–2781.
- 425 Chang, J. P., de Ridder, S., and Biondi, B. L. (2016). High-frequency Rayleigh-wave tomography using
426 traffic noise from Long Beach, California. *Geophysics*, 81(2):B1–B11.
- 427 Chen, Q.-F., Li, L., Li, G., Chen, L., Peng, W.-T., Tang, Y., Chen, Y., and Wang, F.-Y. (2004). Seismic
428 features of vibration induced by train. *Acta Seismologica Sinica*, 17(6):715–724.
- 429 Degrande, G., Schevenels, M., Chatterjee, P., Van de Velde, W., Hölscher, P., Hopman, V., Wang, A.,
430 and Dadkah, N. (2006). Vibrations due to a test train at variable speeds in a deep bored tunnel
431 embedded in London clay. *J. Sound Vibration*, 293(3):626–644.
- 432 Ellison, R. A., Woods, M. A., Allen, D. J., Forster, A., Pharaoh, T. C., and King, C. (2004). *Geology of*
433 *London: special memoir for 1: 50000 geological sheets 256 (north London), 257 (Romford), 270*
434 *(south London), and 271 (Dartford) (England and Wales)*. British Geological Survey.
- 435 Environment Agency (2015). *Management of the London Basin Chalk Aquifer*. Status Report,

436 <https://www.gov.uk/government/publications/london-basin-chalk-aquifer-annual-status-report>, ac-
437 cessed May 2016.

438 Fäh, D., Kind, F., and Giardini, D. (2001). A theoretical investigation of average H/V ratios. *Geophys.*
439 *J. Int.*, 145(2):535–549.

440 Fäh, D., Rüttener, E., Noack, T., and Kruspan, P. (1997). Microzonation of the city of Basel. *J. Seismol.*,
441 1(1):87–102.

442 Field, E. H. and Jacob, K. H. (1995). A comparison and test of various site-response estimation
443 techniques, including three that are not reference-site dependent. *Bull. Seism. Soc. Am.*, 85(4):1127–
444 1143.

445 Groos, J. C. and Ritter, J. R. (2009). Time domain classification and quantification of seismic noise in
446 an urban environment. *Geophys. J. Int.*, 179(2):1213–31.

447 Hudson, J. A. and Douglas, A. (1975). Rayleigh wave spectra and group velocity minima, and the
448 resonance of P waves in layered structures. *Geophys. J. Int.*, 42(1):175–188.

449 Ibs-von Seht, M. and Wohlenberg, J. (1999). Microtremor measurements used to map thickness of soft
450 sediments. *Bull. Seism. Soc. Am.*, 89(1):250–259.

451 Lermo, J. and Chávez-García, F. J. (1993). Site effect evaluation using spectral ratios with only one
452 station. *Bull. Seism. Soc. Am.*, 83(5):1574–1594.

453 Lin, C.-J., Chuah, Y. K., and Liu, C.-W. (2008). A study on underground tunnel ventilation for piston
454 effects influenced by draught relief shaft in subway system. *Appl. Therm. Eng.*, 28(5):372–379.

455 McNamara, D. E. and Buland, R. P. (2004). Ambient Noise Levels in the Continental United States.
456 *Bull. Seism. Soc. Am.*, 94(4):1517–1527.

457 McNamara, D. E., Stephenson, W. J., Odum, J. K., Williams, R. A., and Gee, L. (2015). Site response
458 in the eastern United States: A comparison of Vs30 measurements with estimates from horizontal:
459 vertical spectral ratios. *Geological Society of America Special Papers*, 509:67–79.

460 Nakamura, Y. (1989). A method for dynamic characteristics estimation of subsurface using microtremor
461 on the ground surface. *Railway Technical Research Institute, Quarterly Reports*, 30(1).

462 Nakamura, Y. (2000). Clear identification of fundamental idea of Nakamura's technique and its
463 applications. In *Proceedings of the 12th World Conference on Earthquake Engineering*. Auckland,

464 New Zealand.

465 Panou, A., Theodulidis, N., Hatzidimitriou, P., Stylianidis, K., and Papazachos, C. (2005). Ambient
466 noise horizontal-to-vertical spectral ratio in site effects estimation and correlation with seismic
467 damage distribution in urban environment: the case of the city of Thessaloniki (Northern Greece).
468 *Soil. Dyn. Earthq. Eng.*, 25(4):261–274.

469 Peck, L. (2008). Overview of Seismic Noise and its Relevance to Personnel Detection. Technical
470 Report ERDC/CRREL TR-08-5, Cold Regions Research and Engineering Laboratory.

471 Peterson, J. (1993). Observations and Modeling of Seismic Background Noise. Technical Report
472 Open-File Report 93-322, U.S. Department of Interior, Geological Survey.

473 Riahi, N. and Gerstoft, P. (2015). The seismic traffic footprint: Tracking trains, aircraft, and cars
474 seismically. *Geophys. Res. Lett.*, 42(8):2674–2681.

475 Royse, K. R., de Freitas, M., Burgess, W. G., Cosgrove, J., Ghail, R. C., Gibbard, P., King, C., Lawrence,
476 U., Mortimore, R. N., Owen, H., and Skipper, J. (2012). Geology of London, UK. *Proc. of the*
477 *Geologists' Association*, 123:22–45.

478 Sheen, D.-H., Shin, J. S., Kang, T.-S., and Baag, C.-E. (2009). Low frequency cultural noise. *Geophys.*
479 *Res. Lett.*, 36(17).

480 Su, F., Aki, K., Teng, T., Zeng, Y., Koyanagi, S., and Mayeda, K. (1992). The relation between site
481 amplification factor and surficial geology in central California. *Bull. Seism. Soc. Am.*, 82(2):580–602.

482 Sumbler, M. G. (1996). *London and the Thames Valley*, volume 13. HMSO for the British Geological
483 Survey.

484 Thomas, G., Koper, K. D., Burlacu, R., and Drobeck, D. (2013). A model of ambient seismic
485 noise recorded by the Utah regional network of strong-motion seismometers. *Seism. Res. Lett.*,
486 84(5):759–771.

487 Truscott, J. R. (1964). The Eskdalemuir Seismological Station. *Geophys. J. R. Astr. Soc.*, 9(1):59–68.

488 United Nations (2014). *World Urbanization Prospects: The 2014 Revision, Highlights*
489 *(ST/ESA/SER.A/352)*. Department of Economic and Social Affairs, Population Division, United
490 Nations Publications. ISBN 978-92-1-151517-6.

491 Willis, J. (1997). *Extending the Jubilee Line: The Planning Story*. London Transport, London, UK.

492 Yang, Y. and Hung, H. (2008). Soil Vibrations Caused by Underground Moving Trains. *J. Geotech.*
493 *Geoenviron. Eng.*, 134(11):1633–1644.

Table 1. Details of the deployed Güralp broadband seismometers, the median acceleration noise levels at 02:00 and 08:00 (approximately the diurnal minimum and maximum, Figure 4e and f) at three periods, and the proximity to major noise sources.

Station	Location (Lat/Lon)	Deployment Dates (2015)	Güralp Model (Corner Period)	Median Acceleration Noise Levels (dB wrt $1(m^2/s^4)/Hz$)						Comment on Noise Sources
				02:00 GMT			08:00 GMT			
				0.1 s	0.4 s	1.0 s	0.1 s	0.4 s	1.0 s	
London Stations										
ALB	51.52650N 0.12459W	12-Aug to 27-Aug	3ESPC (60s)	-88.2	-104.9	-130.9	-81.1	-95.2	-122.8	No rail or subway within 200m
IMP	51.49950N 0.17589W	4-Aug to 9-Sep	3ESPC (60s)	-98.5	-103.0	-127.1	-89.9	-91.5	-118.3	No rail or subway within 600m
LFS	51.49258N 0.11992W	13-Aug to 26-Aug	3ESPC (60s)	-94.0	-107.9	-130.7	-82.5	-96.7	-121.0	60m from overground train line
OWB	51.50606N 0.12459W	28-Jul to 27-Aug	40T (30s)	-91.1	-96.4	-126.4	-89.6	-89.8	-119.2	Heavy road traffic; subway at 100m
SJP	51.50150N 0.14388W	28-Jul to 12-Aug	3ESPC (60s)	-92.8	-102.2	-128.9	-83.9	-91.2	-119.1	Directly above subway line
Other UK Stations										
BKN	51.36420N 1.18690W	Permanent	3ESPC (60s)	-115.4	-123.2	-132.6	-94.6	-104.1	-132.6	Semi-rural location, local daytime traffic
EKB	55.33386N 3.19228W	Permanent	3T (120s)	-152.0	-151.0	-139.0	-145.7	-148.2	-139.2	Quiet rural location local daytime traffic

Table 2. Properties of the overburden in the simplified four-layer geological model of London used to calculate the HVSR resonance frequency (f_{est}). These are compared to measured HVSR resonance frequencies ($f_{measured}$, see Figure 5). The full-width at half maximum (fwhm) are provided to give a measure of the spectral sharpness of the peaks.

Station	Depth to overburden base (m)	V_s surface (m/s)	V_s overburden base (m/s)	f_{est} (Hz)	$f_{measured}$, [fwhm] (Hz)
ALB	52	101	365	1.1	1.2 , [1.3]
IMP	88	101	407	0.72	0.78, [0.70]
LFS	61	101	377	0.98	1.3, [1.5]
OWB	67	101	386	0.91	1.1, [1.0]
SJP	71	101	390	0.86	1.0, [1.0]

Table 3. Examples of spectral content, given in terms of period, T , for transportation generated seismic signals reported in urban locations.

Source	Spectral Content (s)	Location	Reference
Road	0.1 to 1.5	London, UK	This Study
	0.04 to 1	Bucharest, Romania	Groos and Ritter (2009)
	0.03 to 1	Auckland, New Zealand	Boese et al. (2015)
	<0.3	Long Beach, California, US	Chang et al. (2016)
	0.17 to 0.5	Wyoming, US	Behm et al. (2014)
Rail	0.014 to 0.3, and 20 to 50	London, UK	This Study
	0.02 to to 1	Beijing, China	Chen et al. (2004)
	0.03 to 0.13	Auckland, New Zealand	Boese et al. (2015)
	0.03 to 0.1	Long Beach, California	Riahi and Gerstoft (2015)
	20 to 100	Palisades, US	Sheen et al. (2009)
Subway	0.01 to 0.1 (dynamic) 1 to 100 (quasi-static) >30 (air-piston)	London, UK	This Study
	0.008 to 0.05	London, UK	Degrande et al. (2006)
	<0.2, and 20 to 100	Seoul, South Korea	Sheen et al. (2009)

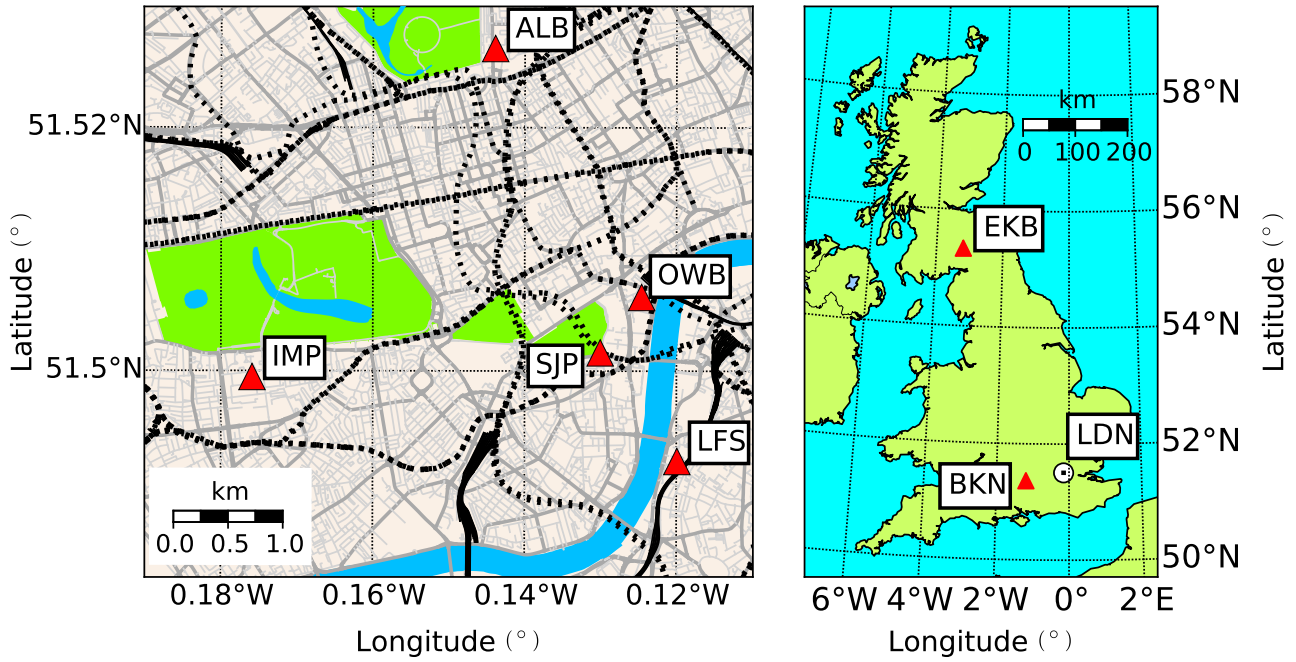


Figure 1. A simplified map (left hand panel) showing stations deployed in central London (red triangles). Roads are shown in grey, with major routes denoted by wider lines. Surface train lines are shown as solid black lines, underground train lines are shown as dashed black lines. The right hand panel shows the location of the two UK stations used to compare against noise levels in London (LDN). Mapping information taken from OpenStreetMap (© OpenStreetMap contributors). The color version of this figure is only available in the electronic edition.

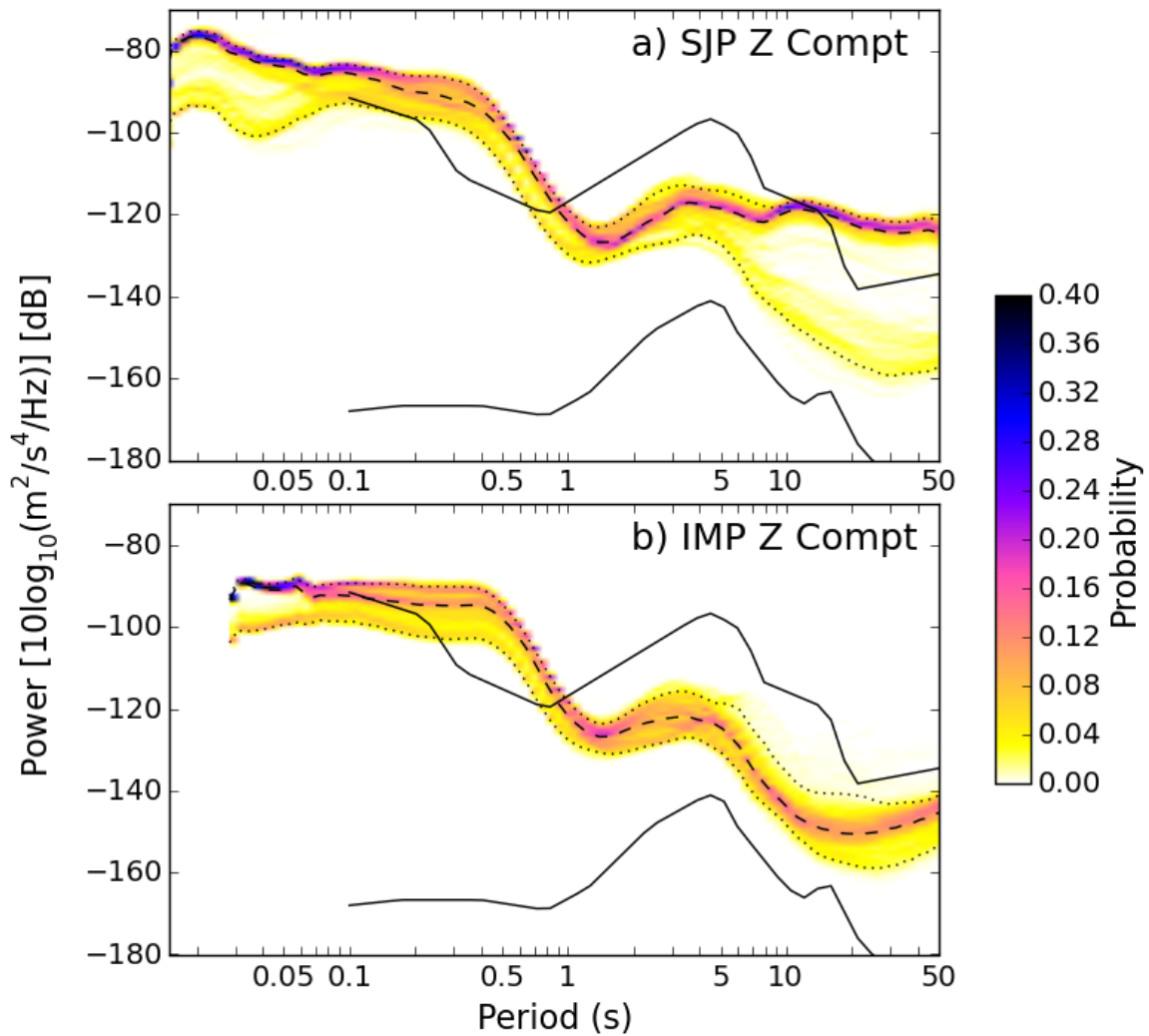


Figure 2. A comparison of the broadband vertical component noise power probability density functions at stations a) SJP and b) IMP, calculated using the methodology of McNamara and Buland (2004). Note the sampling rate differed at the two stations, IMP = 100 Hz, SJP = 200 Hz. Solid black lines are the New Low and High Noise Models of Peterson (1993). Dashed black lines are the median PDF values, while dotted black lines are the 5 and 95% PDF values at each period. The color version of this figure is only available in the electronic edition.

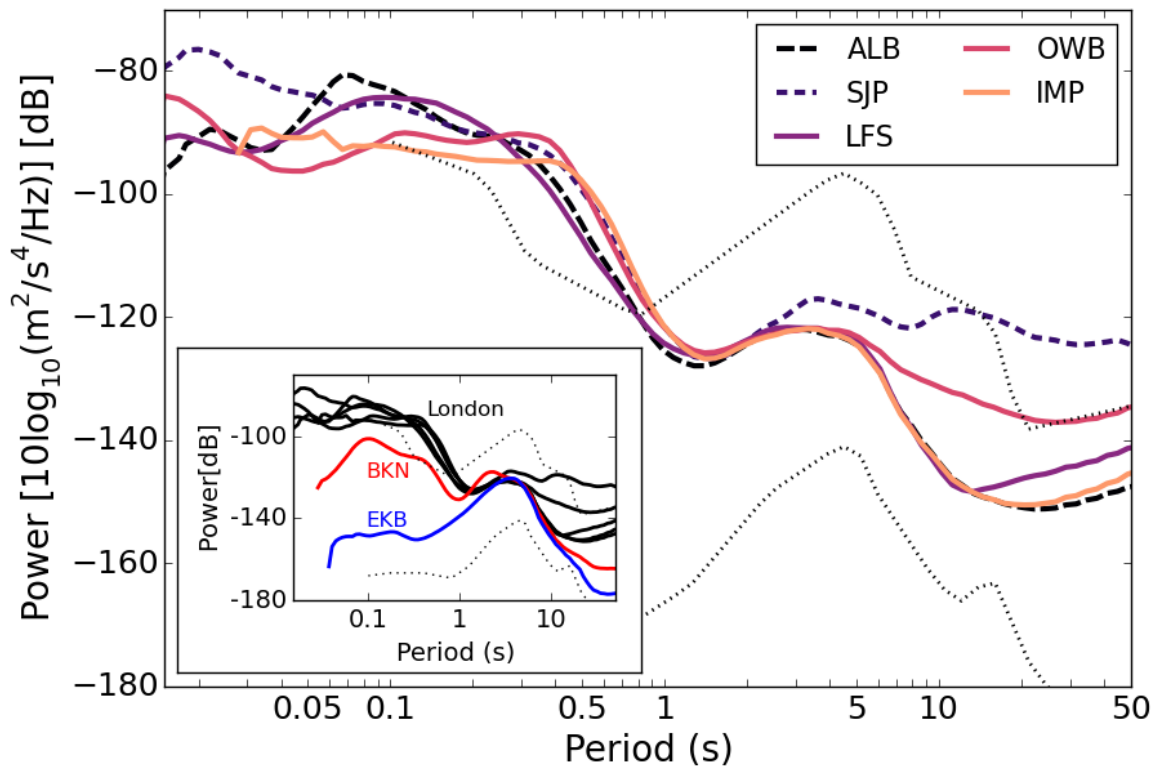


Figure 3. Median vertical component noise power levels calculated at the five broadband sensors within the temporary London station network (data values provided in Table S1, available in the electronic supplement to this article). Sensor names are given in the legend; locations are shown in Figure 1. The black dotted lines are the vertical acceleration New Low and High Noise Models of Peterson (1993). The inset compares the London median noise levels with those from two other UK stations: BKN located at AWE Blacknest (51,364N,1.187W), and EKB located at Eskdalemuir, southern Scotland (55.334N,3.192W). The data for BKN and EKB were taken from the same time period as the OWB deployment (Table 1). The color version of this figure is only available in the electronic edition.

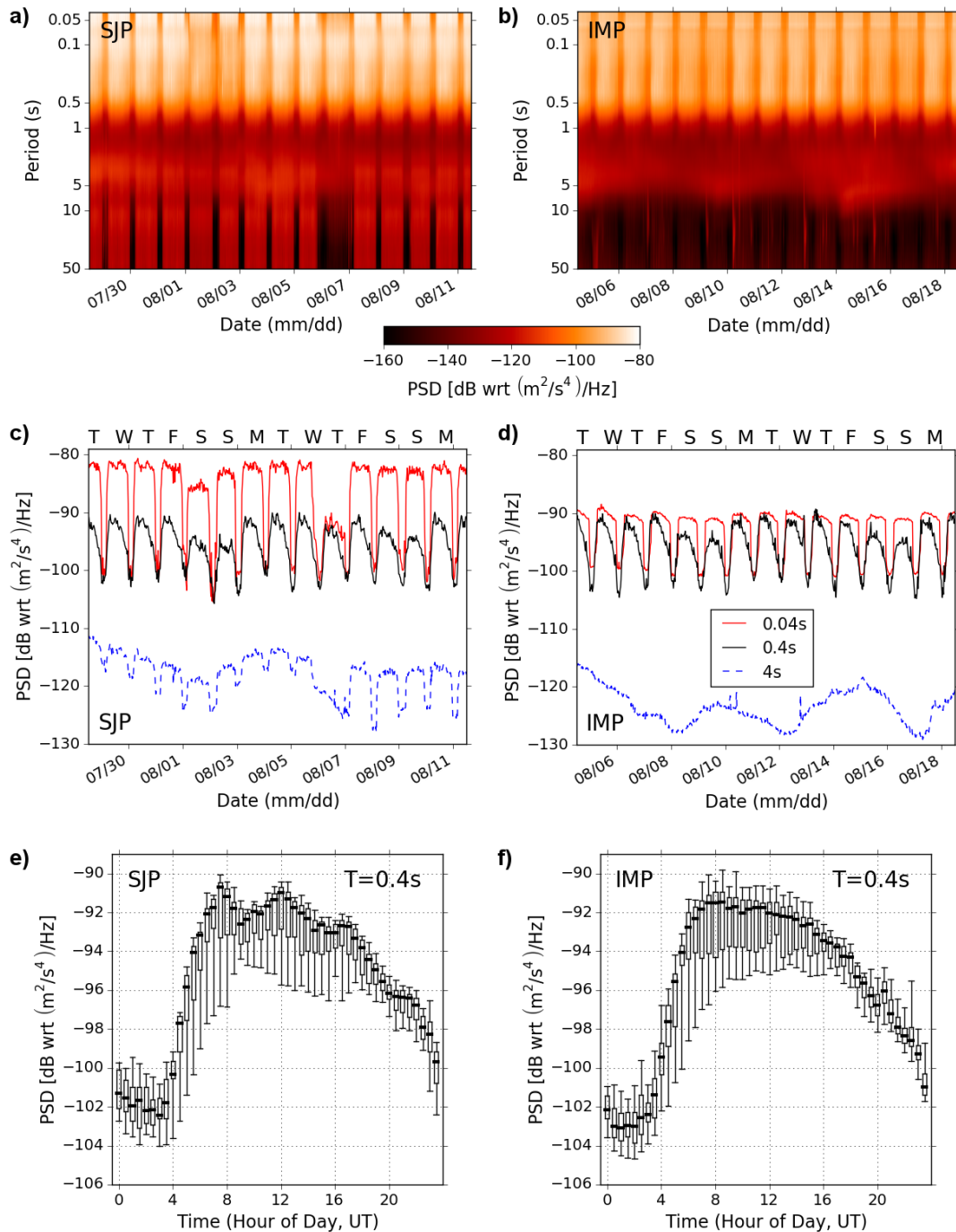


Figure 4. Diurnal variations of vertical component noise measurements at stations SJP (panels a, c and e) and IMP (panels b, d and f). The upper panels show the variation of noise power as a function of time and period. Note that although the y-axis scales are identical the time periods are different (but overlapping) due to different deployment schedules. The middle panels show diurnal noise variations at three periods, representing horizontal slices through panels a) and b). The lower plots are boxplot summaries of the noise variation in half-hour bins across the entire station deployments at 0.4 s. The thick central line indicates the median value, the box limits are the 25th and 75th percentiles, while the whiskers represent the 5th and 95th percentiles of the noise distributions. The color version of this figure is only available in the electronic edition.

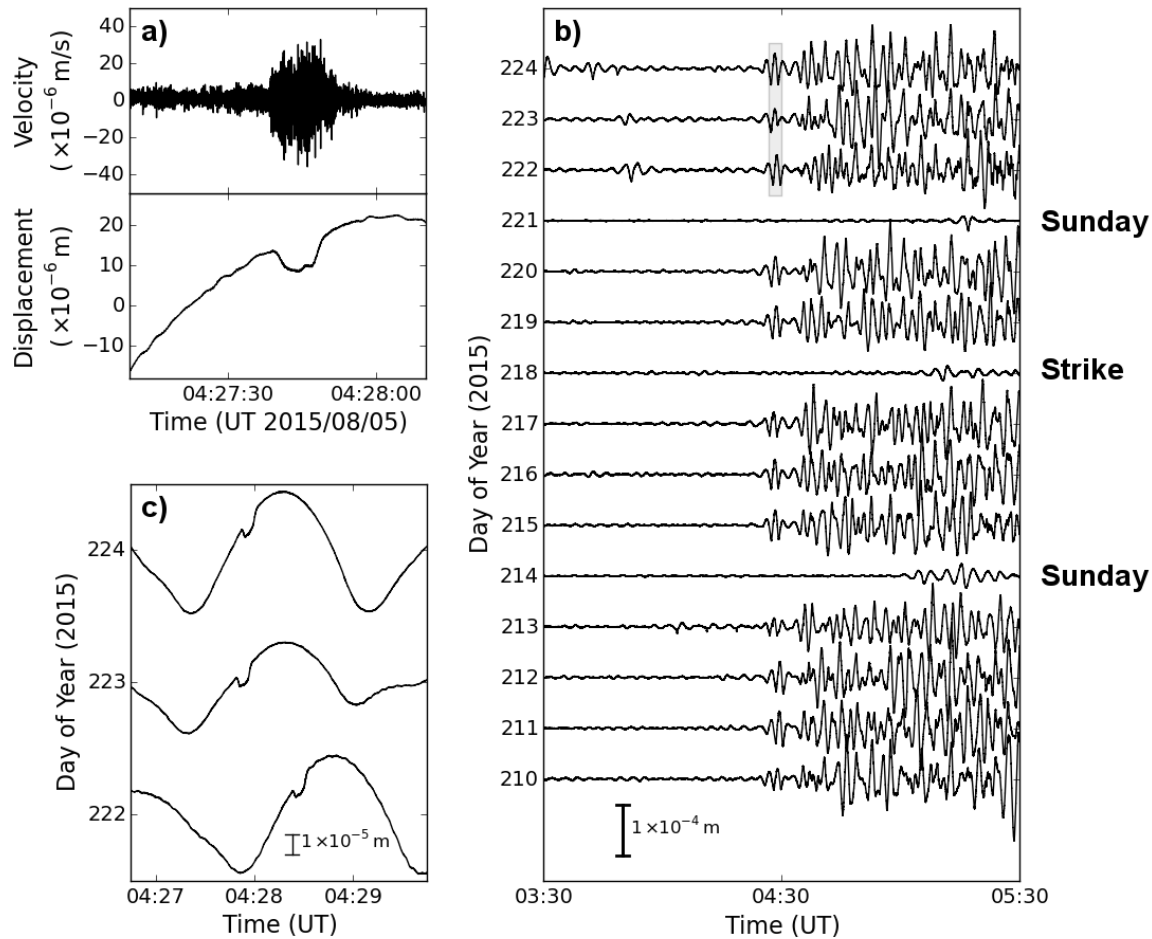


Figure 5. The effect of subway trains on recordings at SJP. Panel a) shows the vertical ground velocity, and displacement, associated with the passage of one Eastbound train beneath station SJP. Panel b) shows the long-period vertical displacement oscillations associated with the start-up of train services in the subway every morning, and c) shows the details of the oscillations from three days (corresponding to the light grey box in panel b). All traces are unfiltered, except for the high-pass filter discussed in the Methods section that suppresses periods $>200 \text{ s}$ to reduce instrument response deconvolution artifacts.

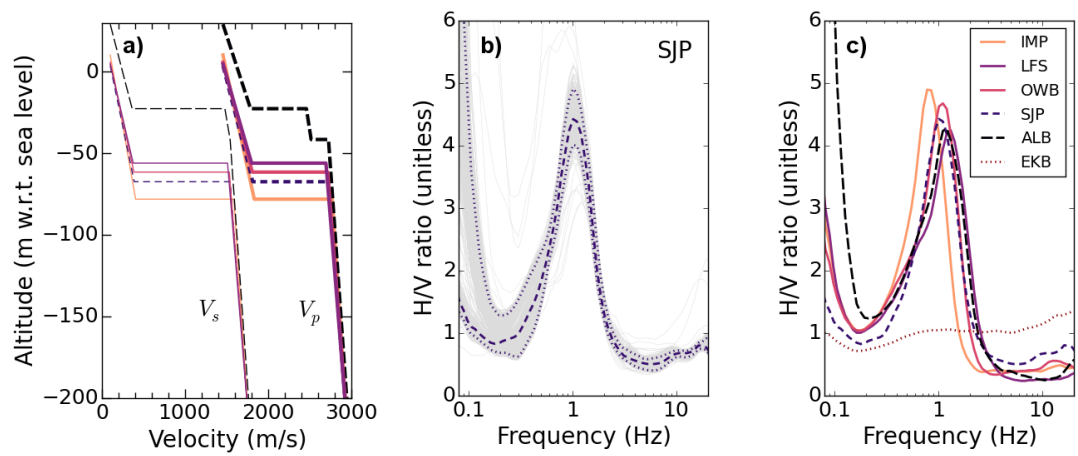


Figure 6. Confirmation of a low-velocity overburden from the seismic data. Panel a) shows velocity profiles for the upper layers of the 4-layer simplified BGS geology-derived velocity model: P -wave speeds as thick lines, S -wave speeds as thin lines. Panel b) shows H/V ratio spectra calculated from each half-hour seismic spectra recorded at SJP (grey lines). The thick dashed line is the median value at each frequency, the dotted lines provide the 5 and 95% percentile values. Panel c) shows the median H/V ratio spectra for the London deployments and the seismometer at EKB, Eskdalemuir (Figure 1). The color version of this figure is only available in the electronic edition.