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Title: Mechanistic model for design, analysis, operation and control of microalgae cultures: calibration and application to tubular photobioreactors

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Corresponding Author: Professor Joan Garcia, PhD

Corresponding Author's Institution: Technical University of Catalonia

First Author: Alessandro Solimeno

Order of Authors: Alessandro Solimeno; Francisco G Acien Fernández; Joan Garcia, PhD

Abstract: Closed photobioreactors (PBRs) are usually used for the production of high-value microalgae biomass at higher productivities than in open ponds. A large variety of different PBRs have been developed to optimize the biomass productivity and photosynthesis efficiency. At the same time mathematical models for PBRs are also increasing in popularity for design of new systems and for improving understanding of the complex processes occurring inside. The aim of the present study is to calibrate of the new mechanistic model for microalgae growth using experimental data from two different tubular photobioreactors. Hydrodynamic and light attenuation through the medium were added in the model to obtain a realistic representation of photobioreactor. Furthermore, the model was able to predict microalgae production under different climatic conditions and the oxygen accumulation throughout the photobioreactor.



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ENGINEERING AND MICROBIOLOGY

Dear Editor,

We have received the comments from the Editor and Reviewers, and we have modified the manuscript accordingly. Comments suggested were considered, the manuscript and the captions of the figures have been carefully modified in order to meet the suggestions.

Furthermore, the manuscript has been edited by a native English speaking Lauren Parker from the California Polytechnic State University of San Luis Obispo.

We hope that the revised manuscript fully complies with comments and suggestions addressed by Reviewers.

Yours sincerely,

Joan García Serrano

Corresponding author

A handwritten signature in blue ink, appearing to be 'JG'.

Answers to reviewer's comments

(Comments in black and answers in red)

Reviewer #1:

Re reviewer has accepted the revisions, a few minor comments below. During my last read of the manuscript I noted a number of minor corrections and areas that need further clarification directly on the PDF of the document, which you can download from the EES system. Also, the manuscript should be edited by a native English speaking colleague. Please provide a final revision that appropriately addresses these suggestions for final approval.

Reviewer #1: Most of the proposed corrections were adequately addressed, I can recommend this MS for publication now.

Well done. Regards!

L315 extent instead of extend

We have modified the manuscript accordingly. Comments suggested were considered, the manuscript and the captions of the figures have been carefully modified in order to meet the suggestions.

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1 1. Introduction

2 ~~Microalgae biomass production is an industrial sector that continues growing~~
3 ~~each year. Products made from microalgae are nowadays presented by industry as a~~
4 ~~natural and green solution to the energy, food, economic and climate challenges facing~~
5 ~~the Earth [1, 20]. Although still there are some technical challenges (e.g. cost efficient~~
6 ~~production and harvesting systems), in general it is believed that microalgae fuels,~~
7 ~~feeds, plastics and other chemicals will be price competitive within the next years.~~
8 ~~Some are price competitive already [15, 31].~~

9 ~~Another potential market application of microalgae is their use in the context of~~
10 ~~wastewater treatment. Although this is not a new application, the feasibility of~~
11 ~~microalgae cultures for wastewater treatment and at the same time encouraging resource~~
12 ~~recovery and feedstock production has revived the interest on this technology [13].~~
13 ~~Microalgae treatment systems are currently viewed as a future alternative to~~
14 ~~conventional activated sludge treatment plants, where produced biomass can be~~
15 ~~valorised in the form of biofuels or bioproducts therefore optimising treatment costs~~
16 ~~[25, 29].~~

17 ~~In practice, industrial Industrial production of microalgae can be accomplished~~
18 ~~in open or closed photobioreactors. Open systems are ~~made up by~~ shallow channels in~~
19 ~~the shape of race tracks (raceway reactors) ~~which and~~ have been extensively studied in~~
20 ~~the past [9, 15]. Though open photobioreactors represent an efficient economic solution~~
21 ~~in front of closed photobioreactors, they ~~can be more~~ can be easily contaminated by~~
22 ~~other microorganisms ~~different from those of the culture,~~ and ~~are more~~ difficult to~~
23 ~~control. These disadvantages make closed photobioreactors more suitable when high-~~
24 ~~value products are the target of the culture. ~~These e~~ Closed systems ~~allow a strict~~ strictly~~
25 ~~control ~~of~~ chemical, physical and biological factors and can ~~better match ideal~~ improve~~
26 ~~conditions for microalgae growth by optimizing light absorption due to turbulent~~
27 ~~conditions in the culture [9, 11, ~~3330, 3431~~].~~

28 Closed photobioreactors (as well as open raceways) are sensitive to carbon
29 limitations and pH variations that could limit photosynthesis and therefore biomass
30 production [16]. ~~This is usually~~ Carbon and pH limitations ~~can be~~ corrected by
31 supplying carbon dioxide (CO_2) in order to maintain high photosynthesis rates and pH
32 control. However the two most critical issues of closed photobioreactors are the risk of
33 overheating and their potential for oxygen accumulation and subsequent growth
34 inhibition [2420]. ~~Therefore~~ To prevent overheating, closed photobioreactors often
35 require cooling as well as degasser systems [3532]. Concentrations of dissolved oxygen
36 (DO) in the culture above 250% ~~of~~ air saturation ~~value~~ can dangerously inhibit
37 microalgae activity [12].

38 ~~In the~~ Over the last few decades, mathematical models have proven to be useful
39 tools for the design, analysis, operation and control in multiple engineering problems
40 [5]. Nowadays, models have become essential tools for understanding complex
41 processes, such as those occurring in photobioreactors. In the case of microalgae
42 cultures, models are ~~still in their infancy in comparison~~ less developed than those seen in
43 ~~to other fields, and are not in common practice because most of them~~ When models
44 ~~contain too~~ are based in few parameters, ~~and are not able to capture the~~ they risk the
45 ~~capability of not capturing the~~ complexity of microalgae cultures in long-term
46 scenarios, ~~and therefore can be unreliable~~. Having this in mind, Solimeno et al. (2015)
47 [2927] developed a ~~rather~~ complete mechanistic mathematical model that includes
48 crucial physical and biokinetic processes ~~for the that description describe of~~ microalgae
49 growth in different types of cultures, ~~and in particular~~ ly in wastewater (where ~~growth is~~
50 ~~controlled by~~ carbon and nitrogen limitations ~~for growth can be significant~~). This model
51 was calibrated with data from a complete stirred culture fed with simulated treated
52 wastewater using a 0D domain [2927]. A global sensitivity analysis was carried out
53 using the same ~~data set~~ set of data [3028]. In the present paper we intend to go beyond
54 our previous works, calibrating the model with data from ~~more complex systems~~

55 ~~consisting of~~ two different pilot scale tubular closed photobioreactors fed with different
56 types of medium culture. In this present case, a 2D domain, ~~which is used to represents~~
57 the hydrodynamics of the system (i.e., transport of diluted species and mass transfer
58 phenomena), ~~is~~ coupled with the previous mechanistic model [2927]. The resulting
59 model has been implemented ~~into~~ the COMSOL Multiphysics™ software, which solves
60 equations using the finite elements method (FEM).

61 The aim of the present study is ~~therefore the to -calibration -calibrate~~ of the new
62 ~~and more complex~~ mechanistic model of Solimeno et al. (2015) [2927] using
63 experimental data from two different tubular photobioreactors. ~~Furthermore, t~~The
64 potential of the model is demonstrated by means ~~of~~ practical study cases in which we
65 simulate oxygen concentrations (the most critical growth inhibition factor of closed
66 photobioreactors) and predict microalgae production as a function of temperature and
67 light intensity. Simulations show the potentiality of photobioreactor configurations to
68 optimize microalgae production. The overall objective of this model is to become a
69 reference to simulate physical, chemical and biokinetic microalgae processes in
70 different types of photobioreactors fed with different types of medium cultures.

71

72 **2. Methods**

73 *2.1 Pilot closed photobioreactors and experimental data*

74 Both photobioreactors were located in Spain, one in “Estación Experimental Las
75 Palmerillas”, property of Fundación CAJAMAR in Almeria, and the other in
76 “Agropolis”, property of Universitat Politècnica de Catalunya-BarcelonaTech in
77 Barcelona (Fig. 1). The vertical tubular photobioreactor (PBR) in Almeria includes a
78 loop solar receiver made of transparent plastic tubes of 0.09 m diameter with a total
79 horizontal length of 400 m, and a 0.4 m diameter bubble column with 3.5 m of height,
80 and has a total working volume of 3,000 L. The PBR unit is used to produce the

81 microalgae *Scenedesmus almeriensis*, which is characterized by a high growth rate;
82 ~~supporting and tolerance~~ temperatures up to 45 °C and ~~tolerance to~~ pH values up to 10
83 [1, 2725]. The ~~culture-PBR works by creating~~ continuously flow ~~of cultures~~ between
84 ~~the~~ loop and bubble column by means ~~of~~ a centrifuge pump located at the bottom of the
85 column. The pump provides a constant flow velocity of 0.8 m s⁻¹ inside the loop. The
86 pH of the culture is controlled by ~~on-demand~~ injection of pure CO₂ at 5 L min⁻¹. In the
87 bubble column, ~~excess dissolved oxygen DO in excess~~ is removed by a constant airflow
88 rate of 140 L min⁻¹. ~~Furthermore, T~~ the culture temperature is ~~controlled-maintained~~
89 ~~through an internal heat exchanger located at the bubble column~~ by passing cooling
90 water at 1500 L h⁻¹ ~~through an internal heat exchanger located inside the bubble~~
91 ~~column for cooling. When fresh culture medium is poured into the system, The the~~
92 ~~culture is~~ harvested ~~ed of the culture is reaped~~ through an overflow ~~at the~~ ~~located on~~ top of
93 the column. ~~when fresh culture medium is poured into the system.~~ Temperature, pH and
94 ~~dissolved oxygen DO~~ are measured at several locations along the tube using Crison
95 probes (Crison Instruments, Spain) connected to a control-transmitter unit MM44
96 (Crison Instrument, Spain); ~~-. liquid-Liquid~~ and gas flow rates are measured using
97 digital flowmeters (PF2W540 and PF2A510, from SMC, Japan). All of these ~~measures~~
98 ~~monitoring systems~~ are in turn connected to a control computer through a data
99 acquisition device NI Compact FieldPoint (National Instruments, USA) [15]. Data for
100 the present study ~~were-were~~ obtained at the end of ~~an a two month~~ experiment ~~of 2~~
101 ~~months~~ in which the photobioreactor was operated in continuous mode, ~~at a~~ medium
102 flow rate of 1020 L d⁻¹, ~~and~~ under controlled pH (7.8) and temperature (lower than 35
103 °C). As a result, ~~the amount of~~ microalgae biomass ~~amount~~ was kept fairly constant.
104 Culture medium used was Mann&Myers, prepared using agricultural fertilizers. ~~Data~~
105 ~~Collected data used-were-were~~ retrieved in batch mode by switching off the feeding ~~only~~
106 ~~for~~ 24 hours (at the end of the ~~2-two~~ months). Dissolved oxygen and pH data were
107 recorded every 30 minutes, while temperature and irradiance were measured every hour.

108 The horizontal tubular photobioreactor in Barcelona is composed of 2 open-air
109 tanks made of polypropylene ~~with a size of and is~~ 1.8 x 1 x 0.4 m (L x W x H) ~~in size~~.
110 These tanks include paddlewheels that provide enough head pressure to move the
111 culture through 12 (6 per each flow direction) transparent 0.125 m diameter
112 polyethylene tubes (~~each~~ 50 m ~~in length~~ ~~each one~~). Culture flows from one tank to the
113 other at a constant velocity of 0.125 m s⁻¹. Tanks also allow release of exceeding
114 oxygen accumulated along tubes. The PBR has an effective volume of 8.5 m³. Note that
115 in this PBR there is no CO₂ injection or pH control. Data used for the present work were
116 retrieved from a 3 day's batch experiment and measured in each tank. For this
117 experiment the PBR was filled with 8 m³ of agricultural runoff from a nearby
118 agriculture canal which were inoculated with 0.5 m³ of inoculum with microalgae from
119 a previous experiment (Table 1). The PBR contained different microalgae species
120 belonging to the genus *Pediastrum sp.*, *Chlorella sp.* and *Scenedesmus sp.*

121 The horizontal PBR has dissolved oxygen and pH online sensors in each tank
122 that record data every hour, and temperature and irradiance online sensors that record
123 data every 2-3 hours. Gathered data are stored ~~via~~ using a Programmable Logic
124 Controller (PLC) that is connected to a computer with ~~a~~ supervisory control and a data
125 management system (Green web manager 2.0). During the ~~3~~ three days of experiments,
126 offline samples were taken every ~~2-3~~ two-three hours and analyzed in the laboratory for
127 nitrates and alkalinity. Analysis of nitrate ~~The ion chromatographic chromatography~~
128 ~~analysis of nitrates~~ was accomplished using a Thermo Finnigan chromatograph with a
129 metallic detector TCD (thermal conductivity detector). ~~Alcalinity~~ Alkalinity was
130 analysed using conventional titrimetric procedures indicated in ~~the~~ Standard Methods
131 [3]. Note that bicarbonate was calculated ~~from~~ using alkalinity measurements, pH, and
132 equilibrium constants of carbon species (Eq. 1).

133

134
$$\text{Alkalinity} = 50 * \left[\frac{S_{\text{HCO}_3}}{12} + 2 * \frac{S_{\text{CO}_3}}{12} + S_{\text{OH}} - S_{\text{H}} \right] \quad (1)$$

135

136 2.2 Conceptual model

137 The new mechanistic model presented by Solimeno et al. (2015) [2927]
138 considers crucial physical, chemical and biokinetic processes for the description of
139 microalgae growth in different types of cultures, ~~and most~~ particularly in wastewaters.
140 The main relevant feature of the model, respect to any previous model for microalgae
141 production [4, 6, 2423], consists in the inclusion of a carbon limitation on the growth of
142 microalgae, as well as a dynamic model for photosynthesis, photolimitation, ~~and~~ light
143 attenuation, ~~and the description of the effect of~~ photorespiration. In the model,
144 microalgae grow with light, consume nutrients (i.e., carbon and nitrogen), and release
145 oxygen (Fig. 2).

146 Note that other nutrients (e.g., phosphorus) and micronutrients are not
147 considered to be limiting factors because are usually highly available in wastewaters
148 (which is the type of culture ~~that~~ mainly addresses by the model) [19]. Dependency of
149 microalgae growth on phosphorus could ~~be easily~~ be implemented in the model ~~through~~
150 by creating a limiting Monod function, ~~similar how the other like the other~~ nutrients
151 (i.e., carbon and nitrogen) ~~were represented~~. In the model, as a result of microalgal
152 activity in the presence of light, hydroxide ions concentration and pH increase. ~~Such~~
153 increases in pH displace the equilibrium of the carbon species towards the formation of
154 carbonates (which are not bioavailable for growth). Note that this model assumes that
155 carbon dioxide as well as bicarbonate are bioavailable for growth. In darkness,
156 endogenous respiration of microalgae release carbon dioxide, the concentration of
157 hydrogen ions increase and the pH decreases. ~~By~~ With decreasing pH, the carbon
158 equilibrium shifts and carbonate turns into bicarbonate, which can be used as substrate
159 again in the presence of light [3330]. A detailed description of the model, ~~their~~
160 includings components, and processes can be found in Solimeno et al. (2015) [2927]. A

161 list of the processes included in the model, the equations describing their rates and the
162 matrix of stoichiometric parameters are shown in Supplementary Tables (4-5).

163 *2.3 Model domain*

164 The Pphotobioreactor's configuration was assumed to have a 2D geometry. The
165 domain was divided into two sub-domains (D1 and D2) corresponding to the loop
166 configuration and the bubble column for the vertical system in Almeria, and to the
167 open-air tanks and the tubes for the horizontal system in Barcelona (Fig. 3). In the case
168 of the vertical system, D1 was 400 m long in the longitudinal direction and 0.09 m in
169 diameter, while in the horizontal system it was 50 m long and 0.125 m in diameter. D2
170 domains were designed allocating the volume of the bubble column (vertical system)
171 and open-air tank (horizontal system) along a surface interface area ~~through~~
172 ~~which~~where gases ~~can be~~were transferred to the atmosphere, fixing the corresponding
173 D1 diameter. Thus, the bubble column is ~~defined with~~ 3.3 m ~~length~~long and 0.09 m
174 ~~width~~deep, while the tank is 5.76 m long and 0.125 m ~~width~~deep. These simplifications
175 allow ~~to simulate~~simulate ~~of the~~ hydrodynamics ~~of within the~~ systems. Note that in
176 the present model it was necessary to divide the domain into two sub-domains due to
177 the different domain conditions. Transfer of gases to the atmosphere ~~takes~~took place
178 exclusively in the bubble column and open-air tanks. A periodic condition was applied
179 at boundaries 1 and 2 to reproduce the continuous culture flow from domain 2 to 1
180 (degasser to loop and tank to tube).

181 *2.4 Hydrodynamics of the system, light attenuation and temperature*

182 In our previous work [2927], the calibration of the model was conducted in a
183 complete mixed reactor represented by a 0D domain in order to simplify
184 hydrodynamic's complexity. In the present work, as a result of the motion of the culture
185 through the tubes and bubble column or open-air tank, a 2D domain was needed, which

186 including hydraulic and transport equations. On the other hand, in the previous work
187 [2826], it was assumed that microalgae cells captured photons at all depths (light
188 attenuation was neglected due to 0D domain). ~~In the~~The present work incorporates light
189 attenuation ~~due to the presence of is added, including light limitations related to~~
190 ~~scattering and mutual shading effects of~~ microalgae.

191 In the model microalgae processes are influenced by temperature [2927]. It is
192 known that the growth rate ~~of microalgae is highly dependent on increases when~~
193 ~~temperature; it increases when goes up to an optimum temperature is reached~~ and
194 ~~decrease drastically decreases when with optimum temperature over the optis~~
195 ~~exceedidimum~~ [14]. In the present study, microalgae production was simulated in a
196 study case at different temperatures, showing the dependence of microalgae growth on
197 temperature.

198 Hydrodynamics of system was modelled through the COMSOL Multiphysics™
199 software, previously used for the calibration of the microalgae model in a ~~complete~~
200 completely stirred experiment, which solves differential equations using the finite
201 elements method (FEM).

202 2.4.1 Hydraulic Considerations

203 In the PBR used in this work the culture is set in motion by an external pump
204 (vertical system) or by paddlewheels (horizontal system), and enters the model domain
205 with a certain velocity. To predict the flow regime without starting a simulation, the
206 Reynolds number was firstly calculated. The Reynolds number quantifies the ratio of
207 inertia to viscous forces, characterizing the flow regime (Eq. 2):

$$208 \quad Re = \frac{\rho * v * d}{\mu} \quad (2)$$

209 where ρ is the culture density (~~it is~~ assumed to have the same density as water, 1000 kg
210 m^{-3}), v is the culture velocity ($m s^{-1}$), d is the tube diameter (0.09 m and 0.125 m for

211 vertical and horizontal systems, respectively), and μ is the dynamic viscosity of the
212 culture (assumed to be the same as water $0.003 \text{ kg m}^{-1}\text{s}^{-1}$). The Reynolds number was
213 calculated to be approximately 27,000 for the vertical system and 5,000 for the
214 horizontal. Note that in tubes with a flow with a Reynolds number above 4,000 is
215 already considered turbulent [3229], and in these conditions transversal variations of
216 culture properties (temperature, dissolved oxygen, biomass concentration, etc.) may be
217 neglected and Navier-Stokes equations can be solved directly. ~~At these~~ With such high
218 Reynolds number's temperature does not significantly influence the motion, because
219 viscous forces (μ) are very small when compared to ~~the~~ inertial forces (v), ~~and~~
220 temperature does not influence significantly the motion.

221 For turbulent flow, Comsol MultiphysicsTM solves the Navier-Stokes as well as
222 continuity equations. Turbulent effects are modeled using “Turbulent Mixing”
223 interfaces for “Transport of Diluted Species” physics. In “Turbulent Mixing” models
224 the additional mixing caused by turbulence is estimated by adding turbulent diffusivity
225 to the molecular diffusivity considering:

$$226 \quad D_T = \nu_T / Sc_T \quad (3)$$

227 where, D_T is the turbulent diffusion, ν_T is the turbulent kinematic viscosity at 20 °C
228 ($1.004\text{E-}06 \text{ m}^2 \text{ s}^{-1}$) and Sc_T is the turbulent Schmidt number (0.7).

229 2.4.2 Transport of dissolved and particulate components

230 Transport of diluted and particulate components with a concentration S_i [g m^{-3}]
231 by convection and diffusion is given by:

$$232 \quad \frac{\delta S_i}{\delta t} + (-D_T \cdot S_i) + \mathbf{u} \cdot \mathbf{c}_i = r_i \quad (4)$$

$$233 \quad r_i = \sum_j v_{j,i} * \rho_j \quad (5)$$

234 where $i=1,2\dots m$ are the different components considered (Table 2), and j is the number
 235 of processes shown in Supplementary Table (4); \mathbf{u} [m s^{-1}] is the vector of velocity, r_i [g
 236 $\text{m}^{-3}\text{s}^{-1}$] is the reaction rate, ρ [$\text{g m}^{-3}\text{s}^{-1}$] is the process rate corresponding to the biokinetic
 237 and chemical j processes described in Solimeno et al. (2015) [2927] and $v_{j,i}$ is the
 238 stoichiometric coefficient. Mathematical expressions of the stoichiometric coefficient
 239 and values of biokinetic, physical and chemical parameters are shown in Supplementary
 240 Tables (6-9).

241 2.4.3 Light attenuation

242 In the present study light intensity decay was described using Lambert-Beer's
 243 Law, which dictates that intensity decreases exponentially as it penetrates into a
 244 perfectly homogeneous section of the culture with a short penetration pathway [2725],
 245 as it is the case of both PBR. In this case light is attenuated by the presence of
 246 microalgae inside the reactors. The average light intensity (I_{av} , [$\mu\text{mol m}^{-2}\text{s}^{-1}$]) at any
 247 point within the culture is therefore calculated as [17]:

$$248 \quad - \quad I_{av} = I_0 \cdot \psi (1 - \exp(-k_i \cdot X_{ALG} \cdot d)) / k_i \cdot X_{ALG} \cdot d \quad (6)$$

249 where, I_0 [$\mu\text{mol m}^{-2}\text{s}^{-1}$] is the incident light intensity, k_i is the extinction coefficient for
 250 microalgae biomass [$0.1 \text{ m}^2 \text{ g}^{-1}$] [8], X_{ALG} is the concentration of microalgae, ψ is the
 251 solar irradiance fraction available in the reactor and d [m] is the diameter of tube.

254 2.4.4 Temperature

255 In our model, the influence of temperature on microalgae activity was
 256 implemented by the thermic photosynthetic factor ($f_{T,FS}$), that which takes into account
 257 the effects of temperature on microalgae growth, and also on endogenous respiration
 258 and inactivation processes (1a, 1b, 2 and 3 in Supplementary Table 4, respectively).

259 | Water temperature varies ~~on~~ both on hourly and daily scales, ~~affecting~~ ~~affecting~~ both
260 | microalgal photosynthesis and respiration rates. The thermic photosynthetic factor is
261 | represented in the model following the work of Dauta et al. (1990) [14]:

$$262 \quad f_{T,FS}(T) = e^{-\left(\frac{T-T_{opt}}{s}\right)^2} \quad (7)$$

263 | where T_{opt} (optimum temperature) was assumed ~~equal to~~ be 25 °C [14] and s equal to 13
264 | [14] (it is a parameter value for empirical fitting).

265 | 2.5 Calibration procedure

266 | Model outputs results are very highly sensitivity sensitive to the maximum
267 | specific growth rate of microalgae (μ_{ALG}), ~~and the~~ mass transfer coefficient for oxygen
268 | (K_{a,O_2}), and carbon dioxide (K_{a,CO_2}). ~~Especially the~~ The mass transfer coefficients
269 | depend on the extension of the surface interface and photobioreactor design [~~2927~~].
270 | Therefore, these parameters were calibrated in the two different tubular
271 | photobioreactors. The model was first calibrated using experimental data obtained from
272 | the vertical photobioreactor located in Almeria (Spain). Dissolved oxygen, pH,
273 | temperature and irradiance were monitored for 24 hours on ~~28th of~~ February 28th, 2012.
274 | Afterwards, the model was calibrated with experimental data from the horizontal
275 | photobioreactor located in Barcelona (Spain). Data used for this calibration were
276 | retrieved from ~~a 3~~ three days's batch experiment from April 16th, 2012 to April 19th.
277 | 2012. of April. Available data used for the calibration procedure are shown in
278 | Supplementary Tables (1-2). The initial concentrations of components in the vertical
279 | and horizontal photobioreactors at the beginning of the experiments are shown in Table
280 | 3. In the horizontal PBR the concentrations of NH_4^+ and NH_3 were lower than the
281 | analytical method's detection limit ~~of the analytical method~~ and therefore are
282 | considered to be zero for ~~the this~~ model ~~as 0~~. Note ~~that the~~ difference in initial

283 | concentrations of microalgae (X_{ALG}) ~~is different in~~between the two PBRs due to their
284 | different operating conditions

285 | 2.6 Study cases

286 | Practical study cases have been done to evaluate the influence of both
287 | temperature and irradiance on microalgae production, and the effect of oxygen
288 | concentration in the loop. The vertical photobioreactor of Almeria (Spain) was selected
289 | as reference for these studies.

290 | Starting from the initial concentrations used for ~~the~~ calibration of the model in
291 | the vertical photobioreactor, average daily microalgae production was simulated using
292 | daily temperature and irradiance variations ~~of from the~~ 17th day of each month of year.
293 | Two scenarios were evaluated. In the first set of simulations the vertical photobioreactor
294 | was under controlled temperature by passing cooling water at 1500 L/h through an
295 | internal heat exchanger located in the bubble column of the photobioreactor. In a second
296 | set of simulations, temperature was obtained from meteorological annals of Almeria
297 | (Spain). ~~An estimation of the total annual production for these~~ These two scenarios
298 | were compared and an estimation of the total annual production using monthly
299 | irradiance variations was calculated. Irradiance, expressed as photosynthetically active
300 | radiation (PAR), was estimated for Almeria (Spain) from the mathematical equations
301 | presented in Supplementary Table 10 [2].

302 | Moreover, ~~keeping the reactor under controlled temperature,~~ oxygen
303 | concentration throughout the 400 m ~~length of the~~ vertical photobioreactor was evaluated
304 | while maintaining the reactor under controlled temperature. Dissolved oxygen profile
305 | in the loop configuration was simulated at noon in the months of July and January,
306 | when ~~it was recorded~~ the highest and lowest temperature, respectively, were recorded.
307 | and irradiance, respectively.

308 |

309 3. Results

310 In this work simulations for two different photobioreactors were studied. First
311 we present the results of the model calibration for the vertical photobioreactor. Fig. 4
312 shows that the model was able to accurately match ~~dissolved oxygen~~DO and pH trends
313 over the course of one day inside the system, with decreasing and low pH ~~decreases~~
314 ~~during the day~~ due to CO₂ injection (which displaces the equilibrium of carbon species).
315 ~~As can be seen the model is able to accurately capture pH variations.~~

316 Fig. 5 shows the results of the calibration in the horizontal photobioreactor.
317 Experimental and simulated dissolved oxygen and pH values inside the open-air tanks
318 of the horizontal photobioreactor are presented. As can be seen, the wavelike trend of
319 pH varied ~~with a general wavelike trend~~ due to microalgae activity, which is quite well
320 simulated by the model. Moreover, Fig. 6 shows the experimental and simulated nitrate
321 (N_NO₃) and bicarbonate (C_HCO₃) concentrations in the horizontal system. The
322 model was able to reproduce quite well the trend of experimental data. In absence of
323 ammonia species, only nitrates are used as nitrogen substrates for microalgae growth.
324 The low concentration of nitrate in the culture medium limited the activity of
325 microalgae. As can be seen, microalgae consumed ~~quickly~~ nitrate concentrations
326 quickly in the first hours of experiment (Fig. 6). Likewise, Fig. 6 shows that bicarbonate
327 concentrations decreased faster in the first hours due to intense microalgae activity.
328 After 22 hours, in absence of nitrate, daily variations of bicarbonate are related to
329 changes in equilibrium species of carbon.

330 Note that, in general, simulations of the vertical PBR were more accurate than
331 those of the horizontal due to ~~the fact that in in~~ the horizontal system there was some
332 growth of other microorganisms different from microalgae (e.g., bacteria and protozoa);
333 . This was to be expected as the culture water ~~for culture~~ was from an irrigation
334 channel. The activity of these microorganisms ~~affected~~ affected simulated factors

335 | thought it is not known to ~~which-what extend~~extent, because unfortunately we ~~haven't~~
336 | ~~numbers do not have values~~ for ~~this-these~~ organisms.

337 | Table 4 presents the values of the parameters that were calibrated in each
338 | photobioreactor. Note that maximum specific growth rate (μ_{ALG}) and the transfer of
339 | gases to the atmosphere (K_{a,O_2} and K_{a,CO_2}) were also calibrated in our previous works
340 | [2927, 3028]. In this previous works ~~the -model output results are demonstrated to be~~
341 | very sensitive to these parameters [2927, 3028], and therefore should be calibrated with
342 | great accuracy. Furthermore, ~~especially~~ gas transfer parameters depend on the extension
343 | of the surface interface. Due to different ~~PBRs design-of the PBR~~, modifications of
344 | these parameters were considered worthwhile.

345

346 | 4. Discussion

347 | 4.1 New features of the model

348 | In comparison to our previous work [2927], where a 0D domain was applied,
349 | here ~~in the present work a~~ 2D domain was used to represent the two tubular
350 | photobioreactors. The domain was divided in two sub-domains (D1 and D2), where
351 | different conditions from the tubes (D1) to the open body (D2) of the photobioreactors
352 | were applied. According to the function of bubble column in the vertical system and the
353 | open-air tank in the horizontal system, the transfer of gases to the atmosphere was only
354 | applied to the D2 domain that ~~corresponded~~corresponds to the total volume of these
355 | specific parts.

356 | A periodic condition was applied at boundaries 1 and 2 to reproduce the
357 | recirculation of flow from the loop configuration to the bubble column in the vertical
358 | system, and from the tubes to the open-tank in the horizontal system. Simulation results
359 | demonstrated that these simplifications were adequate to describe the specific parts of
360 | different tubular photobioreactors. Moreover, fluid flow and transport equations were

361 added in the current model to obtain a realistic representation of the hydrodynamics in
362 the photobioreactors.

363 ~~Respect from~~In addition to the previously mechanistic model presented by
364 Solimeno et al. (2015) [2927] light attenuation through the medium was implemented.
365 Light intensity decays exponentially due to microalgae biomass ~~accumulated~~
366 accumulation inside the reactors. Assuming a perfect mixing of medium, due to
367 turbulent flow regime, an irradiance average I_{av} was used to represent any point ~~of~~
368 thewithin the reactor.

369

370 4.2 Calibration of the model

371

372 Results of the sensitivity analysis, reported in our previous work [3028], had
373 indicated that the maximum specific growth rate of microalgae (μ_{ALG}) and the mass
374 transfer coefficient for oxygen (K_{a,O_2}) and carbon dioxide (K_{a,CO_2}) were the parameters
375 with the greatest impact on simulation outputs. Therefore, calibration of these
376 parameters ~~have to be calibrated~~must be occur in each particular case.

377 The calibrated maximum specific growth rate of microalgae ($\mu_{ALG} = 1.7 [d^{-1}]$) in
378 the vertical photobioreactor fits well within literature range $[0.4-2.0 d^{-1}]$. Also, the mass
379 transfer coefficient in the bubble column for oxygen which was $K_{a,O_2} = 2.9E-03 s^{-1}$ fits
380 into the range values for vertical photobioreactors $[1.2E-03 \text{ to } 7.7E-03 s^{-1}]$ [18]. The
381 mass transfer coefficient for carbon dioxide ($K_{a,CO_2} = 2.8E-03 s^{-1}$) was consistent with
382 range values $[1.1E-03-7.0E-03 s^{-1}]$ for bubble column systems [18]. These same
383 parameters were calibrated with experimental data over ~~3-three~~ days from the horizontal
384 photobioreactor located in Barcelona (Spain). Likewise ~~the previously~~as in the previous
385 calibration, the values generated for the maximum growth rate of microalgae ($\mu_{ALG} =$
386 $1.7 [d^{-1}]$)-~~and~~, the mass transfer of oxygen ($K_{a,O_2} = 9.2E-03 [s^{-1}]$) and carbon dioxide

387 | ($K_{a,CO_2} = 9.0E-03 [s^{-1}]$) were all in agreement with literature ranges for tubular
388 | photobioreactors [9].

389 | Mass transfer coefficients depend on ~~the~~ temperature, ~~the~~ mixing and especially
390 | most importantly, the extension of the surface interface. Thus, variable values of mass
391 | transfer coefficients from vertical and horizontal photobioreactors are due to different
392 | design and scale-up of bubble column and open-tanks, respectively.

393 | Also the culture medium influences the mass transfer coefficients and the
394 | maximum growth rate of microalgae. In this work the horizontal photobioreactor was
395 | filled with agricultural runoff ~~in~~ which could be present ~~cointein~~ few concentrations of
396 | bacteria and other microorganisms. The activity of these microorganisms could
397 | influence dissolved oxygen and carbon dioxide concentrations in the medium culture,
398 | and therefore could slightly affect the values of the calibrated parameters. However,
399 | single microscopic observations during the experiment indicated that their concentration
400 | was irrelevant in comparison to microalgae (as usual in this type of PBR), and thus their
401 | influence is considered very low or almost negligible. Calibrating the model in two
402 | different photobioreactors (e.g., horizontal and vertical) ~~and using with~~ different types of
403 | media has ~~allowed to determinate~~ proved the robustness and resilience of the
404 | mathematical model to operate under variables conditions. ~~of the mathematical model,~~
405 | ~~which can operate under variables conditions.~~

406 | *4.3 Study case: microalgae production as a function of temperature and*
407 | *irradiance*

408 |
409 | Irradiance and temperature play an important role in microalgae production.
410 | These physical factors influence biokinetic and chemical processes related to
411 | microalgae growth. Irradiance is strictly correlated to photosynthesis rate. At high level
412 | of irradiance, microalgae become 'light saturated' because photosynthesis cannot
413 | process more photons. As result, the rate of photosynthesis ~~starts to progressively~~ starts

414 | to stabilize [9, 13]. Temperature influences the equilibrium of chemical species (carbon
415 | and nitrogen), ~~the~~ uptake of nutrients, ~~and~~ transfer of gases to the atmosphere, ~~but and~~
416 | especially the microalgae growth rates. The optimal temperature for microalgae growth
417 | ranges between 15°C and 25°C, depending on the species [5, 19]. Temperature above or
418 | below this range negatively affects ~~negatively~~ biomass yields.

419 | Thanks to the model, previously calibrated with daily experimental data, has
420 | been possible to make predictions of microalgae production over long-term knowing
421 | with different environmental factors, such as temperature and irradiance. Simulations of
422 | the average daily microalgae production at a monthly scale in the vertical
423 | photobioreactor are presented in Fig 7. As can be observed simulations indicate that
424 | production is generally higher under daily temperature variations due to a more
425 | favorable temperature range (Supplementary Table 3). Table 5 presents the annual
426 | microalgae production comparing the two scenarios studied: under controlled
427 | temperature and with daily temperature variations. Although the growth of microalgae
428 | decreases ~~by with~~ high temperature and irradiance during the months of June, July and
429 | August (when the highest temperatures of the year occur), total annual production of
430 | microalgae exposed to daily temperature variations is higher than the reactor under
431 | controlled temperature. To optimize production, it might be considered to only use
432 | cooling water ~~might be only used~~ during the hottest months (June, July and August).
433 | Moreover, simulations results show that during the summer the production is also
434 | inhibited due to high dissolved oxygen concentrations ~~throughout~~ throughout loop
435 | configuration up to 250% of air saturation (see next section).

436

437

438 | *4.4 Study case: oxygen concentration*

439

440 | Fig. 8 shows the simulations of the dissolved oxygen profile throughout the 400
441 | m length of the vertical photobioreactor at noon (when the highest temperature occurs)

442 in the months of January and July. These two months were selected as they represent
443 the minimum and maximum microalgae activity in a monthly basis time scale. As can
444 be seen, the lower light intensity and temperature in January gives as a result lower
445 dissolved oxygen concentrations in contrast to July. Also it can be observed in both
446 months how dissolved oxygen concentration increases throughout the loop and
447 decreases in the bubble column. In July, transfer of excess of dissolved oxygen to the
448 atmosphere throughout the airlift permits to re-establish, at the beginning of loop
449 configuration, the oxygen level under the maximum concentration of oxygen dissolved
450 in water ($32 \text{ gO}_2 \text{ m}^{-3}$) equal 350% of saturation ($9.07 \text{ gO}_2 \text{ m}^{-3}$) [1, 8]. This property of
451 the photobioreactor design is especially important in warm months (such as July), when
452 a high photosynthetic activity could cause inhibition due to oxygen accumulation.

453 The model presented in this work allows to simulate and study microalgae
454 growth inhibition due to high dissolved oxygen concentrations thanks to the inclusion of
455 a photorespiration factor $f_{PR}(S_{O_2})$ [2927]. The function ($f_{PR}(S_{O_2})$) in Fig. 9 describes that
456 for dissolved oxygen concentrations lower than the $250\% S_{O_2}^{SAT}$ ($22.67 \text{ gO}_2 \text{ m}^{-3}$) the
457 photosynthesis rate is reduced ~~of by~~ 10%. Above this value, the photosynthesis rate
458 decrease more quickly with a vertical asymptote and is equal at zero when dissolved
459 oxygen reaches the 350% saturation limit ($\tau S_{O_2}^{SAT} = 32 \text{ gO}_2 \text{ m}^{-3}$).

460 In process design, the current model can be used to ~~study which could be find~~ the
461 maximum photobioreactor length to avoid oxygen inhibition. ~~Here, as For~~ example, ~~we~~
462 ~~present~~ for the month of July, simulations were conducted using half the previous
463 ~~which we analyse what is the effect of reducing the~~ bubble column volume to the half
464 (from 0.44 m^3 to 0.22 m^3) in the vertical photobioreactors loops ~~of~~ (400 m and 250 m).
465 As seen in Fig. 10, ~~shows simulation results, and as can be seen~~ reducing the volume of
466 the bubble column and ~~keeping-keeping~~ the original loop configuration length (400 m),
467 the simulation results show that the DO ~~dissolved oxygen~~ exceeds the saturation limit
468 ~~and will~~ inhibiting microalgae growth. The volume of bubble column is not enough to

469 transfer the excess of dissolved oxygen to the atmosphere. On the contrary, simulations
470 indicate that a 250 m length, photobioreactor greatly reduces the oxygen accumulation.

471

472 **5. Conclusion**

473

474 In this paper ~~the a~~ new mechanistic model to simulate microalgae growth was
475 calibrated in two different tubular photobioreactors. Fluid flow, transport equations and
476 light attenuation were included in the model described in our previous work and
477 implemented in COMSOL MultiphysicsTM software. ~~Uncertainly—Uncertainty~~
478 parameters from previous ~~by sensibility—sensitivity~~ analysis were calibrated in each
479 ~~particular~~ photobioreactor. The results of calibration indicate that the mass transfer of
480 gases and the maximum specific growth rate of microalgae fit well within literature
481 ranges. Moreover, the developed model demonstrates potential prediction of oxygen
482 accumulation throughout the loop configuration and daily microalgae production as a
483 function of temperature and irradiance. The model proves to be an efficient tool for
484 photobioreactor design and ~~production production~~ optimization.:-

485

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Table 1. Agricultural runoff characteristics during batch experiment in the tubular horizontal photobioreactor located in Barcelona (Spain).

Parameter	Agricultural runoff
pH	8.4
Dissolved oxygen (g m^{-3})	6.6
NO_3^- -N (g m^{-3})	0.6
Alkalinity ($\text{g CaCO}_3 \text{ m}^{-3}$)	223

Table 2. Dissolved and particulate components considered in the model.

Component	Description	Units
<i>Dissolved Components</i>		
S_{NH_4}	Ammonium nitrogen	$\text{gN-NH}_4 \text{ m}^{-3}$
S_{NH_3}	Ammonia nitrogen	$\text{gN-NH}_3 \text{ m}^{-3}$
S_{NO_3}	Nitrate nitrogen	$\text{gN-NO}_3 \text{ m}^{-3}$
S_{CO_2}	Carbon dioxide	$\text{gC-CO}_2 \text{ m}^{-3}$
S_{HCO_3}	Bicarbonate	$\text{gC-HCO}_3 \text{ m}^{-3}$
S_{CO_3}	Carbonate	$\text{gC-CO}_3 \text{ m}^{-3}$
S_{O_2}	Dissolved oxygen	$\text{gO}_2 \text{ m}^{-3}$
S_{H}	Hydrogen ions	gH m^{-3}
S_{OH}	Hydroxide ions	gH-OH m^{-3}
<i>Particulate Component</i>		
X_{ALG}	Microalgae biomass	gTSS m^{-3}

Table 3. Initial concentrations of the components in the vertical photobioreactor of Almeria (Spain) and horizontal photobioreactor of Barcelona (Spain).

Components	Concentrations		Units
	Vertical PBR	Horizontal PBR	
X_{ALG}	774.14	251	gTSS m^{-3}
S_{NH_4}	14	-	$\text{gN-NH}_4 \text{ m}^{-3}$
S_{NH_3}	0.684	-	$\text{gN-NH}_3 \text{ m}^{-3}$
S_{NO_3}	4.2	0.6	$\text{gN-NO}_3 \text{ m}^{-3}$
S_{CO_2}	1.59	0.068	$\text{gC-CO}_2 \text{ m}^{-3}$
S_{HCO_3}	100	7.59	$\text{gC-HCO}_3 \text{ m}^{-3}$
S_{CO_3}	0.62	0.085	$\text{gC-CO}_3 \text{ m}^{-3}$
S_{O_2}	7.2	6.64	$\text{gO}_2 \text{ m}^{-3}$
S_{H}	6.31E-6	3.55E-6	gH m^{-3}

S_{OH}	1.58E-3	2.82E-3	$gH-OH m^{-3}$
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Table 4. Values of calibrated parameters in the vertical and horizontal photobioreactors.

Parameter	Description	Value	
		Vertical PBR	Horizontal PBR
μ_{ALG}	Maximum specific growth rate of microalgae	$1.7 d^{-1}$	$1.7 d^{-1}$
K_{a,O_2}	Mass transfer coefficient for oxygen	$2.9E-03 s^{-1}$	$9.2E-03 s^{-1}$
K_{a,CO_2}	Mass transfer coefficient for carbon dioxide	$2.8E-03 s^{-1}$	$9.0E-03 s^{-1}$

Table 5. Comparing total annual production under controlled temperature and daily temperature variations versus optimizing system using cooling water during summer.

Total annual production	Value
Optimizing system	$1796.86 gTSS m^{-3}$
Daily temperature variations	$1714.53 gTSS m^{-3}$
Under controlled temperature	$1604.48 gTSS m^{-3}$

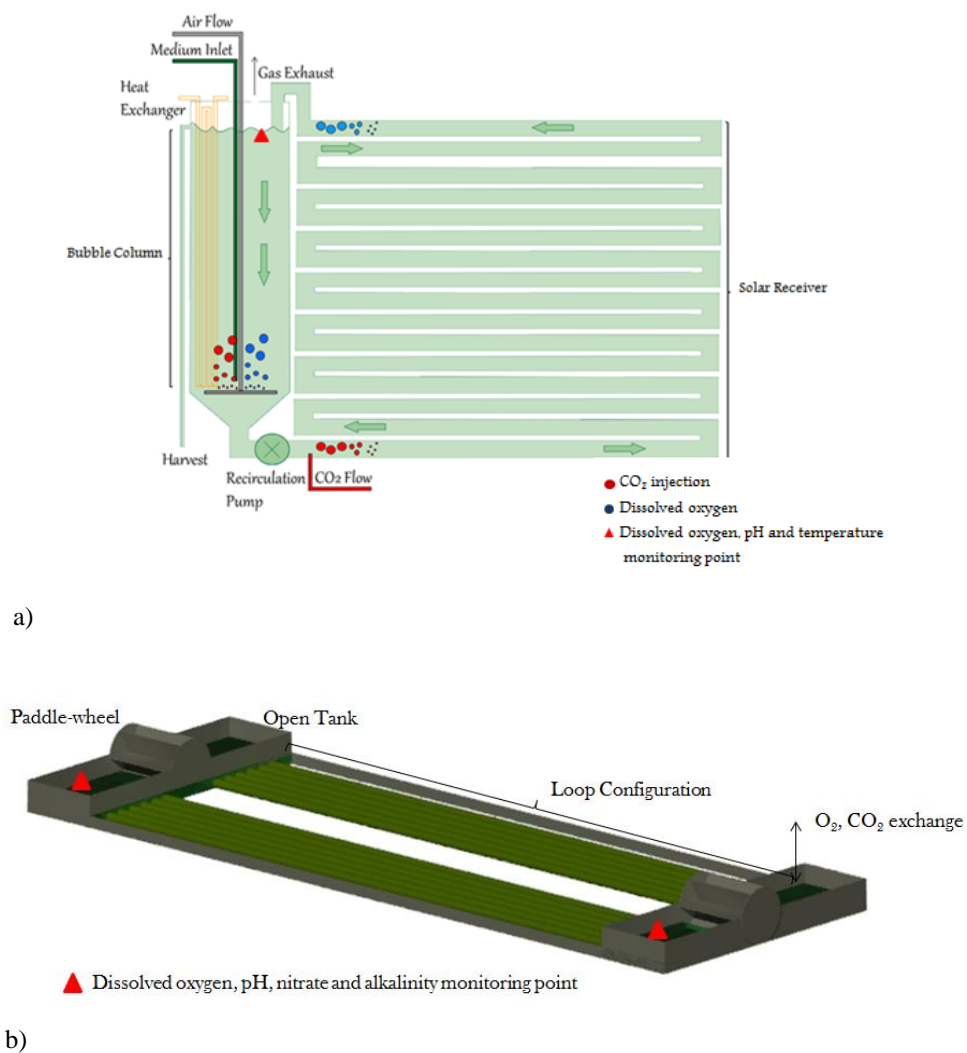


Fig. 1. a) Tubular vertical photobioreactor located in Almeria (Spain) with details of the solar receiver (a continuous tubular loop) and a mixing unit (a bubble column). The culture is continuously recirculating from one to the other part using airlift and mechanical pumps. [16], b) Tubular horizontal photobioreactor located in Barcelona (Spain) with details of the two open-air tanks and the loop configurations (6 tubes per each flow direction). Mechanical paddlewheels promote the recirculation of the culture through the system.

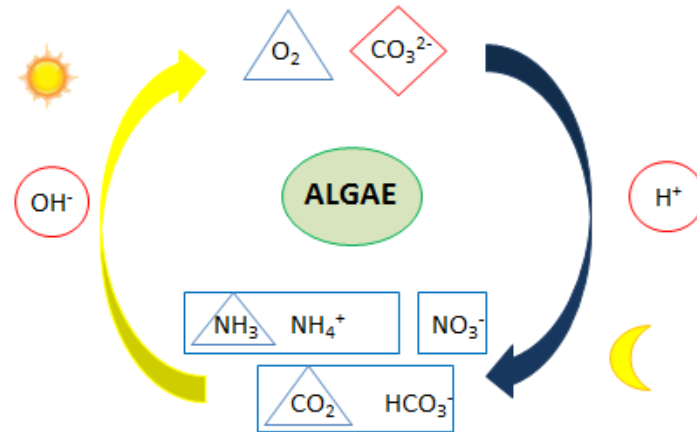


Fig. 2. General schematic representation of the conceptual model by Solimeno et al. (2015) [27]. Microalgae (green ellipse), substrates (rectangles), gaseous species (triangles) and species depending on algal activity which are neither substrates nor gases (diamonds and circles). Other nutrients (e.g. phosphorus) and micronutrients are not limiting factors.

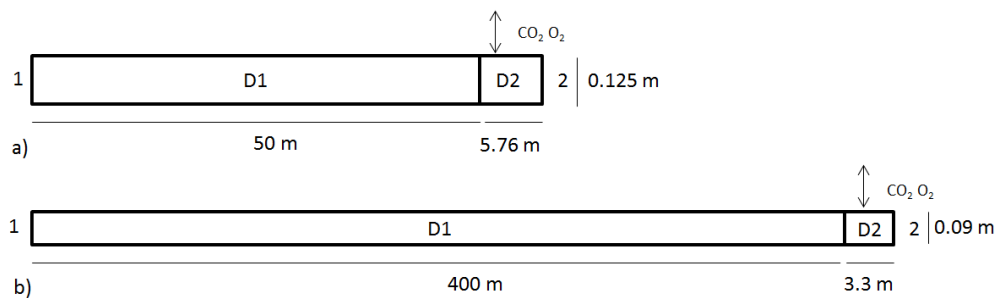
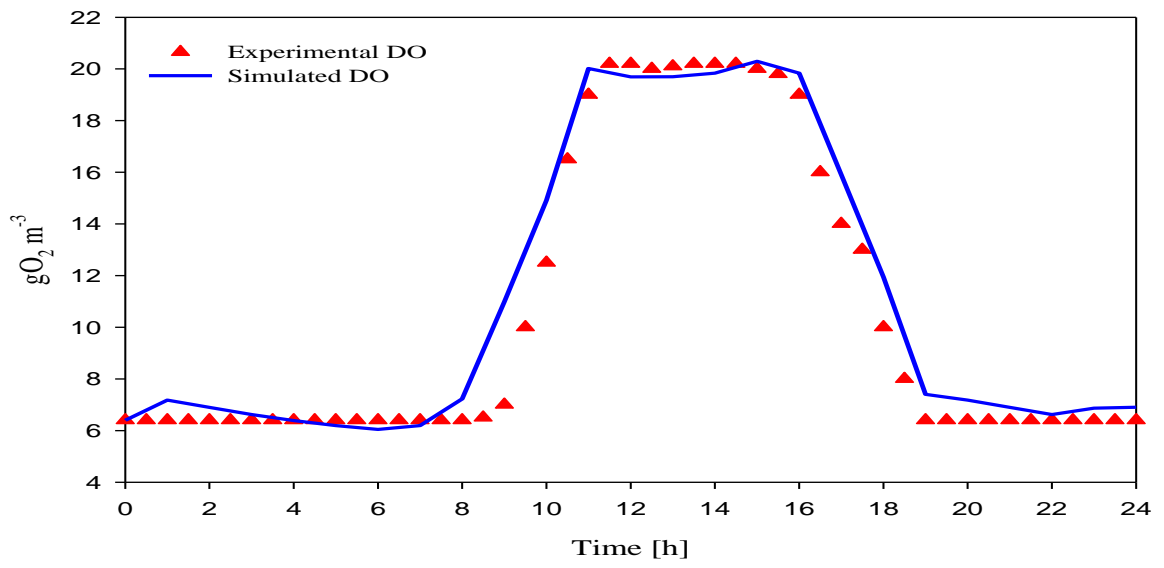
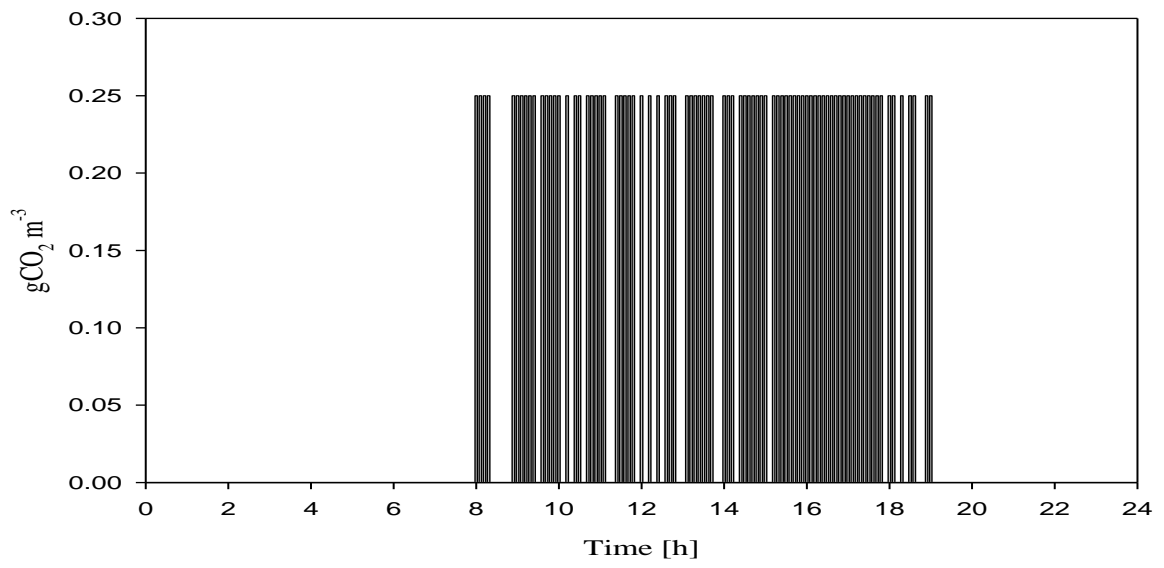


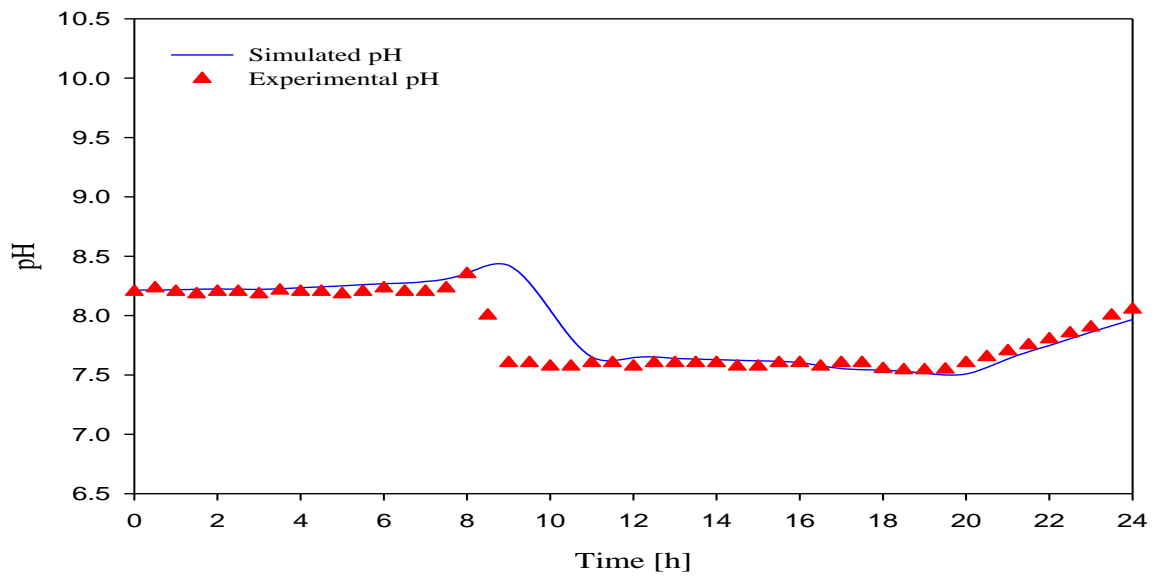
Fig. 3. Schematic representation of the model domain, a) simplification of the horizontal photobioreactor located in Barcelona (Spain), b) simplification of the vertical photobioreactor in Almeria (Spain). D1 represents the loop configuration of both PBRs and D2 is the total volume of open-air tank (a) and bubble column (b) respectively for horizontal and vertical photobioreactor. A periodic condition was applied at boundaries 1 and 2 to reproduce the continuous culture flow.



a)

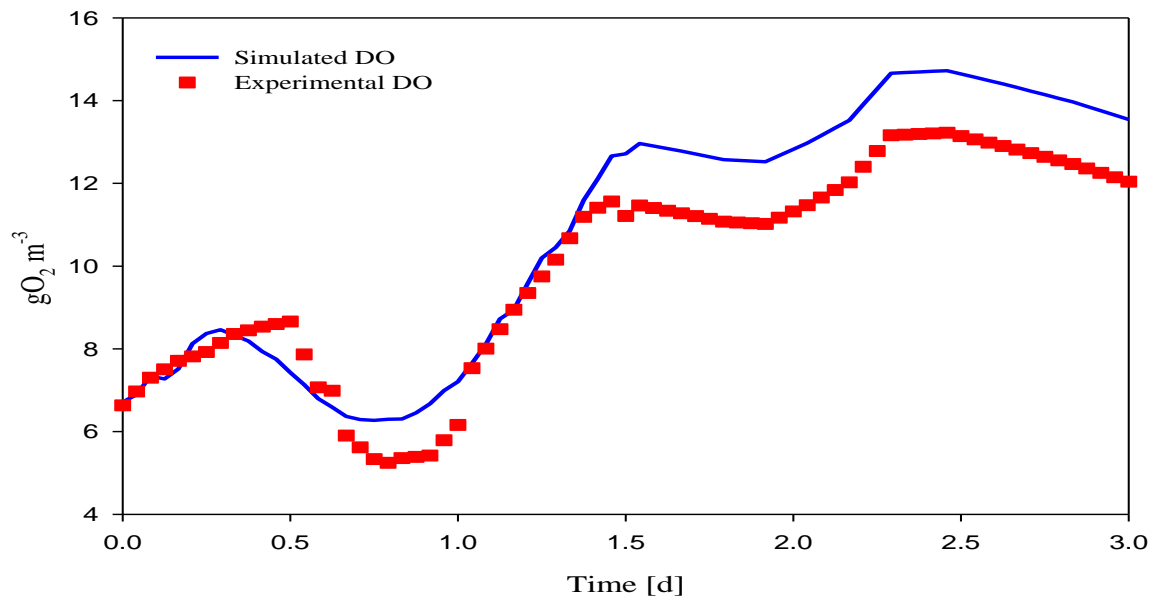


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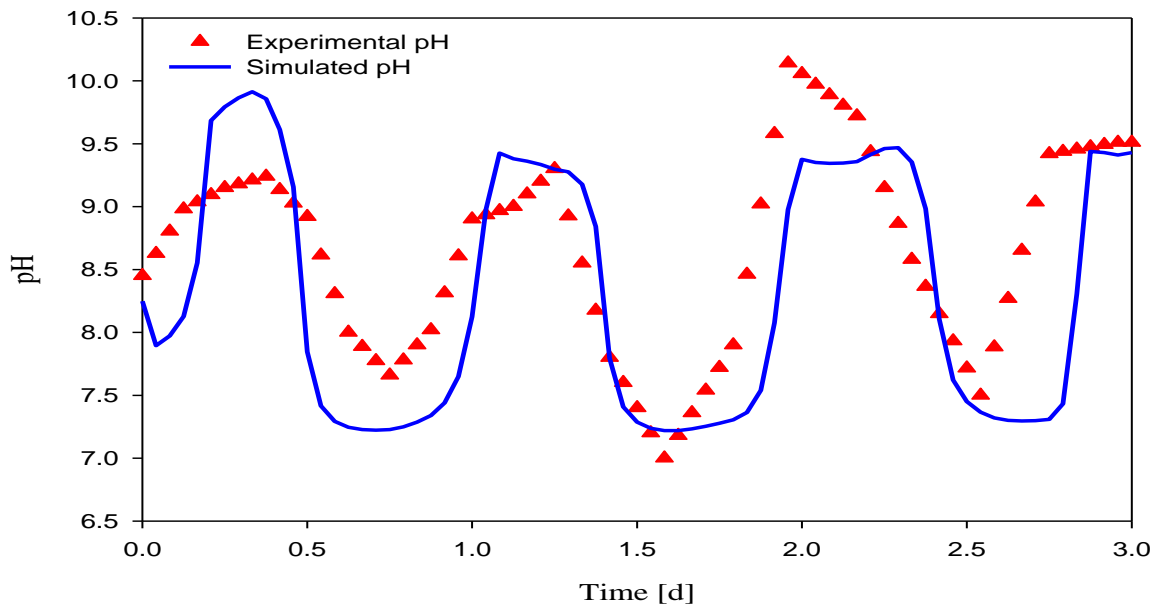


c)

Fig. 4. Experimental (red triangles) and simulated (blue line) (a) dissolved oxygen (DO) and (c) pH values as a function of CO₂ injection (b) over the 24 hours in the vertical photobioreactor in Almeria (Spain).

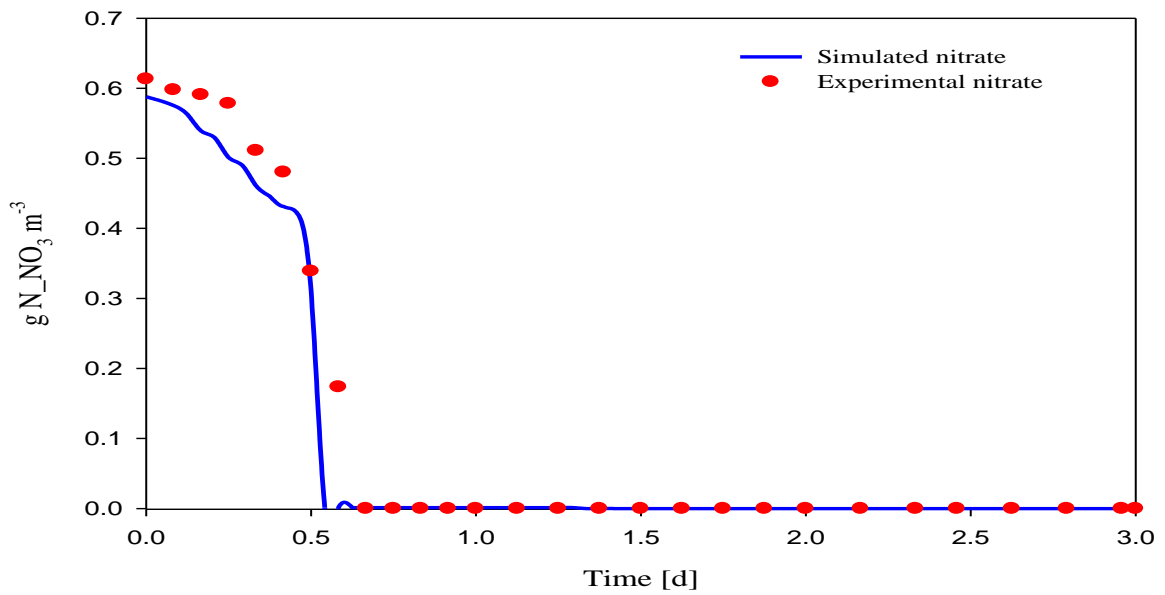


a)

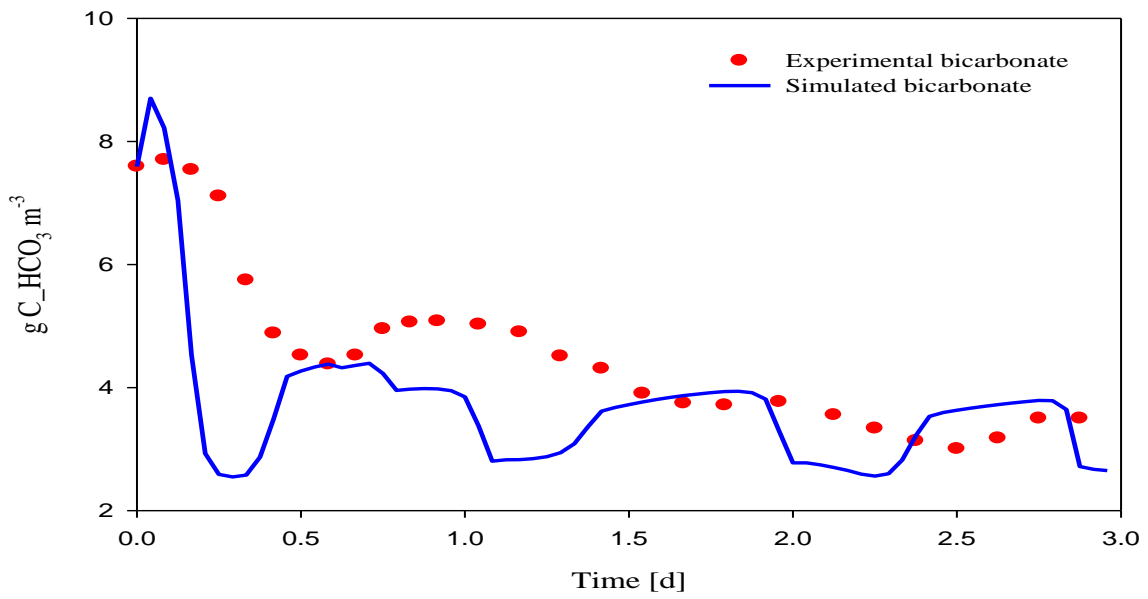


b)

Fig. 5. Experimental (red triangles) and simulated (blue line) (a) dissolved oxygen (DO) and (b) pH values over the three days in the horizontal photobioreactor in Barcelona (Spain).



a)



b)

Fig. 6. Experimental (red dots) and simulated (blue line) (a) nitrate and (b) bicarbonate concentrations over the three days in the horizontal photobioreactor in Barcelona (Spain).

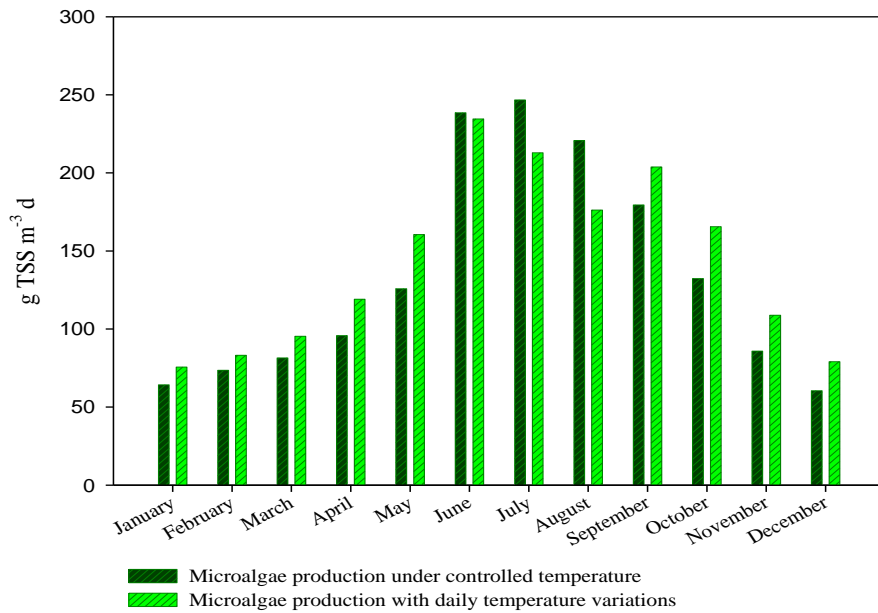


Fig. 7. Average daily microalgae production for each month of the year under controlled temperature and with daily temperature variations.

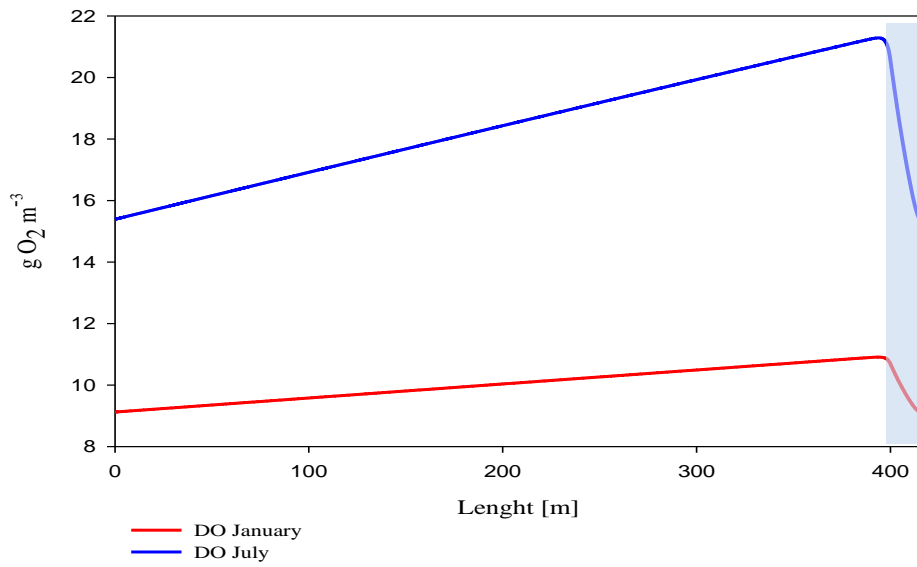


Fig. 8. Simulations of dissolved oxygen (DO) concentration profile throughout the vertical photobioreactor in Almeria (Spain) in the months of January and July. Bubble column position is represented by blue region.

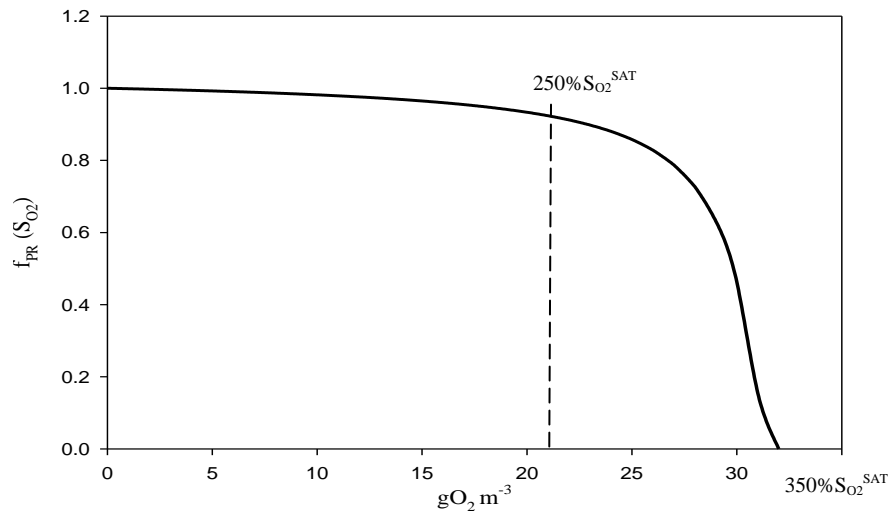


Fig. 9. Profile of photorespiration factor function for value of dissolved oxygen concentrations below the saturation limit ($\tau S_{O_2}^{SAT}$).

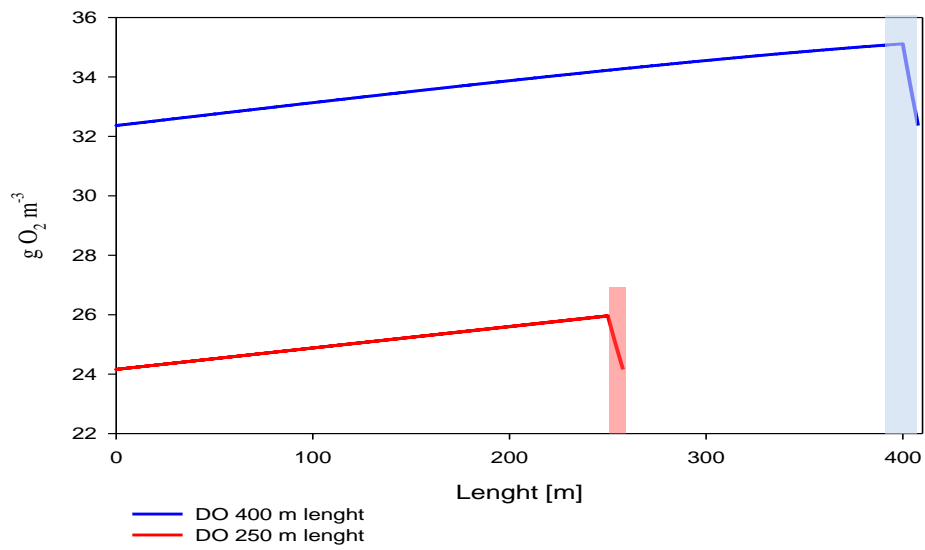
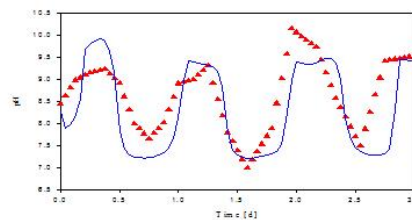
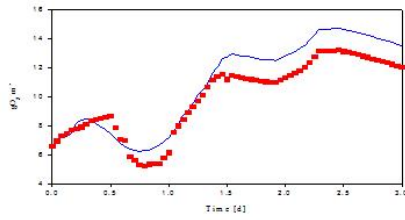
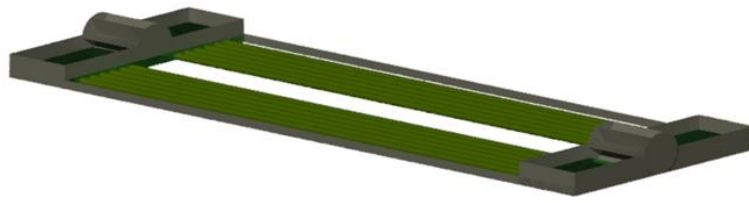


Fig. 10. Simulations of dissolved oxygen (DO) concentration profile throughout 400 m and 250 m length of the vertical photobioreactor in Almeria (Spain) in the months of July. Bubble column position is represented by blue and red rectangle, for 400 m and 250 m length of vertical photobioreactor, respectively.

Supplementary Material

[Click here to download Supplementary Material: Supplementary Tables - review.docx](#)

Graphical abstract



Highlights

- New mechanistic model for microalgae production in closed photobioreactors is developed.
- The model integrates the biological and engineering aspects of the systems.
- The accuracy of the model has been validated using real pH and dissolved oxygen values.
- The model has been verified in two different closed photobioreactors.

1 **1. Introduction**

2 Industrial production of microalgae can be accomplished in open or closed
3 photobioreactors. Open systems are shallow channels in the shape of race tracks
4 (raceway reactors) and have been extensively studied in the past [9, 15]. Though open
5 photobioreactors represent an efficient economic solution in front of closed
6 photobioreactors, they can be easily contaminated by microorganisms and difficult to
7 control. These disadvantages make closed photobioreactors more suitable when high-
8 value products are the target of the culture. Closed systems strictly control chemical,
9 physical and biological factors and can improve conditions for microalgae growth by
10 optimizing light absorption due to turbulent conditions in the culture [9, 11, 30, 31].

11 Closed photobioreactors (as well as open raceways) are sensitive to carbon
12 limitations and pH variations that could limit photosynthesis and therefore biomass
13 production [16]. Carbon and pH limitations can be corrected by supplying carbon
14 dioxide (CO_2) in order to maintain high photosynthesis rates and pH control. However
15 the two most critical issues of closed photobioreactors are the risk of overheating and
16 their potential for oxygen accumulation and subsequent growth inhibition [20]. To
17 prevent overheating, closed photobioreactors often require cooling as well as degasser
18 systems [32]. Concentrations of dissolved oxygen (DO) in the culture above 250% air
19 saturation can dangerously inhibit microalgae activity [12].

20 Over the last few decades, mathematical models have proven to be useful tools
21 for the design, analysis, operation and control in multiple engineering problems [5].
22 Nowadays, models have become essential tools for understanding complex processes,
23 such as those occurring in photobioreactors. In the case of microalgae cultures, models
24 are less developed than those seen in other fields. When models contain too few
25 parameters, they risk the capability of not capturing the complexity of microalgae
26 cultures in long-term scenarios, and therefore can be unreliable. Having this in mind,
27 Solimeno et al. (2015) [27] developed a complete mechanistic mathematical model that

28 includes crucial physical and biokinetic processes that describe microalgae growth in
29 different types of cultures, particularly in wastewater (where growth is controlled by
30 carbon and nitrogen limitations). This model was calibrated with data from a complete
31 stirred culture fed with simulated treated wastewater using a 0D domain [27]. A global
32 sensitivity analysis was carried out using the same set of data [28]. In the present paper
33 we intend to go beyond our previous work, calibrating the model with data from two
34 different pilot scale tubular closed photobioreactors fed with different types of medium
35 culture. In this present case, a 2D domain, which represents the hydrodynamics of the
36 system (i.e., transport of diluted species and mass transfer phenomena), is coupled with
37 the previous mechanistic model [27]. The resulting model has been implemented into
38 the COMSOL MultiphysicsTM software, which solves equations using the finite
39 elements method (FEM).

40 The aim of the present study is to calibrate the new and more complex
41 mechanistic model of Solimeno et al. (2015) [27] using experimental data from two
42 different tubular photobioreactors. The potential of the model is demonstrated by means
43 of practical study cases in which we simulate oxygen concentrations (the most critical
44 growth inhibition factor of closed photobioreactors) and predict microalgae production
45 as a function of temperature and light intensity. Simulations show the potential of
46 photobioreactor configurations to optimize microalgae production. The overall objective
47 of this model is to become a reference to simulate physical, chemical and biokinetic
48 microalgae processes in different types of photobioreactors fed with different types of
49 medium cultures.

50

51 **2. Methods**

52 *2.1 Pilot closed photobioreactors and experimental data*

53 Both photobioreactors were located in Spain, one in “Estación Experimental Las
54 Palmerillas”, property of Fundación CAJAMAR in Almeria, and the other in
55 “Agropolis”, property of Universitat Politècnica de Catalunya-BarcelonaTech in
56 Barcelona (Fig. 1). The vertical tubular photobioreactor (PBR) in Almeria includes a
57 loop solar receiver made of transparent plastic tubes of 0.09 m diameter with a total
58 horizontal length of 400 m, and a 0.4 m diameter bubble column with 3.5 m of height,
59 and has a total working volume of 3,000 L. The PBR unit is used to produce the
60 microalgae *Scenedesmus almeriensis*, which is characterized by a high growth rate and
61 tolerance temperatures up to 45 °C and pH values up to 10 [1, 25]. The PBR works by
62 creating continuous flow of culture between loop and bubble column by means of a
63 centrifuge pump located at the bottom of the column. The pump provides a constant
64 flow velocity of 0.8 m s⁻¹ inside the loop. The pH of the culture is controlled by
65 injection of pure CO₂ at 5 L min⁻¹. In the bubble column, excess DO is removed by a
66 constant airflow rate of 140 L min⁻¹. The culture temperature is maintained by passing
67 cooling water at 1,500 L h⁻¹ through an internal heat exchanger located inside the
68 bubble column. When fresh culture medium is poured into the system, the culture is
69 harvested through an overflow located on top of the column. Temperature, pH and DO
70 are measured at several locations along the tube using Crison probes (Crison
71 Instruments, Spain) connected to a control-transmitter unit MM44 (Crison Instrument,
72 Spain). Liquid and gas flow rates are measured using digital flowmeters (PF2W540 and
73 PF2A510, from SMC, Japan). All of these monitoring systems are in turn connected to a
74 control computer through a data acquisition device NI Compact FieldPoint (National
75 Instruments, USA) [15]. Data for the present study were obtained at the end of a two
76 month experiment in which the photobioreactor was operated in continuous mode,
77 medium flow rate of 1,020 L d⁻¹, and under controlled pH (7.8) and temperature (lower
78 than 35 °C). As a result, the amount of microalgae biomass was kept fairly constant.
79 Culture medium used was Mann&Myers, prepared using agricultural fertilizers.

80 Collected data were retrieved in batch mode by switching off the feeding for 24 hours
81 (at the end of the two months). Dissolved oxygen and pH data were recorded every 30
82 minutes, while temperature and irradiance were measured every hour.

83 The horizontal tubular photobioreactor in Barcelona is composed of two open-
84 air tanks made of polypropylene and is 1.8 x 1 x 0.4 m (L x W x H) in size. These tanks
85 include paddlewheels that provide enough head pressure to move the culture through 12
86 (6 per each flow direction) transparent 0.125 m diameter polyethylene tubes (each 50 m
87 length). Culture flows from one tank to the other at a constant velocity of 0.125 m s⁻¹.
88 Tanks also allow release of exceeding oxygen accumulated along tubes. The PBR has
89 an effective volume of 8.5 m³. Note that in this PBR there is no CO₂ injection or pH
90 control. Data used for the present work were retrieved from a three days batch
91 experiment and measured in each tank. For this experiment the PBR was filled with 8
92 m³ of agricultural runoff from a nearby agriculture canal which were inoculated with 0.5
93 m³ of inoculum with microalgae from a previous experiment (Table 1). The PBR
94 contained different microalgae species belonging to the genus *Pediastrum sp.*, *Chlorella*
95 *sp.* and *Scenedesmus sp.*

96 The horizontal PBR has dissolved oxygen and pH online sensors in each tank
97 that record data every hour, and temperature and irradiance online sensors that record
98 data every two to three hours. Gathered data are stored using a Programmable Logic
99 Controller (PLC) that is connected to a computer with supervisory control and a data
100 management system (Green web manager 2.0). During the three days of experiments,
101 offline samples were taken every two-three hours and analyzed in the laboratory for
102 nitrates and alkalinity. Analysis of nitrate ion chromatography was accomplished using
103 a Thermo Finnigan chromatograph with a metallic detector TCD (thermal conductivity
104 detector). Alkalinity was analysed using conventional titrimetric procedures indicated in
105 Standard Methods [3]. Note that bicarbonate was calculated using alkalinity
106 measurements, pH, and equilibrium constants of carbon species (Eq. 1).

107

$$108 \quad \text{Alkalinity} = 50 * \left[\frac{S_{\text{HCO}_3}}{12} + 2 * \frac{S_{\text{CO}_3}}{12} + S_{\text{OH}} - S_{\text{H}} \right] \quad (1)$$

109

110 *2.2 Conceptual model*

111 The new mechanistic model presented by Solimeno et al. (2015) [27] considers
112 crucial physical, chemical and biokinetic processes for the description of microalgae
113 growth in different types of cultures, particularly in wastewaters. The main relevant
114 feature of the model, respect to any previous model for microalgae production [4, 6, 23],
115 consists in the inclusion of a carbon limitation on the growth of microalgae, as well as a
116 dynamic model for photosynthesis, photolimitation, light attenuation, and
117 photorespiration. In the model, microalgae grow with light, consume nutrients (i.e.,
118 carbon and nitrogen), and release oxygen (Fig. 2).

119 Note that other nutrients (e.g., phosphorus) and micronutrients are not
120 considered to be limiting factors because are usually highly available in wastewaters
121 (which is the type of culture mainly addresses by the model) [19]. Dependency of
122 microalgae growth on phosphorus could easily be implemented in the model by creating
123 a limiting Monod function, similar how the other nutrients (i.e., carbon and nitrogen)
124 were represented. In the model, as a result of microalgal activity in the presence of light,
125 hydroxide ions concentration and pH increase. Increases in pH displace the equilibrium
126 of the carbon species towards the formation of carbonates (which are not bioavailable
127 for growth). Note that this model assumes that carbon dioxide as well as bicarbonate are
128 bioavailable for growth. In darkness, endogenous respiration of microalgae release
129 carbon dioxide, the concentration of hydrogen ions increase and the pH decreases. With
130 decreasing pH, the carbon equilibrium shifts and carbonate turns into bicarbonate,
131 which can be used as substrate again in the presence of light [30]. A detailed description
132 of the model, including components, and processes can be found in Solimeno et al.

133 (2015) [27]. A list of the processes included in the model, the equations describing their
134 rates and the matrix of stoichiometric parameters are shown in Supplementary Tables
135 (4-5).

136 *2.3 Model domain*

137 The photobioreactor's configuration was assumed to have a 2D geometry. The
138 domain was divided into two sub-domains (D1 and D2) corresponding to the loop
139 configuration and the bubble column for the vertical system in Almeria, and to the
140 open-air tanks and the tubes for the horizontal system in Barcelona (Fig. 3). In the case
141 of the vertical system, D1 was 400 m long in the longitudinal direction and 0.09 m in
142 diameter, while in the horizontal system it was 50 m long and 0.125 m in diameter. D2
143 domains were designed allocating the volume of the bubble column (vertical system)
144 and open-air tank (horizontal system) along a surface interface area where gases were
145 transferred to the atmosphere, fixing the corresponding D1 diameter. Thus, the bubble
146 column is 3.3 m long and 0.09 m deep, while the tank is 5.76 m long and 0.125 m deep.
147 These simplifications allow to simulate of hydrodynamics within the system. Note that
148 in the present model it was necessary to divide the domain into two sub-domains due to
149 the different domain conditions. Transfer of gases to the atmosphere took place
150 exclusively in the bubble column and open-air tanks. A periodic condition was applied
151 at boundaries 1 and 2 to reproduce the continuous culture flow from domain 2 to 1
152 (degasser to loop and tank to tube).

153 *2.4 Hydrodynamics of the system, light attenuation and temperature*

154 In our previous work [27], the calibration of the model was conducted in a
155 complete mixed reactor represented by a 0D domain in order to simplify
156 hydrodynamic's complexity. In the present work, as a result of the motion of the culture
157 through the tubes and bubble column or open-air tank, a 2D domain was needed, which

158 include hydraulic and transport equations. On the other hand, in the previous work [26],
159 it was assumed that microalgae cells captured photons at all depths (light attenuation
160 was neglected due to 0D domain). The present work incorporates light attenuation due
161 to the presence of microalgae.

162 In the model microalgae processes are influenced by temperature [27]. It is
163 known that the growth rate of microalgae is highly dependent on temperature; it
164 increases when optimum temperature is reached and drastically decreases when
165 optimum temperature is exceeded [14]. In the present study, microalgae production was
166 simulated in a study case at different temperatures, showing the dependence of
167 microalgae growth on temperature.

168 Hydrodynamics of system was modelled through the COMSOL MultiphysicsTM
169 software, previously used for the calibration of the microalgae model in a completely
170 stirred experiment, which solves differential equations using the finite elements method
171 (FEM).

172 *2.4.1 Hydraulic Considerations*

173 In the PBR used in this work the culture is set in motion by an external pump
174 (vertical system) or by paddlewheels (horizontal system), and enters the model domain
175 with a certain velocity. To predict the flow regime without starting a simulation, the
176 Reynolds number was firstly calculated. The Reynolds number quantifies the ratio of
177 inertia to viscous forces, characterizing the flow regime (Eq. 2):

$$178 \quad Re = \frac{\rho * v * d}{\mu} \quad (2)$$

179 where ρ is the culture density (assumed to have the same density as water, 1000 kg m^{-3}),
180 v is the culture velocity (m s^{-1}), d is the tube diameter (0.09 m and 0.125 m for vertical
181 and horizontal systems, respectively), and μ is the dynamic viscosity of the culture
182 (assumed to be the same as water $0.003 \text{ kg m}^{-1}\text{s}^{-1}$). The Reynolds number was

183 calculated to be approximately 27,000 for the vertical system and 5,000 for the
 184 horizontal. Note that in tubes with a flow with a Reynolds number above 4,000 is
 185 already considered turbulent [29], and in these conditions transversal variations of
 186 culture properties (temperature, dissolved oxygen, biomass concentration, etc.) may be
 187 neglected and Navier-Stokes equations can be solved directly. With such high Reynolds
 188 number's temperature does not significantly influence the motion because viscous
 189 forces (μ) are very small when compared to inertial forces (ν).

190 For turbulent flow, COMSOL MultiphysicsTM solves the Navier-Stokes as well
 191 as continuity equations. Turbulent effects are modeled using “Turbulent Mixing”
 192 interfaces for “Transport of Diluted Species” physics. In “Turbulent Mixing” models
 193 the additional mixing caused by turbulence is estimated by adding turbulent diffusivity
 194 to the molecular diffusivity considering:

$$195 \quad D_T = \nu_T / Sc_T \quad (3)$$

196 where D_T is the turbulent diffusion, ν_T is the turbulent kinematic viscosity at 20 °C
 197 ($1.004E-06 \text{ m}^2 \text{ s}^{-1}$) and Sc_T is the turbulent Schmidt number (0.7).

198 *2.4.2 Transport of dissolved and particulate components*

199 Transport of diluted and particulate components with a concentration S_i [g m^{-3}]
 200 by convection and diffusion is given by:

$$201 \quad \frac{\delta S_i}{\delta t} + (-D_T \cdot S_i) + \mathbf{u} \cdot \mathbf{c}_i = r_i \quad (4)$$

$$202 \quad r_i = \sum_j v_{j,i} * \rho_j \quad (5)$$

203 where $i = 1, 2 \dots m$ are the different components considered (Table 2), and j is the
 204 number of processes shown in Supplementary Table (4); \mathbf{u} [m s^{-1}] is the vector of
 205 velocity, r_i [$\text{g m}^{-3} \text{ s}^{-1}$] is the reaction rate, ρ [$\text{g m}^{-3} \text{ s}^{-1}$] is the process rate corresponding to
 206 the biokinetic and chemical j processes described in Solimeno et al. (2015) [27] and $v_{j,i}$

207 is the stoichiometric coefficient. Mathematical expressions of the stoichiometric
208 coefficient and values of biokinetic, physical and chemical parameters are shown in
209 Supplementary Tables (6-9).

210 *2.4.3 Light attenuation*

211 In the present study light intensity decay was described using Lambert-Beer's
212 Law, which dictates that intensity decreases exponentially as it penetrates into a
213 perfectly homogeneous section of culture with a short penetration pathway [25], as it is
214 the case of both PBR. In this case light is attenuated by the presence of microalgae
215 inside the reactors. The average light intensity (I_{av} , [$\mu\text{mol m}^{-2}\text{s}^{-1}$]) at any point within the
216 culture is therefore calculated as [17]:

217

$$218 \quad I_{av} = I_0 \cdot \psi (1 - \exp(-k_i \cdot X_{ALG} \cdot d)) / k_i \cdot X_{ALG} \cdot d \quad (6)$$

219

220 where I_0 [$\mu\text{mol m}^{-2}\text{s}^{-1}$] is the incident light intensity, k_i is the extinction coefficient for
221 microalgae biomass [$0.1 \text{ m}^2 \text{ g}^{-1}$] [8], X_{ALG} is the concentration of microalgae, ψ is the
222 solar irradiance fraction available in the reactor and d [m] is the diameter of tube.

223 *2.4.4 Temperature*

224 In our model, the influence of temperature on microalgae activity was
225 implemented by the thermic photosynthetic factor ($f_{T,FS}$), which takes into account the
226 effects of temperature on microalgae growth, endogenous respiration and inactivation
227 processes (1a, 1b, 2 and 3 in Supplementary Table 4, respectively). Water temperature
228 varies both on hourly and daily scales, affecting microalgal photosynthesis and
229 respiration rates. The thermic photosynthetic factor is represented in the model
230 following the work of Dauta et al. (1990) [14]:

231
$$f_{T,FS}(T) = e^{-\left(\frac{T-T_{opt}}{s}\right)^2} \quad (7)$$

232 where T_{opt} (optimum temperature) was assumed to be 25 °C [14] and s equal to 13 [14]
233 (it is a parameter value for empirical fitting).

234 *2.5 Calibration procedure*

235 Model output results are highly sensitive to the maximum specific growth rate of
236 microalgae (μ_{ALG}), mass transfer coefficient for oxygen (K_{a,O_2}), and carbon dioxide
237 (K_{a,CO_2}). The mass transfer coefficients depend on the extension of the surface interface
238 and photobioreactor design [27]. Therefore, these parameters were calibrated in the two
239 different tubular photobioreactors. The model was first calibrated using experimental
240 data obtained from the vertical photobioreactor located in Almeria (Spain). Dissolved
241 oxygen, pH, temperature and irradiance were monitored for 24 hours on February 28th,
242 2012. Afterwards, the model was calibrated with experimental data from the horizontal
243 photobioreactor located in Barcelona (Spain). Data used for this calibration were
244 retrieved from three days batch experiment from April 16th, 2012 to April 19th, 2012.
245 Available data used for the calibration procedure are shown in Supplementary Tables
246 (1-2). The initial concentrations of components in the vertical and horizontal
247 photobioreactors at the beginning of the experiments are shown in Table 3. In the
248 horizontal PBR the concentrations of NH_4^+ and NH_3 were lower than the analytical
249 method's detection limit and therefore considered to be zero for this model. Note the
250 difference in initial concentrations of microalgae (X_{ALG}) between the two PBRs due to
251 their different operating conditions

252 *2.6 Study cases*

253 Practical study cases have been done to evaluate the influence of both
254 temperature and irradiance on microalgae production, and the effect of oxygen

255 concentration in the loop. The vertical photobioreactor of Almeria (Spain) was selected
256 as reference for these studies.

257 Starting from the initial concentrations used for calibration of the model in the
258 vertical photobioreactor, average daily microalgae production was simulated using daily
259 temperature and irradiance variations from 17th day of each month of year. Two
260 scenarios were evaluated. In the first set of simulations the vertical photobioreactor was
261 under controlled temperature by passing cooling water at 1500 L/h through an internal
262 heat exchanger located in the bubble column of the photobioreactor. In a second set of
263 simulations, temperature was obtained from meteorological annals of Almeria (Spain).
264 These two scenarios were compared and an estimation of the total annual production
265 using monthly irradiance variations was calculated. Irradiance, expressed as
266 photosynthetically active radiation (PAR), was estimated for Almeria (Spain) from the
267 mathematical equations presented in Supplementary Table 10 [2].

268 Moreover, oxygen concentration throughout the 400 m of vertical
269 photobioreactor was evaluated while maintaining the reactor under controlled
270 temperature, Dissolved oxygen profile in the loop configuration was simulated at noon
271 in the months of July and January, when the highest and lowest temperature,
272 respectively, were recorded.

273

274 **3. Results**

275 In this work simulations for two different photobioreactors were studied. First
276 we present the results of the model calibration for the vertical photobioreactor. Fig. 4
277 shows that the model was able to accurately match DO and pH trends over the course of
278 one day inside the system, with decreasing pH due to CO₂ injection (which displaces the
279 equilibrium of carbon species).

280 Fig. 5 shows the results of the calibration in the horizontal photobioreactor.
281 Experimental and simulated dissolved oxygen and pH values inside the open-air tanks
282 of the horizontal photobioreactor are presented. As can be seen, the wavelike trend of
283 pH varied due to microalgae activity, which is quite well simulated by the model.
284 Moreover, Fig. 6 shows the experimental and simulated nitrate (N_{NO_3}) and
285 bicarbonate (C_{HCO_3}) concentrations in the horizontal system. The model was able to
286 reproduce quite well the trend of experimental data. In absence of ammonia species,
287 only nitrates are used as nitrogen substrates for microalgae growth. The low
288 concentration of nitrate in the culture medium limited the activity of microalgae. As can
289 be seen, microalgae consumed nitrate concentrations quickly in the first hours of
290 experiment (Fig. 6). Likewise, Fig. 6 shows that bicarbonate concentrations decreased
291 faster in the first hours due to intense microalgae activity. After 22 hours, in absence of
292 nitrate, daily variations of bicarbonate are related to changes in equilibrium species of
293 carbon.

294 Note that, in general, simulations of the vertical PBR were more accurate than
295 those of the horizontal due to in the horizontal system there was some growth of other
296 microorganisms different from microalgae (e.g., bacteria and protozoa). This was to be
297 expected as the culture water was from an irrigation channel. The activity of these
298 microorganisms affected simulated factors though it is not known to what extent,
299 because unfortunately we do not have values for these organisms.

300 Table 4 presents the values of the parameters that were calibrated in each
301 photobioreactor. Note that maximum specific growth rate (μ_{ALG}) and the transfer of
302 gases to the atmosphere (K_{a,O_2} and K_{a,CO_2}) were also calibrated in our previous works
303 [27, 28]. In this previous work the model output results are very sensitive to these
304 parameters [27, 28], and therefore should be calibrated with great accuracy.
305 Furthermore, gas transfer parameters depend on the extension of the surface interface.

306 Due to different PBRs design, modifications of these parameters were considered
307 worthwhile.

308

309 **4. Discussion**

310 *4.1 New features of the model*

311 In comparison to our previous work [27], where a 0D domain was applied, here
312 2D domain was used to represent the two tubular photobioreactors. The domain was
313 divided in two sub-domains (D1 and D2), where different conditions from the tubes
314 (D1) to the open body (D2) of the photobioreactors were applied. According to the
315 function of bubble column in the vertical system and the open-air tank in the horizontal
316 system, the transfer of gases to the atmosphere was only applied to the D2 domain that
317 corresponds to the total volume of these specific parts.

318 A periodic condition was applied at boundaries 1 and 2 to reproduce the
319 recirculation of flow from the loop configuration to the bubble column in the vertical
320 system, and from the tubes to the open-tank in the horizontal system. Simulation results
321 demonstrated that these simplifications were adequate to describe the specific parts of
322 different tubular photobioreactors. Moreover, fluid flow and transport equations were
323 added in the current model to obtain a realistic representation of the hydrodynamics in
324 the photobioreactors.

325 In addition to the previous mechanistic model presented by Solimeno et al.
326 (2015) [27] light attenuation through the medium was implemented. Light intensity
327 decays exponentially due to microalgae biomass accumulation inside the reactors.
328 Assuming a perfect mixing of medium, due to turbulent flow regime, an irradiance
329 average I_{av} was used to represent any point within the reactor.

330 *4.2 Calibration of the model*

331 Results of the sensitivity analysis, reported in our previous work [28], had
332 indicated that the maximum specific growth rate of microalgae (μ_{ALG}) and the mass
333 transfer coefficient for oxygen ($K_{\text{a,O}_2}$) and carbon dioxide ($K_{\text{a,CO}_2}$) were the parameters
334 with the greatest impact on simulation outputs. Therefore, calibration of these
335 parameters must occur in each particular case.

336 The calibrated maximum specific growth rate of microalgae ($\mu_{\text{ALG}} = 1.7 \text{ [d}^{-1}\text{]}$) in
337 the vertical photobioreactor fits well within literature range $[0.4\text{-}2.0 \text{ d}^{-1}]$. Also, the mass
338 transfer coefficient in the bubble column for oxygen which was $K_{\text{a,O}_2} = 2.9\text{E-}03 \text{ s}^{-1}$ fits
339 into the range values for vertical photobioreactors $[1.2\text{E-}03 \text{ to } 7.7\text{E-}03 \text{ s}^{-1}]$ [18]. The
340 mass transfer coefficient for carbon dioxide ($K_{\text{a,CO}_2} = 2.8\text{E-}03 \text{ s}^{-1}$) was consistent with
341 range values $[1.1\text{E-}03\text{-}7.0\text{E-}03 \text{ s}^{-1}]$ for bubble column systems [18]. These same
342 parameters were calibrated with experimental data over three days from the horizontal
343 photobioreactor located in Barcelona (Spain). Likewise as in the previous calibration,
344 the values generated for the maximum growth rate of microalgae ($\mu_{\text{ALG}} = 1.7 \text{ [d}^{-1}\text{]}$), the
345 mass transfer of oxygen ($K_{\text{a,O}_2} = 9.2\text{E-}03 \text{ [s}^{-1}\text{]}$) and carbon dioxide ($K_{\text{a,CO}_2} = 9.0\text{E-}03 \text{ [s}^{-1}\text{]}$)
346 were all in agreement with literature ranges for tubular photobioreactors [9].

347 Mass transfer coefficients depend on, temperature, mixing and most importantly,
348 the extension of the surface interface. Thus, variable values of mass transfer coefficients
349 from vertical and horizontal photobioreactors are due to different design and scale-up of
350 bubble column and open-tanks, respectively.

351 Also the culture medium influences the mass transfer coefficients and the
352 maximum growth rate of microalgae. In this work the horizontal photobioreactor was
353 filled with agricultural runoff which could contain few concentrations of bacteria and
354 other microorganisms. The activity of these microorganisms could influence dissolved
355 oxygen and carbon dioxide concentrations in the medium culture, and therefore could
356 slightly affect the values of the calibrated parameters. However, single microscopic
357 observations during the experiment indicated that their concentration was irrelevant in

358 comparison to microalgae (as usual in this type of PBR), and thus their influence is
359 considered very low or almost negligible. Calibrating the model in two different
360 photobioreactors (e.g., horizontal and vertical) with different types of media has proved
361 the robustness and resilience of the mathematical model to operate under variables
362 conditions.

363 *4.3 Study case: microalgae production as a function of temperature and irradiance*

364 Irradiance and temperature play an important role in microalgae production.
365 These physical factors influence biokinetic and chemical processes related to
366 microalgae growth. Irradiance is strictly correlated to photosynthesis rate. At high level
367 of irradiance, microalgae become 'light saturated' because photosynthesis cannot
368 process more photons. As result, the rate of photosynthesis progressively starts to
369 stabilize [9, 13]. Temperature influences the equilibrium of chemical species (carbon
370 and nitrogen), uptake of nutrients, transfer of gases to the atmosphere, and especially the
371 microalgae growth rates. The optimal temperature for microalgae growth ranges
372 between 15°C and 25°C, depending on the species [5, 19]. Temperature above or below
373 this range negatively affects biomass yield.

374 Thanks to the model, previously calibrated with daily experimental data, has
375 been possible to make predictions of microalgae production over long-term with
376 different environmental factors, such as temperature and irradiance. Simulations of the
377 average daily microalgae production at a monthly scale in the vertical photobioreactor
378 are presented in Fig 7. As can be observed simulations indicate that production is
379 generally higher under daily temperature variations due to a more favorable temperature
380 range (Supplementary Table 3). Table 5 presents the annual microalgae production
381 comparing the two scenarios studied: under controlled temperature and with daily
382 temperature variations. Although the growth of microalgae decreases with high
383 temperature and irradiance during the months of June, July and August (when the

384 highest temperatures of the year occur), total annual production of microalgae exposed
385 to daily temperature variations is higher than the reactor under controlled temperature.
386 To optimize production, it might be considered to only use cooling water during the
387 hottest months (June, July and August). Moreover, simulations results show that during
388 the summer the production is also inhibited due to high dissolved oxygen concentrations
389 throughout loop configuration up to 250% of air saturation (see next section).

390

391 *4.4 Study case: oxygen concentration*

392 Fig. 8 shows the simulations of the dissolved oxygen profile throughout the 400
393 m length of the vertical photobioreactor at noon (when the highest temperature occurs)
394 in the months of January and July. These two months were selected as they represent
395 the minimum and maximum microalgae activity in a monthly basis time scale. As can
396 be seen, the lower light intensity and temperature in January gives as a result lower
397 dissolved oxygen concentrations in contrast to July. Also it can be observed in both
398 months how dissolved oxygen concentration increases throughout the loop and
399 decreases in the bubble column. In July, transfer of excess of dissolved oxygen to the
400 atmosphere throughout the airlift permits to re-establish, at the beginning of loop
401 configuration, the oxygen level under the maximum concentration of oxygen dissolved
402 in water ($32 \text{ gO}_2 \text{ m}^{-3}$) equal 350% of saturation ($9.07 \text{ gO}_2 \text{ m}^{-3}$) [1, 8]. This property of
403 the photobioreactor design is especially important in warm months (such as July), when
404 a high photosynthetic activity could cause inhibition due to oxygen accumulation.

405 The model presented in this work allows to simulate and study microalgae
406 growth inhibition due to high dissolved oxygen concentrations thanks to the inclusion of
407 a photorespiration factor $f_{PR}(S_{O_2})$ [27]. The function ($f_{PR}(S_{O_2})$) in Fig. 9 describes that
408 for dissolved oxygen concentrations lower than the $250\%S_{O_2}^{SAT}$ ($22.67 \text{ gO}_2 \text{ m}^{-3}$) the
409 photosynthesis rate is reduced by 10%. Above this value, the photosynthesis rate

410 decrease more quickly with a vertical asymptote and is equal at zero when dissolved
411 oxygen reaches the 350% saturation limit ($\tau S_{O_2}^{SAT} = 32 \text{ gO}_2 \text{ m}^{-3}$).

412 In process design, the current model can be used to find the maximum
413 photobioreactor length to avoid oxygen inhibition. For example, for the month of July,
414 simulations were conducted using half the previous bubble column volume (from 0.44
415 m^3 to 0.22 m^3) in the vertical photobioreactors loops (400 m and 250 m). As seen in Fig.
416 10, reducing the volume of the bubble column and keeping the original loop
417 configuration length (400 m), the simulation results show that the DO exceeds the
418 saturation limit l inhibiting microalgae growth. The volume of bubble column is not
419 enough to transfer the excess of dissolved oxygen to the atmosphere. On the contrary,
420 simulations indicate that a 250 m length, photobioreactor greatly reduces the oxygen
421 accumulation.

422

423 **5. Conclusion**

424 In this paper a new mechanistic model to simulate microalgae growth was
425 calibrated in two different tubular photobioreactors. Fluid flow, transport equations and
426 light attenuation were included in the model described in our previous work and
427 implemented in COMSOL MultiphysicsTM software. Uncertainty parameters from
428 previous sensitivity analysis were calibrated in each photobioreactor. The results of
429 calibration indicate that the mass transfer of gases and the maximum specific growth
430 rate of microalgae fit well within literature ranges. Moreover, the developed model
431 demonstrates potential prediction of oxygen accumulation throughout the loop
432 configuration and daily microalgae production as a function of temperature and
433 irradiance. The model proves to be an efficient tool for photobioreactor design and
434 production optimization.

435

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