- 1 Post-failure evolution analysis of a rainfall-triggered landslide
- 2 by Multi-Temporal Interferometry SAR approaches
- 3 integrated with geotechnical analysis
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Abstract

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- Persistent Scatterers Interferometry (PSI) represents one of the most powerful techniques for Earth's surface
- deformation processes' monitoring, especially for long-term evolution phenomena. In this work, a dataset of 34
- 35 TerraSAR-X StripMap images (October 2013-October 2014) has been processed by two PSI techniques Coherent
- 36 Pixel Technique-Temporal Sublook Coherence (CPT-TSC) and Small Baseline Subset (SBAS) in order to study the
- evolution of a slow-moving landslide which occurred on February 23, 2012 in the Papanice hamlet (Crotone
- municipality, southern Italy) and induced by a significant rainfall event (185 mm in three days). The mass movement
- caused structural damage (buildings' collapse), and destruction of utility lines (gas, water and electricity) and roads.
- The results showed analogous displacement rates (30-40 mm/yr along the Line of Sight –LOS of the satellite) with
- respect to the pre-failure phase (2008-2010) analyzed in previous works. Both approaches allowed to detect the
- 42 landslide-affected area, however the higher density of targets identified by means of CPT-TSC enabled to analyze in
- detail the slope behavior in order to design possible mitigation interventions. For this aim, a slope stability analysis has
- been carried out, considering the comparison between groundwater oscillations and time-series of displacement.
- 45 Hence, the crucial role of the interaction between rainfall and groundwater level has been inferred for the landslide
- 46 triggering. In conclusion, we showed that the integration of geotechnical and remote sensing approaches can be seen
- as a best practice to support stakeholders to design remedial works.
- 48 **Keywords:** Persistent Scatterers Interferometry; SAR; Coherent Pixels Technique-Temporal Sublook Coherence;
- 49 Small Baseline Subset; Landslide; Crotone Province; Slope stability analysis.

51 1. Introduction

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Ground failures and ground instability hazards are globally widespread phenomena caused by natural geological and climatic processes such as landslides and slope movements (Di Martire et al., 2016a), soil volumetric changes in relation to dry and wet periods, soil/rock dissolution, oscillations of groundwater levels (Chaussard et al., 2014), seismic and volcanic activity (Lagios et al., 2013), neo-tectonic uplift or subsidence (Di Martire et al., 2016b) or induced by anthropogenic sources such as ground water pumping, (Modoni et al., 2013), inappropriate water management (Valipour et al., 2015 and references therein), gas and oil withdrawal, mining activity (Ferretti et al., 2011b), subsurface and surface engineering works (Bandini et al., 2015). They determine a significant number of human losses and injury as well as extensive economic damage to private and public properties. (Schuster & Fleming, 1986). In Europe and especially in Italy, slope instabilities represent the primary cause of death caused by natural hazards (Guzzetti et al., 2012). A recent statement by the Research Institute for Geo-Hydrological Protection (IRPI) (Figure 1), affirms that in Italy landslides are "recurrent, widespread and dangerous phenomena" and in the first semester of the 2015 only, 3 victims and 9 casualties have been already reported (IRPI, 2015). The landslide risk scenario has worsened in the last 50 years, in relation with an inappropriate land management, following the "economic miracle" of the early 60s, which increased the exposure to natural hazards for Italian towns (Di Martire et al., 2012). Most of the Southern Italy landslides classified as slow to moderate kinematic (Cruden & Varnes, 1996) are rainfall-triggered: significant examples are represented by the cases of Agnone (200 mm in the 72 hours before the event) (Calcaterra et al., 2008), Maierato (200 mm in 15 days) (Gattinoni et al., 2012) San Fratello (900 mm in 4 months) (Bardi et al., 2014; Bianchini et al., 2015) and Montescaglioso (246 mm in 72 hours) (Manconi et al., 2014). These events are comparable in terms of geological and geomorphological settings as well as of poor geotechnical properties of the involved materials. The latter correspond to clay-dominant tectonized terrains, geologically and geotechnically known as Structurally Complex Formations (SCF) (Esu, 1977). The adverb "complex" refers to heterogeneity with respect to the epigenetic lithological characteristics, while "structurally" points to the effect of tectonic processes due to syngenetic folding, faulting or fracturing. Such a complexity poses major difficulties in terms of obtaining and testing representative samples to be used to formulate suitable models for slope stability in order to plan mitigation works.

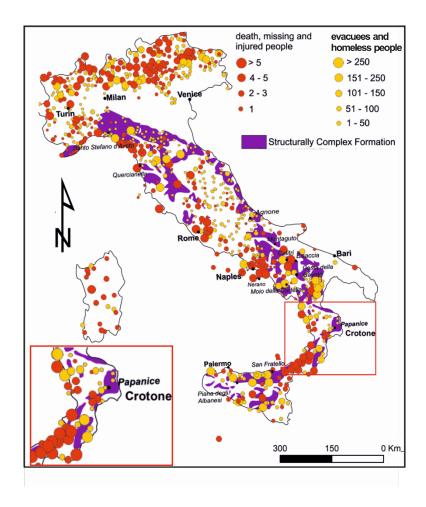


Figure 1 - Map of the landslide events with "victims" in the time span 1964-2013, with the spread of the Structurally Complex Formations (SCFs) in the whole Italian territory (modified from IRPI, 2015). In the red box, Calabria region.

Globally slope movements in SCFs and in weak soils have a long evolutionary history characterized by several reactivations of the previously deformed mass in case of prolonged or intense rainfalls, seismic events or human activities (D'Elia et al., 1998; Bozzano et al., 2004; Di Maio et al., 2010). For this reason, the monitoring phase represents a paramount task for geoscientists and for public administrations to reduce or avoid potential calamities. In the last decades, remote sensing devices provided an important support in landslide monitoring at relatively low costs (Tofani et al., 2013; Scaioni et al., 2014). Among the remote sensing techniques (GPSs, Laser scanners, LiDAR, etc.), Persistent Scatterers Interferometry (PSI, Hooper et al., 2004), which represents an advanced configuration of classical Synthetic Aperture Radar Differential Interferometry (DInSAR), is surely one of the most valuable tools which has achieved relevant improvements within the last two decades (Colesanti & Wasowski, 2006; Cascini et al., 2010; Calò et al., 2012; Herrera et al., 2013; Novellino et al., 2015; Bonì et al., 2016), in particular thanks to Very High Resolution images (VHR) (StripMap, up to 3 m resolution; SpotLight, up to 1 m resolution) and short revisit time of the latest space-born constellations (6-11 days - TerraSAR-X, COSMO-SkyMed and SENTINEL-1A and 1B).

Many PSI techniques have been developed in the last 15 years (e.g., Permanent Scatterer - PS (Ferretti et al., 2001), Small Baseline Subset Approach - SBAS (Berardino et al., 2002), SqueeSAR (Ferretti et al., 2011) and Coherence Pixel Technique - CPT (Mora et al., 2003; Blanco-Sanchez et al., 2008; Iglesias et al., 2014a), allowing to capitalize large SAR datasets and hence to investigate long-term events with the generation of precise time series of ground-displacements. In this work, two PSI techniques have been applied: SBAS, implemented on the SARscape software (www.sarmap.ch), and CPT, developed on the SUBSOFT processor (Mora et al., 2003). Such approaches have been selected and applied to Papanice, a hamlet in Crotone suburb (Southern Italy), in order to analyze the post-failure evolution of the landslide occurred in February 2012, and to integrate the previous analysis concerning the pre-failure phase (Confuorto et al., 2015). The pre-failure analysis (2008-2010) showed how both PSI approaches were able to identify displacement rates up to 30 mm/yr along the Line of Sight (LOS) direction. For this work, the dataset consists of 34 TerraSAR-X images, acquired over ascending pass (October 2013 - October 2014). The novelty of this work is represented by the detailed analysis of a landslide for different stages of its state of activity, because of the high spatial and temporal resolutions of the multiple monitoring techniques available. The integration of different monitoring systems can assume a key role in planning of remedial works, in order to assure the stability of urban settings. This has allowed to evaluate the hydrologic mechanism that control the landslide dynamic and, ultimately, the landscape evolution and hazard assessment within the study area, a finding that in previous earthflows studies (Bardi et al., 2014; Raspini et al., 2015), especially for southern Apennines, is usually associated with considerable uncertainty. Moreover, the application of PSI techniques has been for the first time tested for landslide studies in Crotone province, after Confuorto et al., (2014, 2015).

The paper is organized as follows: first, the Papanice test site is described and a brief depiction of the rainfall event which triggered the landslide is reported. The Papanice landslide is successively described according to field and monitoring survey. Further, an overview of basic concepts of PSI technique is given also showing the deformation rates obtained by combining CPT and SBAS processing. At the end, SAR results are integrated with geotechnical analyses, such as the slope stability test, showing the important role of rainfall and of groundwater level as well for the trigger of landslides in such contexts.

2. Geological and Geomorphological Setting

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Papanice is a small settlement of ca. 3500 people, 11 km east from Crotone city center, on the top of the NW-SE trending Marchesato hill (Figure 2a). Papanice is included in the Crotone Basin, a large sedimentary basin, whose opening began between the Middle and the Upper Miocene (Serravallian and Tortonian) (Roda, 1964; Van Dijk, 1990). The Crotone Basin is bounded by two main shear-zones: the Rossano-San Nicola shear zone in the northern sector, and

the Petilia-Sosti one in the southern part (Meulenkamp et al., 1986; Van Dijk & Okkes, 1990, 1991; Van Dijk, 1991) (Figure 2a). In detail, the Papanice bedrock belongs to the most recent part of the Crotone Basin, where the Cutro marly-clayey formation crops out. Locally such formation can reach a thickness of few hundred meters and it is essentially made of marly and silty clay strata (Massari et al., 2002; Zecchin et al., 2012). The so-called S. Anna Synthem, in form of marine terraces, overlies the Cutro marly-clayey formation and represents the unit where the Papanice settlement arises. The synthem is composed of sands and conglomerates, at time intercalated with bioclastic limestones (Figure 2b). No evidence of tectonic deformations have been recognized in the study area, where the weak resistance to the erosion and the low permeability of the Cutro marly-clayey formation and Sant'Anna Synthem, make the Papanice succession very prone to instability phenomena. The area of the 2012 Papanice landslides, the Pironte district, is, from a geomorphological point of view, a N-S oriented peninsula, whose upper surface is characterized by a flat area or locally with weak gradient, while the surrounding slopes present a higher inclination. This kind of setting is very prone to generate gravitational phenomena, especially during strong precipitation events as well as seasonal streams. When the instabilities have a retrogressive evolution (WP/WLI, 1993) they involve the buildings located at the edge of the Pironte area. As shown in the Landslide Inventory Map of the Hydro-Geomorphological Setting Plan (HSP) (Calabria Regional Basin Authority, 2006), the whole settlement is surrounded by landslides (Figure 3): most of them can be classified as areas affected by deep slow deformation, but slide and complex phenomena also occur (Cruden & Varnes, 1996). In the detail, the Pironte neighborhood is affected by two different dormant landslides, on the slope facing east: an area affected by deep slow deformation and a rotational slide. The geomorphological setting of the area has been severely modified by the intense growth of Papanice, started in the early 60s; indeed, 50 years ago the Pironte area was almost uninhabited (Figure 2c). Only 30% of the whole urban area is dated before 1955, while the major development started in 1956, and still in recent years (from 1983 onward) an evolution can be recorded, especially in the NW sector, where the Pironte neighborhood is located, and in the SW sector of the settlement. This urban growth also altered the risk scenario, exposing more areas to landslide hazard. In addition, the use of landfill materials to reshape terrains by flattening areas has worsened the local geotechnical setting.

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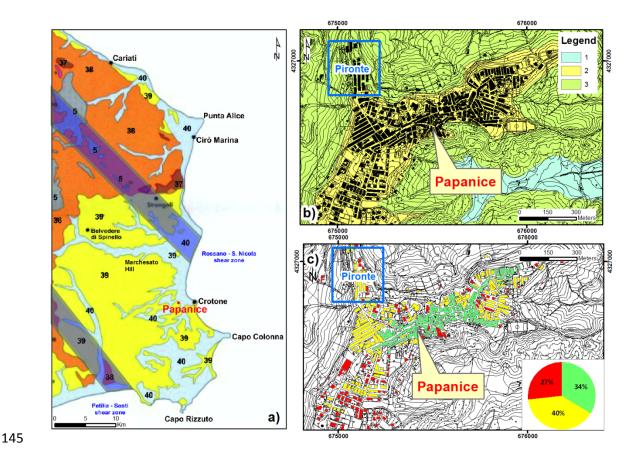


Figure 2 - a) Geological sketch map of Crotone province: 5 – Meta-limestones, phyllites (Devonian age); 6 – Granites (Permian-Carboniferous age); 37 - Varicolored clays (Tortonian age); 38 - Clays and marls, evaporitic deposits (Lower Pliocene-Tortonian age); 39 – Calcarenites, sands, clays and conglomerates (Lower Pleistocene – Middle Pleistocene age); 40 – Alluvial deposits (Holocene – Upper Pleistocene). In blue bands, the two shear zones. Modified from Bonardi et al., 1976; b) Geological sketch map of Papanice area: 1 - Recent Alluvial Deposits (Holocene), 2 - Sant'Anna Synthem (Ionian), 3 - Cutro marly-clayey Formation (Piacentian – Calabrian) (SCF formation). In blue square, Pironte district; c) Urban evolution of Papanice settlement during 1953-2014: green = urban area before 1955, yellow= 1956-1982 expansion, red= 1983-2014 expansion (modified from ARPACAL, 2013). In blue square, Pironte district.

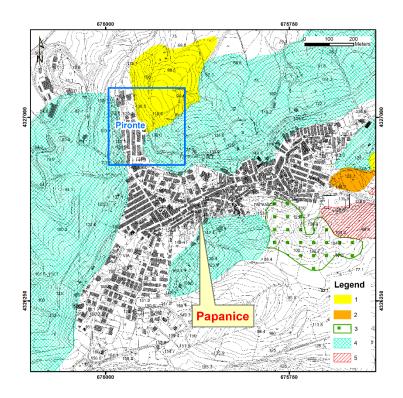


Figure 3 - Landslide inventory map of Papanice, modified from Calabria Regional Basin Authority, 2006. 1) Slide; 2)
Complex landslide; 3) Area affected by shallow slow deformation/movements; 4) Area affected by deep slow deformation/movements; 5) Area affected by deep erosion. The blue square marks the area interested by the 2012

3. Rainfall analysis

landslides (Pironte district).

Precipitations play an important role in global energy, therefore their accurate knowledge assumes a major significance for land use management, agriculture hydrology and for landslide and flooding risk reduction (Schneider et al., 2011; Valipour, 2016) Between February 21 and February 23, 2012, an intense and prolonged rainfall event occurred in Calabria Region, with the most significant precipitations being registered on February 22. Starting from February 21, an intense cloudiness generated a high instability on the Ionian coastline of Calabria with frequent showers and thunderstorms. The precipitations became stronger, as shown by the daily value of 126.8 mm registered in the rain gauge of Santa Cristina d'Aspromonte at midnight February 21. On February 22, the precipitations on the Ionian sector of Calabria intensified: they first hit the SE Ionian Coast and then the Crotone area. On February 23, the phenomenon became less concentrated, characterized by a reduction of the rainfalls on the Ionian area, with still diffuse but less intense rain. The availability of a capillary network (252 rain gauges), set up by the Multi-hazard Functional Center of the Calabrian Regional Agency for the Environmental Protection (ARPACAL) covering the whole regional territory

(Figure 4), allowed to rebuild the spatial distribution of precipitations during these 3 days. In many areas along the Ionian coast and in the inner part of the region, the daily precipitations exceeded 200 mm. In the Papanice area, rainfall data have been collected from the Crotone – Papanice rain gauge (Figure 5a), located at a distance of 200 m from the landslide area, and plotted as cumulated rainfall for the year 2012 (640 mm; Figure 5b), February 2012 (280 mm; Figure 5c) and the 19-25 February weekly rainfalls (185 mm; Figures 5d). It is worth pointing out that the analysis of the precipitation occurring in the previous 15 years shows an increase in the three years preceding the main landslide event (2009-2011), recording in this case an annual average of 1001.7 mm (1,092.2 mm for 2009, 1,025.9 for 2010 and 887.0 for 2011), while the average annual value of Papanice, recorded between 1998 and 2009, is of about 652 mm (Table 1), from a minimum of 375.0 mm in 2001 to a maximum of 862.8 in 2004. In this case, an increase of 35% has been reported in the three years preceding the 2012 landslide event, pointing out the role of precipitations for ground failure. However, such finding cannot be attributed to a general precipitation increase tendency. As reported in Brunetti et al. (2004), a negative trend in number of wet days is shown all over Italy, while a positive trend in precipitation intensity can be noted. Therefore, the increase of rainfall amount in the years preceding landslide event can be connected to more high intensity precipitation events

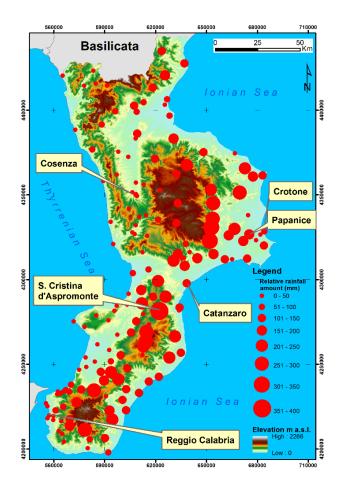
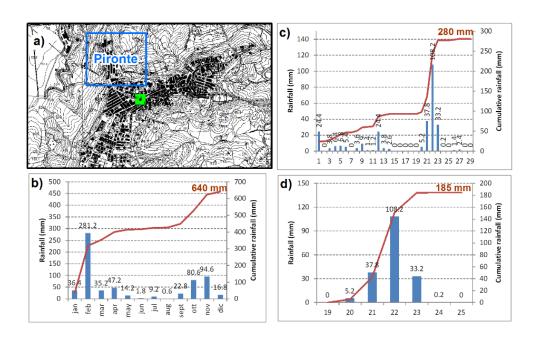


Table 1 - Annual rainfall (mm) from 1998 to 2012 recorded at Papanice rain gauge.

Year	Rainfall (mm)
1998	419.6
1999	495.6
2000	505.4
2001	375.0
2002	740.2
2003	640.4
2004	862.8
2005	585.2
2006	558.6
2007	410.8
2008	536.9
2009	1,092.2
2010	1,025.9
2011	887.0
2012	640.0

To this regard, the February 2012 precipitations are equal to 45% (280 mm out of 640 mm) of the annual rainfall occurred and the pre-event rainfall (21-23rd of February) corresponds to 28% of the 2012 annual amount (180 mm out of 640 mm), hence representing the triggering factors for the reactivation of the landslide. Taking into account the work of Vennari et al. (2014), which deals with the rainfall thresholds for shallow landslide occurrence in Calabria, the pre-event rainfall has been plotted on the duration versus the cumulated rainfall graph (Figure 6). The Papanice case conditions perfectly match the circumstances resulting in shallow landslides in Calabria.



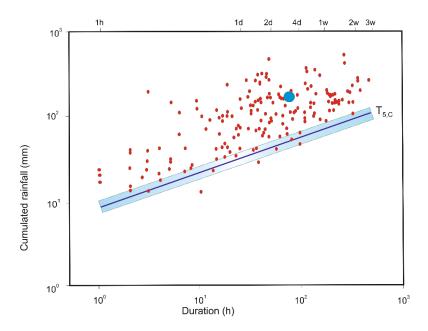


Figure 6 - Rainfall duration vs. cumulated event rainfall, conditions which resulted in shallow landslides in Calabria (red dots), and related threshold with a 95% confidence level. Shaded areas show uncertainties associated with the threshold. Blue dot = Papanice landslide. Modified from Vennari et al., 2014.

4. The Papanice landslide

4.1 Geomorphological field survey

In order to investigate the long-term evolution of the past ground movements (Confuorto et al., 2015), further geological and geomorphological survey have been carried out allowing to redefine the landslide boundaries. The analysis started from the chronicle reports and the HSP Landslide Inventory Map redacted by the Calabria Regional Basin Authority (see Figure 3). The landslides (about 10 hectares large) occurring in the Pironte area can be considered as reactivations of pre-existing dormant landslides. Such reactivations took place on February 23, 2012, and their boundaries have been redefined according to the 2013 Fall and 2014 Summer field activities, whereas for the nearby landslides several evidences of the retrogressive trend movements have been shown (Figure 7). A general instability in the sector and along other slopes surrounding the settlement was already reported in the two years preceding the main event, according to ARPACAL (2013). The movement strongly damaged man-made structures located in the urban

area: fractures and tilting of the prominent houses have been documented as well as fractures in the road surface; moreover, the chronicles reported the evacuation of five houses. The displacement involved landfills due to human activities and the most superficial part of the Sant'Anna Synthem, made of strongly weathered silty clays. Within the SW landslide, the clearest evidence of the reactivation is represented by a ca. 140 m long fracture along Via Piave, a road located next to the crown area (Figure 8a). Longitudinally, a similar strong evidence is visible down to a dirt road just below the last row of houses; in addition, superficial signs have been recognized along the whole slope. When compared to the northern part of the landslide, where the displacement seems less intense, the SW landslide proves to be more affected by severe damage, as shown by gas and electric networks involvement, as well as fence and road signs sloped downwards.

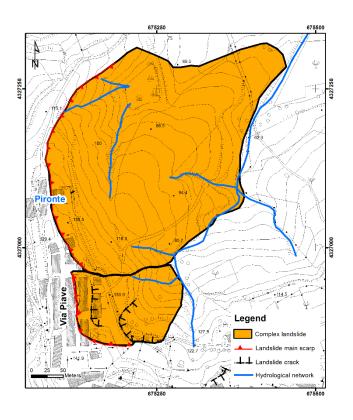


Figure 7. Field survey landslide inventory map of the Pironte district

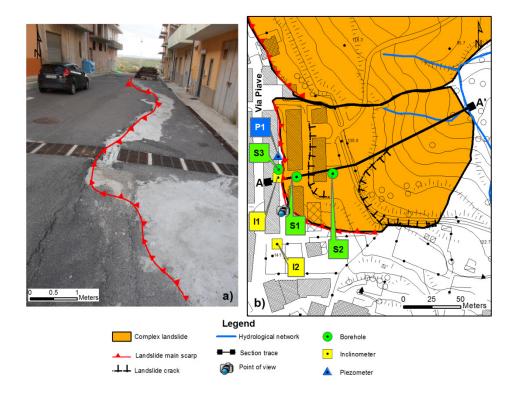


Figure 8. a) Landslide main scarp (Modified from Confuorto et al., 2015); b) Detail of the SW landslide and monitoring system installed after the 2012 main reactivation.

4.2 Monitoring campaign

In order to investigate the SW landslide's evolution and to protect the buildings located outside the landslide area, ARPACAL set up a monitoring campaign immediately after the triggering phase occurred on February 23, 2012. It consisted of 6 boreholes (see Figure 8b) located along the crest of the landslide, which allowed to reconstruct a geological and geotechnical profile of the landslide (Figure 9). Different lithological units have been defined, whose main parameters are here reported:

- Lithotechnic unit 0: Chaotic material of the units 1, 2, 3;
- Lithotechnic unit 1: Mostly sandy and silty landfill; average geo-mechanical parameters: γ=17-17.5 kN/m³,
 c=0.00 kPa, φ=27-30°;
- Lithotechnic unit 2: Alternation of silty-clayey sands, clayey-sandy silts and sandy-clayey silts, avano-coloured
 (S. Anna synthem); average geo-mechanical parameters: γ=19.8-20 kN/m³, c_u=0.00- 83.36 kPa, c= 3.92- 13.72 kPa,
 φ=26-30°;

- Lithotechnic unit 3: Silty-clayey cover with locally grey bands (weathered soil of the Cutro marly-clayey formation); average geo-mechanical parameters: γ =19.8-20 kN/m³, c_u = 66.68-88.26 kPa, c= 12.75 - 18.63 kPa, ϕ =22-25°;

- Lithotechnic unit 4: Marly-silty clayey sedimentary substrate, grey-blue-coloured (Cutro marly-clayey formation); average geo-mechanical parameters: γ =20-20.2 kN/m³, c_u = 107.87-176.52 kPa, c= 17.65-27.46 kPa, ϕ =26-27°;

where γ is the volume unit weight, c_u the undrained cohesion, c the cohesion and ϕ the friction angle. The boreholes have been eventually equipped with two inclinometer chains and one piezometer. The inclinometer data have been acquired every fourteen day, during the time period October 2013 – October 2014.

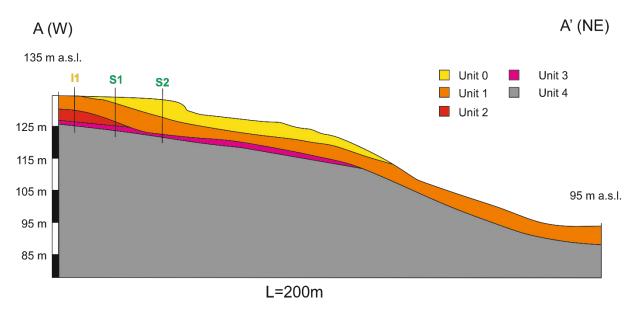


Figure 9 - Geolithological section A-A'. The location of the section is shown in Figure 7. Keys to the Units are given in the text. I1 is the inclinometer, S1 and S2 are the two boreholes along the section.

Inclinometers show a maximum displacement at the shallowest level (-8 m for I1 and -11 m for I2) of about 2 mm in the above-mentioned timespan, thus demonstrating that the area behind the landslide is not yet affected by considerable deformations (Figure 10a). Piezometer P1 (Figure 10b) is also located in proximity of the landslide and the available data are referred to daily measurements from January 1, 2013 to April 15, 2015. The comparison between piezometric readings and rainfall data, for the same time span, shows a good agreement: during dry and rainy periods, a decrease and increase, respectively, of the water table level can be noticed. It is worth pointing out that after mid-November 2013 a sudden uplift of the piezometric level of about 1.2 m has been registered, reaching a very shallow depth (-0.2 m from ground surface) due to the leaking of urban sewage pipes, as reported by a first survey of ARPACAL (2013). After the

resolution of such event, the groundwater kept persistent at a very shallow level (between -0.2 and -0.4 m), because of the high precipitations (up to 115 mm on December 1, 2013). During springtime, rain occurrences explain little oscillations of groundwater level, which started to decrease as soon as the dry season begun (e.g. cumulative rainfall of 51 mm during June and July 2014). In the final part of the analyzed time span, the piezometric levels showed large fluctuations, between 0.4 and 1.1 m, displaying again a correspondence with rainfalls (varying between several rainless days up to daily values of 55 mm).

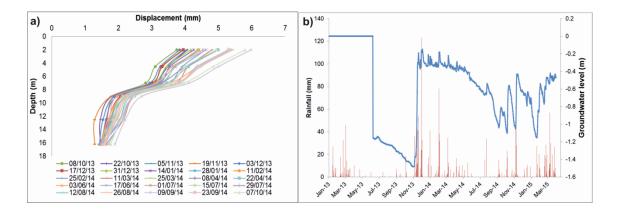


Figure 10 - a) Measurements of the inclinometer I1; b) Comparison between piezometric data from piezometer P1 (blue line) and daily rainfall at Papanice rain gauge (red).

5. PSI overview

5.1 Basic principles

Differential Interferometry SAR (DInSAR) (Gabriel et al., 1989; Massonet & Rabaute, 1993; Bamler & Hartl, 1998; Wegmuller et al., 1998; Franceschetti & Lanari, 1999) is a very effective technique for the measurement of slow ground displacements, of structures and infrastructures, due to several phenomena, like subsidence, landslides, earthquakes and volcanic eruption. It enables to detect ground displacements with independence of the atmospheric conditions reaching a precision up to mm-accuracy. These techniques are based on the exploitation of the phase difference (interferograms) between two SAR images acquired at different times. Differential interferograms can be regarded as the sum of several terms (Hanssen, 2001) and DInSAR techniques are able to isolate, among such terms, the displacement contribution. Furthermore, PSI algorithms provide long temporal series of ground displacement by analyzing long stacks of differential interferograms in order to minimize the negative impact of decorrelation and atmospheric phase screen (APS). In this context, not every pixel of the illuminated scenario can be included in the processing since only those targets with a certain phase quality along the whole set of images or interferograms can be

selected as reliable, i.e, the so-called persistent scatterers. Regarding such selection, different approaches have been performed in this work. The different PSI solutions allow to work at different resolutions and with different nature of scatterers, being the coherence stability or the Amplitude Dispersion (DA), the most common pixels' phase quality estimators. In the first case, the interferometric quality of each pixel, for each multi-looked interferogram, is obtained from the estimated coherences, which are directly related with the standard deviation of the interferometric phase (Lanari et al., 2004). In the second case, the phase stability of targets along the data set is estimated from their DA, in those pixels presenting high signal-to-noise ratio (SNR) values (Ferretti et al., 2000). The coherence stability pixel selection criterion is more suited for the analysis of natural environments with distributed scatterers and performs well even when a reduced number of SAR images is available, while the DA pixel selection criterion, which works at pixel level, is ideal for the identification of point-wise scatterers, such as man-made structures in urban scenarios, however it requires a large number of images to reach a reliable selection. The former approach, which works with distributed scatterers, requires the selection of differential interferograms limiting the maximum value of temporal and spatial baselines in order to reduce decorrelation phenomena. For this reason this method is typically addressed as SBAS. The latter approach, which exploits the nature of point-like scatterers are theoretically not affected by speckle noise and can work with all possible combinations and it is typically referred to as PS. In order to select point-wise scatterers without relying on the amplitude of SAR images, another estimators, such as the Temporal Sublook Coherence (TSC) (Iglesias et al., 2014b) used in this paper, has been recently introduced. This method allows exploiting the spectral properties of point-like scatterers and, therefore, working at high-resolution in scenarios with high dynamics in the temporal evolution of amplitude and/or when a reduced number of images are available (Iglesias et al., 2015). Once a selection of persistent scatterers candidates (PSCs) is obtained, different PSI configurations are available (Ferretti et al., 2001; Berardino et al., 2002; Arnaud et al., 2003; Mora et al., 2003; Werner et al., 2003; Lanari et al., 2004; Duro et al., 2005, Costantini et al., 2008; Hooper, 2008; Prati et al., 2010; Ferretti et al., 2011b and Sowter et al., 2013). The objective of such approaches is the precise estimation of the linear displacement, but also the separation of APS and non-linear displacement contribution to obtain precise time-series of displacement over the PSCs previously selected. Most of these approaches are composed by a first step devoted to estimate the linear contribution of the differential phase, i.e, the linear component of ground displacement and residual topographic error remaining in the differential interferograms due to the lack of precision in the DEM employed during their generation. Such step is especially important in mountainous environments, where the topographic error contribution can be significant and can affect the final results if it is not estimated and compensated for. This linear phase contribution is hence employed to ease the phase unwrapping (PhU) processing and finally a filtering process is carried out in order to separate the APS contribution from the nonlinear displacement contribution, taking advantage of the particular temporal and spatial frequency behavior of these

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two components. In mountainous areas, where landslides typically occur, the separation of APS and non-linear displacement contribution require further analysis. This issue is analyzed in detail in the following Section.

5.2 APS compensation at X-band over areas with steep topography

The mitigation of the negative impact of atmospheric phase screen (APS) results of crucial importance to ensure the reliability of PSI products. The contributions of atmospheric artifacts at X-band in areas with steep-topography, where landslide typically occur, is significant and deserve more explanation. The approach followed in this paper is put forward. These phase anomalies are caused by refractivity gradients in the troposphere (lower part of the atmosphere: from sea level to about 10-11 Km altitude), mainly produced by inhomogeneity in the temperature, pressure and water vapor content, and by dispersive effects in the ionosphere (upper part of the atmosphere: from about 85 km to 600 km), mainly produced by variations of Total Electron Content (TEC). Dealing with ionospheric effects, which contribution is significant for low-frequency SAR sensors (such as the L-band ALOS-PALSAR sensor) is beyond the scope of this paper, which is focused on the exploitation of high-resolution X-band sensors for landslide monitoring applications. Leaving aside the ionospheric contribution, it is common to separate APS into one component related to turbulent mixing processes and other to tropospheric stratification:

- Turbulent mixing comes from mixing processes in the inhomogeneous atmosphere, i.e, at the lower part of the troposphere (up to 2-3 km above ground). This APS contribution is directly related with the day-to-day weather, such as wind, rain, snow, fog, etc., and produces significant changes in the signal path delay. The negative impact of this component is mitigated exploiting the spectral differences between the displacement component and APS through the use of spatio-temporal filters (Ferretti et al., 2000; Hanssen, 2001). Going into more detail, turbulent atmosphere may be defined as a stochastic process with a low spatial frequency behavior (geo-statistically characterized by a specific varioagram with1 km correlation window (Hanssen, 2001) and completely random along the temporal axis). Regarding the spatial behavior, this means that the shorter the distance between two points affected by turbulent atmosphere, the more similar their phase values will be. Regarding the temporal behavior, for a given pixel (belonging to an image, not to an interferogram), APS can be considered as a white process since atmospheric conditions change randomly for each acquisition date. Contrarily, non-linear displacement contribution is considered to present a narrower spatial correlation window compared with APS and to behave smooth along the temporal axis.
- Tropospheric stratification results from temporal variations in the vertical refractive index profile. In other words, the vertical stratification of the troposphere in different layers (with different propagation velocities due to the

different refraction index at different elevations) leads to an additional phase delay, superimposed to the phase component of displacement.

The approach followed in this work is based on adapting spatio-temporal filters, typically used to compensate turbulent mixing, applying at this time an extra reduction of the spatial low-pass filter kernel in order to face the possible rapid fringes related with tropospheric stratification at X-band. As seen, turbulent processes are typically characterized by having a low spatial frequency behavior, typically 1 km correlation window (Hanssen, 2001). In order to compensate tropospheric stratification at X-band, the kernel size of low-pass filtering should be reduced to 100-200 meters.

The final results, both linear term of deformations and the time series, are affected by the uncompensated DEM errors and atmospheric artefacts. The impact of the errors is not easy to evaluate as it depends on many different factors: the topography, the distribution of temporal and spatial baselines, the atmospheric artefacts, etc. and it is beyond the scope of the paper. The PhD thesis of Centolanza (Centolanza, 2015) covers in detail how the errors propagate from the data to the final results.

5.3 SAR data

The PSI analysis of the Papanice landslide has been carried out using StripMap TerraSAR-X images, covering two different time spans, April 2008-June2010 for the pre-failure phase and October 2013-October 2014, for the post-failure phase. Both stacks have been obtained thanks to the participation in DLR GEO1589 and GEO2641 proposals, aiming at the exploitation of satellite interferometric data for landslide studies. In particular, the first stack consisted of 66 and 67 SLC images acquired between April 2008 and June 2010 in StripMap mode (3 m × 3 m ground resolution), along ascending and descending pass, respectively, with mean incident angle of 30°, HH polarization and repeat cycle of 11 days. The second one encompasses 34 ascending and 39 descending SLCs, with a mean incident angle of 30°, HH polarization and 11 days repeat cycle. Finally, a Digital Terrain Model (DTM) with 5 m × 5 m resolution cell has been used during the PSI processing in order to remove the topographical phase contribution and to georeference the results.

6. PSI results

6.1 Pre-processing analysis

PSI methods have shown great potential for landslides monitoring and detection (Wasowski & Bovenga, 2014). However, the application of PSI techniques is still characterized by some limitations, especially in the estimation and the detection of the measurement points (Colesanti et al., 2006). The mapping and monitoring of ground displacements

often show certain restrictions, even with VHR images, depending not only on the sensor's characteristics, but also on the geometrical and geomorphological features of the area of interest. Three geometric distortions, due to the combination of geometry of the acquisition and of the slope of interest, notoriously characterize the SAR imagery: foreshortening, layover and shadowing (Kropatsch & Strobl, 1990). In the scientific community, new pre-processing tools have been developed in order to assess the detection and the quality of the targets. Several procedures have been established in the last six years (Notti et al., 2010, 2014; Plank et al., 2013).

The R-Index equation is a model which is able to calculate the target quality of an area by taking into account the radar geometry, the slope angle and dip orientation (Notti et al., 2010, 2014). The R-Index equation is the ratio between the slant range and the ground range, starting from the geometry of the sensor and the geometry of the surface of analysis. Dip slip and the aspect of the slope, both derivable from a DTM, belong to this last category. The most suitable geometry which allows to have pixels best quality occurs when the slope is parallel to the Line-of-Sight (LOS), corresponding hence to the maximum value of the R-Index, equal to 1; on the contrary, the lowest value of the R-Index comes about in occurrence of foreshortening (0 < R-Index < 0.4) or layovering (R-Index < 0). R-index was used to select the best-suited imaging geometry for Papanice area landslide monitoring. It has been applied to both TerraSAR-X stacks, showing the following results: the landslide's slope, on the ascending orbit, corresponds to pixels with very good quality (≥0.4 on average) (Figure 11a). On the contrary, the descending orbit is characterized by poor quality of the pixels (<0.4 on average), so that this stack cannot be considered suitable for PSI procedures.

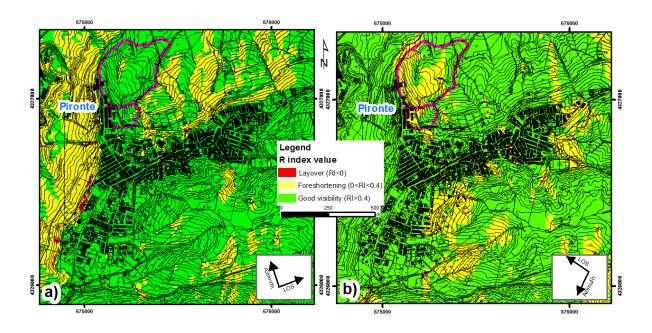


Figure 11 – R-Index computation for ascending (a) and descending (b) orbits. Red colors show the layover areas (R-Index < 0), yellow areas show foreshortening (0 < R-Index < 0.4), green areas mark a good visibility (R-Index \geq 0.4). Landslides are reported in purple line.

6.2 Pre-failure stage analysis

The analysis of the pre-event ground deformation has been successfully carried out using two different software packages with the same pixel selection criteria (PS-like), as reported in Confuorto et al. (2015), in order to investigate and monitor the precursor stages of the landslide involving the Pironte neighborhood in Papanice; the two software are SUBSOFT and SARscapeTM.

The SUBSOFT processor has been developed by the Remote Sensing Lab of the Universitat Politecnica de Catalunya of Barcelona, Spain, using the Coherent Pixel Technique (CPT, Mora et al., 2003; Blanco-Sanchez et al., 2008). For the Papanice landslide, a new implementation, the Temporal Sublook Coherence (TSC) (Iglesias et al., 2015), has been exploited. The latter allows to select point-like scatterers analyzing the spectral properties of the scattered signal. The advantage with respect to the conventional PS selection, based on the amplitude dispersion, is that there is no need of applying a radiometric calibration. Hence, in this case, the pixel selection is carried out exploiting the spectral properties of point-like scatterers. Further description of the technique can be found in Iglesias et al. (2015).

The SUBSOFT results are reported in Figure 12, where points referable to the landslides are more than one hundred, and shown in red. The average velocity (where positive values mean movements toward the satellite, while negative values refer to movements away from it) obtained with the CPT-TSC analysis is of -27.7 mm/yr, while the maximum rates, located in the NW sector of Via Piave landslide, are of -36.0 and -35.6 mm/yr. Other high velocities can be found along the main scarp. The lowest values of movement are located in the southern sector and downslope, with a minimum rate of -14.8 mm/yr. In order to evaluate the reliability of the processing and the expected error, displacement standard deviation of the stable points (behind the landslide affected area) has been calculated, resulting equal to 1.5 mm. Figure 13 shows time-series of displacement for a stable point (S-TSC) and for a point within landslide affected area (TSC1).

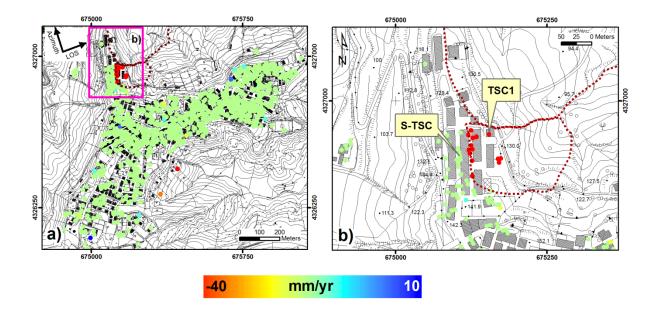


Figure 12 - a) Displacement rate map obtained with the CPT-TSC algorithm for the time interval 2008-2010. In the purple rectangle, a zoom-in of the area of interest (b). Landslides have been reported in brown-dashed line. The points S-TSC and TSC1 have been selected for the time series analysis (Figure 13). Modified from Confuorto et al. (2015).

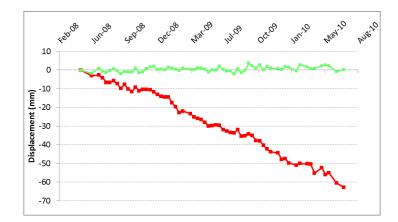


Figure 13 – Time series of displacement of the points S-TSC (green) and TSC1 (red). Modified from Confuorto et al. (2015).

In order to obtain SARscapeTM results, a procedure to improve the PS processing had to be carried out, splitting the stack into two periods (1st period, April 2008 – August 2009; 2nd period, April 2009 and June 2010) and imposing a spatial baseline threshold of ±100 m, as done in Confuorto et al. (2015). The experiments showed that a splitting of the data set into two overlapping stacks strongly increased the number of persistent scatterers compared to a scenario where it has been processed the entire data set in a single step. By analyzing a shorter time period the number of points which are characterized by a high coherence is higher than the number of points showing a high coherence over the entire period analyzed. The two sub-periods overlap each other to guarantee a meaning-full analysis of the measured

displacements. In the first period, 7 PSs have been identified in the landslide area (Figure 14). The exact location, inside the landslide perimeter, is in the NW sector and in the middle part of it, and the average velocity is of -25 mm/yr along the LOS. The highest displacement rates are all located in the NW sector of the landslide, reaching a top value of -32.1 mm/yr. The second period of analysis is based on 27 images, and in this case, 1543 PSs have been recognized. However, just one is ascribable to the movement, and also in this case it is situated in the NW part, along the main scarp, showing a displacement rate of -32.1 mm/yr. Both results showed the potentiality of DInSAR to detect precursor stages of a future slope failure. Also in this case, in order to evaluate the reliability of the processing and the expected error, displacement standard deviation of the stable points (behind the landslide affected area) has been calculated, resulting equal to 1.2 mm. Figure 15 shows time-series of displacement for a stable point (S-PS) and for a point within landslide affected area (PS1).

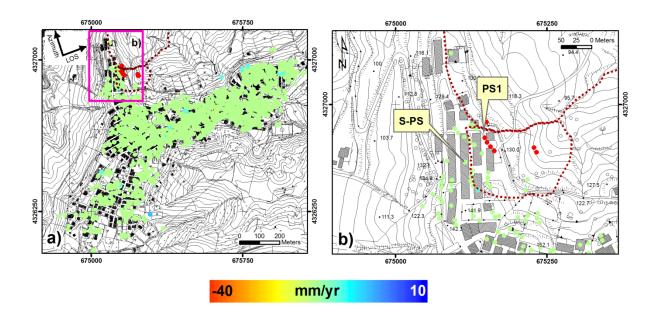


Figure 14 - a) Displacement rate map obtained with the PS (1st period of analysis) algorithm for the time interval 2008-2009. In the purple rectangle, a zoom-in of the area of interest (b). Landslides have been reported in brown-dashed line. The points S-PS and PS1 have been selected for the time series analysis (Figure 15). Modified from Confuorto et al. (2015).



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Figure 15 - Time series of displacement of the points S-PS (green) and PS1 (red). Modified from Confuorto et al. (2015).

6.3 Post-failure stage analysis

The post-failure stage analysis was limited to the TerraSAR-X ascending stack, because of the inadequate R-Index values (Figure 11), as for the previous dataset (2008-2010). The elaboration of the TerraSAR-X imagery has been carried out by means of SUBSOFT and SARscapeTM software. The former aim was to analyze the displacement on a larger scale with the application of the SBAS algorithm, which is more suitable for analysis at a less detailed scale and on regional context. The SARScapeTM software has then been tested with SBAS technique for the assessment of the post-failure phase. In this case, according to the standard procedure, two values of temporal and spatial baseline have been selected, 100 days and the 2.5% of the critical spatial baseline (ca. 5000 m) respectively, which allowed to select 143 interferograms for the final estimation. More than 4000 points have been then recognized (Figure 16), showing two different concentrations of points involved in the displacement: on the NW sector, 12 points can be referred to the landslide movement, and are located within the border and along the scarp of the main landslide documented during field activities, with an average velocity of -4.5 mm/yr. Moreover, another cluster located in the SE part, with average displacement rate of -4.8 mm/yr and maximum value of -8.3 mm/yr, has been identified. All values are referred to the LOS. As previously made, in order to evaluate the reliability of the processing and the expected error, displacement standard deviation of the stable points (behind the landslide affected area) has been calculated, resulting equal to 1.0 mm. Figure 17 shows time-series of displacement for a stable point (S-SBAS) and for a point within landslide affected area (SBAS1).

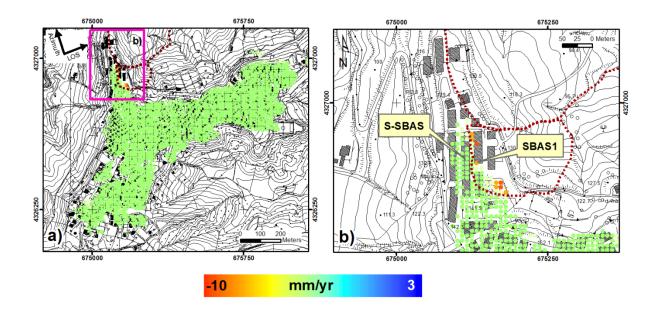


Figure 16 - a) Displacement rate map obtained with the SBAS method for the time interval 2013–2014. In the purple rectangle, a zoom-in of the area of interest (b). Landslides have been reported in brown-dashed line. The points S-SBAS and SBAS1 have been selected for the time series analysis (Figure 17).

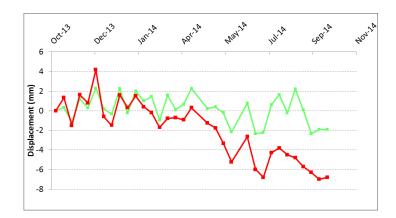


Figure 17- Time series of displacement of the points S-SBAS (green) and SBAS1 (red).

CPT-TSC has then been used on a final selection of 34 images, with a temporal interval of exactly one year (October 2013 – October 2014) in order to verify the above-mentioned results reliability, i.e. to understand whether the movement has truly slowed down in the post-failure phase, or if the SBAS tend to underestimate velocities. For the final pixel selection, a TSC threshold 0.7 has been set, selecting more than 14000 targets (Figure 18), characterized by a phase standard deviation of about 20° which corresponds to a displacement standard deviation of about 1.5 mm. According to this elaboration, the landslide seems to confirm the pre-failure high velocities, showing a cluster of points with relatively high displacement rates, both in the NW sector, already classified as the fastest sector of the landslide in the previous period, and in the southern one, where beforehand no displacement was identified. In this period the

movement rates are higher, with an average displacement of -40 mm/yr in the NW sector, of about -35 mm/yr in the central sector, while mean values of -5.8 mm/yr are detectable in the SE sector.

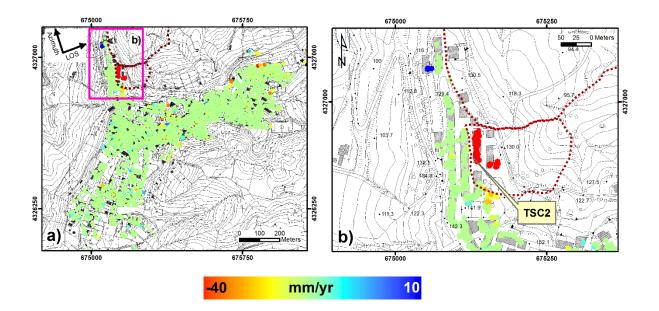


Figure 18 - a) Displacement rate map obtained with the CPT-TSC method for the time interval 2013–2014. In the purple rectangle, a zoom in of the area of interest (b). Landslides have been reported in brown-dashed line. The point TSC2 has been selected for the time series analysis (Figure 19).

7. Slope stability analysis

The rise and the very shallow depth of the piezometric level during the considered time-span can surely represent an important instability factor. According to the considered time series (point TSC2, see Figure 18), derived from the CPT-TSC processing and chosen in proximity of the piezometer P1, the activation of the movement seems to occur when the groundwater surface reaches 0.3 m below the ground surface (Figure 19). Starting from this assumption, a slope stability analysis of the study area has been carried out considering the water table level at such depth, in order to identify the most significant parameters which brought this slope to instability.

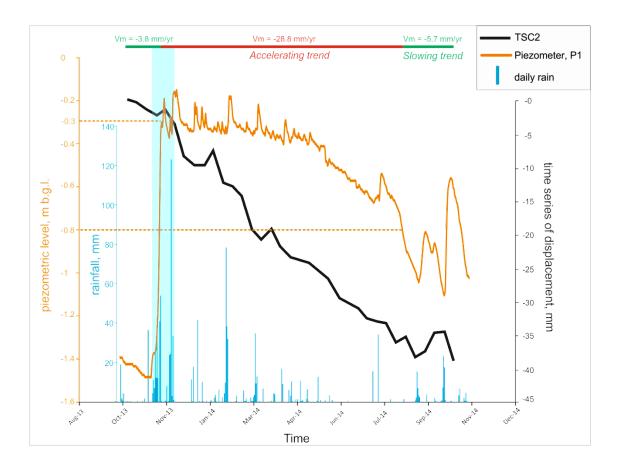


Figure 19 - Comparison between piezometric and rainfall data with time series obtained with the CPT-TSC algorithm. On the top bar, the average trends of the TSC2 time series. The average LOS velocities are shown for the slowing and accelerating trends. Dashed lines show the connection between piezometric level and acceleration and deceleration of the ground movement. The blue shaded column is for the rainy period between November 11, 2013 and December 4, 2013, correspondent to a rapid rise of piezometric level.

The slope analysis has been performed with Slope®, a software by GEOSTRU (http://www.geostru.com/EN/Slope-stability-analysis.aspx), which exploits the limit equilibrium method. The final aim is to obtain the Safety Factor (SF) of a slope, referring to a theoretical model based on the slope stratigraphy and evaluating the global stability through the relationship between maximum shear strength and the stresses acting on the slope surface:

$$SF = \frac{T_{max}}{T_{mob}} \tag{1}$$

with T_{max} representing the maximum shear strength available and T_{mob} being equal to the shear stress mobilized.

The limit equilibrium condition is attained when $T_{max} = T_{mob}$, hence when SF = 1. Consequently, a slope can be considered stable when SF > 1 as well as unstable when SF < 1. Such analysis takes into account a representative section of the slope, as shown in Figure 8b. In detail, two different periods have been considered: a) configuration of the

slope before the 2012 movement, obtained from the Regional Technical Cartography; b) configuration of the slope after the 2012 landslide, obtained by a topographic survey done after the event by ARPACAL, in November 2012. The comparison between such two profiles shows that the slope's morphology is substantially unchanged, even considering the landslide event (Figure 20).

Water table in the pre-event condition has been considered at -0.3 m from the ground level and continuous for all the profile. Such hypothesis can be considered reliable, according to rainfall and piezometric data. Furthermore, the comparison between the time series derived from the PSI elaboration and the piezometer P1 clearly shows that the activation of the displacement took place when the water table level increased up to such height (Figure 19). As to strength parameters, chosen values are the residual ones and they were obtained by means of back-analysis procedure, varying the pre-event friction angle value up to the value of mobilized strength. The stability analysis has been performed according to the Janbu method (Janbu, 1954). Thereby, the landslide body was divided into single elements and for each of them the equilibrium between forces and strength was calculated, thus obtaining the global SF. In order to characterize the terrains, a simple constitutive model was adapted, based on Mohr-Coulomb theory (Mohr, 1914), entering volume unit weight, cohesion and friction angle values.

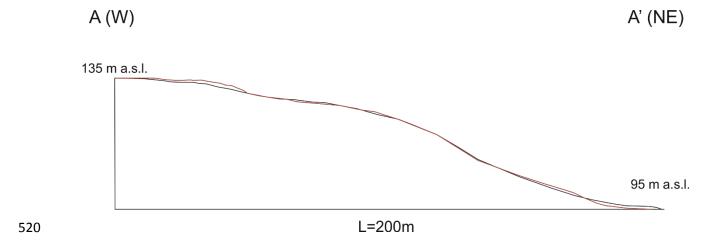


Figure 20 - Profiles of the slope of analysis: pre-event configuration (red line), post-event configuration (black line). The location of the section is shown in Figure 8b.

First, a back analysis based on the pre-event profile has been carried out, in order to determine the slope's condition at the 2012 activation. Three different slip surfaces have been hypothesized (Figure 21). On the base of the available information about the slip surface (cfr. section 4.2), a depth of about 8 m has been assumed, with the edge in proximity of Via Piave (according to inclinometer data and fractures in the roadway observed during the field survey, respectively). Analyses were carried out changing the value of the residual friction angle of the units involved in the landslide, while all the other parameters were kept unchanged. Such procedure calculated that the SF=0.96, less than 1

(limit equilibrium condition), is reached when $\phi'_r = 17^\circ$, which represents the shear strength of the units mobilized along the specific slip surface.

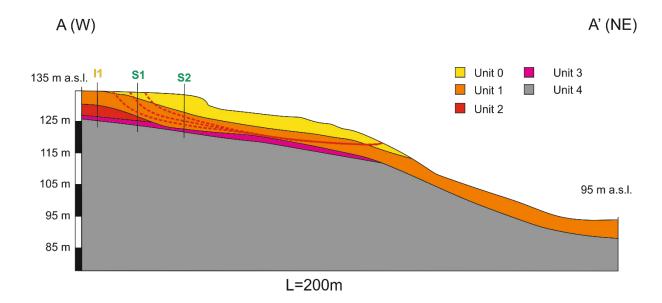


Figure 21 - Back-analysis simulation, where the three hypothetical slip surfaces are represented with red-dashed lines. I1 is the inclinometer, S1 and S2 are the two boreholes along the section.

The next step was to verify the conditions in post-event configuration, starting from the same residual friction angle ($\phi'_{r} = 17^{\circ}$). An analogue stability analysis has been carried out on the post-event configuration (Figure 22).

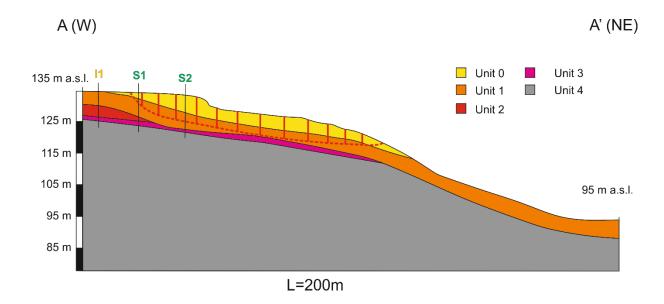


Figure 22 - Stability analysis on the post-event profile. The slip surface identified is indicated in red-dashed line. The vertical red lines represents the different slices drew following Jambu method. I1 is the inclinometer, S1 and S2 are the two boreholes along the section.

The surface highlighted in Figure 22, obtained by this procedure, is very similar to the one presumed for the preevent phase and assumes a value of SF = 0.97 when the water table lies at -0.3 m from the ground surface, thus posing a
critical issue for the current stability of the slope. Moreover, also according to the PSI analysis, the area appears to be
still moving, even after the triggering phase. As a consequence of these results, in order to increase the SF and to
guarantee the maximum stability of the slope, a possible solution could be to operate on the water table level. A
suggestion could be the implementation of drainage trenches along the whole landslide body, trying to decrease the
groundwater level until at least 0.8 m below the surface. In such condition, the SF would be equal to 1.07, therefore
guaranteeing the stability of the slope. Time series analysis confirms that the stability of the slope is obtained through
the lowering of the water table level: a slowdown of the movement can be noticed when the groundwater level reaches 0.8 m from the ground surface (Figure 19), thus validating the well-known connection between groundwater presence
and triggering/reactivation of slow-moving landslides.

8. Discussion

Piezometric data allowed to investigate the relationship between slope movements and groundwater level. The comparison between PSI time series and rainfall data clearly shows accelerations soon after abundant precipitations, as well as decelerations during dry periods (Figure 19). For instance, during a very rainy period which occurred at the end of 2013 (275 mm between November 18 and December 1), the time series derived from the CPT-TSC processing shows an acceleration of the displacement, starting from December 3. In the same time-span, the piezometric level suddenly increased (Figure 19), as a response to heavy rainfalls (275 mm in 14 days) and the presumable leaking of water pipes; water level increases more than 1 m (from -1.4 to -0.2 m), reaching a very shallow depth. After that, the displacement seems to undergo a drastic acceleration, starting from December 3, 2013. In the subsequent phase, the piezometric level keeps constant at a very shallow level, between -0.2 and -0.4 m, with small oscillations due to the variable intensity of the daily precipitation. During this time-span, the displacement also keeps persistent, with small accelerations soon after intense rainfalls. Starting from mid-May 2014, this superficial aquifer drops at least of 0.2 m, throughout the dry season, and simultaneously the movement slows down (average LOS velocity of -5.7 mm/yr), as shown in the time series. In the last part of the analyzed period, water level went through severe oscillations, due to very high daily rainfalls, and accordingly the time series continue to show a rapid response of the ground to such events. However, it must be specified that the time response to rain can be quite variable, owing to several factors, such as the geotechnical properties of landslide terrains, the morphology of the slope, the depth and volume of the landslide body, etc.

After the first results presented in Confuorto et al. (2015) one of the main objectives was the need of a more complete and accurate analysis of the studied slope in order to investigate predisposing factors and the possible

evolution of the movement by means of remote sensing techniques and with the support of conventional methods. The whole time-span of observation along the slope of interest showed a total displacement of almost 10 cm in more than 3 years of monitoring (Figure 23). The first part of the present study showed how PSI methods are able to detect, even at a very local scale, displacements and precursor stages of slow-moving landslides. To achieve this goal, two different kinds of PSI algorithms were applied: the CPT-TSC on the SUBSOFT processor and the SBAS on SARscape. The availability of different PSI techniques allowed to compare a PS-like method with an SBAS-like one, to evaluate their performance on such phenomena and finally highlight possible differences or similarity in the results. The first results obtained in Confuorto et al. (2015) demonstrated the high accuracy of two PS-like techniques in such settings. In this work SBAS seems to underestimate the velocities of the displacement in the landslide area, with respect to the prefailure stage, and the comparison with field survey, during which evidences of movement with considerable displacements have been reported, confirms this thesis. Moreover, the time series produced with the SBAS algorithm appears to be affected by higher noise (Figure 17), thus showing less accurate measurements and proving to be not well suited for local deformations affecting, for example, single buildings. In fact, the coarse resolution induced by the multilooking factors (5×5 for azimuth and range, respectively, for the Papanice analysis) of SBAS algorithm led to an underestimation of the real velocities of displacement. For this reason, the comparison between SAR and piezometric data has been carried out exclusively on

the CPT-TSC time series. With this method, more reliable velocities of the displacement have been obtained. Such

reliability is due to the comparison with rainfalls and piezometric data, and actually the activation of the displacement

begins when the rapid rise of the groundwater level occurs.

However, both SBAS and CPT-TSC were able to detect the area affected by displacements, as seen by the high concentration of points located in the neighborhood of the slope (Figure 16 and 18). In Figures 24 and 25, the displacement evolution of whole hamlet for pre- and post-failure activity, according to CPT-TSC results, are shown, highlighting the progress of the deformation only in the Pironte neighborhood. This cluster falls within the main scarp, and, as also displayed in the pre-failure phase, in the NW part of the landslide. In addition to the pre-failure movements within the 2013-2014 time-span, there is also a clear evidence of an activation of movements in the opposite sector of the landslide. In the SE part of it, clusters of at least 15 targets, showing average displacement rates of 5 mm/yr, have been equally identified by the two techniques, and in both cases the maximum value of 8.3 mm/yr was measured, on a target located in the backyard of a woodshed next to the slope. Hence, SAR analyses, even with different algorithms, highlights a new sector of the landslide previously considered as stable, and, after the triggering phase, involved in the instability. This remarkable result points out the critical role of such methods for predictive purposes. In fact, as it has been possible to forecast the 2012 landslide in the 2008-2010 time-span, the same can be done in this second time

interval, hence considering this new area activation as a sign of a potential enlargement of the movement, thus involving new buildings and new areas. The integration of PSI methods with conventional devices and geotechnical analyses assumes, likewise, a paramount importance in the landslide analysis. The comparison between time series of displacement and piezometric monitoring showed the relationship of such phenomena with rainfalls and with oscillations of the water table level, clearly pointing out and confirming the role of groundwater for the slow-moving landslide triggering, as also proved during the slope stability test.

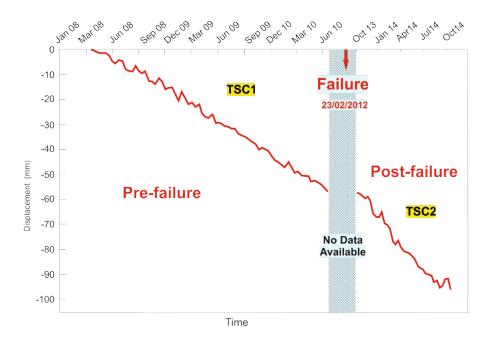


Figure 23 - Time series of displacement of the whole time-span monitored. The blue column highlights the time-span not covered by TerraSAR-X imagery. The red arrow shows the date of the slope failure (23th February 2012).

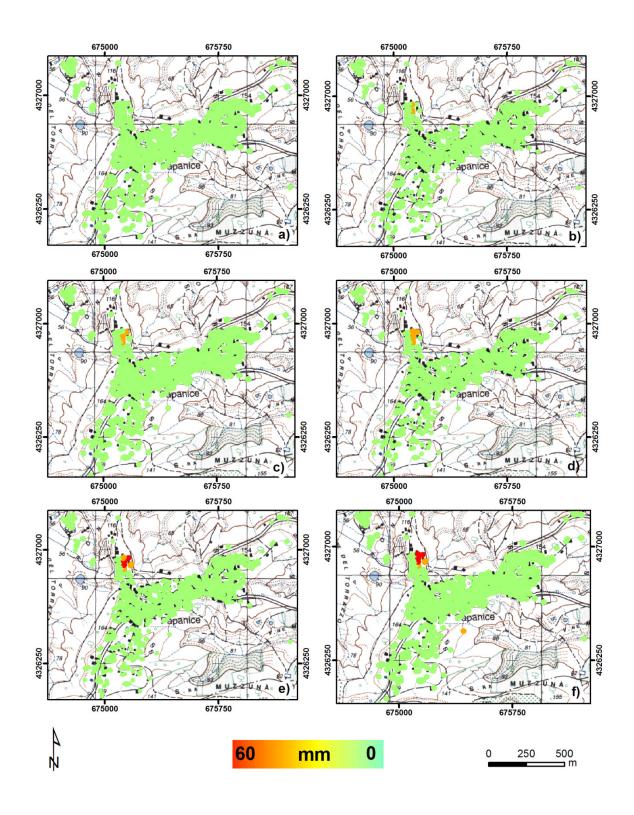


Figure 24 – Pre-failure displacement evolution in Papanice. a) April 27, 2008; b) December 3, 2008; c) February 18, 2009; d) June 30, 2009; e) January 3, 2010; f) June 28, 2010.

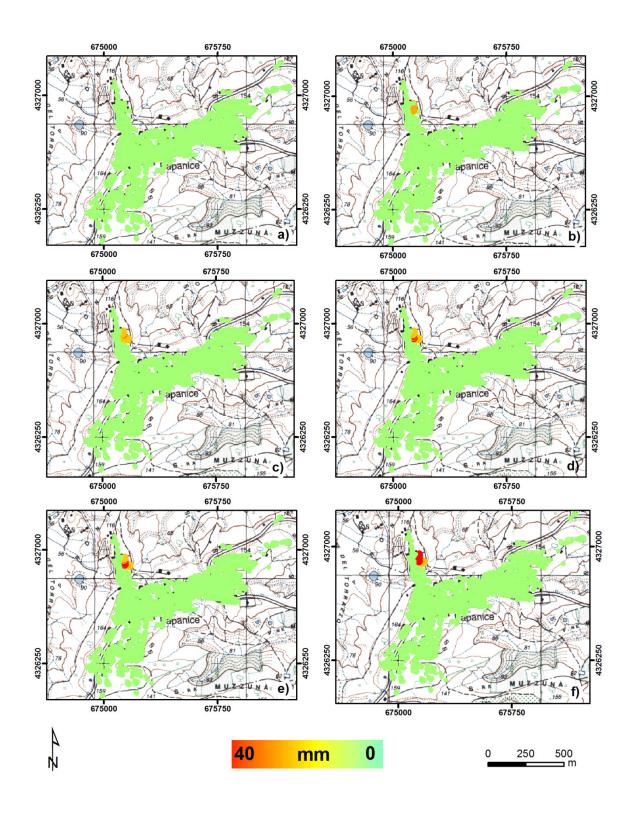


Figure 25 – Displacement evolution in Papanice. a) October 9, 2013; b) February 18, 2014; c) June 30, 2014; d) August 2, 2014; e) August 24, 2014; f) October 18, 2014.

9. Conclusion

This paper demonstrated the reliability of two Persistent Scatterers Interferometry (PSI) techniques for the comprehension of gravitational phenomena such as slow-moving landslides, especially when coupled with conventional methods. In this case, due to the presence of two different stacks, acquired during two separate time spans (2008–2010 and 2013–2014) it has been possible to follow the evolution of a slow-moving landslide case study, located in Crotone municipality, in the hamlet of Papanice. Here, on February 23, 2012, after abundant precipitations (185 mm in 3 days, ca. 28% of the average annual precipitation) a reactivation of a landslide already depicted in the Hydro-Geomorphological Setting Plan (2006) by the Calabria Basin Authority occurred, causing damage to buildings and utility lines. The precursor stages of the slope failure (2008-2010) were observed by means of PSI. Processing of the second, post-failure, period of analysis (2013-2014) confirmed with two different approaches the state of activity previously recognized on the NW sector of the landslide (characterized by average displacement rates along the Line of Sight of -40 mm/yr), and detected the activation of a sector not considered before as unstable, with an average velocity of -6 mm/yr along the LOS. The comparison between the Small Baseline Subset Approach (SBAS) and Coherent Pixel Technique (CPT) with the Temporal Sublook Spectral Coherence pixel selection approach (TSC) highlighted their different behavior on local scale studies, pointing out the better suitability of CPT-TSC in such contexts.

The slope stability analysis, finally, showed the supporting role of PSI techniques for geotechnical analyses. In this case, the piezometric surface used as input for the test has been selected according to the comparison between the time series and the groundwater monitoring, where an activation of the displacement has been recognized in occurrence of a rapid rise of the water, reaching very shallow depths. Therefore, the integration between remote sensing and conventional geological methods can represent a significant tool for intervention works planning, providing the right indication on how and where to operate in order to reduce the risk and to increase the safety factor of the area. In conclusion, we demonstrated the reliability of the PSI techniques for geological interpretation of a slow-moving landslide, and how valid they are when coupled with geological and geomorphological field activities. These tools can be considered a very useful instrument supporting urban planning or landslide hazard assessment, on behalf of public administration.

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LIST OF FIGURE CAPTIONS

- 870 Figure 1 Map of the landslide events with "victims" in the time span 1964-2013, with the spread of the Structurally
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