

Properties of Bio-based Gum Arabic/Clay Aerogels

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Abstract

Lightweight bio-based aerogels from sustainable gum Arabic (GA) and sodium montmorillonite (Na⁺-MMT) clay were prepared by means of a simple freeze-drying process. GA/clay aerogels showed high porosity (87.9%-94.9%) of mainly open type and the mechanical properties were improved by the clay. When 40% of clay was added to pure GA, the specific modulus and the absorbed energy of resultant aerogels increased by 1.6 and 4.2 times respectively. On the other hand, the exponent value for modulus in the power-law model for cellular materials increased from 1.95 to 3.28 due to the more anisotropic structures induced by the presence of the clay. In terms of thermal stability and flame retardancy, clay content played a dominant role. With 50% of clay loading, the initial decomposition temperature increased by nearly 16 °C and the peak of heat release rate was 3-fold reduced.

Keywords: Gum Arabic; Aerogels; Clay; Porosity; Flame retardancy; Thermal stability.

1. Introduction

Increasing concern on environmental protection requires the limitation of usage of petroleum-based synthetic plastics and the development of new ecological solutions to

30 replace them in order to reduce pollution, wastes and green-house gases. Foams are
31 one of the common forms for polymers with applications including thermal insulation,
32 packaging or cushioning to mention a few (Oertel, 1994). The majority of the
33 low-density foams existing in the market are derived from petroleum and are not
34 biodegradable. Therefore, alternatives based on polymers derived from renewable
35 resources (bio-based polymers) are attracting an increasing attention. Among the
36 different bio-based polymers, namely polyesters, proteins and polysaccharides, the
37 latter have a great potential to be transformed into aerogels, a porous, lightweight
38 foam-like material (Mikkonen et al., 2013).

39 Plastic foams are formed by a solid matrix skeleton and a gaseous phase which is
40 derived from a blowing agent, and where the foaming process is carried out by
41 applying mechanical, physical or chemical procedures to the solid material. In
42 contrast, aerogels are created when the liquid contained in a wet gel is replaced by air.
43 Aerogels are mainly obtained through supercritical drying (SCD) and contain a
44 network of interconnected mesopores (2-50 nm). Due to their high surface area, they
45 are used as drug carrier, catalyst, adsorbent or in insulating applications.
46 Garcia-González et al. (2011) summarized the fundamental processing parameters and
47 methods for preparing different polysaccharide-based aerogels through SCD, showing
48 that polysaccharides can be used as an alternative to silica-based aerogels for drug
49 delivery. Quignard et al. (2008) also employed this technique to prepare different
50 marine polysaccharide aerogels for heterogeneous catalyst supports based on alginates,
51 carrageenan and chitosan. Those aerogels presented a high specific surface area
52 ($200\text{-}570\text{ m}^2/\text{g}$) and were stable in most organic solvents. Superabsorbent alginate
53 aerogels were prepared by Mallepally et al. (2013). In their work, the aerogels were
54 capable of absorbing about 120 times their weight in saline water in 24 hours. The
55 observed behavior was attributed to the large pore volume and high specific surface
56 area ($\sim 500\text{ m}^2/\text{g}$) of the aerogels as well as the polymer increasing in charge in the
57 presence of salt ions. Finally, Rudaz et al. (2014) reported the preparation of
58 superinsulating mechanically strong aerogels from pectin having a thermal
59 conductivity as low as $0.016\text{-}0.020\text{ W}/(\text{m}\cdot\text{K})$ which was attributed to the low density

60 ($< 0.15 \text{ g/cm}^3$) and nanometric dimensions of pores, leading to a decrease of
61 conduction in the gas phase.

62 In contrast to SCD, freeze-drying applied to polysaccharide solutions usually
63 yields structures having micron-sized pores. The nucleation and ice growth destroy
64 the gel network, creating large pores and thus having considerably lower specific
65 surface area. The aerogel structure is the result of the ice sublimation and is composed
66 of a solid phase and a large fraction of air, which correspond to the volumes occupied
67 by the biopolymer and ice in the frozen gel, respectively. In this process, the water
68 solubility, swelling and gel-forming capability of polysaccharides contribute to the
69 stability of the so-formed aerogels (Quignard et al., 2008). Several
70 polysaccharide-based aerogels have been prepared through freeze-drying. Sehaqui et
71 al. (2010) produced high porosity foam-like materials based on cellulose nanofibers.
72 Due to its high affinity with cellulose, xyloglucan was employed to increase the
73 strength and stiffness of the resultant micro-porous aerogels. Bendahou et al. (2014)
74 combined extracted cellulose, cellulose nanofibers and nanozeolite particles to create
75 hybrid aerogel monoliths. The thermal conductivity of cellulose nanofibers aerogels
76 was found to decrease with nanozeolite content whereas it remained almost constant
77 in the case of extracted cellulose aerogels. This was attributed to the different
78 microstructures and the embedment of nanozeolite in cellulose nanofibers. Valentin et
79 al. (2003) compared SCD with freeze-drying in chitosan aerogels, finding that SCD
80 yields considerably higher porosity although freeze-dried aerogels showed even lower
81 density than the ones dried with supercritical carbon dioxide. In general, these open
82 cell freeze-dried bio-aerogels exhibit the properties of the precursor polymer but
83 usually have low Young's modulus and reduced load-bearing capacity. Nevertheless,
84 different approaches such as crosslinking (Pojanavaraphan et al., 2010) or filler
85 reinforcement (Svagan et al., 2008) can be followed to improve aerogel performance.
86 Among these methods, clay addition has been proved to be an economic and
87 straightforward way to enhance both the thermal and mechanical properties and to
88 expand the range of its potential applications. Following this approach, Chen et al.
89 (2012) used a combination of alginate and sodium montmorillonite clay to create low

90 flammability robust aerogels with mechanical properties close to that of balsa wood.
91 Calcium cation crosslinking increased the solution viscosity leading to a finer network
92 structure and to a further enhancement of mechanical properties. In another approach,
93 xanthan gum /clay aerogels were produced by Wang et al. (2014). The increase of the
94 content of xanthan gum lead to a network structure which increased the mechanical
95 properties. However, a synergic effect was found by the introduction of agar. In the
96 presence of both polysaccharides, the resultant aerogels displayed a significant
97 improvement in mechanical properties as compared to those containing a single
98 biopolymer. Chen et al. (2013a) combined clay and cation crosslinking to form
99 pectin/clay aerogels with enhanced mechanical properties and thermal resistance. The
100 introduction of clay generated a much rougher microstructure and also contributed to
101 increase the decomposition temperature due to the themal insulation and
102 mass-transport barrier created by the clay layers. Among the different polysaccharides,
103 gum Arabic (GA) exhibits a very high solubility in water. Unlike other gums, GA can
104 be dissolved even at high concentrations (up to 50% w/v) withouth showing a
105 remarkable increase in viscosity. These characteristics make GA a very attractive
106 precursor for producing GA/clay hybrid aerogels.

107

108 Gum Arabic is an exudate from the *Acacia* tree and its precise molecular
109 structure is little known. It is recognized by many researchers that gum Arabic
110 consists of a mixture of arabinogalactan polysaccharide (major component) and
111 hydroxyproline protein (minor component) (Idris et al., 1998; Islam et al., 1997;
112 Randall et al., 1988). The main structural feature of the major component is a
113 β -(1 \rightarrow 3)-galactose backbone and 1,6-linked galactose side chains terminating in β -D
114 glucuronic acid. Moreover, the properties of GA differ according to the botanical
115 source (Cozic et al., 2009). Due to its unique emulsification, film-forming, and
116 encapsulation properties, GA is extensively used in industry, such as food (Krishnan
117 et al., 2005), paper (Verbeken et al., 2003) and pharmacy (Ward, 2000).

118 In the current work, bio-based light-weight GA aerogels were prepared using an
119 environmentally-friendly freeze-drying process with the aim of providing alternatives

120 to replace packaging materials traditionally prepared from non-biodegradable
121 petrochemical products. Hybrid organic-inorganic aerogels were also created by
122 adding sodium montmorillonite (Na⁺-MMT) clay to GA aqueous solution. The
123 resultant aerogel composites were expected to show improved thermal and
124 mechanical properties than the neat GA aerogels. The microstructures, compression
125 properties, thermal stability and flame retardancy of aerogels were investigated,
126 respectively.

127

128 **2. Material and Methods**

129

130 **2.1. Materials**

131 Gum Arabic in powder form was bought from T3Q Quimica (Spain). Its
132 physicochemical properties resulted from a preliminary characterization are reported
133 in Table 1. Sodium Montmorillonite (Na⁺-MMT, PGW grade) was purchased from
134 Southern Clay (USA), having a density of 2.6 g/cm³ and cation exchange capacity
135 (CEC) of 145 meq/100 g. All materials were used as received.

136

137 **2.2. Aerogel Preparation**

138 *GA aerogels:* GA powder was dissolved in deionized (DI) water at room temperature
139 under magnetically stirring until achieving transparent solutions with different
140 concentrations (5 wt%, 7.5 wt%, 10 wt% and 15 wt%). Then they were poured into
141 cylinder vials (diameter: 30mm) or square-shaped moulds (100 x 100 mm²) before
142 being frozen at -80°C in an ethanol/solid CO₂ bath for 30 minutes. Aerogel samples
143 were obtained after ice sublimation in a lyophilizer (Telstar Lyoquest) for 96 hours
144 using a condenser temperature of -80 °C and vacuum of 0.01mbar.

145 *GA/Clay aerogels:* Clay suspensions were prepared by dispersing Na⁺-MMT clay
146 nanoparticles in DI water using an IKA Ultra-turrax disperser. GA solutions were
147 obtained using the previously mentioned procedure. Then they were blended and
148 mixed to attain homogenous precursor suspensions containing 5 wt% clay and various
149 GA concentrations (5 wt%, 7.5 wt%, 10 wt%, 15 wt%). Finally, the same

150 freeze-drying process was applied to acquire GA/Clay aerogels.
151 Sample identification is GA or clay used followed by their respective concentration in
152 precursor suspensions, i.e., GA5C5 represents a sample that was prepared from an
153 aqueous suspension containing 5 wt% of gum Arabic and 5 wt% of clay.

154

155 **2.3.Characterization**

156 The sugar composition of the gum Arabic was determined by HPLC (Agilent 1100)
157 using the procedure described by Randall et al. (1989). An ICsep ION-300 Interaction
158 analysis column equipped with a refractive index detector was used. The sample (20
159 μdm^3) was injected into the column using 0.013M H_2SO_4 solution as eluent at flow
160 rate of 0.4 cm^3/min . The retention times were monitored using a Beckman 156
161 refractive index detector. Individual standards of glucuronic acid, arabinose, galactose
162 and rhamnose were used.

163 To determine the intrinsic viscosity of gum powder solutions the method of Solomon
164 and Ciuta (1962) was used. Gum powder was dissolved in distilled water to a
165 concentration of 0.01 g/cm^3 and analysed using a Cannon Ubbelohde size 75
166 viscosimeter with precise temperature control through a thermostatic bath at 25 °C.
167 Once the intrinsic viscosity was known, the molecular weight was calculated applying
168 the Mark-Houwink-Sakurada equation:

169

$$170 \quad [\eta] = k (M)^a \quad (1)$$

171

172 Where $[\eta]$ is the intrinsic viscosity, M the molecular weight and k and a are the
173 Mark-Houwink-Sakurada parameters.

174 The apparent density (ρ_{app}) of the aerogel samples was calculated from the mass and
175 the actual specimen dimensions using a precision balance and a digital Vernier calliper,
176 respectively. Five replicas were taken for each composition.

177 Theoretic densities (ρ_{ts}) of the GA/clay composite aerogels were calculated according
178 to the equation:

179
$$\rho_{ts} = \frac{1}{w_{AG}/\rho_{AG} + w_C/\rho_C} \quad (2)$$

180 Where w_{GA} and w_C are the mass fractions of GA and clay in the dry aerogels,
181 respectively ρ_{GA} and ρ_C are the densities of GA and clay, respectively. The clay density
182 was 2.6 g/cm³ according to the supplier; ρ_{GA} (1.302 ± 0.002 g/cm³) was determined
183 using a helium pycnometer (Accupyc 1330) in which dried GA powder was tested.

184 The porosity (P) of the aerogel is defined as the volume fraction of voids and was
185 calculated as follows:

186
$$P = \left(1 - \frac{\rho_{app}}{\rho_{ts}}\right) \times 100\% \quad (3)$$

187 A Jeol 5610 scanning electron microscope (Japan) operated at 10 kV was used to
188 analyse the microstructures of the aerogels. The samples were cryofractured and
189 coated with a gold layer prior to observation.

190 Compression testing was carried out along the vertical axis of the cylinder samples
191 (main direction of ice growth) on a Galdabini (Italy) universal testing machine
192 equipped with a load cell of 1kN following ISO 604 standard. The crosshead rate and
193 maximum deformation were set to 1 mm/min and 70%, respectively. The Young's
194 modulus and the absorbed energy were calculated from the experimental data. Three
195 replicas of each sample were made.

196 TGA was carried out on a Mettler Toledo TGA/DSC1 equipment to study the thermal
197 stability of the aerogels. Samples were loaded in alumina pans and heated at a rate of
198 10 °C/min from 30 to 900 °C under dry nitrogen.

199 The burning behavior of GA/clay aerogels were investigated using a cone calorimeter
200 (Ineltec BECC model, Spain) following ISO 5660 standard. Square-cut samples (100
201 × 100 mm²) with an average thickness of 7 mm were placed in a steel support and
202 exposed to an external heat flux of 50 kW/m².

203

204 **3. Results and Discussion**

205

206 3.1. Gum Arabic Preliminary Characterization.

207 Table 1 shows the results of the preliminary characterization of the raw gum Arabic
208 powder including the determination of sugar content, intrinsic viscosity and molecular
209 weight. Data given by the supplier is also included. In a similar way like other gum
210 exudates from *Acacia* trees, the current one is rich in arabinose and galactose units
211 being rhamnose the minor component. The glucuronic acid was below the detection
212 limit of the equipment ($< 3.5\%$). No other peaks than the ones under analysis
213 appeared, indicating the absence of other majoritarian components such us organic
214 acids or different monosaccharides. The constants of the Mark-Howing-Sakurada
215 equation were found to be $K = 0,01311 \text{ cm}^3/\text{g}$ and $a = 0,5406$ respectively (Masuelli,
216 2013). Accordingly, the resultant molecular weight was $M=1,1 \times 10^6 \text{ g/mol}$ which is
217 consistent with data found in literature for *Acacia* senegal gums (Renard et al. 2006,
218 Randall et al. 1989).

219

220 Table 1. Physicochemical data and composition of gum Arabic powder

Physicochemical data	Value	Composition	Value
Moisture content (%)	7	Galactose (%)	39,8
Ash content (%)	3.4	Arabinose (%)	58,1
Optical rotation (degrees)	-25	Rhamnose (%)	2,1
pH (25% w, 20°C)	4.1-4.8	Glucuronic acid (%)	-
Intrinsic viscosity (cm^3/g)	23.7	Molecular weight (g/mol)	$1,1 \times 10^6$

221

222 3.2. Density and Porosity

223 The results of density and porosity of the samples are summarized in Table 2. Helium
224 is capable of penetrating into open pores of angstrom dimensions, giving the volume
225 occupied by open porosity (Chang, 1988). The skeletal density of sample GA10 was
226 measured using a helium pycnometer. Then the tested sample was ground to break the
227 closed-cell structure. The density of the ground sample was investigated in the same
228 manner. There was no difference between the two measurements, indicating the
229 absence of closed macro-pores in the aerogel. On the other hand, all tested samples

230 exhibited high porosities corresponding to the voids left by ice during its sublimation.

231

232

Table 2. Density and porosity of GA/clay aerogels

Samples	ρ_{app} (g/cm ³)	ρ_{ts} (g/cm ³)	Porosity (%)
GA7.5	0.085±0.001	1.302	93.5±0.1
GA10	0.109±0.018	1.302	91.6±1.4
GA15	0.154±0.009	1.302	88.2±0.1
GA5C5	0.088±0.001	1.735	94.9±0.1
GA7.5C5	0.115±0.001	1.623	92.9±0.1
GA10C5	0.149±0.013	1.562	90.5±0.1
GA15C5	0.180±0.002	1.488	87.9±0.1

233

234 For neat GA aerogels, increasing the GA content from 7.5 to 15 wt%, the porosity
235 reduced by 5.3%. A similar tendency was observed when clay was added. As expected,
236 a higher content of solid component led to a lower void fraction.

237

238 3.3. Morphology

239 Freeze drying of aqueous GA/clay gels produced stable aerogel monoliths retaining
240 the shape of the used mould, as can be seen in Figure 1. Pure clay aerogels are
241 capable to form stable three dimensional objects because the particles are linked
242 edge-to-face creating a “house of cards” structure due the opposite surface and edge
243 charges that exist in clays. However, this material is very brittle. The addition of a
244 polymer yields a more robust material provided that the polymer covers the clay
245 layers and bridges the gaps left by the ice after sublimation.

246

247 The morphological microstructures of GA/clay aerogels are shown in Figure 2.
248 Sample GA7.5 exhibited a layered structure without polymer struts between layers
249 (Figure 2a). When the content of GA was increased to 15 wt%, the layers increased in
250 thickness. However, there was no apparent change in the number of polymeric struts
251 connecting the clay layers (Figure 2b). Compared to other biopolymer aerogels, for
252 example xanthan gum (Wang et al., 2014), GA aerogels prepared from precursor
253 solutions having a high concentration (15 wt%) did not display network structures.

254 The reason is that GA solutions retain a low viscosity even at high concentration. For
255 instance, 30% GA solutions have a lower viscosity than 1% xanthan gum at low shear
256 rates (Phillips and Williams, 2009).

257 When 5wt% of clay was added to the precursor solution of GA7.5, its viscosity
258 was increased. The ice front growth was retarded by the higher fluid viscosity and
259 secondary crystallization occurred (Deville et al., 2006), meaning that ice nucleation
260 and growth occurred in a direction different from the main one (vertical). As a result,
261 smaller ice crystals were generated, resulting in a rough fracture surface (Figure 2c).
262 Increasing the GA concentration in the precursor suspension of GA/clay aerogels
263 (sample GA15C5), a continuous “house of cards” structure (Figure 2d) appeared due
264 to the further increment of viscosity.

265 These different aerogel microstructures are responsible for the mechanical
266 property changes discussed in the following section.

267

268 **3.4. Compressive Properties**

269 The compressive stress-strain curves of the GA and GA/clay aerogels are shown in
270 Figure 3. Generally, these samples showed a compressive behaviour similar to the one
271 of elastic-plastic polymeric foams. Compressive mechanical properties, such as
272 compressive modulus (E), specific compressive modulus (E_s), compressive stress at
273 70% strain (σ_{\max}), and absorbed energy (E_a) are listed in Table 3. It should be
274 mentioned that the sample GA5 was too brittle to be tested.

275 Regarding neat GA aerogels, increasing the polymer content, σ_{\max} and E_a of the
276 samples increased. However, there was no significant change in specific compressive
277 modulus (E_s). This is because the density of polymeric struts between the layers in the
278 aerogels did not increase with GA content, as shown in the SEM observations.

279 When 5wt% of clay was added, the specific modulus of GA7.5C5 increased by
280 1.6 times compared to GA7.5 (see Table 3). This result was consistent with the
281 finding in prior works on biopolymer-clay aerogel composites (Chen et al., 2013a;
282 Chen et al., 2013b). Sample GA15C5 showed a layered structure with denser polymer

283 struts (Figure 2d) as compared to GA7.5C5, thus it exhibited a more robust structure
 284 and better mechanical properties. However, both GA and clay platelet surface are
 285 negatively charged and thus a weak adhesion is produced between them, resulting in
 286 the appearance of small fractures that can be observed as kinks in the compressive
 287 pattern of sample GA15C5 in Figure 3.

288

289

Table 3. Compressive mechanical properties of GA/clay aerogels

Samples	E (MPa)	E_s (MPa/g cm ³)	σ_{max} (MPa)	E_a (kJ/cm ³)
GA7.5	0.6±0.1	7.5±2.1	-	12±2
GA10	1.4±0.3	10.6±2.1	0.25±0.1	49±12
GA15	2.1±0.7	10.9±2.9	1.10±0.1	240±45
GA5C5	1.2±0.2	13.9±2.0	0.35±0.1	44±3
GA7.5C5	2.3±0.1	19.4±1.1	0.40±0.1	62±15
GA10C5	4.0±0.6	30.0±3.4	0.60±0.2	70±1
GA15C5	25.8±4.2	143 ±23	1.30±0.1	315±20

290

291 The addition of clay reinforced the mechanical properties of the aerogels. The
 292 power-law developed by Gibson and Ashby (Gibson and Ashby, 1999) for cellular
 293 solids was used to analyse mechanical properties:

$$294 \quad \frac{K}{K_s} \propto C \left(\frac{\rho}{\rho_s} \right)^n \quad (3)$$

295 Where K means a mechanical property of foams, K_s is the property of the
 296 corresponding fully solid material. ρ and ρ_s are the apparent density and skeletal
 297 density, respectively; ρ_s herein is thought to be equal to the theoretical skeletal density.
 298 C and n are structural parameters (Gibson and Ashby, 1999; Hilyard, 1982). In present
 299 work, exponent values for modulus and ultimate strength of GA aerogels were 1.95
 300 and 3.84, respectively. However, for GA/clay aerogel composites of which the relative
 301 density (ρ/ρ_s) changed, the values of n were 3.53 and 1.46 for modulus and ultimate
 302 strength, respectively.

303 The exponent values changed with the material structures. For open-cell foams,
 304 the exponent was expected to be 2. Wood has an exponent of 3 in the radial direction
 305 due to anisotropy of the structure (Gibson and Ashby, 1999) and silica aerogels show
 306 a value in the range of 2.6-3.8 due to different sample preparation methods (Ma et al.,

307 2000). For pure GA aerogels, the exponent for modulus was 1.95 (Figure 4), which
308 was similar to the one for aerocellulose ($n=1.7$) found by Sescousse et al. (2011) and
309 was also consistent with the open structure generated in the aerogels. This value
310 increased to 3.28 with the addition of clay, similar to the one found in PVOH-clay
311 aerogels (3.74) by Alhassan et al. (2010). It was attributed to the reinforcing effect of
312 clay and the more anisotropic structures induced by clay addition in the composites.
313 Nevertheless, due to the scarce number of data, more experimental analyses on the
314 mechanical properties of this type of aerogels are needed to confirm the results.

315

316

317 **3.5. Thermal Stability**

318 Thermal stability of GA/clay aerogels were studied using thermogravimetric analysis
319 under dry nitrogen atmosphere. The weight loss curves are shown in Figure 5. The
320 decomposition of aerogels can be divided into three stages. The moisture in GA-based
321 aerogels was firstly evaporated under the thermal loading up to 150 °C. Then
322 dehydration and decarboxylation reactions of GA occurred when the temperature was
323 over 250°C until the formation of char (~330 °C) (Cozic et al., 2009). Finally, with
324 increasing temperature, the char was slowly oxidized to yield aromatic components.
325 $T_{d5\%}$ is defined as the temperature at which 5% weight loss occurred after 150 °C
326 ($dW/dT \approx 0$). It was recorded as the initial decomposition temperature of the aerogels.
327 Table 4 summarizes the temperatures at 5% weight loss ($T_{d5\%}$), temperatures at
328 maximum weight loss rate (T_{dmax}), maximum weight loss rates (dW/dT_{max}) and
329 residue amounts (W_R).

330 In comparison to sample GA5, it can be observed that GA5C5 presented a higher
331 $T_{d5\%}$ (275 °C) and a much lower maximum weight loss rate (0.7 %/°C). The clay
332 nanoplatelets acted as a physical barrier, enhancing the heat resistance of materials
333 (Rao and Pochan, 2007). Regarding sample GA15C5, $T_{d5\%}$ increased by nearly 7 °C
334 and the maximum weight loss rate decreased by 0.4 %/°C as compared to GA15,
335 respectively. The differences in thermal stability of the samples GA5C5 and GA15C5

336 were attributed to the relative clay content in the composites. A higher clay content
 337 led to a lower degradation rate and a higher initial decomposition temperature. This is
 338 due to the formation of a denser clay layer char, as can be observed from the
 339 difference in their residue amounts. However, clay addition caused a lower T_{dmax} ,
 340 possibly related to the higher thermal conductivity that is resulted from a denser and
 341 more compact structure of the aerogel.

342

343

Table 4. Parameters for thermal stability of GA/clay aerogels

Samples	$T_{d5\%}$ (°C)	T_{dmax} (°C)	dW/dT_{max} (%/°C)	Residue (%)
GA5	258.6	310.4	1.41	13.2
GA5C5	274.5	299.0	0.69	52.3
GA15	261.2	311.7	1.47	16.5
GA15C5	267.7	308.3	1.09	38.2

344

345 3.6. Combustion Behavior

346 The combustion behavior of the aerogels was investigated using cone calorimetry.
 347 The resultant heat released during burning is determined in terms of heat release rate
 348 (HRR) as a function of burning time, as seen in Figure 6. The detailed flammability
 349 parameters, such as time to ignition (t_i), time to flame extinguish (t_e), peak of heat
 350 release rate (PHRR), total heat release (THR), time to peak of heat release rate
 351 (TTPHRR), and fire growth rate (FGR), are given in Table 5. A double peak signal
 352 appeared in the HRR curves of the sample loaded with clay. It seemed to be due to the
 353 transient protective effect of the clay layers during the combustion (Alexandre and
 354 Dubois, 2000). The combustion of the rest of material occurred when the layer was
 355 broken.

356 The time to ignition was similar in all cases and corresponded to the time for
 357 generating the critical amount of combustible gas in the gas phase. Sample GA15 had
 358 a PHRR value of 233kW/m² and time to PHRR of 36 s. Adding 33% of clay, PHRR
 359 decreased to 121 kW/m² and the FGR values reduced from 6.5 to 4.5kWm⁻²s,
 360 indicating a lower rate of combustion. This tendency was also found for the other
 361 bio-based aerogels when clay was used to improve the flame retardant properties

362 (Wang et al., 2014). This is due to the clay enrichment on the sample surface during
 363 the increasing thermal load (Kashiwagi et al., 2004), which brings a decomposition
 364 rate decrease for the underlying polymer fraction. Moreover, the presence of clay and
 365 its characteristic structural network forms a complex labyrinth through which
 366 combustion gases diffuse out of the material (Chen et al., 2012). Decreasing the
 367 amount of polymer in the GA/clay aerogels, the flame retardant effect of clay was
 368 more remarkable, as displayed in sample GA5C5.

369

370

Table 5. Combustive parameters of GA/clay aerogels

Samples	t_i (s)	t_e (s)	TTHRR (s)	PHRR (kW/m ²)	FGR (kW/m ² s)	THR (MJ/m ²)	Residue (%)
GA15	10	386	36	232.9	6.5	19	2.9
GA15C5	11	146	27	121.1	4.5	17.2	23.6
GA5C5	15	91	24	56.4	2.4	4.9	45.4

371

372

373 **4. Conclusions**

374 Gum arabic, a type of polysaccharide from African plants, was used to prepare “green”
 375 aerogels. Clay was added to form GA/clay aerogel composites. GA-based aerogels
 376 had a typical lamellar structure created by the ice template. Neat GA aerogels behaved
 377 in a brittle manner due to insufficient polymer connection between layers. With the
 378 addition of clay, the compressive mechanical properties were markedly improved. The
 379 thermal stability and flame retardant properties were found to be dependent on clay
 380 content in the aerogel composites. Clay layers formed during the burning process and
 381 acted as a physical barrier, protecting the sample underneath.

382

383

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388

389

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474 **Figure Caption:**

475

476 Figure 1. Photograph showing samples after freeze-drying: (a) pure GA aerogels; (b)
477 GA/clay aerogels.

478 Figure 2. SEM photos of GA/clay aerogels: (a) GA7.5; (b) GA15; (c) GA7.5C5; (d)
479 GA15C5.

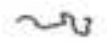


480 Figure 3. Compressive curves of GA/clay aerogels.

481 Figure 4. Compressive modulus of the aerogels as function of relative density. Insert
482 shows the initial part of the curves.

483 Figure 5. TGA weight loss curves of GA/clay aerogels.

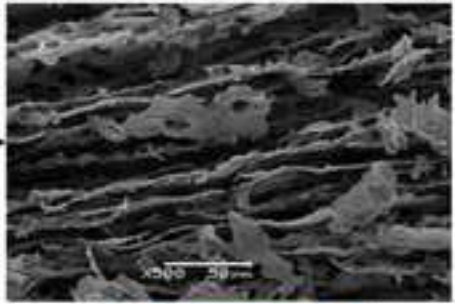
484 Figure 6. Heat release rate as a function of time during cone calorimetry tests.



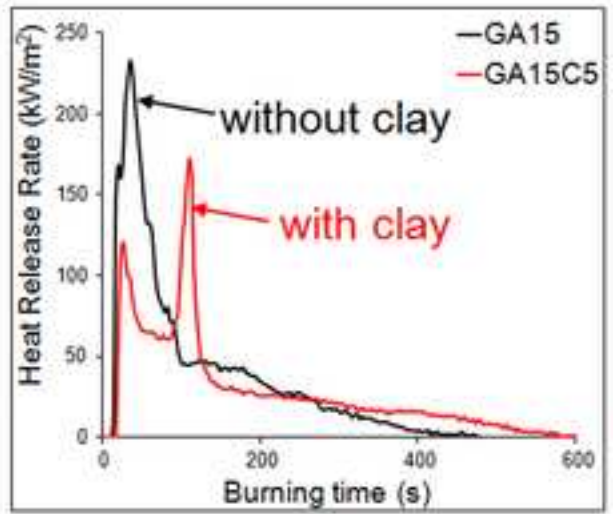
-  Gum Arabic
-  Clay
-  Ice

Gum Arabic/Clay Aerogel

Drying



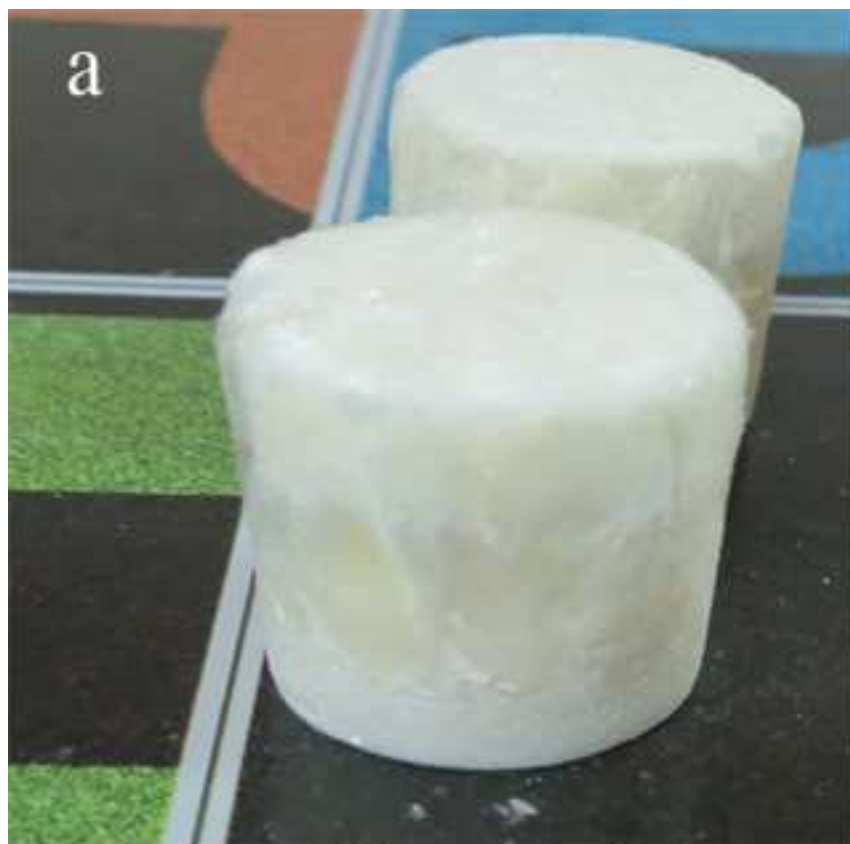
Fire Testing



Highlights:

- “Green” gum Arabic /clay aerogels were prepared using a freeze-drying process.
- The unique solvent used in the preparation process was water.
- Gum Arabic aerogels exhibit a lamellar structure created by the ice template.
- The thermal stability and flame retardancy were improved by clay addition.

Figure 1



GA aerogel



GA/clay aerogel

Figure 2a

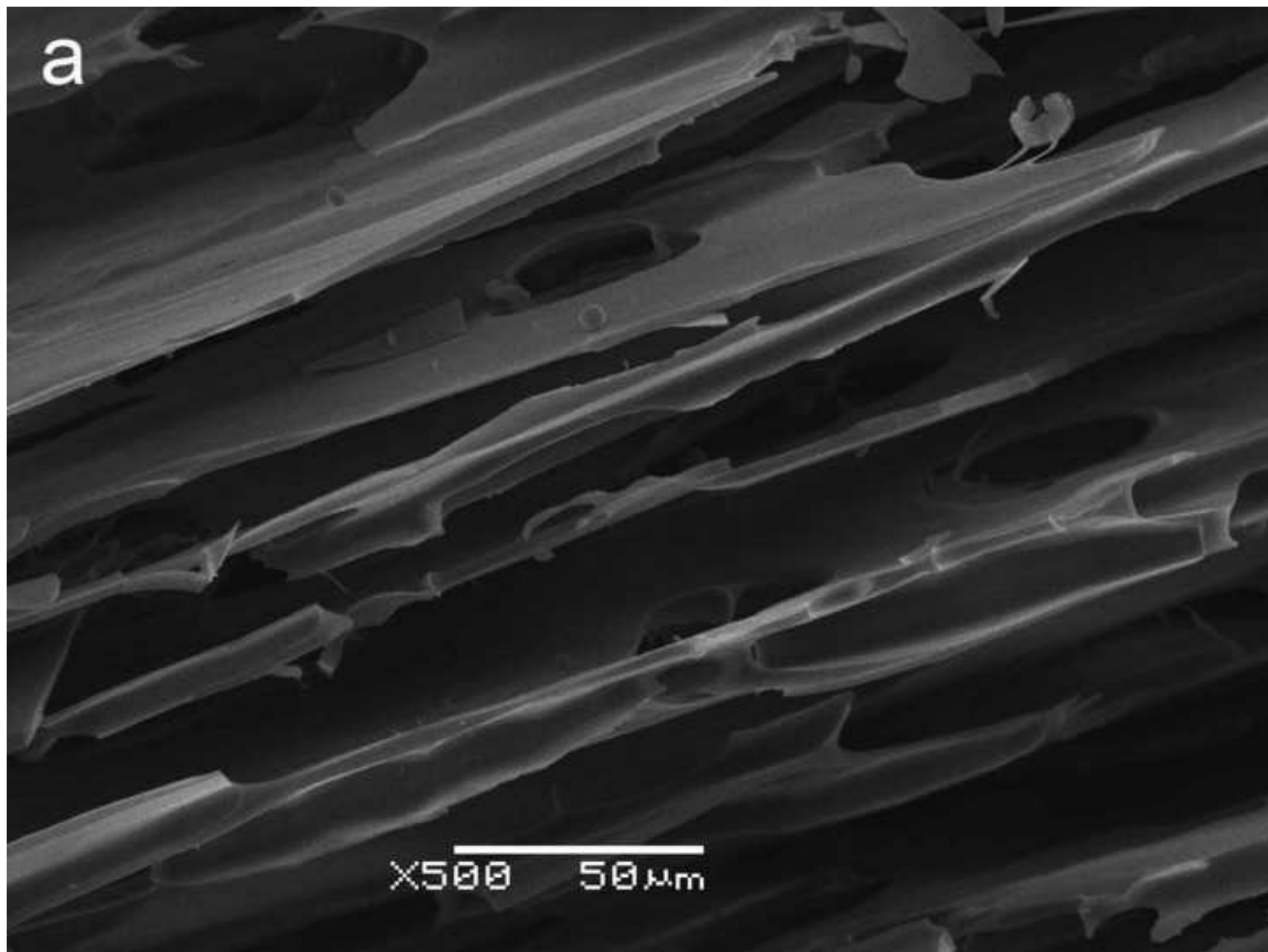


Figure 2b

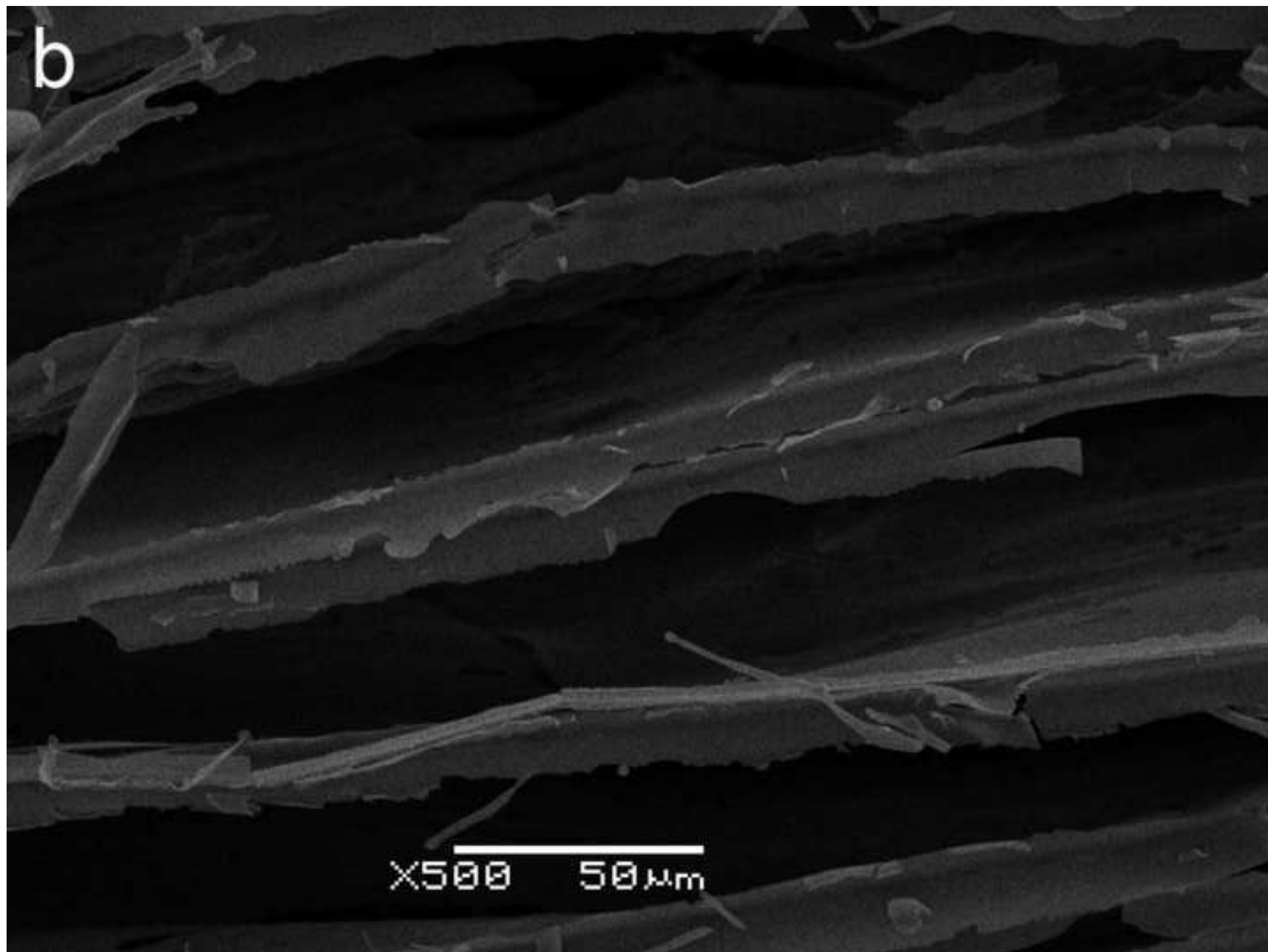


Figure 2c

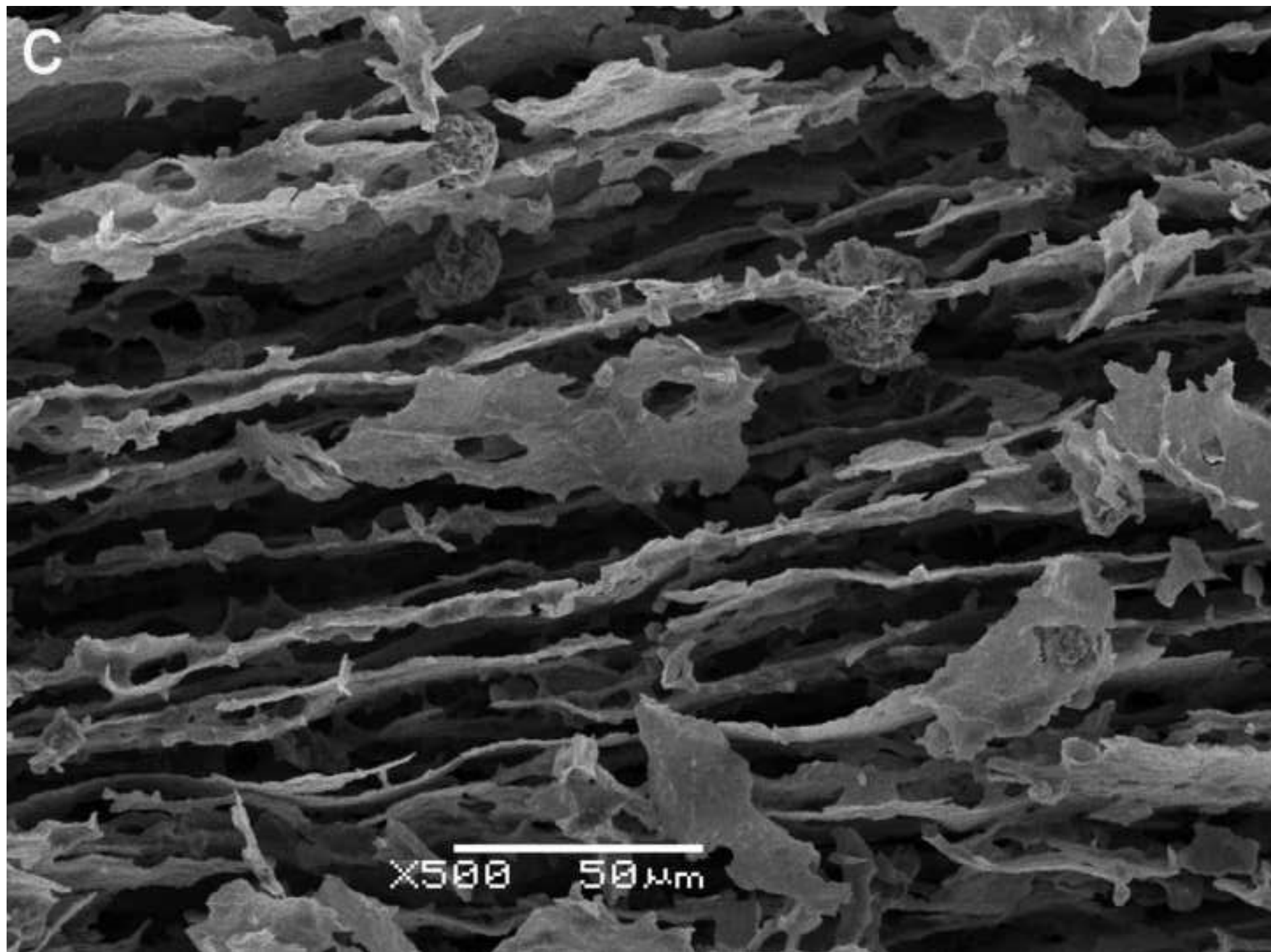


Figure 2d

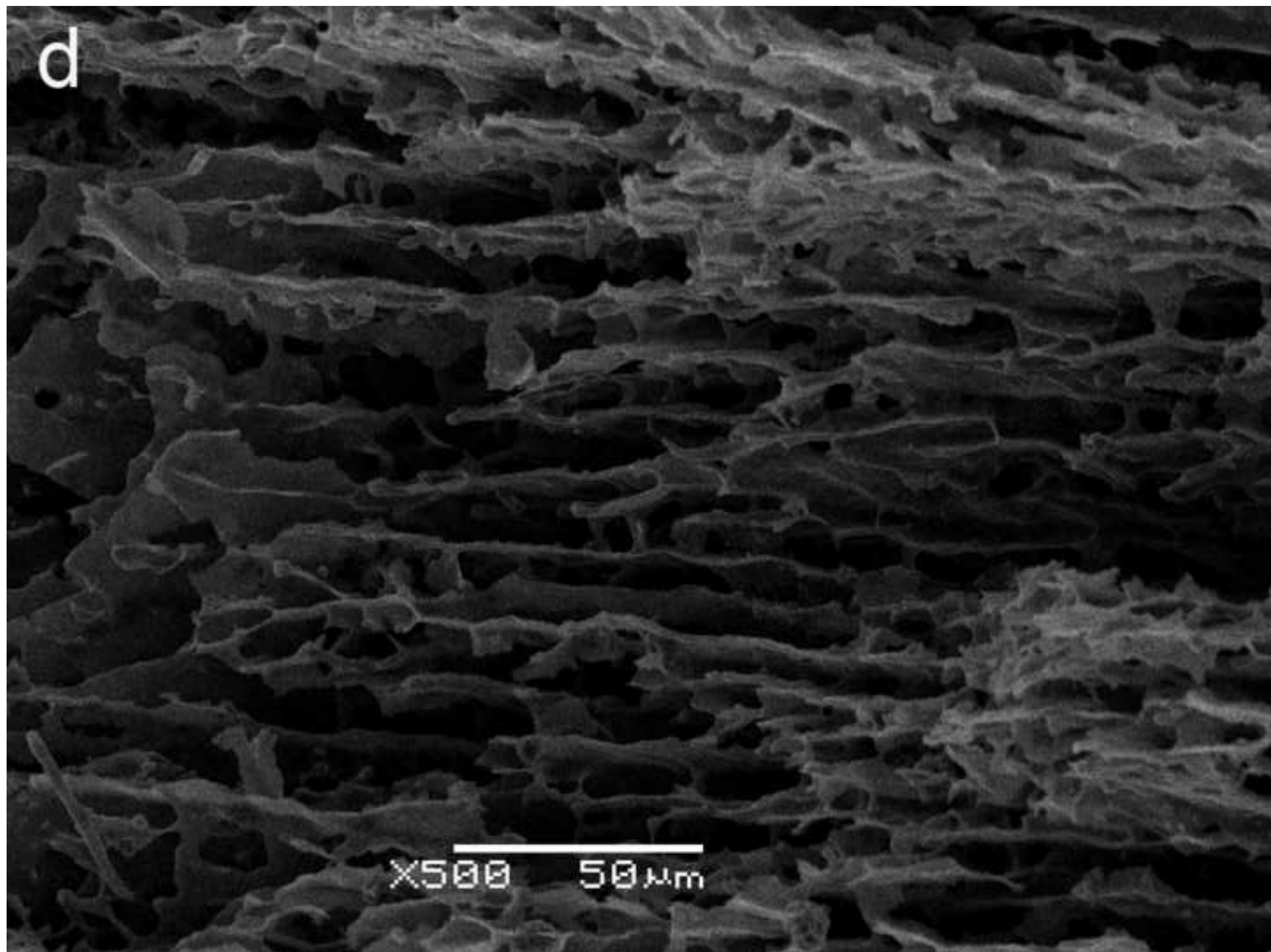


Figure 3

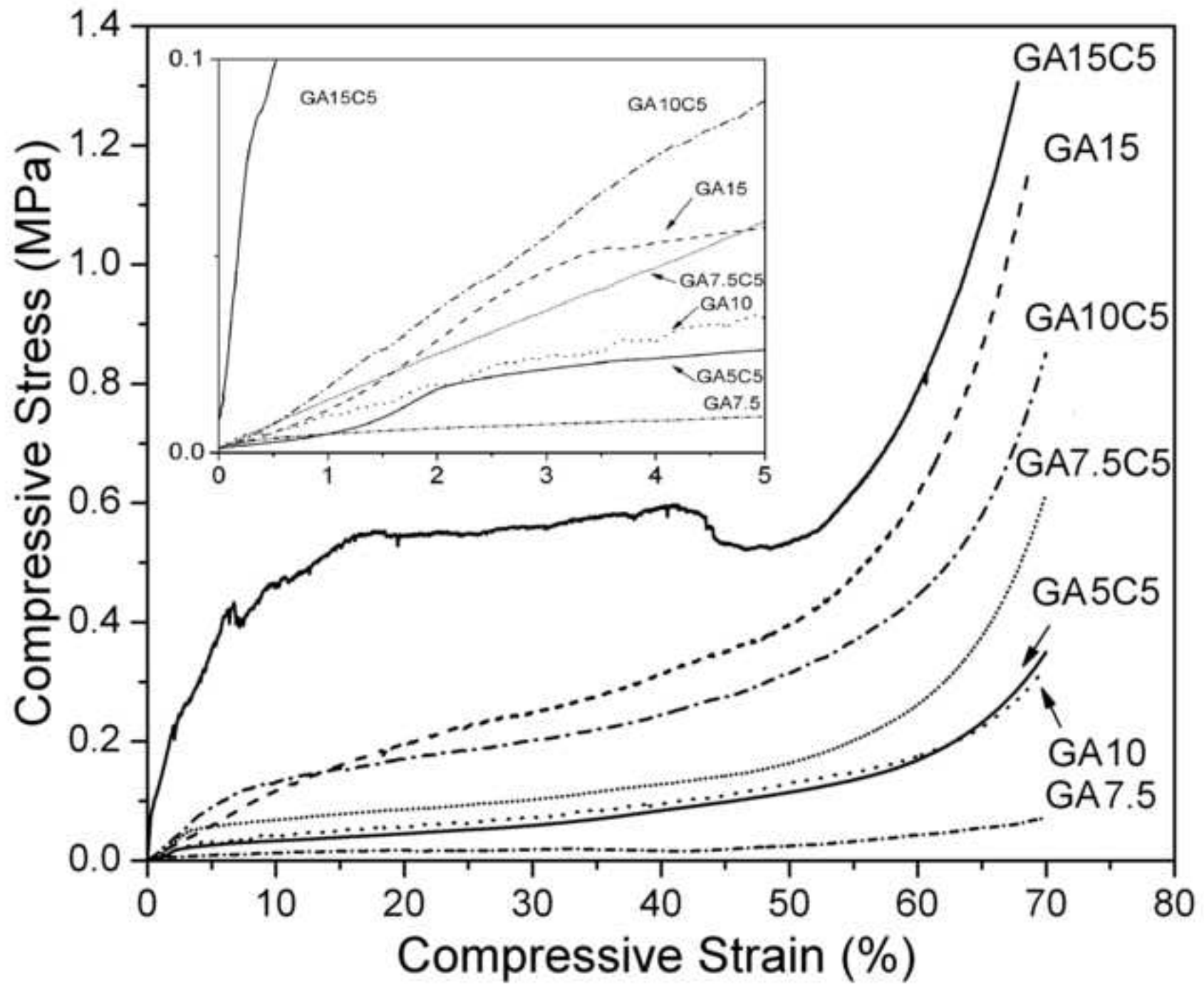


Figure 4

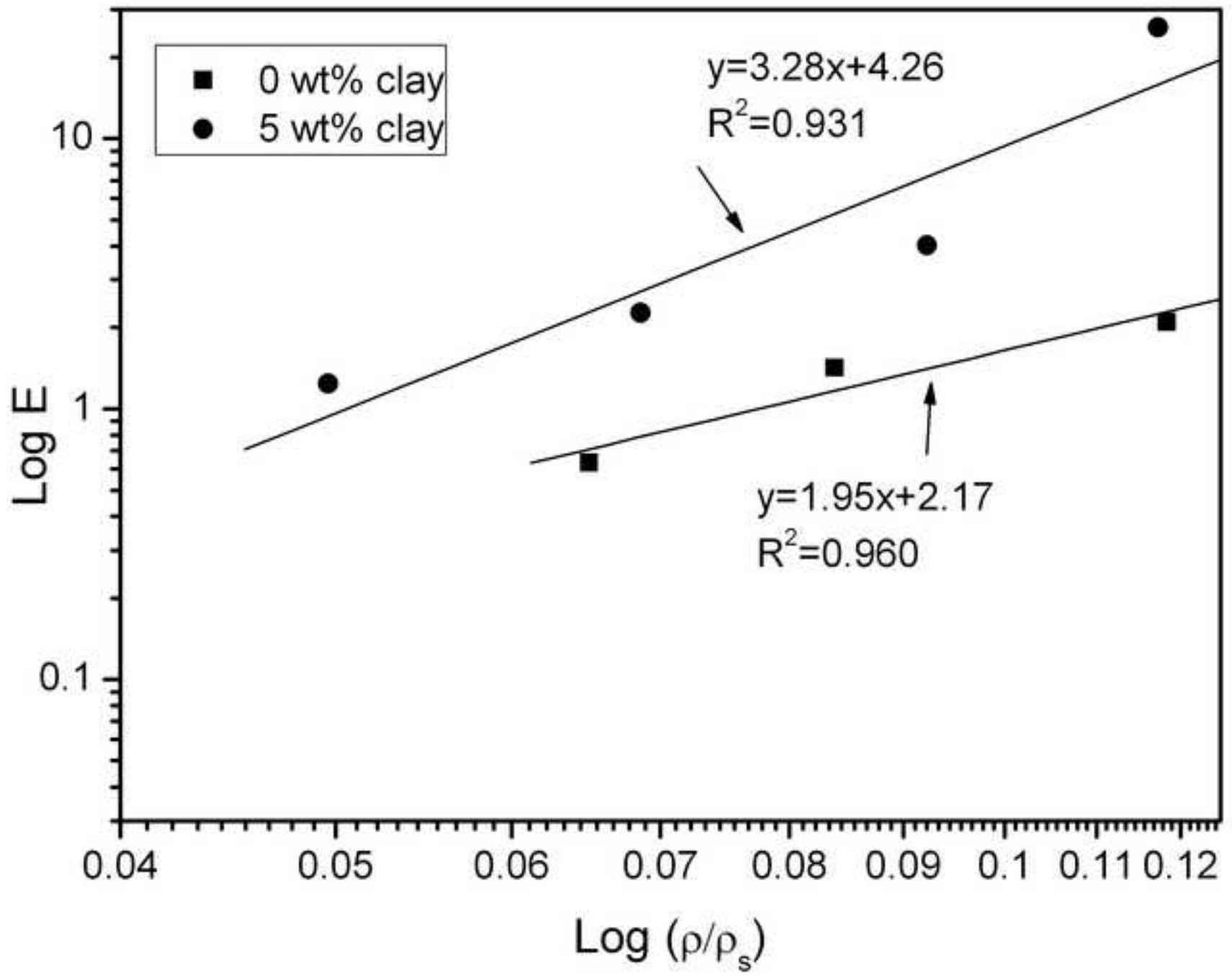


Figure 5

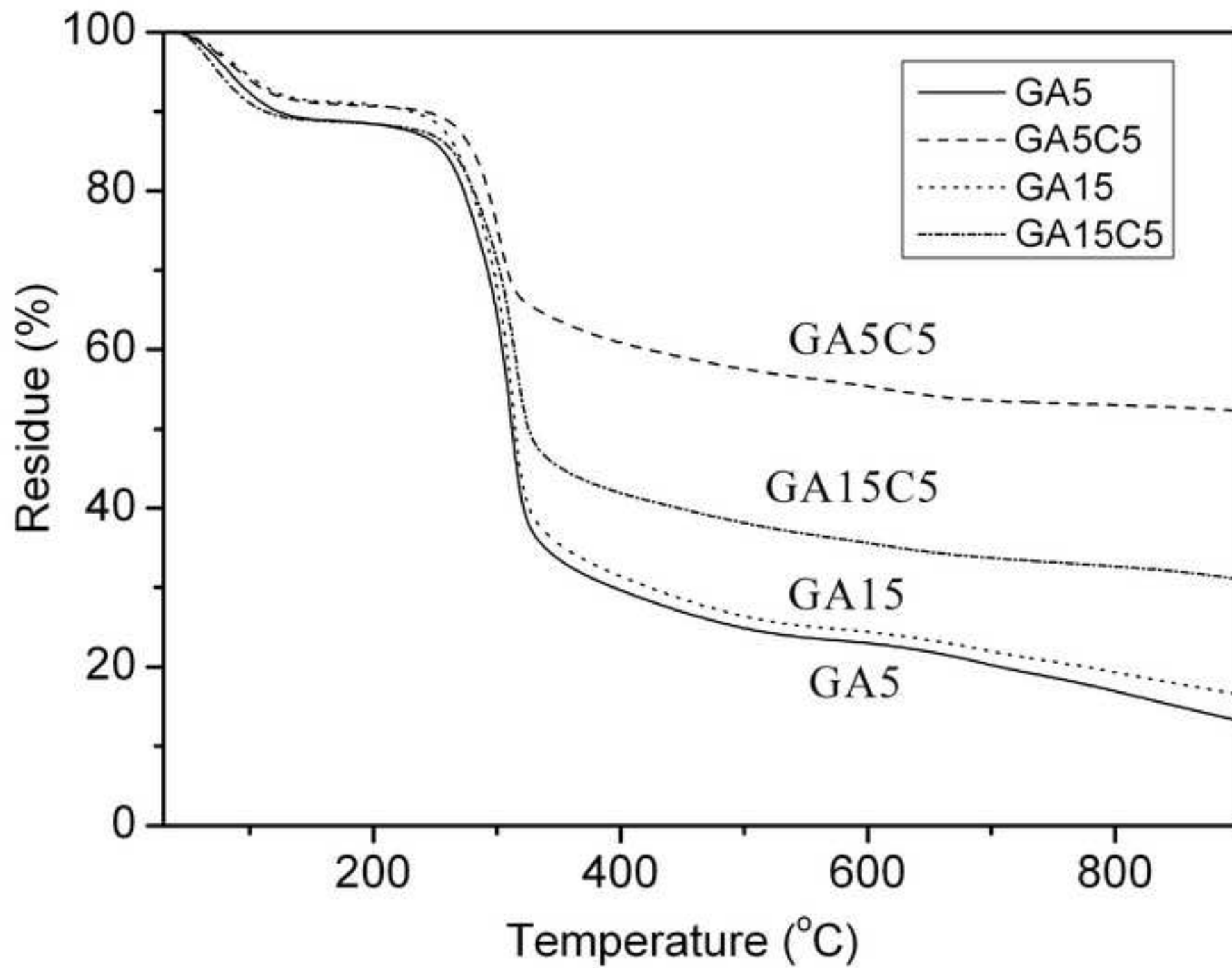


Figure 6

