



<b>Title</b>	<b>Roughness-sublayer correction for the profiles of mean velocity and turbulence over urban areas</b>
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<b>Citation</b>	<b>The Croucher Advanced Study Institute (ASI) Programme 2015-2016: Changing Urban Climate &amp; the Impact on Urban Thermal Environment and Urban Living, The Chinese University of Hong Kong, Hong Kong, 7-11 December 2015.</b>
<b>Issued Date</b>	<b>2015</b>
<b>URL</b>	<b><a href="http://hdl.handle.net/10722/235025">http://hdl.handle.net/10722/235025</a></b>
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# Roughness-sublayer correction for the profiles of mean velocity and turbulence over urban areas

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## Background

- Monin-Obukhov similarity theory (MOST) applies in inertial sub-layer (ISL) but fails in roughness sub-layer (RSL) because the flow structure in RSL is highly inhomogeneous.
- Extrapolation of the conventional logarithmic law of wall into the RSL likely overlooks the inhomogeneity.
- Need for an analytical expression for mean velocity profile and ventilation estimate, including a new RSL correction, that is applicable over the urban boundary layer.

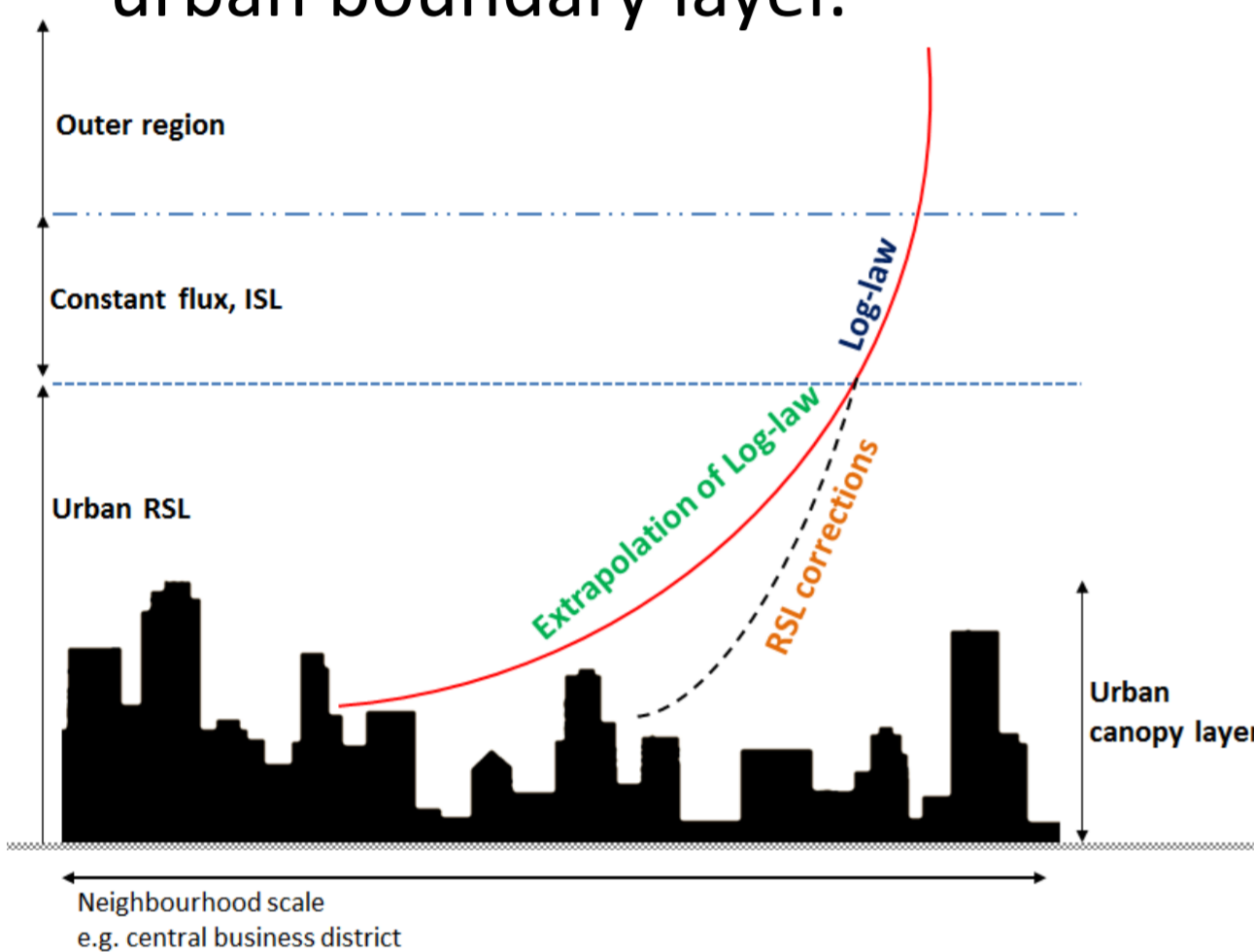


Figure 1: Schematic of different layers of the urban boundary layer, including the RSL and the ISL.

## Analytical Expression for RSL flow correction

### Assumptions:

- $\Phi_m (= \phi_m \hat{\phi}_m)$  is a generalised similarity function of ISL & RSL
- Flows above urban canopy in neutral stratification ( $\phi_m = 1$ )
- $\Phi_m$  is a function of the roughness elements that is independent from the MOST length scale  $L$

$$\Phi_m = \phi_m \hat{\phi}_m = \hat{\phi}_m \left( \frac{z}{z^*} \right) \quad z \text{ is the elevation \& } z^* \text{ the RSL height.}$$

The gradient of the wind profile in dimensionless form is,

$$\frac{du}{dz} = \frac{u^*}{\kappa z} \hat{\phi}_m \left( \frac{z}{z^*} \right) \quad u \text{ is the wind speed, } u^* \text{ the friction velocity \& } \kappa (= 0.41) \text{ the von Kármán constant.}$$

Rearrange & integrate yields,

$$\frac{\kappa}{u_*} u|_{z-d} = \ln \left( \frac{z-d}{z_0} \right) + \int_{z-d}^{\infty} \frac{1-\hat{\phi}_m}{z} dz \quad d \text{ is the displacement height \& } z_0 \text{ the roughness length scale.}$$

We employ the (continuous) function of  $\hat{\phi}_m$

$$\hat{\phi}_m(z) = 1 - e^{-\mu(z/z^*)} \quad \mu \text{ is an empirical constant.}$$

Use series expansion to calculate the exponential integral, an analytical expression for the urban RSL effects is formulated

$$\frac{u|_{z-d}}{u^*} = \frac{1}{\kappa} \left[ \ln \left( \frac{z-d}{z_0} \right) - \gamma - \ln \left( \mu \frac{z-d}{z^*} \right) - \sum_{n=1}^{\infty} \frac{(-1)^n (\mu \frac{z-d}{z^*})^n}{n \cdot n!} \right]$$

$\gamma (\approx 0.57721)$ :  
Euler constant.

ISL

RSL

## Wind Tunnel Measurements

- The open-circuit type wind tunnel at the Department of ME, HKU was used with neutral stratification and a reference wind speed of  $9 \text{ m s}^{-1}$
- Idealised 2D-roughness elements with different aspect ratio ( $AR = h/b$ ) were used to simulate the urban areas
- Cross-wire hot-wire measurements were performed

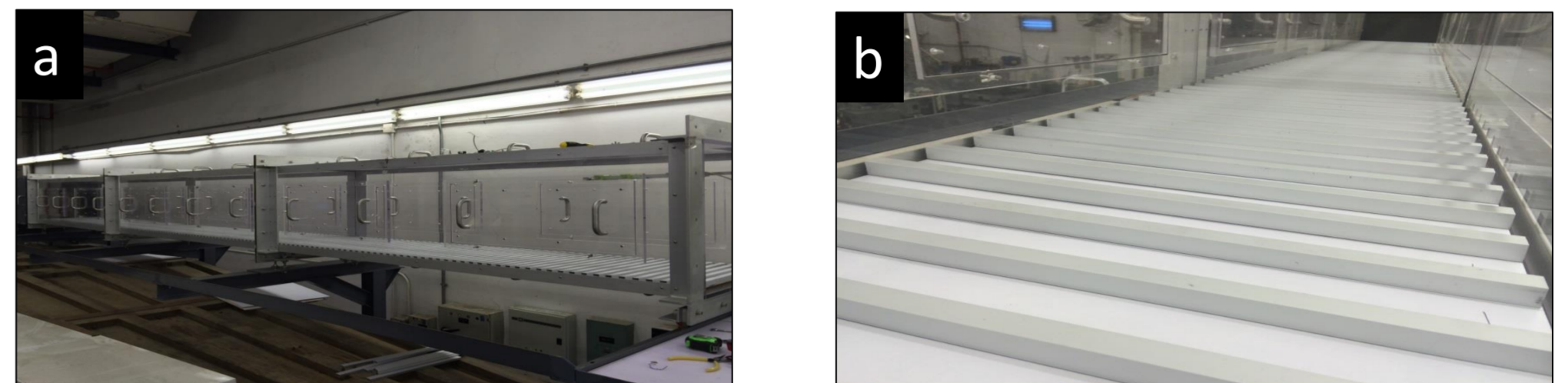


Figure 2. a) Open-circuit wind tunnel at the Department of Mechanical Engineering, HKU, b) Idealised urban area with aspect ratio ( $h/b = 1/3$ )

## Flows and Ventilation Estimates over Idealised Urban Areas

- Flow inhomogeneity over idealised urban areas is revealed (Fig. 3a)
- RSL & ISL are clearly identified
- The newly proposed analytical expression performs well in both RSL & ISL for the prediction of velocity profiles over a wide range of aspect ratios,  $0.5 < ARs < 0.083$  (Fig. 3c)
- Friction factor  $f$  & vertical velocity scale  $\hat{w}$  are used to parameterise ventilation performance over urban areas with RSL corrections (Fig. 3b)

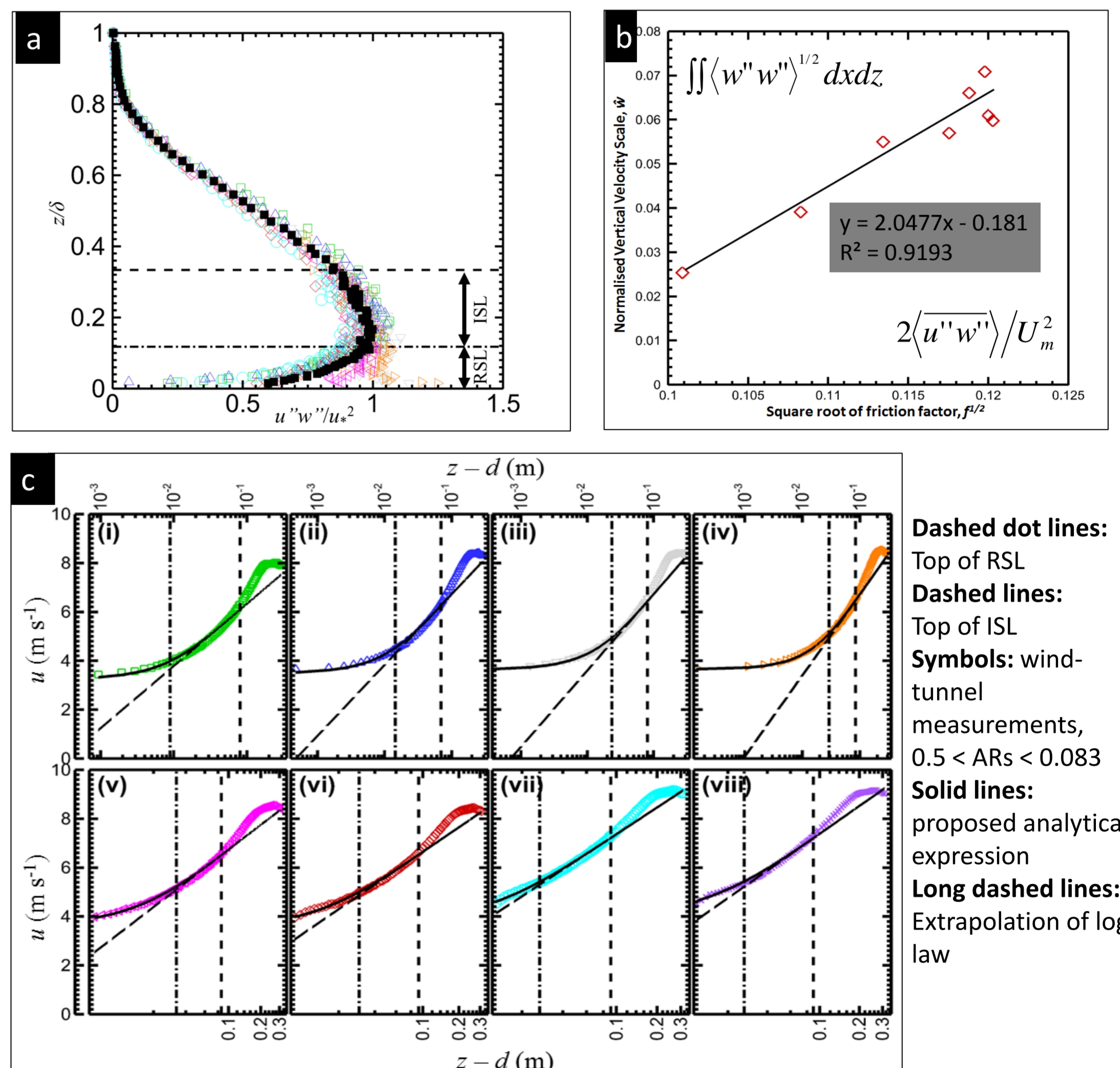


Figure 3. a) Normalised Reynolds stress profiles for  $AR = 0.25$ , b)  $f^{1/2}$  against  $\hat{w}$ , c) Comparison of velocity profiles between wind tunnel measurements the newly proposed analytical expression.

## Next steps

- Tests with additional roughness elements of different forms using wind tunnel experiments, i.e. cube roughness, building height variability or realistic city models.
- Quantify the effect of aerodynamic roughness on RSL flows.
- Examine the RSL turbulence using mixing length models.

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