Paper-based Enzymatic Microfluidic Fuel Cell: From a two-stream flow device to a single-stream lateral flow strip

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Abstract

This work presents a first approach towards the development of a cost-effective enzymatic paper-based glucose/O₂ microfluidic fuel cell in which fluid transport is based on capillary action. A first fuel cell configuration consists of a Y-shaped paper device with the fuel and the oxidant flowing in parallel over carbon paper electrodes modified with bioelectrocatalytic enzymes. The anode consists of a ferrocenium-based polyethyleneimine polymer linked to glucose oxidase (GOx/Fc-C₆-LPEI), while the cathode contains a mixture of laccase, anthracene-modified multiwall carbon nanotubes, and tetrabutylammonium bromide-modified Nafion (MWCNTs/laccase/TBAB-Nafion). Subsequently, the Y-shaped configuration is improved to use a single solution containing both, the anolyte and the catholyte. Thus, the electrolytes pHs of the fuel and the oxidant solutions are adapted to an intermediate pH of 5.5. Finally, the fuel cell is run with this single solution obtaining a maximum open circuit of 0.55 ± 0.04 V and a maximum current and power density of $225 \pm 17 \ \mu A \ cm^{-2}$ and $24 \pm 5 \ \mu W \ cm^{-2}$, respectively. Hence, a power source closer to a commercial application (similar to conventional lateral flow test strips) is developed and successfully operated. This system can be used to supply the energy required to power microelectronics demanding low power consumption.

Keywords

Paper-based biofuel cell Enzymatic Microfluidic

1. Introduction

Since their first appearance in the literature, microfluidic fuel cells have shown their potential for supplying power to small portable electronic devices. They are simple to operate provided that an external pressure system is coupled to the device to maintain separate flow between the anode and cathode reactants without mixing. This avoids the need for a separation membrane, typically Nafion, reduces internal ohmic losses [1], and allows for the use of different pHs at the anolyte and catholyte streams with little reagent crossover issues [2, 3]. However, the need for external pressure sources, like pumps, limits their portability and miniaturization severely [4]. Furthermore, these external pumps represent an extra energy consumption associated with the fuel cell. Although the first generation of microfluidic fuel cells was fabricated with MEMSrelated technologies, it has been demonstrated in the last years that they can also be easily made in glass or plastic [1, 5-7] using rapid prototyping techniques. Moreover, the need for external pumping has been recently overcome with the emergence of microfluidic paper devices [8-13]. These devices substitute classical microfabricated channels by a paper matrix, which provides important benefits. Paper possesses the ability to move fluids via capillary action, allowing passive liquid transport [14]. As a result, no ancillary devices are needed to supply pumping functions. Furthermore, paper presents good compatibility with a high number of chemicals/biochemicals and can be combined with other low cost materials, such as plastics, to provide extra mechanical support.

For many years, paper has been widely employed as a substrate to develop point of care (POC) diagnostics devices [15]. Among them, the most broadly used POC diagnostic devices are paper-based dipsticks (urinalysis dipsticks) and lateral-flow immunoassays (pregnancy tests) [16-19]. Lately, materials used in lateral flow devices have been adapted and reconfigured into 2D or 3D paper matrices. This has led to the creation of new and exciting components, for example valves, mixers and separators [20]. In this way, the capabilities of complex microfluidic functions and the simplicity of diagnostic tests strips have been combined to originate a new generation of paper-based analytical devices (μ PADs) [21-25]. These systems have been identified as especially suitable for point of care purposes in the field of home health-care settings and at medical points of care in developing countries [10, 12, 26, 27]. This is

because they promise to accomplish the ASSURED criteria; they are affordable, sensitive, specific, user-friendly, rapid and robust, equipment free and deliverable to those who need it [21, 25, 28]. Nevertheless, the quantification of the results of a test requires the use of a handheld reader which, in certain scenarios, is not a cost effective solution. This has brought the idea of developing low cost disposable readers; however, examples in the literature are still very scarce. To realize this vision, the search for a new generation of power sources that satisfy the requirements such as high power density, low cost and disposability with minimum environmental impact has attracted a lot of attention. In the last few years, paper has been used as a substrate to develop different kinds of power sources [29], for instance (i) fuel cells [8, 9], (ii) biofuel cells, such as microbial [30, 31] and enzymatic fuel cells [32, 33], (iii) electrochemical batteries [10, 34, 35], (iv) lithium-ion batteries [36], (v) supercapacitors [37, 38] and (vi) nanogenerators [39]. Among these, biofuel cells [40], and specifically enzymatic fuel cells, appear to be one of the most suitable power sources for paper-based µPADs in terms of environmental impact. This is because they use biological catalysts (enzymes) to convert organic fuels (commonly glucose) and oxygen into electrons, CO2, water and/or oxidized fuel by-products [41-44]. For these reasons, enzymatic fuel cells are considered extremely cost-effective and a promising future alternative source of sustainable electrical energy for small electronic devices [42, 45-48].

An intrinsic advantage of paper-based matrixes as substrates for microfluidic fuel cells is their capability of establishing laminar flow. This feature is important when considering microfluidic fuel cells as it means that, fuel and oxidant streams can flow in parallel without mixing.

In this work, we will show that the implementation of a microfluidic enzymatic fuel cell in paper allows us to eliminate the need for pumps without losing electrical performance. In order to gain simplicity in its use, the two inlets typically used in a Y-shaped fuel cell have been simplified into one inlet, so that the fuel and the electrolytes could be added together in a single step. This results in a fuel cell working with the simplicity of lateral flow test strips. This replaces the two parallel flow solutions by a single one that combines the anolyte and the catholyte components. In order to achieve this ease of use, the fuel cell has to work with a single electrolyte which required a compromise in the pH values between anolyte and catholyte solutions. Free from the size restrictions and power requirements of external equipment, the system presented in this paper can become an alternative for providing energy to power small single use point-of-care devices [49].

2. Experimental

2.1. Fuel cell design and fabrication

Two different microfluidic devices were constructed using paper, a Y-shaped and an I-shaped fuel cells. The paper selected as substrate for the systems was Whatman[®], grade Fusion 5, due to its high wicking rate. The system was designed using Vectorworks 2012 student edition (Techlimits, Spain). The paper sheet was attached onto a flexible plastic carrier covered with a low-strength adhesive layer to provide mechanical support during the cutting process. The paper strips were cut using a Roland GX-24 cutter plotter with a force and speed of 30 g and 1 cm s⁻¹, respectively, and the cutting was performed in two passes in order to prevent any tearing of the paper [50]. The thickness of the Fusion 5 substrate (and consequently the height of the microfluidic channel) was 370 μ m and the fuel cells had final dimensions of 45 x 5 mm². After cutting, the paper structures were released from the plastic support.

Carbon paper from Fuel Cell Earth (type TG-H-060) was used as the electrodes of the fuel cells. They were cut in a rectangular size of $5 \times 15 \text{ mm}^2$ and positioned in parallel 2 cm downstream (from the reactant inlets) and separated 1 mm from each other. In this configuration, the active electrode area exposed to the microfluidic channel is 0.10 cm^2 . A piece of a conducting copper tape (3M-1182) purchased from RS (Spain) was used to contact the outer part of the carbon paper electrodes. Fig. 1 (a) and (b) shows the pictures of the Y-shaped and the I-shaped paper strips together with the carbon paper electrodes.



Fig. 1 (a) Y-shaped and (b) I-shaped paper fuel cells fixed on glass slides, displaying carbon paper electrodes attached to a piece of cooper foil.

2.2. Microfluidic device assembly

A holder made of poly(methyl methacrylate) - PMMA - was designed and made with a Roland MDX-40 milling machine (Roland DG, Spain). This component was fabricated to facilitate the connection of different elements of the measurement setup to the fuel cell. A pocket milled into the holder was used to hold the glass slide that supports de paper fuel cell. Two adhesive magnetic bands, placed on the sides of the PMMA block, allow fixing a PMMA bar with two fuel reservoirs at the paper inlets. Also the fuel cell wicking pad (an absorbent wipe from Kimtech Science) and the external electrical connections of the device are held by PMMA pieces. All of these plastic components host small magnets that keep them attached to the holder. For the external electrical connections, spring-loaded pins (Preci-Dip, Switzerland) were inserted in the PMMA plugs that at the same time were in contact with the copper foil over the electrodes.

2.3. Equipment and chemicals used in the enzymatic solutions

The salts acting as supporting electrolyte, the enzymes for the electrodes (Glucose oxidase from *Aspergillus niger* –EC 1.1.3.4, Type X-S, 175 units/mg of solid, 75% protein– and laccase from *Trametes Versicolor*), glucose, Nafion and solvents were purchased from Sigma Aldrich and used as received. The proton conducting binder was Nafion 5% by wt. in an alcoholic suspension EW1100. Hydroxylated MWCNTs (10–30 µm length, 1.6% –OH functionalization) were acquired from cheaptubes.com and used as received. Ethylene glycol diglycidyl ether (EGDGE) was purchased from Polyscience Inc. (Warrington, USA). 2-Anthracenecarboxylic acid was obtained from TCI chemicals and used as received.

The redox polymer $Fc-C_6$ -LPEI used at the anode along with the glucose oxidase was synthesized as previously reported [51]. Tetrabutylammonium bromide (TBAB)-modified Nafion was prepared as previously reported [52]. Anthracene-2-carbonylchloride for anthracene-modified MWCNTs was synthesized as per previously published procedures [53, 54].

Phosphate buffer was prepared with sodium phosphate dibasic, sodium phosphate monobasic and sodium nitrate (Na₂HPO₄, NaH₂PO₄ and NaNO₃) for a final concentration of 100 mM. The pH of the buffer was adjusted with hydrochloric acid and sodium hydroxide (HCl and NaOH) to match the optimal pH required by the enzymes. A 1 M stock glucose (α -D(+)-glucose) solution in distilled water was prepared 24 hours before use and stored at 4°C to allow it to mutarotate.

Electrochemical measurements were conducted with a CH Instruments electrochemical workstation model 650A (Austin TX). Ag/AgCl electrode (saturated KCl) and a commercial platinum electrode were used as reference and counter electrodes, respectively. All of the experiments were carried out at room temperature.

2.4. Enzymatic bioelectrode modification

The carbon paper electrodes were functionalized depositing polymer/enzyme solutions on them prior to their incorporation in the microfluidic fuel cell. The chemicals used to obtain the biocatalytic solutions and the process for preparing the enzyme-mixture inks are described below. The electrolyte solutions and the fuel used to run the fuel cell are also listed.

For the anodic side, the enzymatic solution was prepared with the blend of 3 μ l of enzyme glucose oxidase (10 mg ml⁻¹ in distilled water), 7 μ l of redox polymer Fc-C₆-LPEI (10 mg ml⁻¹ in distilled water) and 0.4 μ l of the crosslinker EGDGE (10% v/v). All of the previous components were mixed together by vortexing.

The cathodic solution was prepared by dissolving 1.5 mg of laccase enzyme in 74 μ l of 100 mM phosphate buffer at pH 7, 7.5 mg of anthracene modified MWCNT's and 25 μ l of TBAB-modified Nafion. The above components were sonicated and vortexed intermittently until the mixture was completely suspended.

Then, 10 mm² of carbon paper electrode was modified with 42 μ l of the corresponding enzymatic mixture by drop-casting. The electrodes were allowed to dry for 24 hours at room temperature and after this they were positioned side by side over the paper substrate with its catalytic side in contact with the paper strip. Fig. 2 shows a scheme of the reactions taking place in our biofuel cell. For clarity, the voltages associated with the reactions (*vs.* Ag/AgCl reference electrode) obtained experimentally have been added.



Fig. 2 Depiction of the glucose/ O_2 biofuel cell after enzymatic drop-coating with the reactions taking place. The figure represents the flow of electrons from the oxidation of glucose to the reduction of oxygen, showing the potentials involved in the reactions *vs.* Ag/AgCl [7, 51, 55, 56].

3. Results and discussion

3.1. Operation of the Y-shaped flow paper fuel cell

Microfluidic fuel cells made on paper rely on the capillary flow of reactants to cause the movement of liquids without external pressure sources. Generally, this is accomplished by attaching an absorbent pad at one end of the paper strip. Then, when a fluid is applied in the device inlet, the liquid moves through the strip until the liquid fill it and reaches the wicking pad. From this point, the flow regime is called fully-wetted [57]. In our particular case, when the advancing liquid front reaches the pad, the liquid exits a region of only 370 μ m thick (the strip) and enters a second porous region that is typically >1000 μ m thick (the combined thickness of both the strip and the pad). From this point, a sustained flow across the strip is established [58] and the flow rate inside the paper matrix decreases from an initial value of 33.5 ul.min⁻¹ to 5ul.min⁻¹ in a lapse of 100 min, which results in an average decrease rate of 0.28 ul.min⁻¹. Therefore, liquid flow rates can be estimated depending on the time interval selected to perform the experiments.

After enzymatic electrode modification, the Y-shaped paper microfluidic fuel cell is assembled in the PMMA holder shown in Fig. 3. For the fuel cell characterization, the electrolytes are selected with a pH that is the optimum for each enzyme. Specifically, sodium phosphate buffer at pH 7.4 with 100 mM glucose is applied to the anodic side, whereas phosphate buffer at pH 4.5 is introduced as the catholyte. Polarization experiments are performed with these solutions and the obtained curves are represented in Fig. 4. As it can be observed, the open circuit voltage is 0.6 ± 0.05 V and the maximum current and power densities are $320 \pm 30 \ \mu$ A cm⁻² and $45 \pm 9 \ \mu$ W cm⁻² (at 0.23 V), respectively. Data is taken within the first 15 minutes after application of anolyte and catholyte solutions to the fuel cell. According to the values obtained from paper flow characterization (see the supplementary information for further explanation of fluid transport in paper devices) flow rates inside the paper can be considered to range from 30 to 20 μ l min⁻¹ during the time interval of the experiments.



Fig. 3 Y-shaped paper-based fuel cell showing the different parts forming the experimental setup for measurements.

In order to compare the power output obtained using paper to drive the fluid with the ones obtained with a pumped microfluidic fuel cell, the maximum power densities obtained in previous published results [7] (at the same flow rates) are depicted with dashed lines in the polarization curve of Fig. 4. It can be seen that the power output achieved with the paper fuel cell is similar to the values previously obtained with the active microfluidic fuel cell (at 20 μ l min⁻¹ and 25 μ l min⁻¹ the power is 41 μ W cm² and 48 μ W cm², respectively). These results demonstrate that the paper fuel cell performance, when using the same enzymatic electrodes, lies within the range of levels from the syringe pump range. Furthermore, since no energy is spent in pumping the solutions, all of the power generated can be considered as net power. Thus, our paper device represents an important simplification as compared with the typical microfluidic fuel cells that use syringe pumps.



Fig. 4 Polarization and power curves for the Y-shaped microfluidic fuel cell measured at a time compressed between 10 to 15 minutes (representing a flow velocity of 20-25 μ l min⁻¹). Dashed lines show the power density values for the same ranges of velocities for a fuel cell using a syringe pump instead of the capillary of paper.

3.2. Bioelectrode characterization at different pHs

In order to gain simplicity in fuel cell operation, the two inlets of the Y-shaped fuel cell can be merged into only one, so that the fuel and the electrolytes can be added together in a single step. This would result in a fuel cell working with the simplicity of lateral flow test strips. In order to achieve this simplicity, the fuel cell has to work with a single electrolyte which requires us to find a compromise in the pH values between anolyte and catholyte solutions. In our Y-shaped device, the fuel cell electrolytes had the optimum pH for each enzyme (i.e. the pH at which enzyme activity is maximized) corresponding to a pH of 4.5 for laccase and 7.4 for glucose oxidase.

With the objective of determining the pH at which laccase and glucose oxidase can operate losing the minimum overall fuel cell performance, glassy carbon electrodes (BASi, West Lafayette, IN) are modified with the appropriate enzyme-solution (depending if they are working as anode or cathode) and their electrochemical responses are studied at different ranges of pH.

The catalytic behaviour of the modified glassy carbon electrodes are measured in 100 mM phosphate buffer with 100 mM glucose by cyclic voltammetry. The pH of the buffer is varied between 4.5 and 7.4 using HCl or NaOH when required. Laccases optimally operate in slightly acidic solutions, at pH values ranging from 3 to 5 [59]. In contrast, glucose oxidases show their better responses around neutral pH values [55]. The voltammograms of the bioelectrodes are recorded and peak currents are extracted from each curve. Fig. 5 shows the obtained values of

the current density curves achieved at the bioanode and the biocathode, where it can be observed that an intermediate pH value for both enzymes can be set at around 5.5.



Fig. 5 pH analysis of glassy carbon electrodes modified with the corresponding biocatalytic solution. Representation of the influence of pH on the current density at room temperature in buffer phosphate at 100 mM and 100 mM glucose. Red line, biocathode behavior. Black line, response of the bioanode. The experiments are repeated three times and the error bars correspond to the standard deviation.

Glassy carbon modified electrodes based on glucose oxidase (bioanode) or electrodes based on laccase (biocathode) differ considerably depending on the pH of the electrolyte used. These results corroborate that the fuel cell yields the best performance when pH of the electrolytes are 7.4 at the anode and 4.5 at the cathode. The current densities under these conditions are $635 \pm 95 \ \mu A \ cm^{-2}$ and $180 \pm 60 \ \mu A \ cm^{-2}$, respectively. These results indicate that the fuel cell is limited by the cathode performance, probably due to the low concentration of dissolved O₂ as well as by the lower activity of the laccase as compared with the glucose oxidase.

A comparison of the linear sweep voltammograms of the bioelectrodes working at pH 5.5 and at its optimum pH are represented in Fig. 6. At pH 5.5, the bioanode (Fig. 6 (a)) shows a current density corresponding to $269 \pm 30 \ \mu A \ cm^{-2}$. At the cathode (Fig. 6 (b)) the current density is 120 $\pm 35 \ \mu A \ cm^{-2}$, displaying a shift of about 0.05 V of the oxygen reduction potential towards a more negative potential when the solution at pH 5.5 is saturated with air.



Fig. 6 Representative linear sweep voltammograms of enzymatic GC electrodes at 5 mV s⁻¹. (a) GOx/Fc-C₆-LPEI bioanodes in 100 mM sodium phosphate at pH 7.4 (red), at pH 5.5 (green) and without glucose (dotted line). (b) An-MWCNTs/laccase/TBAB-Nafion biocathode in 100 mM sodium phosphate in air saturated conditions at pH 4.5 (red), at pH 5.5 (green) and in N₂-saturated conditions (dotted line).

3.3. Operation of the single-stream paper fuel cell.

The performance of the I-shaped paper fuel cell (shown in Fig. 1(b)) is measured in a solution consisting of a mixture of phosphate buffer at the intermediate pH of 5.5 and 100 mM glucose. The resulting polarization and power curves are represented in Fig. 7. For comparison, the polarization and power curves that are previously obtained using the Y-shaped fuel cell are added as well. The I-shaped fuel cell yields an open circuit voltage around 0.55 V \pm 0.04, a slightly lower value than that at the Y-shaped system. This is probably due to the potential shift in the oxygen reduction reaction that can be observed at Fig. 6 (b). The maximum current and power density of the I-shaped fuel cell are 225 \pm 17 µA cm⁻² and 24 \pm 5 µW cm⁻², respectively. This corresponds to a power output drop of almost 50% compared to the Y-shaped fuel cell in which the optimum pH for each enzyme is used.



Fig. 7 Polarization and power curves of two enzymatic paper-based fuel cells. Solid line shows the performance of the two stream fuel cell (Y-shaped) working with buffer phosphate at pH 4.5 at the cathode and pH 7.4 with 100 mM at the anode. Dotted lines correspond to the one stream fuel cell (I-shaped) working with a single solution of sodium phosphate at pH 5.5 with 100 mM glucose.

In summary, it is demonstrated that the single stream enzymatic paper-based fuel cell is able to work properly despite showing lower performance as compared with the Y-shaped fuel cell. However, the fuel cell format presented is much closer in design to lateral flow test strips which gives to the system important advantages toward commercial applications [8].

Conclusions

In this paper, we have demonstrated that it is possible to run a paper-based microfluidic fuel cell producing about the same power output as the microfuel cell presented in previously published work [7], where an external syringe pump was used for the supply of reactants. Our fuel cell represents a great simplification as compared to the previous one, as it allows us to obtain electrical power without any ancillary devices. Second, the system was further simplified. For this purpose, the paper-based fuel cell was operated using a single solution instead of the two streams employed in conventional Y-shaped fuel cells. That implied the need of finding a compromise between anolyte and catholyte pHs, a value that was set at 5.5, after carefully studying the enzymatic performance of the bioelectrodes at different solution pHs.

The single stream fuel cell was characterized at 100 mM glucose in an electrolyte at pH 5.5. The values obtained were: 0.55 V at the open circuit voltage, a maximum current density of $225 \pm$

17 μ A cm⁻² and a maximum power density of 24 ± 5 μ W cm⁻² (at 0.19 V). Although the efficiency of the system decreases compared with the Y-shaped microfluidic fuel cell, the single-stream configuration is much easier to be implemented in a real application.

Finally, the presented fuel cell performance and its simplicity of operation inspires the possibility of using ubiquitous fuel sources to generate power [60]. In this context, soft drinks (whose pH range from 3 to 6) can be used to generate electrical energy and feed small electronic devices because they are cheap, broadly available and have high contents of sugar.

In conclusion, the enzymatic paper-based microfluidic fuel cell presented here exhibits multiple benefits as compared with traditional microfluidic fuel cells. On the other hand, the limited lifetimes of enzymes restrict their application to portable power devices where long-term operation is not required [42, 61]. In this sense, associating these biological fuel cells with the advantage of paper networks can be significant for developing inexpensive, mass-producible, and portable diagnostic devices.

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