# 1 Cherry stones-based activated carbons as potential adsorbents for CO<sub>2</sub>/CH<sub>4</sub>

# 2 separation: Effect of the activation parameters

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# 5 Abstract

6 A low-cost biomass, cherry stones (CS), was used as carbon precursor to synthesize two activated carbons to be used for CO<sub>2</sub>/CH<sub>4</sub> separation. Single-step 7 8 activation with two activating agents, carbon dioxide and steam, was used. The 9 activation conditions that maximize the CO<sub>2</sub> adsorption capacity by the adsorbents at 10 25 °C and atmospheric pressure were determined by response surface methodology 11 (RSM). The optimum values were 885 °C and 12% of solid yield when activating with 12 carbon dioxide, but 850 °C and 15.3% of solid yield when activating with steam. 13 Heating rate did not show a significant effect on the CO<sub>2</sub> uptake. CO<sub>2</sub> adsorption 14 capacity values up to 11.45 and 10.56 wt.% were achieved under such conditions using 15 carbon dioxide and steam as activating agents, respectively. Carbon dioxide activation 16 promoted the development of microporosity, whereas both micropores and mesopores 17 were developed during steam activation. The CO<sub>2</sub>/CH<sub>4</sub> separation performance at 3 bar 18 of the optimum adsorbents indicated that both cherry stones-based activated carbons 19 could have great potential as CO<sub>2</sub> adsorbents for CO<sub>2</sub>/CH<sub>4</sub> separation. The adsorbent 20 activated with carbon dioxide, CS-CO<sub>2</sub>, showed a slightly higher adsorption capacity, 21 but the steam activated sample, CS-H<sub>2</sub>O, had an enhanced selectivity to separate CO<sub>2</sub> 22 from CO<sub>2</sub>/CH<sub>4</sub> binary mixtures.

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*Keywords*: Activated carbon; Cherry stones; CO<sub>2</sub>/CH<sub>4</sub> separation; CO<sub>2</sub> uptake;
 Response surface methodology

#### 25 1 INTRODUCTION

Biogas is produced from the decomposition of organic wastes, and is rich in CH<sub>4</sub> (35-75 vol.%). Its release into the atmosphere largely contributes to greenhouse gas concentration. However, the energetic content of the biogas is high (higher heating value of 15-30 MJ Nm<sup>-3</sup>) and its exploitation involves significant revenues or avoided costs.<sup>1</sup>

31  $CO_2$  is present in the biogas in large quantities (almost balanced to the 32 percentage of CH<sub>4</sub>), and as it is an inert gas in terms of combustion, it decreases the 33 energetic content of the biogas. The main technology used for enriching biogas in CH<sub>4</sub> 34 by means of  $CO_2$  separation is pressure swing adsorption (PSA) on zeolites, due to their 35 high selectivity towards CO<sub>2</sub>. Nevertheless, activated carbons (ACs) can be promising 36 materials for CO<sub>2</sub>/CH<sub>4</sub> separation due to their high adsorption capacity at atmospheric 37 pressure, hydrophobic character, significant lower cost than zeolites, high surface area and amenability to pore structure modification and surface functionalization.<sup>2</sup> 38 39 Moreover, a lower amount of energy is needed to regenerate activated carbons 40 compared to zeolites. Some of the requirements that need to fulfil the ACs in order to be 41 competitive materials for CO<sub>2</sub>/CH<sub>4</sub> separation purposes are availability, high stability, 42 ease of regeneration and low cost, as well as high CO<sub>2</sub> selectivity and adsorption capacity. Carbon adsorbents can be obtained at low cost if a renewable, relatively 43 44 abundant and globally available source, such as biomass, is used as precursor material.

45 The production of carbon adsorbents from biomass precursors can involve 46 physical or chemical activation to develop the porosity.<sup>3</sup> The adsorption capacity of an

47 AC is mainly dependent on its pore structure. In the present work, physical activation 48 was selected due to its lower energy consumption and processing time, as well as it has 49 a lower environmental impact when using CO<sub>2</sub>, H<sub>2</sub>O or air as activating agent. Physical 50 activation is generally carried out in a two-step procedure: carbonization and activation. 51 Single-step activation has been less explored, although good adsorption characteristics 52 for removal of NO<sub>2</sub> from air or pollutants from water have been reported in literature 53 after biomass activation by a single-step procedure using CO<sub>2</sub> or steam as activating agents.<sup>4-7</sup> Single-step activation was therefore selected in the present work for preparing 54 55 cherry stones-based activated carbons.

56 Every carbon precursor requires specific activation conditions, and so an 57 increase in the activation degree could only be justified if a significant improvement in 58 the adsorption capacity of the adsorbent was observed. Therefore, CO<sub>2</sub> adsorption on 59 the activated carbons prepared in the present work was optimized in relation to 60 temperature, heating rate and solid yield during the single-step activation by means of 61 response surface methodology (RSM). RSM is a statistical technique which has lately been applied in research related with CO<sub>2</sub> capture to evaluate the effects of several 62 factors and determine the optimum conditions for the studied process.<sup>8,9</sup> It uses the 63 design of experiments and the multiple regression analysis to model the relationship 64 between several independent variables and a response variable.<sup>10</sup> 65

66 The commercial synthesis of activated carbons is currently demanding cheap,
67 easily accessible and widely available precursors. An agricultural by-product, such as
68 cherry stones (CS), is abundant in Spain, especially in the regions of Extremadura and
69 Aragón, from the industrial production of Kirsch (cherry brandy) and jam. The cherry
70 stones could be recycled by means of the production of activated carbons, since they

71 constitute a source of renewable carbon with a low cost. In addition, they are suitable 72 for preparing microporous activated carbons due to their low ash content. To the best of 73 our knowledge, few studies have been published on the preparation of activated carbons 74 from cherry stones, which were synthesized by conventional two-step activation and they were characterized and evaluated for adsorbing gases such as NO<sub>2</sub> or H<sub>2</sub>S and 75 liquid impurities.<sup>11-14</sup> However, studies on one-step CO<sub>2</sub> or steam activation of cherry 76 77 stones have not been reported in literature. Therefore, in the present work two 78 microporous activated carbons were for the first time prepared from cherry stones by 79 single-step activation with carbon dioxide and steam for application in CO<sub>2</sub>/CH<sub>4</sub> 80 separation. CO<sub>2</sub> adsorption on these adsorbents was optimized in relation to the 81 activation conditions (temperature, heating rate and solid yield) by means of RSM. 82 Afterwards, two activated carbons were produced on a larger scale using the resulting 83 optimum activation conditions and were texturally characterized. The performance to 84 separate CO<sub>2</sub> from CO<sub>2</sub>/CH<sub>4</sub> binary mixtures, representative of biogas streams, was evaluated. 85

## 86 **2 EXPERIMENTAL**

#### 87 **2.1 Single-step activation with CO<sub>2</sub> or steam**

A low-cost biomass, cherry stones (CS), was used as starting material. Cherry stones were ground and sieved, and samples with a particle size between 1 and 3 mm were selected. The proximate and ultimate analyses of the raw material are collected in Table 1. The single-step activation with carbon dioxide or steam was carried out in a Setaram TAG24 thermobalance, methodology previously validated in our laboratory.<sup>15</sup> Accordingly, in order to choose the activation temperature range, non-isothermal mass loss profiles of raw CS under carbon dioxide and steam up to 1000 °C were conducted 95 (data not shown). The temperature of commencement of mass loss, after the loss of
96 moisture and volatile matter, was taken as the minimum activation temperature. Thus, a
97 range of activation temperature of 750-950 °C was selected for the subsequent statistical
98 study with both activating agents.

99 Given that single-step activation does not include a preliminary carbonization step, the term "solid yield" instead of "burn-off degree" was preferred in the present 100 101 work. The solid yield was calculated by dividing the mass of the resulting activated 102 carbon by the initial mass of the dried precursor. Samples of approximately 40 mg were 103 used. In the case of the carbon dioxide activated adsorbents, the cherry stones samples were physically activated in a 100 mL min<sup>-1</sup> stream of CO<sub>2</sub>, whereas for the steam 104 activated carbons, the activation was carried out under a 100 mL min<sup>-1</sup> stream 105 106 containing 35 vol.% of H<sub>2</sub>O (balance N<sub>2</sub>). Prior to activation the samples were dried at 107 100 °C under an inert atmosphere of N<sub>2</sub>. The duration of the activation process was 108 dependent on the solid yield targeted in each experiment.

109 The preparation of the two optimum activated carbons on a larger scale 110 following the experimental conditions determined from the above study was carried out 111 in a vertical furnace from Carbolite. Samples of approximately 10 g were activated 112 under the same conditions used in the thermobalance.

113

# 2.2 Response surface methodology

114 Response surface methodology was used to optimize the activation variables 115 that maximize the CO<sub>2</sub> adsorption capacity at 25 °C and atmospheric pressure of each 116 cherry stones-based activated carbon. Three independent variables were evaluated: 117 activation temperature (*T*) between 750 and 950 °C, heating rate (*HR*) between 10 and 118 20 °C min<sup>-1</sup> and solid yield after activation (*Y*) between 7 and 17% for CS activated with carbon dioxide and between 7 and 22% for CS activated with steam. The response or
dependent variable, which is measured during the experiments, was the CO<sub>2</sub> uptake.

121 The experimental design selected in this study was the central composite design 122 (CCD), which consists of the following parts: (1) a full factorial design; (2) a star design 123 in which experimental points are at a certain distance,  $\alpha$ , from its centre and (3) a replicated central point. The  $\alpha$ -value depends on the number of variables, k, and can be 124 calculated by  $\alpha = 2^{k/4}$ ; for three variables, it is 1.682. The CCD design involved 20 125 experiments, including eight factorial points  $(2^3$  full factorial design), six axial points 126 127 and six replicates of the centre of the design. The experiments were conducted in a 128 random order. Prior to the application of RSM, the independent variables were coded in 129 dimensionless values so that variables with different units or of different orders of 130 magnitude could be compared. The coded (in parentheses) and the decoded values of 131 the independent variables (T, HR and Y), together with the experimental results obtained 132 for the response variable (CO<sub>2</sub> uptake) are shown in Table 2 for the carbon dioxide activated-CS and steam activated-CS adsorbents, respectively. 133

134 The experimental data collected from CCD for the three independent variables, 135  $x_1(T), x_2(HR)$  and  $x_3(Y)$ , were mathematical-statistically fitted to the following second-136 order polynomial model:

137 
$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{11} x_1^2 + \beta_{22} x_2^2 + \beta_{33} x_3^2 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3 +$$
  
138  $\beta_{123} x_1 x_2 x_3 + \varepsilon$  (1)

139 where y is the response variable;  $\beta_0$  is the constant term;  $\beta_1$ ,  $\beta_2$  and  $\beta_3$  are the coefficients 140 of the linear parameters;  $\beta_{11}$ ,  $\beta_{22}$  and  $\beta_{33}$  are the coefficients of the quadratic parameters; 141  $\beta_{12}$ ,  $\beta_{13}$ ,  $\beta_{23}$  and  $\beta_{123}$  are the coefficients of the interaction parameters and  $\varepsilon$  is the 142 residual associated with the experiments. The experimental data were fitted to Eq. (1) 143 by multiple regression analysis (least squares) and the  $\beta$  coefficients that generate the 144 lowest possible residual were determined. The fitness of the quadratic model to the 145 experimental data was evaluated by analysis of variance (ANOVA) and lack-of-fit tests. 146 A model was considered to fit the experimental data well when it showed a significant 147 regression (p-value<0.05 to a confident level of 95%) and a non-significant lack of fit 148 (*p*-value>0.05 to a confident level of 95%). The accuracy of the fitted polynomial model was expressed by the coefficient of determination  $R^2$  and by Adj- $R^2$ , which penalizes the 149 statistic  $R^2$  as extra variables are included in the model. The absolute average deviation 150 151 (AAD) was also calculated in order to check the accuracy of the model. ADD describes 152 the deviations between the experimental and calculated values. It must be as small as possible and is calculated as follows:<sup>16</sup> 153

154 AAD (%) = 100 
$$\left[ \sum_{i=1}^{n} \left( \frac{|y_{i,exp} - y_{i,cale}|}{y_{i,exp}} \right) \right] / n$$
 (2)

where  $y_{i,exp}$  and  $y_{i,calc}$  are the experimental and calculated responses, respectively, and *n* is the number of experiments. The statistical analyses were carried out using SPSS Statistics 21.0 software.

To visualize the combined effects of two factors on the response, the threedimensional plot of the model, i.e., response surface plot, was obtained. The twodimensional display of the surface plot generates the contour plot, where the lines of constant response are drawn on the plane of the two independent variables. Response surface and contour plots were generated using the SigmaPlot 10.0 software. Then, the optimum values for each independent variable that would produce the best response in the experimental region under study were determined.

165 **2.3 CO<sub>2</sub> uptake** 

The CO<sub>2</sub> capture capacity of the adsorbents was evaluated in a Setaram TAG24 thermogravimetric analyser at 25 °C and atmospheric pressure. Prior to the adsorption measurements, the samples (approximately 40 mg) were dried in situ. Afterward, a CO<sub>2</sub> adsorption test was conducted under a CO<sub>2</sub> flow rate of 100 mL min<sup>-1</sup> at 25 °C up to constant mass. The maximum CO<sub>2</sub> uptake at atmospheric pressure and 25 °C was evaluated from the increase in mass experienced by the sample and it was expressed in terms of mass of CO<sub>2</sub> per mass of dry adsorbent.

# 173 **2.4 Textural characterization of the optimum activated carbons**

174 The porosity in the optimum cherry stones-based ACs was determined by means of physical adsorption of N<sub>2</sub> at -196 °C and CO<sub>2</sub> at 0 °C in volumetric devices from 175 176 Micromeritics. This allows the assessment of the porosity in the samples from the 177 mesopores (sizes between 2 and 50 nm) down to the narrowest micropores (sizes less 178 than 0.7 nm). The usefulness of both adsorptives to characterize the porosity of carbon materials has been previously reported.<sup>17</sup> Moreover, considering the wide range of 179 180 micropore size distributions that could be achieved during physical activation of a 181 carbonaceous precursor, the combination of the two adsorptives is critical to tailor the 182 characteristics of the AC for a specific application.

The apparent surface area was calculated from the  $N_2$  isotherms using the Brunauer-Emmett-Teller equation  $(S_{BET})^{18}$  in the relative pressure range 0.01-0.1, whereas the total pore volume  $(V_p)$  was estimated from the amount of nitrogen adsorbed at a relative pressure of 0.99. It is known that the CO<sub>2</sub> capture performance of carbon materials mainly involves the microporosity in the samples, so the Dubinin-Radushkevich (D-R) equation<sup>19</sup> was used to estimate the micropore volume, W<sub>0</sub>, and the characteristic energy, E<sub>0</sub>, as realized by the corresponding molecular probe, N<sub>2</sub> or 190 CO<sub>2</sub>. The average micropore width,  $L_0$ , of the locally slit-shaped micropores is related 191 to the characteristic energy by means of the Stoeckli-Ballerini relation<sup>20</sup>, as follows:

192 
$$L_0 (nm) = 10.8/(E_0 (kJ mol^{-1}) - 11.4)$$
 (3)

In addition, the micropore volume corresponds to  $W_0 = (S_{mic}/2) L_0$ , assuming a slit-shaped geometry and, consequently, the surface area of the micropore walls can be estimated by the geometrical relation:<sup>21</sup>

196 
$$S_{mic} (m^2 g^{-1}) = 2000 W_0 (cm^3 g^{-1})/L_0 (nm)$$
 (4)

197 The micropore size distributions in the range of 0.3-1 nm were estimated by 198 means of the Non Local Density Functional Theory (NLDFT) on a slit pore carbon 199 model applied to the  $CO_2$  adsorption isotherms.<sup>22</sup>

# 200 2.5 Adsorption and separation of CO<sub>2</sub>/CH<sub>4</sub> tests on the optimum activated carbons

The adsorption isotherms of pure  $CO_2$  and  $CH_4$  of the cherry stones-based ACs prepared under the optimum activation conditions were measured up to 10 bar at 30 °C in a high pressure magnetic suspension balance (Rubotherm-VTI). Details on the set-up and the experimental procedure can be found elsewhere.<sup>23</sup> The absolute amounts of  $CO_2$ and  $CH_4$  adsorbed over the pressure range tested were estimated following the procedure described in García *et al.*<sup>24</sup>

The experimental CO<sub>2</sub> and CH<sub>4</sub> adsorption isotherms of the cherry stones-based
 ACs were fitted to the Sips model according to the following expression:

209 
$$q = q_s \frac{(bP)^{1/n}}{1 + (bP)^{1/n}}$$
 (5)

where q represents the concentration of the adsorbed specie and  $q_s$  the saturation capacity, P the pressure of the adsorptive and b the affinity constant. The parameter nshows the heterogeneity of the system and its value is usually greater than unity; therefore, the larger the value of *n*, the more heterogeneous is the system. The fitting of the experimental data to the Sips model was conducted by means of the *Solver Excel* tool assuming  $q_s$  and *n* to be equal for both CO<sub>2</sub> and CH<sub>4</sub> and departing from values of  $q_s$  and *n* of 1 and  $b_{CO2}$  and  $b_{CH4}$  of 0. The goodness of the fit was evaluated on the basis of the minimum squared relative error *(SRE)* as given by the following expression:

218 
$$SRE(\%) = \sqrt{\frac{\sum_{i} [(q_{\exp,i} - q_{\text{mod}_i})/q_{\exp,i}]^2}{N-1}} \times 100$$
 (6)

where  $q_{\exp,i}$  and  $q_{\text{mod},i}$  are the experimental and Sips-predicted adsorbed amounts, respectively, and *N* is the total number of experimental data points.

Using the fitted parameters from the pure component adsorption data, the adsorption data from a binary mixture of  $CO_2$  and  $CH_4$  may be predicted by an extended Sips model, similarly to the extended Langmuir equation for multicomponent adsorption. Rudziński *et al.*<sup>25</sup> stated that the application of the Ideal Adsorbed Solution Theory (IAST) with the concept of hypothetical pure-component pressure for normal activated carbons results in the following equation:

227 
$$q_{i} = \frac{q_{s}b_{i}y_{i}P\left(\sum_{k=1}^{N}b_{k}y_{k}P\right)^{(1/n)-1}}{1+\left(\sum_{k=1}^{N}b_{k}y_{k}P\right)^{1/n}}$$
(7)

Eq. (8) stands for the Sips multicomponent model where *i* represents the species for which the isotherm  $q_i$  is being evaluated, *y* is the mole fraction of the corresponding component (denoted by subscript *i* or *k*) in the gas phase, and *N* is the total number of components in the gas mixture.

#### 232 **3 RESULTS AND DISCUSSION**

# 3.1 Effect of the activation parameters on CO<sub>2</sub> adsorption capacity of activated carbons: Response surface methodology

235 Table 3 shows the results of fitting Eq. (1) to the experimental data of both 236 activated carbons, carbon dioxide activated-CS and steam activated-CS, by multiple regression analysis and those obtained from evaluating the fitness of the model by 237 means of ANOVA, together with the  $R^2$ , Adj- $R^2$  and AAD values. The coefficient 238 239 values of the polynomial models presented in Table 3 are coded coefficients. Thus 240 comparison of these values for a given material gives information of the relative 241 influence of each independent variable on the response. The ANOVA tests showed that 242 the models for the CO<sub>2</sub> capture capacity obtained were statistically significant to a 95% 243 level of confidence (*p*-value<0.05), whereas their lack of fit was found to be statistically 244 non-significant to a 95% confidence level (p-value>0.05). Table 3 also shows which 245 terms of the models are statistically significant to a 95% confidence level (p-246 value<0.05); those that were not statistically significant (p-value>0.05) were later 247 eliminated in the final models. The variable HR does not present a statistically 248 significant effect on the CO<sub>2</sub> capture capacity for any studied material, CO<sub>2</sub> or steam activated. Lua and Guo<sup>4</sup> prepared activated carbons from oil palm stones by one-step 249 CO<sub>2</sub> activation and they also found that the heating rate had no significant effect on the 250 porosity development of the adsorbents. On the contrary, Yang et al.<sup>5</sup> observed very 251 252 slight increases in the texture development when heating rate was raised from 5 to 10 °C  $\min^{-1}$ . 253

No interaction effects between *T*, *HR* and *Y* were detected in the experimental region under study, since the *T*·*HR*, *T*·*Y*, *HR*·*Y* and *T*·*HR*·*Y* interaction terms in the models proved to be statistically non-significant to a 95% confidence level (pvalue>0.05), as it is shown in Table 3. Once the non-significant terms were eliminated from the models, the coded coefficient values were decoded in order to obtain the polynomial equations that address the response variables as a function of the actual independent variables. The models obtained for both activated carbons were the following:

262 CO<sub>2</sub> uptake carbon dioxide activated-CS (wt.%) = 
$$-60.71300 + 0.15307 T + 0.73377 Y$$
  
263  $-0.00009 T^2 - 0.03057 Y^2$  (9)

264 CO<sub>2</sub> uptake steam activated-CS (wt.%) = -23.07866 + 0.06211 T + 0.94793 Y

 $265 -0.00004 T^2 - 0.03103 Y^2 (10)$ 

Fig. 1 represents the response surface and contour plots for the  $CO_2$  capture capacity as a function of the significant independent variables, i.e., activation temperature and solid yield, for carbon dioxide activated-CS (Fig. 1a) and steam activated-CS (Fig. 1b). For both activated carbons, the curve-shaped response surface and contour plot isolines clearly indicate that a maximum response is achieved in the temperature and solid yield ranges studied, i.e., within the experimental region considered.

273 For the carbon dioxide activated-CS adsorbent (Fig. 1a), the highest CO<sub>2</sub> capture 274 capacity (11.45 wt.%) was achieved at an activation temperature of 885 °C and a solid 275 yield of 12%. This means that as the activation temperature increases from 750 °C, a 276 marked increase in the CO<sub>2</sub> capture capacity is observed up to a maximum value. However, when the activation temperature increases above 885 °C, a slight decrease is 277 278 observed in the CO<sub>2</sub> uptake up to 950 °C. An optimum solid yield can be also identified, 279 although this parameter has a lower influence on the response. This is indicated by the 280 lower coded coefficient for the Y term compared to that for the T term in Table 3.

Therefore, temperature is the most influential activation parameter on the  $CO_2$  uptake of the carbon dioxide activated-CS adsorbent. This fact suggests that an increase in the activation temperature (up to 885 °C) is more efficient in raising the  $CO_2$  capture capacity of the synthesized adsorbent than a similar decrease in coded units in the solid yield between 17 and 12%.

286 For the steam activated-CS activated carbon (Fig. 1b) the highest  $CO_2$  capture 287 capacity (10.56 wt.%) was however attained at an activation temperature of 850 °C and 288 a solid yield of 15.3%. Even though an optimum activation temperature can be observed 289 for steam activated-CS, this parameter shows little influence on the response. Thus, the 290 CO<sub>2</sub> capture capacity is only slightly affected by temperature at a given solid yield. In 291 this case, as the solid yield decreases from 22%, a strong increase in the CO<sub>2</sub> uptake is 292 observed up to a maximum value. Nevertheless, when the solid yield decreases below 293 15.3%, the CO<sub>2</sub> adsorption capacity rapidly drops. The solid yield is therefore the most 294 influential activation parameter on the CO<sub>2</sub> capture capacity for the steam activated-CS 295 adsorbent. This can also be inferred from the higher coded coefficient of the Y term 296 compared to that of the T term in Table 3. From all these results, it is also confirmed 297 that, in the experimental region studied, the activation parameters do not similarly 298 influence the capture capacity of both ACs.

Higher solid yields are the result of lower activation degrees. Thus, the existence of a maximum in the  $CO_2$  capture capacity indicates that at low temperatures and activation degrees (high solid yields) the extent of the activation is too weak and hence the microporosity development in the materials is poor. However, when temperature and activation degree are increased (lower solid yields), the  $CO_2$  capture capacity rises up to the maximum value. Then, a further increase in temperature and activation reduce the microporosity in the samples due to the collapse of adjacent pore walls; this resultsin lower CO<sub>2</sub> uptakes.

The highest  $CO_2$  uptake at atmospheric pressure and 25 °C corresponded to the carbon dioxide activated-CS adsorbent, which reached 11.45 wt.%, but a relatively high  $CO_2$  uptake value (10.56 wt.%) was also attained by steam activated-CS. This could indicate that a higher micropore volume might be expected by means of  $CO_2$  activation compared to steam, since it has been shown that adsorbents with high volumes of micropores in the narrow micropore size domain are required to maximize  $CO_2$ adsorption capacity at low pressures and room temperature.<sup>26,27</sup>

314 When steam is used as activating agent, the maximum CO<sub>2</sub> uptake is achieved at 315 a temperature of 850 °C, indicating that the optimum textural development for this 316 application may be reached; higher temperature values would lead to extensive 317 gasification, ruining the porosity created and hence reducing the adsorption capacity. 318 However, when a less reactive gas such as carbon dioxide is used as activating agent, 319 activation proceeds slower and higher temperatures, 885 °C in the present study, are 320 needed to reach the optimum textural development and consequently the maximum CO<sub>2</sub> 321 uptake. Moreover, a longer activation time (lower solid yield) is also needed to reach 322 the optimum development of the carbon porosity when activating with carbon dioxide. 323 In single-step activation of biomass residues under oxygen atmospheres, it has been 324 found that the combination of a less reactive activating agent (i.e., air with a reduced 325 oxygen content) together with a higher activation temperature further develops the 326 narrowest pores, those with greater adsorption potential and therefore being more effective for adsorbing CO<sub>2</sub> at ambient conditions.<sup>28</sup> On the other hand, Gergova and 327 Eser<sup>7</sup> highlighted that the evolution of porosity is much more difficult to control during 328

activation with steam than that with  $CO_2$  due to the higher reactivity of the solid carbons under steam conditions compared to  $CO_2$ . Therefore, the lower reactivity of the CS precursor under a carbon dioxide atmosphere compared to steam has probably influenced the higher  $CO_2$  uptake found when the activation was carried out with carbon dioxide. Even at lower temperatures, the reaction rates of the carbon material with steam might be higher than with carbon dioxide, which would accelerate the development of the porosity.

According to the results from the RSM study, the temperature, heating rate and solid yield values selected for the activation in the vertical tube furnace were as follows: 885 °C, heating rate of 15 °C min<sup>-1</sup> and 12% of solid yield for the optimum CS activated with carbon dioxide; and 850 °C, heating rate of 15 °C min<sup>-1</sup> and 15.3% of solid yield for the CS activated with steam. These two optimum samples will be referred to as CS-CO<sub>2</sub> and CS-H<sub>2</sub>O, respectively, hereafter.

#### 342 **3.2** Textural characterization of the optimum activated carbons

343 In Fig. 2, the N<sub>2</sub> and CO<sub>2</sub> adsorption isotherms at -196 and 0 °C, respectively, 344 are plotted. Table 4 summarizes the textural parameters calculated from these isotherms. 345 Both ACs are mainly microporous: the microporosity, as represented by  $W_{0,N2}$ , accounts for more than 83% of the total pore volume for CS-CO<sub>2</sub> and more than 70% in the case 346 347 of CS-H<sub>2</sub>O, which confirms the assumptions stated about the superior ability of carbon 348 dioxide to create microporosity during the carbon material activation. It has been 349 reported in the literature that carbon dioxide activation of almond shells and olive and 350 peach stones mainly results in the creation of microporosity, whilst steam activation 351 widens the microporosity from the early stages of the activation process, lowering the micropore volume in the resulting activated carbons.<sup>29,30</sup> Likewise, according to the 352

shape of the N<sub>2</sub> adsorption isotherms (Fig. 2a), CS-CO<sub>2</sub> is nearly strictly microporous and displays a pronounced elbow at low relative pressures whereas CS-H<sub>2</sub>O shows a linear increase in the N<sub>2</sub> uptake over the middle section of the isotherm and a characteristic hysteresis loop that denotes the presence of mesoporosity. The presence of mesoporosity could benefit the adsorption process dynamics as these pores could act as feeding pores. Average micropore widths around 0.9 nm and characteristic energies over 23 kJ mol<sup>-1</sup> were obtained for both cherry stones-based ACs (Table 4).

360 Regarding the assessment of the narrow microporosity (of less than 1 nm in 361 size), the CO<sub>2</sub> adsorption isotherms of both ACs nearly overlapped up to relative 362 pressures of 0.02 and slightly diverged from there, where the adsorbed volume was 363 slightly higher for CS-CO<sub>2</sub> (Fig. 2b). Table 4 shows that similar features in terms of 364 narrow micropores are encountered in both ACs, although slightly higher values of 365 narrow micropore volume, W<sub>0,CO2</sub>, and narrow micropore surface, S<sub>mic,CO2</sub>, were 366 obtained for CS-CO<sub>2</sub>. The characteristic energy also addresses a slight difference between both ACs, pointing out a stronger interaction with CO<sub>2</sub> in the case of CS-H<sub>2</sub>O. 367 368 The average narrow micropore width,  $L_{0,CO2}$ , for both adsorbents was between 0.7-369 0.8 nm. The micropore size distributions in the narrow microporosity range (Fig. 2c) 370 reveal great similarities between both ACs. Nevertheless, the CO<sub>2</sub> activated carbon 371 shows a broader distribution in the 0.5-0.7 nm range and the steam activated carbon 372 presents a higher volume of micropores of approximately 0.5 nm.

373 It has been demonstrated that different porosity features (micro, meso and 374 macroporosity) are developed during the activation of biomass precursors according to 375 the activation conditions. This is in agreement with, previous works on biomass-derived 376 adsorbents.<sup>4,5,7</sup> From the textural characterization of the cherry stones-based ACs it may be concluded that differences in the activation agent have an impact in the porosity development, although to a small extent, given that the preparation conditions were optimized in terms of a maximum  $CO_2$  uptake at atmospheric pressure. The results showed that carbon dioxide activation promotes the development of microporosity whereas during steam activation micropores as well as mesopores are developed.

383

# 3.3 Adsorption and separation of CO<sub>2</sub>/CH<sub>4</sub>

The CO<sub>2</sub> uptakes obtained in the TGA at atmospheric pressure are higher than those of commercial activated carbons previously reported for CO<sub>2</sub> adsorption under similar conditions.<sup>31</sup> Moreover, they are in good agreement or are higher than the CO<sub>2</sub> uptakes of biomass-based carbon adsorbents evaluated for post-combustion capture.<sup>27,28</sup> Those results therefore show the potential of the produced activated carbons from cherry stones to be used as CO<sub>2</sub> adsorbents.

390 As a first step in the characterization of the two cherry stones-based ACs for 391 CO<sub>2</sub>/CH<sub>4</sub> separation purposes the pure component CO<sub>2</sub> and CH<sub>4</sub> adsorption isotherms were measured. Fig. 3a plots the experimental CO<sub>2</sub> and CH<sub>4</sub> adsorption isotherms at 392 393 30 °C on both cherry stones-based ACs. The isotherms are Type I in IUPAC 394 classification. Both CS activated carbons showed preferential adsorption of CO<sub>2</sub> over 395 CH<sub>4</sub> in the pressure range tested. The microporosity in both samples seems large 396 enough to neglect shape selectivity effects based on the kinetic diameters of the two gas molecules (3.30 Å for CO<sub>2</sub> and 3.80 Å for CH<sub>4</sub>)<sup>32</sup>. However, the large quadrupolar 397 398 moment of CO<sub>2</sub> (CH<sub>4</sub> does not hold a quadrupole moment) may account for such a difference in adsorption performance. The quadrupole moment produces a strong 399 400 attraction to the adsorbent surface that results in an increased uptake. The polarizability

401 could also influence the adsorption performance. Nevertheless, both  $CO_2$  and  $CH_4$  show 402 high polarizability  $(31 \times 10^{-25} \text{ cm}^3 \text{ for } CO_2 \text{ and } 26 \times 10^{-25} \text{ cm}^3 \text{ for } CH_4)^{32}$  and this 403 attraction force is much weaker than the quadrupole moment.

404 The performance of both materials to  $CO_2$  and  $CH_4$  adsorption presents great 405 similarities: the isotherms nearly overlapped at subatmospheric pressures but  $CS-CO_2$ 406 attains greater uptakes in the higher pressure range.

407 The fittings of the pure component CO<sub>2</sub> and CH<sub>4</sub> adsorption data at 30 °C to the 408 Sips model (Eq. (6)) are also plotted (lines) in Fig. 3a. The optimal parameters and 409 squared relative errors from the performed fittings are listed in Table 5. Fig. 3a shows 410 that the Sips model fitted with good accuracy the experimental CO<sub>2</sub> and CH<sub>4</sub> adsorption 411 data over the tested pressure range. However, small deviations of the model from the 412 experimental CH<sub>4</sub> adsorption data occur in the pressure range above 5 bar. It has to be 413 borne in mind that during the optimization procedure, the saturation loading and the 414 parameter n (heterogeneity) for both adsorbates, CO<sub>2</sub> and CH<sub>4</sub>, were considered equal. 415 This may impact to a greater extent the adsorbate with the weaker affinity, i.e., CH<sub>4</sub>. 416 The goodness of the fitting is corroborated by the small values of the SRE reported in 417 Table 5. The affinity constants for  $CO_2$  ( $b_{CO2}$ ) are one order of magnitude greater than 418 those for  $CH_4$  ( $b_{CH4}$ ). The stronger affinity towards  $CO_2$  is clearly reflected in the 419 greater experimental CO<sub>2</sub> uptakes from the adsorption isotherms and may account for 420 this difference. The values of the parameter n show certain heterogeneity in the system 421 that would not be adequately represented by the more conventional and theoretical 422 Langmuir equation.

Table 5 shows that the fitting of the adsorption data to the Sips model for both cherry stones-based ACs delivers similar values of the optimized parameters. 425 Nevertheless, a small difference is seen in the value of the saturation loading,  $q_s$ , which 426 is higher in the case of the CS-CO<sub>2</sub> activated carbon. The fitted values of the saturation 427 loading,  $q_s$ , of both adsorbents are in good agreement with those found in the literature 428 for commercial activated carbons.<sup>33</sup>

Based on the fitted parameters from the pure component adsorption data, the multicomponent Sips equation (Eq. (8)) was used to predict the adsorption performance of  $CO_2$  and  $CH_4$  in binary mixtures at 30 °C and 3 bar. These conditions were selected to be representative of  $CO_2$  separation from biogas streams. Fig. 3b shows the predicted isotherms for both cherry stones-based activated carbons. The selectivity of both ACs to separate  $CO_2$  from  $CO_2/CH_4$  binary mixtures was estimated from the following expression:

436 
$$S_{CO2/CH4} = \frac{q_{CO2}/q_{CH4}}{y_{CO2}/y_{CH4}}$$
(11)

437 where  $q_{CO2}$  and  $q_{CH4}$  where estimated from the multicomponent Sips model for the 438 different molar fractions of CO<sub>2</sub> ( $y_{CO2}$ ) and CH<sub>4</sub> ( $y_{CH4}$ ) in the binary mixtures.

439 The pure component CO<sub>2</sub> and CH<sub>4</sub> uptakes at 3 bar for both cherry stones-based 440 ACs are represented by the predicted multicomponent uptakes at CH<sub>4</sub> mole fractions of 441 0 and 1, respectively. As expected, both components show a decreasing trend in the 442 uptake with increasing mole fraction of the other component in the binary mixture. On 443 the other hand, the adsorption of CH<sub>4</sub> from a binary mixture seems to be more affected 444 than that of CO<sub>2</sub>: CH<sub>4</sub> only holds a 27% of the pure component uptake when mixed with CO<sub>2</sub> in a 50:50 binary mixture whereas CO<sub>2</sub> keeps a 65% of the pure component 445 446 adsorption capacity at 3 bar. On the other hand, the performance of both cherry stones-447 based ACs is very similar in terms of the predicted CO<sub>2</sub> and CH<sub>4</sub> uptakes from binary 448 mixtures at 3 bar in agreement with the pure component experimental adsorption data at

449 this pressure. Moreover, both carbons show a decreasing trend in the selectivity to separate  $CO_2$  with increasing  $CH_4$  mole fraction. At 3 bar the selectivity of the cherry 450 451 stones-based ACs for CO<sub>2</sub> remains in the range of 3.2-4, which is higher than the values reported from experimental data of mesocarbon microbeads<sup>34</sup> and activated carbon 452 beads<sup>35</sup> as well as from molecular simulations in slit shaped pores.<sup>36</sup> On the other hand, 453 454 the values of the selectivity for both carbons differ and CS-H<sub>2</sub>O shows enhanced 455 selectivity to separate CO<sub>2</sub> from CO<sub>2</sub>/CH<sub>4</sub> binary mixtures at 3 bar than CS-CO<sub>2</sub>. The 456 narrower character of the microporosity in CS-H<sub>2</sub>O could account for such a difference.

# 457 **4 CONCLUSIONS**

Two low cost carbon adsorbents,  $CS-CO_2$  and  $CS-H_2O$ , were produced from cherry stones by single-step activation with  $CO_2$  and steam, respectively. The effect of activation temperature, heating rate and solid yield on the  $CO_2$  uptake of the biomassbased activated carbons was evaluated by means of the Response Surface Methodology. The most influential variable on the  $CO_2$  uptake was the activation temperature for the  $CS-CO_2$  adsorbent and the solid yield for the  $CS-H_2O$  activated carbon.

464 The highest CO<sub>2</sub> uptakes achieved at 25 °C and atmospheric pressure were: 465 11.45 wt.% when the precursor was activated with carbon dioxide and 10.56% when the 466 precursor was activated with steam. Carbon dioxide activation promoted the 467 development of microporosity whereas during steam activation both micropores and 468 mesopores were developed. Pure and multicomponent adsorption tests at 3 bar on the 469 optimum activated carbons showed a similar CO<sub>2</sub>/CH<sub>4</sub> separation performance for CS-470 CO<sub>2</sub> and CS-H<sub>2</sub>O. Even though the adsorbent activated with carbon dioxide showed a 471 slightly higher adsorption capacity, the activation with steam led to a slightly more 472 selective activated carbon to separate CO<sub>2</sub> from CH<sub>4</sub>. In summary, due to their textural

- 473 development and low cost, the cherry stones-based activated carbons prepared are
- 474 deemed as good adsorbents in CO<sub>2</sub> adsorption based applications; more precisely for the
- 475 separation of  $CO_2$  from  $CO_2/CH_4$  mixtures.

## 476 Acknowledgements

- 477 This work was carried out with financial support from the Spanish MINECO
- 478 (Project ENE2011-23467), co-financed by the European Regional Development Fund
- 479 (ERDF) and from the Gobierno del Principado de Asturias (PCTI-GRUPIN14-079).
- 480 N.A-G. acknowledges a FPI Predoctoral fellowship from the Spanish MINECO, co-
- 481 financed by the European Social Fund.

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- 580
- 581

# 582 Figure captions

583 Fig. 1. Response surface and contour plots for the CO<sub>2</sub> capture capacity as a function of

- the activation temperature and solid yield corresponding to the carbon dioxide
- 585 activated-CS (a) and steam activated-CS (b) adsorbents.
- 586 Fig. 2. N<sub>2</sub> adsorption isotherms at -196 °C (a), CO<sub>2</sub> adsorption isotherms at 0 °C (b) and
- 587 micropore size distributions assessed from the NLDFT-CO<sub>2</sub> slit shaped carbon model
- 588 (c) for the optimum cherry stones-based activated carbons.
- 589 Fig. 3. CO<sub>2</sub> and CH<sub>4</sub> adsorption isotherms at 30 °C (a) and predicted CO<sub>2</sub> and CH<sub>4</sub>
- 590 adsorption and selectivity for binary CO<sub>2</sub>/CH<sub>4</sub> mixtures at 3 bar and 30 °C (b) for the
- 591 cherry stones-based activated carbons.

Table 1 Proximate and ultimate analyses of the raw cherry stones (CS) used as carbon precursor in the present work

Sample	CS
Proximate analysis <sup>a</sup>	
Moisture (wt.%)	3.90
Volatile matter (wt.%, db)	82.78
Ash (wt.%, db)	0.40
Fixed carbon (wt.%, db) <sup>b</sup>	16.82
Ultimate analysis (wt.%, daf) <sup>a</sup>	
С	52.76
Н	6.18
Ν	0.76
S	0.02
$O^{b}$	40.28

db: dry basis; daf: dry and ash free bases. <sup>a</sup> The proximate analysis was conducted in a LECO TGA-601, and the ultimate analysis in a LECO CHNS-932. <sup>b</sup> Calculated by difference.

595 596

Run	Independent vari	Response		
	$T(^{\circ}C)$	HR (°C min <sup>-1</sup> )	Y (%)	CO <sub>2</sub> capture (%)
Carbo	n dioxide activated-	CS		
1	790.5 (-1)	12.03 (-1)	9.03 (-1)	10.57
2	909.5 (+1)	12.03 (-1)	9.03 (-1)	11.52
3	790.5 (-1)	17.97 (+1)	9.03 (-1)	10.61
4	909.5 (+1)	17.97 (+1)	9.03 (-1)	10.97
5	790.5 (-1)	12.03 (-1)	14.97 (+1)	10.54
6	909.5 (+1)	12.03 (-1)	14.97 (+1)	10.95
7	790.5 (-1)	17.97 (+1)	14.97 (+1)	10.44
8	909.5 (+1)	17.97 (+1)	14.97 (+1)	10.97
9 <sup>a</sup>	850.0 (0)	15.00 (0)	12.00 (0)	11.24
10	750.0 (-1.682)	15.00(0)	12.00(0)	9.60
11	950.0 (+1.682)	15.00(0)	12.00(0)	11.22
12	850.0 (0)	10.00 (-1.682)	12.00 (0)	11.89
13	850.0 (0)	20.00 (+1.682)	12.00(0)	11.35
14	850.0 (0)	15.00 (0)	7.00 (-1.682)	10.03
15	850.0 (0)	15.00 (0)	17.00 (+1.682)	10.99
Steam	activated-CS			
1	790.5 (-1)	12.03 (-1)	10.04 (-1)	9.64
2	909.5 (+1)	12.03 (-1)	10.04 (-1)	9.72
3	790.5 (-1)	17.97 (+1)	10.04 (-1)	9.56
4	909.5 (+1)	17.97 (+1)	10.04 (-1)	9.58
5	790.5 (-1)	12.03 (-1)	18.96 (+1)	10.10
6	909.5 (+1)	12.03 (-1)	18.96 (+1)	10.15
7	790.5 (-1)	17.97 (+1)	18.96 (+1)	9.83
8	909.5 (+1)	17.97 (+1)	18.96 (+1)	10.54
9 <sup>a</sup>	850.0 (0)	15.00(0)	14.50(0)	10.50
10	750.0 (-1.682)	15.00 (0)	14.50 (0)	9.95
11	950.0 (+1.682)	15.00 (0)	14.50 (0)	10.13
12	850.0 (0)	10.00 (-1.682)	14.50 (0)	10.44
13	850.0 (0)	20.00 (+1.682)	14.50 (0)	10.66
14	850.0 (0)	15.00 (0)	7.00 (-1.682)	8.42
15	850.0 (0)	15.00 (0)	22.00 (+1.682)	8.90

601 
**Table 2** Independent variables and experimental values of the response variable for the central composite design (CCD) using the CS adsorbents

<sup>a</sup> Central point mean of six replicates *T*: activation temperature; *HR*: heating rate; *Y*: solid yield.

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 $\begin{array}{c} 607\\ 608\\ 609 \end{array}$ 

experimental data of activated carbons Steam activated-CS Carbon dioxide activated-CS Coded Coded Sum of Sum of DF DF p-value p-value coefficient squares coefficient squares Intersection 11.235 758.836 1 0.000 10.494 0.000 662.037 1 Т 0.364 1.812 1 0.002 0.085 0.099 1 0.125 0.164 HR -0.110 0.229 0.020 0.627 1 1 0.704 Y 0.062 0.052 0.485 0.214 0.005 0.002 1 1  $T^2$ -0.292 1.229 0.006 -0.124 0.220 0.033 1 1  $HR^2$ 0.136 0.265 1 0.135 0.057 5.387 0.276 1  $Y^2$ -0.257 0.950 0.013 -0.611 0.046 0.000 1 1  $T \cdot HR$ -0.059 0.028 0.609 0.075 0.054 0.283 1 1 0.017  $T \cdot Y$ -0.046 0.687 0.083 0.045 1 1 0.241  $HR \cdot Y$ 0.054 0.023 1 0.640 0.043 0.014 1 0.534  $T \cdot HR \cdot Y$ 0.089 0.063 0.445 0.090 0.065 0.204 1 1 Model 4.647 10 0.014 6.578 10 0.000 0.311 Residual 0.887 9 9 6.889 19 Total 5.535 19 Lack-of-fit 0.189 0.243 0.641 4 0.114 4 0.122 5 Pure error 0.247 5 0.955  $R^2$ 0.840 Adj-R<sup>2</sup> 0.662 0.905 AAD (%) 2.07 1.31

Table 3 Results of multiple regression analysis and ANOVA for the fit of the polynomial model to the CO2 capture capacity

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**Table 4** Textural characteristics of the optimum cherry stones-based activated carbons

Sample	Sample N <sub>2</sub> adsorption at -196 °C					CO <sub>2</sub> adsorption at 0 °C				
	SBET	V <sub>p</sub>	$W_{0,N2}$	L <sub>0,N2</sub>	E <sub>0,N2</sub>	S <sub>mic,N2</sub>	W <sub>0,CO2</sub>	L <sub>0,CO2</sub>	E <sub>0,CO2</sub>	S <sub>mic,CO2</sub>
	$(m^2 g^{-1})$	$(cm^3 g^{-1})$	$(cm^{3} g^{-1})$	(nm)	(kJ mol <sup>-1</sup> )	$(m^2 g^{-1})$	$(cm^{3} g^{-1})$	(nm)	(kJ mol <sup>-1</sup> )	$(m^2 g^{-1})$
CS-CO <sub>2</sub>	1045	0.48	0.40	0.93	23.0	848	0.35	0.78	25.3	906
CS-H <sub>2</sub> O	998	0.53	0.38	0.89	23.6	847	0.33	0.74	26.0	899

Sample	$q_s (\mathrm{mmol}  \mathrm{g}^{-1})$	n	$b_{CO2}$	$b_{CH4}$	SRE (%)
CS-CO <sub>2</sub>	10.45	1.40	$1.7 \times 10^{-3}$	4.7x10 <sup>-4</sup>	3.27
CS-H <sub>2</sub> O	9.31	1.39	2.1x10 <sup>-3</sup>	5.2x10 <sup>-4</sup>	2.42



Fig. 1 Response surface and contour plots for the  $CO_2$  capture capacity as a function of the activation temperature and solid yield corresponding to the carbon dioxide activated-CS (a) and steam activated-CS (b) adsorbents.



Fig. 2 N<sub>2</sub> adsorption isotherms at -196 °C (a), CO<sub>2</sub> adsorption isotherms at 0 °C (b) and
micropore size distributions assessed from the NLDFT-CO<sub>2</sub> slit-shaped carbon model
(c) of the optimum cherry stones-based activated carbons.





Fig. 3  $CO_2$  and  $CH_4$  adsorption isotherms at 30 °C (a) and predicted  $CO_2$  and  $CH_4$ adsorption and selectivity for binary  $CO_2/CH_4$  mixtures at 3 bar and 30 °C (b) for the cherry stones-based activated carbons.

- 640
- 641