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6	Performance evaluation of micro-aerobic hydrolysis of mixed sludge: Optimum
7	aeration and effect on its biochemical methane potential
8	
9	S. MONTALVO ^{1*} , F. OJEDA ¹ , C. HUILIÑIR ¹ , L. GUERRERO ² , R. BORJA ³ and
10	A. CASTILLO ¹
11	
12	^{1*} Chemical Engineering Department, Universidad de Santiago de Chile, Ave. Lib. Bdo
13	O'Higgins 3363, Santiago de Chile
14	² Chemical and Environmental Engineering Department, Universidad Federico Santa
15	María, Valparaíso, Chile
16	³ Instituto de la Grasa (CSIC), Campus Universitario Pablo de Olavide, Edificio 46,
17	carretera de Utrera, km 1, 41013-Sevilla, Spain
18	
19	ABSTRACT
20	
21	This study evaluated the performance of a micro-aerobic hydrolysis of mixed sludge and its
22	influence as a pretreatment of this waste for its subsequent anaerobic digestion. Three
23	experimental series were carried out to evaluate the optimum micro aeration levels in the
24	range from 0.1 to 0.5 vvm and operation times within the range 24-60 h. The maximum

26 *Address correspondence to Professor Silvio Montalvo, Chemical Engineering Department

- 27 University of Santiago de Chile; phone : 56-2-27181826
- 28 e-mail: <u>silvio.montalvo@usach.cl</u>

29 methane yield (35 mL CH_4/g VSS added) was obtained for an aeration level of 0.35 vvm.

- 30 This methane yield value increased 114% with respect to that obtained with the non-aerated 31 sludge. In the micro aeration process carried out at an aeration level of 0.35 vvm, increases 32 in soluble proteins and total sugars concentrations of 185% and 192% with respect of their 33 initial values were found respectively after 48 h of aeration. At the above micro-aerobic 34 conditions, soluble COD augmented 150% while volatile suspended solids (VSS) content 35 decreased until 40% of their initial respective values. Higher COD_S increases and VSS 36 decreases were found at 60 h of micro-aeration, however, the above parameters did not vary 37 significantly with respect to the values found at 48 h.
- 38

39 **Keywords:** Aerobic hydrolysis, anaerobic digestion, methane production, mixed sludge.

40

41 INTRODUCTION

42

The anaerobic process, commonly called anaerobic digestion, is the most used treatment technology for organic matter removal from primary and waste activated sludge (WAS).^[1-3] The benefits associated with anaerobic technology include mass reduction, odor removal,^[4-5] pathogen reduction, and more significantly, energy recovery in the form of methane.^[6] However, it should be emphasized that sludge contains 10 times the energy required to treat it. It has been proven to be technically feasible to recover energy from the 49 sludge, which can be directly used in wastewater treatment or be sold to the network, 50 reducing the facility's dependency on conventional electricity and helping the stressed 51 Nevertheless, the anaerobic digestion of sewage sludge has several public budgets. 52 disadvantages such as relatively low methane production, 30 - 50 % biodegradability and 53 the presence of some inhibitory compounds that make necessary the use of high retention times in the digesters with high mixing costs.^[7-9] These limiting factors are generally 54 associated with the hydrolysis stage.^[10-11] During hydrolysis, cell walls are ruptured and 55 56 extracelular polymeric substances (EPS) are degraded resulting in the release of readily 57 available organic material for the acidogenic microorganisms. This mechanism is 58 particularly important in mixed sludge digestion, since the major constituent of its organic 59 fraction are cells, being a relatively unfavorable substrate for microbial degradation.

In order to avoid or reduce the existence of the hydrolysis process in the sludge anaerobic
digestion several methods have been studied, alone or in combination such as thermal^[12-14]
, physical-chemical^[15-16] and mechanical.^[17-18] Some biological methods have been also
investigated.^[19-20]

64 Among biological, the use of micro aeration as a treatment prior to anaerobic digestion has 65 received less attention, even though it has been reported that the limited oxygen supply 66 caused an increase of the enzymatic hydrolysis rates for the case of complex organic matter in batch tests.^[21] Results from some micro aerobic research carried out with municipal solid 67 68 wastes and other wastes suggest that hydrolysis, and therefore, the COD solubilization might be improved by micro aeration.^[22-24] However, the presence of oxygen in the 69 70 anaerobic digestion can also produce a problem regarding to the use and degradation of 71 organic matter. In presence of oxygen, there is a competition by the substrate between facultative and strict anaerobes^[25], which could reduce the organic matter available for 72

methanogenic archaea, because part of the substrate is used for the production of CO_2 and biomass by facultative microorganisms. Therefore, the management of micro-aeration should be carefully carry out in order to improve the hydrolytic rate with a minimum consume of organic matter by facultative microorganisms with CO_2 and biomass production.

78 Regarding the effect of micro-aeration on sewage sludge anaerobic digestion, few studies have been reported. Jenicek et al.^[26], using a continuous bioreactor and pumping air 79 80 continuously into the sludge recirculation stream, showed that VSS/TSS ratio of the 81 digested sludge, soluble COD concentration, ammonia nitrogen and phosphate concentration decreased in all experiments with micro aerobic conditions. Jenicek et al.^[27] 82 83 working with a continuous stirred tank reactor (CSTR) under continuous micro aeration, 84 indicated that efficient H₂S removal, higher specific methane production, lower methane 85 concentration in biogas due to dilution by nitrogen remained from the air dosed were 86 achieved in the anaerobic digestion of the pre-aerated sludge, while better sludge liquor 87 quality and lower foaming potential and foam stability were observed in the pre-treated sludge after using micro aeration. Montalvo et al.^[28] determined that applying 0.3 vvm, and 88 89 at temperature of 35 C were the best operational conditions increasing hydrolysis rate of 90 mixed sludge. However they did not find the optimum amount of air for hydrolysis nor 91 tested the effect of aerobic hydrolysis to different aeration rates on anaerobic digestion 92 sludge

Given this background, the behavior and performance of the micro aerobic hydrolysis of mixed sewage sludge looking for the optimum level of aeration were evaluated in the present research work with the aim of achieving maximum efficiency of hydrolysis. The effect of the micro-aeration level of the mixed sludge on the methane yield was also

97 evaluated in biochemical methane potential tests carried out at 35 °C in batch mode,
98 comparing the results obtained with the pre-aerated sludge with those achieved for control
99 sludge without pre-aeration.

100

101 MATERIALS AND METHODS

102

103 Three experimental runs were carried out at laboratory-scale. A summary of the operating104 conditions assayed in each experimental run is shown in Table 1.

105 The substrate used in all the assays was a mixed sludge (mixture of waste activated sludge 106 and primary sludge). This mixed sludge was obtained from the urban wastewater treatment 107 plant (UWTP) called "La Farfana", which is located in Santiago de Chile city. Each studied 108 experimental run was carried out by duplicate.

109 The experimental run I was performed with one sample of mixed sludge while the 110 experimental series II and III were carried out with four samples of mixed sludge taken 111 during different times along the day with the aim of obtaining more representative results.

112 In the experimental run I, batch reactors of 5 L of total volume and 4 L of working volume 113 were used for the micro aeration process. After micro aerobic pretreatment, 200 mL of 114 pretreated sludge is passed into batch anaerobic digesters of 280 mL of total volume. After 115 that, 50 mL of anaerobic inoculum is added to each anaerobic digester. The anaerobic 116 inoculum came from the anaerobic plants that digest waste activated sludge at "La Farfana" 117 UWTP. This anaerobic inoculum had a VSS concentration of 10 g/L and a specific 118 methanogenic activity of 0.32 g COD-CH₄/(g VSS \cdot d). The anaerobic digesters were sealed 119 and headspace flushed with N₂ at the beginning of the test. The produced biogas was 120 measured by liquid displacement after going through a 3% (w/w) NaOH solution to capture 121 the produced CO₂; the remaining gas was assumed to be only methane. The anaerobic tests 122 were run for a period of c.a. 20-25 days until the accumulated gas production remained 123 essentially unchanged, i.e. on the last day production was lower than 3% of the 124 accumulated methane produced. The main objective of this experimental run was to obtain 125 the best aeration level within the range from 0.1 to 0.5 vvm (volume of air/(volume of 126 reactor \cdot minute)) taken into account as criterion the methane production achieved in the 127 batch anaerobic digestion experiment of the pre-aerated sludge. The experiment 128 corresponding to an aeration level of 0.3 vvm was extended until 60 h with the aim of 129 assessing the evolution of proteins and total sugars with time.

130 The experimental run II had two main objectives: firstly, to obtain the optimum aeration 131 level and, secondly, to assess the influence of aeration time on the hydrolysis process. After 132 this run, no batch anaerobic digestion experiments of the pre-aerated sludge were made.

Finally in the experimental run III, the performance of the micro-aerated hydrolysis was evaluated from the evolution of different parameters such as soluble proteins and sugars with time and its influence on the methane production of the pre-aerated sludge. In this run II, it was used the best aeration level obtained in the second experimental run (0.35 vvm).

The operating temperature selected for the micro aerobic hydrolysis experiments was 35 °C according to previous results reported in the literature.^[28] This temperature was also used for batch anaerobic digestion experiments of the pretreated sludge because it coincides with the optimum temperature reported for achieving maximum methane production within the mesophilic interval.^[7]

All chemical analysis were determined according to American Public Health Association
 Standard Methods.^[29] Specifically, chemical oxygen demand (COD) and volatile suspended
 solids were analysed according to the closed digestion and colorimetric 5220D method and

145	2540B method, respectively of the Standard Methods (APHA, 2012). ^[29] pH was determined		
146	using a pH-meter model Crison 20 Basic.		
147	Soluble proteins and total sugars were determined using the ASTM D5712 and ASTM		
148	D6406 standard methods, respectively.		
149	For the statistic processing and analysis of the data, the software Minitab 8 was utilized. An		
150	ANOVA analysis was done and a comparison of confidence intervals for mean values was		
151	made with a confidence of 95%.		
152			
153	RESULTS AND DISCUSSION		
154			
155	No significant differences in the behavior of duplicate reactors were observed in all assays.		
156	Therefore, only the results of one of the duplicate reactors will be shown.		
157			
158	Assay I		
159			
160	Figure 1 shows the evolution of the methane production (measured as mL methane/g of		
161	volatile suspended solids (VSS) added), which will allow to assess the variation of the		
162	accumulated methane with time per each gram of VSS added at the beginning of the		
163	anaerobic digestion process.		
164	As can be seen for an aeration level of 0.1 vvm only a small increase in methane production		
165	was observed compared to the control (not subjected to aeration). An ANOVA analysis of		

167 significant with a confidence level of 95%. In this case, the following values of statistical

the data revealed that this difference in production of methane was not statistically

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168 parameters were obtained: F=0.141; p=0.709; F_{critical}=4.130 (F_{critical} value was higher than

169 F). By contrast, for an aeration level of 0.3 vvm an increase of 114% in the methane 170 production of the pre-aerated sample was achieved compared to the control without 171 aeration. In this case, the difference was statistically significant as was shown in the 172 statistical analysis (F = 6.789; p = 0.013; $F_{critical} = 4.149$). Finally, for the experimental run 173 of 0.5 vvm, no significant differences between the methane production of the pre-aerated sludge and the control were detected (F=0.044; p=0.834; F_{critical}=4.130), which 174 175 demonstrates that a high aeration may not be beneficial, and, even, harmful for the 176 anaerobic digestion process.

177 Therefore, according to these results an aeration level of 0.3 vvm contributes to better 178 performance of methanogenic microorganisms confirmed by the methane production 179 obtained in this case. When the aeration level increased up to 0.5 vvm a decrease in 180 methane production was observed as consequence of the higher concentration of dissolved 181 oxygen, which inhibited the metabolism and activity of methanogens. Gerritse and Gottschal^[30] demonstrated that an aeration level of 0.1 vvm did not increase the methane 182 183 formation compared to a control sample. However, a short time of exposure to oxygen did 184 not reduce the methanogenic activity and under these conditions the methanogens can survive more time than previously expected.^[31] For instance, oxygen concentration levels 185 in the range of 4.9-6.4 mg/L are required to inhibit 50% of the methanogenic activity.^[32] 186 187 All these results clearly indicated that an adequate optimization of oxygen supply to 188 aeration is required in all cases to avoid the inhibition of methanogenic activity.

As was shown in Figure 1, the maximum methane yield ($35 \text{ mL CH}_4/\text{g VSS}$ added) was obtained for an aeration level of 0.3 vvm. This value represents an increase of 114% in methane production compared to that obtained with the non-aerated sludge. This increase in the methanogenic activity is attributed to an improvement in the growth of facultative anaerobic microorganisms, which can keep a low redox potential, providing the best
conditions for the growth of strict anaerobes.^[23]

Table 2 shows the effect of aeration on the final pH of the reactors. As can be seen, a pH increase of 7.1% and 3.2% was achieved in the reactors with aeration and non-aeration, respectively. This pH increase can be due to two main factors: firstly, the hydrolysis of proteins produces the liberation of amino groups (-NH₂), which are converted into ammonia (NH₃), which when is dissolved generates ammonium (NH₄⁺) and hydroxyl ions (OH⁻), causing a pH increase.^[33] Second, when micro-aeration is applied, a CO₂ stripping takes place by the air supplied to the process.

Figures 2 shows the evolution of the soluble proteins (measured as equivalent concentration of bovine serum albumin, BSA) during the micro-aeration process at 0.3 vvm of the three samples of sludge.

205 As can be seen in Figure 2, an increase in the soluble proteins of 185% was observed after 206 48 h of aeration (at 0.3 vvm), while that an increase of only 7.8% was detected in the non-207 aerated reactor. The evolution of the soluble proteins with time had a behavior of bell-208 shaped, achieving a maximum value at 48 h of aeration. This behavior can be explained 209 taking into consideration that a part of the mixed sludge is composed by waste activated 210 sludge, which consisted of flocs formed by clusters of cells and organic matter within a 211 viscous material. For this reason, there was an increase in soluble proteins until 48 h, which 212 were released and at the same time the insoluble proteins retained in the flocs could also be 213 solubilized. This process is called de-flocculation, and is caused, among other factors, by a 214 decrease in the aeration of the activated sludge process, reducing the amount of dissolved 215 oxygen, which coincides with the operating parameters in the present work, where low air 216 flows were injected, causing the low amount of dissolved oxygen in the reactors, its 217 concentration was found to be zero in all measurements carried out.

Another possible explanation of the increase in the protein concentration during the first 48 h of aeration is the solubilization of insoluble proteins found in the organic matter of the sludge by proteases enzymes.

Finally, once the maximum protein concentration was achieved at 48 h, a decrease in the protein content was observed due to its degradation by non-hydrolytic bacteria.

223 Figure 3 shows evolution of total sugars (measured as equivalent concentration of glucose).

As it is known hydrolysis is the rate-limiting step for the carbohydrates conversion.^[34] 224 225 Therefore, the total sugar concentration also increased in a similar manner during the first 226 48 h of aeration, obtaining an increase of 192% with respect of its initial value (Figure 3). 227 This rise can be mainly attributed to the hydrolysis of polysaccharides to monosaccharides 228 when micro-aeration is applied, which is extremely beneficial for anaerobic digestion. A 229 maximum value in the sugar concentration was achieved at 48 h of aeration, after which a 230 soft decrease was detected. This may be attributed to a certain conversion of 231 polysaccharides after this time and the beginning of the transformation of the 232 monosaccharides. By contrast, the increase in the total sugars in the non-aerated reactor 233 was only of 3%.

Table 3 summarizes the values of the concentration of total ammonia (TAMON), total COD (COD_T), soluble COD (COD_S) and VSS (average of the three samples of mixed sludge) after micro-aeration (0.3 vvm) during 48 h and after non-aeration conditions.

The results shown in Table 3 indicate that the micro aeration process of mixed sludge influence the significant increase of ammonia nitrogen, which is due to the hydrolysis of proteins and their further conversion to amino-acids and ammonia nitrogen. This agrees

240 with the increase of pH from 5.8 to 6.0-6.2, which results beneficial for the anaerobic 241 digestion process of the pre-aerated sludge. Despite the increase in ammonia concentration 242 up to values of 920 mg/L, this value cannot be considered as toxic o inhibitory for anaerobic process, whose values range from 1500-3000 mg/L^[35-36] The COD_s also 243 244 increased both in the non-aerated as in the micro-aerated reactors. However, in the reactors 245 with micro-aeration, the COD_S increased 150% with respect of its initial value, while in the 246 non-aerated ones this increase was only of 27%. These values showed that micro-aeration 247 promotes the hydrolysis of the complex organic matter and its conversion to soluble matter with a considerable rise of the COD_S as a result of the enzymatic reaction.^[37] 248

On the other hand, the COD_T experimented a relatively small decrease in both cases studied, being this decrease quite less for the non-aerated reactor. This implies that the complex organic matter can be transformed into more simple matter but never to develop a removal process of organic matter aerobically, which would imply a much higher energy expenditure.

Finally, the VSS concentration also decreased in all reactors, although this decrease was quite higher in the micro-aerated reactors (40%) compared to that achieved in the control reactors (11%). This again shows the micro-aeration promote the hydrolysis of the complex organic matter, and this matter is precisely the substrate of enzymatic reaction.^[38]

258

259 Assay II

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Figure 4 shows the evolution of the COD_S with time for each one of the four samples of mixed sludge (A, B, C and D) subjected to micro-aerobic hydrolysis using aeration levels of 0.3, 0.35, 0.4, 0.45 and 0.5 vvm. As can be seen, an increase in COD_S with the aeration

time was observed in most cases. Specifically, increases in COD_S of between 100% and 383% were observed for the three experimental runs carried out (Figures 8 B, C and D) when the aeration intensity increased from 0.3 to 0.5 vvm. Therefore, when aeration was increased between the mentioned values, the COD_S was at least doubled. For the best aeration level tested (0.35 vvm) an increase in the solubility from 8% to 23% was obtained when the aeration time increased from 48 to 60 h.

270 The variation of the VSS with time for the four experimental runs carried are with different 271 aeration intensities is shown in Figure 5. A decrease in the VSS content was observed for 272 all the cases studied. VSS reduction percentages in the range from 11.5% to 23.6% were 273 achieved after 60 h of aeration. This reduction represents the decomposition of the complex 274 organic matter that is transformed in the substrate of the hydrolytic reactions. The highest 275 VSS removal was reached with an aeration level of 0.35 vvm. Therefore, the use of a 276 controlled aeration with a specific aeration level allow eliminating certain non-277 biodegradable compounds or compounds more difficult to biodegrade using only anaerobic digestion.^[39] VSS reductions of between 2-5% were only reached between the 48 and 60 h 278 279 of aeration for the experiments carried out with an aeration level of 0.35 vvm.

Finally, the VSS removal percentages obtained at an aeration level of 0.35 vvm (23.6%)

281 were higher than others reported in the literature using an increase of temperature between

40 and 50°C (20% VSS reduction) instead of a micro-aeration step.^[40]

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284 Assay III

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Figure 6 shows the variation of the COD_T with time during the anaerobic digestion processes of the non-aerated sludge (control) and micro-aerated sludge at 0.35 vvm. As can

288 be seen a higher COD_T removal efficiency was always observed for the micro-aerated 289 sludge compared to the control, being the final COD_T removal efficiency for the pre-aerated 290 sludge at 23th day of digestion time 17% higher than for the control, difference that can be 291 considered statistically significant.

Figure 7 illustrates the variation of the VSS with digestion time for the anaerobic digestion of micro-aerated sludge and control. As can be seen a clear decrease in the VSS content with time was observed from the beginning of the process, in which the hydrolytic stage takes place, achieving low values of this parameter, especially in the case of the pre-aerated sludge. Similar trends in the evolution of VSS with time were reported by Diak et al.^[41], although final VSS values close to 15000 mg/L were obtained in this case, being this value much higher than those reached in the present work

299 Figure 8 shows the variation of methane production (measured as accumulated CH₄ in 300 mL/g VSS added) as a function of the digestion time, which allows evaluating the volume 301 of methane produced per each gram of VSS added at the beginning of the anaerobic 302 digestion process. According to the data shown in this Figure, a significant increase (110%) 303 in the production of methane was obtained when applying to the mixed sludge aerobic 304 hydrolysis compared to the digestion process of non-aerated sludge. These results are 305 consistent with the evolution of the COD and VSS presented previously. Lower increments 306 in the methane yield (21%) were previously reported during the anaerobic co-digestion of 307 brown water and food waste (during 45 day operation time) previously subjected to an micro-aerobic pretreatment with an aeration intensity of 0.0375 L O₂/L_{reactor}/day.^[41] 308

309

310 CONCLUSIONS

312 This study demonstrated that biological hydrolysis by micro aeration of mixed sludge from 313 urban wastewater treatment plants is an effective pretreatment of this waste for its 314 subsequent anaerobic digestion. The most efficient aeration level to increase significantly 315 the methane yield of the micro aerated sludge compared to a control without pre-aeration 316 was 0.35 vvm. Although higher COD increases and VSS decreases were found at 60 h of 317 micro aeration, the above parameters did not vary significantly with respect to the values 318 found at 48 h. Therefore, it would be necessary carefully evaluate the need to extend the 319 aeration for more than 48 h since the process improvement was not significantly increased 320 after 2 days of aeration. The application of a hydrolysis by micro aeration also allowed 321 stimulating the production of exoenzymes that carried out the degradation of slowly 322 biodegradable compounds which were otherwise resistant to degradation under completely 323 anaerobic conditions.

324

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326

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329

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456	FIGURE CAPTIONS
457	Figure 1. Variation of the methane production with time for the different experiments
458	carried out in the assay I
459	Figure 2. Evolution of the soluble protein concentration during the micro-aeration process
460	at 0.3 vvm
461	Figure 3. Evolution of the total sugars concentration during the micro-aeration process at
462	0.3 vvm
463	Figure 4. Effect of the aeration level on the COD _S concentrations during the micro-aerobic
464	hydrolysis of the four samples of mixed sludge from urban wastewaters
465	Figure 5. Effect of the aeration level on the VSS contents during the micro-aerobic
466	hydrolysis of the four samples of mixed sludge from urban wastewaters
467	Figure 6. Evolution of the total COD (COD_T) with time in the anaerobic digestion
468	processes of the non-aerated and micro-aerated mixed sludge
469	Figure 7. Evolution of the VSS with time in the anaerobic digestion processes of the non-
470	aerated and micro-aerated mixed sludge.
471	Figure 8. Variation of the methane production (mL CH_4/g VSS) with time in the anaerobic
472	digestion processes of the non-aerated and micro-aerated mixed sludge.
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500 Figure 5.









# Assay	Aeration level	Aeration Time	Operating	Batch anaerobic
	(vvm)	(hours)	Temperature	digestion at
			(°C)	35℃
	0	48	35	YES
	0.1	48	35	YES
Ι	0.3	48	35	YES
	0.5	48	35	YES
	0.3	24 - 48 - 60	35	NO*
	0.35	24 - 48 - 60	35	NO*
III	0.4	24 - 48 - 60	35	NO*
	0.45	24 - 48 - 60	35	NO*
	0.5	24 - 48 - 60	35	NO*
III	0	48	35	YES
	0.35	48	35	YES

Table 1. Operational conditions of the three experimental runs carried out

Γ	Aeration level [vvm]	Initial pH (t=0 h)	Final pH (t=48 h)
	0	$5.80\ \pm 0.05$	6.00 ± 0.04
	0.35	$5.80\ \pm 0.05$	6.20 ± 0.03
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Table 2. Influence of aeration on the final pH of the reactor

570 Table 3. Variation of the concentration of total ammonia (TAMON), COD_T, COD_S and

Parameter	Aeration level	Aeration time		Increase (+) o decrease (-) (%)
(mg/L)	(vvm)	(hours)		
		0	48	
TAMON	0	300	375	25 (+)
	0.3	300	920	207 (+)
COD _T	0	48900	47433	3 (-)
	0.3	48900	39609	19 (-)
COD _S	0	2500	3175	27 (+)
	0.3	2500	6250	150 (+)
VSS	0	33457	29776	11(-)
	0.3	33457	20074	40 (-)

571 VSS after the micro-aeration and non-aeration processes