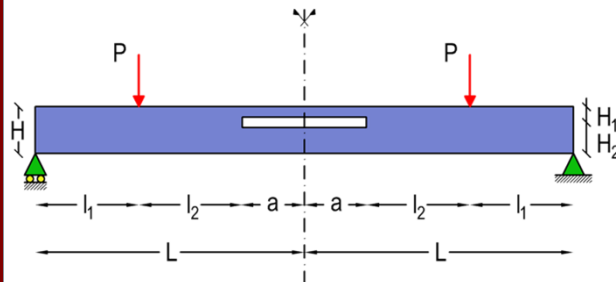


Introduction

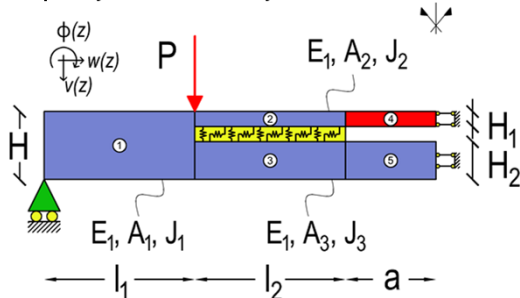
Delamination of composite laminates can have multiple causes, such as manufacturing defects, high interlaminar stresses, low-energy impacts, etc. Delamination cracks propagate under both static and fatigue loads [1].

We analyse the delamination growth promoted by local buckling in a laminate subjected to four-point bending [2].



Mechanical model

The mechanical model considers the specimen as an assemblage of sublaminates, modelled as beams, partly connected by an elastic interface.



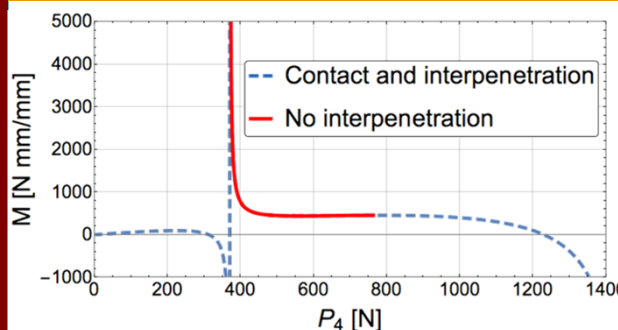
Mathematical problem

The model is described by a set of 10 differential equations + 30 b.c.

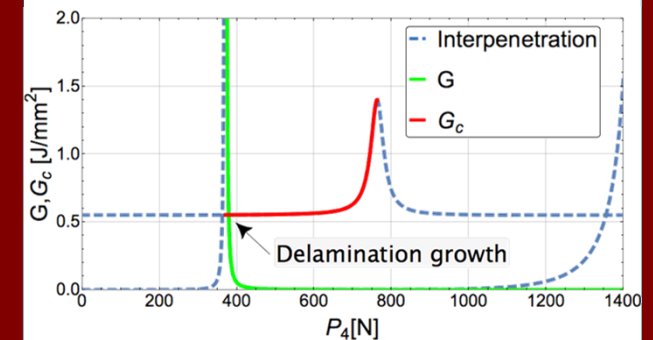
$$\begin{cases} E_1 J_1 v_1^{IV}(z) = 0 \\ E_1 A_1 w_1^{II}(z) = 0 \\ E_1 J_2 v_2^{IV}(z) - Bk_y(v_3(z) - v_2(z)) - \frac{1}{2} H_1 E_1 A_2 w_2^{III}(z) = 0 \\ E_1 A_2 w_2^{II}(z) = Bk_z \left(w_3(z) - w_2(z) + \frac{1}{2} H_2 v_2'(z) - \frac{1}{2} H_1 v_2'(z) \right) \\ E_1 J_3 v_3^{IV}(z) + Bk_y(v_3(z) - v_2(z)) + \frac{1}{2} H_1 E_1 A_3 w_3^{II}(z) = 0 \\ E_1 A_3 w_3^{II}(z) = -Bk_z \left(w_3(z) - w_2(z) + \frac{1}{2} H_2 v_2'(z) - \frac{1}{2} H_1 v_2'(z) \right) \\ E_1 J_2 v_4^{IV}(z) + P_4 v_4^{II}(z) = 0 \\ E_1 A_2 w_4^{II}(z) = 0 \\ E_1 J_3 v_5^{IV}(z) = 0 \\ E_1 A_3 w_5^{II}(z) = 0 \end{cases}$$

A general analytical solution is deduced for the differential problem. The b.c. are non-linear with respect to the axial force in the buckled sublaminates, P_4 . By taking the latter quantity as representation parameter, numerical solutions are determined for specific problems.

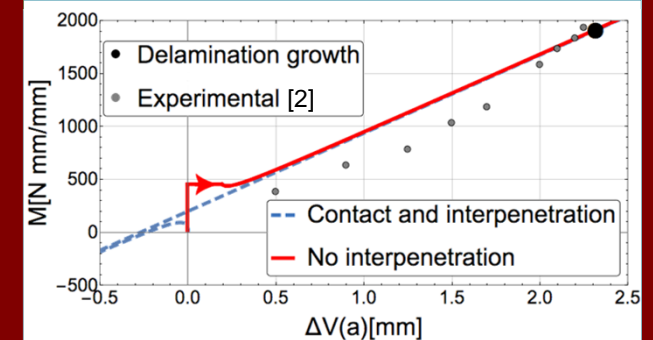
Applied bending moment vs. P_4



Delamination growth



Equilibrium path



Essential references

- [1] V.V. Bolotin: Delaminations in composite structures: Its origin, buckling, growth and stability, *Compos. Part B* **27** (1996) 129–145.
- [2] M. Kinawy, R. Butler, G.W. Hunt: Bending strength of delaminated aerospace composites, *Phil. Trans. R. Soc. A* **370** (2012) 1780–1797.