Self-Powered Microneedle-Based Biosensors for Pain-Free High-Accuracy Measurement of Glycaemia in Interstitial Fluid

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Abstract

In this work a novel self-powered microneedle-based transdermal biosensor for pain-free high-accuracy real-time measurement of glycaemia in interstitial fluid (ISF) is reported. The proposed transdermal biosensor makes use of an array of silicon-dioxide hollow microneedles that are about one order of magnitude both smaller (borehole down to 4 μ m) and more densely-packed (up to $1x10^6$ needles/cm²) than state-of-the-art microneedles used for biosensing so far. This allows self-powered (i.e. pump-free) uptake of ISF to be carried out with high efficacy and reliability in a few seconds (uptake rate up to 1 μ l/s) by exploiting capillarity in the microneedles. By coupling the microneedles operating under capillary-action with an enzymatic glucose biosensor integrated on the back-side of the needle-chip, glucose measurements are performed with high accuracy (±20% of the actual glucose level for 96% of measures) and reproducibility (coefficient

of variation 8.56%) in real-time (30 s) over the range 0-630 mg/dl, thus significantly improving microneedle-based biosensor performance with respect to the state-of-the-art.

Keywords: microneedles, biosensors, glycaemia, diabetes, pain-free

1. Introduction

According to estimation of the International Diabetes Federation (IDF) 382 million people worldwide have diabetes (IDF Diabetes Atlas, 2013). IDF projects that people living with diabetes will be 592 million in 2035. A number of recent studies clearly indicated that implementing strict glycaemic control can effectively reduce the risk of serious complications (American Diabetes Association, 2010) in diabetic patients (DPs) and, in turn, deaths (UK Prospective Diabetes Study Group,2008; Holmann et al.,2008; The Diabetes Control and Complications Trial Research Group, 1993; Nathan et al., 2005; Kitzmiller et al.,2008).

Long-term, accurate sensing of blood glucose concentration is a major concern for diabetic patients (Gilligan et al., 2004), and satisfactory compliance with testing is difficult to achieve, given the painful repetitive nature of the commonly used finger-prick systems available on the market (Martin et al., 2006; Shlomowitz et al., 2014). It has been recently shown that interstitial fluid (ISF) glucose concentrations parallel those of blood glucose (Stout et al.,2001; Vesper et al.,2006). Subcutaneously-implanted systems working on ISF and allowing for continuous glucose monitoring up to one week have then come to market in the effort to alleviate discomfort by repeated injections (Tamborlane et al.,2008; Lodwig et al.,2014). Nonetheless, these systems make use of catheters that must be inserted in the subcutaneous tissue and replaced intermittently.

Microneedles systems emerged in the mid-1990s as a result of progress in micro- and nano-technologies. They have been demonstrated to be pain-free and potentially low-cost and easy-to-use (Kim et al.,2012; El-Laboudi et al.,2012). Over the last decade they have been widely used for the transdermal delivery of a number of drugs and compounds (insulin, proteins, DNA, vaccines, and others) (Kim et al.,2012), but only a few studies have been reported on their use for glucose measurements by either extraction of biological fluid and successive analysis or in-situ analysis (Kim et al.,2012; El-Laboudi et al.,2012). Microneedles targeting ISF are particularly appealing, with respect to those sampling blood, for their unique characteristic of being pain-free and blood-free (Kim et al.,2012; El-Laboudi et al.,2012).

The analysis of the state-of-the-art on the use of microneedles for glucose measurements in ISF underlines how chips containing a reduced number of needles, ranging from 1 to 300, with length from 200 to 1500 μ m and tip radii from 15 to 400 μ m have been proposed for ISF extraction and subsequent glucose concentration measurement [Mukerjee et al., 2004; Wang et al., 2005; Sakaguchi et al., 2012; Zimmermann et al., 2003). However, in most of this works the needles are only used to pierce the skin, whereas collection of ISF is carried out using either vacuum pumps or hydrogel patches, and measurements of the glucose concentration is performed off-line by using standard analytical equipments (Mukerjee et al., 2004; Wang et al., 2005; Sakaguchi et al., 2012). To the best of our knowledge, only two works report the use of microneedles for real-time glucose measurements in ISF (Zimmermann et al., 2003; Miller et al., 2012). Nonetheless, in (Zimmermann et al., 2003) ISF is pumped with a flow-rate of 100 μ l/min through an integrated enzyme-based glucose sensor for in-line glucose measurement and

the sensor linearity range is limited to 0-160 mg/dl; in (Miller et al., 2012) hollow polymer microneedles with borehole of 400 μ m and length of 1500 μ m are filled with enzyme-enriched carbon paste material and used for in-situ glucose detection in the range 0-216 mg/dl, but no ISF uptake through the needles is carried out.

In this work we make use of hollow silicon-dioxide microneedles that are up to one order of magnitude both smaller (needle borehole with diameter of 4 μ m) and more densely packed (1×10⁶ needles/cm²) than those commonly reported in the state-of-the-art literature. We demonstrate for the first time that, by exploiting capillarity in such microneedles, accurate, reproducible, and fast uptake of liquids (e.g. water, standard physiological solution, ISF) is achieved, without the need of using external pumps. We show that, by coupling such microneedles operating under capillary-action with an enzymatic glucose biosensor integrated on the back-side of the needle-chip, self-powered real-time measurement (in-vitro) of glucose concentration in ISF is carried out with high accuracy, high reproducibility, and excellent linearity over the range 0-630 mg/dl.

2. Materials and Methods

2.1 Microneedle chip: design and fabrication

Fabrication of the microneedle chips is carried out by: 1) microneedle integration, on the front-side of a silicon die, and 2) reservoir integration, on the back-side of the same silicon die, as detailed in (Strambini et al., 2012). The needles protrude from the front-side of the chip and are in connection, through an internal channel, with the reservoir grooved on the back-side of the chip.

Two different types of microneedle chips are fabricated and tested, both of which integrating, over an area of 0.5 cm x 0.5 cm, needles with same silicon-dioxide thickness (about 1 μ m) and same protruding length (about 100 μ m), but different pitch p, external diameter d_e , and internal diameter d_i . In particular, type#1 microneedle chips are characterized by pitch $p=16 \mu \text{m}$ (density 6.25×10^5 needles/cm²), external diameter $d_e=9$ μ m, and internal diameter $d=7 \mu$ m; type#2 microneedle chips are characterized by pitch $p=10 \ \mu \text{m}$ (density 1×10^6 needles/cm²), external diameter $d_e=6 \ \mu \text{m}$, and internal diameter d_i =4 μ m. In both cases, the internal channel of the needles has length l=200 μ m and allows fluidic connection of the needles with the trapezoidal-shaped reservoir grooved on the back-side of the chips. Size and depth of the reservoir are: 0.5 cm x 0.5 cm and 500 µm (geometrical volume 10 µl) for chips used in experiments aimed at demonstrating self-powered uptake of interstitial fluid using microneedles operating under capillaryaction; 0.70 cm x 0.57 cm and 500 µm (geometrical volume of about 18 µl) for chips used in experiments aimed at demonstrating in-vitro glucose measurement in interstitial fluid using microneedles operating under capillary-action.

2.2 Testing solutions: preparation and titration

Synthetic ISF solutions containing 11 g/l of total proteins is prepared by dissolving human albumin (fraction V) and α -globulins (Cohn fraction IV-1) (both supplied by Sigma-Aldrich) in a ratio 60: 40 in isotonic saline (9.0 g/l NaCl) containing 6 mg/l of ProClin 150 (Supelco-Sigma-Aldrich) as preservative (Fogh-Andersen et al., 1995; Collison et al., 1999).

Standard solutions containing known amount of glucose are prepared starting from a 1 M stock solution of D(+) glucose (Sigma-Aldrich) in ISF and in PBS. Eight glucose calibrators in the physiopathological range (0-35 mM corresponding to 0-630 mg/dl) are obtained both in ISF and in PBS. In order to check possible matrix effects and as a overall control of the calibrator preparation, glucose concentration of all the calibrators are measured in triplicate by AU400 platform by Beckman Coulter using an enzymatic hexokinase method. This system provides a linear response between 0 - 45 mM (0 to 800 mg/dl). Sensitivity, which is evaluated as mean value plus 3x standard deviations of 20 repeated measurements of glucose-free samples, is 0.04 mM (0.72 mg/dl). Both for ISF and PBS solutions the mean within-run variation relative to three replicate measures is <0.5% at all the glucose concentrations. Total protein concentration in the ISF solution is also confirmed by AU400 system measure. Glucose is undetectable in the ISF solution at baseline (before addition of known glucose amount), indicating the lack of interference effects due to the matrix on glucose measure by hexokinase method on Beckman-Coulter system. For all the different glucose calibrators, both in ISF and PBS, a quantitative recovery of the added glucose is achieved. Glucose measure is free from significant media effects, as demonstrated by the linearity of the response (glucose measured vs glucose added) and by the intercept values not significantly different from zero (for the ISF solution y=1.04 x - 3.14; $R^2=0.997$).

Density and dynamic viscosity of PSS, and ISF solutions are measured using standard pycnometer and U-tube viscosimeter, respectively, using deionized water (DIW) as reference. Contact angle of DIW, PSS, and ISF solutions with silicon dioxide surface,

obtained by dry thermal oxidation and chemically modified with Piranha solutions, are measured by standard static sessile drop method.

2.3 Fluid drawing by capillary-action with microneedles: measure protocol

A known volume (10 ml) of the liquid under test is placed into a glass Petri dish positioned on top of an analytical microbalance (accuracy 0.1 mg) that allows monitoring volume changes of the liquid substance over time by measuring weight losses, which are mainly due, in our experiments, to microneedle uptake by capillary-action and evaporation by free-convection (unwanted effect). The microneedle chip, with the needles pointing downward, is brought in contact with the liquid through the use of a micropositioner so as to submerge the needles into the liquid for their entire protruding length, thus mimicking insertion of the needles into skin in real-word operation. As soon as the needles are immersed in the liquid, the volume, and in turn the weight, of the liquid in the Petri dish reduces due to liquid uptake through the needles by capillary action until the reservoir of the chip is completely filled, as well as due to free-convection evaporation over time. For each tested liquid at least six measurements are carried out over a time span of 900 s, for both type#1 and type#2 chips, at room temperature. Correction of free-convection evaporation is carried out for each single measure by performing the linear regression of experimental data in the range 300-900 s, for which weight reduction is linear and clearly due to only free-convection evaporation. The slope of the regression line (R²>0.999 for any experimental measurement) gives the evaporation rate, which is used to eliminate evaporation effects and to only retain capillary-uptake effects.

After each single measurement, the chip is cleaned according to the following procedure: rinsing in deionized water for 10 minutes, cleaning in Piranha solution (sulfuric acid, H_2SO_4 95-98% in water, and hydrogen peroxide, H_2O_2 30% in water, 3:1 by volume) for 15 minutes to remove possible organic components, rinsing in deionized water for 10 minutes and with ethanol for 1 minutes, and eventually nitrogen flow drying. Before and after any set of measurements with a specific liquid, six control measurements in DIW are carried out to check possible either partial or total occlusion of the needles upon testing. The whole measurement protocol is repeated several times in order to investigate reliability of liquid uptake by capillary-action through the microneedles.

2.4 Screen-printed glucose biosensor: design and preparation

Biosensor electrodes are screen-printed using a DEK 248 machine (DEK, Weymouth, UK), using both carbon-based polymeric ink (Electrodag 423 SS, from Acheson, UK) and insulating ink (TCI8700, from Visprox BV, The Netherlands). A polyester flexible foil (Autostat CT5, from MacDermid Autotype Ltd, UK), is used as the printing substrate. The carbon ink is used to define counter and working electrodes, as well as contact leads on the polyester foil, then curing at 120 °C for 10 min of the printed carbon layer is performed. The insulating ink is used to partially cover the electrode surfaces so as to define the electrode working area (7 mm²), as well as to cover unnecessary part of the contact leads. Curing of the printed insulating layer is then performed at 70 °C for 20 min. The electrodes are modified using an enzyme layer consisting of a hydrophilic polymer (carboxymethylcellulose (CMC), Sigma-Aldrich), an oxidoreductase (Glucose oxidase (GOD), from *Aspergillus niger*, Type II-S, Sigma-Aldrich), and an electron

acceptor (K₃[Fe(CN)₆], Sigma Aldrich). In particular, 5 μL of a solution containing 1% CMC, 2 U/electrode of GOD, and 100 mM Ferricyanide in 0.1 M phosphate saline buffer (PBS) pH 7.4 (PBS) is cast over the whole electrode working area, then dried in a warm air drier (40°C for 10 min). Eventually, electrodes are bagged, sealed, and stored at 4°C until use.

2.5 Microneedle-based biosensors: architecture and measure protocol

For the realization of microneedle-based biosensors for real-time measurement of glucose in ISF samples collected by capillary-action through the needles, both type#1 and type#2 chips are coupled with the screen-printed graphite electrodes modified with glucose-oxidase enzyme, which is inserted in the reservoir of the chip for a depth of 300 μ m, thus reducing the reservoir volume to 5 μ l in operating condition.

A volume of 5 µl of the solution under test is drained through the microneedles by capillary-action into the reservoir so as to completely fill the detection chamber and, in turn, get in contact with the active area of the glucose biosensor. A wait-time of 5 s and 35 s after the needles are brought in contact with the solution under test is applied for type#1 and type#2 chips, respectively, before polarization of the glucose biosensor. Chrono-amperometric measurements are performed using an applied potential of +0.5 V (vs pseudo-reference electrode). This value is optimized by both cyclic voltammetry and chrono-amperometry. Current recorded at such a potential value is due to potassium ferrocyanide (i.e. the mediator) oxidation and corresponds to glucose concentration, according to the reaction mechanism occurring in "second generation" (mediator-based) glucose biosensors (Wang, 2008). Analytical parameters are calculated for different

sampling times, from 5 to 200 s, over the whole range of glucose concentrations, from 0 to 35 mM, as here in the following reported. All measurements are performed at room temperature and without degassing the samples.

2.6 Analytical parameters: definition and calculation

Accuracy A is evaluated by calculating errors between measured and actual glucose concentrations, that is $A=C_m-C_a=I_m-I_a/S$, where C_m and C_a are respectively the measured and actual glucose concentration, I_m and I_a the measured and ideal sensor current value for the specific glucose concentration C_a , and S the sensitivity.

Linearity is evaluated as the squared correlation coefficient R² of the linear regression curves best-fitting experimental data.

Reproducibility is evaluated by calculating for each sampling time the coefficients of variation $\%CV = \sigma/\mu*100$ of each glucose concentration point, being σ the standard deviation and μ mean value of each point, then averaging the calculated %CV values over the whole range of glucose concentrations, thus achieving an average %CV ($\%CV_{av}$) for each specific sampling time.

Sensitivity S is evaluated from the slope of the linear regression curves best-fitting experimental data.

Resolution is evaluated by calculating the limit-of-detection LoD= $3\sigma/S$, being σ the standard deviation value of the tested solution at zero-glucose concentration.

3. Results and Discussions

3.1 Self-powered uptake of interstitial fluid using microneedles operating under capillary-action

The microneedle chip of this work is sketched in Figure 1a and consists of a silicon die featuring a two-dimensional array of hollow silicon-dioxide needles protruding from the front-side of the chip for one hundred microns, in connection with a reservoir integrated on the back-side of the chip. Two different types of microneedle chips are fabricated and tested, namely type#1 and type#2, featuring needles with different period/density and external/internal diameter, but same reservoir, as detailed in Section 2.1. Scanning Electron Microscope (SEM) images at two different magnifications of type#1 microneedles are reported in Figg. 1c and 1d, with a typical insulin needle sitting on their top for comparison. SEM images at two different magnifications of a part of the reservoir integrated on the back-side of the same chip are shown in Figg. S1a and S1b.

Both type#1 and type#2 microneedle chips (Fig. 2a) are used to investigate and quantify the ability of such tiny and dense needles to collect liquid substances efficiently into the reservoir integrated on the back-side by exploiting capillary action, once the needles are immersed into a liquid for a depth equal to their protruding length, thus mimicking insertion of the needles into tissues.

Three different liquid solutions are taken into account for the tests: i) deionized water (DIW), which is used as control solution, ii) standard physiological solution (PSS) (0.9% NaCl) and iii) interstitial fluid (ISF), which are of clinical interest. The ISF is a synthetic surrogate solution mimicking in-vivo ISF and containing a concentration of 11 g/l of protein obtained by solubilizing in the ratio 60:40 human albumin and α -globulins in standard physiological solution, prepared as detailed in Materials and Methods section.

Typical time-resolved liquid-uptake curves of DIW, PSS, and ISF obtained for both type#1 and type#2 microneedle chips operating under capillary-action are shown in Figure 2b. The curves are properly corrected from free-convection evaporation of the liquid over time at room temperature under atmospheric pressure, as shown in Fig. S1c (Supporting Materials), according to the procedure detailed in section Materials and Methods. It is apparent that type#1 needles are significantly faster (a factor 10 for ISF) than type#2 needles for any tested liquid. For both the microneedle chips and independently of the liquid under test, time-resolved liquid-uptake curves feature a firstorder-system kinetics $V(t) = V_{\infty}(1 - e^{-t/\tau})$, being V_{∞} the steady-state value of the volume in the reservoir, which is measured to be 17 μ l \pm 1 μ l for all the tested liquids and mainly depends on the reservoir geometric features, and τ the characteristic time-constant of the system, which depends on both microneedle size and density as well as on the specific liquid under test (namely, τ is about 12.4 s and 110.7 s for ISF uptaking using type#1 and type#2 needles, respectively). Figure 2c shows the characteristic time-constant τ (mean value and standard deviation) for the three tested liquids, both for type#1 and type#2 chips, obtained through best-fitting of experimental data with a first-order-system kinetics curve ($R^2>0.998$). The liquid uptake dynamics is mainly determined by a balance between capillary pressure, which drives the liquid throughout the needles, and viscous losses of the liquid at the needle internal surface, which act as dissipation factor. Contact angle of the liquid at the needle internal surface, dynamic viscosity of the liquid, radius, length, and period of the needles, width and height of the reservoir in contact with the needles will all play a role on the capillary uptake of liquids, accordingly to capillarymicrofluidics theory (Joos, 1999). The liquid uptake-rate (UR) through the microneedle chips can be calculated by taking the first derivative of time-resolved liquid-uptake curves, that is UR=dV(t)/dt, which yields $UR=(V_{\infty}/\tau)e^{-t/\tau}$ and highlights as the uptake-rate has an initial maximum value $UR_0=V_{\infty}/\tau$ (at t=0) and monotonically reduces (down to zero at $t=\infty$) as the uptake time (drained volume) increases. For ISF uptaking, the maximum uptake-rate value UR_0 is about 1.37 μ l/min and 0.15 μ l/min using type#1 and type#2 needles, respectively.

Control measurements in DIW carried out before and after tests with PSS and ISF confirm that experiments and results of liquid-uptake by capillary-action are not affected by significant artifacts, independently of the liquid under test and of the type of chip (Fig. 2d). For both type#1 and type#2 chips, time-constant and, in turn, the time needed to fill the reservoir, increases from DIW to PSS and ISF. This can be explained in terms of different properties, e.g. surface tension, viscosity and density, of the tested liquids (Table S1 in Supporting Materials). Experimental evaluation of the time required to uptake a volume of 5 μ 1 of ISF, in which quantify glucose with type#1 and type#2 chips, results in about 5 s and 35 s for type#1 and type#2 chips, respectively (Fig. S1d in Supporting Materials).

It has to be noted that for both type#1 and type#2 chips high accuracy and good reproducibility of the capillary-uptake process is achieved for all the tested liquids, as it is apparent from the small standard deviation of the performed measurements. On the one hand, the very small borehole of the needles allows to significantly increase capillary force and, in turn, to improve efficiency and accuracy in liquid collection. On the other hand, the very high needle density allows to effectively address possible occlusion of

some needles within the array and, in turn, to improve reproducibility and uptake-rate in liquid collection.

3.2 In-vitro glucose measurement in interstitial fluid using microneedles operating under capillary-action

Both type#1 and type#2 chips are used for the realization of microneedle-based transdermal biosensors for real-time measurement of glucose in ISF samples (volume of 5 μ 1) collected by capillary-action through the needles. To this end, the reservoir integrated on the back-side of the chips is slightly modified as in Figure 3a-1 to allow coupling of the microneedles (Figure 3a-2) with a glucose biosensor (Figure 3a-3), this latter consisting of screen-printed graphite electrodes modified with glucose-oxidase enzyme. The trapezoidal-shaped reservoir has size of 0.70 cm x 0.57 cm and depth of 500 μ m (geometrical volume of about 18 μ 1). This value reduces to 5 μ 1 in operating condition, that is after coupling of the microneedle chip with the glucose biosensor, which is inserted in the reservoir for a depth of 300 μ m. Optimization of the analytical performance of the glucose biosensor is out of the scope of this work and attainable, if necessary, by using a more sophisticated surface chemistry (Jang et al.,2012; Chen et al., 2013; Yang et al.,2014; Piao et al.,2014; Taguchi et al., 2014) that could be exploited to improve analytical performance of the microneedle-based biosensor.

The microneedle-based glucose biosensors (Figure 3a-4) are characterized using glucose solutions, both in interstitial fluid (ISF) (which is a complex matrix) and in Phosphate Buffered Saline (PBS) (as control solution), with different concentrations in the range 0-35 mM (0-630 mg/dl), which is of clinical interest for diabetes. Preparation, titration, and

characterization of all the tested solutions are detailed in section Materials and Methods. A volume of 5 µl of the solution under test is drained through the microneedles by capillary-action so as to completely fill the detection chamber at open circuit potential. This is achieved by applying a wait-time of 5 s for type#1 chips and 35 s for type#2 chips, after the needles are brought in contact with the solution and before biasing the biosensor, according to the time required to uptake 5 µl of ISF (which has the slowest uptake-rate) by capillary-action using the microneedles (Fig. S1d). Afterward, the glucose biosensor is biased with a voltage of 0.5 V and the resulting current is recorded over time for 200 s. Stand-alone (i.e. without needles) glucose biosensors (Figure 3a-3) are characterized using same solutions and procedures, and used as reference to which microneedle-based biosensors are compared in terms of analytical parameters (i.e. accuracy, linearity, reproducibility, sensitivity, resolution). Experimental data on type#1 and type#2 microneedle-based biosensors and stand-alone biosensors, measured over the glucose concentration range 0-35 mM at different sampling times between 5 s and 200 s, both in ISF and PBS solutions, are summarized in Figures S2, S3, and S4 (Supporting Materials), respectively. Figure 3b shows calibration curves of type#1 microneedle-based glucose biosensors measured over the concentration range 0-35 mM in ISF solutions, at different sampling times between 5 s and 200 s. It is worth noting that, in chronoamperometry the current (at a planar electrode) increases with analyte concentration and decays with time as given by the Cottrell equation, which explains why both current and sensitivity decrease as sampling time increases. Similar results are obtained both for type#2 microneedle-based glucose biosensors and for stand-alone glucose biosensors. Figure 3c show experimental data on type#1 and type#2 microneedle-based glucose biosensors superposed to those of the stand-alone biosensor, measured over the concentration range 0-35 mM in IFS solutions, for sampling times of 5 s, 30 s, and 100 s. Solid lines representing linear regression curves are superposed to experimental data both in Figs. 3b and 3c.

Performance of self-powered microneedle-based biosensors for glucose measurement in ISF results to be excellent, in terms of accuracy, linearity, reproducibility, sensitivity, and resolution, over the whole range of concentrations investigated and for any sampling time from 5 s to 200 s. For all the tested cases, control measurement with stand-alone biosensors yields analytical parameters that are in good agreement to those of microneedle-based biosensors.

Best performance (in terms of compromise between sensitivity, accuracy, and reproducibility) of microneedle-based glucose biosensors is achieved at sampling time of 30 s, for which type#1 (type#2) biosensor accuracy A is within ±20% of the actual glucose level for 96% (92%) of measures carried out on ISF solutions over the whole range 0 – 35 mM (0 – 630 mg/dl) of glucose concentrations. For comparison, 96% of measures have accuracy within ±20% for stand-alone biosensors, in ISF. Accuracy A is evaluated as error between measured and actual glucose concentrations. These values comply with current FDA standards, according to which above 75 mg/dl (4.2 mM), 95% measures must be within ±20% of the actual glucose level (International Organization for Standardization, 2003). As per FDA guidelines, further analytical parameters are evaluated at sampling time of 30 s (in ISF solutions over the whole range 0–35 mM of glucose concentrations) for both type#1 and type#2 microneedle-based biosensors, and compared to those of stand-alone biosensors. Linearity, which is evaluated in terms of

squared correlation coefficient R² of the linear regression curves best-fitting experimental data, is 0.995 and 0.998 for type#1 and type#2 biosensors, respectively (R²=0.994 for stand-alone biosensors, in ISF). Reproducibility, which is evaluated in terms of coefficient of variations averaged over the whole range of glucose concentrations, %CV_{av}, is 8.56% and 8.74% for type#1 and type#2 biosensors, respectively (%CV_{av}=6.55% for stand-alone biosensors, in ISF). Sensitivity S, which is evaluated in terms of slope of the linear regression curves best-fitting experimental data, is 0.43 μA/mM and 0.46 μA/mM for type#1 and type#2 biosensors, respectively (S=0.49 µA/mM for stand-alone biosensors, in ISF). Resolution, which is evaluated in terms of limit-of-detection LoD, is 0.3 mM and 0.9 mM for type#1 and type#2 biosensors, respectively (LoD=0.63 mM for stand-alone biosensors, in ISF). Analytical parameters of microneedle-based biosensors at sampling time of 30s (best case) are summarized in Table I both for IFS and PBS solutions, and compared to those of stand-alone biosensors. Control experiments using PBS solutions (Fig. 3d) yield analytical parameters that are in good agreement with those obtained using ISF solutions, both for type#1 and type#2 microneedle-based glucose biosensors and for stand-alone biosensors, despite being ISF a more complex matrix with respect to PBS. Control experiment results further validate reliable and accurate measurements of the glucose concentration in ISF collected by capillary-action through such microneedles, thus foreseeing future true pain-free measurement of glycaemia by microneedle-based transdermal biosensors.

4. Conclusions

In this work a self-powered microneedle-based transdermal biosensor that allows for pain-free high-accuracy real-time measurement of glucose in ISF is demonstrated. Self-powered (pump-free) uptake of ISF is efficiently carried out with rate up to 1 μ l/s by exploiting capillarity in tiny (borehole down to 4 μ m) and densely-packed (up to 1x10⁶ needles/cm²) microneedles. By coupling the microneedles operating under capillary-action with an enzymatic glucose biosensor integrated on the back-side of the needle-chip, FDA-compliant in-vitro glucose measurement in ISF is performed with accuracy within ±20% of the actual glucose level for 96% of measures and coefficient of variation 8.56% in real-time (30 s) over the range 0-630 mg/dl, thus significantly improving microneedle-based biosensor performance with respect to the state-of-the-art.

Further work will be devoted to the investigation of in-vivo performance of the proposed self-powered microneedle-based biosensor, on the one hand, as well as to the integration of an enzyme-based biosensor right into the reservoir, on the other hand. As to the former, effective capillary uptake of ISF from skin will be investigated and lower potential values can be explored, with the aim of addressing possible clogging problems of microneedles and minimizing interference effects due to other chemical compounds; as to the latter, reduction of sample volume can be foreseen, which would be favorable in point-of-care applications.

This work envisages a novel class of minimally-invasive biosensors for point-of-care applications that (besides glucose concentration) would be employed to monitor parameters of clinical relevance in-situ, via transdermal route, through the use of ISF, with the advantage of eliminating discomfort due to needle pains and bypassing all the risks connected with blood extraction and manipulation, at the different levels.

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Figures

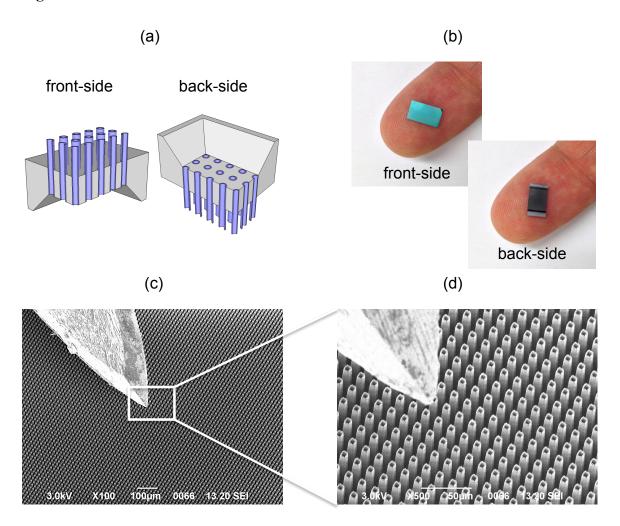


Figure 1

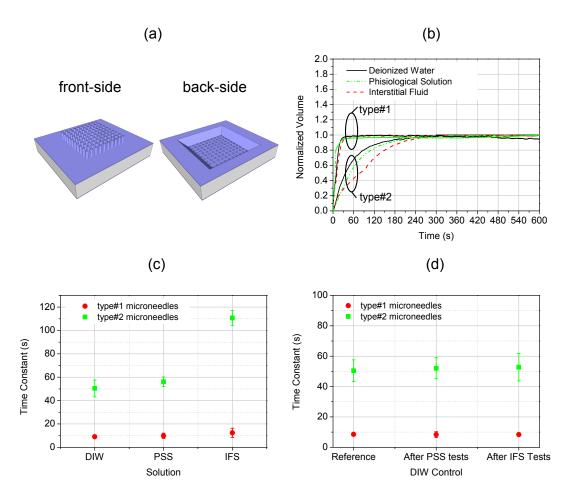


Figure 2

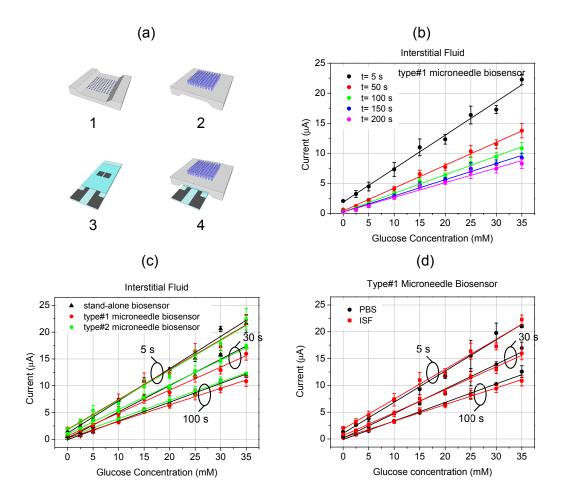


Figure 3

	Type#1 microneedle-based biosensor	Type#2 microneedle-based biosensor	Stand-alone biosensor
	ISF	ISF	ISF
	PBS	PBS	PBS
Accuracy (A)	96%	92%	96%
(measures within	92%	96%	99%
±20%)			
Linearity (R2)	0.995	0.998	0.994
(0-35 mM)	0.993	0.998	0.999
Reproducibility	8.56%	8.74%	6.55%
$(\%CV_{av})$	6.37%	7.06%	7.42%
Sensitivity (S)	0.43	0.46	0.49
(µA/mM)	0.46	0.43	0.46
Resolution (LoD)	0.3	0.9	0.6
(mM)	0.2	0.5	0.51

Table I

Figure Captions

Figure 1. High-density out-of-plane microneedle chip. (a) Schematic of a part of the microneedle chip used in this work highlighting the array of hollow silicon-dioxide needles protruding from the front-side surface and in connection with the reservoir integrated on the back-side of the chip. (b) Optical image of a type#1 microneedle chip on top of a finger. (c) and (d) Bird-eye-view scanning electron microscope (SEM) images at two different magnifications of type#1 microneedles with a typical insulin needle sitting on their top for comparison.

Figure 2. Capillary (pump-free) uptake of interstitial fluid with hollow microneedles. (a) Schematic – front-side and back-side – of the chip used for capillary uptake of liquids with hollow microneedles. (b) Typical time-resolved curves for uptake of DIW, PSS, and ISF by capillary-action using type#1 and type#2 microneedles. (c) Characteristic time-constant τ (mean value and standard deviation) for uptake of DIW, PSS, and ISF by capillary-action with type#1 and type#2 microneedles. (d) Control measurements in DIW of liquid-uptake by capillary-action using type#1 and type#2 microneedles.

Figure 3. Real-time glucose measurement by microneedle-based transdermal biosensors. (a) Schematic – front-side (1) and back-side (2) of the microneedle chip, stand-alone glucose biosensor (3) – of the microneedle-based biosensor (4) used for real-time glucose measurements by capillary-action. (b) Calibration curves (experimental data and linear regression) of type#1 microneedle-based glucose biosensors measured over the concentration range 0-35 mM in ISF solutions, at different sampling times between 5 s and 200 s. (c-d) Calibration curves (experimental data and linear regression) of type#1 and type#2 microneedle-based glucose biosensors superposed to those of stand-alone biosensors, measured over the concentration range 0-35 mM in ISF (c) and PBS (d) solutions, at sampling times of 5 s, 30 s, and 100 s.

Table I. Analytical parameters of microneedle-based transdermal biosensors (best case). Comparison of the performance of microneedle-based transdermal biosensors and

stand-alone biosensors at sampling time of 30 s, in terms of accuracy, linearity, reproducibility, sensitivity, and resolution, for glucose concentratios in the range 0-35 mM, both for ISF and PBS solutions.