

Review

Inorganic Photovoltaics - Planar and Nanostructured Devices

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34 Abstract

35 Since its invention in the 1950s, semiconductor solar cell technology has evolved in
36 great leaps and bounds. Solar power is now being considered as a serious leading contender
37 for replacing fossil fuel based power generation. This article reviews the evolution and
38 current state, and potential areas of near future research focus, of leading inorganic materials
39 based solar cells, including bulk crystalline, amorphous thin-films, and nanomaterials based
40 solar cells. Bulk crystalline silicon solar cells continue to dominate the solar power market,
41 and continued efforts at device fabrication improvements, and device topology advancements
42 are discussed. III-V compound semiconductor materials on c-Si for solar power generation
43 are also reviewed. Developments in thin-film based solar cells are reviewed, with a focus on
44 amorphous silicon, copper zinc tin sulfide, cadmium telluride, as well as nanostructured
45 Cadmium telluride. Recent developments in the use of nano-materials for solar power
46 generation, including silicon and gallium arsenide nanowires, are also reviewed.

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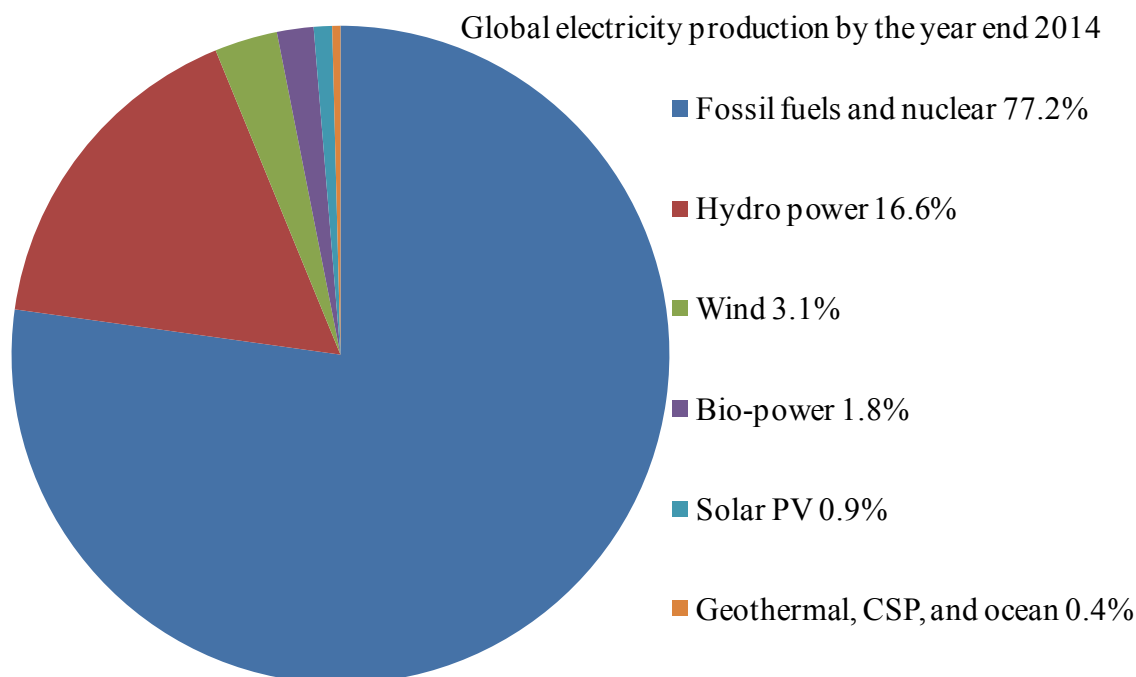
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205 **1.0 Introduction**

206 The increase in energy demand, decline in conventional energy resources, and carbon
207 dioxide (CO₂) emission from fossil fuel sources has prompted research in photovoltaics (PV).
208 With current total global power needs of 15TW, and with a projection of 30TW by the year
209 2050 [1], renewable energy is expected to play a critical role in meeting those needs. Among
210 the renewable energy sources, the PV installation for energy harvesting was about 38.7GW in
211 2014, and in 2015, the demand rose to about 42.8GW [2]. Nevertheless, despite the
212 tremendous continuing economic effort on PV research, the total contribution coming from
213 the PV sector is only about 0.9% [3] of the total global electric energy consumption. In the
214 first quarter of 2015, the average price for solar cells, modules, and installed utility systems
215 were \$0.31/watt, \$0.72/watt, and \$1.58/watt respectively [4]. Considering the current global
216 energy concerns (i.e. insufficient fossil energy supply due to high demand) together with the
217 problems related to excessive CO₂ gas emission, the huge interest in investing in the PV
218 sector is obvious. At the same time, if only about 0.1% of the Earth surface were covered
219 with PV modules with an average efficiency of 10%, this could fulfill the total energy needs
220 of humanity [5], which provides further impetus to research and development in the PV field.
221 As a side note, in every second, the sun produces 3×10^{26} W (or J/Sec) [6] of power, in other
222 words, in every second the sun produces ~500,000 years of our current energy requirements
223 [7].

224

225



226

227 Fig. 1 Percentage of global electricity production in 2014. Renewable energy accounts for 22.8%. Note that the
 228 contribution from PV is only 0.9%. CSP stands for concentrating solar power. For high-efficiency solar cells,
 229 <100> wafers are widely used in industry since easy texturing can be achieved by anisotropic etching.
 230 Texturization of <100> c-Si results upright pyramids with <111> orientation that leads to higher surface
 231 recombination rate due to an increased surface area in <111> orientation. Nevertheless, the decrease in optical
 232 losses substantially compensates small reduction in voltage from solar cell. Fig.1 data from [3].

233

234 Various methods have been developed to harvest energy from the sun that involve
 235 capturing and conversion, e.g. solar cells which absorb sun light and convert it into
 236 electricity, solar thermal collectors which absorb and convert energy from the sun into usable
 237 heat, and wind turbines (wind is an example of solar energy since it is created when the sun
 238 heats the Earth) etc. Worldwide electrical energy production is shown in Fig. 1 [3]. Replacing
 239 1kW of electrical energy from fossil fuel sources by PV cells would mitigate CO₂ production
 240 [8] by 1 tonne/year. Fossil sources (oil, natural gas, coal) produce CO₂ an average of 260-
 241 330g/kWh [9] and 48g/kWh [10] of CO₂ equivalent for PV. The latter is the average of CO₂
 242 equivalent for various technologies such as crystalline silicon (c-Si), multicrystalline silicon
 243 (mc-Si), amorphous silicon (a-Si:H), copper indium gallium selenide (CIGS), and cadmium
 244 telluride (CdTe).

245 Among various PV technologies, conventional c-Si p-n junction solar cells currently
246 play a dominant role. These solar cells have improved over the decades and are expected to
247 play a prominent part in solar power generation for the foreseeable future. However, the
248 cost-per-watt peak ($\$/W_p$, the term “peak” refers to peak sun hours – global average of about
249 5 hrs/day) of c-Si solar cells are still relatively high. High-efficiency and reduced production
250 costs are crucial factors to achieve grid parity (cost of PV generated electricity on par with
251 grid electricity known as grid parity). There are two approaches for low-cost (i.e. low $\$/W_p$)
252 c-Si solar cells: (i) lower the cost using cheaper consumables such as spin-on sources for
253 doping [11,12], low cost metallization schemes, thinner wafers and lower quality Si feedstock
254 etc., and (ii) increase the cell efficiency by using selective emitters, local back surface fields
255 etc., in front junction cells, or by using an interdigitated back contact structure in back
256 junction cells. In the back contact structure, the p-n junction lies at the rear side of the c-Si
257 wafer, and no contact grids are present at the front side. Therefore, the losses due to
258 shadowing are eliminated, which results in an increase in short circuit current and efficiency.
259 For c-Si based front junction and back junction solar cells, the metal/c-Si interface regions
260 are sites of high electron hole (e-h) recombination rates, and this affects efficiency. In the
261 case of front (a-Si/c-Si) heterojunction, and back (a-Si/c-Si) heterojunction (BHJ) cells, the
262 metal/a-Si interface is electronically separated from the c-Si bulk by inserting an intrinsic a-
263 Si:H layer, which also acts as a passivation layer to c-Si. A BHJ solar cell is a combination of
264 front heterojunction and back junction cells. In the BHJ design [13,14], shadowing loss can
265 be avoided completely due to a grid-less front side; an interdigitated pattern of p- and n-type
266 contacts collects the photogenerated current on the rear. In thin-film solar cells, fabrication of
267 a-Si:H cell is relatively simple with low fabrication cost [15]. However it also comes with
268 lower performance. Efficiency of thin-film heterojunction solar cells such as CIGS, copper-
269 zinc-tin-sulfide (CZTS) and CdTe based cells lie in between c-Si based cells and a-Si:H cells.

270 Nanowire (NW) solar cells such as Si nanowire (SiNW) [16] and gallium arsenide (GaAs)
271 have recently caught research attention. While optical absorption may be low in individual
272 NWs, the use of mats or forests of NWs in a solar cell potentially may overcome that issue.
273 Optical absorption is also potentially increased through light-trapping in those forests. NWs
274 may be used in different ways in a solar cell, which provides greater options for design. They
275 also lend themselves to flexible solar cells, an important current research focus.

276 In this article, we review inorganic wafer based solar cells that include c-Si based
277 solar cells- front junction, back junction, front heterojunction, and back heterojunction. We
278 also review multi-junction (III-V or perovskite on c-Si) solar cells, and thin-film solar cells,
279 viz. a-Si:H, CZTS, and CdTe based solar cells. Apart from planar devices, cadmium sulphide
280 (CdS)/CdTe, SiNW, and GaAs nanostructured solar cells are reviewed. We present current
281 developments in R&D, existing problems that need further research, and identify some points
282 where research is stagnant. We provide explanations to the problems associated with different
283 solar cells. Limiting factors for efficiency and how to improve efficiency are discussed.
284 Current challenges and possible strategies to overcome those challenges are mentioned.

285 **2.0 c-Si based solar cells: Front junction**

286 In this section, fabrication of conventional aluminum (Al) back surface field (Al-BSF)
287 solar cell is reviewed in detail. Other types of solar cells, such as passivated emitter rear
288 contact (PERC), passivated emitter rear locally-diffused (PERL), metal wrap-through
289 (MWT), and emitter wrap-through (EWT) cells are also discussed. Low-cost approaches for
290 producing cheap wafers, doping and metallization are outlined.

291 **2.1 Historical approach: Evolution of the c-Si solar cells to present**

292 The photovoltaic effect was first observed in 1839, when Becquerel [17] produced a
293 current intensity by exposing silver (Ag) electrodes to radiation in an electrolyte. Later, in
294 1877, Adams and Day observed that the exposure of selenium (Se) electrodes to radiation

295 produced electric voltage and current [18]. However, no significant research was reported on
296 the photovoltaic effect until 1949 when Shockley [19], Bardeen, and Brattain [20] reported
297 their work on the transistors and the physics of the p-n junction. The history of the modern
298 PV started at the Bell Labs in USA in 1954 when researchers, realized that p-n junction
299 diodes produced voltage under illumination. One year after this discovery, Bell Labs
300 produced a c-Si p-n junction solar cell with 6% efficiency [21]. In 1960, several authors
301 developed the fundamentals of the p-n junction solar cell and the relations between bandgap
302 (hereafter E_g or bandgap), incident sunlight dependence, the influence of temperature,
303 thermodynamics of the solar cells, efficiency limits, etc. In 1961, Shockley and Queisser [22]
304 reported the maximum theoretical efficiency of 29% (known as Shockley and Queisser limit
305 or S-Q limit) using a p-n junction solar cell, establishing the basis to understand the
306 performance of the solar cells and the losses mechanisms.

307 The first world oil embargo was instituted on 1973 by the Persian Gulf oil producers.
308 This incident produced a strong impulse for PV as many governments from industrialized
309 countries began programs to develop renewable energy and to reduce the oil dependence.
310 Consequently, the terrestrial application of photovoltaics was reinforced. During the 1980's,
311 the industry started producing Si PV modules, focusing in scaling up the fabrication systems,
312 the manufacturing processes, and reinforcing the cost analysis [23].

313 In 1985 the first high-efficiency c-Si solar cell under standard measurement
314 conditions was reported by University of New South Wales, Australia [24]. In the 1990's, the
315 use of solar cells for commercial purposes was extended. In 1995, a German project
316 demonstrated the use of PV installation on roofs, favoring PV legislation in Germany, Japan
317 and several countries encouraging the introduction of PV systems at homes. In 1997,
318 worldwide PV production reached 100MW, and in 1999 the cumulative worldwide installed
319 photovoltaic reached 1000MW. The annual production in 2014 has increased to 45GW

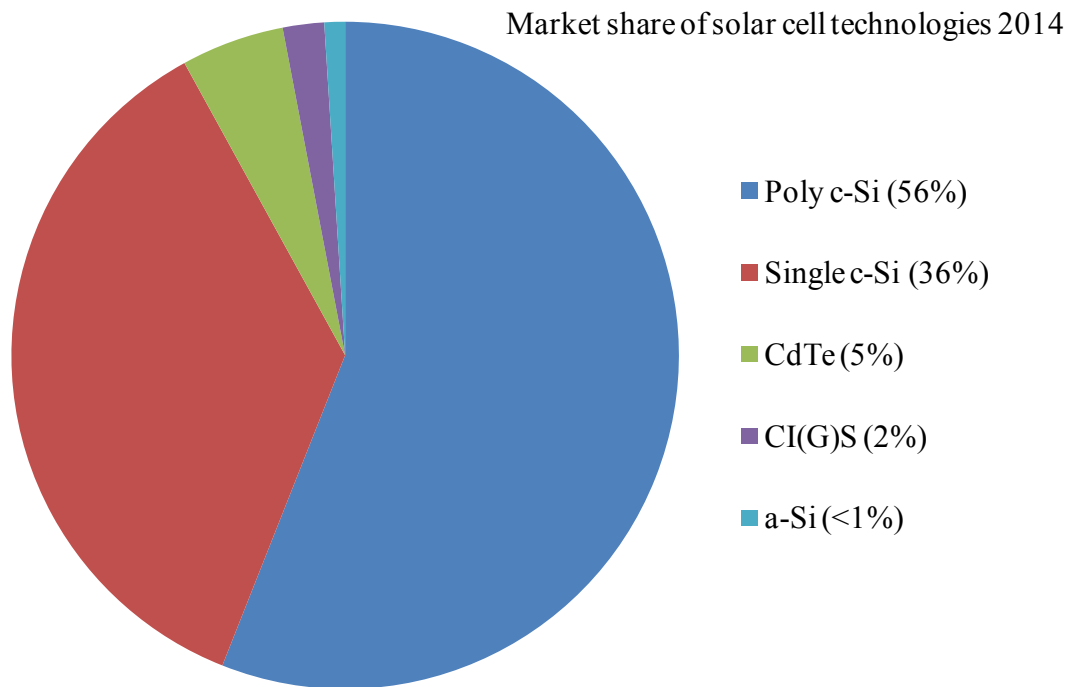
320 (reported production vary between 39 and 49GW_p), and the accumulated power installed
321 around the world has reached 183GW_p at the end of 2014 [25].

322 As shown in Fig. 2, the solar cell market is led by standard crystalline technology,
323 using single-junction solar cells, with 92% of the total market. Other technologies such as
324 CdTe, CI(G)S, and a-Si:H thin-films etc., make up the rest [26].

325 Single-junction c-Si solar cells present several advantages [27]. Si is an abundant non-
326 toxic material, composing about a 25% of the Earth's crust, and c-Si based photovoltaic
327 modules are long-term stable outdoors, with a lifetime longer than 20 years. The current
328 technology has relatively high energy conversion efficiency in comparison with many other
329 technologies and lower system costs. This enables installation of high-power systems. As we
330 will also discuss, single-junction technology still has a considerable potential for further cost
331 reductions.

332 On the other hand, the disadvantages of this technology include a limitation to
333 substantially increase the efficiency of the solar cells, as it is already close to its technical
334 limit. Moreover, at the present, fabrication of solar cells requires high-temperature and
335 energy. A large amount of Si is required for the wafer, and the wafering process (accounts
336 for 22% of the entire production cost of c-Si cell) [28] itself wastes approximately the 50% of
337 the Si ingot. The wafers are also very fragile. At a broader level, the c-Si solar cell
338 technology currently requires the support of three different factory equipments for wafer, cell,
339 and module production, and several times its integration in a single factory is not easy, which
340 in turn can affect the overall business if competitive prices are required.

341



342

343 Fig. 2 Market share of different solar cell materials in 2014 showing the dominance of c-Si (92%) followed by
 344 CdTe [26]. In the case of a-Si:H solar cells, the main issue with a-Si:H, light induced degradation, has not been
 345 solved so far. For CdTe solar cells, cadmium is abundant and tellurium is not abundant. CdTe is less toxic than
 346 cadmium and disposal of CdTe solar panel is an issue in the large-scale commercialization since CdTe modules
 347 pollute during decommissioning. CdTe disposal is a major concern in developing countries. As a side note, in
 348 the middle and late 1980s, the use of indium tin oxide in LCD products has increased indium demand and price
 349 rose to several hundred dollars per kilogram. Similarly, the demand for indium may increase with large
 350 production of CIGS based solar cells, and may results in unstable price in CIGS module.

351

352 Considering the Carnot limit for a solar cell and due to the temperature of the Sun, the

353 thermodynamic efficiency limit is about 86%. However, this limit is only calculated in terms

354 of the working temperature of the system. As mentioned above, in 1961 the first study on the

355 efficiency limit of a solar cell was calculated [22] using a detailed balance. In that work the

356 electron generation due to the absorbed photons and radiative recombination was analyzed.

357 This efficiency limit was calculated for solar cells based on a semiconductor with a valence

358 and a conduction band separated by bandgap. This study has several assumptions: (i) there is

359 only one semiconductor material per solar cell, (ii) there is only one p-n junction per solar

360 cell, and (iii) the sunlight is not concentrated and all the energy is converted to heat from

361 photons with energy larger than the bandgap. The result of this calculation indicates that there

362 is a maximum efficiency of 33% for any type of single-junction solar cell. The limitation in

363 the efficiency is due to the 47% of the solar energy directly converted to heat, 18% not
364 absorbed by the solar cells and 2% lost in local recombination. However, according to S-Q
365 limit, a maximum efficiency of 29% can be obtained [22, 29, 30].

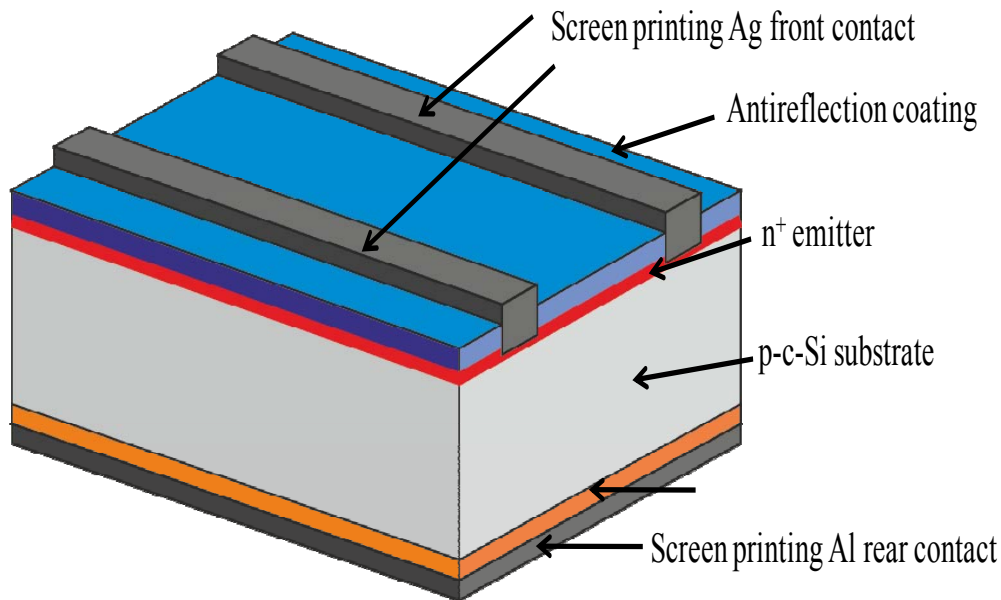
366 The evolution of the single-junction solar cells technology has been extensively
367 discussed [31]. Since the early 1950s there have been important milestones in the field. In
368 Bell Lab the first cells were fabricated on p-type c-Si and they showed efficiencies of around
369 4.5%. Using arsenic-doped n-type c-Si with a boron-doped emitter [21], the efficiency
370 reached values above 6%. In the early 1960s, due to requirements of solar cells for space
371 flights, p-type c-Si with a phosphorus-doped emitter was developed [32]. The second
372 important improvement occurred at the beginning of the 1980s, when the PERC solar cell
373 was produced. This reached 20% efficiency in 1985 [33]. Currently, the efficiency record for
374 p-n junction c-Si is ~25%, which was reached in 1998. For mc-Si the efficiency is 21.25%
375 (area 156x156 mm²) which was reached in 2015 [34]. There has been no change in the
376 maximum efficiency for c-Si and mc-Si solar cells, from 1998 and 2004 respectively.
377 However, in the industrial production line, some steps as new texturization methods (to
378 increase photons absorption), local BSF, and selective emitter have been included by the
379 most important production lines manufacturers to increase the average commercial efficiency
380 to 19% for c-Si and 18% for mc-Si. One of the challenges of the industry and also one of the
381 reasons to review this section is to describe how these advances have been transferred from
382 laboratory to production scale, allowing at the same time high-throughput and high-efficiency
383 in the solar cells. Current challenges for this technology are the implementation of new
384 concepts to target and reduce the loss mechanisms.

385 Recombination losses can be reduced using new passivation layers and chemical
386 processes. However, from the point of view of the industry, most of these techniques are not
387 cost-effective due to the requirement of high vacuum and energy. Also the process times are

388 not affordable to accomplish a competitive industry production. On the other hand, light not
 389 absorbed can be reduced using multiple anti-reflection coatings (ARCs), or including other
 390 absorber materials. Both strategies have not been integrated in the industrial production lines
 391 due to their high cost. In our opinion, these strategies should be subject of increased study in
 392 the future.

393 2.2 Conventional c-Si based solar cells

394 To understand the single-junction solar cell fabrication steps, it is necessary to first
 395 understand the device structure. A schematic diagram of a simple p-n junction p^+p-n^+ type
 396 solar cell is shown in Fig. 3. At the rear side, a heavily Al-doped p^+ -region (Al-Si alloy) in p-
 397 type c-Si forms a high-low (p^+/p) junction known as Al-BSF. The thickness of the Al-BSF
 398 region is around $0.2\ \mu\text{m}$. The phosphorous diffused emitter thickness is around $0.8\ \mu\text{m}$.
 399 Detailed fabrication steps are mentioned in Sec. 2.3.



400

401 Fig. 3 Schematic diagram of p^+p-n^+ type solar cell having Al-BSF [27]. Solar cell works as follows: Incident
 402 light generates electron-hole pairs in the p-type c-Si absorber. Due to built-in electric field across the p-n
 403 junction, electrons travel towards the n-type electrode and are in turn collected by the grid electrodes. Holes, on
 404 the other hand, travel across bulk c-Si and are collected by the Al back electrode. The potential barrier at the
 405 high-low (p^+/p) junction provides an additional mechanism to drive electrons away from reaching the back
 406 electrode and towards the p-n junction. This increases V_{oc} and J_{sc} due to reduced back surface recombination
 407 [11].

408

409 The wafer size used commercially has been increasing over the years. For a
410 considerable length of time, the Czochralski Si (Cz-Si) wafer diameter was 4" as it was the
411 standard size in the microelectronic industry and the Si wafers came mainly from stocks
412 offering quality standards just under those accepted by the microelectronic industry. Then,
413 due to the microelectronic industry requirement, and subsequently to the photovoltaic
414 industry requirement, the wafers have passed from $10 \times 10 \text{cm}^2$ (4"x4") to the current standard
415 $15.6 \times 15.6 \text{cm}^2$ (6"x6"). The wafer also has evolved from circular to pseudo-square and to
416 square shape to maximize the solar module active area. A pseudo-square wafer comes from a
417 circular wafer where the inner square is obtained showing the typical 45° cut corners.

418 In the case of mc-Si, the manufacturers have been offering square surfaces since the
419 beginning because of the fabrication procedure. The thickness of the wafer has been reduced
420 over the last decades to save Si, as it is the main component of the Si solar cell cost. Thus,
421 from $500 \mu\text{m}$ at the beginning of the 1990s, currently the wafer thickness is around 180-220
422 μm [35]. There has been considerable research activity in relation to further reductions of
423 wafer thickness to save Si, and to obtain flexible properties for the wafer. However a
424 reduction in the wafer thickness may also result in reduction of the efficiency and yield of the
425 final solar cell unless appropriate light trapping and surface passivation solutions are
426 implemented.

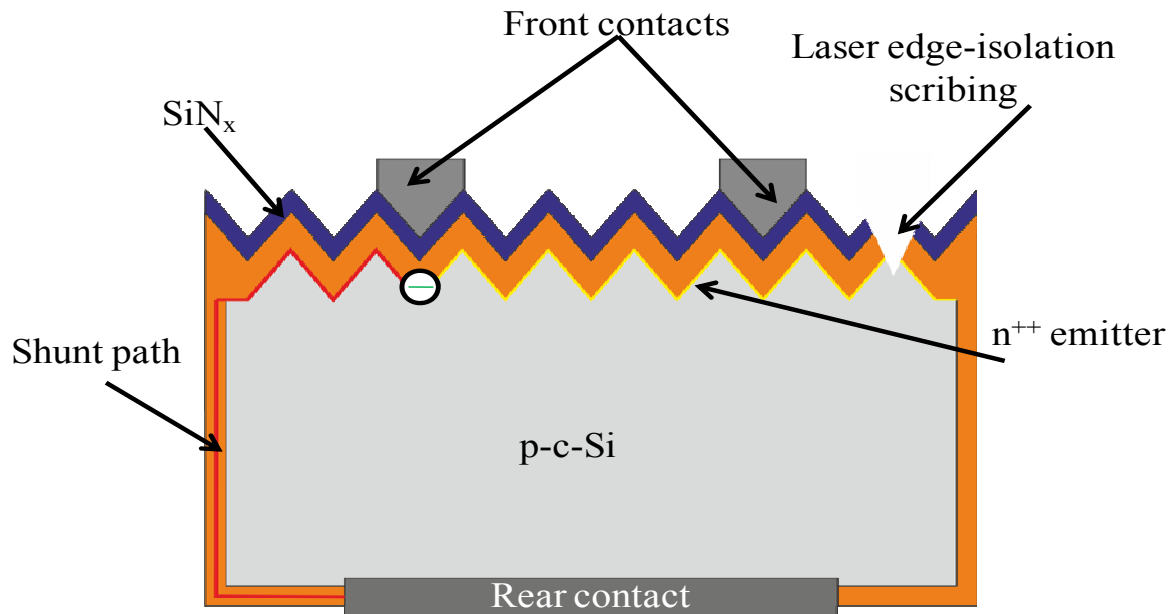
427 The base doping level of the wafer is around 10^{16} atoms/ cm^3 , which correspond with a
428 resistivity of $1 \Omega\text{-cm}$. This doping level is related to the optimum recombination properties of
429 the wafer to improve the cell efficiency.

430 Currently, the c-Si PV market is dominated by p-type Si wafers. However p-type
431 wafers are sensitive to chemical impurities that can be activated in high-temperature
432 processes, resulting in efficiency loss. P-type c-Si solar cells possess degradation of minority-
433 carrier lifetimes induced by illumination or carrier injection [27]. This lifetime degradation is

434 stabilized after one day, which concomitantly also produces a degradation of the solar cell
435 efficiency. In some cases, depending of the wafer quality, this degradation can reach 1% of
436 the total efficiency. This effect is clearly related to the presence of boron and oxygen. N-type
437 c-Si solar cells are an alternative to avoid the carrier-induced degradation of p-type c-Si, as
438 the former do not present this effect, even when high concentrations of oxygen are detected in
439 the Si wafer. This difference is related with the ratio of electron to hole capture cross sections
440 of the corresponding defects, which is greater than unity. Therefore, n-type c-Si wafers have
441 higher minority-carrier lifetime and hence higher minority-carrier diffusion length for the
442 same concentration of impurities present in bulk Si.

443 A passivation layer on the crystal surface is used to reduce surface defects. In addition
444 the front side of the wafer is normally textured in order to improve the absorption of the
445 incident radiation. Also the front surface is doped with phosphorus to form the p-n junction.
446 The phosphorous surface concentration is around 2×10^{20} atoms/cm³, with a sheet resistivity
447 (R_{sh}) between 50 and 75Ω/sq. The front side is a $\lambda/4$ (where λ is wavelength of light) coated
448 thin layer of amorphous hydrogenated SiN for an effective reduction of front reflection.
449 Finally the metallic contacts are placed by the screen printing technique: Ag is placed in the
450 front side, with a finger and busbar structure to allow solar incident radiation to the emitter,
451 and fully covered by an Al back side contact. The paste used must be dried and fired to
452 produce a proper Ohmic contact [36]. The solar cells are edge isolated (Fig. 4) in order to
453 avoid contact between front and the back side during the fabrication process.

454 In the standard cell process, the metal impurities can be reduced and even totally
455 deactivated when the wafers are submitted to the diffusion process, due to gettering effects
456 (explained in Sec. 2.3.3.). Below we review briefly on raw materials and wafer production
457 technology.



458

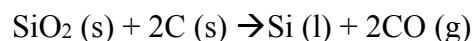
459 Fig. 4 Solar cells are edge isolated on both sides to avoid shunting between top and bottom contacts [37]. Edge
 460 isolation is performed by plasma etching, laser or laser scribing or chemical etching. In plasma etching, solar
 461 cells are coin stacked and then edges are etched away using plasma. If edge isolation is not performed,
 462 phosphorous diffusion on the edges provide short circuit to electrons and reach back electrode. For efficient
 463 solar cell operation, very high shunt resistance is required.

464

465 2.2.1 Raw materials

466 There are several processes involved in reaching the desired purity of c-Si for solar
 467 applications. To obtain solar grade Si, it is necessary to produce metallurgical grade Si (mg-
 468 Si) with a minimum of 98.5% Si content [23]. Mg-Si is produced by the introduction of the
 469 raw material in electric arc furnaces with quartz and carbon materials. The following reaction
 470 occurs:

471



472

where SiO_2 , C, CO are silicon dioxide, carbon and carbon monoxide respectively.

473

474

To carry out above reaction, lumpy quartz with appropriate purity and thermal
 resistance is required. The refined liquid Si is decanted from the ladle into a cast iron mold or
 475 onto a bed of Si fines. The casting should be removed from the mold while it is still not fully
 476 solidified. In this step, the mg-Si becomes mc-Si. This is smashed to obtain pieces of around
 477 10cm. There are several processes [23] to produce electronic grade Si of highest purity

478 (99.9999999% or 9N purity). The most frequently used process is based on the
479 decomposition of trichlorosilane (TCS) with temperatures around 1100°C on a heated Si
480 filament placed in a deposition chamber. This process is called Siemens process [38].

481 **2.2.2 Wafer technology description: Cz, Fz, and mc-Si**

482 When the literature refers to crystalline Si, one (or more) of three different materials is
483 implied: the Cz-grown c-Si, float-zone (Fz c-Si), and mc-Si. C-Si ingots are formed by Cz
484 process, based on the melting of electronic grade Si and using a rotating Si seed. The ingot is
485 formed when the seed is pulled out of the crucible [23]. The cooling down process is critical
486 to obtaining high quality Si ingot. The rotation velocity can be adjusted to obtain different
487 sizes.

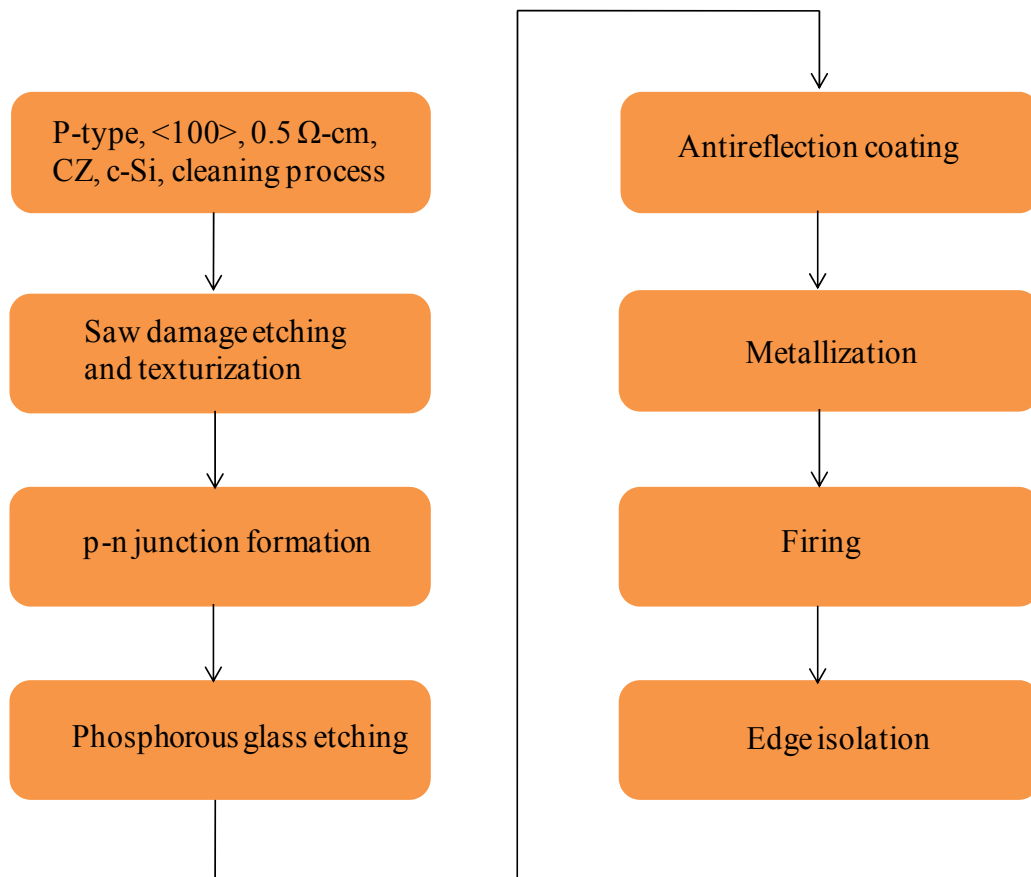
488 The floating zone process is performed on polysilicon rod to convert polysilicon into
489 single crystal Si ingot. In this process, seed crystal plays an important role. By heating one
490 end of the rod, seed crystal is fused and then seeded molten zone is passed through the length
491 polysilicon rod to convert it into single crystal Si ingot.

492 Directional solidification is the conventional method for producing mc-Si ingots. Si
493 seed crystal is not used to produce mc-Si ingots. In this method, Si scrap is used as the
494 starting material. After melting the starting material, molten Si is poured into a square shaped
495 crucible. By cooling, directional solidification takes place and large crystals grow in a
496 random direction. The mc-Si technology presents several advantages with respect to the Cz-
497 Si technology: (i) the fabrication procedure is easier, (ii) lower manufacturing costs, and (iii)
498 higher feedstock tolerance. Also, the mc-Si wafers are rectangular or square yielding a larger
499 utilization of the module area in comparison with round or pseudosquare Cz-Si or Fz-Si
500 wafers. However, as compared to Cz-Si and Fz-Si, mc-Si has much higher defect content,
501 which reduces the expected efficiency of the solar cells. Consequently, as the spot price of c-

502 Si and mc-Si varies in the market and different wafer qualities can be purchased, it is not easy
 503 to define the best wafer option for producing Si-based solar cells.

504 **2.3. Fabrication of Al-BSF c-Si solar cell**

505 The Al-BSF solar cells concept includes several physical structures with slight differences. In
 506 the following flow chart (Fig. 5), the main steps are depicted.



507

508 Fig. 5 Processing steps for front junction c-Si solar cell. Since electron mobility is about three times higher than
 509 the hole mobility, conventional solar cells are fabricated on p-type c-Si wafers for easy minority (electrons)
 510 carrier collection. Also, it is easy to obtain high-quality phosphorous diffusion than boron diffusion. However,
 511 boron-oxygen complex formation in Cz p-type c-Si reduces minority-carrier lifetime. In production, Fz c-Si
 512 wafers are used due to less oxygen content in Si wafer. An ideal resistivity and thickness of c-Si are 0.5Ω-cm
 513 and 180-200μm. For larger resistivity values, Al/p-Si interface becomes rectifying contact (Schottky barrier)
 514 and reduces V_{oc} and fill factor due to narrow depletion width of schottky junction [39]. Energy payback time
 515 [40] for c-Si solar cell is ~2 years.

516

517 Passivation of the front side is very important to obtain high-efficiency. To reduce
 518 surface recombination velocity (SRV) at the rear side, it is necessary to carry out passivation
 519 using a p^+ -layer, otherwise the solar efficiency will decrease dramatically. The easiest

520 procedure to obtain the p⁺-layer in the rear side is using boron doped Al paste to avoid high
521 recombination velocities in the rear side of the solar cell. This process is called Al-BSF [27].

522 **2.3.1 Cleaning process**

523 Cleaning process and the environmental control is critical to avoid contamination and
524 to allow high-efficiency. Several cleaning processes have been commonly used in R&D,
525 depending on the purpose. Radio Corporation of America (RCA) cleaning procedure [41] is
526 the standard process for removing contaminants from Si wafers. It consists of two steps:

527 (i) RCA 1 is used for organic cleaning. Organic contaminants are dissolved by immersing c-
528 Si wafer in a solution containing de-ionized (DI) water having resistivity of about 19MΩ.cm,
529 ammonium hydroxide (NH₄OH) and hydrogen peroxide (H₂O₂) in the ratio of 5:1:1. NH₄OH
530 is added to DI water and finally H₂O₂ is added. To remove organic residues, the wafer is
531 treated in the bath at 80°C for 15 min. This process oxidizes Si and leaves a thin oxide on the
532 Si surface that can be removed if pure Si surface is required.

533 (ii) RCA 2 is used to remove metal ions from c-Si wafer. The solution contains DI water,
534 hydrochloric acid (HCl) and H₂O₂ in the ratio of 5:1:1. HCl is added to DI water and then
535 finally H₂O₂ is added. This clean is performed around 90°C for 15 min.

536 Note that, to our best of knowledge, RCA cleaning process is not used in industry to
537 reduce production cost and to avoid the need of recycling chemicals. Before saw damage
538 removal, soap solutions are used to clean wafers.

539 **2.3.2 Saw damage etching/texturing processes**

540 The sawing process generates a high degree of damage on the “as-cut” surfaces,
541 producing a low quality surface with a large amount of defects on it [42]. These defects can
542 produce fracture during the solar cells processing and lower the performance of the solar cells
543 [43]. Thus, one of the necessary steps to obtain high-efficiency Si solar cell is to introduce

544 saw damage etching of the wafer at the beginning of the fabrication process, and it is carried
545 out by immersion of the wafer in a chemical solution [27].

546 Optical losses of the solar cells can be improved by means of a texturing process on
547 the front surface of the Si wafer [36]. The aim of the texturing process is to produce a specific
548 morphology on the Si surface able to redirect reflected light into the device to improve the
549 light absorption, i.e., diminish the reflection losses from the front surface. To carry out
550 texturing, several methods are available, such as mechanical grooving [43,44], reactive ion
551 etching (RIE), anisotropic alkaline etching [43], acidic etching [45], chemical etching using a
552 metallic catalyst [46], dry etching processes as plasma texturing [47], and laser texturization
553 [48]. Among these methods, wet chemical etching is the mostly used in industrial process and
554 commercially it is also the most commonly used procedure for c-Si solar cells. This is
555 because of its low-cost, high etching rate, and large-area uniformity [49]. Saw damage
556 etching and the texturization process can be carried out in the same step when chemical
557 solutions are used.

558 For c-Si, pyramid formation is due to anisotropic etching resulting from the difference
559 in etching rates for the $\langle 100 \rangle$, $\langle 111 \rangle$ planes of c-Si. The pyramids size and height are highly
560 depending on the etchant and the etching parameters [43]. Mixed alkaline solutions, such as a
561 sodium hydroxide (NaOH) or a potassium hydroxide (KOH) solution, with isopropyl alcohol
562 (IPA) are used to texture the monocrystalline Si surface. However, IPA cost limits the use of
563 these solutions. For chemical anisotropic etching, the solutions without IPA have been
564 acquiring more relevance during recent years [50, 51]. Cheaper alternative solvents are
565 sodium carbonate (Na_2CO_3) [52], potassium carbonate (K_2CO_3) [53] and sodium phosphate
566 (Na_3PO_4) [54].

567 Recently a mixture of Na_2CO_3 and sodium bicarbonate (NaHCO_3) has been
568 optimized. This has significantly reduced the amount of the solvents and their costs [43], and

569 has proved to be the most promising to be used in c-Si texturing processes. Another chemical
570 used to perform wet chemical etching is tetramethyl ammonium hydroxide (TMAOH). It is
571 also a cost-effective procedure and does not produce metal contaminations on the wafers
572 [51].

573 As mc-Si is composed of several Si crystals or grains with different orientations,
574 anisotropic etching cannot be applied efficiently for random pyramid texturization. For this
575 reason, isotropic etching in acidic solutions is the most cost-effective procedure to texture
576 mc-Si wafers. Acidic texturing is normally based on solutions containing hydrofluoric acid
577 (HF) and nitric acid (HNO₃) in acetic acid (CH₃COOH) or DI water [55, 56]. Also vapor
578 etching using these solutions [57] has been applied because of a resultant enhanced etching
579 rate control. Other alternatives to control the etching rate, such as NaOH/sodium hypochlorite
580 (NaOCl) based solutions, have been reported [58]. For mc-Si wafers, the challenge is to find
581 out a reproducible process to decrease the reflectance and to increase the photocurrent. The
582 research is currently focused on RIE processes [59].

583 In addition to traditional approaches to texturization, several alternatives have also
584 been developed. Laser texturing, lithography and plasma texturing are mainly used in
585 laboratory scale due to their cost and requirements [45]. Laser texturing is a promising
586 technique to obtain nanostructured surfaces under certain illumination and power conditions.
587 The types of surfaces obtained are known as black Si [60]. Using a femtosecond laser a
588 reduction of the reflectance to around 3% when this is used [61] has been reported. Recently
589 a two-step laser surface texturing process has been proposed and studied, where a high-
590 fluence laser ablation step was followed by a low-fluence laser-induced melting, producing a
591 molten material flow and re-solidification step to smooth the ablated dimple bottom surface
592 [62]. This study shows that the two-step laser surface texturing process can produce micro
593 dimples with very smooth bottom surfaces.

594 Plasma texturing, also called RIE, includes lithographic techniques in some cases.
595 This technique encloses different approaches as selective etching through alumina template,
596 SiO₂ micro-masks, catalytic action of various metals and nano-imprint lithography. These
597 approaches have been developed for the fabrication of sub-wavelength structure surfaces that
598 act as black Si.

599 **2.3.3 P-N junction formation: Doping from solid/liquid/gas sources**

600 When p-type wafers are used as base material, phosphorus incorporation on front side
601 of c-Si is performed to obtain p-n junction. There are several methods to carry out the step,
602 diffusion and ion implantation being the most usual processes. The obtained doping profiles
603 are highly dependent on the used technique. Doping by ion implantation is mentioned in Sec.
604 2.5.4.

605 If the diffusion process is considered, there are two possibilities from the point of
606 view of the dopant: (i) doping using solid/liquid sources, and (ii) doping using gas sources.
607 Doping from solid/liquid sources, also called dopant oxide solid source (DOSS) processes,
608 where a liquid doping, normally H₃PO₄ (phosphoric acid) or PCl₃ (phosphorus trichloride), is
609 spin coated on the surface and a phosphorus glass is formed when the samples are introduced
610 in the furnace. In this case, the doping is considered constant and finite, and the obtained
611 profile can be represented by an erfc function.

612 When doping from gas sources, a carrier with samples is introduced in a hot tubular
613 furnace. Pure nitrogen is used as a carrier gas guided through a container of liquid
614 phosphorus oxychloride (POCl₃) and released to the chamber mixed with oxygen to perform
615 the pre-deposition. This deposited material is a phosphorus silicate glass (PSG) and the flow
616 of POCl₃ is closed [27]. In comparison with the spin on dopant technique, in-line diffusion
617 from gas sources avoids contamination from the ceramic rolls on the conventional furnace,
618 and is the most widely used technique in commercial fabrication lines.

619 The thermal processes used to diffuse the dopants into the wafer are usually based on
620 the conventional furnace process (CFP) with a temperature around 850°C and times around
621 one hour. However rapid thermal processes (RTP) are increasing their importance [63]
622 because the diffusion time is reduced to the range of few minutes. In both the CFP and RTP
623 processes, after diffusion and thermal processes, phosphorus glass formed on top of the
624 wafers is etched away by using 10% HF solution.

625 Over the last decade, research in diffusion processes has been focused in its
626 optimization [52]. Current research in this step (i.e. emitter formation) is focused on
627 producing optimized selective emitters to enhance efficiency. This is discussed in Sec.2.5.6.

628 At this point it is also important to mention gettering (absorption) process. After
629 defect reduction in the saw damage etching step, electrically active metallic impurities in the
630 wafer are still present that reduce the lifetime of photogenerated carriers. The thermal
631 processes that diffuse the dopant to form the emitter can also neutralize the electrical activity
632 of some of these impurities by gettering (i.e. absorption of impurities) the locations along the
633 wafer into an inactive energy states, improving the diffusion lengths in the material. This
634 gettering process can also be introduced when Al-based contacts are fired in the fabrication
635 process of the cell. Just as etching is used for the formation of texturing and saw damage
636 etching simultaneously, the formation of the emitter and the firing of Al-based contact are
637 simultaneously used for producing gettering on the electrically active metallic impurities.

638 **2.3.4 Anti-reflection/passivation coating**

639 The c-Si solar cell has two types of losses - optical and electrical losses. Optical losses
640 reduce the quantity of photons that can be absorbed in the Si wafer as they are reflected on
641 the Si surface or on the front side metallic contacts. Also, photons with energy shorter than
642 the bandgap are not absorbed.

643 Texturization, as discussed above, is one way to reduce optical losses. Another is the
644 deposition of ARC on the front side of the solar cell to enhance the solar radiation absorption
645 and, at the same time, to passivate the c-Si surface. C-Si wafers have an average reflectance
646 between 30% and 40% in the 300-1200 nm range, so an ARC is needed to improve the solar
647 cell. As the quantum efficiency (QE) of Si based solar cell is optimal at 600nm, the refractive
648 indices of air and Si at 600nm are 1 and 3.46, respectively, the ARC refractive index should
649 be around 2 and, consequently, the ARC thickness is around 75nm. For this purpose, Si
650 nitride (SiN) layer is deposited on the Si surface. This step is usually performed by means of
651 a plasma enhanced chemical vapor deposition (PECVD) system by mixing silane (SiH₄), and
652 ammonia (NH₃) in the reaction chamber to form SiN layer on top of Si surface [27].
653 Improvements in texturization has resulted in a strong focus on SiN as ARC since specific
654 area and the light beam path are different in a pyramidal textured wafers in comparison with
655 non-textured wafers [64].

656 A surface passivation process consists of the saturation of Si surface bonds to improve
657 and stabilize the electronic properties of the surface. This is used to control and minimize the
658 recombination rate of the charge carriers at the surface, since the charge carrier
659 recombination velocity of an unpassivated surface is very high (around 10⁴-10⁶ cm/s), which
660 decreases the photocurrent.

661 The SiN anti-reflecting layer acts as effective surface passivation layer for Si surfaces,
662 matching both requirements simultaneously for the fabrication of c-Si based solar cells. As it
663 has been mentioned, this layer is normally deposited using the PECVD technique [65] at a
664 low-temperature of ~300°C. The effects of the bandgap and defects of SiN on carrier lifetime
665 and the transmittance in c-Si solar cells are currently being studied for increasing the values,
666 as the mixing of the precursor gases, flux ratios and temperatures greatly influence the final
667 properties of the solar cell.

668 Another option is indium tin oxide (ITO). This material is a transparent conductive
669 oxide widely used in solar cell applications. Its optical properties make it an excellent ARC,
670 and its high electrical conductivity allows it to improve the collection efficiency in solar cells.
671 Magnetron sputtering is the common technique used to deposit ITO. A subsequent annealing
672 of the wafer is required to improve the electrical properties of the device. Also, titanium
673 dioxide (TiO_2) has been largely used as ARC in solar cells because the deposition of this
674 material on the Si surface can be performed by atmospheric pressure chemical vapor
675 deposition (APCVD) at low-temperatures. Also, this material is non-toxic, non-corrosive, has
676 a low-cost and shows good surface passivation properties [66]. However, in the 1990s it was
677 replaced by SiN in the standard process because SiN has better surface passivation properties,
678 and can also passivate bulk defects by hydrogenation [23].

679 SiO_2 grown by thermal oxidation has also been used as ARC and surface passivation
680 layer. However the growth process here is carried out at high temperatures (900-1100°C),
681 making it expensive and incompatible with certain steps that do not withstand those high
682 temperatures. The refractive index of SiO_2 is also not as optimal as SiN for c-Si based solar
683 cells. The amorphous Si oxynitride films observed in the interface between SiO_2 /c-Si also
684 introduce recombination traps for carriers that reduce their lifetime. Alternatively, porous Si
685 formed by chemical [67], electrochemical [68] or vapor [57, 69] etching shows impressive
686 properties as ARC. Porous Si in combination with Si oxide (SiO_x , $0 < x < 2$) can be tuned to the
687 refractive index of the layer. However, the electrical properties of the Si wafer with porous Si
688 layers on the surface traditionally have been very poor for efficient solar cell applications
689 [70]. Hydrogen is the best passivating material for Si surfaces but it is meta-stable. Finally,
690 TiO_2 is an excellent ARC due to its high refractive index of 2.6 at 600 nm, and high
691 transmittance in the range of 300 and 1200 nm. Also, published results are promising because

692 it can be deposited by APCVD offering cost reduction and an easy implementation of this
693 alternative in the semiconductor industry [71].

694 **2.3.5 Metallization**

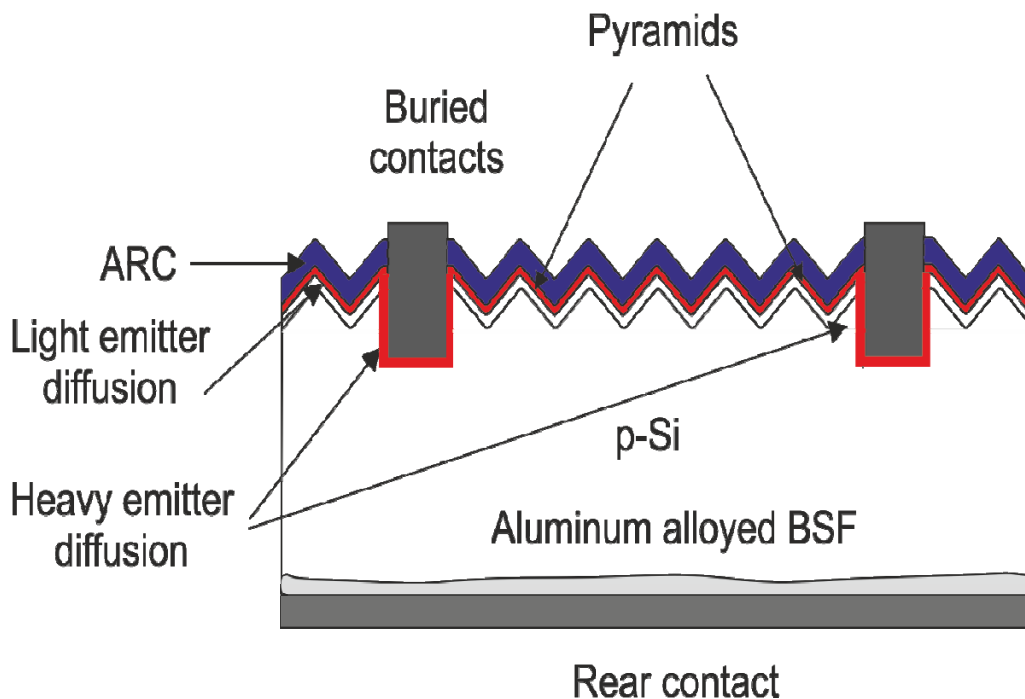
695 Once the p-n junction has been formed and the ARC deposited on top, the next step is
696 the metallization on the top and bottom side of the cell. The front side metallization is a grid
697 composed of busbars (usually two or three), and several thin fingers (70-100 μm wide) that
698 cover the front side of the cell. The front side metallization produces shadowing losses, series
699 resistance losses, and determines emitter diffusion profile and surface doping concentration,
700 and influences the choice of a defined surface passivation technique [72]. For p-type c-Si
701 wafer, Al is used for back contact and Ag is used for front contact.

702 A widely used technique to place the metallic contact is screen printing. In the mid-
703 1970s screen-printed solar cell was first developed [73]. This technique uses a paste, an Al
704 compound for the back side, and a Ag compound for the front side [74] with micrometric
705 metal particles and additives. These compounds are pressed to pass through a mesh of steel or
706 polyvinyl to print the metallic pattern on the Si surface. After the metallic paste is placed, a
707 firing process is required to produce an Ohmic contact on the Si surface. This technique is
708 commonly used for in-line c-Si solar cells manufacturing. It is a four step process that
709 involves: (i) Ag front side metallization and drying, (ii) Ag back side metallization (busbars)
710 to connect the solar cells into the solar module and another drying process, (iii) back side
711 blanket Al metallization, and (iv) the firing process, normally between 750°C-850°C [75]. A
712 complementary option is the finger roller-printing technique. This consists of a rubber wheel
713 coated with a thin layer of metallization paste that rolls across the wafer for finger contact
714 [76].

715 The rear contact also can be placed by physical vapor deposition methods such as
716 sputtering, thermal or e-beam based evaporation. Using these techniques the formed layers

717 show very high conductivities. Therefore to reach the performance needed, thinner contact is
 718 enough, compared to the screen-printed contacts [27].

719 One of the most promising techniques [77, 78], normally used with the selective
 720 emitter, is the buried contact metallization (Fig. 6). It was commercially applied first by BP
 721 Solar in the late 1990s. By means of laser fusion technology, it is possible to make a groove
 722 of approximately 20 μm wide and up to 100 μm deep into Si surface. This technique provides
 723 two advantages: (i) the reduction of the shadowing loss, from typically 8% from screen
 724 printing solar cells to around 3%, and (ii) the filling of the grooves with contact material,
 725 reducing around three times the standard width of the metallic, from typically 100 μm in
 726 screen printing to 30 μm widths.



727

728 Fig. 6 Cross-sectional diagram shows buried contact solar cell. Buried contact solar cell was developed more
 729 than 20 years ago and transferred to production line in the early 1990. Laser grooved buried contact solar cell is
 730 a high-efficiency commercial technology. Buried contact overcomes disadvantages of screen-printed contacts
 731 such as shadowing and series resistance caused by metal grid pattern. To lower shadowing loss and series
 732 resistance, metal contact is buried inside the cell with high aspect (height/width) ratio. Using this technology, a
 733 narrow strip of closely spaced metal grids can be used on the surface and at the same time high transparency can
 734 be maintained. In screen-printed solar cells, 5-7% of incoming light is blocked due to shadowing, whereas in
 735 buried contact solar cells, metal lines can be less than 20 μm and this corresponds to <3.5% shadowing. Lower
 736 shadowing loss results less reflection from the surface, and improvement in J_{sc} .
 737

738 The main reasons that the buried contact metallization has not been further introduced
739 in the industrial process for manufacturing solar cells are that this technique produces defects
740 on the Si surface, leading to decrease in cell performance and increase in the production cost.
741 Consequently, these drawbacks need to be overcome for the buried contact metallization to
742 surpass screen printing as the preferred technology for metallic contacts of Si solar cells.

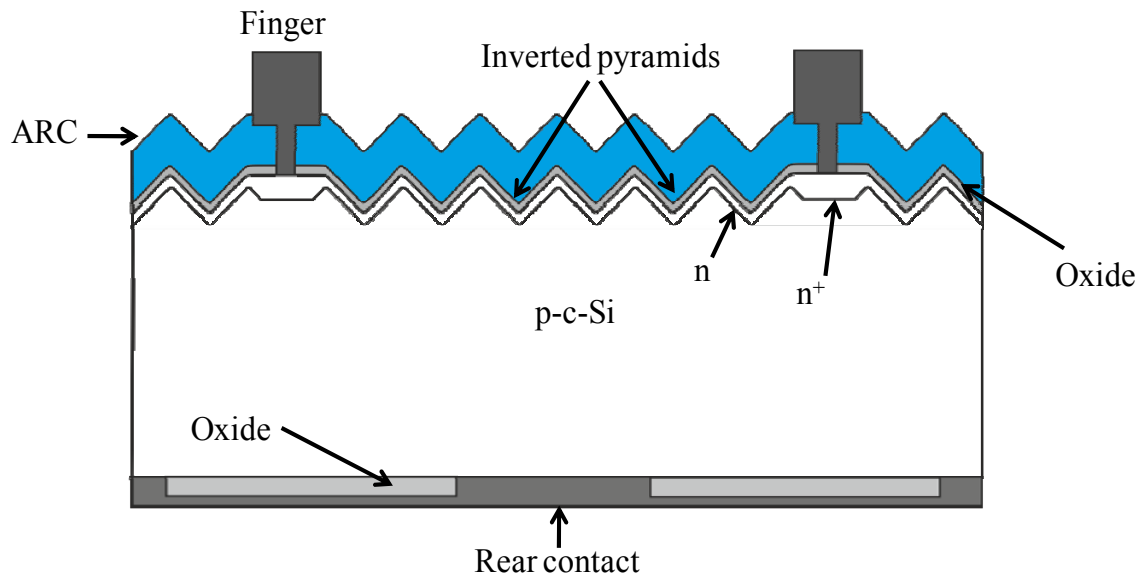
743 Currently, standard metals used for the front side and back side metallization are Ag
744 and Al, respectively. However other less expensive alternatives for the front side, such as
745 copper (Cu), has been studied for more than 10 years [79] to replace Ag. A recent work [80]
746 analyzes the current and future front side metallization scenario, suggesting that the
747 metallization with Ag is expected to be reduced in the coming next 10 years, decreasing from
748 the current 90% to a 50% of the market share. Simultaneously Cu and other alternative
749 materials will increase their relevance as substitutes of Ag. An important reason why one
750 metal may replace another over the years when it comes to solar cells is global demand-and-
751 supply of various metals.

752 **2.4 Other types of c-Si based solar cells**

753 Some of the solar cells discussed in this section are very expensive compared to the
754 ones obtained by the standard procedure described in Sec. 2.3 and commonly used in the
755 industry. However as research into these solar cells continues, a subsequent reduction in
756 production costs may be expected. At the same time, some of the features of these solar cells
757 may be incorporated to current commercial standard procedures and result in efficiency and
758 cost improvements.

759 As reported [81], advanced solar cells such as PERC, bifacial solar cells (light
760 sensitive on both sides) and n-type solar cells have gained relatively considerable attention. In
761 the PERC structure, as shown in Fig. 7, full area Al-BSF is replaced by a dielectric
762 passivation, which is locally opened for the placement of the metallic contact [82]. 21.2%

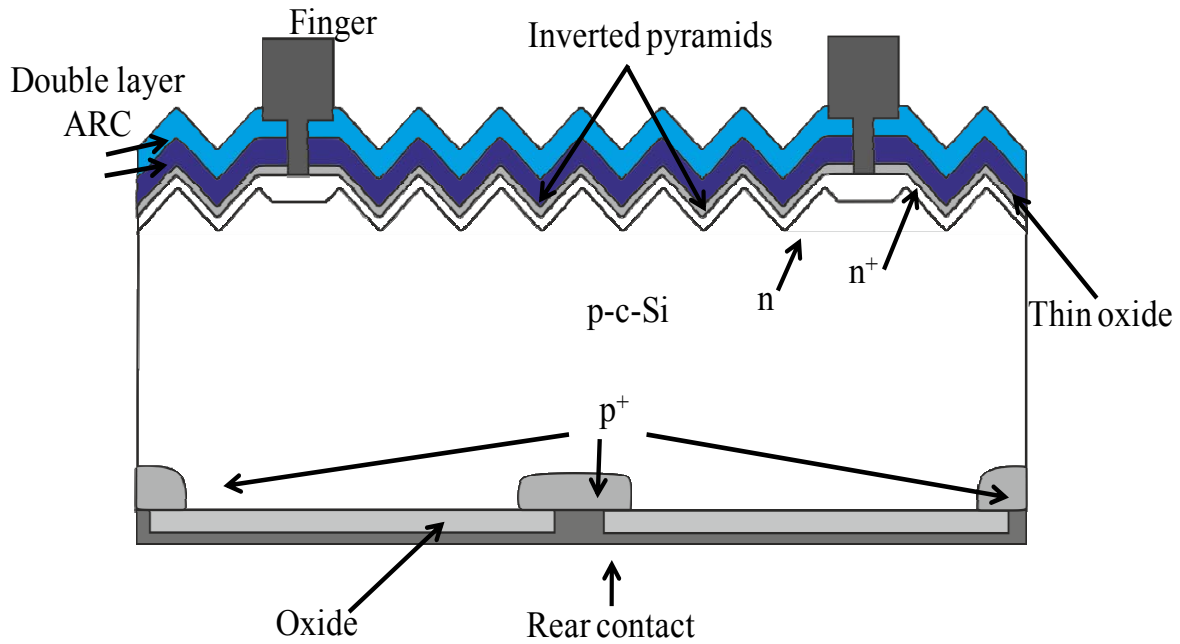
763 efficiency is the highest value reported so far [83]. Rear side dielectric passivation layer(s)
 764 improve passivation quality and internal reflection compared to full area Al-BSF.



765

766 Fig. 7 Schematic diagram shows cross-section of PERC solar cell structure. The rear side of PERC cell is
 767 passivated by dielectric/stack except at the region where contact metal is touching c-Si. Rear side dielectric
 768 (oxide) acts as mirror, reflects light into the bulk and thereby improving photocurrent. A major advantage of
 769 using rear side passivation instead of full area Al-BSF is the enhancement in J_{sc} that comes from enhanced
 770 reflectivity of 90-95% at 1000 nm compared to 65% from full area Al-BSF [84]. By reducing metallization
 771 fraction at the rear side, defects at metal/c-Si interface becomes less effective and the difference in V_{oc} and J_{sc}
 772 between PERC and PERL cells becomes small. When thinner c-Si is used for fabrication, reflectivity from rear
 773 structure becomes significant. PERC technology developed by Roth & Rau and successfully implemented under
 774 the name MB-PERC.

775 In other words, compared to full area Al-BSF cell, PERC advantages are lower SRV
 776 and an improved optical performance. However, additional reduction of the SRV and optimal
 777 use of high-resistivity materials can be performed in the PERL cell structure, which has at
 778 present 1 sun world efficiency record of 25% for c-Si based solar cells since 1998. PERL
 779 type bifacial structures have also been introduced in the industrial production lines over the
 780 last 5 years, substituting the inverted pyramids by chemically formed pyramids. Cross-
 781 sectional diagram of PERL cell is shown in Fig. 8. Advantages and disadvantages of local
 782 BSF are discussed in Sec.2.5.7.

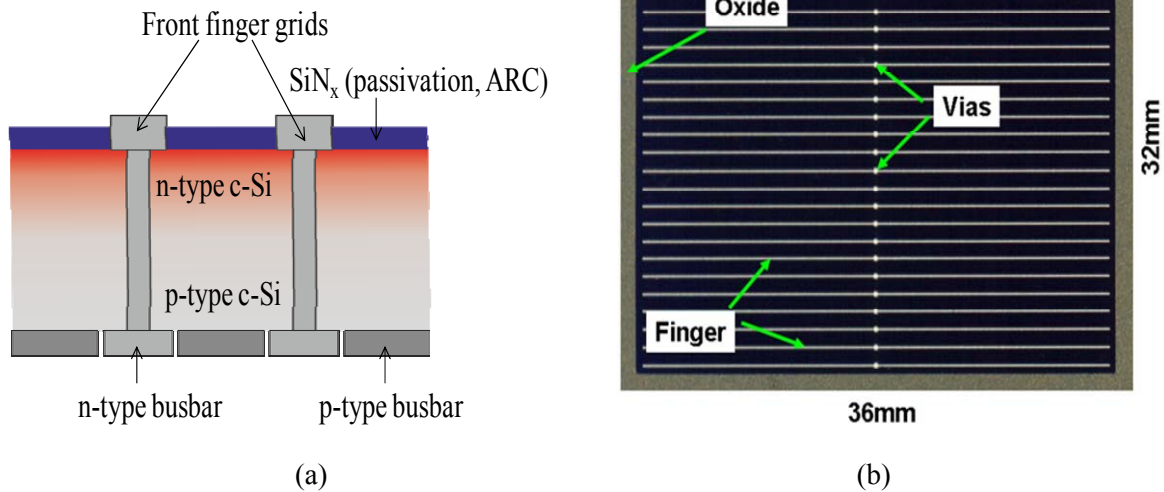


783

784 Fig. 8 Schematic diagram shows PERL solar cell structure. In the inverted pyramid surface, incident light
 785 undergoes double bounces meaning that incident light will have two chances of transmission into c-Si. In PERL
 786 structure, at the rear side, to reduce minority-carrier recombination at the metal/c-Si interface, boron diffusion is
 787 performed locally under the metal contact, whereas in PERC structure local diffusion is not performed under the
 788 metal contact. Local BSF in PERL cell improves V_{oc} and J_{sc} since electric field in the BSF region between p+/p
 789 junction drives electrons away towards the p-n junction and reduces surface recombination at the defective
 790 metal/c-Si interface. PERL cell technology named as Pluto was developed by Martin Green and Stuart Wenham
 791 at University of New South Wales and commercialized by Suntech Power.

792

793 The MWT solar cell is a back contact solar cell that uses a technology very similar to
 794 that of conventional screen-printed solar cells. MWT solar cell is shown in Fig. 9. As
 795 compared to conventional solar cell technology, only two additional steps are required, viz.
 796 (i) via drilling for the interconnection between front and back side, and (ii) the metallization
 797 through vias (holes). An efficiency gain of about 0.5% in absolute terms and a current gain of
 798 about 3.5% due to less shading on the front side are achieved as compared to the standard cell
 799 concept [85]. A highest average and peak efficiency of 19.6% and 20.0% has been reported
 800 for MWT c-Si solar cells [86].



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Fig. 9 (a) Schematic diagram of MWT solar cell [87], and (b) top view showing front finger grids and absence of busbars [88]. On the rear side busbars are wide and therefore, series resistance loss arising due to busbar can be eliminated. MWT cells have higher efficiency (~0.5%) than conventional solar cells due 50% less shading/metallization area on the front side [89, 90]. Less shading improves J_{sc} and fill factor. MWT c-Si solar cell technology has been transferred successfully to production [86, 91] and the cells have produced an average and peak efficiency of 19.6% and 20.0% respectively. For MWT cells, welding is not required when assembling MWT cells into modules and results in lower power loss and lower cell breakage rate. Fig. 9 (b) from [88], Tobias Fellmeth, Michael Menkoe, Florian Clement, Daniel Biro, Ralf Preu, Highly efficient industrially feasible metal wrap through (MWT) Si solar cells, *Solar Energy Materials & Solar Cells* 94 (2010) 1996–2001. © Elsevier 2010. License number 3457011111677.

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The EWT solar cells are similar to the MWT solar cells. The difference lies in the fact that here the n-type contacts are placed on the rear side. The rear surface of the wafer presents an emitter structure that is connected through with the front surface emitter. EWT solar cell is shown in Fig. 10.

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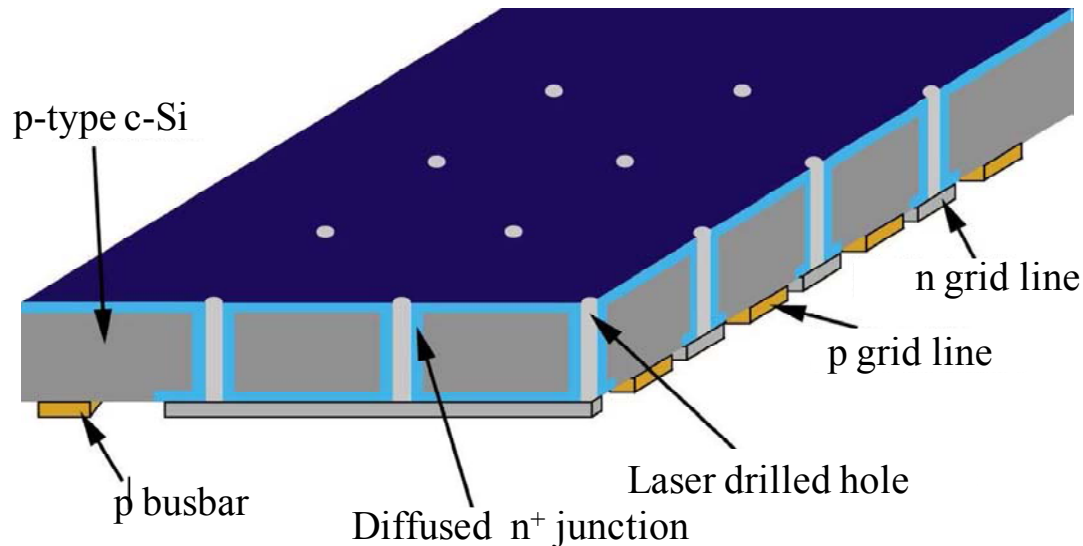
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The emitters on the front and rear side can both collect charge carriers. This makes the EWT cell very attractive for low lifetime materials. However this structure presents a series resistance problem [27]. Moreover expensive metallic formation techniques are required. The lack of significant current research focus on EWT, as gauged through the paucity of research publications per year, suggests that the future of EWT solar cells is uncertain.



823

824 Fig. 10 Picture shows EWT solar cell structure [92] quite similar to back contact back junction solar cell. Laser
 825 drilling is used to open 15000 vias (holes) having each $80\mu\text{m}$ diameter. Several thousands of vias/sec can be
 826 drilled [93]. In EWT cell, no grids lines, and no busbars are present on the light entering side (note that in MWT
 827 structure, grid lines are present on the light entering side, and no busbar is present). Both p-type and n-type grids
 828 as well as busbars are placed on the rear side, and trade-off between shadowing loss and series resistance is
 829 eliminated. Grid less front surface enhances light incident area and improves J_{sc} , fill factor since on the rear side
 830 grid lines and busbars can be wide. Reproduced from [92], James M. Gee, Prabhat Kumar, James Howarth,
 831 Todd Schroeder, Jeff Franklin, Jason Dominguez and David Tanner, Development of industrial high-efficiency
 832 back-contact czochralski-Si solar cells, Prog. Photovolt: Res. Appl. 19 (2011) 887. © Copyright 2011 John
 833 Wiley & Sons, Ltd. License number 3457020769998.

834

835 Another interesting area of current research is the realization of bifacial solar cell with

836 boron diffusion either from a gas source or a solid source such as a boron silicate glass. A

837 conversion efficiency of 18.4% has been obtained on c-Si wafers using boron BSF and Si

838 carbide (SiC)/SiN ARCs. This structure easily fits with the development of a selective emitter

839 at the front side of the cell and can potentially achieve conversion efficiencies above 19%

840 [94].

841 2.5 Low-cost c-Si based solar cells

842 Since cost and efficiency of solar cells are the most important determining factors for

843 commercial utilization, it is worthwhile to further explore how these issues are being

844 currently addressed. In the context of solar cell development, low-cost always refers to cost

845 per unit of energy or power, being the figure of merit $\$/\text{Wp}$ preferred to that of $\$/\text{kWh}$ due to

846 the fact that the former focuses on technology and discards the influence of radiation, system

847 reliability and other factors. Lowering the cost means minimizing the \$/Wp, and to fulfill this
848 goal, two approaches can be followed: reduce the numerator (so, looking for cheaper
849 processes) or increase the denominator (so, producing more efficient cells), or both.

850 To lower the cost of c-Si solar cell, the following routes are pursued: use of lower
851 quality Si feedstock and wafers, search for cheaper dopant sources, and search for cheaper
852 metallization schemes. To increase the efficiency, the efforts in the field of front junction
853 solar cells have been focused in implementing selective emitters at the front and reducing
854 BSF recombination at the rear by industrially feasible processes. All these concepts are
855 reviewed in the following sections.

856 **2.5.1 Low-cost Si wafers: Relaxing feedstock specifications**

857 The raw material for Si solar cells has traditionally come from the polysilicon market
858 for microelectronics, providing a ultrapure feedstock at a cost that accounts for around 15%-
859 20% of the total PV module cost (in \$/Wp). The availability of Si due to the tremendous
860 growth of the PV sector and the search for cheaper purification routes have motivated
861 research into alternatives to the traditional so-called Siemens process. As mentioned in Sec.
862 2.2.1, in this process, metallurgical Si is transformed into a volatile compound, typically
863 TCS, which is further purified and then converted back to solid Si in a chemical vapor
864 deposition process. Some of the alternatives rely on the same basis, but introduce significant
865 changes in certain steps of the process. For example, using SiH₄ as the intermediate volatile
866 compound produces Si deposition in a fluidized bed reactor or a free space reactor [95]. Their
867 promoters claim that the quality of the resulting material is similar to the conventional one, so
868 no further adaptation of the solar cell process is needed. Recycling the byproducts efficiently
869 is also an option.

870 Another group of alternatives avoids the conversion of metallurgical Si into a volatile
871 compound, and upgrade the metallurgical Si through a combination of steps suited for

872 different impurities [96,97], decreasing to some extent the energy consumption in the
873 deposition step and hence the cost of the process. The purity usually reached with these
874 processes is lower than that of the TCS route, but that does not necessarily mean that the
875 material cannot be used for solar cells. In fact, by introducing some changes in the thermal
876 profiles of the crystallization and solar cell processing steps, similar solar cell efficiencies
877 have been achieved with this material to the semiconductor grade one [98-101].

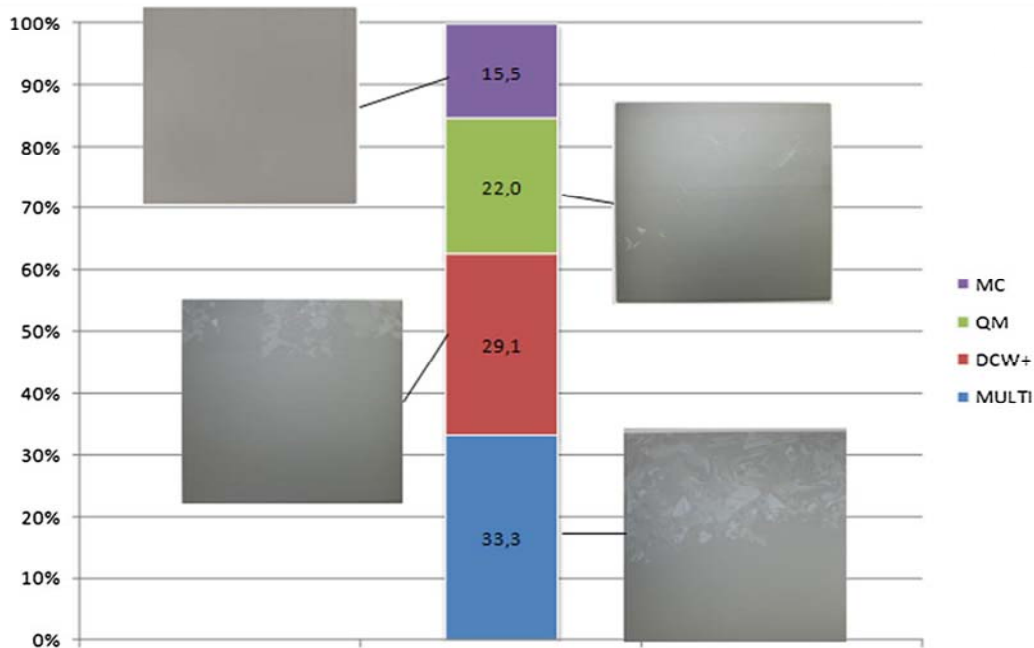
878 At a broader level, though, a drastic reduction in cost of conventional polysilicon is
879 hindering the development of these alternatives. In order to be commercially viable, there is a
880 need to clearly justify their good performance versus satisfactory yield and cost-effectiveness
881 in order to undertake the large investments with the production.

882 **2.5.2 Producing cheaper wafers**

883

884 Si wafers for solar cells are made by slicing ingots grown by either monocrystalline
885 technique or the multicrystalline one. Recently, a new crystallization process has been
886 proposed that aims to combine the high-throughput of the latter with the better quality of the
887 former. This is done through the use of monocrystalline seeds on the bottom of the crucible in
888 a directional solidification furnace [102]. It has been called mono-like or quasi-mono, due to
889 the fact that the ingot is not 100% monocrystalline, as crystals of different orientations
890 nucleate from the walls of the crucible. Figure 11 depicts an example of wafer-type
891 distribution. Even though efficiency increases of 1-1.5% in absolute have been reported
892 compared to traditional casting, to fully exploit the potential of the material a few issues
893 should be industrially addressed: the need of sample classification to apply different solar cell
894 process conditions to different samples (which comes for example from the different
895 texturing techniques applied to mono and multi wafers), and the fact that part of the material,
896 even the monocrystalline one, is rich in dislocations [103-105].

897



898

899 Fig. 11 Wafer-type distribution of a mono-like ingot according to their percentage of macroscopic
 900 monocrystalline feature: MC: mono-casting (100% mono); QM: quasimono (>90% mono); DCW+
 901 PLUS (>75% mono); MULTI: mono/multi and mc-Si (<75% mono). With permission from [105], Ismael
 902 Guerrero, Vicente Parra, Teresa Carballo, Andrés Black, Miguel Miranda, David Cancillo, Benito Moralejo,
 903 Juan Jiménez, Jean-François Lelièvre, Carlos Cañizo, About the origin of low wafer performance and crystal
 904 defect generation on seed-cast growth of industrial mono-like Si ingots, Prog. Photov. Res. Appl. **22** (2012)
 905 923. Copyright © 2012 John Wiley & Sons, Ltd. License number 3457490569073.

906

907 Another approach that offers the advantage of eliminating the slicing process is the

908 growth of thin Si ribbons directly from a polysilicon melt. Several technologies, such as edge

909 defined film-fed growth, string ribbon, dendritic web (WEB, recently revisited as Ribbon on a

910 Sacrificial Template), and ribbon growth on wafer has been promoted [106]. Industrial

911 efficiencies in the range of 15-16% have been reached by the most advanced techniques,

912 while others are on the 13-14% level [107-109]. With more sophisticated processing,

913 efficiencies around 18% have been reached [110,111]. Although their cost reduction potential

914 remains, there are also other current market conditions that are slowing their development.

915 The drawback of all of them is the high density of defects (dislocations, grain boundaries,

916 impurities) and the uneven surfaces that require specific processes for texturing, phosphorus

917 diffusion, SiN) deposition or screen printing for implementing in the solar cell process. These

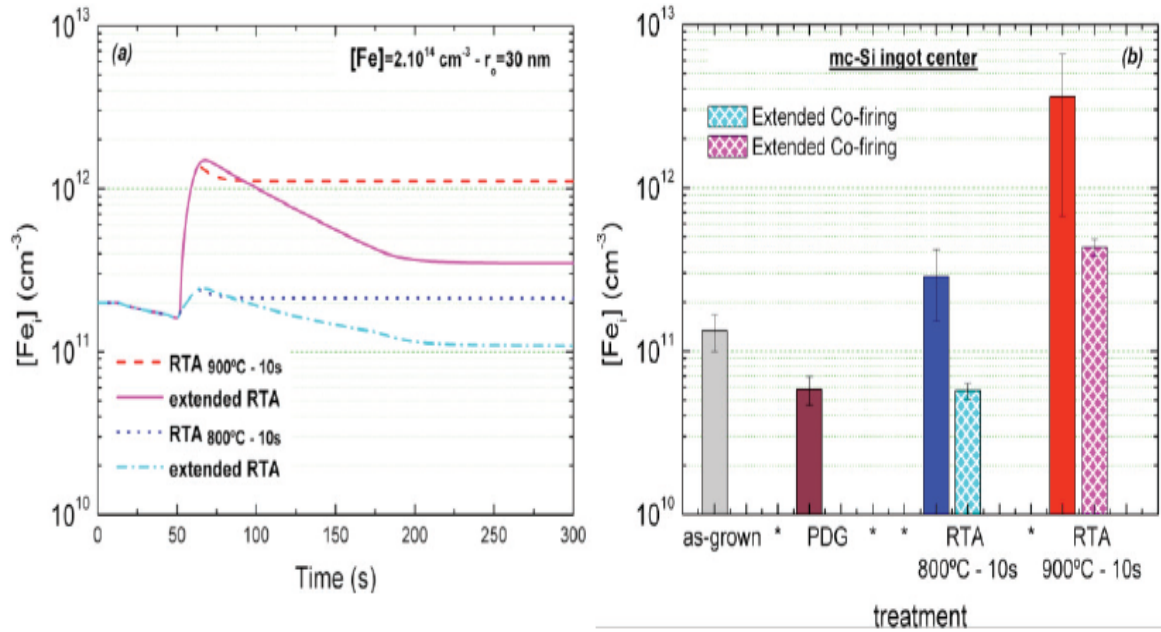
918 processes may even need replacement with alternative techniques, for example, the direct
919 writing of Ag pastes for metallization [112,113].

920

921 **2.5.3 Living with defects and impurities**

922

923 Solar cell processing should integrate steps that can reduce the deleterious effect of
924 impurities and crystalline defects. These steps are gathered under the concept of defect
925 engineering. In fact, solar cells made of traditional Si sources already benefit from them, in
926 particular from external gettering of impurities to the phosphorous and Al layers, as we
927 explained in Sec. 2.3.3. In wafers from low-cost sources, or even in those coming from the
928 border and edge regions of multicrystalline ingots where the density of impurities is higher
929 due to in-diffusion from the crucible, defect engineering techniques aim at manipulating
930 metal concentrations and distributions to reduce their impact in solar cell performance [114].
931 For example, it has been shown that a slow cool down or a low-temperature plateau after
932 phosphorous diffusion reduces iron (Fe) interstitials, and increases carrier lifetime and solar
933 cell efficiency [115-117]. Other strategies such as implementing thermal pretreatments or
934 changing the firing step thermal profiles are being studied [118-120]. As an example taken
935 from Ref. [119], Fig. 12 compares the effect of a standard firing step (realized in this case in
936 a RTP furnace), which produces an increase in interstitial Fe concentration due to precipitate
937 dissolution. On the other hand, with a modified one (which is called extended RTP)
938 segregation gettering is enhanced and so contamination levels are reduced.



939

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942 Fig. 12 (a) Simulated interstitial iron $[Fe_i]$ concentration as a function of time during a 10s standard and
 943 extended RTP, for two different process temperatures and an arbitrary as-grown Fe concentration and
 944 distribution, (b) measured Fe_i concentration obtained for mc-Si wafers taken from the center of an industrial
 945 ingot, showing the reduction due to the extended RTP (stripped bars) as compared to the standard (full bars).
 946 Reproduced from [119], S Glunz, A Aberle, R Brendel, A Cuevas, G Hahn, J Poortmans, R Sinton, A Weeber,
 947 J-F. Lelièvre, J. Hofstetter, A. Peral, I. Hoces, F. Recart, C. del Cañizo, Dissolution and gettering of iron during
 948 contact co-firing, Energy Procedia, **8** (2011) 257. Copyright © 2011 Published by Elsevier Ltd. License number
 949 3457501260401.

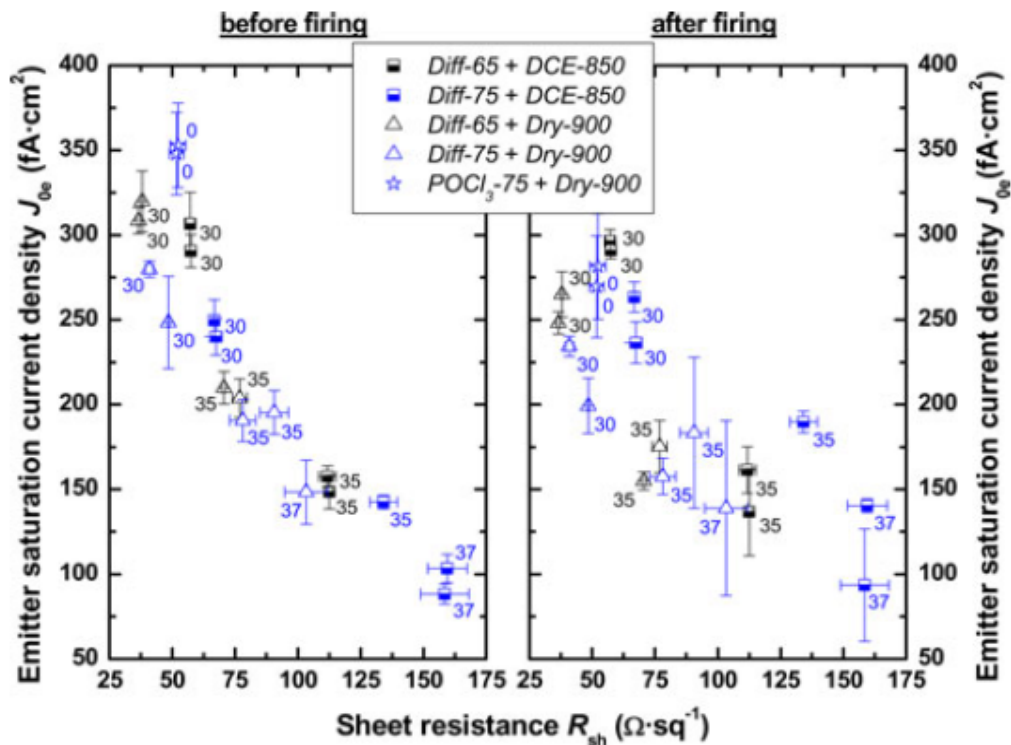
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951 The challenge here is to implement defect engineering techniques at the industrial level,
 952 where modifying thermal step profiles can impact throughput, and where tailoring processes
 953 to specific wafers introduces further complexity.

954 2.5.4 Low-cost approaches for doping

955 Emitter doping from a $POCl_3$ liquid source in a quartz furnace has the drawback of being
 956 a batch type process, and in-line options are promoted, where a phosphorus source is applied
 957 to the wafer surface, dried, and then diffused in an infra-red belt furnace, benefiting from
 958 automation, high-throughput and the ability to implement temperature profiles. Dopant
 959 sources can be screen-printed [121], spun-on [122-126], sprayed-on [127-130], deposited by
 960 CVD [131] or even diffused from a gas source [132]. In some of the reported experiments,
 961 dopant drive-in is performed by RTP and not in an infrared furnace.

962 Efforts in characterizing emitter performance have been successfully applied, in terms of
 963 dopant diffusion, sheet resistance and emitter saturation current. An example of the
 964 comparison of the saturation current with state-of-the-art POCl_3 diffusion is given in Fig.13,
 965 taken from Ref. [131].
 966



967
 968 Fig. 13 Emitter saturation current densities (represents sum of all recombination currents in the emitter),
 969 obtained from lifetime measurements, of passivated samples doped by the method proposed on [127] before and
 970 after firing. Values for two different diffusion processes (Diff-65 and Diff-75) and two different oxidation
 971 processes (DCE-850 and Dry-900) are given. The values are under those of a typical POCl_3 process (which is
 972 marked with stars with the number 0). Reproduced with permission from [131], Fallisch A, Wagenmann D,
 973 Keding R, Trogus D, Hofmann M, Rentsch J, Reinecke H, Biro D., Analysis of Phosphorus-Doped Si Oxide
 974 Layers Deposited by Means of PECVD as a Dopant Source in Diffusion Processes. IEEE J. Photovoltaics, 2
 975 (2012) 450. Copyright © 2012 IEEE. License number 3504480294880.

976
 977 Solutions currently exist that take advantage of these low-cost doping technologies,
 978 addressing key aspects such as emitter homogeneity, lack of shunting and gettering ability,
 979 and successful implementation of emitter profiles with convenient sheet resistances.
 980 Furthermore, some of these approaches have the potential to achieve high-efficiencies, with
 981 efficiencies of 18%-19% being reported for c-Si [125,126] and 15%-16% for mc-Si [123,133]
 982 based solar cells.

983 Boron, as a p-type dopant can substitute Al in BSF layers, reducing recombination
984 and bowing, and can also form the p-n junction on n-type c-Si wafers. Cost-effective
985 techniques to diffuse boron are being promoted [134-136], as the traditional boron tribromide
986 (BBr_3) source in a diffusion furnace implies a batch type process, and a somewhat involved
987 process optimization [137,138]. The use of these alternative dopant sources can also facilitate
988 the implementation of local BSFs. Passivation of boron doped layers is also an aspect that
989 needs specific solutions [139].

990 Finally, ion implantation is another option, for both phosphorus and boron doping
991 [140,141] that benefits from its wide use in microelectronics. Ion implantation allows for an
992 accurate control of the dose and depth of the dopant, and needs a subsequent annealing to
993 reduce the damage introduced by the implantation.

994 **2.5.5 Low-cost approaches for metallization**

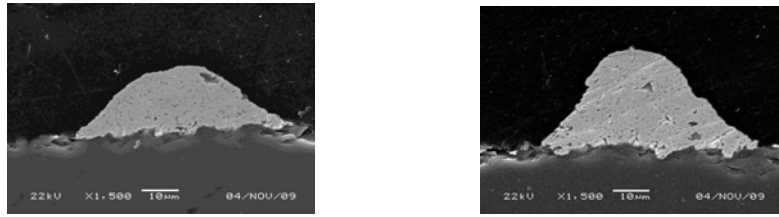
995 Traditional screen printing metallization is evolving towards lower consumption of
996 expensive Ag, thinner fingers to improve the aspect ratio (height/width), and different paste
997 formulation to contact lowly doped emitters. Substituting mesh screens by stencil-based
998 screens may help to reach finer lines (50-60 μm) with better aspect ratios, and benefit from a
999 slower deterioration of the printed patterns [142]. Separating screen printing for fingers and
1000 busbars (which is called dual printing) may help in optimizing separately geometry and paste
1001 formulation [143].

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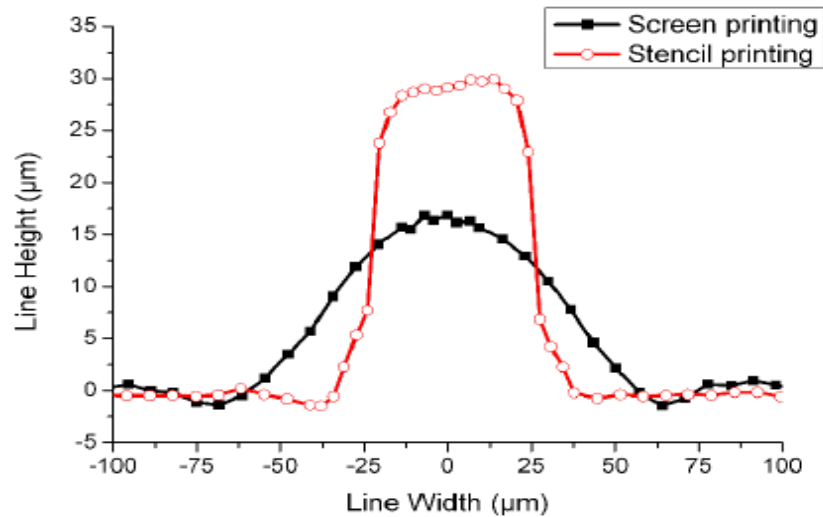
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1007

(a) Single print

Double print

(b)



1008

1009 Fig. 14 (a) Finger cross-section of single and double print [143], (b) Fired finger profile comparison between
 1010 stencil (60µm) and screen (105µm opening) [142]. Figure 14 (a) from [143], Tung Pham, Weiming Zhang,
 1011 Tracy Gou, Dean Buzby, Kristin Murphy, Improving electrical performance by double print method and non-
 1012 contact busbars, 25th EU PVSEC/5th World Conference on Photovoltaic Energy Conversion, 6-10 September
 1013 2010, Valencia, Spain, pp.2378-2380, permission granted. Figure 14 (b) from [142], Hoornstra J, Heurtault B,
 1014 Stencil print applications and progress for crystalline silicon solar cells, 24th EU PVSEC Proc. European
 1015 Photov.Sol .Ener. Conf., 21-25 September 2009, Hamburg, Germany 2009, pp.989-992. Permission granted.

1016

1017

Another approach that is compatible with the use of stencil screens or the dual

1018

printing is to separate metal deposition in two steps: first a layer designed for good contact

1019

with Si is deposited, which is followed by a second layer designed to increase conductivity.

1020

The simplest would be to optimize the properties of two different pastes that are being used in

1021

industry as double printing or print-on-print [144,145]. Alternatively, the contact layer can be

1022

done by roller printing [146], pad printing [147] or nickel plating [148]. Inkjet printing is also

1023

being explored, as it can produce thin lines and as a non-contact method it can avoid

1024

mechanical problems with very thin wafers [149]. To overcome limitations in metal particle

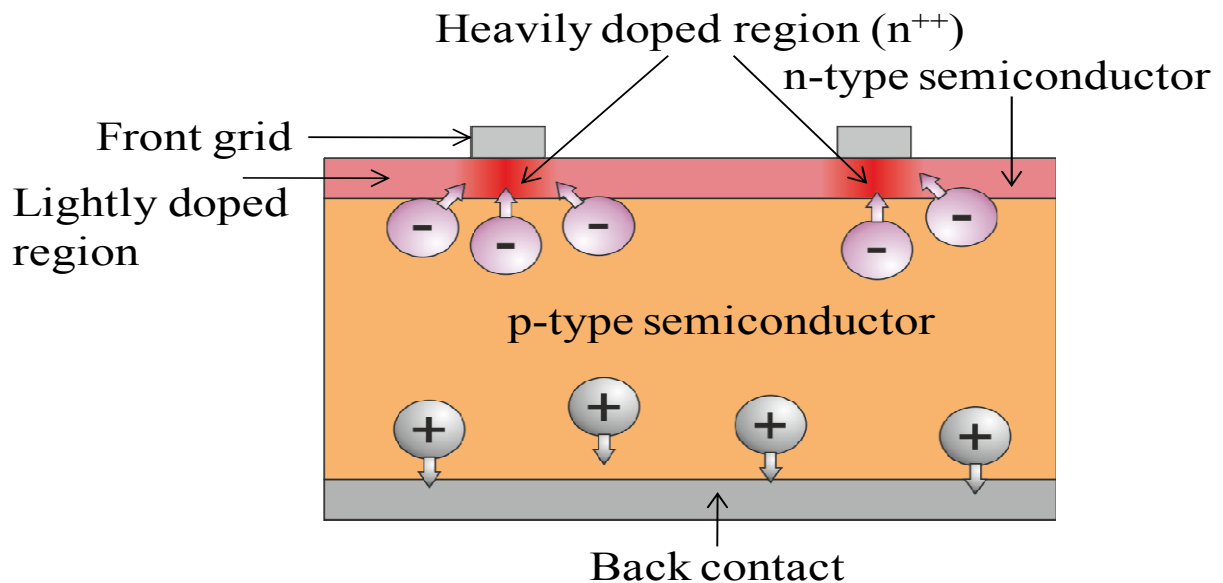
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sizes that may obstruct the printer, an aerosol technique can be implemented instead [150].

1026 For thickening of the layer, light-induced electroplating is a good candidate that can give very
 1027 favorable aspect ratios [151]. Examples of techniques resulting in improved finger cross
 1028 sections are shown in Fig.14. The challenge in all these cases is to implement the techniques
 1029 at the industrial level with sufficient throughput and reproducibility [152].

1030 **2.5.6 Efficiency enhancement: Industrially feasible selective emitter technologies**

1031
 1032
 1033 A selective emitter [153] is formed by heavily doping underneath the contact grid and
 1034 by weakly doping the illuminated area (Fig.15). This doping also results in an adequate sheet
 1035 resistance to improve the electrical properties of the front metallic contact and low resistance
 1036 in the illuminated areas.



1037

1038 Fig. 15 Schematic diagram shows the location of the selective emitter having a low sheet resistance of 35-55
 1039 Ω/\square . A selective emitter is a front junction, front contact solar cell configuration. Using this approach, in
 1040 selective regions, i.e. surface regions underneath the grids are heavily doped to improve electrical (ohmic)
 1041 contact between the grid and Si. The remaining emitter surface regions between the grids are lightly doped to
 1042 minimize recombination losses and to improve cell's blue response. In other words, selective emitter structure is
 1043 used to reduce losses originating from the front side. Selective emitter can be formed by laser doping, doped Ag
 1044 paste, screen printing, etchback etc.

1045

1046 The optimum emitter profile is different for a contacted region than for a passivated
 1047 non-contacted one (with higher surface concentration and longer junction depth in the first
 1048 case). While in traditional cells a design compromise is reached, resulting in emitters of 50-
 1049 75 Ω/square , the process here can implement selective emitters, provided the gain in

1050 efficiency justifies the increase in complexity. While selective emitters have been
1051 implemented in laboratory cells since long ago [154], recent efforts have succeeded in
1052 adapting the concept to an industrial environment through the use of a number of techniques
1053 [153].

1054 (i) Performing two separate diffusions, a heavier one restricted to the regions to be metallized
1055 by a screen-printed or deposited by mask [155].

1056 (ii) First diffusing a homogeneous thick emitter by conventional means; then applying a
1057 screen-printed or inkjet mask to protect the regions to be metallized, and removing the
1058 superficial dead layer in the non-protected region by a plasma etch [156], a wet etch [157] or
1059 an etching paste [158].

1060 (iii) Diffusing a solid dopant in the areas to be contacted, so that a highly doped emitter is
1061 formed there, while a much lighter diffusion takes place at the uncovered regions from the
1062 gas phase [159].

1063 (iv) Protecting the regions that will not be contacted with a mask, so that during phosphorous
1064 diffusion a highly doped emitter is formed in the non-protected areas, while under the
1065 protected ones only a smaller dose of dopant is able to diffuse into the Si because the mask
1066 slows down penetration, giving thus a low doped emitter there. The mask is subsequently
1067 removed [160].

1068 (v) Forming first a high sheet resistance emitter, and then screen printing a metallization
1069 paste containing phosphorus, so that when firing, a heavily doped alloyed layer is formed
1070 under the metal fingers [161]. The drive-in of the heavier doped region can also be done by
1071 laser [162].

1072 Most of these techniques require some kind of pattern aligning to print the front contact
1073 fingers on the heavily-doped regions, something suitable for state-of-the-art automatic
1074 equipment. Gains in absolute efficiency of around 0.5% have been reported.

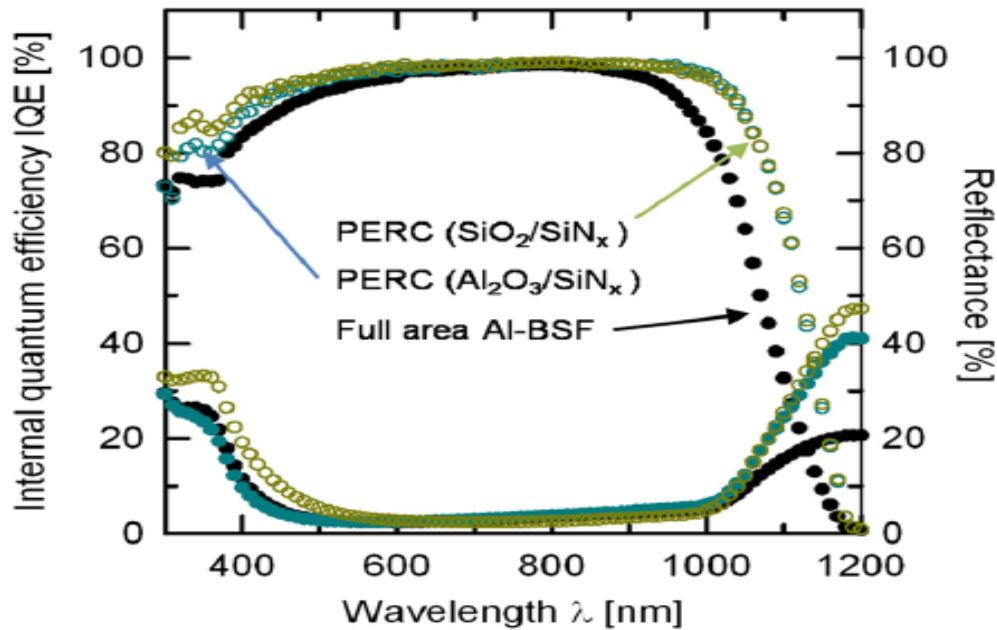
1075 **2.5.7 Local BSF at the rear: Advantages and drawbacks of the technologies**
1076 **implemented in industry**
1077

1078 Passivating the rear surface with a dielectric film can increase cell efficiency, especially
1079 for wafers where carrier diffusion length is higher than thickness. Rear side recombination can
1080 be reduced as compared to a full BSF, and good reflecting properties can be achieved,
1081 provided the Si surface morphology is adequately prepared [163]. The rear metal contact can
1082 be implemented locally, in dots or lines, together with a BSF, or without it. In the second
1083 case, attention should be paid so that contact resistance is maintained in reasonable levels.

1084 Since this concept has been implemented to produce high-efficiency laboratory solar cells
1085 [164], efforts have been made to transfer this technology to industry, with the focus on
1086 throughput. Layers such as SiO_x [165], Al oxide [166], Si oxynitride [167] and SiC [168] are
1087 the best potential candidates. A-Si:H has been also applied as rear side passivating layer
1088 [169], but its full potential is exploited in the heterojunction structure, as discussed in Sec.4.

1089 Care must be taken with the potential loss of passivation due to the subsequent
1090 metallization, as high-temperature steps can degrade the passivating properties of the layers
1091 [170,171]. Another issue is the possibility of shunting by interaction between the layer and
1092 the metallization due to the existence of charges in the layer, as is the case of SiN layers
1093 [172].

1094 With proper process optimization, or by combining several layers in stacks, the low
1095 effective rear surface recombination velocities, in the range of few cm/s, have been
1096 successfully obtained in solar cells to improve efficiency [173-177]. A clear proof of the gain
1097 obtained with the rear surface passivation can be seen in the internal quantum efficiency
1098 (IQE) curve in an example taken from Ref. [145], and shown in Fig. 2.16.



1099

1100 Fig. 16 Comparison of internal quantum efficiency and reflectance between cells with different rear passivation
 1101 stacks, $\text{Al}_2\text{O}_3/\text{SiN}$ and SiO_2/SiN , as compared to a full-area Al-BSF reference cell [145]. With permission from
 1102 Thorsten Dullweber, Sebastian Gatz, Helge Hannebauer, Tom Falcon, Rene Hesse, Jan Schmidt, Rolf Brendel,
 1103 Towards 20% efficient large-area screen-printed rear-passivated Si solar cells, Prog. in Photov: Res. Appl., **20**
 1104 (2011) 630. Copyright © 2011 John Wiley & Sons, Ltd. License number 3457590457465.
 1105

1106 2.6 Future outlook

1107 Efficiency of traditional c-Si solar cells has increased relatively significantly since
 1108 their invention in the mid-twentieth century. To a great extent this has been due to several
 1109 improvements related to larger photon and charge carrier collection, improved
 1110 photoconversion processes, and shadowing reduction, as has been mentioned in previous
 1111 sections. Consequently, the current efficiency for commercial c-Si solar cells is quite close to
 1112 the world records obtained in lab. Due to the mass scale adaption of laboratory techniques in
 1113 the industry, such as buried contacts, selective emitters, etc., in recent years the cost of these
 1114 new techniques has been lowered sharply. One of the most important challenges of the c-Si
 1115 technology is to increase short-circuit current density (J_{sc}), using low-cost manufacturing
 1116 processes. Currently, the results obtained applying the RIE process are very promising, and
 1117 its inclusion in the commercial production lines may be explored in to increase the J_{sc} values.
 1118 Other improvements, such as the introduction of back reflectors, can be implemented with the
 1119 current state-of-art of the metallization techniques such as evaporation. The main challenge

1120 for this technique is to become as cost-competitive as screen printing. Multilayers are also an
1121 attractive option for improving the J_{sc} values, especially as the price of the PECVD systems
1122 dropped in recent years. In order to improve the open-circuit voltage (V_{oc}) of the solar cells,
1123 ion implantation is one of the most interesting techniques to obtain more repeatable profiles.
1124 Also, it is possible to obtain higher accuracy in the doping profile, and also improve the
1125 current selective emitter formation procedure. However, due to Si material properties, V_{oc} for
1126 a single-junction solar cell is now very close to the theoretical limit. Further incremental
1127 improvements in V_{oc} require investments in sophisticated fabrication/manufacturing
1128 techniques, which will increase the cost. Finally, to reduce shadowing losses new pastes and
1129 materials have been tested in laboratories in recent years, which show remarkable results in
1130 terms of electrical performance improvements. Consequently, in the next 5 years narrower
1131 and thinner metallic contacts in the solar cells will be commercially applied to c-Si solar
1132 cells. These new materials will reduce shadowing and, at the same time, result in low series
1133 resistance. On a side note, the main challenge in solar cell is to reduce surface/bulk defects to
1134 achieve low emitter saturation current density.

1135 Conventional front junction cells also continue to make rapid advances. Many
1136 alternatives to front junction solar cells with front and rear contacts are being promoted, and
1137 the traditional structure has demonstrated strong potential to reduce costs. Over the last
1138 several years, impressive improvements have been achieved thanks to a successful transfer to
1139 industry of some of the concepts being pursued by the research community. These have
1140 included the use of lower cost feedstock, cheaper ingots and wafers, development of low-cost
1141 dopant and metallization schemes, and implementation of selective emitters and rear
1142 passivating stacks. These achievements have brought the cost of c-Si PV modules well below
1143 \$1/Wp (excluding balance of systems), a reduction of around 75% in ten years. There is
1144 however still room for further improvement of front junction solar cells towards the

1145 \$0.50/W_p range, thanks to technology improvements and economies of scale. In a tough
1146 competitive environment, those concepts combining the lowest costs with the highest
1147 improvements in efficiency will become dominant.

1148 **3.0 c-Si based solar cells: Back junction**

1149
1150 The major advantage of the interdigitated back contact (IBC) c-Si solar cells is the
1151 absence of front side metallization grid, since both p-type and n-type metal electrodes for
1152 emitter and base respectively are located on the rear side of the solar cell. Due to the absence
1153 of front side metallization grid, IBC cells exhibit zero-shading losses, which results in
1154 strongly increased J_{sc} . Moreover, the front surface can be optimized for optimum light
1155 trapping and surface passivation properties, without having to allow for the low contact
1156 resistance. This way the front surface recombination can be reduced and light trapping
1157 improved. Furthermore, the series resistance losses of the metallization grid can be reduced,
1158 because both electrodes are on the back side where the width and thickness of the
1159 metallization grid is not limited by the shading losses. All of these positive effects result in a
1160 relatively very high-efficiency potential of this type of c-Si solar cell.

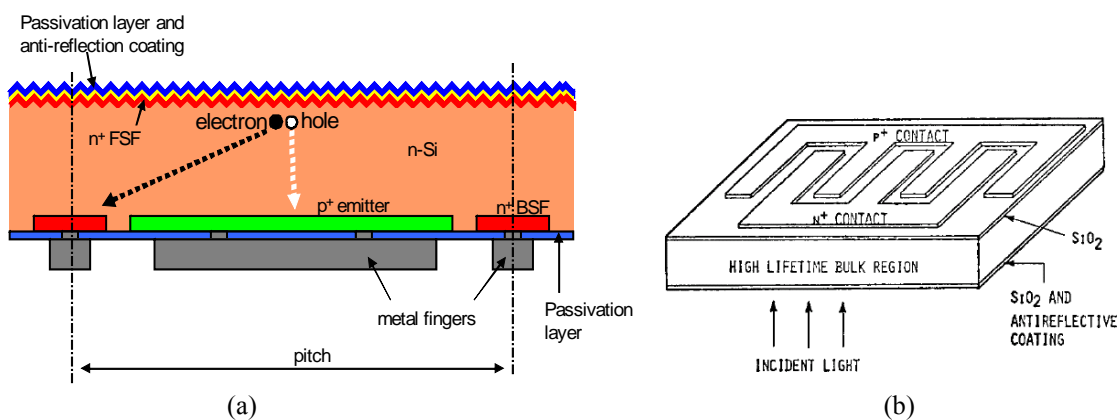
1161 **3.1 Introduction**

1162 The schematic diagram of IBC back junction solar cell is shown in Fig. 17. A
1163 remarkable example of the high-efficiency potential of this cell structure are the IBC cells
1164 developed by the SunPower Corp., with the highest reported efficiency for the large-area
1165 (155.1 cm^2 n-type Cz c-Si) IBC solar cell of 24.2% [178], and module based on IBC cells
1166 with efficiency over 20% [179]. The decrease in module efficiency is attributed to the fact
1167 that (i) the module area is not fully covered with solar cells (i.e. there is inactive area), (ii) the
1168 encapsulation foils and glass sheet in module introduce additional optical losses, and (iii)
1169 finally the interconnections of the individual solar cells in the PV modules cause some
1170 resistive losses.

1171 The IBC cell structure also offers advantages for the module manufacturing. Both
 1172 electrodes on the rear side allow for the potentially easier and fully automated co-planar
 1173 interconnection of the back-contact solar cells in the module assembly process. The issue of
 1174 the module technology for the interconnection of the IBC cells is under investigation and
 1175 should allow for further reduction of the PV modules based on the IBC cells structure [180-
 1176 182]. Also, the attractive and uniform appearance of the finished IBC modules should be
 1177 noted, as it is especially of importance in the field of building integrated photovoltaics
 1178 (BIPV).

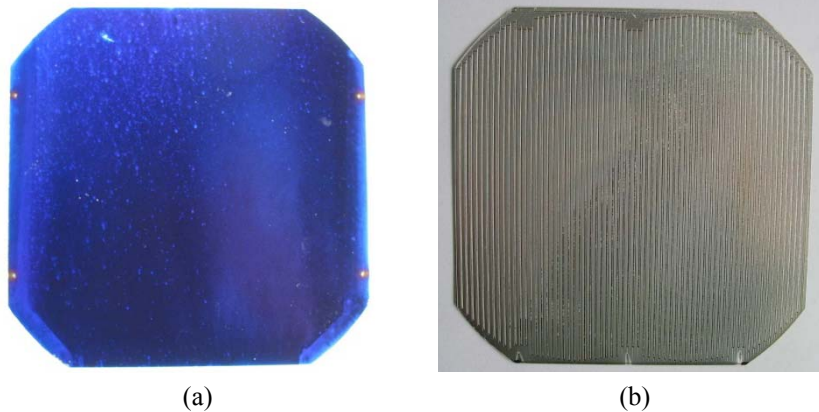
1179 The operating principle of the IBC c-Si solar cell is shown in Fig. 17 (a), and the
 1180 examples of the photographs of the IBC solar cells are shown in Fig. 18. The incoming
 1181 photons generate electron-hole pairs. Most of the absorption takes place close to the front
 1182 surface of the IBC solar cell, resulting in a charge carrier (electrons and holes) concentration
 1183 gradient through the c-Si bulk. The concentration gradient of the carriers results in the
 1184 diffusion transport towards the rear side, where the p-n junction is located and carriers are
 1185 collected by their respective electrodes. The p-n junction on the rear side may have a point-
 1186 like structure, or a line structure with the respective width. The distance between two metal
 1187 contacts of the same polarity is called pitch.

1188

1189
1190

1191 Fig. 17 (a) Schematic cross-section of an n-type high-efficiency IBC c-Si solar cell having p-n junction at the
 1192 rear side, (b) schematic angle view of the IBC cell introduced by Lammert and Schwartz [183]. To avoid
 1193 minority-carrier recombination at the rear side and to enhance the minority-carrier collection probability, emitter
 1194 size is kept larger than the BSF size. Front surface field blocks minority carriers reaching the front surface. The

1195 drawings are not to scale. From [183], M.D. Lammert and R.J. Schwartz, "The interdigitated back contact solar
 1196 cell: a silicon solar cell for use in concentrated sunlight", IEEE Transactions on Electron Devices, ED **24** (1977)
 1197 337-42. Copyright © 1977, IEEE. Permission granted. License number 3582481103872.



1198
 1199

1200 Fig. 18 Photographs of the (a) grid-less front side, and (b) rear side of the large area IBC solar cells developed in
 1201 the course of the Quebec project at Fraunhofer ISE, without the use of photolithography [184]. Solar cell area is
 1202 147.4 cm². Both p-type and n-type contacts are formed at the rear side of the c-Si wafer. Light enters from grid-
 1203 less front side of c-Si wafer. Photogenerated carriers created at the front side travel across the bulk of the wafer
 1204 due to concentrated gradient. Since electric field is present at the rear side across the p-n junction, these carriers
 1205 are collected by their respective electrodes. From [184], F. Granek, Ph.D thesis, "High-efficiency Back-Contact
 1206 Back-Junction Silicon Solar Cells", Verlag Dr. Hut, ISBN 978-3-86853-348-4 (2009). Permission granted.

1207
 1208

Historically, the concept of the IBC cells was introduced in 1977 by Lammert and
 Schwartz. Initially the IBC cells were developed for the operation under high level of
 sunlight concentration. The research group led by R.Swanson at Stanford University and at
 the SunPower Corp., founded by R. Swanson paved the way for the remarkable development
 of IBC cell physics, design, and technology [178,179,185-190]. Currently many research
 groups and industrial laboratories are investigating the IBC cell concept due to its inherent
 high-efficiency potential, with the goal to reduce the costs of the c-Si PV modules.

The other two categories of the c-Si back contact solar cells are the MWT cells [191-
 193], in which the front surface collecting junction and the front metallization grid are
 connected to the interconnection pads on the back surface via laser-drilled holes (Fig.9), and
 the EWT cells [194-198], in which the front surface collecting junction is connected to the
 interdigitated contacts on the back surface via laser-drilled holes (Fig. 10). The MWT and
 EWT cell structures are covered in Sec. 2.4. The interested reader is referred to [199] and to
 the above listed references for more details.

1222 3.2 Challenges related to c-Si back junction solar cells

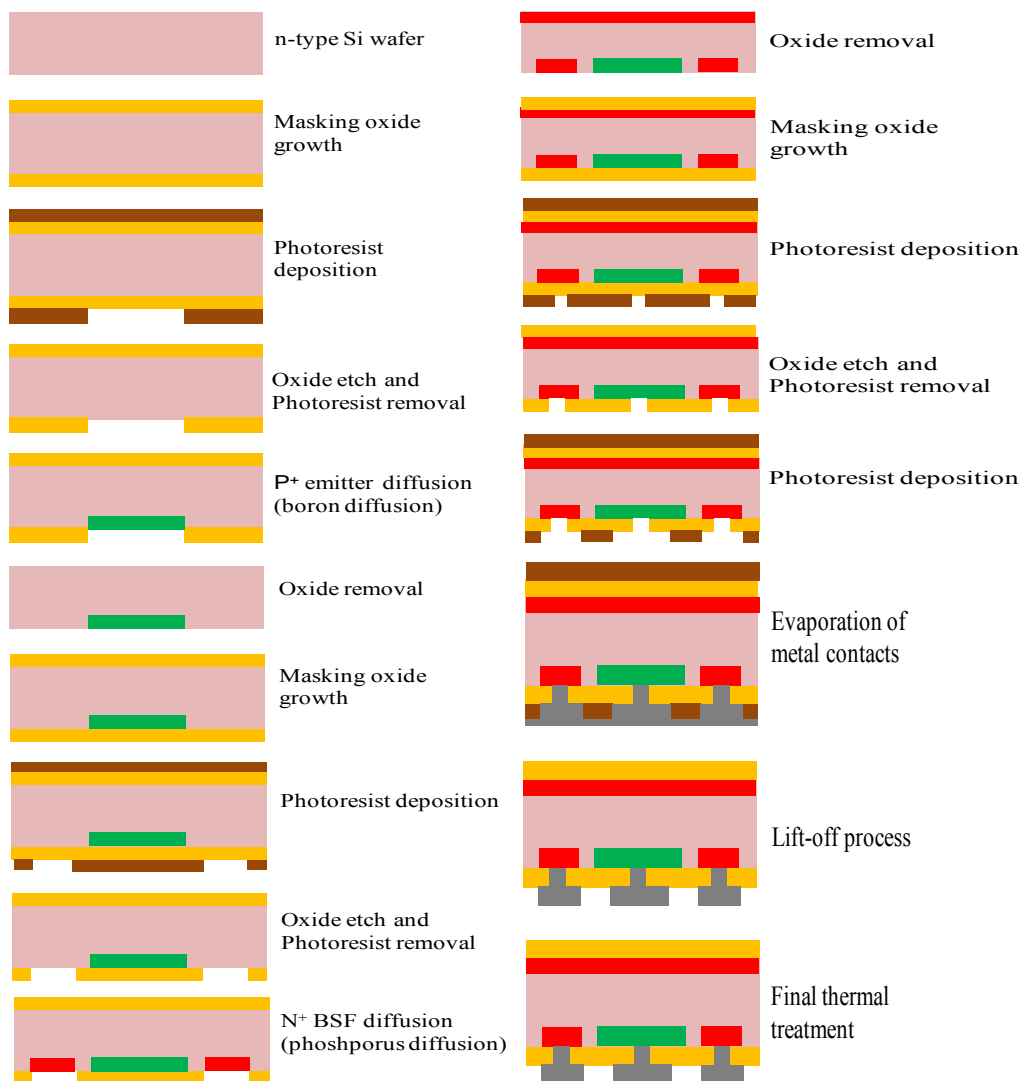
1223 One of the main challenges to the spread of IBC solar cells into mass production is the
 1224 complexity of the processing technology. Processing of major rear side features of IBC cells
 1225 such as: (i) emitter and BSF doping areas, (ii) contact openings in the passivation layer, and
 1226 (iii) the metallization grid, requires four to six masking steps. Laboratory development
 1227 usually includes application of the photolithography process, as shown in Fig.19, for
 1228 structuring of the rear side of the IBC cells.

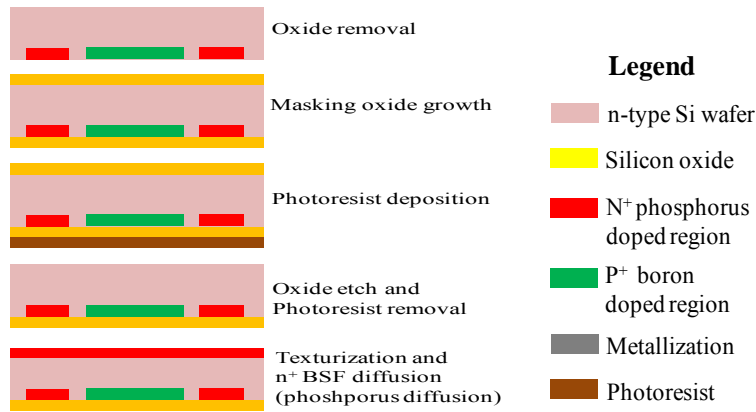
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1235 Fig. 19 Possible example of a complex laboratory scale process flow for the IBC solar cell processing using
1236 photolithography and high-temperature diffusion processes. The sequence for fabrication is first the left column
1237 and later the right column. Highly pure, lightly doped Fz c-Si wafers with diffusion length at least 4 times
1238 higher than the wafer thickness, and life-time of 1-3 msec are required. High accuracy masking steps are
1239 required to avoid shunting between p-type and n-type electrodes. Instead of expensive photolithography process,
1240 laser processing and screen-printing are used to obtain high-throughput.

1241

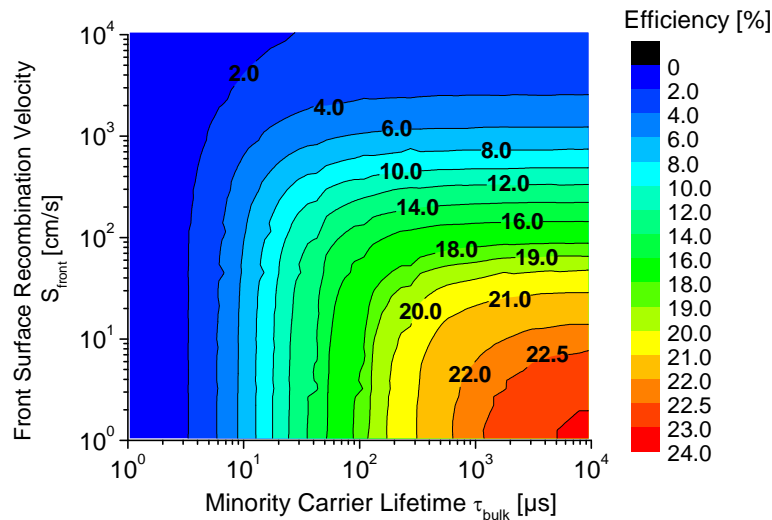
1242 Photolithography is however not a cost-effective process for mass production in the
1243 photovoltaic industry. The processing sequence of the IBC cells is therefore much more
1244 complex than conventional c-Si solar cells, which results in increased manufacturing costs.
1245 There exists the need for simplified processing schemes, where costly photolithography
1246 process is replaced with low-cost and high-throughput structuring schemes using laser
1247 processing and screen-printing, etc. However since there exists a risk of fatal shunting
1248 between the p- and n-type electrodes due to errors in the masking processes, requirements of
1249 high positioning accuracy and resolution are imposed on the masking steps. In addition to the
1250 complexity of the processing technology, IBC require high quality of c-Si wafer and the high-
1251 quality passivation of the wafer surfaces.

1252 The above issues of processing complexity and c-Si material requirements are of
1253 major importance and are therefore discussed in detail in the following sections.

1254 **3.3 Requirements for front surface passivation and bulk minority-** 1255 **carrier lifetime**

1256

1257 Due to absorption properties of c-Si, most of the photogeneration occurs at the front
1258 side of the cell (Fig. 17a). At the same time, in the IBC cell structure, the collecting p-n
1259 junction is located on the back side. Due to concentration gradient across the bulk,
1260 photogenerated charge carriers travel from front side to rear side and are collected by their
1261 respective electrodes. For poorly passivated front surface, photogenerated minority-carriers
1262 can be easily lost by recombining at the front surface instead of reaching the back junction.
1263 Moreover, even if the front surface is well passivated, a risk of recombination within the bulk
1264 c-Si exists. The carriers which need to diffuse through the wafer thickness can recombine in
1265 bulk c-Si before reaching the back junction if the bulk lifetime of the minority-carriers is
1266 insufficient. Therefore, minority-carrier lifetime in bulk (τ_{bulk}) and front SRV are the two
1267 most critical parameters in the IBC solar cell structure. The importance of these two critical
1268 parameters is shown in Fig. 20. The starting Si material needs to be of high quality (the
1269 minority-carrier lifetime should be in the range of 1-3ms) and its quality needs to be
1270 maintained during the whole solar cell processing sequence in order to reach high-
1271 efficiencies. The rule-of-thumb is that the diffusion length of the minority-carriers in c-Si
1272 needs to be at least four times higher than the thickness of the c-Si wafer in the IBC solar
1273 cells, to allow for efficiencies above 21-22%. This means that τ_{bulk} needs to be in the range of
1274 milliseconds. Simultaneously the front SRV needs to be kept extremely low in the finished
1275 device in order to enable high-efficiencies. The effective front SRV should be kept below
1276 10cm/s.



1277
 1278 Fig. 20 Example of numerical simulations of the efficiency of a back junction solar cell structure as a function
 1279 of bulk life-time and front surface recombination velocity. Front surface recombination velocity and diffusion
 1280 length of minority-carriers are the ultimate parameters controlling the efficiency. For high-efficiency, effective
 1281 front surface recombination velocity should be less than 10cm/s. Simulations were done using PC1D [200]
 1282 program (graph adopted from [184]). From [184], F. Granek, Ph.D thesis, “High-efficiency Back-Contact Back-
 1283 Junction Silicon Solar Cells”, Verlag Dr. Hut, ISBN 978-3-86853-348-4 (2009). Permission granted.

1284

1285 3.3.1 Minority-carrier lifetime considerations

1286

1287 The extremely high requirements for the minority-carrier lifetime can be in practice
 1288 met only by an n-type Si as base material. In p-type boron-doped oxygen-contaminated c-Si,
 1289 minority-carrier lifetime is strongly reduced under illumination or carrier injection [201,
 1290 202]. Due to the lack of boron in n-type Si, no degradation occurs. Also, n-type c-Si exhibits
 1291 lower sensitivity to the impurities as interstitial Fe [203]. Many laboratories are developing
 1292 front junction and rear junction solar cells based on n-type c-Si [137, 204-209], and
 1293 commercially available solar cells with the highest-efficiency are produced on n-type c-Si
 1294 wafers [178]. The drive for low-cost in the PV world requires however that the Si wafers
 1295 need to be manufactured using industrially relevant manufacturing methods. In reality only
 1296 phosphorus doped n-type wafers cut from Cz-grown ingots meet these requirements [28,
 1297 210]. The lifetime of the minority-carriers in n-type c-Si is significantly higher than in the
 1298 case of p-type c-Si. For example, extremely high minority-carrier lifetime in the range of
 1299 milliseconds was reported for n-type mc-Si by Cuevas et al. [211].

1300 3.3.2 Front surface passivation considerations

1301
1302 High quality of front surface passivation can be achieved by the application of
1303 dielectric passivation layers such a thin thermal SiO₂ layer covered by the PECVD SiN ARCs
1304 [212]. However, the front surface passivation is usually additionally improved by the
1305 additional phosphorus doping layer on the front side. This is called front surface field (FSF)
1306 and its role is to reduce the concentration of the minority charge carrier close to the wafer
1307 surface, and thus reduce the effective recombination velocity [213,214]. The methodology for
1308 numerical optimization of the doping profile of the FSF for the passivation purposes was
1309 presented by del Alamo and Swanson [215]. The application of the FSF has also additional
1310 important positive impacts on the IBC cell performance. FSF improves long-term stability of
1311 the front surface passivation under UV illumination [212]. It also improves the current
1312 linearity of the IBC cells at low light intensities, thus improving the efficiency at the low-
1313 illumination intensities [216]. An FSF layer is also seen to significantly improve lateral
1314 current transport by reducing the lateral base series resistance losses [217].

1315 **3.4 Approaches to minimize losses related to the rear side** 1316 **structure**

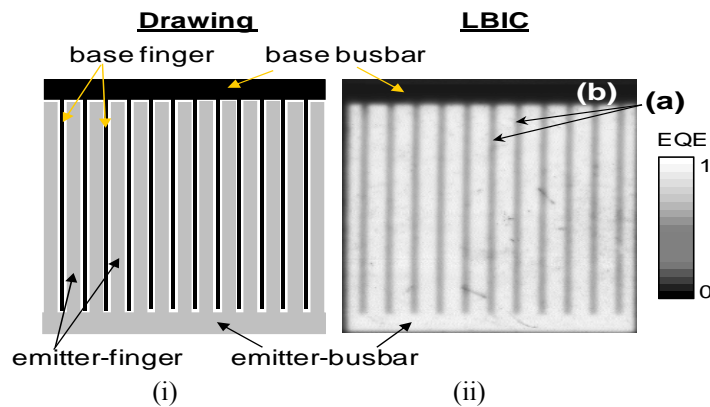
1317 The next main challenge in achieving very high conversion efficiencies in IBC cells is
1318 in the rear side structure. Introduction of the complex doping grid of the interdigitated emitter
1319 and base areas on the rear side is not only technologically challenging, but also accompanies
1320 some additional risks to achieving high-efficiencies. The recent study of Kluska et al. [218]
1321 investigates systematically the loss mechanisms on the high-efficiency IBC solar cells. Next
1322 to the front surface and bulk recombination of the minority-carriers, this study describes free
1323 carrier absorption and electrical shading as the critical loss mechanisms.

1324 In the free carrier absorption process [219,220], the incident photon's energy is
1325 absorbed by free carriers. This is a parasitic absorption (optical absorption that does not
1326 produce e-h pair is known as parasitic absorption) process, leading to a reduction of the

1327 photogenerated current. The free carrier absorption process is significant only in the highly
 1328 doped c-Si wafers. A careful optimization of the doping profiles of the emitter and BSF
 1329 regions is therefore a must when reducing the free carrier absorption losses and at the same
 1330 time minimizing the rear surface recombination losses [221].

1331 Electrical shading losses are recombination losses of the minority-carriers at the rear
 1332 side areas not covered by the emitter (shown schematically in Fig. 21). Electrical shading
 1333 losses have a significant impact on the efficiency of the IBC solar cells. Therefore careful
 1334 optimization of the rear side geometry, doping profiles, and rear surface passivation quality
 1335 are crucial in order to achieve high-efficiency [221-224].

1336

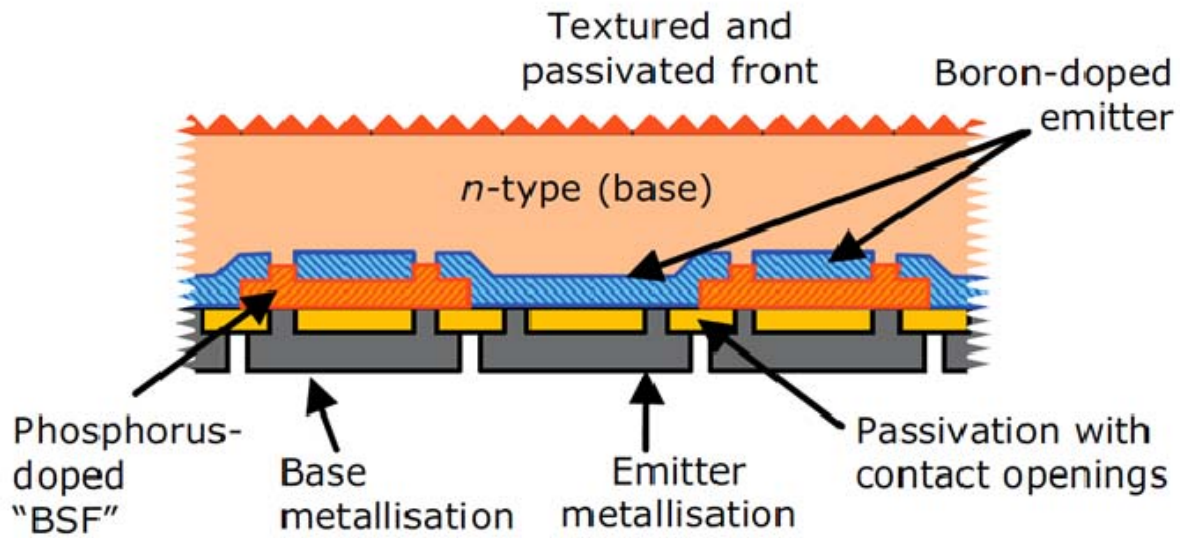


1337
1338

1339 Fig. 21 Sketch of the (i) rear side, and (ii) light beam induced current (LBIC) map of the laboratory scale
 1340 ($2 \times 2 \text{ cm}^2$) IBC c-Si solar cell. The reduced signals above the base fingers and the base busbar due to electrical
 1341 shading are clearly visible [222]. Here, (a) and (b) refers to base finger and base bus bar. Cell efficiency is
 1342 affected by electrical shading (losses) at the rear side. Doping profile and pitch size at the rear side should be
 1343 optimized for high-efficiency. With permission from [222], M. Hermle, F. Granek, O. Schultz-Wittmann, S. W.
 1344 Glunz, "Shading Effects in Back-Junction Back-Contacted Silicon Solar Cells", 33rd IEEE Photovoltaic
 1345 Specialist Conference, San Diego, CA (2008). Copyright © 2008, IEEE. Permission granted. License number
 1346 3582490239489.

1347 In order to reduce the electrical shading losses, other approaches emerged recently to
 1348 drastically reduce the rear side surface related losses apart from the optimization of the rear
 1349 side emitter and BSF doping profiles in the classical IBC cell structure. These approaches are
 1350 based on decoupling the geometries for the minority-carrier collection and metallization.
 1351 They should allow for nearly complete elimination of the electrical shading losses. A
 1352 prominent example of such approaches include buried emitter IBC solar cell [221, 225, 226],

1353 which introduces a local overcompensation of the emitter by the BSF doping and drastically
 1354 improves the emitter coverage on the rear side seen from the front surface side (see Fig. 22
 1355 for explanation of the buried emitter structure). Another example involves decoupling
 1356 emitter from metallization geometry by the application of the insulating thin-films, which can
 1357 lead to efficiencies up to 23% [227,228].



1358

1359 Fig. 22 Cross sectional view of the buried emitter back junction solar cell. When looking from the top of the
 1360 solar cell, the boron emitter is extended over almost the entire rear side of the solar cell. This allows for efficient
 1361 collection of minority-carriers at the rear side. At the same time the emitter regions are electrically insulated
 1362 from the base metallization by BSF layer, which prevents shunts between base metallization and emitter doping
 1363 [225, 229]. Buried emitter structure allows for using similar area fractions for base and emitter metallization,
 1364 without the need for any dielectric insulation. Reprinted with permission from [225], N.-P. Harder, V. Mertens,
 1365 and R. Brendel, Buried emitter solar cell structures: Decoupling of metallisation geometry and carrier collection
 1366 geometry of back contacted solar cells, *phys. stat. sol (RRL)*, **2** (2008) 148. Copyright © 2008 published by
 1367 John Wiley & Sons. Permission granted. License number 3582490855869

1368

1369 **3.5 Current developments for the low-cost IBC solar cell** 1370 **processing**

1371

1372 Currently the focus in the processing of the IBC cells is on simplifications of the
 1373 process flow, and overall cost reduction. The examples below show selected approaches to
 1374 reduce the processing complexity, and cost of the IBC cells.

1375 **3.5.1 Ion-implantation**

1376

1377 Due to its directional character, the ion-implantation process allows for one-step
 1378 patterning of the doped regions. This means that in the ion-implantation process only one

1379 single surface of the wafer is modified. Thus, unlike in the high-temperature diffusion
 1380 process, there is no need to carefully protect the other (non-modified) surface during the
 1381 implantation step. This feature of ion implantation can potentially allow for major
 1382 simplifications in the processing of the complex rear side structure of the IBC cells.
 1383 Moreover, a single high-temperature annealing process, at the final stage of the IBC cell
 1384 processing, can deliver growth of the front and rear side Si oxide passivation layer and anneal
 1385 multiple doping processes. A possible process flow to manufacture high-efficiency IBC cells
 1386 with ion implantation is shown in Fig. 23. An ion-implantation application to the production
 1387 of high-efficiency IBC cells is under development by various industrial and research groups
 1388 [140, 230, 231]. In this example the front side oxide is removed (process step: oxide etch
 1389 front) in order to grow a thin passivation oxide on the front surface, for the subsequent ARC
 1390 SiN.



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Fig. 23 Example of a process flow used for processing of ion implanted IBC cells [230]. Ion implantation process allows one-step patterning of doped areas. Processing steps can be simplified by using ion implantation process. Multiple dopants can be annealed in a single annealing process. With permission from [230], N. Bateman, P. Sullivan, C. Reichel, J. Benick, M. Hermle, “High quality ion implanted boron emitters in an interdigitated back contact solar cell with 20% efficiency”, Energy Procedia 8 (2011) 509. Copyright © 2011 Published by Elsevier Ltd. Permission granted. License number 3584831043918.

1400 3.5.2 IBC c-Si back heterojunction solar cells

1401
 1402 Heterojunctions are known for their excellent surface passivation properties. Their
 1403 application to the IBC solar cells can therefore improve the open circuit voltages
 1404 significantly. At the same time, the deposition of the a-Si:H layers can be done through a
 1405 mask at low-temperatures, which offers a potential of reduction of the complexity of the IBC
 1406 cell process flow [232-234]. Si based back heterojunction solar cells are presented in Sec.5.

1407 **3.5.3 Epitaxial doping layers**

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1409

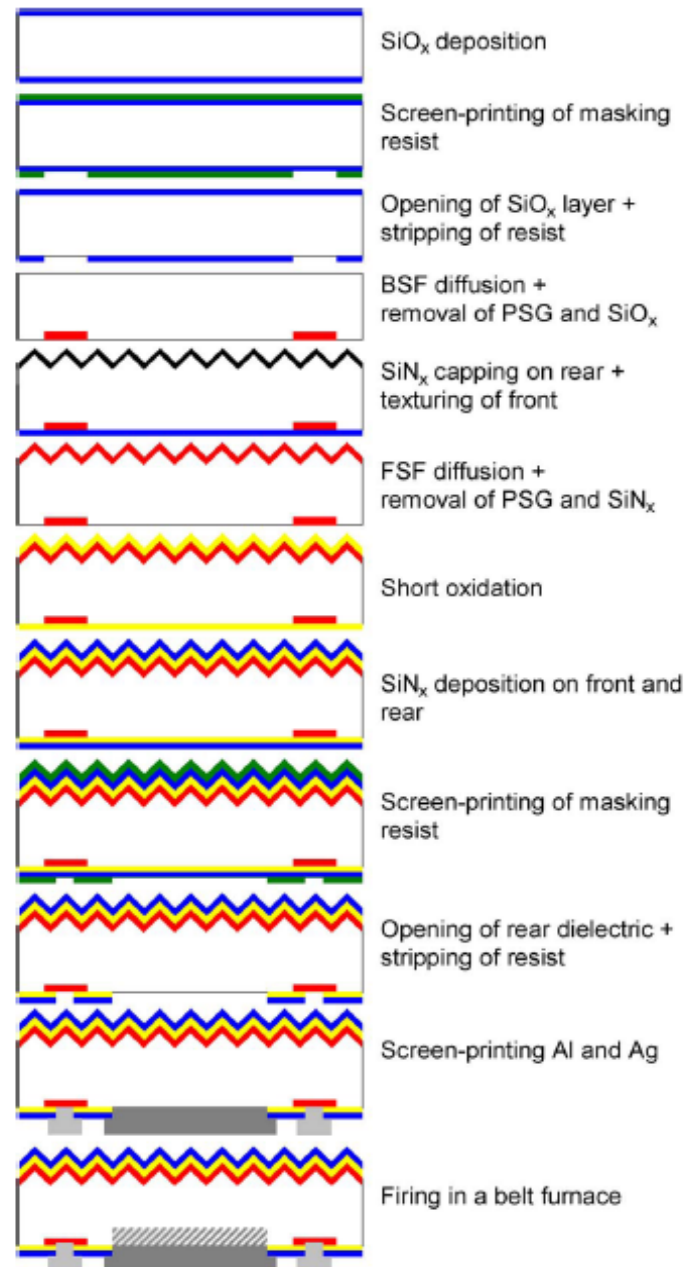
1410 Another opportunity for the simplification of the processing flow for the IBC cells is
1411 the epitaxy for the formation of the highly doped regions. Epitaxy is the method of deposition
1412 of the respective material on a crystalline wafer, in which the deposited material maintains
1413 the crystallographic orientation of the crystalline wafer. The technological process of epitaxy
1414 allows for the precise formation of the doping profiles, which are not possible to achieve with
1415 the traditional high-temperature diffusion process. A study by Baker-Finch and Basore [235]
1416 demonstrated the potential of the epitaxy process in the formation of the front surface field
layer in the IBC cells.

1417 **3.5.4 Laser processing and screen-printing for low-cost structuring of IBC** 1418 **cells**

1419

1420

1421 The masking steps to process IBC cells are often performed using photolithography,
1422 which is costly and thus not applicable for mass production of IBC cells. Low-cost and high-
1423 throughput alternatives to photolithography are being developed and applied in the
1424 processing of IBC cells. These structuring alternatives include laser processing and screen-
1425 printing processes. Engelhart et al. demonstrated IBC cells with efficiency of 22% with
1426 application of laser structuring [196]. Granek et al. applied screen-printed processes for
1427 masking of the IBC cells to reach 21.3% efficiency [217]. Examples of the low-cost IBC cell
1428 processes with the focus on applying the screen-printed metallization on IBC cells were
1429 developed by Halm et al. [236], Castano et al. [237], Galbiati et al. [238], and Lamers et al.
1430 [239]. Wohl et al. [240, 241] developed an industrially feasible IBC process with the Al
1431 alloyed emitter, to eliminate the boron diffusion process. This process flow is shown in Fig.
24.



1432

1433 Fig. 24 Process sequence for all-screen-printed IBC cell with Al alloyed emitter on an n-type wafer [240].
 1434 Instead of diffused (boron) emitter process, p⁺-Al alloyed emitter is formed during the firing process of the Al
 1435 paste. Contact metals are formed by screen-printing Al and Ag. Reprinted with permission from [240], R.
 1436 Woehl, J. Krause, F. Granek, D. Biro, 19.7% efficient all-screen-printed back-contact back-junction silicon solar
 1437 cell with aluminum-alloyed emitter, IEEE Electron. Dev. Lett., **32** (2011) 345. Copyright © 2011, IEEE.
 1438 Permission granted. License number 3582500441017.

1439

1440 3.5.5 Formation of the interdigitated metallization grid

1441

1442 The formation of the interdigitated metallization grid is often achieved using

1443 photolithography masking and thermal evaporation of the metal layers. However, as

1444 mentioned earlier, photolithography is not cost-effective for solar cell production. Different
1445 methods to create interdigitated metallization grid from the full area deposited (e.g. by the
1446 means of thermal evaporation or sputtering) metal layer are under evaluation. These include:
1447 (i) bi-level metallization scheme proposed by Sinton et al. [242] and currently under
1448 development by De Vecchia et al. [243], (ii) self-aligned metallization scheme proposed by
1449 Sinton in 1988 [186], (iii) laser ablation of the masking layer and etching of the bulk metal
1450 [244], (iv) local etching of the metal layers through screen-printed masks [184], and (v) lift-
1451 off and laser assisted lift-off using screen-printed layers [184]. There exist another approach
1452 to metallization, namely direct plating of metal on the rear cell surface, which has been
1453 investigated for the front side metallization of the standard c-Si solar cells [245].

1454 Broadly, research advances in this field have not been reported widely so far, which
1455 indicated a potential for further cost reduction and process flow simplifications in the
1456 processing of c-Si IBC solar cells.

1457 **3.6 Future outlook**

1458 Recetly Panasonic and Sharp [246,247] research laboratories have reported
1459 efficiencies of over 25 % at the laboratory scale for IBC solar cells, and the milestone of 26
1460 % efficiency seems to be practically achievable with the single-junction c-Si IBC cell. These
1461 groups combine an IBC cell structure with high level of surface passivation for the metal
1462 contact regions using a heterojunction of a-Si:H/c-Si interfaces. Currently recombination
1463 losses at the metallized areas are one of the dominant recombination mechanisms in high-
1464 efficiency IBC cells. Therefore research efforts are currently focused on the introduction of
1465 industrially feasible passivated contact concepts with the goal of drastically reducing
1466 minority-carrier recombination rate at the metal contacts. One important area of
1467 recombination is at the edge. It is expected that in the future the best efficiencies of IBC cells
1468 would be reported on large solar cell surfaces, where the relative impact of the edges will be

1469 low. The next significant modification to the IBC cell structure may be the application of a
1470 novel module interconnection technology based on patterned back-sheet foil [181]. Such
1471 interconnection will allow for eliminating the necessity of complicated metallization busbar
1472 and finger grids on the IBC cells side, and will allow for more design freedom for the solar
1473 cell engineers. This can potentially have a positive impact on the efficiency and packaging
1474 density of the solar cells in a module.

1475 **4. Crystalline Si based solar cells: Front heterojunction**

1476 A-Si:H/c-Si front heterojunction (hereafter called Si heterojunction or SHJ) solar
1477 cells are fabricated by deposition of a few nm thin intrinsic a-Si:H followed by doped a-Si:H
1478 onto (typically) c-Si wafers. Their working principle is very similar to conventional Si wafer
1479 cells with diffused junctions; it can be summarized briefly as follows (Fig. 25): The incident
1480 light generates electron-hole (e-h) pairs in the c-Si wafer. The minority charge carriers are
1481 collected on the cell's front side by the Si heterojunction, and are laterally transported
1482 towards the metal front grid through a thin transparent conducting oxide (TCO) layer that
1483 also acts as an anti-reflection coating. Majority charge carriers are collected by the BSF,
1484 which is also formed by an a-Si:H/c-Si heterojunction. The rear side contact is completed by
1485 a full area metallization. Often, another TCO layer is inserted between the a-Si:H and metal
1486 on the back side to improve the optical properties of the cell in the infrared part of the
1487 spectrum.
1488

1489

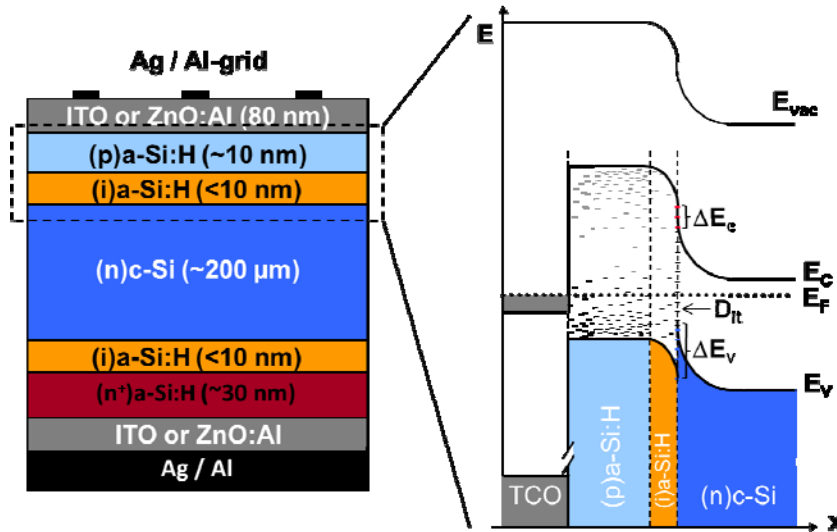
1490 **4.1 Introduction**

1491 Si heterojunction device architecture enables very high energy conversion efficiencies
1492 of 24.7% on industrially relevant cell sizes ($>100\text{cm}^2$) [248] and above 21% ($>18\%$ module
1493 efficiency) in industrial production [249]. The key feature of this technology is that the metal
1494 contacts, where the recombination velocity is high in traditional diffused-junction cells, are

1495 spatially and electronically separated from the absorber by insertion of a wider bandgap a-
1496 Si:H layer. This general idea was introduced by Fuhs et al. in the 1970s using a direct
1497 heterojunction between doped a-Si:H and c-Si [250] and augmented by the company
1498 Sanyo in the 1990s with the introduction of a low-defect intrinsic a-Si:H buffer layer between
1499 the doped a-Si:H and the c-Si wafer [251]. It enables V_{oc} s above 700 mV. Furthermore, the
1500 cell process is based on comparatively simple full-area deposition steps and screen-printed
1501 contacts, whereas in conventional c-Si cells with diffused emitters, efficiencies well above
1502 20% can only be reached using local contacting schemes, which require expensive patterning
1503 techniques. Additionally, since all process steps occur at temperatures around or below
1504 200°C, the cell has a low thermal budget [252]. In contrast to conventional diffusion
1505 processes that lead to wafer bowing and increased breakage, the SHJ process is compatible
1506 with very thin wafers (the 24.7% cell was fabricated on a 98 μm thin wafer) or Si absorbers
1507 on glass with a thickness of few μm , which have indeed lately shown promising V_{oc} s and
1508 efficiencies of up to 656mV and 11.8%, respectively [253, 254].

1509 Many aspects of the SHJ device concept will be discussed only briefly in the
1510 following. For further reading, an extensive review article on SHJ solar cells published by de
1511 Wolf et al. [255], and a monograph [256] on the same subject are recommended.

1512 4.2 c-Si based front heterojunction cell design – an overview



1513

1514 Fig. 25 Schematic cross-section and energy band diagram of a p-type a-Si:H/intrinsic a-Si:H/n-type c-Si
 1515 heterojunction solar cell. The intrinsic a-Si:H acts as passivation layer between c-Si (absorber)
 1516 active metal (or TCO) contacts. Both p-n junction and BSF are formed by a-Si:H/c-Si heterojunctions. E_c , E_v
 1517 are the band edges, ΔE_c , ΔE_v the band offsets between the intrinsic a-Si:H and the c-Si, E_f the Fermi level and
 1518 D_{it} the density of defect states at the intrinsic a-Si:H/c-Si interface. Note the asymmetry of the band offset: ΔE_v
 1519 is much larger than ΔE_c . For clarity, texturization of the wafer is not shown.

1520

1521 In SHJ cells, a-Si:H/c-Si heterojunctions are used to form the p-n junction and BSF of
 1522 the cell. Figure 25 shows a simplified sketch of this cell type, including the intrinsic buffer
 1523 layers, together with a schematic band diagram. Note that the usual texturization of the wafer
 1524 has been omitted for clarity. As already mentioned above, the Si heterojunction is the solution
 1525 to the conflicting requirements to (i) passivate electronically the surfaces of the c-Si absorber,
 1526 where charge carriers are photogenerated, in order to obtain a large splitting of the quasi
 1527 Fermi levels and thereby a high V_{oc} , and to (ii) extract the photogenerated charge carriers
 1528 efficiently through the same surfaces, yielding a low series resistance/high fill-factor. In the
 1529 SHJ concept, this problem is solved by inserting a passivating, semiconducting film between
 1530 the absorber and the highly recombination active metal (or TCO, see below) contacts. This
 1531 passivating a-Si:H film, in turn, is usually divided into two parts, i.e. the passivation layer
 1532 proper, consisting of low-defect not intentionally doped (intrinsic) a-Si:H and a doped, more
 1533 defective a-Si:H layer that induces the appropriate band bending to form the p-n junction or

1534 the BSF. Electrical contacts to the cell are then formed using TCOs and a metallization layer
1535 (grid/full-area).

1536 The main differences between semiconductors in the Si heterojunction cell and the equivalent
1537 homojunction cell are:

1538 **(i) Abrupt interfaces:** In contrast to the usual diffused emitter and BSFs, the Si
1539 heterojunction is abrupt on the monolayer length scale. Thus the doping profile usually is a
1540 step function. Similarly, it is believed that the second heterojunction in the cell, the TCO/n-
1541 a-Si:H junction, should also be as abrupt as possible.

1542 **(ii) Defect states in the a-Si:H bandgap and at the a-Si:H/c-Si interface:** These are an
1543 intrinsic property of overconstrained semiconducting glasses in general [257]. They consist of
1544 the so-called Urbach tails, i.e. exponential distributions of electronic states reaching from the
1545 band edges into the bandgap of the material, and of unsaturated, dangling Si bonds deep in
1546 the bandgap, which can be saturated by the hydrogen present in the a-Si:H film. At the
1547 a-Si:H/c-Si interface, surface contamination by atoms or molecules adsorbed to the c-Si
1548 wafer surface prior to a-Si:H deposition can lead to additional extrinsic defect states at the
1549 interface. Controlling surface contamination and the initial stages of a-Si:H growth are
1550 therefore key issues to obtaining low defect density a-Si:H/c-Si interfaces.

1551 **(iii) Band offsets:** The difference in E_g between c-Si ($E_g \sim 1.12$ eV at room temperature) and
1552 a-Si:H ($E_g = 1.6-1.9$ eV, depending on deposition conditions) gives rise to discontinuities in
1553 the valence and conduction band edges, usually denoted by ΔE_v and ΔE_c , respectively, see
1554 the schematic band diagram in Fig. 25. Band offsets also exist at the TCO/a-Si:H interface.
1555 For the contact layers, the differences to conventional homojunction cells are:

1556 **(iv) TCO:** Instead of the usual SiN ARC, SHJ cells use TCO, which provide both the ARC
1557 properties as well as a high lateral conductivity. This is necessary because even the
1558 conductivity of doped a-Si:H films is smaller by orders of magnitude. Thus, charge transport

1559 proceeds essentially perpendicular through the entire a-Si:H/c-Si/a-Si:H cell structure (Fig.
1560 25), then laterally through the TCO to the contact fingers.

1561 **(v) Metallization:** For industrially relevant cell processes, screen printing is widely used.
1562 Pastes for SHJ cells must yield good electrical properties for curing temperatures around
1563 200°C, which necessitates the use of a relatively high content of Ag. Lately, electroplated
1564 contacts have also been introduced successfully [258,259].

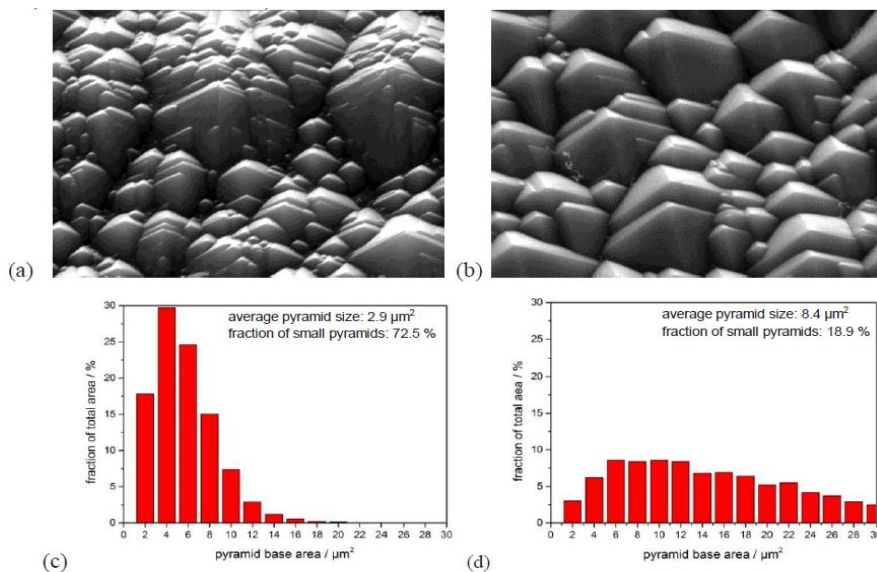
1565 Conceptually, the SHJ band offsets (i.e., band-edge misalignments) are the main
1566 difference to the p-n homojunction. They are an experimental approximation of the idea that
1567 contacts to a solar cell should act as a semi-permeable membrane through which charge
1568 carriers are extracted [260]. The unwanted charge carriers in the vicinity of a contact – i.e. the
1569 minority-carriers at the BSF, and the majority carriers at the p-n junction – are hindered by
1570 the band offsets in the heterojunctions and the low conductivity of the doped a-Si:H for the
1571 unwanted carrier polarity to reach the cell contacts, and thereby recombination at the contacts
1572 is effectively suppressed. Thus, a high separation of quasi-Fermi levels is obtained, and low
1573 reverse diode saturation currents and high V_{oc} can be expected in the cell. The advantage of
1574 having suitable band offsets at the contacts of a solar cell, similar to the case of
1575 heterostructure lasers, has been pointed out already in the 1980s, and their benefit to cell V_{oc}
1576 has been shown for the SiO_x/c -Si tunnel-heterojunction case, in the so-called semi-insulating
1577 polysilicon cell [261]. Another similar device is the metal-insulator-semiconductor cell [262],
1578 where a thin oxide layer acts as the semi-permeable membrane that has to be traversed, in this
1579 case by tunneling.

1580 **4.3 c-Si wafers, surface texture and cleaning**

1581 SHJ cells can be realized on both n- and p-type wafers, although the highest cell
1582 efficiencies have been demonstrated on n-type [263]. Typical doping levels are in the range
1583 also used for homojunction cells, 1-5 Ω -cm. In order to realize the high V_{oc} potential of SHJs,

1584 a high minority charge carrier lifetime, i.e. low density of recombination-active defects in the
 1585 wafer is needed. A bulk minority-carrier lifetime of several milliseconds for generation rates
 1586 corresponding to air mass 1.5 (AM1.5) illumination is desired. Today, with improved crystal
 1587 growth technology, this carrier lifetime range is readily achievable in low-cost Cz wafers.

1588 As explained in Sec.2, the wafers are textured to improve light trapping, usually with
 1589 a random pyramid texture, and thoroughly cleaned using the so-called RCA process
 1590 developed as a standard cleaning process by the Radio Corporation of America [41] or a
 1591 variant thereof. The native Si oxide layer grown in the last process is then usually removed
 1592 by a short etch in diluted HF (1%, 1 min) immediately before the wafer is loaded into the
 1593 PECVD system for a-Si:H deposition. Alternative pre-cleaning and oxide removal steps
 1594 (chemical smoothing of wafer surface) have also been explored [264].



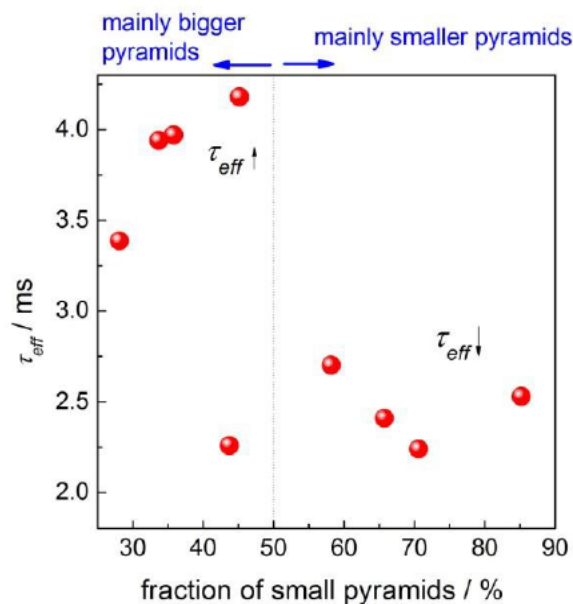
1595

1596 Fig. 26 SEM images of textured Si wafers: (a) after 5μm side damage etch removal and 20min texture etching
 1597 time; (b) after 10μm side damage etch removal and 10min texture etching time. Scanning size of both images:
 1598 25μm × 19μm, tilt: 30°; (c and d) histograms of the statistical analysis of the corresponding pyramid sizes in the
 1599 SEM images above. Data is obtained from at least 3 measurements at different positions on the sample.
 1600 Reprinted with permission from [265], Bert Stegemann, Jan Kegel, Mathias Mews, Erhard Conrad, Lars Korte,
 1601 Uta Stürzebecher, Heike Angermann "Passivation of Textured Si Wafers:Influence of Pyramid Size
 1602 Distribution, a-Si:H Deposition Temperature, and Post-treatment." Energy Procedia, **38**(2013)881. Copyright ©
 1603 2013 The Authors. Published by Elsevier Ltd. License number 3472391033286.

1604

1605 Recently, the influence of the random pyramid surface topology has been investigated
 1606 in detail. Figure 26 shows that the morphology can be modified within a wide range to yield

1607 either mostly smaller pyramids or a broader distribution with predominantly large or very
 1608 large ones. When passivated with a-Si:H, these surfaces behave very differently (Fig. 27).
 1609 The effective minority charge carrier lifetime, a measure for the V_{oc} potential in cells
 1610 produced with such passivation layers, increases strongly when the fraction of small
 1611 pyramids is reduced [265]. It can be surmised that this behavior is related to the difficulty of
 1612 growing well-passivating layers in the valleys and at edges of the pyramids [266]. With
 1613 decreasing fraction of small pyramids, the line density of such valleys and ridges also
 1614 decreases.



1615

1616 Fig. 27 Dependence of the effective carrier lifetime on the fraction of small pyramids. As can be seen, carrier
 1617 lifetime increases when the fraction of small pyramids is reduced. This is probably due to the poor passivation
 1618 quality in the valleys and edges of the pyramids. Reprinted with permission from [265], Bert Stegemann, Jan
 1619 Kegel, Mathias Mews, Erhard Conrad, Lars Korte, Uta Stürzebecher, Heike Angermann "Passivation of
 1620 Textured Si Wafers: Influence of Pyramid Size Distribution, a-Si:H Deposition Temperature, and Post-
 1621 treatment." Energy Procedia, 38(2013)881. Copyright © 2013 The Authors. Published by Elsevier Ltd. License
 1622 number 3472391033286.

1623 4.4 Hydrogenated amorphous Si

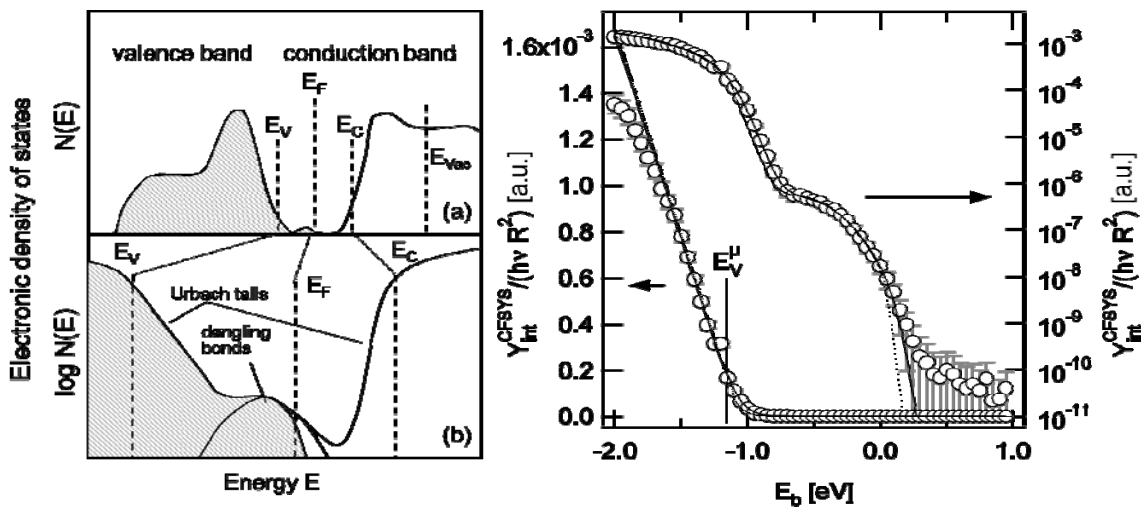
1624 As sketched in Fig.25, the emitter and BSF contacts of SHJ solar cells consist of
 1625 doped and intrinsic a-Si:H films with a thickness of the order of 10 nm. These films are
 1626 grown using PECVD at deposition temperatures around 200°C, with growth rates of the order
 1627 of 10 nm per minute. Precursor gases for undoped a-Si:H films are SiH₄ and hydrogen (H₂).

1628 Doping is usually achieved by admixture of phosphine (PH_3) for n-type and diborane (B_2H_6)
1629 or trimethylboron ($\text{B}(\text{CH}_3)_3$) for p-type doping. Generally, processes are similar to those used
1630 for a-Si:H thin-film p-i-n solar cells. In the field of SHJ cells, most results have been reported
1631 for a-Si:H grown in conventional parallel plate reactors with radio frequency (RF,
1632 13.56 MHz) excitation, [267-269]. However, it appears that suitable deposition regimes can
1633 be found for most PECVD and related a-Si:H deposition techniques. Good surface
1634 passivation properties and/or solar cells have also been reported for a-Si:H grown with very
1635 high frequency (VHF \geq 40 MHz) excitation [263], hot-wire chemical vapor deposition
1636 (CVD) [270], DC saddle field PECVD [271], electron cyclotron resonance (ECR)-
1637 CVD [272] etc.

1638 The insertion of thin (2-8 nm) intrinsic a-Si:H interlayers for c-Si surface passivation
1639 between the c-Si wafer and the doped a-Si:H films used to form the p-n junction or BSF can
1640 be seen as a breakthrough for realizing the unique potential of SHJ cells, namely their
1641 outstandingly high V_{oc} . Indeed, Sanyo had patented this use of an intrinsic a-Si:H buffer and
1642 named their solar cells accordingly as heterojunction with intrinsic thin layer (HIT) cells
1643 [251]; the patent for the intrinsic buffer layer expired in 2011. This prompted attempts to
1644 achieve good cell performance also without using intrinsic a-Si:H (i-a-Si:H) layer with, at the
1645 time, notable results of 19.8% and 18.4% efficient cells for p-type a-Si:H/n-type c-Si and the
1646 inverse cell structure, respectively [273, 274]. However, V_{oc} s were generally much lower, of
1647 the order of only 630-640 mV. This is related to a doping-dependent defect generation
1648 mechanism in a-Si:H, as discussed below in Sec. 4.4.2. Thus, it is indeed essential to
1649 passivate the c-Si surface to reduce the density of defect states (D_{it}) in the bandgap (Fig. 25)
1650 by saturating dangling bonds at the c-Si surface using a low-defect i-a-Si:H layer.

1651 4.4.1 Intrinsic a-Si:H films

1652 Many studies conducted in the past years have led to the conclusion that the microscopic
 1653 structural and electronic configuration of ultrathin a-Si:H layers is governed by the same
 1654 mechanisms as that of thick a-Si:H films, as described, for example, in Ref. [275,276]. The
 1655 deposition conditions systematically affect the layer properties, and a combination of low-
 1656 temperature deposition and a subsequent anneal was shown to yield best results in terms of
 1657 a-Si:H/c-Si interface passivation. Interestingly, not only conventional hot plate anneals for
 1658 several minutes, but also accelerated annealing using microwave radiation can be used. The
 1659 latter process requires only a few seconds [277]. Furthermore, a cyclic sequence of short a-
 1660 Si:H deposition and hydrogen plasma steps [278] or a post-treatment of the grown layer with
 1661 a hydrogen plasma [279] have been useful in improving a-Si:H/c-Si interface passivation.



1662

1663 Fig. 28 Schematic sketch of the density of states (DOS) in the valence and conduction band of a-Si:H on the (a)
 1664 linear and (b) semilog scale. The states occupied by electrons are marked as hatched area (left side), after [276].
 1665 Urbach tails (i.e. exponential distribution of electronic states from band edges into the bandgap) are induced
 1666 by strain in the amorphous network. Occupied DOS as measured by using near-ultraviolet photoelectron
 1667 spectroscopy, linear and semilog scale (right side). Reproduced with permission from [256], Wilfried G. J. H.
 1668 M. van Sark, Lars Korte, Francesco Roca, Physics and Technology of Amorphous-Crystalline Heterostructure
 1669 Silicon Solar Cells, 2011. Springer, 2011. Copyright © Springer-Verlag Berlin Heidelberg. License number
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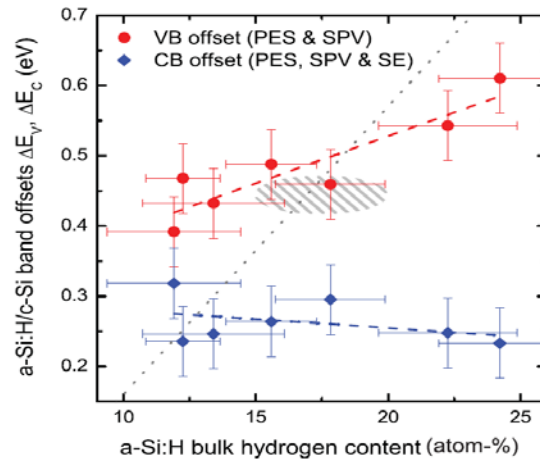
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1672 The density of states of a-Si:H is depicted in Fig. 28. In the valence and conduction

1673 bands, it is similar to that of c-Si, but has additional defect states in the bandgap. Urbach tails

1674 decay exponentially into the bandgap and are induced by strain in the amorphous network,
1675 whereas a broad distribution of defects near midgap consists of dangling (broken/unsaturated)
1676 Si-Si bonds, with density N_d . The exponential slope of the Urbach tails, the so-called Urbach
1677 energy (E_0), is a measure for the overall strain in the amorphous network (increased E_0 means
1678 increased strain), and dangling bonds are created when the strain in the bonds forming the
1679 Urbach tails becomes too large. Thus, it is intuitively clear that E_0 and the dangling bond
1680 density are related. Broadly speaking, if the a-Si:H network is in thermodynamic equilibrium,
1681 an increase in E_0 also yields an increased N_d . This is the gist of defect generation models
1682 proposed by Stutzmann [280] and by Powell & Deane [281,282]. The latter, so called defect
1683 pool model also considers electronic contributions to the system's free energy, which makes
1684 N_d and its distribution across the bandgap dependent on the position of the Fermi level.

1685 Electronically, the a-Si:H bandgap defects behave differently. While the band tail
1686 states act as traps for charge carriers from the band they are originating from, dangling bonds
1687 deeper in the gap are recombination centers. Dangling bonds are amphoteric defects, i.e., the
1688 sp^3 hybridized orbital of the dangling bond can be occupied by 0, 1 or 2 electrons, leading to
1689 the charge states D^+ , D^0 and D^- . In the single-electron band diagram picture, the energy
1690 positions for the possible transitions of the dangling bond from unoccupied to singly
1691 occupied, $D^{+/0}$, and from singly to doubly occupied, $D^{0/-}$, are represented by two Gaussian
1692 distributions in the bandgap [281-283]. The $D^{+/0}$ states have donor character, the $D^{0/-}$ states
1693 are acceptor-like. In the description of recombination, this amphoteric character of the defects
1694 leads to a behavior that differs from the conventional Shockley-Read-Hall formalism [283-
1695 285].



1696

1697 Fig. 29 Valence band offsets of i-a-Si:H/n-c-Si heterostructures with varying hydrogen content. The conduction
 1698 band offset is determined based on the valence band offset, using the optical bandgap of the a-Si:H films as
 1699 determined from spectral ellipsometry. As hydrogen content increases in the film, the main variation occurs in
 1700 ΔE_v while ΔE_c is almost constant. For state of the art a-Si:H films (with 10-15% hydrogen) ΔE_v and ΔE_c
 1701 are approximately 0.45eV and 0.25eV, respectively. Reproduced from [286] with permission, T. F. Schulze, L.
 1702 Korte, F. Ruske, and B. Rech, Band lineup in amorphous/crystalline silicon heterojunctions and the impact of
 1703 hydrogen microstructure and topological disorder, Phys. Rev. B **83** (2011) 165314. Copyright © 2011 American
 1704 Physical Society. License number 3583611410416.

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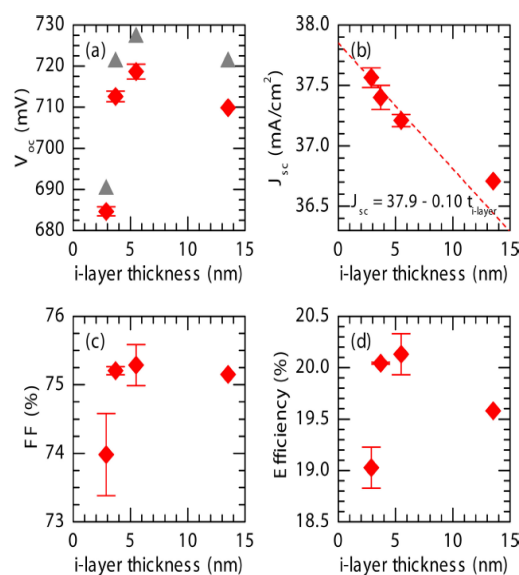
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The deposition of a-Si:H on a c-Si wafer leads to the formation of a type I heterojunction (straddling gap, i.e., the gap of the smaller bandgap material is completely within the gap of the wider bandgap material). Thus, as can be seen from Fig. 25, the band offset at the a-Si:H/c-Si interface acts as barrier for both electrons and holes coming from the c-Si wafer. The value of the valence band offset ΔE_v can be determined reliably using near-UV photoelectron spectroscopy [287-289]. As the bandgap of a-Si:H can be varied by changing the hydrogen content of the film, the band offsets also have to vary. As shown in Fig. 29, it was found that the main variation occurs in ΔE_v , whereas ΔE_c is almost unchanged [286]. State of the art a-Si:H films (hydrogen concentration 10-15%) have $\Delta E_v \sim 0.45$ eV, $\Delta E_c \sim 0.25$ eV. No variation of the bandgap with film thickness or doping was found [288]. To date, there exist no systematic investigations of the influence of the increase in ΔE_v , i.e., in the barrier for hole transport, on solar cell properties.

At the a-Si:H/c-Si interface (Fig.25), as-deposited D_{it}/cm^2 is determined by the local network structure at the interface, which is in a non-equilibrium state for samples deposited at

1720 low-temperature [267]. The subsequent annealing step leads to thermodynamic equilibration
 1721 between the a-Si:H bulk and the a-Si:H/c-Si interface. The equilibrated a-Si:H/c-Si interface
 1722 region then does not possess unique electronic properties but is determined by the a-Si:H bulk
 1723 density of states distribution [290]. The a-Si:H bulk volume defect density (N_d) / cm^3 is
 1724 related to the a-Si:H/c-Si interface defect density by the relation $D_{it} = N_d \times d_t$, d_t is the
 1725 characteristic length, in the nm range, over which charge carriers generated in the c-Si wafer
 1726 can travel into the a-Si:H and then recombine via a-Si:H defects. A calculation based on the
 1727 assumption that the charge carriers tunnel into the a-Si:H yields $d_t = 2.7$ nm [291]. Indeed,
 1728 recombination at the a-Si:H/c-Si interface can be described consistently using a projected a-
 1729 Si:H density of states as c-Si surface defect density of states [284].

1730 For high J_{sc} , photogeneration in the c-Si absorber must be maximized. Thus, it is
 1731 desired to reduce parasitic absorption in the a-Si:H layers by reducing their thickness. Fig. 30
 1732 shows an example of typical findings. Here, the j_{sc} decreases with a slope of $\sim 0.1 \text{ mA/cm}^2$ per
 1733 additional nm of i-a-Si:H buffer layer thickness. However, it is found that a minimum i-a-
 1734 Si:H buffer layer thickness of 5 nm or slightly below is needed. For even thinner films (<5
 1735 nm), the a-Si:H/c-Si interface passivation breaks down, therefore V_{oc} is reduced and the cell's
 1736 fill factor also decreases [292].



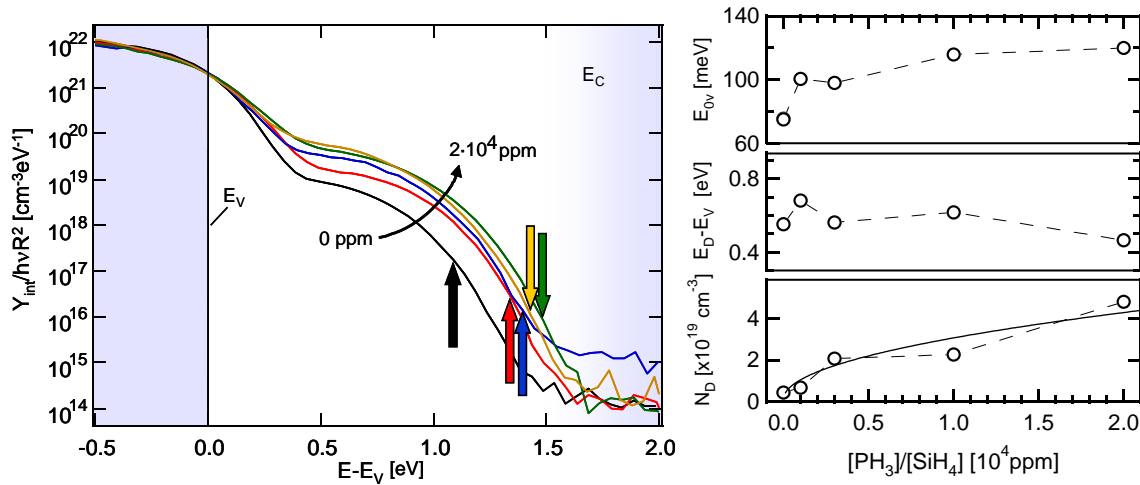
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1738 Fig. 30 Output characteristics of 4cm² solar cells with varying i-a-Si:H layer thickness. Each data point
 1739 represents the average value of three cells, except the data for the thickest layer, for which only one cell was
 1740 measured. The gray triangles in (a) represent the implied V_{oc} s of the cells prior to ITO deposition and
 1741 metallization, determined from quasi-steady-state photoconductance (Sinton) measurements. The dashed line in
 1742 (b) is the calculated dependence of J_{sc} on i-a-Si:H layer thickness. Reproduced from [292] with permission,
 1743 Holman, Z.C.; Descoedres, A.; Barraud, L.; Fernandez, F.Z.; Seif, J.P.; De Wolf, S.; Ballif, C., Current Losses
 1744 at the Front of Silicon Heterojunction Solar Cells, IEEE Journal of Photovoltaics, **2** (2012)7. Copyright © 2012,
 1745 IEEE. License number 3498231121849.

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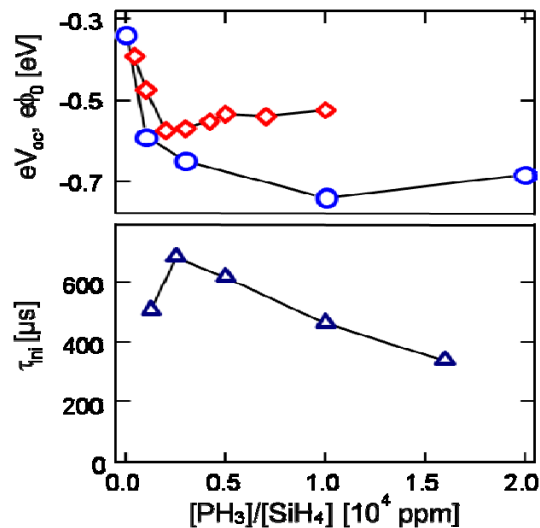
1748 **4.4.2 Doping of a-Si:H - formation of the p-n junction and doping induced defects**

1749 The a-Si:H film stack for the p-n junction and the BSF is completed by the deposition
 1750 of doped a-Si:H layers on the i-a-Si:H buffers. As shown in Fig. 31, for increasing n-type
 1751 doping of ~10 nm thin a-Si:H films, the defect density in a-Si:H increases with doping level,
 1752 a behavior already well known for thick a-Si:H films [275]. Therefore, an optimum a-Si:H
 1753 doping level exists for SHJ cells. For high doping levels, the increase in band bending at the
 1754 heterojunction, which is beneficial for forming a well-working p-n junction (high cell V_{oc} and
 1755 efficient carrier extraction, thus high fill factor, at the maximum power point), is balanced
 1756 against increasing defect concentration. The latter is detrimental due to the enhanced
 1757 recombination rate at the interface and in the a Si:H layers. This is exemplified in Fig. 32 for
 1758 n-a-Si:H/p-c-Si solar cells without i-a-Si:H buffer: While the built-in potential of the p-n
 1759 junction $e\phi_0$ increases up to a gas phase doping of 10⁴ ppm, V_{oc} reaches a (rather low, due to
 1760 the missing i-a-Si:H) maximum already at a moderate doping of ~2000 ppm and is reduced
 1761 for higher doping. The minority-carrier lifetime τ_{ini} (in this case measured by surface
 1762 photovoltage) follows the same trend as the V_{oc} : As shown in Fig. 32, lower panel, τ_{ini} peaks
 1763 at the same doping level as the V_{oc} . Clearly, at doping levels above 2000 ppm, the increasing
 1764 defect density at the a-Si:H/c-Si interface overcompensates the still (up to 10⁴ ppm) slightly
 1765 improving field effect passivation.



1766

1767 Fig. 31 Density of occupied states in the a-Si:H bandgap for increasing gas phase doping ($[\text{PH}_3]/[\text{SiH}_4] = 0 \dots$
 1768 10,000 ppm), arrows mark the Fermi level position (left side). Defect parameters, viz. valence band Urbach
 1769 energy, energetic position and density of the dangling bond defect distribution (right side). As can be seen (right
 1770 side), by increasing n-type doping in the a-Si:H film, defect density increases with doping level. Reproduced
 1771 from [293], with permission, L. Korte, and M. Schmidt, Investigation of gap states in phosphorous-doped ultra-
 1772 thin a-Si:H by near-UV photoelectron spectroscopy, *J. Non-Cryst. Sol.* **354** (2008) 2138. Copyright © 2008
 1773 Elsevier B.V. License number 3472101463232.



1774

1775 Fig. 32 Upper panel: built-in potential $e\phi_0$ (circles) and solar cell V_{oc} (lozenges, rescaled to eV units). Lower
 1776 panel: surface photovoltage decay time constant τ_{ini} . A heterojunction was formed between n-a-Si:H and p-c-Si
 1777 without using a buffer layer (intrinsic a-Si:H). Note that minority-carrier lifetime (τ_{ini}) and V_{oc} peak at the same
 1778 doping level. V_{oc} reaches a maximum at a doping level of 2000ppm and then decreases for higher doping. The
 1779 built-in-potential increases up to a doping level of 10^4 ppm, then decreases slightly for higher doping.
 1780 Reproduced with permission from [256], Wilfried G. J. H. M. van Sark, Lars Korte, Francesco Roca, *Physics*
 1781 *and Technology of Amorphous-Crystalline Heterostructure Silicon Solar Cells*, 2011. Springer, 2011. Copyright
 1782 © Springer-Verlag Berlin Heidelberg. License number 3498221350973.

1783

1784 For doped a-Si:H deposited on i-a-Si:H buffer layers, an additional effect has to be
 1785 considered: As shown by de Wolf et al. the shift in the i-a-Si:H Fermi level induced by
 1786 deposition of the doped a-Si:H film on top of the i-a-Si:H leads to Si-Si bond rupture in the i-

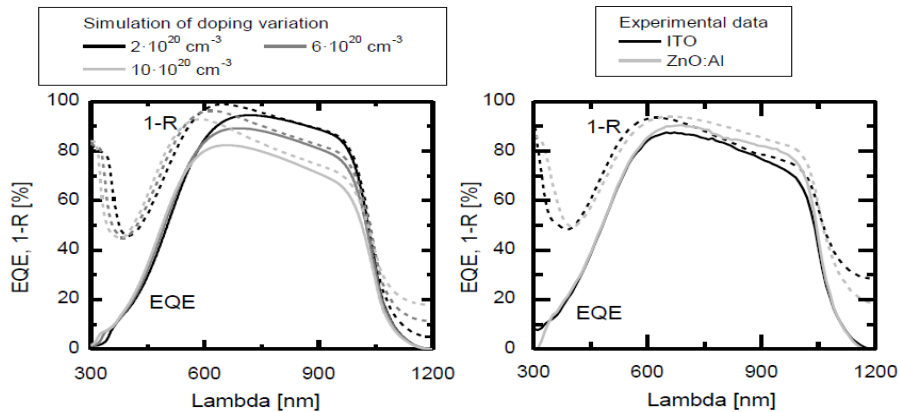
1787 a-Si:H buffer layer, i.e. generation of additional defects in the i-a-Si:H that counteract the
1788 movement of Fermi energy (E_F) and are recombination-active [294]. It can be surmised that
1789 this effect is closely related to the defect equilibration mechanisms described by the Fermi-
1790 level dependence of defect creation in the defect pool model.

1791 **4.5 TCOs for SHJ heterojunction cells**

1792 The TCO's role in SHJ cells is two-fold: (i) to provide sufficiently low contact and sheet
1793 resistance in order to transport the charge carriers coming from the a-Si:H to the metal
1794 contacts, and (ii) to act as an ARC, i.e. to maximize light incoupling into the solar cell. The
1795 quasi-standard TCO material in SHJ cells is ITO, another option is Al-doped zinc oxide
1796 (ZnO:Al) as shown in Fig.33, more recently indium oxide (In_2O_3) doped with hydrogen
1797 ($\text{In}_2\text{O}_3\text{:H}$) [295] or hydrogenated tungsten-doped In_2O_3 [296] have also been used.

1798 TCOs are degenerately doped wide bandgap semiconductors (E_g typically >3 eV): To
1799 fulfill the requirement (i), $R_{sh} < 100 \Omega/\text{sq}$ is desired. Furthermore, the required refractive
1800 index around 2 together with the necessity to achieve destructive interference in the 600 nm
1801 range lead to a thickness of the order of $d_{\text{TCO}} = 80$ nm. Maximum carrier mobility (μ) is in the
1802 order of 10 to 70 cm^2/Vs , thus with $R_{sh} = 1/(q N \mu d_{\text{TCO}})$, carrier concentrations (N) in the
1803 range of $10^{20}/\text{cm}^3$ are required. Such high carrier concentrations lead to a widening of the
1804 optical bandgap (Burstein-Moss shift), partially offset by a bandgap narrowing due to
1805 electron-impurity many body interactions, and an appreciable free carrier absorption in the
1806 longer wavelength range around the c-Si bandgap wavelength [292,297, 298]. Figure 33
1807 shows an exemplary comparison of simulated $1 - R$ and external quantum efficiency (EQE)
1808 curves for a HIT solar cell on flat wafer for various doping levels of a 85nm thick front
1809 ZnO:Al layer [299]. It is apparent from the simulation that for higher TCO doping, current is
1810 lost in the device due to inferior anti-reflection properties of the highly doped films ($1 - R$
1811 decreases) and increasing absorption in the TCO (area between $1 - R$ and the EQE increases).

1812 Comparison between the simulation (Fig. 33, left side) and experimental data obtained from
 1813 ZnO:Al and ITO used as TCOs in HIT cells (Fig. 33, right side), shows that ZnO:Al yields a
 1814 higher EQE due to the lower carrier concentration in the ZnO:Al. Further details can be found
 1815 elsewhere [299].



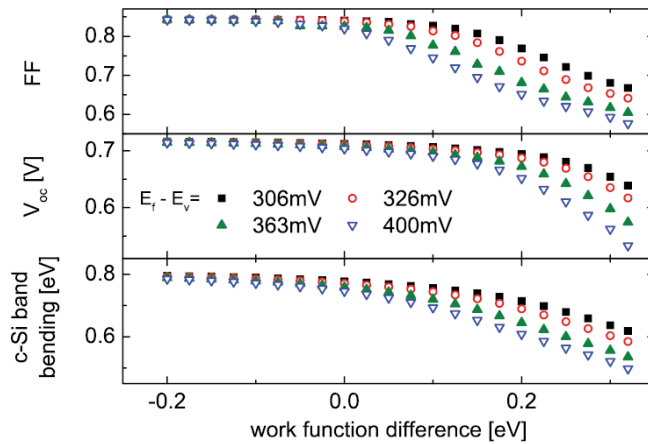
1816

1817 Fig. 33 Left side: Simulated reflectance (1-R) and EQE curves for a HIT solar cell on flat wafer for various
 1818 doping levels of the 85nm thick front ZnO:Al layer. Right side: Experimental data for a similar system using
 1819 ITO and ZnO:Al as front TCO materials. EQE is decreased for higher TCO doping. This is due to an increased
 1820 absorption and poor anti-reflection properties in the highly doped TCO film. Experimental data from ITO and
 1821 ZnO:Al used in HIT cells shows higher EQE for ZnO:Al film due to lower carrier concentration in ZnO:Al.
 1822 Reprinted with permission from [299], R. Rößler, C. Leendertz, L. Korte, N. Mingirulli, and B. Rech, Impact of
 1823 the transparent conductive oxide work function on injection-dependent a-Si:H/c-Si band bending and solar cell
 1824 parameters, *Journal of Applied Physics* **113** (2013) 144513. Copyright © 2013 American Institute of Physics.
 1825 License number 3472401268226.

1826

1827 Another aspect that has to be considered in optimizing a TCO for the use in SHJ cells
 1828 is the band alignment with the a-Si:H (Fig.25). As shown in Fig. 34, the work function of the
 1829 TCO plays an important role for the solar cell parameters. In the simulated case, a work
 1830 function difference of only 0.1 eV between the TCO and the p-a-Si:H emitter already leads to
 1831 an appreciable decrease in V_{oc} and, more pronouncedly, fill factor [299]. The reason is that
 1832 on top of the desired p-n junction diode, an undesired counter diode is formed by the
 1833 TCO/doped a-Si:H junction. This is depicted schematically in Fig.35, where an equivalent
 1834 circuit consisting of the p-n diode and the TCO/p-a-Si:H counter diode with a parallel shunt
 1835 resistance is sketched. These two diodes together with the resistance indeed yield a calculated
 1836 current-voltage (I-V) curve that can go from slightly decreased fill factors to S-shapes. Such

1837 S-shaped I-V curves are observed experimentally [300,301] and also in numerical simulations
 1838 such as the one used to generate Fig. 34 [302].

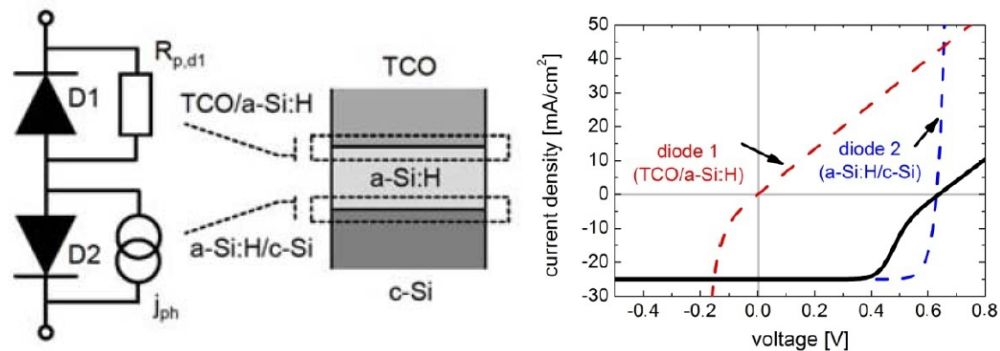


1839

1840 Fig. 34 Simulated solar cell parameters as a function of the work function difference between the TCO and the
 1841 p-a-Si:H emitter, even a work function difference of 0.1eV leads to a significant decrease in V_{oc} and fill factor. This is
 1842 due to an undesired counter diode formed by the TCO/doped a-Si:H junction. Reprinted with permission from
 1843 [299], R. Rößler, C. Leendertz, L. Korte, N. Mingirulli, and B. Rech, Impact of the transparent conductive oxide
 1844 work function on injection-dependent a-Si:H/c-Si band bending and solar cell parameters, Journal of Applied
 1845 Physics **113** (2013) 144513. Copyright © 2013 American Institute of Physics. License number 3472401268226.

1847

1848



1849

1850

1851 Fig. 35 Sketch of the TCO/a-Si:H/c-Si interface region, together with an equivalent circuit consisting of the
 1852 desired a-Si:H/c-Si p-n junction and an antiparallel, parasitic TCO/a-Si:H diode (left side). Resulting I-V curve
 1853 and contributions of the two diodes (right side). A parasitic diode is formed when there is a work function
 1854 difference between TCO and doped a-Si:H. After [303], with permission, R. Rößler, L. Korte, C. Leendertz, N.
 1855 Mingirulli, M. El Mhamdi, and B. Rech, ZnO:Al/(p)a-Si:H Contact Formation and Its Influence on Charge
 1856 Carrier Lifetime Measurements, edited by G. Willeke, H. Ossenbrink, & P. Helm. Proc. 27th European
 1857 Photovoltaic Solar Energy Conference and Exhibition, Munich: WIP Munich, 2012, p.1443.

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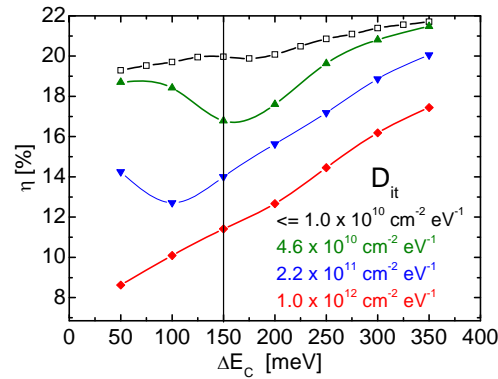
1859 This problem of an unsuitable work function is a general one for the usual n-type TCOs

1860 forming junctions with p-a-Si:H. However, it appears that it is less pronounced for the case of

1861 ITO than for ZnO:Al [299,303]. Still, one might speculate that this is a possible reason for the
1862 consistently lower fill factors in SHJ cells as compared to diffused junction cells with similar
1863 V_{oc} [255,290].

1864 **4.6 Charge transport in SHJ: I-V curves and device operation**

1865 For the SHJ cell, charge transport across the junctions may proceed both by diffusive
1866 transport as well as by tunneling processes, the detailed transport mechanisms being
1867 dependent on the materials properties (defect densities, bandgap/band offset height) as
1868 already discussed above, and also on the regime of the applied bias voltage. Under high
1869 forward bias, at the operating point of the cell, diffusive transport prevails at least in state-of-
1870 the art SHJ cells, and indications for tunnel transport are found in low forward and reverse
1871 bias [268,304,305]. If, for example, the band offset for the holes at the p-a-Si:H/n-c-Si
1872 contact depicted in the band diagram of Fig.25 becomes too high, charge carrier transport can
1873 be hindered because the charge carrier has to overcome the band offset barrier by thermionic
1874 emission or tunneling processes. Depending on the details of charge distribution and
1875 recombination at the heterointerface, this can manifest in the solar cell characteristics curve
1876 as an effect similar to a series resistance, or in an S-shaped I-V curve, [300,306] which,
1877 however, can also arise from the TCO/a-Si:H junction, as mentioned above. On the other
1878 hand, an increased band offset can also decrease the cell's sensitivity to high defect densities
1879 at the a-Si:H/c-Si junction. This is depicted in the simulation result in Fig.36, where together
1880 with a general trend of increasing cell efficiency with increasing minority-carrier band offset
1881 (in this case, ΔE_c , because an n-a-Si:H/p-c-Si cell is simulated), it is also observed that the
1882 drop in cell efficiency for increasing a-Si:H/c-Si interface defect densities is less severe if
1883 ΔE_c is large.



1884

1885 Fig. 36 Dependence of the simulated efficiency of n-a-Si:H/p-c-Si solar cells on the minority-carrier band offset
 1886 and the interface trap density (D_{it}) at the a-Si:H/c-Si interface. Cell efficiency increases with increasing
 1887 minority-carrier band offset (ΔE_C). An increased band offset decreases the cell's sensitivity to high defect
 1888 densities at the n-a-Si:H/p-c-Si junction. Also, the drop in cell efficiency is less severe (for increasing D_{it} at the
 1889 a-Si:H/c-Si interface) when ΔE_C is large. After [300], Fritzsche, A., K. Brendel, L. Elstner, W. Fuhs, K.
 1890 Kliefoth, and M. Schmidt. "Interface recombination in heterojunctions of amorphous and crystalline silicon." J.
 1891 Non-Cryst. Sol. **299-302** (2002) 663.

1892

1893 State of the art SHJ cells can be described very well with the usual 2-diode-model plus

1894 series and parallel resistance. Furthermore, it was found that the description of an a-Si:H/c-Si

1895 cell in high forward bias, i.e. notably, at the maximum power point, or V_{oc} , can be carried out

1896 in terms of the simple Shockley diffusion model, just as for (ideal) homojunction solar

1897 cells [268]. The SHJ cell essentially behaves like a single-sided junction (space-charge region

1898 only in the c-Si, recombination at the a-Si:H/c-Si interface), with one important difference:

1899 The analysis of the ideality factor (n_1) and activation energy of the reverse saturation current

1900 carried out in [268] shows that the heterojunction aspects of carrier transport across the p-n

1901 junction become more pronounced with enhanced interface passivation, and are responsible

1902 for a deviation from the ideal value of $n_1 = 1$.

1903 4.7 Double sided SHJ solar cells - state of the art

1904 De Wolf's review [255] provides an excellent and comprehensive overview on the R&D

1905 groups working on SHJ cells and their best published results. In the following, some

1906 important results are mentioned and updates are given. Note that single-sided SHJ cells are

1907 excluded from this summary, since they are discussed in Sec. 5.

1908 Many groups are today able to manufacture SHJ solar cells with efficiencies exceeding
1909 20%, and V_{oc} s well above 700 mV. However, since the rediscovery of the SHJ concept in the
1910 1990s, and the introduction of the i-a-Si:H buffer layer, the record in SHJ cell efficiency has
1911 been held by Sanyo, now Panasonic. The currently best double-sided SHJ cell has an
1912 efficiency of 24.7% ($V_{oc} = 750\text{mV}$, $J_{sc} = 39.5\text{mA/cm}^2$, fill factor = 83.2%) [248]. The cell
1913 was fabricated from a $98\mu\text{m}$ thin wafer on an area of 100cm^2 . With this step, the HIT cell not
1914 only surpasses the best published result for a large area production type cell, i.e. SunPower's
1915 24.2% efficient rear contact cell [178], but falls short by only 0.3% of the PERL cell
1916 manufactured by UNSW that holds the world record for a c-Si solar cell and is fabricated on
1917 a small area (4cm^2), with photolithographic processes that are incompatible with large-scale,
1918 low-cost industrial production. It is interesting to note that the improvement over Sanyo's
1919 previous 23.7% cell stems mainly from an improved fill factor, which went up by 2.3% as
1920 compared to the previous best cell. With a fill factor of 83.2%, the HIT cell has now indeed
1921 closed the fill factor gap that was (and, for other groups working in the field, still is) present
1922 between highest efficiency homojunction and heterojunction solar cells [303]. Furthermore,
1923 the high V_{oc} of Sanyo/Panasonic's cell is also related to the low wafer thickness. For solar
1924 cells with excellently passivated surfaces, the total (wafer thickness integrated) density of
1925 recombination-active states is dominated by the c-Si bulk recombination centers, thus scales
1926 with wafer thickness. Therefore, the photogenerated charge carrier density, thus the V_{oc} ,
1927 increases until the wafer is too thin to absorb the incoming sunlight sufficiently well.
1928 Therefore, the theoretical maximum V_{oc} peaks at 769mV for $100\mu\text{m}$ wafer thickness [307], a
1929 value that Sanyo has come surprisingly close to.

1930 Further remarkable high-efficiencies reported by the Institute of Microengineering (IMT)
1931 at Ecole Polytechnique Fédérale de Lausanne (EPFL), for SHJ cells based on n-type and p-

1932 type c-Si wafers [263] are 22.1% and 21.4%, respectively. To our knowledge, the latter is the
1933 highest reported for a SHJ cell on p-type wafers.

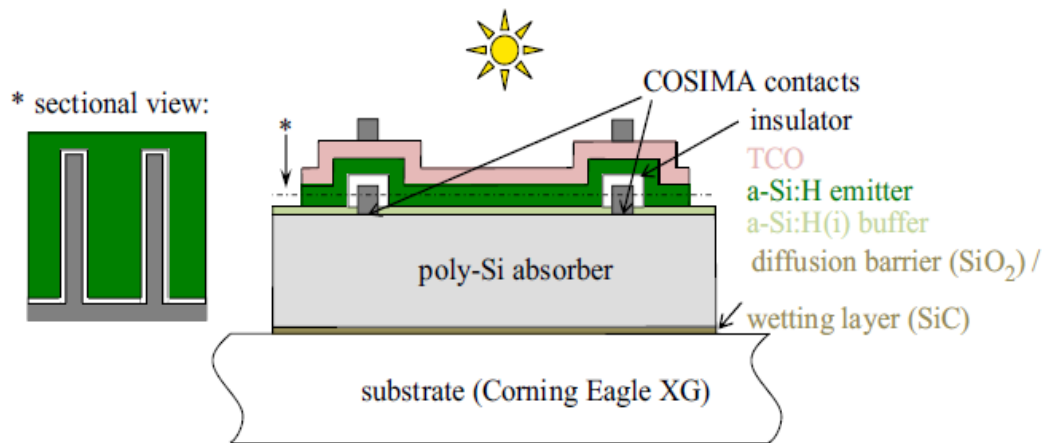
1934 Regarding highly efficient cells on large area and industrialization of the SHJ concept,
1935 Sanyo/Panasonic have shown above 21% cell efficiency (>18% module efficiency) in
1936 industrial production [249]. The French Institut National de l'Énergie Solaire (INES) has
1937 reported 21% and 22.2% efficient cells on 103cm² made with Ag screen-printed and Cu
1938 plated contacts, respectively [259], and Roth&Rau/Meyer Burger have shown large area (6")
1939 cells with 21.3% efficiency [308]. Very recently, Choshu industry has reported a 24.1%
1940 efficient SHJ cell on an area of 243.4cm², which features cerium oxide and hydrogen co-
1941 doped indium oxide films as TCOs [309]. Further important steps to lowering the levelized
1942 cost of energy are Roth&Rau's 21.6% efficient cell on a 239 cm² pseudosquare Cz wafer
1943 with a Ag-free front grid, cells above 21% efficiency on a pilot line equipment and their
1944 demonstration of a 303W SHJ module made of sixty 6" pseudosquare SHJ cells [310]. A
1945 production line with a throughput of 4800 wafers/h and a target efficiency of 21% is also
1946 available.

1947 Si heterojunctions have also been used in hybrid cell concepts, i.e. cells where only one of
1948 the junctions is formed as a SHJ. An example of this concept is an inverted SHJ hybrid cell,
1949 where in addition, the p-n junction is located on the rear of the cell instead of the front side
1950 that is facing the sun. With a rear side SHJ (i.e. back heterojunction) in combination with a
1951 diffused (thus, homojunction) front surface field and point contacts on the front, a cell
1952 efficiency of 22.8% has been reported [311].

1953 Another hybrid concept is pursued by Hekmatshoar et al. who introduce a thin, highly
1954 doped epitaxial c-Si film between the c-Si wafer and an a-Si:H on one side, and an a-Si:H
1955 heterojunction with an additional a-Ge:H interlayer on the rear, leading to a 21.4% efficient
1956 cell [312].

1957 **4.8 Future direction**

1958 Given the rapid progress discussed, it is very likely that c-Si wafer based SHJ technology
1959 will approach the 25% cell level efficiency in production. However, there remain many
1960 challenges for further improving SHJ cell technology. For example, in order to improve J_{sc} ,
1961 better transparency of the contact layers is needed. For the a-Si:H films, this might lead to
1962 their substitution by microcrystalline Si (μc -Si:H), amorphous Si oxide (a-SiO_x:H) or
1963 amorphous Si carbide (a-SiC_x:H) films. TCOs with increased transparency/carrier mobility
1964 could be based on hydrogen doped In₂O₃, or alloys of indium and oxygen with other metals
1965 [309]. For the TCO, the indium cost issue might be solved by its substitution, e.g. by ZnO:Al,
1966 although the problem of an unsuitable work function/parasitic diode on p-a-Si:H needs to be
1967 solved, probably by TCO/a-Si:H interface engineering (by insertion of suitable interlayers).
1968 Another cost driver is the high amount of Ag used in screen-printed contacts. This has
1969 already led to approaches using electroplating. However, their long-term reliability is as yet
1970 unproven. Looking further into the future of c-Si based PV, it is clear that SHJ are an ideal
1971 technology not only for fabricating cells on ever thinner wafers, but also for innovative
1972 approaches based on high quality wafer-like thin-film Si solar cells on glass. In this case, the
1973 key feature of the SHJ technology is that process temperatures stay below 200°C at all times,
1974 i.e. far below the melting temperature of the glass. Promising results have been demonstrated
1975 for SHJ on kerf-loss free Si thin-films transferred to a glass carrier [313], and also for a-
1976 Si:H/poly-Si cells (Fig. 37), where a ~10 μm thin Si film is deposited onto the glass with high
1977 rate e-beam evaporation, then recrystallized by scanning with a line-shaped electron or laser
1978 beam. This yields a polycrystalline Si film with grain sizes up to a cm^2 [314].



1979

1980 Fig. 37 Schematic cell design of the Front ERA (front contacted electron beam recrystallized absorber)
 1981 a-Si:H/poly-Si heterojunction solar cell on glass. The poly-Si absorber is a $\sim 10\mu\text{m}$ polycrystalline Si thin-film
 1982 consisting of grains with a width in the mm range, and up to several cm long. Polycrystalline Si thin-film is
 1983 deposited by e-beam evaporation with high deposition rate, and then recrystallized by electron or laser beam.
 1984 Reproduced from [314], Haschke, J. and Jogschies, L. and Amkreutz, D. and Korte, L. and Rech, B.
 1985 Polycrystalline silicon heterojunction thin-film solar cells on glass exhibiting 582mV open-circuit voltage, *Solar*
 1986 *Energy Materials & Solar Cells*, **115** (2013) 7. Copyright © 2014 Elsevier B.V. License number
 1987 3472100659635.

1988 Furthermore, their high-efficiency makes SHJ cells (and other high-efficiency c-Si
 1989 based solar cells concepts) a very interesting candidate for combining them with wide
 1990 bandgap cells into double-junction solar cells, which have the potential to break the
 1991 efficiency limit of single-junction solar cells. Combinations of III-V based top cells with c-Si
 1992 cells are discussed in Sec.6. However, due to the thermal constraints, the combination of III-
 1993 V with SHJ cells is difficult. An alternative approach that has recently drawn much attention
 1994 are metal halide perovskite-based top cells (see Sec. 10), which can be combined with SHJ
 1995 cells in either monolithically integrated 2-terminal devices [315, 316, 317] or by mechanical
 1996 stacking of the two sub-cells, leading to a 4-terminal device, where each subcell has its own
 1997 electrical connection. For the monolithically integrated 2-terminal devices, efficiencies have
 1998 reached 21.4% [315]. For the 4-terminal cells, efficiencies between 13 and 22.8% have been
 1999 reported [318, 319,320].

2000 The development of compatible processes and, importantly, semi transparent contact
 2001 systems for the perovskite top cells are currently an important field of research, with different
 2002 approaches ranging from sputtered TCOs to solution processed layers such as Ag nanowires

2003 [319] or graphene [321]. Furthermore, it has been recognized that tuning of the perovskite top
2004 cell's bandgap to an optimum value of around 1.74eV will allow for further improvements of
2005 double-junction cell efficiency. Recently, it was experimentally shown that a photostable
2006 perovskite based on mixtures of cesium and formamidinium as well as mixed iodide and
2007 bromine can be employed to tune the bandgap to 1.74eV enabling a high V_{oc} of 1.2eV [322].

2008 **5.0 Crystalline Si based solar cells: back heterojunction**

2009
2010 A reasonable estimate for the technologically achievable efficiency limit of single-
2011 junction c-Si based solar cells is about 28% ($J_{sc} = 42.5\text{mA}/\text{cm}^2$, $V_{oc} = 760\text{mV}$, fill factor =
2012 87%) [323]. To approach the theoretical efficiency limit in Si based solar cell [307], several
2013 strategies can be explored. One of the most attractive technologies is the IBC cell structure.
2014 Here, as mentioned in Sec.3, both cell electrodes are located on the rear side of the solar cell
2015 and laid out as two interdigitated combs. If the front surface recombination processes have
2016 been reduced, this approach overcomes the main limitation to the J_{sc} of the cell imposed by
2017 the front grid shaped contact shadowing. The shadowing is about 8% of the cell area and can
2018 be reduced to 4% using relatively sophisticated and expensive techniques [76]. In the IBC
2019 structure the front side of the cell is completely exposed to the sun to maximize light
2020 absorption when an appropriate anti-reflection coating is deposited on the device surface.
2021 IBC concept, initially proposed by Lammert and Schwartz [183], is the most relevant feature
2022 of the SunPower solar cell that achieved a record efficiency of 24.2% on n-type Fz c-Si wafer
2023 [178]. Here, the choice of Si heterojunction, instead of high-temperature emitter diffusion to
2024 form a homojunction, has demonstrated several advantages, such as: (i) high V_{oc} due to the
2025 potentiality of SHJ and due to the good c-Si surface passivation promoted by the a-Si:H layer
2026 that reflects in high cell efficiency as demonstrated by several groups as listed in Ref.[324].
2027 Even though the SunPower homojunction record efficiency cell reaches a V_{oc} value of 720
2028 mV, the highest V_{oc} value of 750 mV, as well as cell efficiency of 24.7% on c-Si based

2029 101.8cm² solar cell have been recently demonstrated by Sanyo-Panasonic heterojunction HIT
2030 cell [325]; (ii) excellent stability since the extremely thin a-Si:H layer used in the HJ
2031 technology is not prone to the undesired Staebler-Wronski degradation effect [326] that still
2032 affects the a-Si:H thin-film solar cells; (iii) lower voltage reduction under thermal stress
2033 during sunlight exposure with respect to conventional c-Si based cells (-0.3%/°C vs -
2034 0.5%/°C). This represents a great advantage in operating conditions since the cells are
2035 packaged using glass and plastic and left under sunlight with low possibility to dissipate the
2036 thermal excess; (iv) lower cell manufacturing cost due to reduced process time and to lower
2037 thermal budget in the cell fabrication. The last allows the use of very thin c-Si wafer [327]
2038 that can strongly reduce the photovoltaic cost [29,328].

2039 By merging the SHJ and IBC concepts it is possible to realize a promising technology
2040 for c-Si solar cell [329]. In this section, relevant issues of IBC-SHJ (i.e. back heterojunction)
2041 design for solar cell fabrication will be discussed and the industrial perspective of this cell
2042 concept will be also be discussed.

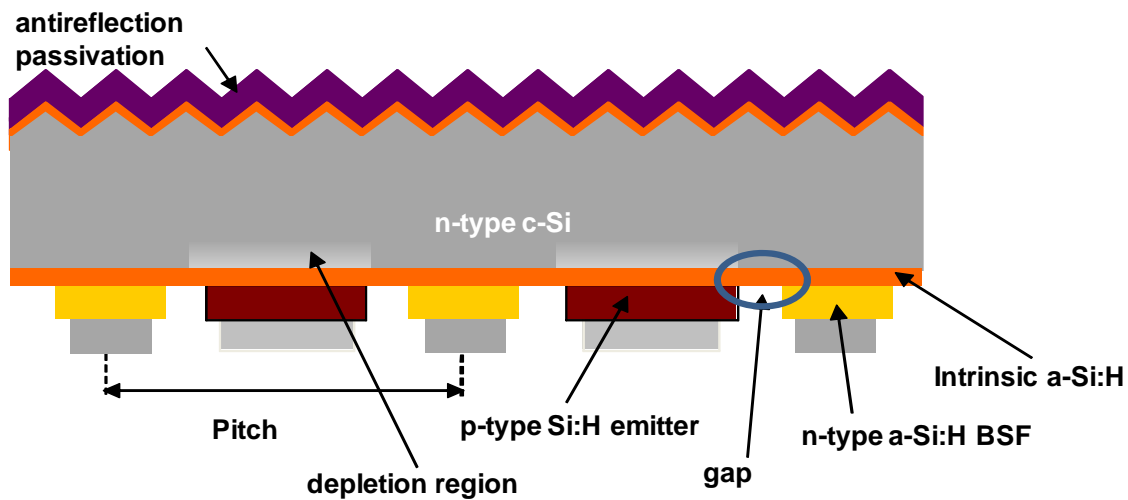
2043

2044 **5.1 Brief history and status of art**

2045 The idea to apply the IBC concept to the HJ cell, to take advantage of low thermal
2046 budget process and high V_{oc} together with a fully exposed sunward side, was proposed by Lu
2047 et al. [330]. They developed cells based on polished 2.5 Ω -cm n-type c-Si Fz 300 μ m thick
2048 wafer. Both 20 nm thick each p-type a-Si:H emitter and n-type a-Si:H base contact were
2049 deposited in a multi-chamber PECVD system at temperature of 200°C at the rear side of the
2050 cell to form an interdigitated structure, by photolithography, consisting of 1.2mm wide strips
2051 for emitter and 0.5mm for base contact, separated by 2 μ m wide non-diffused and non-
2052 passivated region. The sunward side was passivated by 20 nm intrinsic a-Si:H layer,
2053 subsequently covered with ITO and magnesium fluoride double layer as ARC. In subsequent
2054 publication [331] the same group of authors demonstrated the role of Si surface passivation

2055 between the doped regions to achieve higher cell efficiency. Tucci et al. presented a novel
2056 scheme for heterojunction called **Back Enhanced Heterostructure with INterDigitated**
2057 **(BEHIND)** contact solar cell [332-334]. This method neither involved wet chemical steps,
2058 nor photolithography to pattern the two interdigitated back contacts. They were deposited by
2059 PECVD as a comb shape with the help of metallic masks, self-mechanically aligned in a
2060 specifically designed holder for both the c-Si wafer and the masks. In principle this method
2061 may easily be scaled up for large area cells, appropriate for industrial applications. The
2062 BEHIND solar cells were fabricated on 200 μ m thick, <100>, 1 Ω -cm p-type, Cz c-Si wafer.
2063 After front side alkaline texturing and RCA cleaning, a double layer stack of a-Si:H/SiN was
2064 deposited on the sunward side, acting as passivation and anti-reflection layer [335]. Then on
2065 the whole polished wafer backside, after a short 2% HF procedure to remove the native
2066 oxide, an intrinsic a-Si:H buffer layer was deposited before the n-type a-Si:H emitter. To
2067 increase the emitter conductivity a chromium silicide (CrSi) layer was then formed [336] by
2068 chromium (Cr) evaporation and wet chemical removal. A metallic mask, fabricated from a
2069 100 μ m thick molybdenum foil having a comb shaped aperture, was fixed over the emitter
2070 layer. A dry etching procedure using nitrogen trifluoride gas was performed to remove the n-
2071 type a-Si:H portion not covered by the mask, using settings defined on the base of previous
2072 experiments [337]. Subsequently, keeping the mask in the same position, the cell base contact
2073 was formed by an intrinsic a-Si:H buffer and a p-type a-Si:H layers. Through the same mask,
2074 a 30nm thick Cr layer was evaporated. Then a low-temperature sintering Ag paste was
2075 screen-printed on both interdigitated contacts [338]. The BEHIND cell was the first IBC-BHJ
2076 (Fig. 38) cell fabricated without any photolithographic step and it demonstrated the
2077 possibility to deposit a-Si:H film through metal masks. The total area of the solar cell was
2078 6.25cm². Different versions of the cell process were presented in literature and the best results

2079 are reported in Table 1. Schematic diagram of IBC-BHJ cell is shown in Fig. 38. Here, n-type
 2080 c-Si, p-type a-Si:H and n-type a-Si:H acts as base, emitter and BSF respectively.



2081

2082

2083 Fig. 38 Schematic diagram of IBC-BHJ cell showing grid-less front surface. Neglecting the recombination at
 2084 front and rear c-Si surface, when charge carriers are photogenerated within the c-Si wafer, due to concentration
 2085 gradient, charge carriers diffuse to the rear side of the cell where they can be collected by their respective
 2086 electrodes if charge carriers are able to arrive in the depletion region formed close to the p-type a-Si:H emitter
 2087 layer. Therefore, in principle, the distance between two emitter regions should be thinner than half of minority
 2088 carrier diffusion length. Photogenerated electrons can be collected in the n-type a-Si:H contact if able to
 2089 overcome the intrinsic a-Si:H passivation layer. BHJ design eliminates shadowing effect caused by metal grids
 2090 and allows sufficient metal to be used at the rear side to minimize resistive losses.

2091

2092 In early 2011, Helmholtz-Zentrum Berlin (HZB) together with Institute for Solar

2093 Energy Research Hamelin (ISFH) group developed a 20.2% efficient IBC-BHJ cell [232] on

2094 n-type 3Ω-cm Fz wafer. The front side was textured and phosphorous diffused to form a front

2095 surface field, and then passivated by SiO₂/SiN. The back side area was covered by 60%

2096 emitter contacts (p-type), 28% base contact (n-type) and 12% gap space between these,

2097 passivated by a SiO₂/SiN stack, with pitch in the range of millimetres. The metal contact was

2098 Al for both emitter and base regions. Two different approaches were considered: with or

2099 without intrinsic buffer layer just under the emitter, obtaining in both cases nearly 20%

2100 efficiency. In the first case V_{oc} is 40mV higher (673mV), but the fill factor is nearly 3%

2101 absolute lower (75.7%); due to the J_{sc} (39.7mA/cm²) the efficiency was 20.2%. Without

2102 buffer layer the V_{oc} was 633mV but the fill factor was as high as 78.8% with the same

2103 current, so that the efficiency was 19.8%. The entire cell fabrication process was performed
2104 on 1cm² area by photolithographic steps. The best results are summarized in Table 1.

2105 The participants of the SHARCC project in France developed an innovative process
2106 called SLASH (Structuring by Laser Ablation of Si Heterojunction). They suggested the
2107 following sequence of steps: (i) emitter deposition and patterning by laser ablation; (ii) base
2108 contact deposition and laser patterning; (iii) front ARC deposition; (iv) ITO deposition; (v)
2109 screen-printing at low-temperature; (vi) laser ablation to separate the contacts. With this
2110 technology a 19% efficiency (Table 1) on 25 cm² area has been demonstrated [259,339].

2111 The IBC-BHJ proposed by IMEC Belgium started from Cz n-type, 3-4Ω-cm <100> c-
2112 Si wafer with thickness of either 150 or 280μm. Different front side passivation schemes
2113 were adopted: n⁺-diffusion (POCl₃) and HJ on both textured and flat surface. Then on the rear
2114 side of the wafer a i-a-Si:H passivation layer, and p⁺-doped emitter were deposited by
2115 PECVD at temperatures less than 200°C. An ITO transparent conductive oxide was deposited
2116 on the a-Si:H layers. Photoresist was spun on both sides of the wafer, and patterned on the
2117 rear side, before etching through the ITO. Openings through the a-Si:H layer were performed
2118 by wet chemical etch. After HF dip, Al base contacts were deposited by e-beam evaporation.
2119 The emitter contact was obtained by depositing Ti/Pd/Ag using e-beam evaporation on the
2120 ITO layer using shadow masks. A final anneal was performed in nitrogen at low-temperature.
2121 An efficiency of 15.2% efficiency was achieved on 1cm² area [340]. The best results are
2122 summarized in Table 1.

2123 The BACH (Back Amorphous-Crystalline Si Heterojunction) cell was developed at
2124 University of Toronto. The cell was fabricated on n-type 300μm thick 20 Ω-cm Fz c-Si
2125 wafer. In this case the fabrication process consisted of different photolithographic steps with
2126 at least 4 photomasks. The process sequence also included initial oxidation of the n-type
2127 wafer to have surface passivation, and electrical isolation between emitter and base contacts

2128 at the back side. The front surface was textured. The efficiency of IBC-BHJ cells with an area
 2129 of circa 1cm^2 was of 16.7%, with V_{oc} of 641mV, and J_{sc} of $33.7\text{mA}/\text{cm}^2$. However fill factor
 2130 was appreciably higher than 77% [341,342]. The major limiting factor for both V_{oc} and J_{sc}
 2131 was recognized due to surfaces passivation.

2132 The latest design is by LG Electronics. However very few details are available on the
 2133 technology adopted. The design started on n-type Cz and Fz c-Si. After texturing, n-a-
 2134 Si:H/ARC films were deposited for FSF front surface passivation. Then on the wafer rear
 2135 side, n-type a-Si:H base and p-type a-Si:H emitter were deposited. On both doped regions the
 2136 TCO was deposited and subsequently an Ag metal contact was screen printed, or Cu
 2137 electrodes were electroplated [343]. In February 2014 Panasonic company announced
 2138 efficiency higher than 25% [344] on very large area device as reported in Table 1, in which
 2139 all the best results are reported.

2140 Table 1 List of PV parameters of the IBC-BHJ cells.

2141

Institution	V_{oc} (mV)	J_{sc} (mA/cm^2)	Fill factor (%)	Eff. (%)	Area (cm^2)	c-Si wafer	Patterning	Metallization
Panasonic	740	41.82	82.7	25.57	143.7	n-type	-	-
LG Electronics	723	41.8	77.4	23.4	4	n-type Fz	Photolithog.	Sputtered Al
	692	38.4	77.9	20.7	238.95	n-type Cz	Screen printing	Screen Printing Ag
	716	37.5	76.4	20.5	238.95	n-type Cz	Screen printing	Electroplated Cu
HZB	673	39.7	75.7	20.2	1	n-type 3 Ω -cm Fz	Photolithog.	Evaporated Al
INES-CEA	695	36.6	75.2	19	25	n-type 1-5 Ω -cm Fz	laser	Screen Printing Ag
University of Toronto	641	33.7	77.3	16.7	1	n-type 1 Ω -cm	Photolithog.	Evaporated
IMEC	605	39.1	64	15.1	1	n-type 1-4 Ω -cm	Photolithog.	Evaporated
ENEA	695	35.3	60.9	15	6.25	p-type 1 Ω -cm	Shadow mask	Evaporated
University of Delaware	602	26.7	73	11.8	1.32	n-type 2.5 Ω -cm	Photolithog.	Evaporated

2142

2143 5.2 Interdigitated back contact design

2144 Several aspects of the device design are needed to be carefully accounted for to achieve
 2145 high-efficiency solar cell. One of them is, for example, is having minority-carrier lifetime
 2146 corresponding to diffusion length at least three times higher than the wafer thickness.
 2147 Moreover other parameters have to be rightly addressed to design the highest efficiency solar

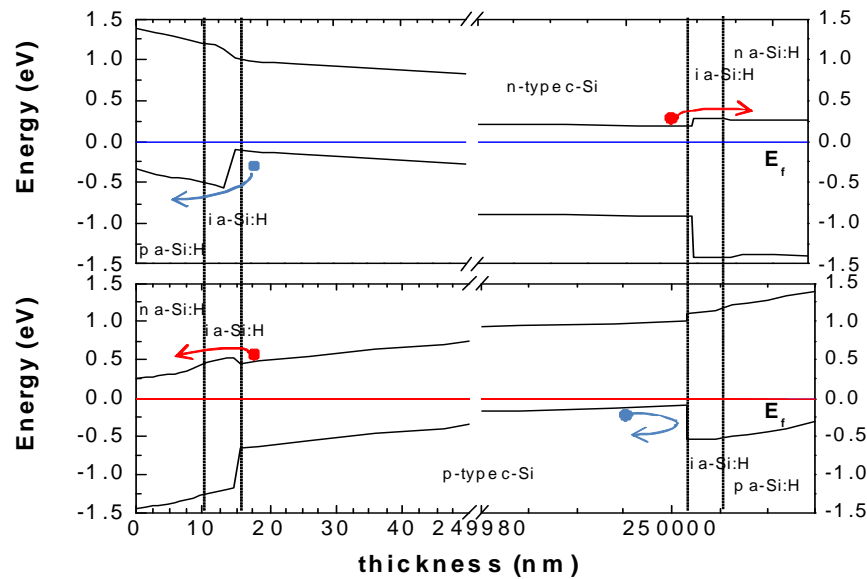
2148 cell. In this section the choice of materials and the design aspects needed to optimize the
2149 IBC-BHJ cell are reviewed.

2150

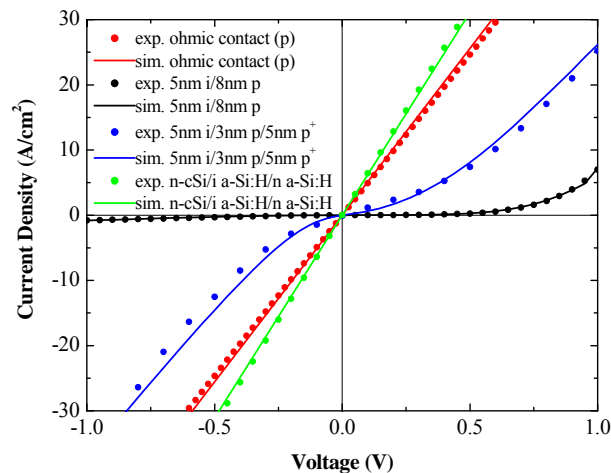
2151 **5.2.1 Choice of c-Si wafer**

2152 The choice of wafer type and doping level play a dominant role in device design due
2153 to the asymmetry of material properties respect to the carriers. Some considerations from
2154 physics, chemistry, and industrial engineering can drive that choice but sometime in opposite
2155 directions. Physically, p-type c-Si should be used in IBC solar cell since the minority
2156 photogenerated carriers move by diffusion and, when p-type is chosen, minority-carriers are
2157 electrons with lower effective mass and higher mobility than holes [341]. On the other hand
2158 n-type c-Si should be preferred to avoid boron-oxygen undesired complex formation, which
2159 is responsible for efficiency degradation under sunlight exposure [345]. The best HJ cell
2160 efficiency was demonstrated on n-type c-Si [327] due to useful band alignment at the both
2161 front and rear interfaces [346], as evident from the upper side of Fig. 39. The asymmetry in
2162 the offset displacement between a-Si:H and c-Si, higher in valence band than in conduction
2163 band [287], plays a role in the device design. It is not a serious problem for the main p-n
2164 junction due to the electric field arising from the junction built-in potential, but it introduces a
2165 difficulty for the base contact [347]. Band distributions, as deduced from numerical
2166 simulations [348] of HJ device based on the two different doping types of c-Si wafers, are
2167 compared in Fig. 39. The n-type c-Si/n-type a-Si:H contact forms an Ohmic contact and a
2168 spontaneous BSF helpful to keep holes away from the base metal electrode. The p-type c-
2169 Si/p-type a-Si:H contact needs some care to ensure the majority carriers collection with
2170 reduced probability of recombination at the base metal electrode. A comparison of I-V
2171 characteristics of HJ base contacts of devices based on p-type or n-type c-Si wafer is shown
2172 in Fig. 40, as deduced from numerical simulations (solid lines) performed on different a-Si:H
2173 layer thicknesses and experimental results (symbols). By comparing experiment and the

2174 simulation results, the perfect Ohmic behaviour of n-c-Si/i-a-Si:H/n-a-Si:H heterostructure is
 2175 evident. In case of p-type c-Si, a p⁺-layer is needed to approach the Ohmic characteristic as
 2176 that obtainable using Al diffusion into p-type c-Si, shown in Fig. 40 as red symbols and solid
 2177 lines. A density of states of $1 \times 10^{15}/\text{cm}^3/\text{eV}$ within intrinsic a-Si:H layer has been used in
 2178 performing the simulations.



2179 Fig. 39 Band diagram comparison of HJ structure based on n-type c-Si wafer (upper side) and p-type c-Si wafer
 2180 (lower side) as deduced from numerical simulations. The light impinges the heterostructure on the left side.
 2181 Electrons (red dots) can easily cross the small band offset at the p-c-Si/n-a-Si:H interface as well as at n-c-Si/n-
 2182 a-Si:H. Holes (blue dots) cross the n-c-Si/p-a-Si:H interface with the aid of electric field, but can be reflected at
 2183 the p-c-Si/p-a-Si:H interface due to the large valence band offset between c-Si and a-Si:H materials. Note that
 2184 band offset is higher in the valence band than in the conduction band, plays a role in the device design. Both
 2185 Ohmic contact and a spontaneous BSF is formed between n-type c-Si/n-type a-Si:H and keeps holes away from
 2186 reaching the metal electrode.
 2187
 2188

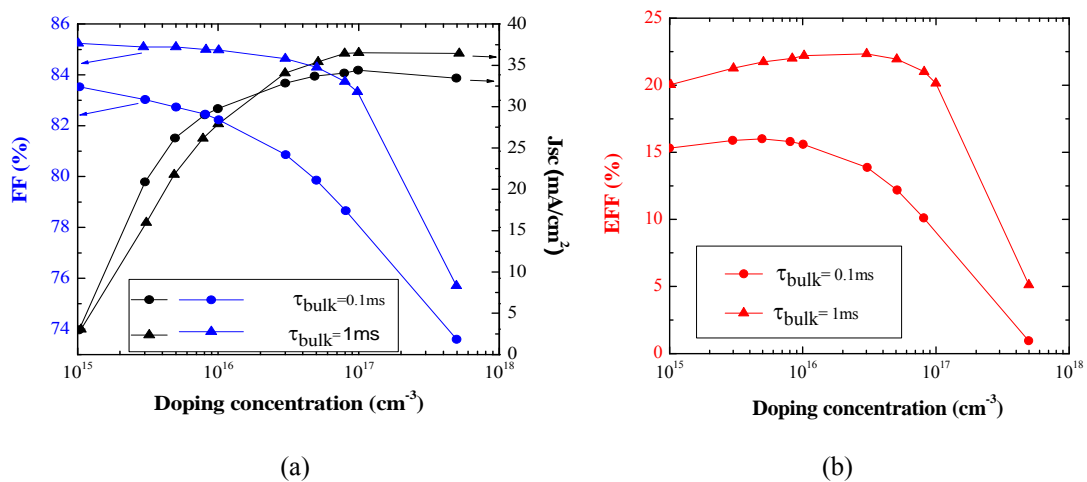


2189 Fig. 40 I-V characteristics in dark conditions of heterojunctions based on p-type and n-type c-Si wafer.
 2190 Experimental data (exp.) and simulations (sim.) are reported as symbols and solid lines respectively. A perfect
 2191

2192 Ohmic contact can be seen for the n-c-Si/i-a-Si:H/n-a-Si:H heterostructure (green dots and curve). For p-c-Si, a
 2193 p⁺-layer is required for Ohmic contact which can be obtained by Al diffusion into p-c-Si (red dots and curve).
 2194 Thicknesses and doping of a-Si:H films are relevant to achieve a properly working contact at p-c-Si/p-a-Si:H
 2195 interface. The n-c-Si/n-a-Si:H is less critical, while the p-c-Si/p-a-Si:H contact needs particular care. Indeed
 2196 only high doping values of p-a-Si:H layer can avoid a barrier formation against carrier transport, as evident
 2197 comparing the blue dots and curve with the black ones.
 2198

2199 Wafer doping and bulk lifetime play a role in interdigitated contact geometry as
 2200 demonstrated by two dimensional numerical simulations of the IBC-BHJ device reported in
 2201 [349], in which p-type c-Si wafer is adopted. As expected, J_{sc} reduces from 37mA/cm² by
 2202 increasing the doping concentration from 10Ω-cm to 0.1Ω-cm due to bulk lifetime
 2203 degradation in highly doped regions, where Auger mechanism dominates the recombination
 2204 process. At the same time fill factor increases due to reduced bulk series resistance.

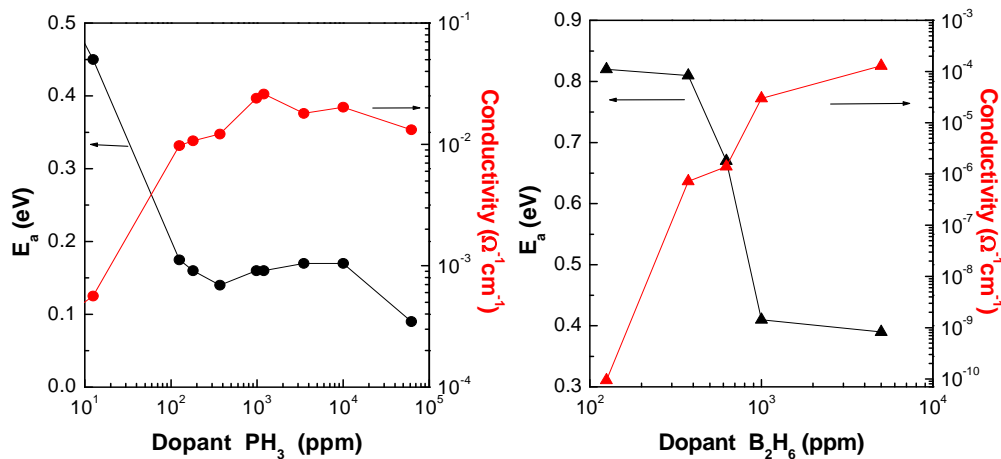
2205 Figure 41 shows the effect of doping concentration on fill factor and cell efficiency
 2206 for different bulk lifetime, taking into account a textured surface for the c-Si. In these
 2207 simulations, the distance between the doped a-Si:H regions has been fixed at 100μm, and a p-
 2208 type c-Si doping density of $5 \times 10^{16}/\text{cm}^3$ (0.5Ω-cm) should be preferred [330].



2209
 2210 (a) (b)
 2211 Fig. 41 Simulation results on the effect of the p-c-Si wafer doping concentration on (a) fill factor (FF) and J_{sc} ,
 2212 and (b) efficiency (EFF) of an IBC-BHJ solar cell. As can be seen, preferred doping concentration is around
 2213 $5 \times 10^{16}/\text{cm}^3$ (0.5Ω-cm). Fill factor and efficiency decreases beyond this concentration. Beyond the doping
 2214 concentration of $5 \times 10^{16}/\text{cm}^3$, J_{sc} remains almost constant. The decrease in efficiency is due to the decrease in
 2215 fill factor. Two different values of bulk lifetime are used in the simulations: 0.1ms and 1ms reported as circles and
 2216 triangles respectively. Higher the bulk lifetime, better the cell performances. In this work, the distance between
 2217 doped a-Si:H regions has chosen as 100μm.
 2218

2219 5.2.2 a-Si:H doping

2220 Another asymmetry to be considered in device design is due to the difference between
 2221 doping effectiveness of n- and p-type a-Si:H material. N-type (p-type) doping, obtainable by
 2222 adding PH₃ (B₂H₆) to the SiH₄ in PECVD chamber during the plasma, ensures higher film
 2223 conductivity and lower activation energy. In Fig. 42, activation energy and conductivities of
 2224 p- and n-type a-Si:H films are reported as a function of dopant concentration in the gas
 2225 mixture during the PECVD process [350]. Unfortunately, in doped a-Si:H thin layer, the
 2226 thinner the film the higher the activation energy [351]. Therefore the choice of any emitter
 2227 thickness should be carefully considered and verified to correctly design an IBC-BHJ solar
 2228 cell.



2229

2230 Fig. 42 Left side: Dark conductivity and activation energy (E_a) of n-a-Si:H films versus phosphine (PH_3) content
 2231 in the gas mixture during the film growth by PECVD. Right side: Dark conductivity and activation energy of p-
 2232 a-Si:H films versus diborane (B_2H_6) content in the gas mixture during the film growth by PECVD. For both
 2233 types of dopants, by increasing dopant concentration, activation energy decreases and conductivity increases.
 2234 High film conductivity and low activation energy are required. Note that, thinner the film, higher the activation
 2235 energy. In BHJ solar cells, doped a-Si:H is used as emitter. Therefore, to design BHJ solar cell, emitter thickness
 2236 should be carefully chosen.

2237

2238 To improve the electrical properties of n-type a-Si:H layer, a chrome silicon (CrSi)
 2239 formation on top of the amorphous film was suggested [336]. This CrSi can be obtained by
 2240 depositing 30nm of Cr on doped a-Si:H and patterning it by wet chemical etch in a solution
 2241 of 30g of cerium ammonium nitrate ($(\text{NH}_4)_2\text{Ce}(\text{NO}_3)_6$), 9ml CH_3COOH and 200ml of DI
 2242 water. Activation energy reduction from 0.24eV down to 0.017eV was obtained. CrSi can
 2243 also be useful in the case of p-type a-Si:H. Indeed the presence of the CrSi layer does not

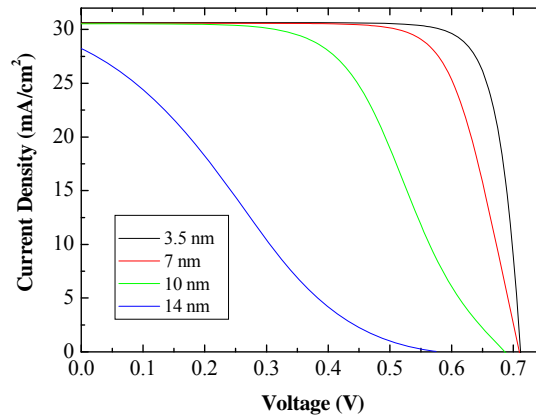
2244 affect the doping type of the doped a-Si:H film on which it is formed. Activation energy
2245 reduction from 0.36eV down to 0.14eV has been achieved [336]. This treatment improves the
2246 p-c-Si/i-a-Si:H/p-a-Si:H/p⁺-a-Si:H heterojunction contact to form an effective ohmic contact,
2247 as shown in Fig. 40 [347]. Since both contacts are on the rear side of the cell the energy gap
2248 of the a-Si:H becomes less relevant. The a-Si:H film on the rear side does not work as a
2249 window layer. Therefore lower bandgap should be preferable in order to reduce the valence
2250 band offset at a-Si:H/c-Si interface, thus enhancing the charge collection as in the case of μ c-
2251 Si:H cell [352]. Nevertheless the buffer layer should continue to be amorphous for better
2252 passivation of c-Si surface. On the other hand higher bandgap materials must be avoided as
2253 suggested in Ref. [13], otherwise the energy mismatch between the two valence bands at the
2254 heterojunction produces a high barrier that cannot be overcome by the electric field.

2255 **5.2.3 Buffer layer - Intrinsic a-Si:H**

2256 It is widely accepted that an effective heterojunction must have intrinsic, high quality
2257 a-Si:H buffer layer to passivate the c-Si surface and to separate the doped a-Si:H film
2258 [325,353]. Its thickness must be carefully optimized taking into account of the monohydrides
2259 (Si-H), dihydrides (Si-H₂) content at the beginning of the a-Si:H film deposition to avoid
2260 epitaxial growth [354]. Potential for further improvements are still under investigation to
2261 reduce the SRV [278, 355]. In the case of IBC-BHJ device, depending upon the patterning
2262 processes, the situation is more complex since the buffer layer should be the same for both
2263 base and emitter contacts. Two dimensional numerical simulations have been used to
2264 evaluate the effect of the buffer layer thickness. In Ref.[338] it is reported that increasing the
2265 i-a-Si:H buffer layer thickness, the light I-V characteristics under standard AM1.5G (G stands
2266 for global) condition are strongly affected resulting in a fill factor reduction. In the simulation
2267 a defect density of $10^{17}/\text{cm}^3/\text{eV}$ is homogeneously distributed along the buffer layer thickness.
2268 This effect is related to the recombination at the a-Si:H/c-Si interface. Indeed when the i-a-

2269 Si:H layer becomes thicker, the p-type a-Si:H base contact is not able to collect the holes due
2270 to the valence band offset at the edge of a-Si:H/c-Si interface. These holes recombine through
2271 a-Si:H/c-Si interface defects, with electrons generated in the c-Si bulk and diffusing toward
2272 the n-type contact. This results in a barrier formation against carrier collection from the base
2273 contact. This recombination produces an S-shape in the I-V curve, such as coming from an
2274 anti-series double diode device. The simulated band bending at the edge of c-Si/i-a-Si:H/p-a-
2275 Si:H is already shown in Fig. 39. Of course the intrinsic layer cannot be completely removed
2276 otherwise the c-Si surface passivation in the region not covered by doped a-Si:H layer will be
2277 immediately lost [232]. However in IBC-BHJ, the c-Si rear side surface passivation is not the
2278 same as in the case of SHJ (i.e. front heterojunction) emitter. Indeed now the emitter region
2279 partially covers the buffer layer on the c-Si surface, while the other part is covered by the
2280 base contact HJ. A gap region between base and emitter contact also has to be considered, as
2281 evident from Fig. 38. This difference between SHJ and IBC-BHJ in surface passivation
2282 accounts for only $\sim 2\%$ of the fill factor change [234]. Moreover the higher the defect density
2283 within the buffer layer the stronger the undesired S-shape effect even for a relatively thin
2284 buffer layer.

2285 The thickness of the intrinsic a-Si:H buffer layer is also important for consideration or
2286 improved performance. The thicker the buffer layer, the lower the cell fill factor as shown in
2287 Fig. 43. Increasing the buffer layer thickness from 3.5nm up to 14nm, a S-shape appears in
2288 the I-V characteristic. Further details concerning the two dimensional simulations shown in
2289 Fig. 43 can be found in Ref. [338].



2290

2291 Fig. 43 Simulated I-V curves as a function of intrinsic a-Si:H buffer layer thickness. By increasing buffer layer
 2292 thickness from 3.5nm up to 14nm, an S-shape appears in the I-V characteristic. This effect refers to a barrier
 2293 formation against carrier collections that forms at the heterojunction interface. Therefore very thin buffer layer
 2294 should be adopted to obtain a proper working heterojunction device. On the other hand, buffer layer thickness
 2295 should not be further reduced otherwise is very difficult to ensure a conformal coverage of Si surface. Moreover
 2296 buffer layer thinner than 5nm does not represent a good choice. Indeed if this buffer is too thin, less than 5nm,
 2297 surface passivation cannot be guaranteed, due to higher content of dihydrides (Si-H₂) radicals at the interface
 2298 between c-Si and a-Si:H. A 5-7nm thick buffer layer represents the best choice for practical use.
 2299

2300 5.2.4 Metal contacts

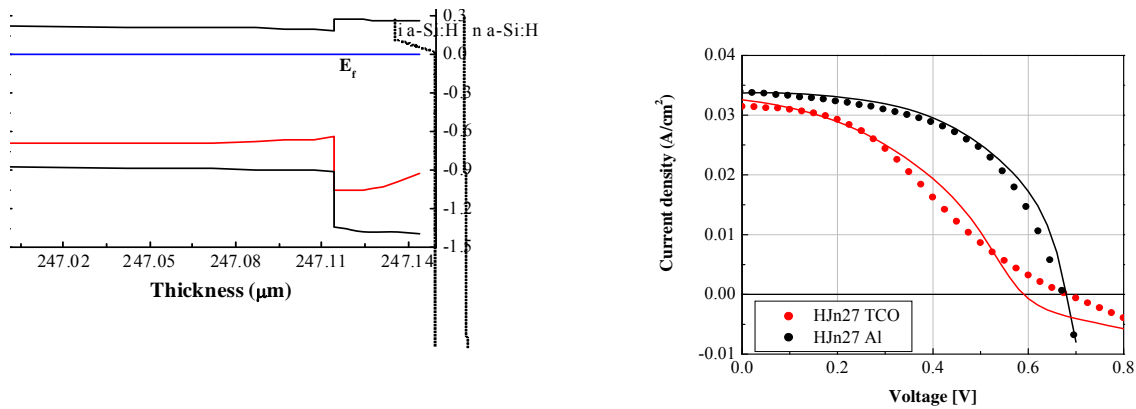
2301 The low conductivity of doped a-Si:H layer has a strong impact on IBC HJ cell. If the
 2302 emitter region is not completely covered by any metal contact, the carriers have to travel
 2303 laterally along the doped a-Si:H film to reach the metal electrode. The longer distance for
 2304 lateral transport introduces resistance loss that results in fill factor reduction, whereas V_{oc} and
 2305 J_{sc} are not affected by the reduction of the metal coverage. Numerical simulations of IBC-
 2306 BHJ device reported in Ref. [349] show that decreasing the coverage ratio from 100% to 50%
 2307 induces an absolute 5% reduction of fill factor, thus reducing the cell efficiency. Therefore
 2308 the whole emitter area has to be contacted by a metal to achieve the best cell performance.
 2309 Concerning the emitter coverage, the use of TCO represents a good choice to improve the
 2310 lateral conductivity of the very low doped a-Si:H layers. This is because CrSi may not be
 2311 sufficient to guarantee a sufficient lateral conduction if the metal contact is narrower than the
 2312 emitter region.

2313 The challenge of TCO patterning without any photolithography processes remains. Up
 2314 to now the most promising technologies are the use of physical shadow mask during the

2315 sputtering process [338, 340] and the laser ablation after TCO deposition [339].

2316 The choice of the electrodes deposited on both contacts represents another relevant
2317 issue. Indeed the electrode work function can affect the doped a-Si:H layer conductivity. In
2318 principle the n-type a-Si:H should be sufficiently thin to avoid series resistance enhancement
2319 and sufficiently doped to avoid depletion induced by the electrode contact due to the work
2320 functions not aligning within the a-Si:H layer. As an example, if the Fermi level assumes a
2321 distance of 4.2eV from the vacuum level to the edge of n-type a-Si:H emitter, work function
2322 of the electrode should not exceed that value to avoid depletion in the a-Si:H layer when in
2323 contact with that electrode, otherwise a Schottky barrier contact arises. This again deforms
2324 the light I-V characteristics introducing a S-shape.

2325 A comparison of band bending distributions at the rear side of the cell is reported in
2326 Fig. 44, as obtained by numerical simulations. Here two different work function values of 4.3
2327 eV (black for Al), and 4.6 eV (Red for TCO) have been applied as rear side metal contact of a
2328 n-c-Si/i-a-Si:H/n-a-Si:H heterostructure, keeping the same doping and density of state
2329 distribution within the n-type a-Si:H layer. The work function were simulated by fixing the
2330 Fermi level at the edge of the n-a-Si:H layer where the metal contact would be. As evident
2331 from Fig. 44, a depletion occurs in both n-type c-Si and a-Si:H that reflects in a barrier
2332 formation for the electrons being collected by the metal contact. This barrier results again in a
2333 S-shape in the light I-V characteristic as reported in Fig. 44 as continuous lines and compared
2334 for two different cells. The metal electrode has been varied from Al (work function = 4.3eV)
2335 to TCO (work function = 4.6eV). Also on the p-type a-Si:H layer an undesired depletion
2336 effect can be obtained if an uncorrected metal work function is chosen.



2337

2338 Fig. 44 Left side: Numerical simulations of band bending distributions of n-c-Si/i-a-Si:H/n-a-Si:H rear side of
 2339 heterojunction solar cell, in which the work function of the metal contact to the n-a-Si:H has been varied from
 2340 4.3 eV (black for Al) to 4.6 eV (red for TCO). Moreover black lines in the band diagram shifted a bit downward
 2341 due to an electron accumulation (inside the barrier) induced by the metal work function. The barrier formation
 2342 results in a S-shape light I-V curve (right side) reported as continuous lines; Right side: Comparison between
 2343 experimental (dots) and numerically simulated (line) I-V characteristics under sun-light illumination of n-c-Si/n-
 2344 a-Si:H rear side of heterojunction solar cell in which the work function of the metal contact to the n-a-Si:H has
 2345 been varied from TCO = 4.6eV (red) to Al = 4.3eV (black).
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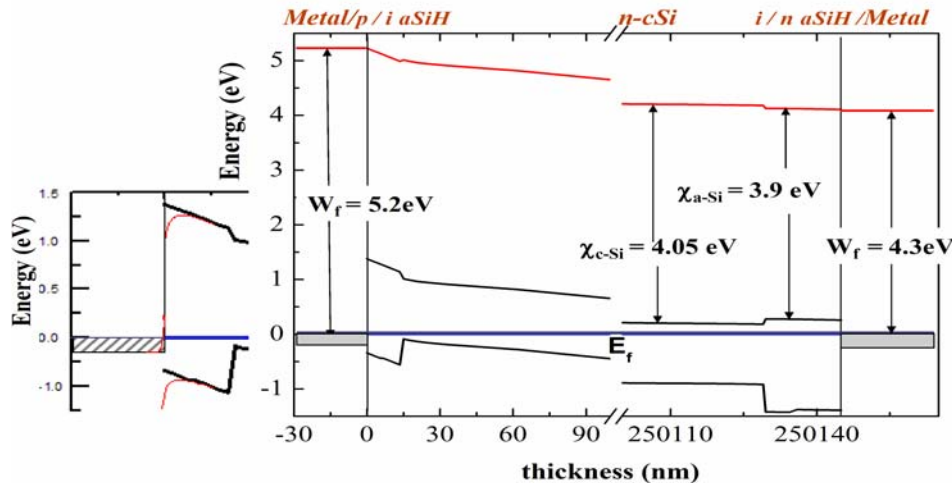
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To reach the highest efficiency, metal work function close to 4.3eV and 5.2eV should be used in case of n- and p-type a-Si:H regions, respectively [346]. According to this approach the built-in voltage of the device also can increase leading to higher V_{oc} values [327]. Band bending simulation of the n-type c-Si based a-Si:H/c-Si heterojunction cell with two different metals work function (5.2eV and 4.3eV) for the emitter and base contact respectively is shown in Fig. 45. This simulation refers to a HJ device able to reach V_{oc} of 760mV and efficiency of 25%. At the left side the band bending at the edge between metal and p-type a-Si:H is magnified to remark the undesired band bending distribution when metal work function lower than 5.2eV is used for the contact.



2356

2357 Fig. 45 Band bending simulation of the n-type c-Si based a-Si:H/c-Si heterojunction cell. This simulation is for
 2358 heterojunction device with V_{oc} and efficiency of 760mV and 25% respectively. Two different metals with work
 2359 function (W_f) of 5.2 eV and 4.3 eV are adopted for the emitter and base contact respectively. These metals have
 2360 the same effect of TCO films from the work function point of view. For small area (lab scale) devices, metal
 2361 work function is not an issue. At the left side, the band bending at the edge between metal and p-type a-Si:H is
 2362 magnified to illustrate the undesired band bending distribution when metal work function lower than 5.2 eV is
 2363 used for the contact. Here, electron affinity and Fermi energy are denoted by E_f and χ respectively.

2364

2365 While at lab scale metal work function does not represent a problem, since different

2366 metals are commonly available and small area samples requires thin layers, the situation

2367 become more complex when production moves to industrial scale. Thicker layer due to large

2368 area device and low-cost metallization processes are needed to be competitive. Towards this,

2369 it is useful to look at the front heterojunction cell manufacturing process where the device

2370 commonly has two TCO for both front and rear side of the cell. TCO layers are usually

2371 obtained by magnetron sputtering, which is a standard technology for large area solar cell.

2372 Even if the TCO is also useful to work as anti-reflection coating, its resistivity around $10^{-4} \Omega$ -

2373 cm is not sufficient to ensure lateral collection without introducing series resistance. Then Ag

2374 metal grids are needed to complete the cell. This metal is commonly using through screen

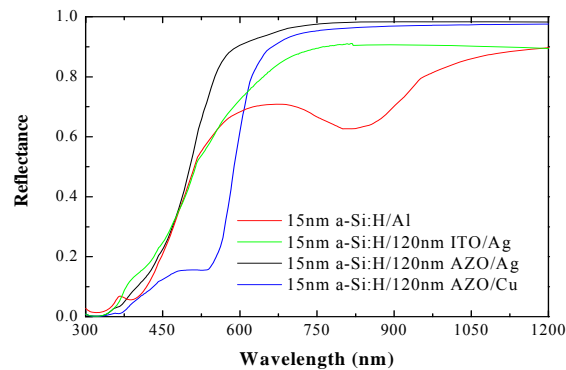
2375 printing process with thermal sintering at temperature below 200°C [346]. This technology

2376 can be applicable also to the IBC-BHJ device due to the low thermal budget required.

2377 Several TCOs such as Al-doped ZnO (ZnO:Al) and ITO can fit the work function

2378 requirements. In particular ITO can offer the possibility to tune the work function depending

2379 on the deposition conditions [356] as well as the amount of indium within the In_2O_3 target of
 2380 the magnetron sputtering system. A 90% In_2O_3 and 10% SnO_2 result in work function of 5.5
 2381 eV and 4.8eV respectively [357]. Moreover in the case of IBC-BHJ device, the TCO
 2382 positioned on the rear side of the cell does not work as anti-reflection coating and thus may
 2383 be thicker leading to a lower sheet resistance. Nevertheless the rear side contact should also
 2384 work as mirror to reflect infrared radiation inward towards the cell, thus enhancing the light
 2385 trapping. ZnO:Al/Ag contact represents a better choice with respect to ITO/Ag or Al . ITO or
 2386 ZnO:Al also represent a good substrate to Cu plating applications to replace the expensive Ag
 2387 layer. In Fig. 46, inward reflectance in the c-Si wafer from different rear side metal contacts
 2388 are compared. All these reflectance curves are obtained using optical simulation software
 2389 [358]. It is interesting to note that 15nm a-Si:H/Al as back contact does not form an optimum
 2390 mirror due to the Al absorption in the wavelength range between 750nm and 1000nm. Cu and
 2391 Ag are seen to behave quite similar as mirror in the near infrared portion of the spectrum
 2392 between 900nm and 1200nm.



2393 Fig. 46 Inward reflectance in the c-Si wafer from different rear side metal contacts. Al is not the best choice due
 2394 to infrared absorption, while Cu and Ag act similar from 900nm to 1200nm. This reflectance is simulated with
 2395 the aid of a numerical model developed in x-ray oriented programs (optical simulation software). Red curve
 2396 shows that back contact formed by 15nm a-Si:H/Al shows an infrared wavelength absorption. Back contact
 2397 should act as mirror, and should reflect infrared wavelength towards bulk. That is, to enhance light trapping,
 2398 rear side contact should reflect infrared radiation towards the bulk of c-Si wafer. ZnO:Al/Ag (i.e. AZO/Ag) is a
 2399 better choice than ITO/Ag or ITO/Al . Also, Cu plating can be done easily over ZnO:Al . Therefore, an expensive
 2400 Ag layer can be replaced easily by Cu .

2402

2403

Contact resistance contributes to series resistance. Contact resistance can be evaluated

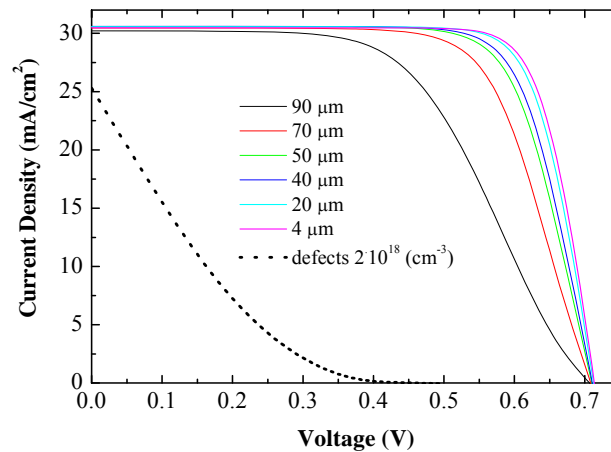
2404 with the aid of two-dimensional (2D) numerical model of the IBC-BHJ cell. To achieve cell
2405 fill factor as high as 83%, a specific contact resistivity of $0.01\Omega\text{-cm}$ for both emitter and BSF
2406 contacts should be obtained. Higher contact resistances of $0.1\Omega\text{-cm}$ and $1\Omega\text{-cm}$ will lead to a
2407 fill factor of 80% and 54%, respectively [349]. Higher values of these parameters induce an
2408 S-shape in the light I-V sun lighted characteristic.

2409 Different metallization approaches have been proposed on a laboratory scale.
2410 According to the previous discussion, industrial production on large area metallization must
2411 fit cell cost and throughput. Since the heterojunction cells can only withstand temperatures
2412 lower than 300°C , screen printing using low-temperature sintering Ag pastes or metal plating
2413 are the only available alternatives. Both these techniques require an interlayer such as TCO
2414 [259] or evaporated metal [333] between the doped a-Si:H film and top metal (i.e. Ag paste)
2415 to fit the work function requirement, and to ensure metal adhesion.

2416 **5.2.5 Distance between doped regions - gap between IBC contacts**

2417 In IBC-BHJ cells the primary fill factor loss is due to lateral current flow. Indeed the
2418 emitter fingers should be much wider than base fingers for efficient minority-carrier
2419 collection; therefore the majority carrier collection is subject to more resistance losses [217].
2420 J_{sc} increases by about 3 mA/cm^2 as the emitter coverage increases from 50% to 95%, because
2421 of the increased area. The same effect is also demonstrated in a back-contacted diffused
2422 junction solar cell [359]. Fill factor increases along with emitter coverage up to a certain
2423 value and then decreases because of the increased series resistance related to the longer travel
2424 of the majority carriers to be collected in the base contact, and to the reduced width of the
2425 base. To better understand this issue several structures have been simulated having different
2426 distance between the two doped a-Si:H contacts. The simulated I-V characteristics in Fig. 47
2427 refer to distance varying between $4\mu\text{m}$ to $90\mu\text{m}$. All the other parameters such as SRV, defect
2428 density at the interface, and doping density of the doped regions have been kept constant. To

2429 achieve the best efficiency the distance between doped contacts should be as short as
 2430 possible. Increasing that distance results in a decrease in fill factor. This effect is due to the
 2431 absence of electric field in crystalline region covered only by the intrinsic a-Si:H layer. The
 2432 photogenerated carriers flowing into these regions cannot escape from c-Si/a-Si:H interface
 2433 recombination. Indeed if the density of states in the i-a-Si:H layer were increased by one
 2434 order of magnitude from $1 \times 10^{17}/\text{cm}^3$, recombination will be stronger and its effect on the I-V
 2435 characteristic will be dramatic, as evident looking at the dotted black characteristic reported
 2436 in the Fig. 47 [338]. In practice it is difficult to obtain a distance between the two doped
 2437 contacts as short as $4 \mu\text{m}$ without any photolithographic process.



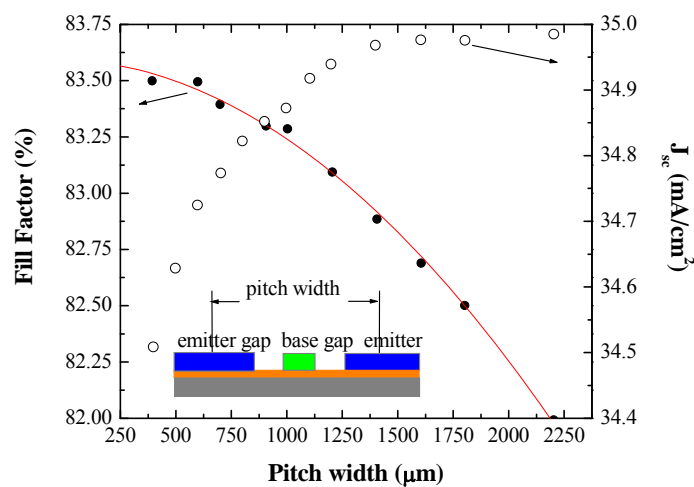
2438

2439 Fig. 47 Influence of gap distance between the emitter and base contacts and the influence of defect density
 2440 within the buffer layer. The simulated I-V characteristics refer to distance varying between $4 \mu\text{m}$ to $90 \mu\text{m}$. All
 2441 the other parameters such as SRV, defect density at the interface and doping density of the doped regions
 2442 have been kept the same for all the simulated distances. To achieve the best efficiency the distance between
 2443 doped contacts should be as short as possible. Increasing that distance, a reduction of fill factor occurs, due to
 2444 the reduction of electric field intensity within crystalline region covered by the intrinsic a-Si:H layer. If the
 2445 density of states in the i-a-Si:H layer is increased to an order of magnitude from $1 \times 10^{17}/\text{cm}^3$, the recombination
 2446 would be stronger and its effect on the I-V characteristic would be dramatic as evident looking at the back
 2447 dotted I-V curve.
 2448

2449 Keeping the gap width fixed at $100 \mu\text{m}$, simulations show that increasing the base
 2450 contact width, the J_{sc} quadratically decreases from $34 \text{ mA}/\text{cm}^2$ at $100 \mu\text{m}$ down to $30 \text{ mA}/\text{cm}^2$
 2451 at $750 \mu\text{m}$ due to recombination at interface n-c-Si/i-a-Si:H/n-a-Si:H, which reduces the
 2452 number of carriers able to reach the emitter region [349].

2453 To better define the rear side geometry of an IBC-BHJ solar cell, a definition of pitch

2454 as the sum of the base, the gaps and the emitter width, is used. Commonly it is in the
 2455 millimetres range. From simulations it is possible to determine the optimum pitch,
 2456 corresponding to the maximum cell efficiency, which is in the range between 600 μm and 900
 2457 μm . This optimum value is determined as a trade-off between emitter coverage and series
 2458 resistance losses due to the increased lateral distances. While the pitch weakly influences the
 2459 J_{sc} that instead strongly depends on SRV, in turn it affects the fill factor as shown in Fig. 48.
 2460 As can be seen in Fig.48, fill factor quadratically decreases as pitch width increases as shown
 2461 by the parabolic red curve fitting the simulation data. These data refer to simulations in which
 2462 the base contact and gap widths were set at 150 μm and 50 μm respectively. J_{sc} data refers to a
 2463 SRV of 50cm/s arising from a front surface field [360]. Instead, Mingirulli et al. [232]
 2464 reported that to achieve the efficiency of 20%, suggests gap, base contact and emitter width
 2465 in the ratio: 12%, 28% and 60% respectively of the pitch.



2466 Fig. 48 Fill factor (line) and J_{sc} (symbols) as a function of pitch width resulting from numerical simulations.
 2467 Continuous red line shows the quadratic behaviour of the fill factor versus pitch width. In the inset, a sketch of
 2468 pitch width definition is shown. In the simulation, base width and gap width were set at 150 μm and 50 μm
 2469 respectively. By increasing pitch width about an order of magnitude from 250 μm , J_{sc} increased slightly, being
 2470 weakly influenced by pitch width. Whereas fill factor decreases quadratically as pitch width increases. J_{sc} data
 2471 corresponds to a surface recombination velocity of 50cm/s. Maximum efficiency corresponds to a pitch width
 2472 between 600 and 900 μm .
 2473

2474

2475 5.2.6 Front surface

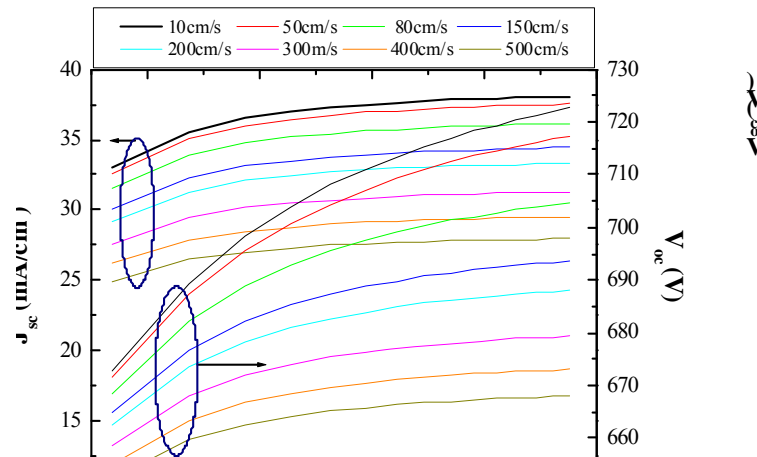
2476 Since the carriers are mostly generated close to the front side of the cell and the

2477 diffusion mechanism toward the back contact is the only way for the collection, the front side
2478 plays a very relevant role in IBC-BHJ cells. An effective front surface passivation is strongly
2479 needed to reduce the SRV, and achieve high-efficiency. From numerical simulations of IBC-
2480 BHJ solar cell, reported in Ref. [360], it is evident that both J_{sc} and V_{oc} are affected by the
2481 front side SRV. In particular, increasing the SRV from 0 to 1000cm/s, the J_{sc} and V_{oc} reduce
2482 from 36mA/cm² to 15mA/cm² and from 760mV to 660mV, respectively, thus reducing the
2483 cell efficiency. The fill factor does not seem to be very strongly influenced. An anti-reflection
2484 coating able to ensure low front SRV can be achieved by SiN passivation, or even more
2485 promising, using a-Si:H/SiN stack double layer [335], or SiO₂/SiN [232]. A front SRV as low
2486 as 10cm/s on p-type was demonstrated in Ref. [213 ,361]. Moreover SiN deposited on front
2487 side of n-type c-Si surface layer can also form a front surface field due to the electron
2488 accumulation induced by the positive charge lying within the SiN film [362].

2489 In principle the use of a front surface field can be very useful to achieve an effective
2490 surface passivation. In Ref. [213] the impact of the front SRV on the QE of IBC cell has been
2491 demonstrated leading to the conclusion that the SRV affects more the cell fabricated on
2492 higher doped c-Si base. As an example, a J_{sc} of 38.5mA/cm² can be achieved for base doping
2493 concentration of 10¹⁴cm⁻³ even in case of SRV = 40000cm/s, whereas the same SRV reduces
2494 the J_{sc} to less than 30mA/cm² for base doping concentrations of above 7x10¹⁵cm⁻³.
2495 Calculations have shown that front surface field on lower base doping results in higher J_{sc} and
2496 reduce the influence of the front SRV [213]. This result is relevant for industrial cell
2497 manufacturing, where good passivation on large areas is still difficult to attain [360]. In
2498 practice it is easier to perform a good passivation on FSF fabricated by light phosphorous
2499 diffusion on n-type c-Si wafer, as suggested in Ref. [232], with respect to light boron
2500 diffusion on p-type c-Si wafer [363]. In turn this approach to the front surface field is in
2501 contrast to the primary goal of achieving a full low-temperature (< 200°C) process able to

2502 reduce the cell manufacturing cost at industrial scale. On the other hand, J_{sc} as high as 38.5
2503 mA/cm^2 have been presented by LG [343] using a n-type a-Si:H/i-a-Si:H front surface field.
2504 In this case, however, an undesired absorption within a-Si:H film occurs that reduces the J_{sc}
2505 of at least $1\text{mA}/\text{cm}^2$. Therefore the use of higher bandgap n-type thin-film to form an
2506 effective front surface field is highly desirable. Doped SiO_x film obtainable by PECVD
2507 process [364] can be a valid solution to overcome the undesired absorption at the front side.

2508 The key issue to obtain high J_{sc} depends not only on SRV but also on diffusion length,
2509 in the bulk c-Si wafer. The effect of both parameters has been explored in Ref. [333], in
2510 which the J_{sc} and V_{oc} of the cell have been simulated by varying the diffusion length and front
2511 side SRV, as depicted in Fig. 49. A numerical model based on PC1D software [365] suggests
2512 that the front side SRV has a greater effect on device performances than diffusion length.
2513 Indeed while a diffusion length of $500\mu\text{m}$ is acceptable to collect the photogenerated carriers
2514 over the entire light spectrum ranging from 350nm to 1200nm, SRV values higher than
2515 $100\text{cm}/\text{s}$ strongly decreases the J_{sc} values, thus reducing the advantage of front metal grid
2516 absence. To obtain high-efficiency solar cell on a p-type $200\mu\text{m}$ thick c-Si wafer, the model
2517 suggests that SRV as low as $10\text{cm}/\text{s}$ and diffusion length around 1 mm are needed to achieve
2518 J_{sc} and V_{oc} values of $38\text{mA}/\text{cm}^2$ and 720mV, respectively. A diffusion length value of 1mm
2519 corresponds to a $300\mu\text{s}$ of bulk lifetime. To obtain the same diffusion length on n-type doped
2520 c-Si wafer, a 1ms bulk lifetime is required [329] because of lower mobility of holes compared
2521 to that of electrons.



2522 Fig. 49 PC1D simulations of J_{sc} and V_{oc} values as a function of diffusion length for different values of front side
 2523 surface recombination velocity. These values are chosen in the range between 10cm/s and 500 cm/s. While the
 2524 former refers to very good Si surface passivation, and the latter refers to a surface passivation commonly
 2525 achieved in the cell production line. Front surface recombination velocity has more influence on device
 2526 performance than diffusion length, and a high J_{sc} depends on these two parameters. To collect photogenerated
 2527 carriers over the spectrum range between 350 and 1200nm, a diffusion length of at least 500 μ m is required.
 2528 When surface recombination velocity >100cm/s, J_{sc} decreases strongly and reducing the advantage of grid-less
 2529 front surface.
 2530

2531

2532 5.2.7 Towards high-efficiency

2533 Currently the highest IBC-BHJ cell efficiency of 25.6% has been demonstrated by
 2534 Panasonic [344]. This result overcomes the 25% efficiency barrier in place for many years in
 2535 a lab device obtained through photolithography steps [366]. It is interesting to note that this
 2536 record has been obtained on very large area device (143.7cm²), and therefore is closer to
 2537 production line than laboratory scale. Moreover this result demonstrated that the IBC-BHJ
 2538 concept is among the most promising approach to achieve the highest efficiency on c-Si
 2539 based solar cell. Since the record cell shows V_{oc} a bit lower than the maximum reached on
 2540 HIT cell [325], there is room to further improve the IBC-BHJ cell.

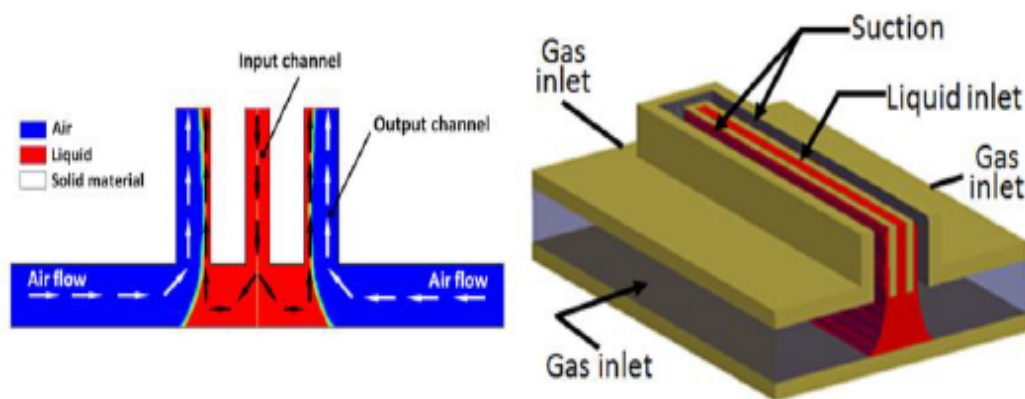
2541 Record efficiency higher than 25% can be achieved if the cell fill factor will reach a
 2542 value of 83%, as obtainable reducing the cell pitch and the contact resistance between metal
 2543 electrodes and a-Si:H layers. But if the IBC-BHJ cell achieves fill factor values lower than
 2544 83% then the cell V_{oc} must be enhanced to compensate for the lower fill factor. Even though

2545 V_{oc} value as high as 750 mV has been recently demonstrated by Sanyo-Panasonic on
2546 conventional transverse heterojunction cell, the same V_{oc} seems not easy to achieve due to
2547 difficulties in performing a surface passivation of the gap between the two contacts able to
2548 nullify the SRV.

2549 **5.3 Future direction**

2550 The way to reduce the Si based solar cell cost and then the PV market price is
2551 represented by thickness reduction of Si wafer down to 100 μ m. On this thin wafer, low
2552 thermal budget technologies should be applicable to avoid wafer warping due to thermal
2553 stress. Si heterojunction device represents a valid choice as already demonstrated by Sanyo-
2554 Panasonic even on thin wafer [367]. Nevertheless Si heterojunction technology has three
2555 important unresolved issues. The first is the use of ITO, which is not available for very large
2556 cell production due to the presence of rare indium. The second is the Ag screen-printed pastes
2557 for the electrodes; indeed Ag cost has not been reducing as the rest of the cell, and accounts
2558 for about 30% of the total cell cost [368]. The third is the connection between cells within the
2559 module now ensured by conductive tape that introduced large series resistance. IBC-BHJ cell
2560 represents a potential solution for these issues. ITO can be potentially successfully replaced
2561 by ZnO:Al since the lateral conductivity is not an issue due to subsequent metallization. In
2562 order to reduce the cell cost, the Ag screen-printed contacts must be replaced by Cu plating.
2563 With respect to conventional solar cells, in which the front side grid shrinks to dimensions
2564 lower than 80 μ m to reduce the shadowing effect and material cost, the IBC device has lower
2565 geometrical constraints. Therefore the use of metal plating, in principle, should be easier to
2566 manage. But the adhesion of plated Cu still represents an issue that can be overcome by
2567 interlayer insertion such as nickel (Ni) or tin (Sn). Moreover the large amount of chemicals
2568 waste produced by the metal plating baths still represents environmental and cost concerns
2569 for the industry. To overcome this problem an innovative solution has been recently proposed

2570 in Ref. [369]. It is based on locally plating by dynamic liquid meniscus formation, as depicted
 2571 in Fig. 50. With the aid of this meniscus all the wet chemical technologies can be performed,
 2572 such as local plating, etching and deposition from liquid phase. Since the liquid meniscus is
 2573 only locally in touch with the wafer, it can be used to deposit Cu or other metals only where
 2574 there is a specific necessity, thus strongly reducing the waste chemicals produced by
 2575 conventional light induced plating systems [370]. With the aid of this new approach the metal
 2576 contact of the IBC-BHJ may potentially not represent an issue [369]. The problem related to
 2577 low fill factor of PV module due to the cell interconnection, conventionally made by
 2578 conductive tape between the heterojunction within the module, can be easily overcome in
 2579 IBC cell.



2580
 2581
 2582 Fig. 50 Schematic diagram of dynamic liquid meniscus formation in touch with the substrate. From the pictures
 2583 it is evident that the red fluid flowing from the center inlet is recalled back through suction at the left and right
 2584 outlet. Therefore the fluid in contact with the substrate is always refreshed. With the aid of this meniscus all the
 2585 wet chemical technologies can be performed, such as local plating, etching and deposition from liquid phase.
 2586 Since the liquid meniscus is only locally in touch with the substrate, it can be used to deposit Cu or other metals
 2587 only where there is a specific necessity, thus strongly reduce the waste chemicals always produced by
 2588 conventional light induced plating systems. With this new approach, an issue related to low fill factor of PV
 2589 module can easily be solved.

2590
 2591 The design of module can be completely rewritten taking into account that both
 2592 contacts are now on the same side of the cell. Therefore the IBC cells can potentially be done
 2593 on a low-cost printed circuit board, instead of a conventional mylar sheet, where two
 2594 interdigitated comb shape metal strips can ensure larger contact area between cells and

2595 interconnections with respect to conventional ribbons. This can enhance the cell fill factor
2596 and the overall module efficiency.

2597 **6.0 III-V multi-junction on c-Si**

2598 Significant effort has been undertaken till date to reduce the cost of multi-junction
2599 solar cell (MJSC) technology by developing methods to manufacture them on low-cost
2600 wafers. The integration of III-V semiconductors on c-Si aims to improve efficiency and to
2601 solve the limitations encountered with other wafers such as germanium (Ge) or gallium
2602 arsenide (GaAs).

2603 This review section focuses on the most relevant work done in the last years on the
2604 integration of III-V semiconductors on c-Si for the manufacture of multi-junction solar cells.
2605 Current state-of-the-art of the two most important techniques (epitaxial growth and wafer
2606 bonding) used for such integration are discussed. In addition to highlighting the most novel
2607 results obtained with each technology, current challenges and possible strategies to overcome
2608 them are also pointed out.

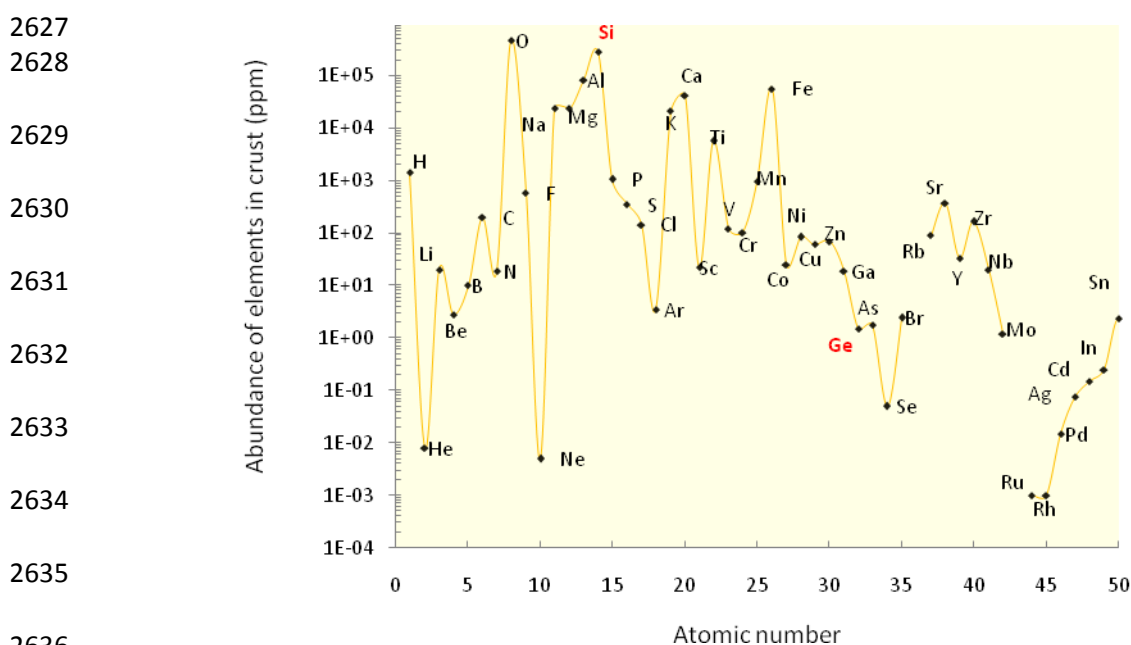
2609 **6.1 Introduction**

2610 MJSCs have demonstrated significant potential to reduce the cost and increase solar
2611 cell efficiency. Concentrator PV systems based on multi-junction solar cells boosts electricity
2612 generation and are expected to reduce the cost of PV.

2613 The first key for the success of this technology lies in the ability to make affordable
2614 PV cells with very high-efficiency. Using concentration, the maximum conversion efficiency
2615 that can be achieved by a PV device with a single p-n junction on c-Si is 44% [371] for cells
2616 made from a material with an optimal bandgap ($E_g \sim 1.3$ eV). MJSCs are formed by stacks of
2617 several p-n junctions connected in series, each of which is intended to transform a portion of
2618 the solar spectrum into electrical energy with minimum losses. The ultimate efficiency of

2619 MJSC with an infinite number of junctions is 86% [371], almost twice of that of cells with a
 2620 single-junction. The second key factor for its success lies in the existence of a family of
 2621 materials, namely III-V semiconductors, with excellent PV properties and ranges of suitable
 2622 bandgaps to implement MJSCs.

2623 The integration of III-V semiconductors on Ge has been successfully investigated in
 2624 the last two decades. A MJSC on Ge has recently beaten the efficiency record for any PV
 2625 device, achieving efficiency close to 42% [372]. However, the exploration of alternative
 2626 wafers to Ge continues because of the shortage and relatively high costs of Ge.



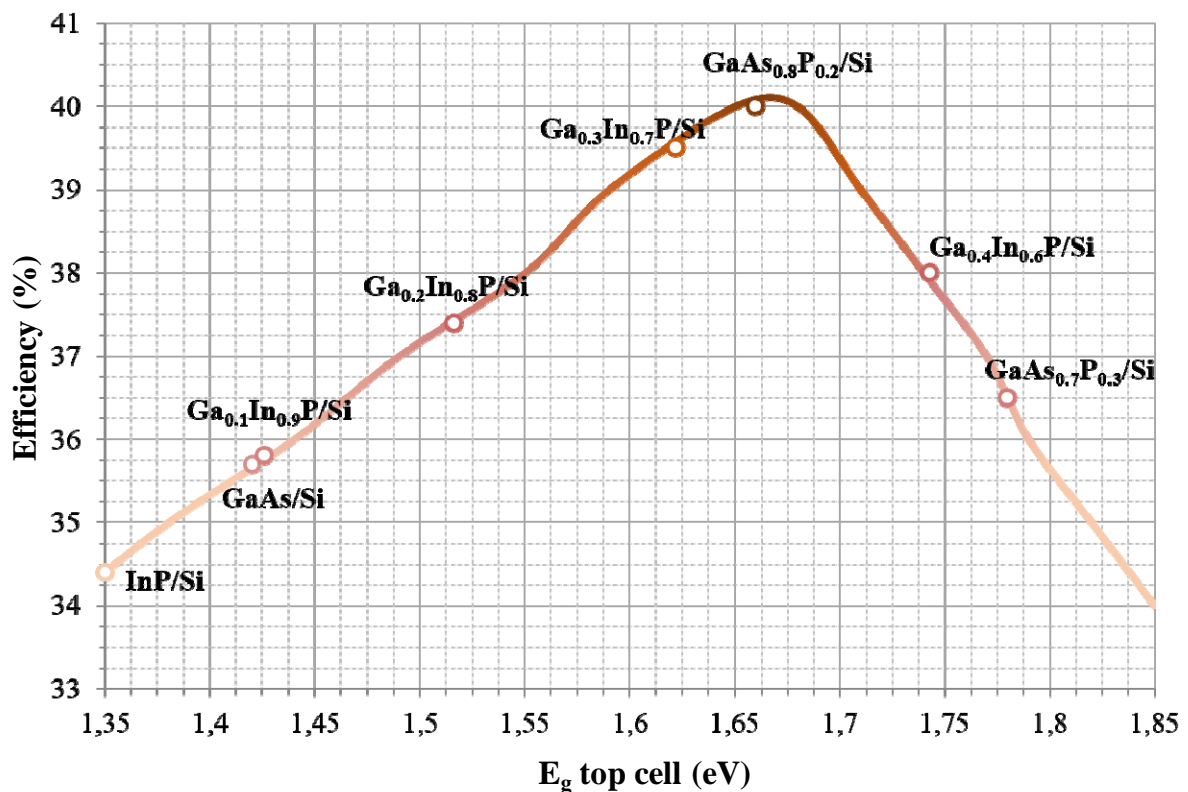
2637 Fig. 51 Abundance of some elements in the Earth's crust versus atomic number. The graph evidences the
 2638 abundance difference existing between the Si and Ge (highlighted in red) in the Earth's crust. Si is more
 2639 abundant than Ge by a factor of 2×10^5 . This difference turns into a big discrepancy in terms of the material cost
 2640 and thus, the selection of Si as an alternative to Ge is clearly justified. Also, semiconductor devices are
 2641 fabricated using Si, a unique electronic and PV material. An ideal candidate for multi-junction solar cells is Si.
 2642 Data taken from [373], David R. Lide, ed., CRC Handbook of Chemistry and Physics, 85th Ed., CRC Press,
 2643 Boca Raton, Fla., Taylor & Francis Group, 2005.

2644 Figure 51 represents a plot of the abundance of some elements [373] in the Earth's
 2645 crust versus their atomic number. This plot shows that Si is a factor of $\sim 2 \times 10^5$ times more
 2646 abundant than Ge in the Earth's crust. Accordingly, the ideal candidate on which to
 2647 manufacture multi-junction solar cells is c-Si (Fig. 51), the ubiquitous electronic and PV

2648 material. Indeed about 95% of semiconductor devices are presently fabricated using c-Si
2649 [374].

2650 According to the iso-efficiency contour maps for concentrated light depicted by
2651 Wanlass et al. [375] for a double-junction solar cell, theoretical efficiencies between 34 and
2652 40% can be achieved with a c-Si bottom cell if an appropriate material with bandgap ranging
2653 from 1.34eV to 1.84eV is used for the top cell. Figure 52 makes evident that there is a wide
2654 variety of III-V materials that meet this requirement. Hence the challenge is to develop
2655 strategies to grow them with good PV quality on a c-Si wafer, which in turn has to be
2656 processed to obtain an equally good performing bottom cell.

2657



2658 Fig. 52 Theoretical efficiency of double-junction solar cells grown on c-Si wafer as a function of top cell
2659 bandgap. For top cell, an appropriate material is required with bandgap ranging between 1.34 and 1.84eV.
2660 According to this graph, the maximum theoretical efficiency can be obtained for III-V/c-Si double-junction solar
2661 cell by using gallium arsenide phosphide (GaAsP) as top cell with arsenic content of 0.8%. This GaAsP/c-Si
2662 couple has an excellent bandgap combination for maximum utilization solar spectrum. Data from [375],
2663

2664 Wanlass M W, Coutts T J, Ward J S, Emery K A, Gessert T A, Osterwald C R., Advanced high-efficiency
2665 concentrator double-junction solar cells, Proc. 22nd IEEE PVSC (Alaska) 1991.

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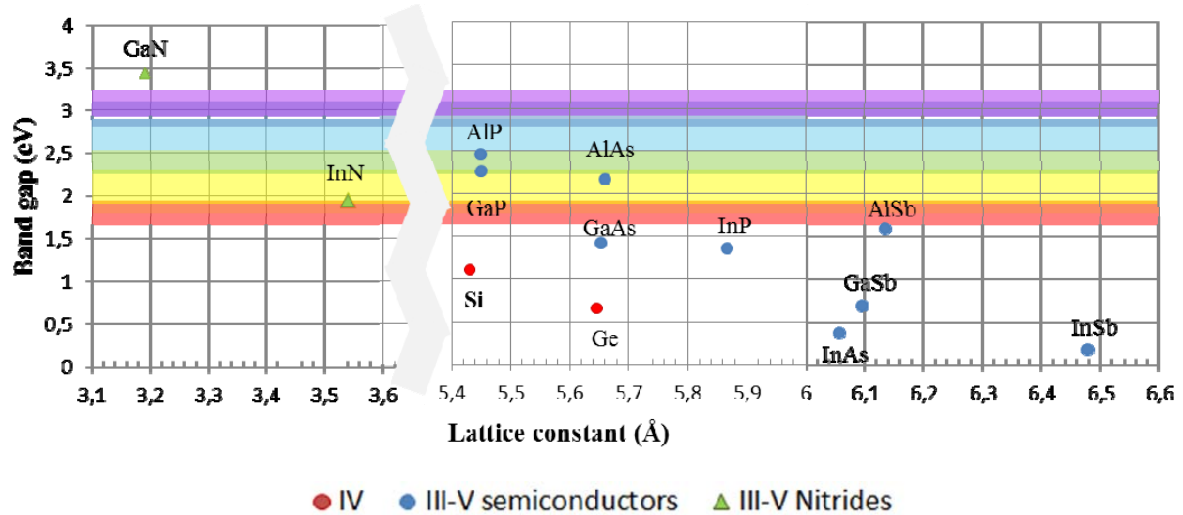
2668 **6.2 Challenges and difficulties**

2669 The integration of III-V semiconductors on c-Si has been a long-sought desire by the
2670 microelectronic industry [374,376]. In the PV field, the integration of III-V compounds on c-
2671 Si was intensively investigated in the 1990s, achieving good results [377-379]. Here, it is
2672 worth mentioning the works reported by Fitzgerald's group at the Massachusetts Institute of
2673 Technology, U.S.A., Umeno's group at the Nagoya Institute of Technology, Japan. All these
2674 groups demonstrated the production of solar cells with efficiencies above 20% by following a
2675 variety of approaches. Despite the excellent results published for an AlGaAs/c-Si solar cell
2676 with a V_{oc} of 1.57 eV, J_{sc} of 23.6mA/cm² and efficiency up to 20% [380], the technology was
2677 not transferred to industry, possibly due to reproducibility issues or complexity in the
2678 process.

2679 In spite of these excellent results, the intensity of research declined considerably
2680 during the late 1990's due to the difficulties in improving material quality, and the rapid
2681 progress of Ge based MJSC technology. The above groups pointed out that the main
2682 challenges for III-V heteroepitaxy on c-Si are: (i) lattice mismatch, (ii) mismatch in thermal
2683 parameters, and (iii) defect confinement. In the following sub-sections, we review each of
2684 these challenges in detail.

2685 **6.2.1 Lattice mismatch**

2686 The obvious problem for III-V heteroepitaxy on c-Si has been the lattice mismatch
2687 between epilayer and wafer (Fig.53). For instance, the lattice constants of c-Si and GaAs– the
2688 two materials whose integration has been long sought, differ by around 4%.



2689

2690 Fig.53 Room temperature bandgap versus lattice constant of common elemental and binary compound
 2691 semiconductors. Lattice mismatch is an issue between epilayer (III-V, for example GaAs) and c-Si wafer. This
 2692 plot evidences the lattice mismatch between gallium arsenide (GaAs) and c-Si, and a small difference between
 2693 gallium phosphide (GaP) and c-Si lattice constants. Lattice mismatch between GaAs and c-Si is around 4%.
 2694 Epitaxial growth can accommodate lattice mismatched materials either by growing strained material or by
 2695 growing material relaxed to its lattice constant. Multi-colored band in the figure is the energy range
 2696 corresponding to visible spectrum.

2697

2698 Therefore, the development of strategies for epitaxial growth, which can accommodate
 2699 this difference, has received special attention. These strategies consider either growing the
 2700 material compressed/strained (i.e. pseudomorphic material) [381,382], or by growing the
 2701 material relaxed to its natural lattice constant (i.e. metamorphic material) [383-387].

2702 6.2.2 Mismatch in thermal parameters

2703

2704 One of the major problems for the growth of III-V materials on c-Si has been
 2705 managing the different thermal properties of both materials [374]. Indeed, the problem of
 2706 heteroepitaxy is not epitaxial growth itself, which is performed at high temperature, but the
 2707 subsequent cooling of the samples. When samples are still at high temperature, their quality
 2708 can be made excellent, despite the lattice mismatch. During the cool-down process, different
 2709 thermal stresses in the sample generate dislocations, other crystalline defects or even cracks
 2710 in extreme cases. To solve these issues, several efforts, such as lowering the growth
 2711 temperature without losing quality in the samples, have been explored to develop epitaxial
 2712 routines that produce lower thermal stress.

2713 **6.2.3 Defect confinement**

2714 Most crystalline defects, originating during the III-V/c-Si integration, occur at the
2715 hetero-interface. However, they can propagate vertically and eventually reach active layers of
2716 the solar cell, producing a degradation of its properties [374,388,389]. Therefore, the
2717 development of epitaxial growth procedures that favor the annihilation or the confinement of
2718 crystal defects in parts of the structure far from the active layers of the solar cell have been
2719 recently pursued.

2720 **6.3 Approaches for PV integration**

2721 Interest in the integration of III-V materials on c-Si has re-emerged lately in the PV
2722 research community [374, 386, 387, 390-394]. Currently, the most developed technique for
2723 such integration is the direct epitaxial growth of III-V compound on c-Si, due to reasonable
2724 scientific understanding of the processes involved in the heteroepitaxy. However, the search
2725 for alternatives has continued. In particular, wafer-bonding technique has received special
2726 attention by demonstrating promising results based on its ability to solve the limitations of
2727 epitaxial growth.

2728 Here we review both techniques by describing their state-of-the-art, emphasizing the
2729 most novel results obtained with each technology, pointing out current challenges, and
2730 possible strategies to overcome them. Finally, the limiting factors and hurdles for efficiency
2731 improvements in each technology are also presented.

2732 **6.3.1 III-V on c-Si epitaxy**

2733 As we have mentioned before, the interest in III-V on c-Si integration, and
2734 particularly the III-V/c-Si epitaxy, has experienced a breakthrough over the last few years.
2735 The reasons for this are based on the progress in understanding the heteroepitaxy process of
2736 III-V semiconductors on c-Si [376]. Moreover, a new generation of metal organic vapor
2737 phase epitaxy (MOVPE) reactors has been developed, and metalorganic precursors adapted

2738 for the growth at low-temperature are readily available. As mentioned above, the use of lower
2739 growth temperature provides more opportunities to handle thermal stress associated with
2740 heteroepitaxy. Finally, the adaptation of new techniques (i.e. strategies to overcome the
2741 defect confinement) to c-Si wafers applied to the metamorphic growth of the InGaAs/Ge has
2742 also contributed to this progress [395].

2743 Despite the wide variety of III-V compounds (Fig. 53), only a few of them are suitable for
2744 direct integration on c-Si wafers. On the one hand, the materials have to be selected in a way
2745 that the bandgap combination (bottom and top cell) is optimum for harnessing the solar
2746 spectrum. On the other hand, the lattice mismatch between both materials has to be
2747 minimized for reducing the formation of structural defects. Unfortunately, only a very small
2748 number of III-V compounds meet both requirements. Thus, two different approaches are
2749 generally used for handling the epitaxial integration of III-V on c-Si: (i) the lattice
2750 mismatched (or metamorphic), and (ii) the lattice matched approach.

2751 **(i) Lattice mismatched approach**

2752 A metamorphic material is the one that grows on a wafer with a different lattice
2753 constant in a way that promotes its relaxation (i.e. its transition to its own lattice parameter)
2754 mainly through the occurrence of misfit and threading dislocations at the interface.
2755 Accordingly, the lattice mismatch approach consists of integrating two materials with a
2756 different lattice constant, in a way that its accommodation is achieved by the generation of
2757 structural defects at the heterointerface. If the propagation of threading dislocations is
2758 minimized and the relaxation process is completed, then the resulting top surface has the
2759 desired lattice constant and a good crystalline quality (this is known as virtual wafer).

2760 Under this approach, III-V materials that can be integrated on c-Si are relatively are
2761 larger, since lattice matching is no longer a requirement. Hence, III-V candidates are selected
2762 to offer an optimum combination of bandgaps when integrating on a c-Si bottom cell. Two

2763 compounds, viz. GaAs and GaAsP, are generally used for achieving high quality
2764 metamorphic III-V/c-Si double-junction solar cells (Fig. 52).

2765 GaAs/c-Si: The integration of GaAs on c-Si wafer consists of direct growth
2766 (monolithic) of the III-V material on the wafer [374, 396]. The bandgap of the GaAs makes it
2767 very attractive for top cell (middle cell) in double-junction solar cell (triple-junction solar
2768 cell), as depicted in Fig. 52. However, as mentioned in Sec. 6.2, several problems exist for
2769 obtaining a defect-free and high quality GaAs/c-Si structure [397-400]. First, the growth of a
2770 polar on a non-polar semiconductor leads to the formation of a high density of antiphase
2771 domains (APDs) which should be controlled for a high quality structure. Work has been done
2772 for minimizing the formation and propagation of these defects [397,401]. Another problem
2773 found during the direct growth of GaAs on c-Si was related to the existing difference in their
2774 lattice parameter (Fig. 53). This difference promotes the generation of misfit dislocations at
2775 the GaAs/c-Si interface and threading dislocations, which can potentially propagate through
2776 the whole structure, and degrade the quality of the solar cell. Finally, the difference in
2777 thermal expansion co-efficients will not only favor the formation of dislocations, but also will
2778 promote the appearance of cracks during the cool down phase in the GaAs layer [397].

2779 Different approaches intended to seal off these limitations have been used [398-400,
2780 402-404]. As an example, the use of III-V intermediate layers based on compositionally
2781 graded buffers, together with thermal cycle annealing [398-400], and the use of lower
2782 temperature for the first few nanometers of the growth [399,402] were implemented for
2783 decreasing the dislocation density. The use of these techniques has brought the dislocation
2784 density from 10^9 - 10^{10} cm⁻², for direct GaAs on c-Si, down to 10^7 cm⁻², which is equivalent to
2785 1-4 ns in terms of minority-carrier lifetime in n-GaAs [405]. However, to produce high-
2786 efficiency III-V top cells, these lifetime values are still low [403,404]. In fact, a low V_{oc} of

2787 ~900mV under AM0 conditions for single-junction GaAs cells on inactive c-Si wafers was
2788 measured in those cells [391].

2789 The above mentioned incompatibilities make it very difficult to achieve a high quality
2790 GaAs/c-Si monolithic device. Hence, another alternative was considered for such integration.
2791 This approach consists of modifying the lattice constant of the c-Si wafer through the use of
2792 group-IV buffer layers. The most developed method so far is the use of a $\text{Ge}_x\text{Si}_{1-x}$ /c-Si virtual
2793 wafer [386,391,406-408]. The SiGe is an intermediate layer aimed to modify the Si lattice
2794 constant by increasing the Ge content during the epitaxial growth. Therefore, the lattice
2795 constant can be increased from 5.43Å (Si) to 5.64Å (Ge), and provide a new template with a
2796 lattice constant closer to the one of GaAs (5.65 Å). However, during the relaxation process,
2797 some misfit dislocations are generated. Some of them can eventually fold up and turn into
2798 threading dislocations, which degrade the device performance [406].

2799 Despite the limitations of this technique, promising results were obtained for GaAs solar
2800 cells grown on SiGe/Ge wafers. Recently, dislocation densities as low as $8 \times 10^5 \text{cm}^{-2}$ within
2801 the relaxed GaAs layer were obtained using Si/Ge wafers for III-V/c-Si integration. This
2802 value corresponds to a minority-carrier lifetime of 10ns for n-type GaAs. To the authors'
2803 knowledge, this is the highest value reported so far for GaAs grown on c-Si [409], resulting
2804 in efficiencies higher than 18% for single-junction GaAs solar cells on c-Si wafers [383,409].

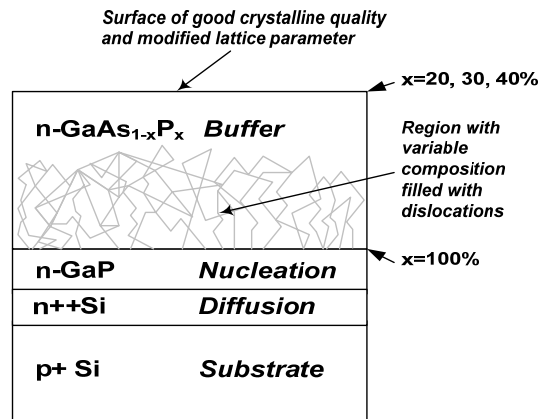
2805 Promising results have been reported recently on MJSCs based on SiGe wafers
2806 [386,391,406-408]. High quality indium gallium phosphide (InGaP)/GaAs double-junction
2807 solar cells have been successfully grown on c-Si wafer through the use of Ge virtual wafers
2808 with SiGe step-graded buffers [386] achieving V_{oc} of 2.2V and an efficiency of 15.3 % for
2809 AM0 conditions [386, 410]. A InGaP/GaAs/SiGe triple-junction solar cell with an efficiency
2810 of 20% under AM0 (1 sun) illumination, and an open circuit voltage higher than 2.6V has
2811 been recently reported [411]. Wang et al. [412] have recently reported a GaAsP/SiGe double-

2812 junction solar cell with an improved bottom cell structure, within a current matching
2813 scenario, with efficiencies up to 20.6% using 1 sun illumination. This work proposes the use
2814 of light trapping techniques and a further optimization of the bottom cell for maximizing the
2815 device performance.

2816 GaAsP/c-Si solar cell: As it has been described before, in the metamorphic approach,
2817 materials are selected to offer an optimum combination of bandgaps. In this respect, the
2818 maximum theoretical efficiency of 40% has been obtained for a III-V/c-Si double-junction
2819 solar cell with top cell material bandgap of 1.66 eV (Fig.52). This ideal material can be
2820 obtained by adding arsenic to GaP to produce $\text{GaAs}_{1-x}\text{P}_x$ (or simply GaAsP). In particular, the
2821 optimum composition (see Fig. 52) is a GaAsP alloy with 80% arsenic and 20% phosphorus
2822 in the group-V sublattice (i.e. $\text{GaAs}_{0.8}\text{P}_{0.2}$).

2823 Due to the mismatch between top and bottom cell materials, the integration of GaAsP
2824 on c-Si is performed through the creation of a virtual wafer, which takes care of the lattice
2825 constant transition and the defect confinement [413, 414]. Therefore, the resulting top surface
2826 has the desired lattice constant and a good crystalline quality, in which the GaAsP top cell
2827 could be easily integrated.

2828 The virtual wafer consists of an initial III-V layer lattice matched to c-Si to obtain a
2829 defect-free III-V template and addresses the problems related to the growth of a polar on a
2830 non-polar c-Si wafer [415-418]. The ideal material for this is GaP since it has a lattice
2831 constant reasonably close to that of Si (Fig. 53). After this step, the growth of a GaAsP
2832 graded buffer layer is included on top of the nucleation layer to handle the lattice parameter
2833 transition from Si to GaAsP and confinement of threading/misfit dislocations (Fig. 54).



2834

2835 Fig. 54 Schematic diagram for the metamorphic integration of gallium arsenide phosphide (GaAsP) on c-Si
 2836 wafer. This process involves the growth of polar material (gallium phosphide GaP) on non-polar wafer (c-Si)
 2837 which results poor morphological quality (i.e. non-homogeneous nucleation layer/isolated islands). To ensure
 2838 high morphological quality, layer-by-layer growth is required for the integration of GaP over c-Si. GaP acts as
 2839 virtual wafer. The integration of GaAsP over c-Si is performed through the virtual wafer. The virtual wafer takes
 2840 care of lattice constant transition (from Si to GaAsP). Therefore, GaP is grown over c-Si since GaP has lattice
 2841 constant close to Si. GaAsP graded buffer is grown on top of a GaP nucleation layer for accommodating the
 2842 lattice mismatch between the top and the bottom subcell materials (i.e. p⁺-c-Si and GaAsP).
 2843

2844 While GaP has been reported to be the most ideal candidate for the nucleation layer,
 2845 the growth of GaP on c-Si presents some limitations, mainly due to the growth of a polar
 2846 (GaP) on a non-polar c-Si wafer [415-418]. In fact, the growth of a polar on a non-polar
 2847 wafer has been reported to favor a non-homogeneous nucleation layer, formed by isolated
 2848 islands, typical from a three-dimensional (3D) growth [419-421]. Moreover, the important
 2849 thermal expansion co-efficient mismatch [417] (the one for GaP is 2.3 times larger than that
 2850 of Si) hinders this integration. In general, a layer-by-layer growth is pursued for the
 2851 integration of GaP on c-Si wafers to guarantee a high morphological quality of the nucleation
 2852 layer. Moreover, wafers must be properly treated before nucleation (i.e. single domain
 2853 structure formed by double steps in the absence of silicon oxide) for minimizing the
 2854 appearance of planar defects, which otherwise, might ruin the electrical behavior of the solar
 2855 cell; and for obtaining a defect-free template for the integration of the GaAsP graded buffer.

2856 In spite of the significant amount of effort that has been done to find the best
 2857 conditions for obtaining a continuous, defect-free GaP surface, this topic remains an open
 2858 issue. The beneficial effect of low-temperature nucleation on obtaining a high quality and

2859 defect-free surface has been reported [422, 423]. On the other hand, Ref.[388, 424] support
2860 the idea of using high nucleation temperatures, together with very high V/III ratios to obtain a
2861 smooth and APD-free structure [388, 424]. In any of those cases, a defect-free GaP layer has
2862 been successfully grown on vicinal $\langle 100 \rangle$ c-Si wafers. The resulting GaP/c-Si virtual wafers
2863 serve as templates for further III-V integration.

2864 Going from GaP to GaAsP involves a significant increase in the lattice constant that,
2865 if not addressed properly, will produce a high concentration of dislocations and crystal
2866 defects that will ruin the PV performance [384,387]. In this case, a metamorphic GaAsP
2867 buffer layer, with variable arsenic content, is grown on the GaP nucleation layer (Fig. 54).
2868 The purpose of the buffer layer is to make an optimal transition between the nucleation layer
2869 and the layer with the composition needed for the top subcell (ideally GaAs_{0.8}P_{0.2}, in this
2870 case). This layer will absorb/avoid the propagation or will even annihilate crystal defects that
2871 will be generated when the gradual change of the lattice constant (i.e. the composition) occurs
2872 during growth. In other words, the goal of the buffer layer is to create a III-V virtual wafer of
2873 high crystalline quality with a different lattice constant than that of the Si that supports it.
2874 Eventually, this virtual wafer will serve as template where GaAsP top cells of the adequate
2875 bandgap can be integrated, thus forming a GaAsP/c-Si double-junction solar cell (Fig. 55a)
2876 with a high theoretical efficiency (Fig. 52).

2877 The development of metamorphic GaAsP/c-Si solar cells has received special
2878 attention over the years. Several research groups [377, 384, 385, 425, 426] have been
2879 working on the development of the structure depicted in Fig. 55a. Their efforts have been
2880 mostly directed towards the optimization of key steps in the epitaxial growth of III-V
2881 compounds on c-Si, such as nucleation layer, graded buffer, and top subcell. The main target
2882 has been the minimization and confinement of crystal defects in the structure. Consequently,

2883 high structural quality graded buffers and promising results in the reduction of the dislocation
 2884 density and annihilation of APD have been reported [384, 388, 390].

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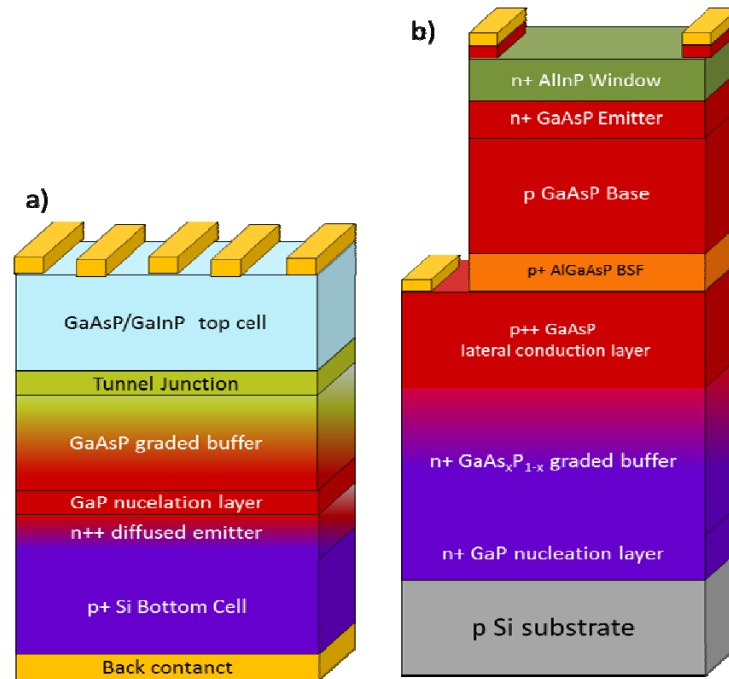
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2895 Fig. 55 (a) Ideal GaAsP/c-Si (or GaInP/c-Si) double-junction solar cell structure based on the metamorphic
 2896 approach. The accommodation of the lattice mismatch is handled through the growth of a GaAsP graded buffer
 2897 layer. The simplification of this structure turns into a single-junction GaAsP solar cell grown on top of an
 2898 inactive c-Si wafer, as depicted in (b). When c-Si wafer acts as template (inactive wafer), technical challenges
 2899 associated between the formation of c-Si bottom subcell and the subsequent formation of the tunnel junction can
 2900 be avoided. Therefore, III-V subcell optimization can be done easily. Data for the latter from [427], Grassman T
 2901 J, Carlin J A, Ratcliff C, Chmielewski D J, Ringel S A., Epitaxially-grown metamorphic GaAsP/c-Si double-
 2902 junction solar cells, 39th IEEE PV Specialist Conf. (Florida) 2013, pp. 0149-0153.

2903

2904 However, there are still some key parts of the structure which have not received
 2905 enough attention in the past, and those optimization is crucial for obtaining high quality
 2906 double-junction solar cell.

2907 The first key point is the formation of c-Si bottom subcell with an optimum emitter (in
 2908 terms of doping and thickness) and maintaining low roughness over the c-Si surface for
 2909 subsequent epitaxial growth. Although an important progress on the optimization of bottom
 2910 cell has been reported recently [428], most groups so far used c-Si wafer as a mere template
 2911 (i.e. inactive wafer) and did not work on bottom cell optimization [377,384,385,387,390].

2912 This alternative (i.e. c-Si as inactive wafer) simply avoids the problems associated between

2913 the formation of the c-Si bottom subcell and the subsequent growth of the tunnel junction
2914 since c-Si wafer only acts as mechanical support and crystallographic template for the
2915 structure. In this way, the optimization of the III-V subcell can proceed independently and a
2916 lateral conduction layer is often included in the III-V solar cell [427] to ease the formation of
2917 rear contact (Fig. 55b). Both top and bottom contacts are formed on III-V layers. Promising
2918 results on obtaining a high-efficiency single-junction GaAsP grown on an inactive wafer has
2919 been reported so far. Lang et al. presented n⁺/p-GaAsP/c-Si solar cell with V_{oc} of 1.10V
2920 [385]. Furthermore, Grassman et al. [384] reported promising light I–V (V_{oc} = 1.04V, J_{sc} =
2921 13.1mA/cm²) and EQE results for a GaAsP/c-Si single-junction prototype solar cell. The idea
2922 is that these structures could be eventually integrated on optimized c-Si bottom subcells for
2923 obtaining high quality GaAsP/c-Si double-junction solar cell.

2924 The second key point is the formation of a tunnel junction to electrically connect the
2925 bottom and the top cell. The aim is to introduce highly doped (>10¹⁹/cm³) layers of a GaAsP
2926 homostructure [429] or a GaInP/GaAsP heterostructure. Latter is preferred since it has been
2927 recently demonstrated that its use reduces optical losses [426]. Preliminary work has been
2928 performed in this area, and promising results were obtained for c-Si based MJSC [426].
2929 However, still some work [429] has to be done to refine the structure and to reduce optical
2930 absorption of the tunnel junction.

2931 Although a great deal of work has to be still done for achieving high quality III-V on
2932 c-Si double-junction solar cell, a prototype of a GaAsP/c-Si double-junction solar cell
2933 [425,427] has recently been reported. This structure has been epitaxially grown by combining
2934 the use of molecular beam epitaxy (MBE) and metal organic chemical vapor deposition
2935 (MOCVD) reactors. The success of this prototype lies in the use of an optimized (i.e. defect-
2936 free) GaP nucleation layer, which acts as a template for a high quality GaAsP metamorphic

2937 graded buffer. Interesting results were obtained in this case, demonstrating the operation of a
2938 double-junction solar cell, with V_{oc} of 1.62V and J_{sc} of 11.0mA/cm² [425].

2939 Though interesting results reported [425,427] for as-grown tunnel junction test
2940 structure (i.e. peak tunneling current densities of 3A/cm²), its integration on the double-
2941 junction structure degrades its properties as a result of its exposure to high temperatures
2942 during the top cell growth. Thus, it limits the electrical behavior of the double-junction solar
2943 cell. Nevertheless, the obtained results are promising, demonstrating that the technology for
2944 such integration is progressing and that current technology is not very far from obtaining a
2945 high quality GaAsP/c-Si metamorphic double-junction solar cell.

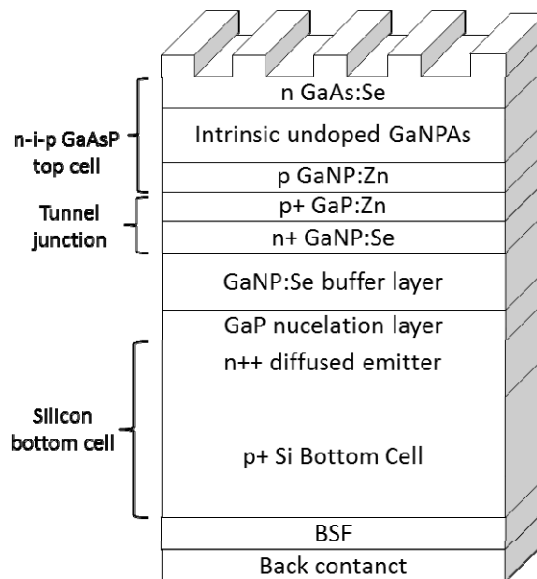
2946 **(ii) Lattice matched approach**

2947 As discussed above, one of the main limitations of III-V on c-Si epitaxy is the
2948 mismatch in lattice parameters. Hence, it is straightforward to assume that a lower lattice
2949 mismatch between the wafer and III-V compound implies a better structural quality of the
2950 resulting structure. Despite the fact that GaP seems to be the ideal candidate for the top cell
2951 material due to its lattice constant proximity to that of c-Si (Fig. 53), its large bandgap (2.2
2952 eV) makes it unsuitable for the top cell material. Therefore, a different material must be
2953 considered for the top cell. In this case, the most studied material for such integration is the
2954 quaternary alloy GaNPAs [381, 382, 430].

2955 Here, the lattice mismatch between the bottom (c-Si) and the top cell (GaAsP) is
2956 reduced by introducing nitrogen into the III-V semiconductor that decreases its lattice
2957 constant and brings it closer to that of Si. The idea is to grow the direct bandgap III-V alloy
2958 GaN_xP_{1-x-y}As_y (hereafter GaNPAs) onto the c-Si wafer and minimize the formation of
2959 structural defects [381, 382, 430] for high-efficiency double-junction solar cell. In 2004,
2960 Geisz et al. first reported the lattice-matched GaNPAs on c-Si double-junction solar cell
2961 [381]. As depicted in Fig.56, the cell is formed by a n-on-p c-Si bottom subcell, a

2962 GaP:Zn/GaNP:Se tunnel junction, and a GaNPAs ($E_g \sim 1.8$ eV) top subcell. As in the case of
 2963 the metamorphic approach, to minimize the occurrence of crystalline defects [381, 382], a
 2964 GaP nucleation layer is also grown before the GaNPAs layer.

2965 The use of nitrides (even diluted nitrides) for reducing the lattice mismatch presents
 2966 an important drawback: the formation of nitrogen-related defects, which greatly reduce the
 2967 diffusion length in the GaNPAs layer, and limits the performance of the top junction [390].
 2968 Geisz et al. [381] proposed the use of a field-aided device through a p-i-n configuration in the
 2969 top cell to maximize its IQE, and to avoid the limitations of the extremely short diffusion
 2970 length measured in the top cell. Thus, a thick GaNPAs intrinsic layer was grown to enhance
 2971 the performance of the device (see Fig. 56).



2972

2973 Fig. 56 GaNPAs/c-Si lattice matched double-junction solar cell. To reduce the lattice mismatch between the top
 2974 cell and bottom cell, nitrogen is introduced in the III-V structure to reduce its lattice constant and bring it close
 2975 to that of Si. Also, nitrogen minimizes structural defects. In the bottom cell, BSF acts as reflector for minority
 2976 carriers and causes the minority carriers (electrons in this case) to move to the bulk towards the p-n junction and
 2977 reduces surface recombination at the rear side. The internal quantum efficiency has been maximized through the
 2978 introduction of a field-aided device in the top cell (i.e. p-i-n configuration). In this double-junction structure, top
 2979 cell limits the device current. Redrawn from [381], Geisz J F, Olson J M, Friedman, D J. Toward a monolithic
 2980 lattice-matched III-V on c-Si double-junction solar cell, 19th European Photovoltaic Solar Energy Conference
 2981 (Paris) 2004.

2982

2983 Interesting results were obtained for each subcell measured separately [431]. For c-Si
 2984 bottom cell, V_{oc} of 536mV and J_{sc} of 14.5mA/cm² have been reported. GaNPAs ($E_g \sim 1.8$ eV)

2985 top cell showed V_{oc} of 1.09 V and J_{sc} of 5.7 mA/cm². This double-junction structure has the
2986 potential for further improvement, since the top cell limits the device current ($V_{oc} = 1.53V$, J_{sc}
2987 = 6.3 mA/cm², AM1.5G efficiency = 5.2%). Currently, efforts are mainly focused on: (i)
2988 reducing the dislocation densities of the buffer layer through a better control of the GaP
2989 nucleation layer, (ii) forming a functioning tunnel junction by increasing the p-type doping,
2990 and (iii) increasing the top cell current by reducing the emitter sheet resistance and
2991 controlling the material quality of the GaNAsP top cell [431].

2992 **6.3.2 III-V on c-Si using bonding technique**

2993 Different alternatives for the epitaxial integration of III-V semiconductors on c-Si
2994 wafers have been reviewed so far. However, as described above, this technique presents some
2995 limitations, which include: (i) as described in Sec.6.3.1.2, monolithic integration is limited
2996 due to lattice matching requirements, which highly reduce the range of III-V materials that
2997 can be integrated on c-Si, (ii) the use of metamorphic growth techniques for integrating
2998 lattice-mismatched compounds is limited due to relatively high dislocation density formed in
2999 the buffer layer (Sec.6.3.1.1). In this regard, alternatives to this process have been recently
3000 explored. In particular, the mechanical stack has emerged as an alternative to avoid the
3001 limitations of the epitaxial process.

3002 Unlike epitaxially grown structures, the wafer bonding interfaces are incoherent. This
3003 implies that it is possible to accommodate any lattice mismatched material without the
3004 formation of the above mentioned misfit dislocations [393,394]. Therefore, the use of wide
3005 variety of materials, including the ones discarded for conventional epitaxial growth, is
3006 allowed for this technique.

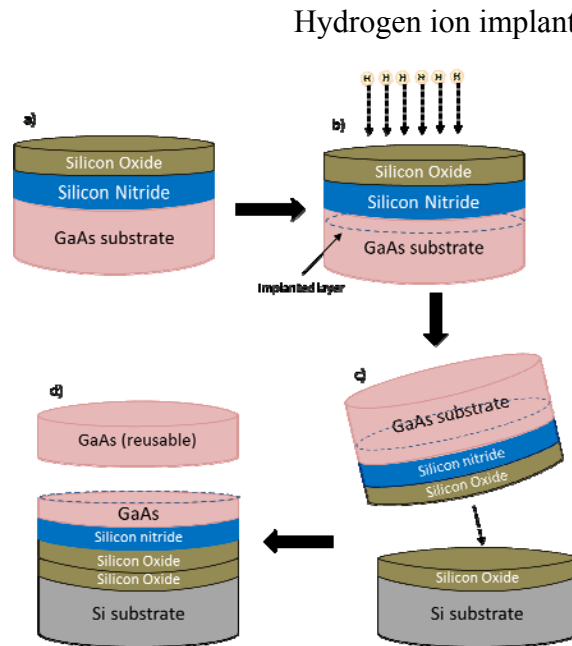
3007 The physical concept of wafer bonding is based on the idea that two surfaces can stick
3008 together as long as the surfaces are perfectly polished, resulting in relatively very little
3009 friction between them [432]. In particular, in the wafer bonding technique, this consists on

3010 transferring a thinned wafer of III-V compound (such as GaAs) to a c-Si wafer. The bonding
3011 can be carried out even at room temperature as a result of the interaction of pure surfaces by
3012 van der Waals forces. In order to guarantee a high quality bonding, surfaces have to be
3013 specularly polished and completely clean to avoid any organic contamination [433].

3014 There are different wafer bonding approaches for the integration of III-V compounds
3015 on c-Si wafers for PV applications. One of them is based on high-temperature sticking of
3016 wafers. In this case, wafers are covered by a glass-like coating that bonds the wafers once the
3017 softening temperature is reached. However, this technique presents some limitations due to
3018 the use of high temperatures that may cause some problems such as defect generation,
3019 diffusion of impurities, thermal stress, etc. [434, 435].

3020 An interesting alternative is the smart cut technology. The procedure for wafer
3021 bonding using this technique is depicted in Fig.57. Initially, handle (c-Si) and donor (GaAs)
3022 wafers are coated with a thin Si oxide, since the bonding of Si oxide surfaces can be done at
3023 room temperature in air. In some cases, a thin SiN layer is deposited before the oxide layer, in
3024 order to favor the adhesion of the III-V compound to the oxide (Fig. 57a). Then, a weakened
3025 layer (formed by hydrogen or helium bubbles) is generated within the donor wafer by the ion
3026 bombardment method (Fig. 57b) [392]. This layer will eventually serve as a predetermined
3027 breaking point. Next step is the preparation of the surfaces for lowering the surface roughness
3028 to obtain good wafer bonding. After putting them into close contact, both wafers are bonded
3029 together as a result of the oxide softening and the application of pressure (Fig. 57c). After
3030 wafer bonding, the exfoliation, i.e. detachment of GaAs wafer along the implanted layer, is
3031 achieved by a heat treatment (Fig. 57d). In order to avoid shearing of interfaces and
3032 separation of both connected materials, it is preferable to work with the lowest possible
3033 temperature, especially when materials with very different thermal expansion co-efficients
3034 are bonded. Several groups are exploring different ways for reducing the exfoliation

3035 temperature [394,436]. Finally, chemical and mechanical treatments of the exposed GaAs
 3036 surface are required for obtaining high quality surface for subsequent epitaxial growth. In this
 3037 technology, the donor wafer can be reused after exfoliation, and therefore the cost of the
 3038 process is highly reduced (as compared to epitaxial growth on GaAs wafers).



3039

3040 Fig. 57 Illustration of the smart cut technology for GaAs/c-Si structures: (a) the process starts with two different
 3041 wafers (i.e. GaAs as donor wafer and c-Si as handle wafer), both are oxidized to favor bonding. To improve
 3042 adhesion between GaAs and Si oxide, in the donor wafer, a thin SiN layer is deposited before the oxide layer
 3043 deposition. (b) a weakened layer is generated within the donor wafer by hydrogen ion implantation through the
 3044 oxide, (c) two wafers are hydrophilically bonded together due to oxide softening and external pressure, (d)
 3045 finally, after bonding, the GaAs wafer is cut away using the implanted region as a reference. Heat treatment is
 3046 used to detach GaAs wafer. Chemical and mechanical treatment is required for the exposed GaAs surface for
 3047 subsequent epitaxial growth. The remaining GaAs wafer can be reused afterward for subsequent processes.

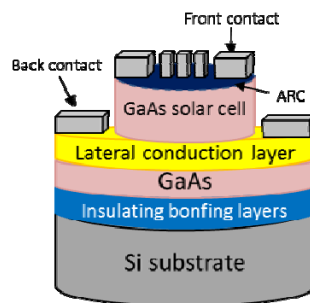
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3049 The use of smart cut technology leads to good quality crystals with a low dislocation
 3050 density below $4 \times 10^5 \text{cm}^{-2}$ [392]. Using smart cut technology, 12% efficiency GaAs/c-Si
 3051 single-junction solar cells have been reported [392].

3052 Other III-V materials such as indium phosphide (InP) have also been used as donor
 3053 wafers for their direct bonding on c-Si wafers [437, 438]. These InP/c-Si stacks have been
 3054 used as templates for subsequent III-V epitaxial growth, obtaining InGaAs/InP solar cells on
 3055 inactive c-Si wafers [437] with V_{oc} of 0.30 V, J_{sc} of 24.9 mA/cm^2 and AM1.5G efficiency of
 3056 13.6%. This InGaAs solar cell is a good candidate for working as the bottom cell of a high-

3057 efficiency triple-junction cell, since it may be current matched with InGaP/GaAs double-
 3058 junction solar cells [439, 440].

3059 However, the use of this technique presents an important drawback: the bonding
 3060 layers are made of Si oxide, an insulating material. Thus, the c-Si wafer is not the active
 3061 region of the structure; on the contrary, it is merely acting as a mechanical support for the
 3062 structure without any active PV role. Hence, this technology requires the development of a
 3063 new solar cell design for contacting the rear side of the solar cell. With this aim, as shown in
 3064 Fig. 58, a lateral conduction layer [392] is grown on the top of the III-V seed layer (before
 3065 growing III-V solar cell epitaxially) for contacting the base layer of the active region.



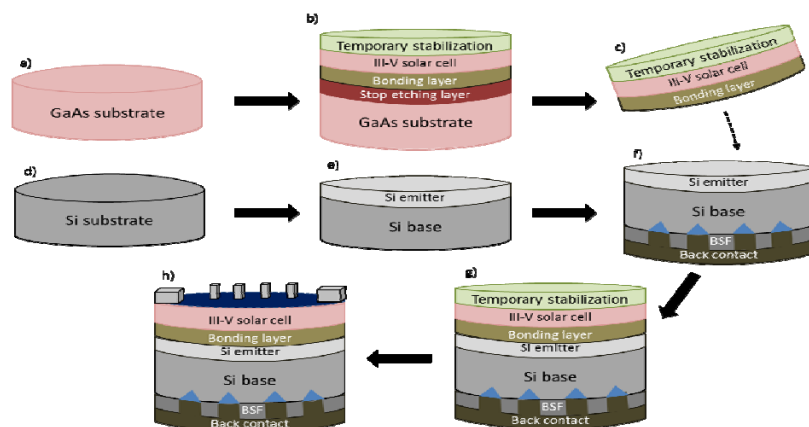
3071 Fig. 58 Single-junction GaAs solar cell on GaAs/c-Si wafer using smart cut technology. Since the c-Si wafer is
 3072 not an active part of the structure, the conventional back contact must be relocated so that the back side the solar
 3073 cell can be contacted. In this case, a lateral conduction layer is grown on top of the GaAs seed layer. Back side
 3074 contact is formed on top of the lateral conduction layer and grid lines are formed at the front side of the solar
 3075 cell for front contact. Lift-off process using photolithography is the conventional method used for the formation
 3076 of front grid contact. Redrawn from [392], Schone J, Dimroth F, Bett A W, Tauzin A, Jaussaud C, Roussin J C,
 3077 III-V solar cell growth on wafer-bonded GaAs/c-Si-wafer, IEEE 4th World Conference on Photovoltaic Energy
 3078 Conversion (Hawaii) 2006.

3080 Many groups have been working on solving the drawback of the inactive wafers [393,
 3081 441, 442]. As a result, an improvement of smart cut technique has been achieved. The main
 3082 modification is the substitution of the insulating bonding layer by a conductive layer. The
 3083 surface-activated wafer bonding process has been illustrated in Fig. 59 [442]. In this case, the
 3084 GaAs wafer is used as a template for epitaxial growth of III-V compounds (Fig. 59 a-c). An
 3085 etch-stop layer and a bonding layer are grown on top of GaAs wafer, before the epitaxial
 3086 growth (Fig. 59b). Simultaneously, as shown in Fig. 59 (d-f), the c-Si wafer is processed

3087 before stacking, so a single-junction c-Si solar cell is formed. The whole structure is then
 3088 attached to a wax-type transfer substrate. Afterwards, the etch-stop layer is etched away
 3089 laterally, so the GaAs wafer is physically detached from the structure in a way that allows for
 3090 its reuse (Fig. 59c). In this process, the surfaces of the cell structures are cleaned by a beam
 3091 of argon (Ar) atoms in a ultra high vacuum chamber. The wafers are brought into intimate
 3092 contact immediately after the surface activation to initialize the bonding (Fig. 59g). Finally,
 3093 the wax-type transfer substrate is removed and the mechanical stacked solar cell is eventually
 3094 processed (Fig. 59h).

3095 To our knowledge, the first direct wafer bonded MJSCs with a c-Si subcell was
 3096 reported on 2012 by Tanabe et al. [393], using an AlGaAs/c-Si double-junction solar cell,
 3097 with an efficiency of 25.2% under one sun ($100\text{mW}/\text{cm}^2$) illumination. GaInP/GaAs/c-Si
 3098 triple-junction solar cell with an efficiency of 20.5% under one sun, and 23.6% under 71 suns
 3099 illumination (AM1.5 conditions) was also reported using the same technique [441, 442].
 3100 Recently, a GaInP/c-Si double-junction solar cell formed by a rear heterojunction GaInP and
 3101 a back junction, back contacted c-Si bottom cell has been reported [443] with an encouraging
 3102 efficiency of 26.2% at 1 sun illumination (AM1.5G).

3103



3104

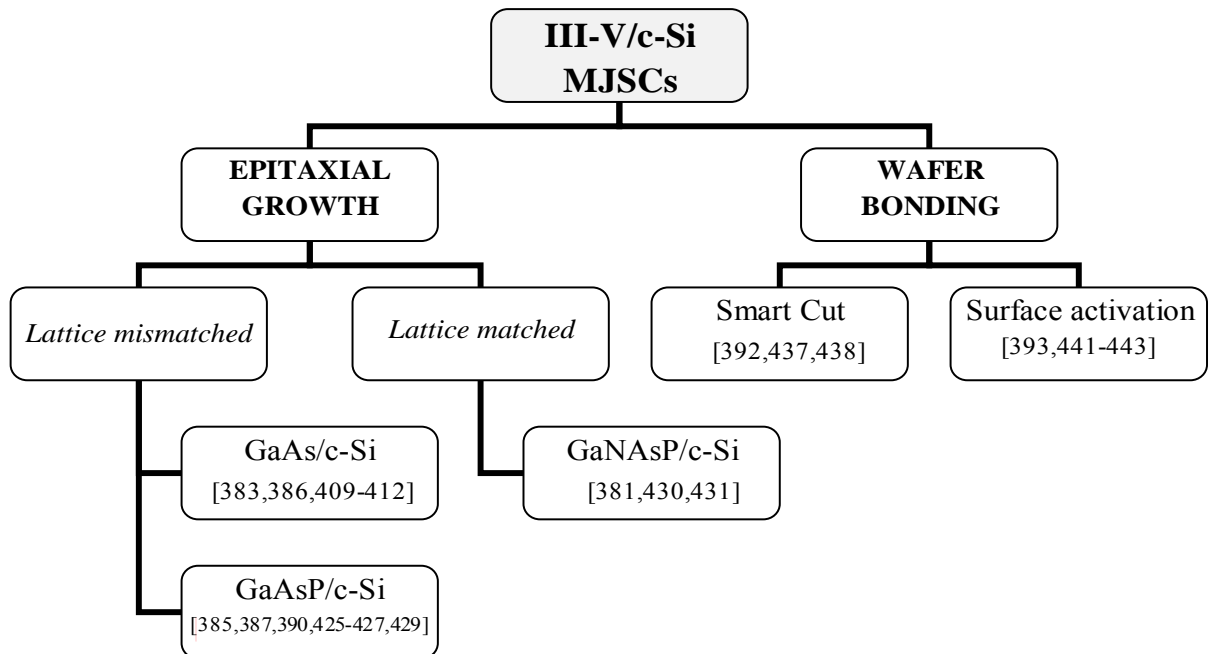
3105

3106 Fig. 59 III-V/c-Si multi-junction solar cell by surface activated wafer bonding process: (a) GaAs wafer for
 3107 epitaxial growth of III-V compound, (b) etch-stop layer and bonding layer are grown right before the epitaxial
 3108 growth of III-V solar cell and then attached to a transfer substrate, (c) lateral etching remove etch-stop layer and

3109 GaAs wafer is detached for reuse, (d-f) single-junction c-Si solar cell process, (g) after cleaning and activating
 3110 the surfaces, wafers are bonded together, (h) wax-type transfer substrate is removed and stacked MJSC cell is
 3111 processed for top contact. This process is an improvement of smart cut technique, supporting wafer (c-Si) is not
 3112 inactive. Supporting wafer is active and used to form bottom cell.
 3113

3114 Although promising results have been achieved recently, the main bottlenecks of this
 3115 technology are the resistance of the bonding surface, and current mismatch between the
 3116 subcells, which limits the device performance. This is primarily limited by the c-Si bottom
 3117 cell [441]. For a better visual comparison of various technologies associated with III-V on c-
 3118 Si MJSC, a block diagram is shown in Fig.60.

3119



3120

3121 Fig. 60 Different III-V compounds on c-Si technology. The integration of III-V semiconductors on c-Si wafers
 3122 by epitaxial growth using two different approaches: lattice matched and lattice mismatch (or metamorphic)
 3123 approach. The main difference between these two approaches lies on handling the lattice mismatch between the
 3124 top and the bottom cell materials. These two different approaches have been found to produce successful results
 3125 for the integration of III-V on c-Si wafers through the wafer bonding approach. An important process is the
 3126 surface activated process, which replaces the isolating bonding layer (used in the smart cut technology) by a
 3127 conductive layer, and thus, the c-Si wafer takes place in the active region of the structure and acting as bottom
 3128 cell.

3129 6.4 Future outlook

3130 Two different technologies have been predominantly used so far for the integration of
 3131 III-V on c-Si: epitaxial growth, and wafer bonding. Epitaxial growth of III-V semiconductors

3132 on c-Si wafers has received a lot of attention over the last decades, resulting in a reasonable
3133 scientific understanding of this process. Although a great deal of work has to be still done for
3134 achieving high quality monolithic III-V on c-Si double-junction solar cell, a prototype of a
3135 GaAsP/c-Si double-junction solar cell [425,427] has been recently reported. This structure
3136 has been epitaxially grown by combining two different techniques: MBE, and MOCVD.
3137 Interesting results were obtained in this case, demonstrating the operation of a double-
3138 junction solar cell, with V_{oc} of 1.62 V and J_{sc} of 11.0 mA/cm² [425]. These results are
3139 promising, and demonstrate that the technology for such integration is progressing. Future
3140 work will be directed towards the development of the tunnel junction and its integration into
3141 the double-junction solar cell, which is the main bottleneck for this structure, limiting the
3142 electrical behavior of the double-junction solar cell. Moreover, future activity must be
3143 directed towards simplification of the technology by means of the development of a
3144 GaAsP/c-Si metamorphic double-junction solar cell into a single reactor (i.e. MOCVD).

3145 On the other hand, wafer bonding has emerged as an alternative for epitaxial growth.
3146 In particular, the surface-activated wafer bonding technology is seen as a promising option
3147 for III-V on c-Si integration. In this respect, a GaInP/c-Si double-junction solar cell formed
3148 by a rear heterojunction GaInP and a back junction back contacted c-Si bottom cell has been
3149 recently reported [443] with an encouraging efficiency of 26.2% at 1 sun illumination
3150 (AM1.5G). In this case work must be directed to overcome the current limitations, such as
3151 resistance of the bonding surface and current mismatch between cells, which are currently the
3152 limiting factors of the cell electrical properties.

3153 **7. Amorphous Si solar cells**

3154 A-Si:H has seen rapid development in industrial processing in the last decade, and has
3155 led to multiple types of large area and roll-to-roll deposition systems. While the Si material

3156 development appears to have reached saturation, the passive parts of devices, such as surface
3157 texture, light trapping designs, development of thinner cells, and cells on new exquisite
3158 nanopillar and nanohole structures have made tremendous progress. Moreover, third
3159 generation concepts are beginning to be applied to thin-films Si devices, making a paradigm
3160 shift in the way a solar cell operates, with existing fabrication tools.

3161 **7.1 Introduction**

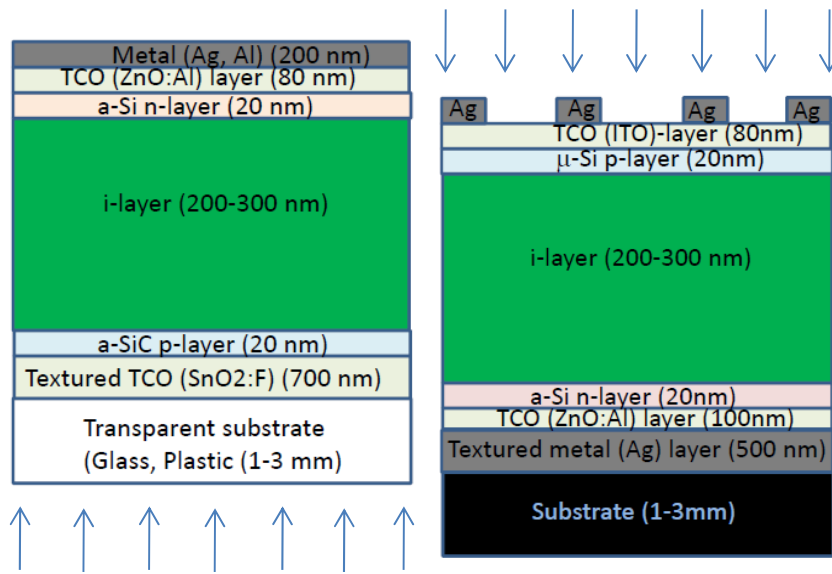
3162 According to European Photovoltaic Industry Association (EPIA) the global
3163 cumulative installed solar power capacity in 2015 crossed 228GW [444]. The learning curves
3164 [445] show a 22% reduction in price for PV; thin-film PV shows a slightly higher rate of cost
3165 reduction compared to c-Si wafer type of cells. Though the cost of thin-film Si modules
3166 commercially is less than that of c-Si, the cost of electricity is essentially similar in both
3167 cases. This makes a c-Si module still most attractive because of its high-efficiency. Among
3168 thin-film PVs, CdTe is the most attractive, due to a very small energy payback time of 0.5
3169 years [446] at the cost of \sim \$0.6/W [447]. These advances clearly pose a commercial
3170 challenge for a-Si:H PV.

3171 The commercial single-junction a-Si:H modules have an efficiency of 4-8%, whereas
3172 the best laboratory efficiencies are in the range of 9.5-10%. According to International
3173 Renewable Energy Agency, among thin-film technologies, a-Si:H thin-film is perhaps the
3174 most challenged by the current low-cost c-Si [448]. Its future is rather uncertain as some
3175 producers have recently either stopped or reduced part of manufacturing capacity, even
3176 though in laboratory it is demonstrated that using a simple thin a-Si:H absorber a stabilized
3177 efficiency of 10% can be achieved [449,450]. Moreover, the energy payback time of thin-
3178 film a-Si:H, as was claimed by TEL Solar Japan (formerly Oerlikon), is less than 1 year, and
3179 a cost of electricity of \$0.088/kWh for ground mounted system is estimated [451]. The
3180 wholesale price of thin-film a-Si:H PV module in July 2013 is only \$0.46/Wp and thin-film

3181 a-Si:H/ μ c-Si:H (micromorph) is at \$0.59/W_p, much lower than \$1.74/W_p in the beginning of
3182 2010 [452].

3183 According to EPIA fact sheet [453], the most critical materials used in PV
3184 technologies are indium, tellurium and Ag. The first two of these are indispensable elements
3185 of the state-of-the-art CIGS and CdTe solar cells respectively. However, these elements are
3186 not absolutely necessary for thin-film Si PV, especially for superstrate type of cells. Typical
3187 schematic diagram of a p-i-n (also called superstrate type) and an n-i-p (also called substrate
3188 type) a-Si:H cell is given in Fig.61. ITO is generally used on the top TCO for n-i-p cells, and
3189 Ag is used as rough template on which n-i-p cell is made. The former can be replaced by an
3190 alternative TCO, such as doped ZnO:Al [454], whereas many types of light trapping features
3191 at the back side can be made; patterning of the substrate (through lithography or embossing
3192 techniques) [455], naturally grown textured ZnO [454], and texture etched ZnO [456]. For p-
3193 i-n cells, white paints [457-459], white sheet (developed by Dupont for Oerlikon) [460], and
3194 Al [461] can be used as back reflector. However, Ag is still used by many companies to
3195 maintain a high-efficiency. A trade-off has to be made between gain in price for high-
3196 efficiency, and the loss due to high cost of Ag in comparison to Al. Since the price of Ag has
3197 fallen recently after a peak in 2011 of above \$1100/kg to now (in 2016) around \$500/kg
3198 [462], this may currently not be an issue with PV, but may be sensitive to future demand-and-
3199 supply. As efficiency increase is an option to reduce the cost [463] (every 1% increase in PV
3200 module efficiency reduces the balance of system (BOS) cost by between \$0.07 and \$0.10/W),
3201 micromorph cells are best suited to serve this purpose with relative simplicity and high-
3202 efficiency. Commercial micromorph module efficiencies are between 6.5 and 9%, though
3203 best laboratory efficiencies are currently in the range of 12-13%. It should be noted that
3204 prototype module efficiencies of up to 11% have been demonstrated. Further efficiency
3205 increase by employing higher number of junctions will have to take into account the possible

3206 cost benefit of a high-efficiency and complexity of production. Bankruptcy of Unisolar
 3207 Ovonics (US) after years of experience in triple-junction cells, and difficulty of other
 3208 companies, especially Kaneka Co. (Japan), in commercializing such products warns us that
 3209 careful design and process simplicity have to be developed for cost reduction, especially the
 3210 capital expenditure (CAPEX), and a new industrially viable processing is a necessity.



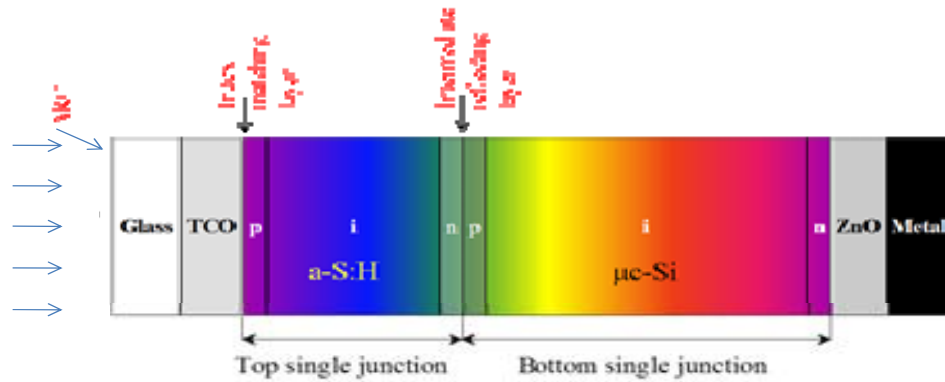
3211
 3212
 3213
 3214 Fig.61 Schematic diagram of a p-i-n or superstrate type (left side) and an n-i-p or substrate type (right side) a-
 3215 Si:H solar cell. In both type of cells, light enters through the p-layer side since hole mobility is lower than the
 3216 electron mobility. Substrate type cells have the advantage that substrate need not be transparent, e.g. metal
 3217 (steel, Al) foil, non-transparent plastics (such as Kapton), tiles, fabrics etc. For superstrate cell, texture etched
 3218 ZnO:Al is also widely used, however, in that case a double p-layer (microcrystalline/amorphous) is used.
 3219 Several types of light trapping features can be made at the rear side such as naturally grown textured ZnO,
 3220 texture etched ZnO and patterning the substrate. Same cell designs are used for μc-Si:H cells (p, i and n layers
 3221 all are μc-Si:H, i-layer thickness 1-2μm) and a-SiGe cells (U, V, or E type graded i-layer 100-150nm).
 3222

3223 In this section we will look at how the thin-film Si technology has evolved through the
 3224 years and show that, in spite of current uncertainty in market, why it is still one of the most
 3225 promising technology for the future.

3226 7.2 Brief history and status of thin-film Si technology

3227 A-Si:H came into existence in 1960s. Amorphous structure contains short range order
 3228 similar to c-Si but deviates in medium range and long range order. The second difference is
 3229 that critical (average) network coordination for a-Si is 2.4 compared to coordination of 4 for

3230 c-Si. Breaking of bonds allows the material to reduce the coordination. Hydrogen has a big
3231 role in reducing the network coordination while retaining local four-fold coordination.
3232 Hydrogen is situated at monohydrides, dihydrides, polyhydrides (Si-H₂)_n, SiH₃ and voids.
3233 The material can be described as continuous random network which contains randomly
3234 distributed weak bonds and dangling bonds. However, the structure also contains another
3235 phase which is hydrogen rich, with low density regions and voids. It was in 1976 that an a-
3236 Si:H solar cell with 2% efficiency was made, with a prediction of 15% efficiency in the
3237 future [464]. However, it was realized that these materials (cells) suffer from light induced
3238 degradation, also called Staebler-Wronski effect, discovered in 1977 [326]. This
3239 phenomenon, with a decrease by an order of magnitude in both dark and light
3240 photoconductivity under illumination from the initial state, is metastable. All optoelectronic
3241 characteristics can be reverted back to the initial state by annealing of the sample above
3242 150°C (above the glass transition temperature of hydrogen in amorphous material). This
3243 phenomenon is caused by a change in midgap density of states (increase in dangling bond
3244 density) resulting in shift of Fermi level towards midgap and increase in recombination.
3245 There are basically two divergent models proposed as origin of this effect; (i) (weak) bond
3246 breaking (hydrogen mediated) that creates isolated defects [465-467], and (ii) voids/volume
3247 deficiencies [468-470]. Hydrogen seems to play an important role in this effect. To mitigate
3248 the Staebler-Wronski effect, materials have been fabricated with low hydrogen content,
3249 smaller Si-H₂/Si-H ratio, lower microstructure factor/void content, lower Urbach energy
3250 (weak-bond density), etc. To that end, high hydrogen dilution of precursor (SiH₄) gas during
3251 deposition is invariably used. Now, use of thinner absorber layers and multi-junctions cell
3252 design has made it possible to control the light induced degradation of efficiency to an
3253 acceptable range below 10%.



3254

3255 Fig. 62 Schematic diagram of typical micromorph superstrate type double-junction cells. An efficient tunnel
 3256 recombination junction made of p- and n- μc layers allows Ohmic contact between the cells. ARC, normally a
 3257 graded refractive-index layer (n) coating reduces partly the 4% reflection loss at the glass/air interface. ARC,
 3258 normally a graded refractive-index layer (n) coating reduces partly the 4% reflection loss at the glass/air interface.
 3259 Refractive index matching layer such as TiO_2 has the function to reduce reflection at the TCO (n~2)/p-layer
 3260 (n~4) interface; intermediate reflector selectively reflects light at the tunnel recombination junction to the top
 3261 cell, a technique by which the top cell thickness can be substantially reduced for better stability. Typical
 3262 intermediate reflector is made from oxides - SiO_x (n or p-type) or ZnO or a Bragg reflector. Typical thickness
 3263 and bandgap of the top cell and the bottom cell are ~200nm, 1.8eV and 1-2 μm , 1.1eV respectively.

3263

3264 Later, alloying a-Si:H with C, Ge, N, O, etc. allowed fabrication of multi-junction
 3265 solar cells with wide bandgap doped layers, and tunnel recombination junction. This was
 3266 considered a major advantage as compared to c-Si cells. Up to beginning of 1990s, a-Si:H
 3267 cells in combination with an a-SiGe:H alloy cells in multi-junction structure were considered
 3268 as among the best options, and a number of industries focused on this technology (Solarex
 3269 [471], Unisolar [472], Sanyo[473] and Fuji electric [474]). By 1990, double and triple-
 3270 junction devices using a-SiGe:H as bottom cell(s) reached global AM1.5 initial efficiency of
 3271 13.0% and 13.7%, respectively. Throughout this period, however, a-Si:H PV went through a
 3272 technological challenge because of “degrading cells” (the Staebler-Wronski effect of a-Si:H
 3273 [326]), and even a-SiGe:H alloys showed substantial degradation [475]. However, the advent
 3274 of device-quality nanocrystalline Si (nc-Si:H) absorber layer in mid 1990s, [476,477] and
 3275 demonstration by Kaneka with cell efficiency of >10% at a high deposition rate (0.5nm/s)
 3276 [478] changed the scenario. Thus, a-Si:H in combination with nc-Si:H (also called μc -Si:H)
 3277 became desirable. This structure, called micromorph cell (Fig.62), allowed a greater range of
 3278 solar spectrum to be absorbed, avoided the toxic and expensive germane gas, and
 3279 demonstrated enhanced stability. This nc-Si:H material has attracted immense research

3280 interest because of its complex structure and yet to be fully understood growth process [479].
3281 A debate exists on whether a-SiGe:H or nc-Si:H is a more profitable proposition as the
3282 bottom cell [480]. The arguments are based on two different scenarios, i.e. whether to use
3283 expensive germane gas, lower deposition rate (~ 0.1 nm/sec), but relatively thinner (~ 100 nm)
3284 absorber layer for a-SiGe:H, or a much thicker layer ($> 2 \mu\text{m}$), accompanied with degradation
3285 of cell performance at high deposition rates for nc-Si:H [481]. One of the strong arguments
3286 used for thin-film Si solar cells has been the non-toxic nature of base materials compared to
3287 other types of thin-films PVs. Germane gas is highly toxic, due to which the preference in
3288 the last decade has tilted in favor of nc-Si:H. Thin-film Si processing also uses toxic dopant
3289 gases (PH_3 , B_2H_6 etc.), however, their concentrations are very small in the gas mixture.

3290 At present the most widely used industrial process is the micromorph structure. TEL
3291 Solar has provided even turnkey solutions for these double-junction cells. Though the use of
3292 a-SiGe:H in a double-junction structure is now rare, because a-Si:H/nc-Si:H potentially
3293 delivers higher efficiency due to perfect bandgap combination of 1.8 eV/1.1eV [482], a-
3294 SiGe:H still holds a lot of promise in triple-junctions, especially for the adjustable bandgap
3295 middle cell. The cell with current record initial efficiency of 16.3% (initial) uses a-SiGe:H in
3296 the middle cell [483] in an n-i-p cell configuration. Though the record stabilized efficiency is
3297 achieved without Ge in a p-i-n type a-Si:H ($E_g \sim 1.73$ eV)/nc-Si:H ($E_g \sim 1.1$ eV)/nc-Si:H (E_g
3298 ~ 1.1 eV) structure [484,485], LG is exploring to use a-SiGe:H films to improve this
3299 technology [486]. LG developed a-SiGe:H cell with a modified E-shape bandgap profile,
3300 originally demonstrated at Utrecht University [487,488], which was used as the middle cell
3301 of a triple-junction structure and delivered an initial efficiency of 14.9%. Moreover, the
3302 direction towards thinner cells (to be discussed shortly) can only be achieved by using a-
3303 SiGe:H, even for double-junction cells. Moreover, it has already been demonstrated that a
3304 very stable a-SiGe:H can be made with protocrystalline (pc-Si:H) condition [489] (i.e. films

3305 deposited just before the onset of microcrystalline regime known as protocrystalline
 3306 condition), though at a low deposition rate (~ 0.06 nm/sec). The success will depend on the
 3307 fabrication of stable low bandgap a-SiGe:H ($E_g \sim 1.3-1.4$ eV) cell, especially at acceptable
 3308 deposition rates (> 0.1 nm/s). In this aspect, two types of development have taken place:
 3309
 3310 (i) μ c-SiGe:H [490], which allows a use of a thinner bottom cell of a double (a-Si:H/ μ c-
 3311 $\text{Si}_{0.83}\text{Ge}_{0.17}$:H [491]), and triple-junction (p-i-n type a-Si:H/ μ c-Si:H / μ c- $\text{Si}_{0.9}\text{Ge}_{0.1}$:H [492], p-
 3312 i-n type a-Si:H/ μ c- $\text{Si}_{0.6}\text{Ge}_{0.4}$:H/ μ c- $\text{Si}_{0.91}\text{Ge}_{0.09}$:H [493]). The total thickness of the double-
 3313 junction [491] and the triple-junction [493] are only 1000nm and 1800nm, respectively.
 3314
 3315 (ii) HWCVD a-SiGe:H has [494] shown that good photosensitive materials can be made for
 3316 bandgap even below 1.4eV, much better than PECVD grown materials. However, this
 3317 process demands high gas flow rate to avoid depletion of the germane gas. The cost
 3318 implication of high germane consumption has to be considered. Table 2 shows the record
 3319 efficiencies of single, double, and triple-junction Si thin-film cells.

3320 Table 2 Record thin-film Si cells. The bandgap and thickness of the layers are: a-Si:H (1.7-1.9 eV, ~ 200 nm), a-
 3321 SiGe:H (~ 1.5 eV, ~ 150 nm) and nc-Si:H (1.1eV, ~ 2000 nm). A-Si:H layers are deposited in protocrystalline
 3322 condition. Whereas the stabilized efficiency of single-junction (even initial efficiency) is well below the S-Q
 3323 limit of 29%, the maximum stabilized efficiency (13.44%) is still much below the theoretically estimated triple-
 3324 junction of $\sim 48\%$. The results suggest enough room for improvement in the cell performance for thin-film Si.
 3325 *independently measured.

3326

Cell	Group	Eff. (% initial)	Eff. (% stabilized)	Ref.
a-Si:H	Sanyo	12.7	-	[495]
a-Si:H	EPFL	-	10.1*	[449]
a-Si:H/a-SiGe:H	Sanyo	11.6	10.6	[496]
nc-Si:H	EPFL	10.9, 10.7*	-	[497]
nc-Si:H	UU	-	10	[498]
a-Si:H/nc-Si:H	EPFL	14.4	-	[499]
a-Si:H/nc-Si:H	Kaneka	14.7	-	[500]
a-Si:H/nc-Si:H/nc-Si:H	LG	-	13.44*	[501]
a-Si:H/nc-Si:H/nc-Si:H	Unisolar	-	13.6	[502]

a-Si:H/a-SiGe:H/nc-Si:H	LG	16.1	-	[501]
a-Si:H/a-SiGe:H/nc-Si:H	Unisolar	16.3	-	[503]

3327

3328 **7.3 Challenges to a-Si:H technology**

3329 As compared to c-Si technology (which dominates around 87% of the market), thin-
3330 film PV has a relatively small share of 13% in the PV market. This is further dominated by
3331 CdTe, leaving behind only a very small market for thin-film Si. The main argument against c-
3332 Si PV is its high cost due to, among others, the use of thick absorber material compared to a-
3333 Si. However, this argument is now challenged. First, high price of c-Si in 2006, due to Si
3334 ingot price increase from \$200/kg to \$400/kg between 2007 and 2008 [504], led to a 30%
3335 reduction of Si material in the manufacturing process. Using thinner wafers (180-200 μ m now
3336 from earlier \sim 300 μ m), process automation and waste recycling, the Si use has now reached a
3337 low 5-10g/W_p [448]. The target is to reach the level of 3 g/W_p or less between 2030 and
3338 2050, pushing the limit further. Moreover, Panasonic showed their best efficiency of 24.7%
3339 for HIT solar cell for a wafer thinner than 100 μ m [505], and even 70 μ m flexible cells can be
3340 made. Attempts are now being made to push it further down to less than 50 μ m, though
3341 sawing and yield require further technological advancement. Moreover, thin-film c-Si by lift-
3342 off methods are also in progress [506], and 16.8% efficiency for 18 μ m c-Si has been
3343 reported and cells even with 10 μ m (8.7%) have been made. Second, the price of polysilicon
3344 has dropped sharply and reached \$20/kg in 2011 [504]. Third, the large production of c-Si
3345 based modules has reduced the price [445]. Moreover, the large over capacity has forced
3346 dumping of PV at low price (around 25GW of global installation compared to around 60GW
3347 of ramped module capacity in 2011) due to which even c-Si modules can be purchased at
3348 very low price and pushed thin-films PV to margin.

3349 Among thin-film PV technology, CdTe made up 46% of total module production in
3350 2012, followed by thin-film Si (a-Si:H single and multi-junctions, 35%) and CIGS (19%).
3351 However, CdTe production is dominated by only one company (First Solar) and CIGS is
3352 predominantly by Solar Frontier, clearly showing that these productions are still very much
3353 process specific. Wide use of off-the-shelf deposition facilities has still not taken place,
3354 unlike with thin-films Si, for which even turnkey solutions are available. Si, though, is
3355 expected to maintain its advantage over other thin-film materials, since it is non-toxic and
3356 abundant.

3357

3358 **7.4 Deposition related issues**

3359 A-Si:H is grown from gas phase in a vacuum chamber. It is a very reproducible
3360 material, and is very weakly dependent on process parameters, deposition systems, reactor
3361 volume or pumping speeds, etc. Standard a-Si:H films are routinely made at many labs with
3362 various deposition processes, such as standard radio frequency (RF) PECVD, VHF PECVD,
3363 hot-wire CVD, microwave PECVD, PhotoCVD, etc., with deposition rates of 0.1-0.3nm/s
3364 with almost comparable physical characteristics, delivering around 10% initial efficiency in
3365 single-junction cells. However, for better stabilized efficiency, the deposition process is
3366 adapted. The first indication for a better stability against light soaking came with the hot-wire
3367 CVD a-Si:H [507] with a smaller hydrogen content (~1%) than that is in standard device-
3368 quality a-Si:H of 10%. Since then, it is more or less established that a-Si:H deposited under
3369 high atomic hydrogen ambient, which is generally, but not necessarily, made with high
3370 hydrogen dilution of SiH₄, just at the edge of transition to nanocrystalline regime is the most
3371 stable material. The amount of dilution H₂/SiH₄ depends on other deposition conditions; for
3372 example, LG uses a very high H₂/SiH₄ value of 60 for their a-Si:H top cell [501]. This
3373 material, called pc-Si (as mentioned already in Sec. 7.2) [508] is, however, sensitive to
3374 deposition process and is fabricated in a narrow deposition regime. Hence, it is prone to

3375 irreproducibility and therefore needs good control in deposition process. Unlike a-Si:H, a pc-
3376 Si:H is thickness dependent. Hence it can make a transition to nc-Si:H with slight change in
3377 thickness. A competing process to make stable materials, and claims to be thickness
3378 independent, is the so called polymorphous Si (pm-Si:H) [509]. So far the stabilized
3379 efficiency with pm-Si:H has still not reached its full potential, and is yet to reach the
3380 efficiency that is obtained by pc-Si:H. One common denominator in all these materials is that
3381 they contain crystalline nanoparticles, brought in the material either by nucleation in the
3382 amorphous matrix (as in case of pc-Si:H), or embedded from gas phase (as in case of pm-
3383 Si:H). The correlation of stability with nanocrystalline incorporation, irrespective of its origin
3384 (whether through hydrogen dilution or Ar dilution of SiH₄) has been speculated for a long
3385 time [510].

3386 Nc-Si:H can be made by a variety of techniques [511], the same that are used for a-
3387 Si:H. Control of ion energy with very VHF RF power and high process pressure have led to
3388 high quality nc-Si:H material, and cells with high-efficiencies above 10%. On the other hand,
3389 high RF power and high gas flows in high pressure gas depletion condition (also called HPD)
3390 has led to high growth rates. However, the monotonic decrease in material quality and solar
3391 cell performance at higher deposition rates [479] is still a lingering issue that needs solution.

3392 **7.5 Recent trends to push the limits: Light management**

3393
3394 Light trapping in the absorber (intrinsic) layer is one of the most widely used concepts
3395 in thin-film Si solar cells for the purpose of either to increase the current or decrease the
3396 thickness of the absorber layer. This is essentially achieved in three ways [512]: (i) scattering:
3397 a random texture is generally used, (ii) geometric optics: features larger than the wavelength
3398 of light is used, the total internal reflections at interfaces of absorber layer is used for this
3399 purpose leading to $4n^2$ light passes in Yablonovitch limit [513], and (iii) diffraction: periodic
3400 pattern. The periodic designed pattern is brought about by hot embossing or nanoimprint

3401 technology [455,514], photolithography plus etching [515], and direct patterning of the hard
3402 substrate, such as glass [499]. The highest cell performance is still dominated by substrates
3403 with random textures. A very recent study indicates that for thick cells with thickness in the
3404 range of or higher than the wavelength of light, also called as geometric thickness, the
3405 random structures will provide excellent light trapping effect. However, for thicknesses much
3406 smaller than wavelength of light, a designed structure is needed to obtain higher current than
3407 the random structure [516].

3408 There are a number of techniques to manipulate the light behavior in a solar cell using
3409 the light interaction at the interfaces of materials of dissimilar refractive indices. The novelty
3410 here is to gain absorption without developing macroscopic textures that have adverse effect
3411 on the growth of the absorber material, and lead to micro/macro defect states. Moreover, very
3412 thin absorber layers can be used without the fear of shunting. Plasmonic effect of light
3413 interaction at the interface of a metal (negative refractive index) and dielectric material
3414 (positive refractive index) is exploited by embedded metallic nanoparticles/structures in a
3415 solar cell [517]. The near field effect of increased absorption and the plasmon polariton
3416 propagation of waves perpendicular to the length of the cells, bring down the necessary
3417 thickness for the cell, whereas the scattering from the plasmonic structures additionally
3418 benefit even thicker cells.

3419 One of the positive outcomes of the research on designed substrate texture
3420 architecture has been the development of almost any design and fine structure on any type of
3421 substrate [518]. This has allowed for the fabrication of high-efficiency solar cells on
3422 temperature sensitive substrates, such as cheap plastics PET, PEN [519], PC [520] etc. These
3423 have temperature limitations due to their glass transition temperatures being less than 150°C,
3424 which is much lower than the optimum deposition temperature (~200°C) of amorphous, or
3425 nc-Si:H material.

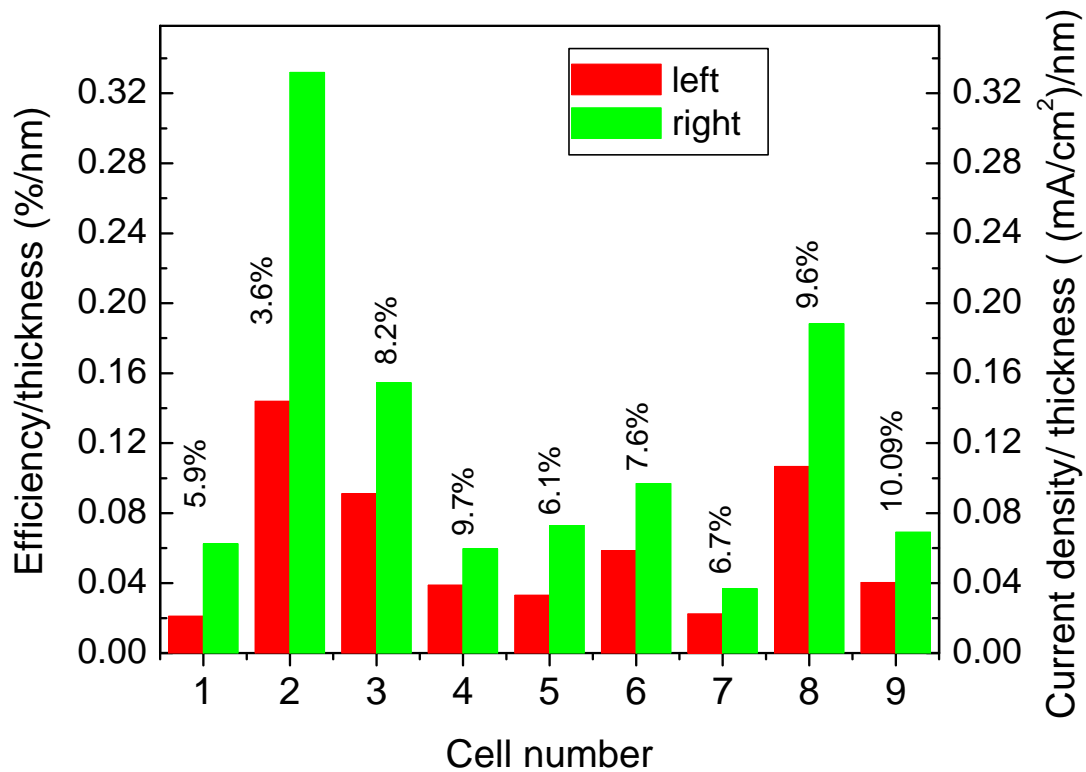
3426 **7.6 Current trend**

3427 Notwithstanding all the developments that have taken place for a-Si:H cells (see Sec.
3428 7.2), efficiency is still an issue. The best stabilized efficiency for a triple-junction is still
3429 much lower than the best that CdTe (21% First Solar [521]) or CIGS (21.7% ZSW [522])
3430 cells can deliver. Even with significant efforts, the defect density for a-Si:H and nc-Si:H
3431 intrinsic layers are still in $10^{15}/\text{cm}^3$ range, and a-SiGe:H has even more than an order higher
3432 defects. Moreover, light induced degradation issue of amorphous materials still persists. In the
3433 last few years, there has been limited research in the material side, and efforts have been
3434 directed towards the passive parts of the cells structure, mostly the optical design and light
3435 trapping. It has now been realized that with the best design used so far (solar cell on textured
3436 surface), the efficiency cannot be increased much further [523]; nc-Si:H growth limits the
3437 maximum root mean square roughness and opening angle of the surface feature that can be
3438 used, whereas the defect density limits the thickness of the a-Si:H and a-SiGe:H layers.
3439 Hence, new unconventional designs are being developed, of which two extreme cases are
3440 presented below; solar cells on (i) high aspect ratio structures, and (ii) flat surface.

3441 **7.6.1 Extremely thin cells**

3442 Traditionally, light trapping schemes, such as that described in the above section, are
3443 employed to mitigate the adverse effect of lower quality of a-Si:H layers compared to
3444 crystalline counterpart that compels the allowed thickness of the a-Si:H or nc-Si:H solar cells
3445 to be much smaller than the penetration depth of visible light. Industries, as well as research
3446 laboratories, are aiming for better stabilized efficiencies that are achieved with thinner cells.
3447 TEL Solar clearly identified this strategy as they brought out ThinFab and popularized the
3448 concept of Think Thin. The strategy provides higher stabilized module power, and
3449 significantly increases the throughput using thin cells. The 2nd generation ThinFab
3450 (ThinFab™140), presented at the World Future Energy Summit 2012, boasts a CAPEX

3451 below $\$1.4/W_p$ (approx. $\$0.97/W_p$ for integrated end-to-end manufacturing line at 140MW).
 3452 This represents a production cost of only $\$0.48/W$, and electricity generation costs of
 3453 $\$0.10/kWh$ [457], while providing a decent efficiency of 10.8%. In fact, a very attractive
 3454 system cost of $\$1.4/W_p$ (ground mounted system) in China has been claimed, which shows
 3455 enormous potential in other (sunny) developing countries such as India, Brazil, South Africa,
 3456 etc. In this context, industries are now looking for new cell designs (and not an incremental
 3457 progress in efficiency) to substantially decrease the tact time.
 3458



3459 Fig.63 Efficiency (initial) and current density per thickness of various one dimensional structured a-Si:H solar
 3460 cells compared to the record stabilized a-Si:H cell [449] on random textured surface. Cell no. 1-9 (9 as reference
 3461 cell) and the corresponding references are mentioned in Table 3. Tandem cell (no. 10 in Table 3) is not
 3462 mentioned in this figure. The cells are electrically thin optically thick. Thickness of the absorber layer is smaller
 3463 than the diffusion length; this ensures collection of carriers at the contacts avoiding recombination. Anti-
 3464 reflection at the top surface and increased absorption due to light trapping in the nanorod arrays result in current
 3465 enhancement. The efficiency is still small compared to standard [449] cells on textured surface, mainly due to
 3466 low V_{oc} and fill factor resulting from non-conformal growth on the nanorods, especially on sidewalls, leading to
 3467 porous regions and shunt paths.
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 3469

3470 Researchers are now responding to that call by introducing extreme thin cells using
3471 the concept of electrically thin optically thick absorber layers. There are essentially two types
3472 of proposed structures, viz. nanorods [524,525,526] and nanoholes [527,528]. In the first
3473 category, a number of reports are now available with different nomenclatures- nanopillar
3474 [529], nanodome [530], nanorod [524], and nanocoax [531] etc. These types of structures
3475 have been made by either top-down or bottom-up approaches. The details of top-
3476 down/bottom-up growth method can be found in Ref. [16] and Sec. 12. The top-down
3477 approach is suitable for c-Si rod cells. Si nanowire solar cells are made by etching of c-Si
3478 substrates by chemicals [532] or plasma (RIE), and a conversion efficiency reaching 10%
3479 [533] has been achieved. However, bottom-up approach with metal induced c-Si nanorod
3480 solar cells have also been demonstrated [534]. For a-Si:H type of cells, on the other hand, a
3481 bottom-up approach is more suitable. Normally a seed layer is used, and the columnar growth
3482 occurs via a combination of mechanisms, viz. preferential direction growth, and growth on a
3483 catalyst seed. A typical catalyst method uses precipitated metal, such as gold induced vapor-
3484 liquid-solid (VLS) growth process [535,536]. In this VLS process, gold film (3-5 nm)
3485 deposited onto c-Si wafer is heated to form Au-Si alloy islands (droplets). When exposed to
3486 source gas (e.g. SiH₄), these islands decompose source gas, and Si diffuses into droplet and
3487 absorbed. After supersaturation, Si precipitates and SiNW grows out of precipitation [16].

3488 Using Sn catalyst, an efficiency of 5.6% has been reported for a radial junction p-i-n
3489 a-Si:H solar cell on p-type c-Si nanowire [537]. Creating such structures directly on the
3490 substrate (such as glass) is an option.

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3501 Table 3 Thin-film Si cells on one dimensional structures. The efficiency of cells on nanoholes or nanorods have
 3502 still not reached the efficiency of cells on standard (~10%) textured surface [449]. However, cells with absorber
 3503 thickness below 100nm, even as small as 25nm are encouraging. This is possible due to flexible structure of
 3504 amorphous material to form homogeneous coating (though still not fully conformal) on these high aspect ratio
 3505 structures. The structures are made either by top-down (etching) or bottom-up (deposition) approaches.
 3506
 3507

Cell No.	Cell type	Substrate	Intrinsic layer thickness (nm)	Source	Current density (mA/cm ²)	Eff. (%)	Ref.
1	n-i-p (a-Si:H)	Nanodome	280	Stanford University, USA	17.5	5.9	[538]
2	n-i-p (a-Si:H)	Nanorod	25	Univ. Utrecht	8.3	3.6	[525]
3	n-i-p (a-Si:H)	Nanocoax	90	Stanford University+Solasta Inc.+EPFL(IMT), Neuchatel	13.9	8.2	[539]
4	n-i-p (a-Si:H)	nanocone	250	Stanford University/EPFL(IMT), Neuchatel/	14.9	9.7	[540]
5	p-i-n (a-Si:H)	nanotube	185	Stanford University, USA	13.5	6.1	[531]
6	p-i-n (a-Si:H)	nanocone	130	IBM T.J. Watson Research Center, USA	12.6	7.6	[541]
7	p-i-n (a-Si:H)	nanorod	300	Carl von Ossietzky University Oldenburg, Germany/University of Bremen, Germany	11.0	6.7	[526]
8	p-i-n (a-Si:H)	Plasmonic nanoprnt	90	Univ. Utrecht/AMOLF	16.94	9.6	[542]
9	p-i-n (a-Si:H) (Reference cell)	Random textured surface	250	EPFL	17.28	10.09	[449]
10	p-i-n Tandem (a-Si:H/nc-Si:H)	Nanohole (Swiss Cheese)	-	Institute of Physics, Prague+Oerlikon Solar-Lab, Switzerland	10.0	10.3	[528]

3508

3509 Table 3 shows the performance of these one dimensional (1D) cells from different
 3510 laboratories. Figure 63 shows the current density and efficiency per thickness of such cells
 3511 compared to that in a standard cell structure [449]. The expected high stability of these cells

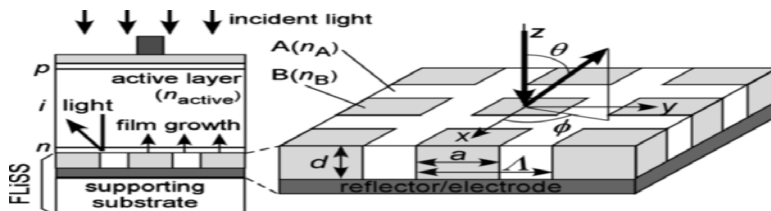
3512 against light soaking has, however, not been demonstrated yet and making conformal growth
 3513 on such 1D structure remains a technological challenge.

3514 7.6.2 Flat cells

3515 In order to improve light trapping without macro or microscopic textures that generally
 3516 lead to defects in the layers grown on them, electrically flat optically rough surfaces have
 3517 been developed [543]. Flat cells employing a structure of mixed materials of different
 3518 refractive indices, called flattened light-scattering substrate (FLiSS), have been demonstrated
 3519 [544] in a nc-Si:H cell (Fig.64). The efficiency obtained for a nc-Si:H cell on FLiSS is
 3520 comparable to that on a textured surface (efficiency $\sim 8\%$), however, the V_{oc} and FF are
 3521 substantially improved. Further improvement in FLiSS is needed to enhance the current to
 3522 make it comparable or higher than that is obtained on textured surface.

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3527 Fig.64 Schematic of a FLiSS (flattened light-scattering substrate or FLiSS) solar cell structure demonstrated in
 3528 a nc-Si:H cell [544]. In this type of cells, mixed materials with different refractive indices are used. The
 3529 substrate is a flattened light-scattering substrate, with a high reflective index contrast consisting of two
 3530 dimensional ZnO grating filled with n-a-Si:H. For a nc-Si:H cell, the FLiSS structure provides substantial
 3531 improvement in the infrared region (almost comparable to textured surface), while maintaining high V_{oc} and fill
 3532 factor, which can be obtained only on flat surfaces. With permission from [544], H. Sai, Y. Kanamori, and M.
 3533 Kondo, Flattened light-scattering substrate in thin-film Si solar cells for improved infrared response, Appl. Phys.
 3534 Lett. 98 (2011) 113502. Copyright © 2011 American Institute of Physics. License number 3513100577119.

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3536 7.7 Industrial competitiveness

3537 One of the industrial successes of a-Si:H is large-scale displays, especially in the
 3538 1990s when Si based thin-film PV was in an initial phase. The processing technologies of
 3539 these large area devices on glass substrates, and the roll-to-roll fabrication on flexible foils
 3540 have been the main arguments in favor of thin-film Si PV. Applied Materials' SunFab with

3541 5.7m² substrate was rolled out to many factories - Moser Baer in India, Signet Solar and
3542 SunFilm in Germany, Masdar Solar in UAE, T-Solar in Spain, Best Solar in China and Green
3543 Energy Technology in Taiwan. The strategy was that large glass would mean faster
3544 throughput, with fewer pieces delivering the same capacity, lowering the cost per watt,
3545 installation costs and BOS savings. As per experience from LCD-display industry, Applied
3546 Materials had seen that every time the glass grew larger, the industry was able to cut costs
3547 dramatically. However this strategy turned out to be a mistake for PV. A SunFab factory
3548 costs about 30% more than standard solar manufacturing equipment- \$80 million to \$160
3549 million price tag for a single line. Glass this large is hard to handle, and few equipment
3550 manufacturers had tools that could deal with it. Signet, Sunfilm, Green Energy Technology
3551 and T-solar became bankrupt. Most SunFab owners ended up selling largely ¼ sized panels
3552 that were the same size as typical solar panels. In contrast, the competitor, Oerlikon company
3553 was more successful, selling a robust technology on an easily processable substrate (1.4 m²),
3554 and a high-efficiency double-junction cell processing at a high growth rate, due to its VHF
3555 technology. However, in the meantime TEL Solar has discontinued the solar business since
3556 2014 and many of industries with TEL Solar/Oerlikon equipments have applied for
3557 insolvency- GADIR Solar, S.A in Spain, Pramac in Switzerland (30MW end-to-end turnkey
3558 line), Inventux in Germany, Auria Solar in Taiwan, Schuco Solar in Germany (Oerlikon and
3559 Applied Material SunFab) and Bosch Solar in Germany (30MW).

3560 Roll-to-roll (R2R) technology on flexible substrates has so far shown the best
3561 promise. However it faces stiff commercial and technological challenges. A lower CAPEX,
3562 high-throughput, and simple processing are needed, particularly for low-cost encapsulation
3563 that should have the moisture barrier property comparable to that of glass. Recent reports
3564 show that using a multilayer of inorganic and organic materials made by same hot-wire CVD
3565 technique results in a water vapor transmission rate of 5×10^{-6} g/m²/day at a temperature of

3566 60°C and a relative humidity of 90%, which will increase the life time of PV to >30 years
3567 [545]. Nuon (the technology previously owned by Akzo Nobel) had to abandon their
3568 indigenously developed R2R technology (Helianthos concept) as it could not commercialize
3569 the product and the new owner of this technology HyET Solar is precisely putting its effort to
3570 make the technology cost-effective.

3571 Though thin-film Si PV manufacturing is currently passing through a trying phase, the
3572 processing has matured, and fast multi-GW large-scale manufacturing is possible once the
3573 bubble of low priced c-Si sector has deflated. Moreover, the problem of light induced
3574 degradation that bothered the industries and investors, has been largely overcome. Applying
3575 all the new developments, such as thin cells, stable materials, and multi-junction, a
3576 degradation of as low as around 4% has been achieved by Unisolar [502].

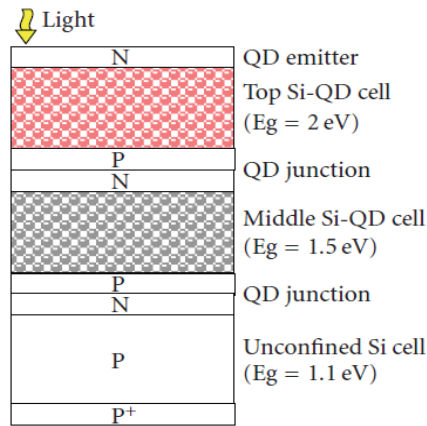
3577 **7.8 Looking towards future: Bridge to third generation PV**

3578 In order to cross the S-Q limit of solar cell efficiency, several third generation PV
3579 concepts, most of which are still in conceptual phase, have been proposed [546]. The idea is
3580 to increase the efficiency to around 40-60% while keeping the cost of production low by
3581 using thin-films PV fabrication process. A few of these concepts, most relevant to thin-film
3582 Si, are described below.

3583 **7.8.1 Hot Carriers**

3584 The importance of thin absorber layer in PV cost reduction was discussed in Sec.
3585 7.6.1. One more advantage of this structure is the ability to use a third generation concept of
3586 tapping the hot carriers before they thermalize, which is caused by phonon interaction in the
3587 lattice. This process can substantially increase the V_{oc} . The underlying principle of this type
3588 of solar cell is to slow down the rate of relaxation of photoexcited carriers, which is achieved
3589 by a quantum dot (QD) Si absorber layer, to allow time for carriers to be collected while they
3590 are still at high energies. The collection of carriers is through a selective (narrow) energy

3591 contact, which can be achieved by single (doped) layer of Si QD providing the resonant level
 3592 through which carriers can tunnel. A theoretical efficiency of 65% under 1 sun can be
 3593 achieved by this solar cell design.



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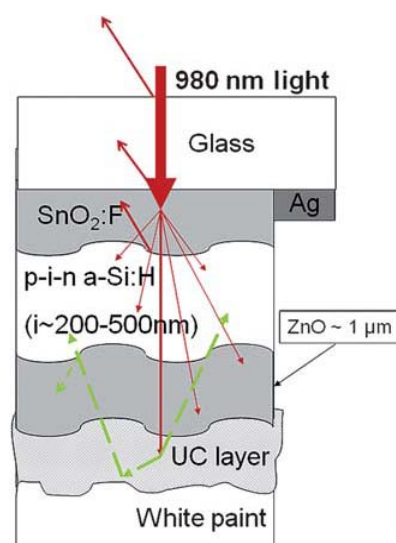
3596 Fig.65 Schematic diagram of proposed quantum dot triple-junction solar cell [547]. The doped layers can be
 3597 standard amorphous and microcrystalline thin-films. The Si quantum dot layers can be made either by
 3598 deposition of nanoparticles from gas phase by various PECVD processes, or by annealing (solid phase
 3599 crystallization) of amorphous materials ($a\text{-SiC}_x$, SiN , $a\text{-SiO}_x$) at high temperature. Monodispersed (<5% size
 3600 distribution) Si nanoparticles of size less than the Bohr's radius (5nm) are embedded in an amorphous matrix
 3601 (which acts as a passivation layer in addition to its role in quantum confinement) with spacings that allow
 3602 current tunneling. Fully quantum dot cells can be made by using SiGe quantum dot, instead of the conventional
 3603 c-Si wafer as the bottom cell. Bandgap is varied by tuning the quantum dot size. Reprinted with permission from
 3604 [539], G. Conibeer, Si and Other Group IV Quantum Dot Based Materials for Tandem Solar Cells, Energy
 3605 Procedia 15 (2012) 200. Copyright © 2014 Elsevier B.V. License number 3513101114061.

3606

3607 7.8.2 Quantum dots

3608 One very promising outcome of the thin-film Si research is the material in which
 3609 nanocrystallites are embedded in an amorphous matrix with 50% crystalline volume fraction
 3610 that leads to high-efficiency nc-Si:H solar cells. This trend can be developed further by
 3611 shrinking the size of the nanoparticles, below the Bohr's radius, and thereby using quantum
 3612 confinement. The resulting QD will be a milestone for third generation solar cells where the
 3613 various properties of QDs such as decoupling of the electronic states from lattice, discrete
 3614 electronic states, direct bandgap nature of light absorption, tuning the bandgap and absorption
 3615 profile by tuning the particle size can be exploited. Though a multi-junction structure has
 3616 been proposed in the third generation concept, this has been used for thin-film Si over a long
 3617 time; in labs and commercial companies triple-junctions using a-Si:H, a-SiGe:H and nc-Si:H

3618 have been made. However, even in lab scale the efficiency has not reached the S-Q limit. It is
 3619 expected that the QDs are internally defect free and their surfaces can be passivated using
 3620 appropriate shell or embedding in a passivating matrix. This way, bandgap variations can be
 3621 made (by appropriate dot size) without increase of defects, which is encountered when
 3622 changing bandgap with alloying such as a-SiGe or a-SiC. Figure 65 shows the schematic of a
 3623 triple-junction based on QD layers. A theoretical efficiency of 47.5% for such a cell is
 3624 expected [546]. Notwithstanding the advantages, the reports so far on solar cell devices with
 3625 QDs have not proved their potential. A c-Si/QD-Si heterojunction cell has shown a
 3626 reasonable V_{oc} of 0.52V, but a very low fill factor of 0.2. QD superlattice as intrinsic layer in
 3627 an n-i-p cell has shown an efficiency of 3.8% with V_{oc} , fill factor and J_{sc} of 518mV, 0.51 and
 3628 14.3 mA/cm², respectively [548]. One of the causes behind the bad performance (in both c-
 3629 Si/QD-Si heterojunction and QD superlattice as intrinsic layer in an n-i-p cell) is that in
 3630 phosphorous-doped QD, the structural distortion is less significant than that for boron-doped
 3631 case [549], and phosphorous-doping significantly increases the QD size compared to boron-
 3632 doping [547]. Defect passivation of the QDs is still an open question. Si QDs have also been
 3633 employed in QD sensitized solar cells whose theoretical efficiency is 44% [550].



3634

3635 Fig.66 Schematic diagram of a single-junction a-Si:H cell with upconversion layer [551]. The TCO layers have
 3636 to be highly transparent for near-infrared photons (lowly doped), highly conductive (high mobility) and thick to
 3637 minimize resistance losses. A non-conducting diffuse back reflector (white paint or foil) instead of Ag is used.
 3638 Upconverter powders (e.g. NaYF₄: 2% Er³⁺, 18% Yb³⁺, dissolved in chloroform with Poly(methyl

3639 methacrylate)) can be drop casted on the back contact. A high bandgap layer with small sub-bandgap absorption
3640 is the most suitable absorber (intrinsic layer) for upconversion cell. This concept is more suitable for high
3641 bandgap absorber materials. Sub-bandgap photons are transmitted through the high bandgap absorber material
3642 used in the cell, and are not utilized for electron-hole pair creation. In upconversion process, two below bandgap
3643 energy photons (transmitted through the cell) are added by the upconversion layer and converted to a single
3644 photon with higher energy and then reflected back to the bulk of the cell for absorption [15].
3645

3646 **7.8.3 Up conversion**

3647 Light spectrum below the bandgap is lost in a solar cell and this long wavelength
3648 spectrum can be converted to above bandgap, thereby utilizing a part of the unused light.
3649 This third generation concept will be most useful for high bandgap absorber materials where
3650 there is a substantial transmission loss, and a-Si:H, especially the pc-Si:H type cell, is a test
3651 case because of its high bandgap of 1.8-2.0eV [551] (Fig. 66). Using lanthanide type up-
3652 converter materials, up-conversions have been achieved for broad band light. However, for a
3653 realistic improvement, a concentrated light of ~500 suns is needed. Use of up-conversion
3654 based on sensitized triplet-triplet-annihilation in organic molecules at the back side of a-Si:H
3655 cell has shown 1% increase in efficiency at 48 suns illumination [552]. However, a solid state
3656 material by a deposition technique is most desirable. One of the solutions to capture a wide
3657 spectrum by a broad band absorption can be achieved by using quantum dot sensitizers or
3658 transition metal ions, which emit at the resonance energy of the up-converter. The latter
3659 (transition metal ions) is yet to be experimentally successfully demonstrated, but the former
3660 has shown promise; QDs absorb over a broad spectral range in the IR, and emit in a narrow
3661 line, e.g. around 1520 nm, resonant with the Er^{3+} upconversion wavelength to which it makes
3662 a radiative transfer [553]. Use of plasmonic structure to either increase the absorption
3663 strength or emission has also been proposed and has also been shown as proof of concept.
3664 One more technique is to use nanofocussing to achieve the light concentration. This can be
3665 done externally using nanolenses, or internally through nanofocussing at a tapered metallic
3666 structure at its edge [554].

3667

3668 **7.9 Future outlook**

3669 Thin-film Si based PV technology, like all other thin-film technologies, will continue
3670 to face commercial pressure from Si wafer based PV for some time to come and will mostly
3671 cater to the niche market. These include small power sources in consumable goods, in
3672 addition to a dedicated market in building integration, thanks to its aesthetics. Once the
3673 dominance of c-Si PV eases, thin-film Si PV technology market is expected to expand
3674 rapidly, as this is the most matured and robust technology positioned to upscale. Gigawatt
3675 level production is possible with its technology with relatively small effort. In this regard, the
3676 large display size solar panels and long rollable modules will be preferred choices because of
3677 the maturity of the fabrication process and technology.

3678 As far as absorber material is concerned, a new direction on deposition/fabrication is
3679 needed. At present, the stabilized efficiency of single-junction cells, whether a-Si:H or nc-
3680 Si:H, is far below (less than half the S-Q limit) the theoretical optimum efficiencies for the
3681 respective band gaps. The stabilized efficiencies of even triple-junction cells are around one
3682 third of the theoretical efficiency of multi-junction. However, considering the enormous room
3683 for improvements in defect density, mobility, etc., considerable scientific interest remains for
3684 long-term efforts. Production of nanowires and quantum dots will be of enormous scientific
3685 interest, however, multi-junction solar cells based on quantum dots, notwithstanding their
3686 potential for high-efficiency beyond S-Q limit, will remain academic for some time to come,
3687 just as other third generation concepts.

3688 In terms of industrial production, a-Si:H will remain central to SHJ type solar cells.
3689 However, as far as pure thin-film Si PV is concerned, there are challenges ahead. There are
3690 ongoing efforts on implementing these type of cells along with others to fabricate parallel
3691 connected (e.g. two terminal devices with optical couplers or honeymoon cells) devices. The
3692 previous decade had experienced great success in developing the passive parts of thin-film Si

3693 cells, especially optical management and light trapping effects, which included nano-textured
3694 surfaces, nanowall/nanopillars and plasmonic effects. Many of these were developed by
3695 groups specializing in optical studies, not necessarily experts in solar cells and device
3696 fabrication. The knowhow of many of these effects is currently being incorporated in solar
3697 cells. Industrial fabrication processes implementing these optical enhancing effects may soon
3698 be developed. This will be the best possible way to increase stabilized cell efficiency to 15%,
3699 which will make the thin-film Si based PV truly industrially competitive. The solar cells on
3700 flexible foils, especially plastics, still remain one of the most fascinating inventions in thin
3701 film silicon based solar cells. It is to be seen how low-cost encapsulating moisture barrier
3702 layers develops in near future to make the plastic solar cells a real success, opening up
3703 applications in wide ranging areas, especially large roof tops.

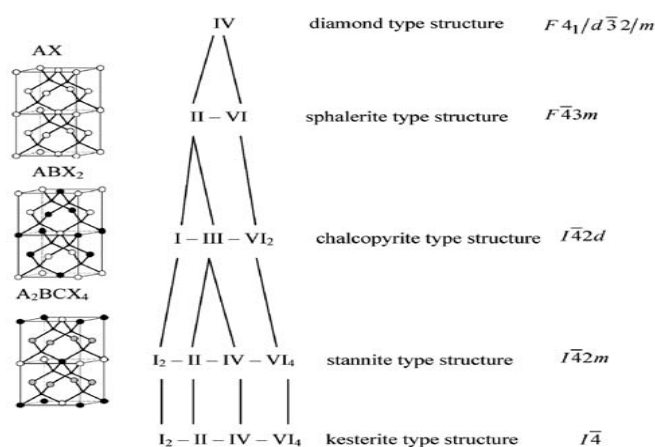
3704 **8.0 CZTSSe (Kesterite) Solar Cells**

3705 The desire for large-scale PV technology based on environmentally friendly, low-cost
3706 absorber compatible with high-throughput fabrication has resulted in an increased research
3707 interest in the kesterite-type $\text{Cu}_2\text{ZnSn}(\text{S},\text{Se})_4$ systems known as CZTS (or CZTSSe in some
3708 cases when Se is present). With similar optoelectronic properties to high-efficiency CIGS and
3709 CdTe materials, and at the same time devoid of highly toxic (such as Cd) and high-demand
3710 rare elements (such as indium), this material has produced solar cells with steadily increasing
3711 efficiency during the recent years [555]. Remarkably, CZTSSe progress has been accelerated
3712 by chemical ink-based approaches surpassing in performance classical high-vacuum
3713 techniques and pushing the efficiency record of these materials by about 1 absolute % per
3714 year up to its current level of 12.6% [556-559]. The combination of these advantages
3715 together with a huge potential for improvement has motivated an expanding volume of
3716 studies, ranging from kesterite synthesis to advanced materials and device modeling. A
3717 number of detailed works have already provided exhaustive coverage of the significant body

3718 of literature on the subject [555,560,561]. Here we will focus on the key aspects of CZTSSe
 3719 material and device developments during the recent years, analyzing the main challenges
 3720 ahead of currently one of the most tempting and complex PV absorber materials.

3721 8.1 CZTSSe materials

3722 Copper zinc tin sulfide ($\text{Cu}_2\text{ZnSnS}_4$) was conceived in the 1980s as a promising PV
 3723 material to provide alternative to indium-based chalcopyrites such as CuInSe_2 and later
 3724 $\text{Cu}(\text{In,Ga})(\text{S,Se})_2$ that at the time were reaching 11% efficiencies, close to the 2013 efficiency
 3725 values of CZTSSe devices [562]. The material comprises a next level of evolution of the
 3726 adamantine (i.e. diamond-like) family of analogous structures where 4-valence atoms are
 3727 consecutively substituted with isoelectronic combinations of growing complexity, for
 3728 example [563], carbon (or Si) \rightarrow ZnS \rightarrow CuInS₂ \rightarrow CuZnSnS₄ (Fig.67). The substitution of
 3729 indium (III valence) in the chalcopyrite with Zn (II valence) and Sn (IV valence) in kesterite
 3730 results in very similar optoelectronic properties – i.e. high absorption co-efficient due to
 3731 direct bandgap, tunable from approximately 1eV to 1.5eV with varying S/Se ratio, the lowest
 3732 values corresponding to pure selenide and the highest to pure sulfide materials.



3733
 3734 Fig. 67 Schematic diagram of a part of the adamantine compound family, including kesterite materials.
 3735 Isoelectronic combinations of different atoms are substituting Roman numbers indicate the valence state of the
 3736 cations (big spheres A,B,C) and anions (small spheres) respectively. The sum of the valences at each step is
 3737 double the sum of the previous. The structure models at the left side are (from top to down) the sphalerite-type
 3738 structure, the chalcopyrite-type structure and the stannite-type structure. CZTS is a kesterite material used as
 3739 absorber in the CZTS solar cell due to its high absorption co-efficient, optimum bandgap of around 1.5eV, and
 3740 its elemental constituents are earth-abundant. Reprinted from Ref. [563], S. Schorr, Structural aspects of

3741 adamantine like multinary chalcogenides, 515 (2007) 5985. Copyright © 2014 Elsevier B.V. Permission
3742 granted. License number 3498551168874.

3743
3744 The dilemma whether to use the classical sulphide or selenide or mixed materials is
3745 similar to that in chalcopyrite technology. On the one hand, sulfur is more benign and orders
3746 of magnitude more Earth-abundant than Se – therefore the natural choice for large-scale
3747 environmentally friendly manufacturing. On the other hand, Se-based materials produce
3748 higher-quality polycrystalline layers and are more tolerant to processing conditions. Neither
3749 long-term availability of Se nor its potential toxicity has yet been viewed as a major limiting
3750 factor for the growth of PV technologies employing it. Se is a largely unused byproduct from
3751 Cu refining and, although harmful in excessive concentrations, is a key micronutrient for
3752 living organisms. An important advantage of mixed sulfoselenide alloys is the ease of
3753 controlling the bandgap from about 1eV (pure selenide) to about 1.5eV (pure sulfide)
3754 analogously to $\text{CuIn}(\text{SSe})_2$. The use of the pentanary $\text{Cu}_2\text{ZnSn}(\text{S,Se})_4$ system allows to take
3755 advantage of the optical and materials quality benefits of the combination of S and Se and has
3756 been employed in the highest-efficiency CZTSSe devices to date [558,559].

3757 The high complexity of the kesterite materials makes them particularly vulnerable to
3758 secondary phase formation – a major challenge for the fabrication of high quality absorbers.
3759 The high temperatures (over 500°C) required for device-quality kesterite film crystallization
3760 [564,565] combined with the high volatility of multiple intermediate species are a serious
3761 challenge [566] for CZTSSe (not only S and Se as in CIGS technology, but also of elemental
3762 Zn and Sn chalcogenide phases). Materials optimization is made even more difficult by the
3763 fact that the two of the most likely secondary phases, viz. $\text{Zn}(\text{S,Se})$ and $\text{Cu}_2\text{Sn}(\text{S,Se})_3$ are
3764 difficult to distinguish by standard characterization techniques such as x-ray diffraction
3765 (XRD) due to peak overlap with the targeted CZTSSe. Raman scattering [567,568] and other
3766 techniques such as neutron diffraction [569] and x-ray absorption near edge structure
3767 [570,571] have been successfully used for phase detection, although there is still a need for

3768 further development of techniques for routine and reliable secondary phases detection in
3769 CZTSSe, especially in the pentanary system.

3770 Some secondary phases can be more detrimental than others. Generally, secondary
3771 phases with bandgaps lower than CZTSSe (for example $\text{Cu}_2\text{Sn}(\text{SSe})_3$, bandgap of 0.8-1eV),
3772 are considered particularly undesirable as they reduce the V_{oc} of the device. It has been
3773 pointed out that the presence of a material with a bandgap lower by only 100meV will reduce
3774 the maximum achievable efficiency by 8% absolute [561]. High-conductivity phases, such as
3775 $\text{Cu}_x(\text{S,Se})$ are especially damaging performance well due to their shunting effect. Similarly to
3776 chalcopyrite PVs employing CIGS or CuInS_2 , they must be avoided by relying on a Cu-poor
3777 absorber or removal techniques such as potassium cyanide (KCN) etch [572,573].

3778 Phases with higher bandgap than CZTSSe are considered less detrimental [561] but
3779 may have negative impact in specific locations – for instance $\text{Zn}(\text{S,Se})$ (bandgap of 2.7-
3780 3.8eV) in the bulk of the film is much less harmful than on the absorber surface [574]. HCl
3781 etch has been successfully applied to remove surface Zn excess leading to improved V_{oc}
3782 [575]. Tin chalcogenides, $\text{Sn}(\text{S,Se})$, may have different impact depending on exact
3783 composition, while SnSe has a relatively high bandgap of 1.3eV and may have little effect on
3784 device performance, SnS has an indirect bandgap of 1eV and can be potentially harmful
3785 [561]. This could be one of the reasons why pure sulphide CZTSSe has lower maximum
3786 efficiency than materials with higher Se content.

3787 All above considerations are in empirical agreement with the currently best strategies
3788 for high-efficiency devices that employ mixed S-Se materials with slightly Zn-rich and Cu-
3789 poor composition [558,559].

3790

3791 **8.2 Fabrication approaches**

3792 Numerous vacuum and non-vacuum CZTSSe fabrication approaches have been
3793 reported [555,556,572,576,577]. One distinguishing property of these materials is Sn-

3794 chalcogenide volatility, especially at high-temperature and in vacuum. This has made direct
3795 process such as co-evaporation at high substrate temperature very difficult to optimize CZTS
3796 films, which was possible with CIGS. Currently, the most successful CZTSSe fabrication
3797 processes are two-step vacuum and non-vacuum deposition techniques where the high-
3798 temperature (over 500°C) crystallization step is done at atmospheric pressure.

3799 The first report on the deposition of CZTSSe films by employing sputtering from
3800 quaternary targets and its use in PV device was performed by Ito and Nakazawa in 1988
3801 [562]. Katagiri et al. [578] employed sputtering from metal targets to systematically study an
3802 extensive matrix of composition and processing parameters. Careful optimization determined
3803 the beneficial Cu-poor, Zn-rich composition, and with the demonstration of 5.75% efficiency
3804 in 2007 [579] that was increased later to 6.8% by simple wet etching technique [555,580],
3805 triggered a rapid growing research interest in CZTSSe PV. Among numerous other reports on
3806 sputtering, the company Solar Frontier has reported the highest efficiency of 9.2% that was
3807 furthermore measured over the total area of a 25cm² mini module [581].

3808 Co-evaporation at high substrate temperature was the technique used for the first time
3809 to demonstrate over 2.3% efficient CZTSSe solar cell in 1997 [566] at the University of
3810 Stuttgart, highlighting for the first time the Sn-loss challenges mentioned above. Fast co-
3811 evaporation helped mitigate this issue and increase the efficiency to 4.1% [582]. Recently the
3812 National Renewable Energy Laboratory team was able to adapt their high-performance CIGS
3813 co-evaporation process to CZTSe, reaching 9.2% efficiency by maintaining temperatures no
3814 higher than 500°C and providing higher Sn flux throughout the whole process [583]. The
3815 same group reported that, similarly to CIGS, Na incorporation in CZTSe has strong impact on
3816 the electronic properties [584]. Successful grading of the composition to create advantageous
3817 bandgap profile similarly to highest performance co-evaporated CIGS has not been reported
3818 yet.

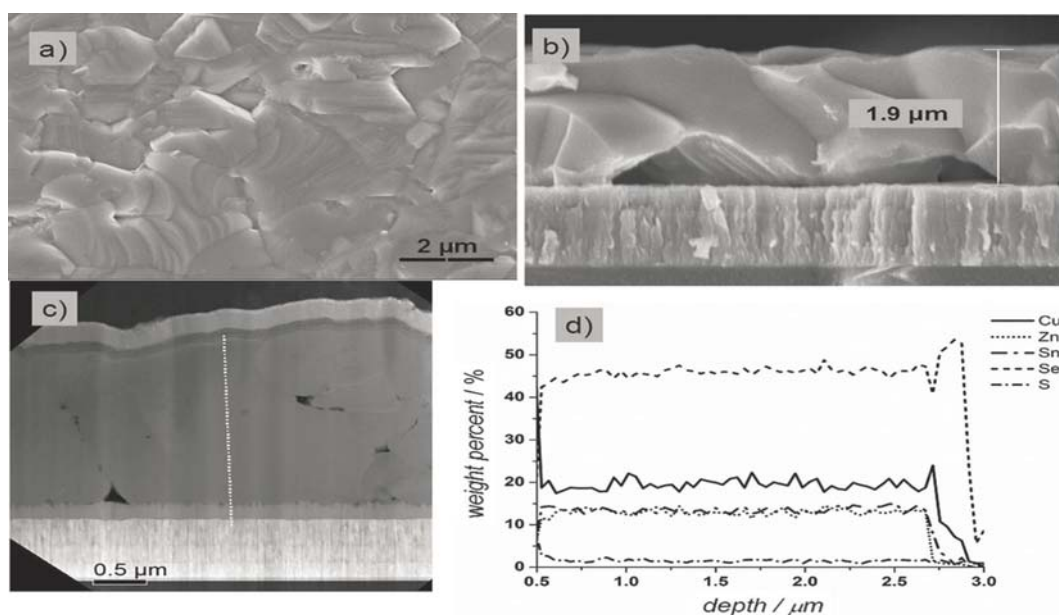
3819 Sequential processes based on evaporation at relatively lower temperature (<200°C)
3820 followed by high-temperature (>500°C) crystallization step have also lead to successful
3821 CZTSSe developments. The first one in this category was reported in 1997 by employing
3822 500°C sulfurization of Zn/Sn/Cu stacks. It yielded 0.66% efficiency [585], which was later
3823 improved to 5.45% by Na incorporation together with optimization of other parameters [586].
3824 The impact of Sn vapor pressure during the high-temperature crystallization step of CZTS
3825 precursors was demonstrated by using sealed-tube anneal with a small amount of Sn source,
3826 where an efficiency of 5.4% was observed [587]. The highest efficiency pure sulfide CZTS
3827 devices were developed at IBM by co-evaporation followed by anneal and have reached 8.4%
3828 [588]. Mixed sulfoselenides by a similar process have demonstrated 8.9% efficiency by use
3829 of TiN diffusion barrier at the back contact [576].

3830 Electrodeposition is a mature industrial non-vacuum deposition technique, attractive
3831 for large-scale CZTSSe manufacturing. Single step and multi-step electrodeposition of
3832 CZTSSe thin-films have been reported [572,573,589,590]. Stacked metal precursor layers,
3833 subjected to sulfurization and KCN etch yielded 3.2% efficiency [572]. Co-electrodeposited
3834 Cu-rich metal precursors, with KCN etching to remove copper sulfide reached 3.4% [573].
3835 IBM process based on electrodeposition of stacked elemental layers with subsequent
3836 sulfurization has reached 7.3% efficiency [590].

3837 Ink-based fabrication processes are compatible with ultrahigh-throughput fabrication
3838 techniques such as printing and casting. Different ink approaches based on solutions,
3839 nanoparticle suspension and mixed solution-nanoparticle slurries could offer unprecedented
3840 scaling potential to CZTSSe.

3841 The first report on nanoparticle CZTSSe deposition involved hot reaction in ethylene
3842 glycol [591]. Guo et al. [592] employed higher-temperature hot injection in oleylamine, and
3843 achieved 7.2% efficient devices. This value was later increased to 8.5% by use of binary zinc

3844 sulphide (ZnS) and ternary copper tin sulphide (Cu_2SnS_3) particles that were subjected to
 3845 selenization [593]. Hybrid solution-nanoparticle slurries in hydrazine based on dissolved Cu-
 3846 Sn-S-Se systems and dispersed Zn-Se phases were developed at IBM, and reached a
 3847 breakthrough 9.66 % efficiency in 2010 [556]. The method was further improved to yield
 3848 10.1% [557] and recently achieved CZTSSe efficiency of 11.1% [558]. Figure 68 shows the
 3849 pinhole-free large-grained microstructure of these materials. The absorber thickness is close
 3850 to 2 μm and the elemental distribution measured by energy-dispersive x-ray spectroscopy
 3851 (EDX) is flat across the film. It must be noted that contrary to CIGS, with CZTSSe no reports
 3852 on successful elemental grading targeting bandgap engineering for enhanced efficiency has
 3853 been reported to date. This however, as will be shown below, is not the main performance-
 3854 limiting factor so far, as efficiencies over 15% [594] have been achieved with CIGS even
 3855 with flat elemental profiles.



3856

3857 Fig. 68 Record efficiency of 11.1% [558] CZTSSe device: (a) SEM top-view, (b) cross-section, (c) TEM cross -
 3858 section, and (d) EDX depth profile. A common feature of high-efficiency kesterite devices is the predominant
 3859 presence of large grains, spanning from the top to the bottom of the film. Voids within the layer and near the
 3860 back contact appear to be benign. Composition profile is relatively flat across the film despite efforts to produce
 3861 gradients for band gap engineering. Figure 68 from [558], Teodor K. Todorov, Jiang Tang, Santanu Bag, Oki
 3862 Gunawan, Tayfun Gokmen, Yu Zhu and David B. Mitzi, Beyond 11% Efficiency: Characteristics of State-of-
 3863 the-Art $\text{Cu}_2\text{ZnSn}(\text{S},\text{Se})_4$ Solar Cells, *Advanced Energy Materials*, 3 (2013) 34. Copyright © 2013 WILEY-VCH

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3865 License number 3498550541225.

3866
3867 Pure solution inks potentially have advantages for uniform synthesis of multinary
3868 compound layers over particle-containing systems due to greater homogeneity at a molecular
3869 scale, as well as reduced probability for aggregate formation causing coating defects. Pure
3870 solutions of metal salts and thiourea in dimethyl sulfoxide have been used to achieve 4.1%
3871 efficient devices [595]. CO₂ solutions in hydrazine (forming hydrazinocarboxylic acid) were
3872 successfully used to dissolve Zn species in hydrazine-based inks, yielding 8.1% efficient
3873 devices [593]. Another pure solution approach for hydrazine systems based on substitution of
3874 elemental Zn with Zn salts was developed with reported efficiency of 10.6% [596].

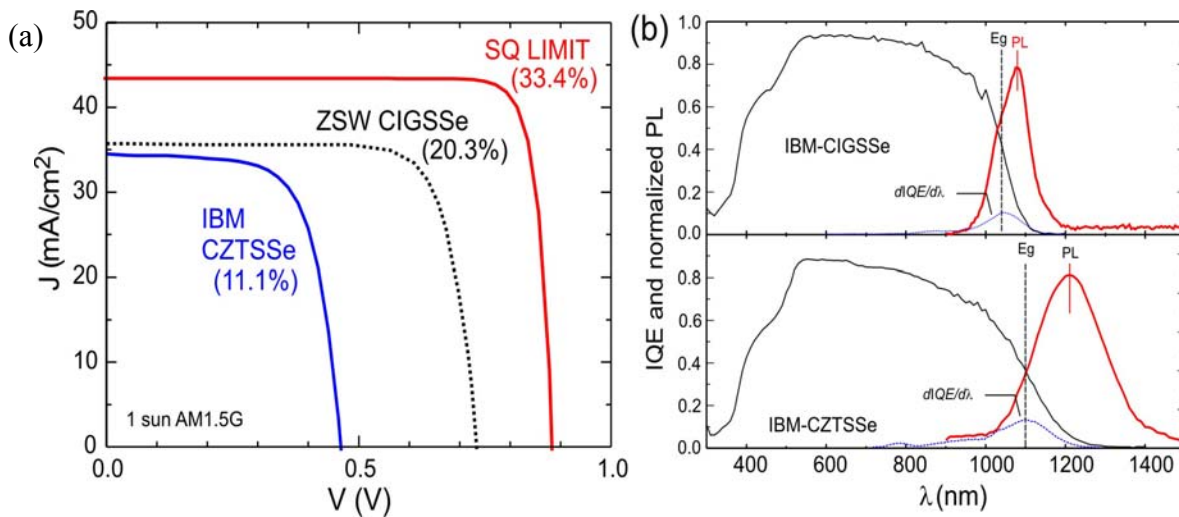
3875 **8.3 Device Characteristics**

3876 Here, we review device characteristics of the high performing CZTSSe cell and
3877 benchmark it against the high performing CIGSSe cells, as well as a hypothetical S-Q single-
3878 junction solar cell (S-Q limit cell) to understand the key problems in the current generation of
3879 CZTSSe cell. We will discuss the general device characteristics of CZTSSe (Sec.8.3.1),
3880 including the V_{oc} deficit issue (Sec. 8.3.2), which is among the leading challenges facing
3881 CZTSSe technology.

3882 **8.3.1 Electrical Characteristics**

3884 Figure 69 shows the (a) J-V curve, (b) IQE and photoluminescence (PL) spectra of
3885 CZTSSe and CIGSSe solar cells. Table 4 shows the J-V characteristics of an example of
3886 leading CZTSSe (IBM-CZTSSe) device with efficiency of 11.1% [558], the leading CIGSSe
3887 cell (20.3% efficiency) from Zentrum für Sonnenenergie-und Wasserstoff-Forschung (ZSW),
3888 Germany [597] and the S-Q limit cell with the same bandgap (1.13eV) (similar discussions
3889 will also apply to the current CZTSSe record efficiency of 12.6%). This S-Q limit cell
3890 presents the ultimate limit of a single-junction solar cell based on S-Q limit calculation

3891 [22,598]. In Table 4, we also present electrical characteristics of a high performance CIGSSe
 3892 cell (IBM-CIGSSe) with 15.2% efficiency made by analogous hydrazine-based processing
 3893 [594]. The bandgap in these cells are determined from the inflection point (i.e. the maxima of
 3894 $|dQE/d\lambda|$ curve) of the QE curve near the bandgap cut-off wavelength [599]. In order to
 3895 perform a fair comparison of J_{sc} and V_{oc} among these cells with little variation in bandgap,
 3896 V_{oc} deficit value, i.e. $V_{oc, def} = E_g/q - V_{oc}$ and normalized J_{sc} value, i.e., $J_{sc,N} = J_{sc}/J_{sc, MAX}$
 3897 where $J_{sc, MAX}$ is the J_{sc} of an S-Q limit cell or the maximum J_{sc} assuming a 100% EQE, are
 3898 monitored.



3899

3900 Fig. 69 (a) J-V characteristics of IBM-CZTSSe, ZSW-CIGSSe leading cells, and a S-Q limit cell with similar
 3901 bandgap (1.13 eV). The S-Q limit is calculated for a single-junction cell with AM1.5G illumination. (b) internal
 3902 quantum efficiency and the photoluminescence spectra (red curve) at room temperature of the 11.1% IBM-
 3903 CZTSSe [558] and the 15.2% IBM-CIGSSe cells [594]. The bandgap (marked as E_g) is determined from the
 3904 inflection point (or the maximum slope) of the external quantum efficiency curve. Fig. 69 (b) reproduced from
 3905 Ref. [600], Tayfun Gokmen, Oki Gunawan, Teodor K. Todorov and David B. Mitzi, Band tailing and efficiency
 3906 limitation in kesterite solar cells, Appl. Phys. Lett. 103 (2013) 103506. Copyright © 2013 AIP Publishing LLC.
 3907 Permission granted.

3908

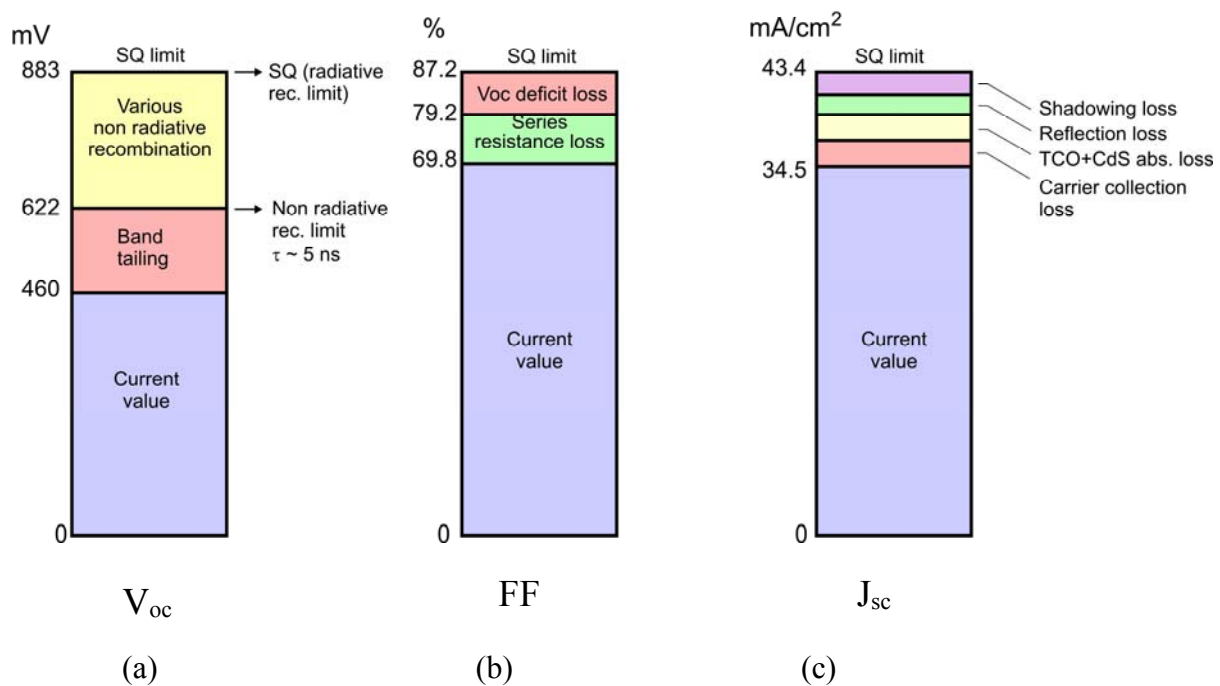
3909 Table 4. Device performance of leading CZTSSe and CIGSSe (from IBM and ZSW respectively) based solar
 3910 cells. The parameters R_{SL} , A , and J_0 respectively are series resistance under light, diode ideality factor and
 3911 reverse saturation current determined using Sites' method [601]. $J_{sc,N}$ and $V_{oc,def}$ are normalized J_{sc} and V_{oc}
 3912 deficit, respectively (see text).

3913

3914

Solar cell	V_{oc} (V)	J_{sc} (mA/cm ²)	Fill factor	Eff. (%)	E_g (eV)	$J_{sc,N}$ (%)	$V_{oc,def}$ (V)	R_{SL} (Ω)	Area (cm ²)	J_0 (mA/cm ²)	Ref.
IBM-CZTSSe	0.460	34.5	69.8	11.1	1.13	79.5	0.670	0.40-0.60	1.48	1.34×10^{-4}	[558]
IBM-CIGSSe	0.623	32.6	75.0	15.2	1.16	78.2	0.547	0.75	1.49	9.8×10^{-6}	[594]
ZSW-CIGSSe	0.730	35.7	77.7	20.3	1.14	83.2	0.410	0.23	1.38	4.2×10^{-8}	[597]
SQ 1.13 eV	0.883	43.4	87.2	33.4	1.13	100	0.247	0	1	4.55×10^{-14}	-

3915



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3919 Fig. 70 breakdown analysis of various loss mechanisms diagram of the 11.1 % CZTSSe cell [558] benchmarked
 3920 against S-Q limit: (a) V_{oc} , (b) fill factor (FF), and (c) J_{sc} . V_{oc} deficit is the number one problem in CZTSSe
 3921 technology and is mainly attributed to various non-radiative recombination, interface recombination, bulk
 3922 recombination, back contact recombination and band tailing. The second dominant factor is the fill factor loss
 3923 attributed to the V_{oc} loss, and series resistance losses from various sources such as metal contact resistance, bulk
 3924 resistance, potential barrier across the contact, and grain boundaries. For higher bandgap or higher [S]/[Se] ratio,
 3925 series resistance tends to increase. The last and least loss factor is the J_{sc} loss which is attributed to the common
 3926 loss factors in thin film solar cells.

3927 We have performed a more detailed breakdown analysis of various loss mechanisms

3928 for the IBM-CZTSSe cell in the frame work of S-Q limit as shown in Fig. 70. The leading

3929 CZTSSe cell has V_{oc} at 52.1%, fill factor at 80.0% and J_{sc} at 79.5% of the S-Q limit cell. It is
 3930 clear that the V_{oc} deficit (Fig. 70 (a)) is the number one problem in the current generation
 3931 CZTSSe. We will discuss factors that account for this V_{oc} deficit in more detail in later
 3932 section.

3933 Second issue is the shortcoming of fill factor. A majority of the fill factor loss is due
 3934 to various sources of series resistances (Fig. 70b) that accounts for 9.4 % absolute from the of
 3935 S-Q limit fill factor such as top metal contact resistance, bulk resistance across the film,
 3936 current blocking secondary phase like ZnS(e) [602] and possible potential barrier
 3937 contribution across back contact or grain boundaries [603]. Note that the CZTSSe series
 3938 resistance tends to increase with higher bandgap, or with higher [S]/[Se] ratio. Overall, the
 3939 series resistance of IBM-CZTSSe is comparable, even slightly better, than the analogous
 3940 hydrazine-processed IBM-CIGSSe device (Table 4). The lowest series resistance ($R_s \sim 0.2\Omega\text{-}$
 3941 cm^2) is found in selenide (no sulfur) kesterite CZTSe cell with lowest bandgap [583,604].

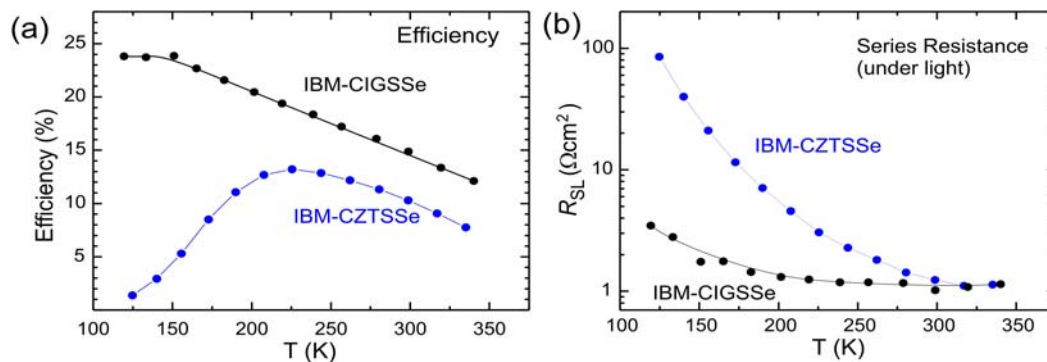
3942 Another contribution of the fill factor losses is accounted by V_{oc} deficit loss [Fig.
 3943 70(b), 8% absolute the maximum fill factor], as low V_{oc} value also inadvertently drags down
 3944 the fill factor. The maximum possible fill factor at a given V_{oc} can be calculated by the
 3945 following phenomenological relationship [605]:

3946 Fill factor = $[V_{OC,N} - \ln(V_{OC,N} + 0.72)] / (V_{OC,N} + 1)$, where $V_{OC,N}$ is the normalized V_{oc} , and
 3947 $V_{OC,N} = qV_{oc} / Ak_B T$, with q is the electronic charge, A is the diode ideality factor, k_B is the
 3948 Boltzmann constant and T is the temperature.

3949 CZTSSe has a dramatically different temperature characteristics at low-temperature
 3950 compared to that of CIGSSe. Figure 71(a) shows that the CZTSSe efficiency collapses at
 3951 low-temperature ($T < 150\text{K}$) while in contrast the CIGSSe cell efficiency keeps increasing.
 3952 The series resistance diverges as much as 100 times from 340K to 120K [603] as shown in

3953 Fig. 71(b). This causes a drastic collapse in fill factor, and correspondingly a decrease in
 3954 observed efficiency [603,606]. This effect is suspected due to dielectric freeze out effect in
 3955 the bulk CZTSSe [607] because of the absence of shallow acceptor in CZTSSe [607,608].
 3956 This is consistent with the theoretical calculation using density functional theory that suggests
 3957 Cu_{Zn} antisite as the dominant, deep acceptor defect in CZTSSe [608,609]. Bandgap
 3958 dependence study indicates that this defect level increases with increasing bandgap or sulfur
 3959 content [607,610]. An alternative view suggests the presence of secondary phase $\text{ZnS}(e)$ at
 3960 the absorber/buffer interface limits the transport across the cell and causes this divergence in
 3961 series resistance [602].

3962 The J_{sc} of IBM-CZTSSe cell is surprisingly very good, with $J_{\text{sc,N}}$ value slightly better
 3963 than that of the IBM-CIGSSe cell. This is most likely a fortuitous effect of the tail states in
 3964 CZTSSe that extend the absorption below the CZTSSe bandgap [600]. The effect of the tail
 3965 states is visible in the QE curve as shown in Fig. 69(b) where we observe more tailing in the
 3966 CZTSSe QE curve around the bandgap cut-off wavelength. Several factors still affect the
 3967 IBM-CZTSSe J_{sc} compared to the S-Q limit J_{sc} . These are shadowing loss of the top metal
 3968 grid, reflection loss mainly from the top stack, absorption loss of the TCO and cadmium
 3969 sulphide (CdS) layer and carrier collection losses in the bulk, which is apparent from lower
 3970 QE response at long wavelength near the bandgap cut-off wavelength. Each of these
 3971 components accounts for about 4-5% loss with respect to the maximum J_{sc} .



3972

3973 Fig. 71 Temperature dependence of (a) efficiency, and (b) series resistance under light condition of the IBM-
 3974 CIGSSe versus IBM-CZTSSe solar cells. The measurement is performed in a liquid nitrogen cooled cryostat
 3975 under simulated 1 sun AM1.5G illumination. CIGSSe cell efficiency keeps increasing even at low-temperature.
 3976 Compared to CIGSSe, at low-temperature, CZTSSe has different temperature characteristics. Cell efficiency
 3977 decreases rapidly at low temperature (<200K) which is related to the divergence in series resistance and drastic
 3978 decrease in fill factor. This effect is attributed to the freeze-out effect in the CZTSSe absorber film due to the
 3979 loss of free carrier at low-temperature which can be attributed to the deep acceptor level in CZTSSe. As can be
 3980 seen in (b), CZTSSe series resistance diverges about 100 times from 340K to 120K.

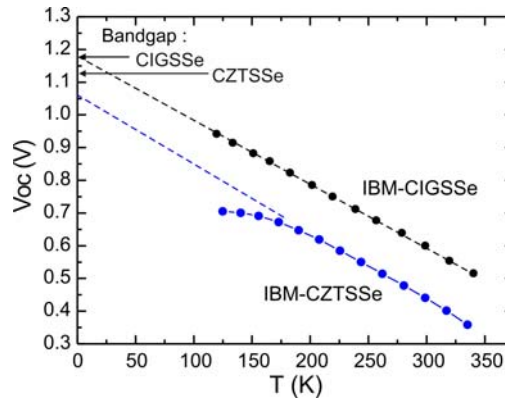
3981

3982 **8.3.2 The V_{oc} deficit in CZTSSe**

3983 The high V_{oc} deficit ($V_{oc,def} = (E_g/q) - V_{oc}$) is among the biggest challenges facing
 3984 CZTSSe-based solar cell, and thus merits a special discussion. Several factors account for
 3985 severe V_{oc} deficit in CZTSSe solar cell. They can be categorized into two major loss
 3986 components as shown in Fig. 70(a): (i) non-radiative recombination, and (ii) band tailing
 3987 effect.

3988 The majority of the V_{oc} deficit loss is accounted for by non-radiative recombination
 3989 (~25% of S-Q limit V_{oc}). Several factors contribute to this loss components, such as interface
 3990 recombination (that may also induce Fermi level pinning at the interface) and bulk
 3991 recombination due to electrically active defects and back contact recombination.

3992 We study the V_{oc} versus temperature characteristics of the CIGSSe and CZTSSe, as
 3993 shown in Fig. 72. The activation energy of the dominant recombination process can be
 3994 obtained (assuming a constant diode ideality factor) from the intercept of the V_{oc} versus T
 3995 extrapolation line at 0K [603,611]. The IBM-CIGSSe cell has activation energy equal to the
 3996 bandgap, as expected for a very good solar cell. However, the activation energy for CZTSSe
 3997 falls short of its bandgap value. This behavior can be accounted by the two V_{oc} deficit factors
 3998 discussed above: (i) non-radiative interface recombination and its consequent Fermi level
 3999 pinning behavior, and (ii) the effect of tail states that artificially lowers the bandgap of
 4000 CZTSSe thus lowering activation energy [600].



4001

4002 Fig. 72 Temperature dependence of V_{oc} for IBM-CIGSSe and IBM-CZTSSe solar cells. The intercept of the
 4003 (extrapolated line at 0K) V_{oc} versus temperature plot at 0K is the activation energy of the dominant
 4004 recombination process. Activation energy is equal to the bandgap for the CIGSSe cell (and other ideal solar
 4005 cells) while for CZTSSe activation energy is smaller than its bandgap. This is attributed to dominant non-
 4006 radiative interface recombination, Fermi level pinning, and tail states that effectively reduces CZTSSe bandgap
 4007 and activation energy.

4008

4009

4010 There are several possible sources of severe interface recombination in CZTSSe solar
 4011 cells, such as defective buffer-absorber interface or secondary phases like ZnS(e) [561] at the
 4012 interface. Another possible source is a cliff-like band alignment where the conduction band of
 4013 the CdS is lower than the absorber layer [612]. However an ultraviolet-photoelectron
 4014 spectroscopy study on CZTSSe reveals the opposite, i.e. a spike-like band alignment in
 4015 CZTSSe solar cell across all bandgap [613]. Separate study suggests that high bandgap (or
 4016 full sulfur) CZTS has a cliff-like band alignment [614]. The discrepancy to earlier study
 4017 [613] is suspected due to variation in sample preparation.

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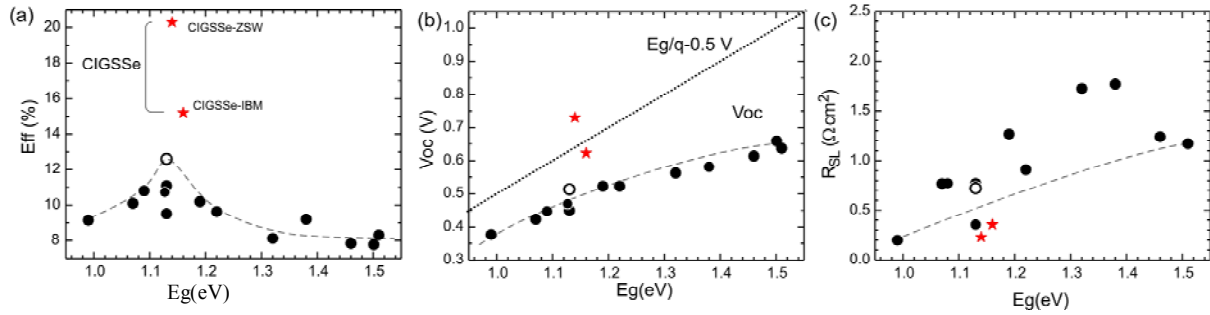
4019 The second major factor that contributes to the V_{oc} deficit in CZTSSe solar cell is the
 4020 tail states that arise from electrostatic potential fluctuations induced by high concentration of
 4021 native defects and strong compensation [600,615,616]. Temperature dependence study of
 4022 time-resolved PL [676] and laser intensity dependence study [616] provide evidence that
 4023 supports this potential fluctuation model. A thorough theoretical study by Chen et al.
 4024 [617,618] on CZTSSe absorber revealed several major features in the electronics properties
 of CZTSSe, such as strong phase competition between the kesterites and secondary
 compounds, intrinsic p-type conductivity due to Cu_{Zn} antisite, Cu vacancies and existence of

4025 charge-compensated defect clusters such as $[2\text{Cu}_{\text{Zn}} + \text{Sn}_{\text{Zn}}]$, $[\text{V}_{\text{Cu}} + \text{Zn}_{\text{Cu}}]$ and $[\text{Zn}_{\text{Sn}} + 2\text{Zn}_{\text{Cu}}]$.
4026 These defect clusters contribute to the severe potential fluctuation in CZTSSe.

4027 One evidence of the tail states effect in CZTSSe can be observed from the weak tail of
4028 the QE curve near the bandgap cut-off as shown in Fig. 69(b). Another evidence is found in
4029 the PL characteristics as shown in Fig. 69(b). CZTSSe PL peak occurs at lower energy values
4030 than its bandgap [561,600]. In contrast, the PL peak of CIGSSe is close to its bandgap values
4031 as expected for a high quality material [600]. This suggests that these tail states artificially
4032 lower the CZTSSe bandgap, thus in effect also lowering the V_{oc} [600]. Furthermore lower
4033 dielectric constant ($\epsilon_r \sim 7-8.5$) [607,619] in CZTSSe (compared to CIGSSe $\epsilon_r \sim 12$) also
4034 causes more severe band tailing effect [600].

4035 The CZTSSe bandgap, which can be controlled by the $[\text{S}]/[\text{Se}]$ ratio, also plays an
4036 important role in the V_{oc} deficit characteristics. We observe an efficiency versus bandgap
4037 profile that peaks around bandgap of 1.15 eV as shown in Fig. 73(a). We found that V_{oc} does
4038 not increase at the same rate as the bandgap [e.g. see $(E_g/q) - 0.5\text{V}$ reference line for
4039 comparison in Fig. 73(b)]. In other words, the V_{oc} deficit gets larger at larger bandgap or at
4040 larger $[\text{S}]/[\text{Se}]$ ratio. Several factors can account for this behavior such as (i) a constant deep
4041 level defect at 0.8eV from the valence band detected by transient photocapacitance study
4042 [620], (ii) electron trapping $[2\text{Cu}_{\text{Zn}}+\text{Sn}_{\text{Zn}}]$ defect clusters that becomes more abundant in
4043 CZTS (full sulfur) [617], and (iii) lower dielectric constant at higher bandgap [619] that leads
4044 to more severe tail states [600], (iv) more severe interface recombination at higher bandgap.

4045 An increasing V_{oc} deficit with bandgap is partly responsible to efficiency profile that
4046 peaks around 1.15eV bandgap as shown Fig. 73(a). Another factor that contributes to this
4047 behavior is increasing series resistance with bandgap [Fig. 73(c)] that lower the fill factor at
4048 high bandgap. Note that analogous effect of increasing V_{oc} deficit and similar optimum
4049 bandgap around 1.15eV have also been observed in CIGSSe [621].



4050
 4051 Fig. 73 Bandgap dependence characteristics of champion CZTSSe (circles) and CIGSSe cells (stars): (a)
 4052 efficiency, (b) V_{oc} and $(E_g/q) - 0.5$ V reference line, and (c) series resistance from light I-V. Empty circles are
 4053 data point for the current CZTSSe champion [559]. Dashed curves are guide to the eye. For CZTSSe solar cell,
 4054 efficiency peaks around 1.15 eV and V_{oc} does not increase at the same rate. V_{oc} deficit becomes higher at higher
 4055 bandgap is due to electron trapping defects, lower dielectric constant at higher bandgap, higher interface
 4056 recombination at higher bandgap and increasing series resistance with bandgap.

4057

4058 8.4 Future direction

4059 Over the past few years CZTSSe PV technology has experienced rapid growth both in
 4060 conversion efficiency and materials understanding. These advances have been achieved by
 4061 the collective effort of an expanding research community interested in this challenging and
 4062 promising multinary material with yet unachieved efficiency potential. Future breakthroughs
 4063 in fabrication strategies are expected to improve phase and electrical uniformity and address
 4064 issues related to the main device limitations. The predominant problem is the V_{oc} deficit,
 4065 which is mainly attributed to the band tail states due to high concentration of native defects
 4066 and strong compensation; and severe non-radiative recombination processes due to bulk
 4067 defects and possible interface recombination. Fortunately these tail states increase the sub-
 4068 bandgap absorption that boosts the J_{sc} and leads to surprisingly good J_{sc} characteristics in
 4069 CZTSSe solar cells on par with CIGSSe. An understanding and control over interface
 4070 recombination and the defects that give rise to the tail states is needed to reduce the V_{oc}
 4071 deficit, and improve the performance of CZTSSe solar cells.

4072 Several approaches can be pursued to reduce the V_{oc} deficit such as:

- 4073 (i) Alternative buffer engineering in attempt to increase the absorber interface quality or to
 4074 alter the bulk property. Recently an $\text{In}_2\text{S}_3/\text{CdS}$ double emitter structure has been shown to

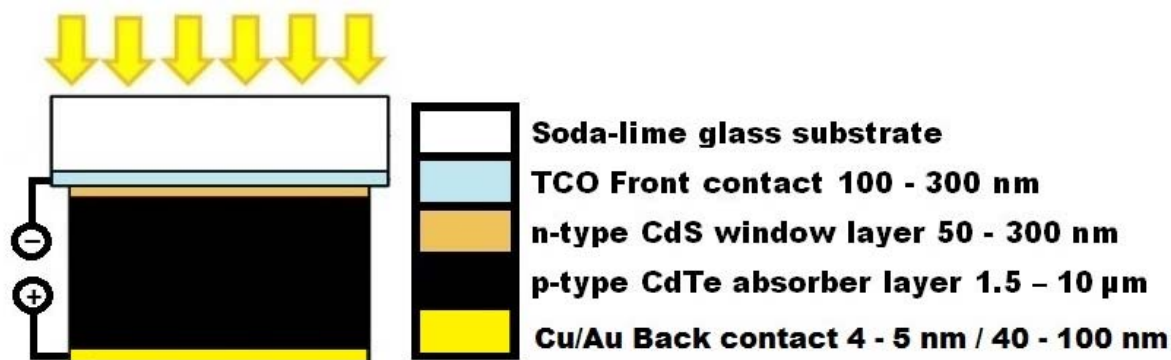
4075 yield a record V_{oc} deficit in lower bandgap CZTSSe [622]. Some of the improvement is
4076 partly attributed to the effectiveness of indium doping to CZTSSe that helps increases the
4077 V_{oc} .

4078 (ii) Focus on low bandgap (selenide) CZTSSe (~ 1.0 eV) to achieve better V_{oc} deficit.

4079 (iii) Effort to minimize the tail states by using alternative elemental substitutions.

4080 **9. Planar thin-film and nanostructured CdTe solar cells**

4081 While the first generation (1G, mainly Si based) solar cell manufacturing and
4082 installation costs are relatively low, the development of second generation (2G) thin-films
4083 polycrystalline solar cells still face higher costs compared to efficiency. Given that c-Si
4084 (commercial wafer thickness $180\mu\text{m}$) based a-Si:H/c-Si solar cells have demonstrated 25.6%
4085 efficiency [484], while planar 2G CdTe solar cells (CdTe thickness $\sim 2\mu\text{m}$) have shown
4086 22.1% efficiency [623,624], there is a scope for extensive research on CdTe based solar cells
4087 to bridge the difference. The schematic diagram of CdTe solar cell is shown in Fig. 74.
4088 Considering that the major barrier for an ultra-large-scale use of solar energy is the high
4089 production cost and low efficiency of the solar cells, one may easily understand the
4090 importance of any investment in strategies to solve these drawbacks. Within this context,
4091 third generation (3G) nanostructured solar cell will play an important role in the future with
4092 the use of new strategies with a competitive efficiency that have been theoretically
4093 understood but experimentally not yet demonstrated.



4094

4095 Fig. 74 Planar (thin-film) CdS/CdTe solar cell. About $1\mu\text{m}$ thick thin-film CdTe (E_g around 1.5 eV) can absorb
 4096 90% of the solar spectrum. In standard process, soda-lime glass or flexible poly(ethylene terephthalate or PET)
 4097 commercial substrate is used. Transparent conductive oxides (TCO) such as tin oxide, indium tin oxide, fluorine
 4098 doped tin oxide and Al-doped zinc oxide are the most widely used materials for the front contact. Window layer
 4099 is deposited over TCO followed by CdTe as absorber layer. Before back contact deposition, cadmium chloride
 4100 (CdCl_2) treatment is essential to improve electronic properties, texture, grain size and hence cell efficiency.
 4101 Also, CdCl_2 treatment reduces lattice mismatch between CdS and CdTe; chlorine compensates native defects in
 4102 the CdTe structure.

4103

4104 In the above context, CdTe is an essential player in general in materials science, and

4105 in particular in the solar cell market, playing an important role both in planar 2G and

4106 nanostructured 3G solar cell where significant efforts are being currently undertaken both for

4107 enhancing efficiency and reducing costs. In fact, CdTe is an ideal absorber where $1\mu\text{m}$ thick

4108 2G solar cell can absorb 90% of the solar spectrum with good conversion efficiency [30,625],

4109 considering a bandgap around 1.5 eV depending on the dopant used. Together with this, the

4110 use of simple and low cost manufacturing process makes CdTe based solar cell an

4111 extraordinary candidate in the photovoltaic field, with the production of commercial 2G

4112 modules of 16.1% efficiency and US \$0.68/W obtained by First Solar [626,627]. This is still

4113 significantly less than the theoretically expected maximum value of 29% for CdTe solar cells

4114 [626]. Recently, an efficiency of 12% has been reported for nanostructured CdS/CdTe solar

4115 cells [628]

4116 In this section the most important results published in the last years are reviewed for

4117 both 2G and 3G CdTe solar cells. After a brief presentation of the CdTe properties, which

4118 makes this material an ideal candidate for absorber, the review is focused on thin-films 2G,
4119 and nanostructured 3G CdTe solar cells.

4120 **9.1 Properties of materials used in CdS/CdTe solar cells**

4121 The materials used as front contact are transparent conductive oxides, i.e. materials
4122 that conduct electricity and also allow the light to pass through them. Tin oxide (SnO₂), ITO,
4123 fluorine doped tin oxide (FTO) and ZnO:Al are the most widely used materials. CdS is used
4124 as window layer in this type of cells, while CdTe is used as an absorber. Physical properties
4125 of materials used in CdTe based solar cells, and interface properties of CdS/CdTe solar cells
4126 are presented in Table 5.

4127
4128 Table 5 Important properties of CdTe based solar cell.
4129

Properties	Value	Ref.
TCO (SnO₂, ITO, FTO and ZnO:Al)		
Lattice constant SnO ₂ (Å)	a=4.72; c=3.19	[629]
Lattice constant ITO (Å)	a=1.12	[630]
Lattice constant FTO (Å)	a=4.69; c=3.16	[631]
Lattice constant ZnO:Al (Å)	a=3.24; c=5.16-5.16	[632,633]
Work function SnO ₂ (eV)	4.7-5.7	[634]
Work function ITO (eV)	4.7	[635]
Work function FTO (eV)	4.4	[636]
Work function ZnO:Al (eV)	3.83	[637]
TCOs Optical Transmission	>80%	[638]
TCOs Resistivity ρ (Ω·cm)	10 ⁻⁴	[638]
Bandgap energy SnO ₂ (eV)	3.9	[629]
Bandgap energy ITO (eV)	3.6	[639]
Bandgap energy FTO (eV)	3.3-3.6	[640,641]
Bandgap energy ZnO:Al (eV)	3.0-3.4	[642]
Window layer (CdS)		
Lattice constant Cubic (Å)	a=5.83	[643]
Lattice constant Hexagonal (Å)	a= 4.14 c = 6.75	[644]
Work function (eV)	4.7	[645]
Bandgap energy (eV)	2.4	[627,639]
Absorber layer (CdTe)		
Lattice constant (Å)	a=6.48	[646]
Work function (eV)	3.88-4.09	[647]
Enthalpy of formation (J/mol)	10 ⁶	[648]
Standard entropy (J/mol.K)	-4.3±0.8	[648]

Carrier concentration/cm ³ (p-type CdTe)	10 ¹⁴	[625, 649,650]
Lifetime electron/holes τ (s) 2 μ m	10 ⁻⁹	[626]
Bandgap energy (eV)	1.45	[639]
Interface (CdS/CdTe)		
Mismatch cubic CdTe and hexagonal CdS	9.7%	[651, 652]
Mismatch cubic CdTe and cubic CdS	-	-
CdTe Absorption co-efficient/cm (at ~600nm)	>10 ⁵	[625, 626,653]
Dielectric constant CdS/CdTe (ϵ/ϵ_0)	10/9.4	[639]
Electron mobility μ_e CdS/CdTe (cm ² /Vs)	350/500-1100	[639, 654]
Hole mobility μ_h CdS/CdTe (cm ² /Vs)	50/60-100	[639,654]
Minority-carrier diffusion length (μ m)	<0.8	[625]
Capture cross section electrons σ_e CdS/CdTe (cm ²)	10 ⁻¹⁷ /10 ⁻¹²	[639]
Capture cross section holes σ_h CdS/CdTe (cm ²)	10 ⁻¹² /10 ⁻¹⁵	[639]

4130

4131

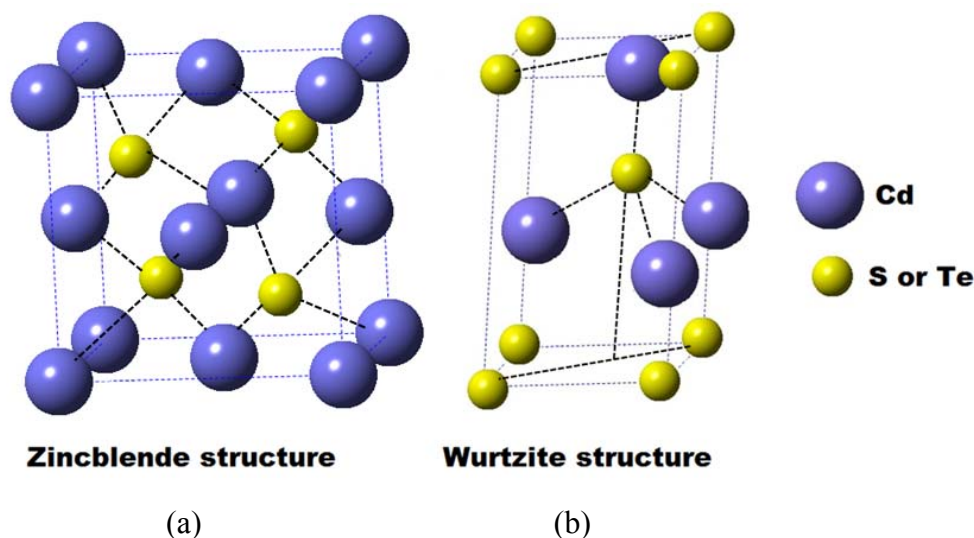
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4134

4135

From crystallographic point of view, the lattice mismatch and crystallographic structure among all components that form the solar cell heterostructure are of essential importance. Figure 75 shows the crystallographic structure of both CdTe and CdS layers in the cubic zincblende (Fig.75a) and hexagonal Wurtzite structure (Fig.75b).



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Fig. 75 Crystallographic structure of (a) zincblende, and (b) hexagonal Wurtzite. In the zincblende structure, tellurium or sulphur atoms occupy the tetrahedral position surrounded by cadmium atoms located in a face-centered cubic structure. While in the Wurtzite structure, tetrahedron is formed when the S atom is in the interior of the hexagonal structure. CRYSTALMAKER program is used to create the structure even though this is a well known structure.

4143

4144

9.2 Thin-film CdS/CdTe solar cells

4145

4146

In general, the transport of the photogenerated minority-carriers in bulk thin film materials and single crystals has the advantage of fast transportation due to low number of

4147 defects. At the same time there is a disadvantage that the production methods require high
4148 energy consumption at high cost and large mass of initial starting materials. The fabrication
4149 of CdS/CdTe solar cell has been mainly carried out using chemical bath deposition (CBD),
4150 sputtering and evaporation, close space sublimation (CSS), and MOCVD [627].

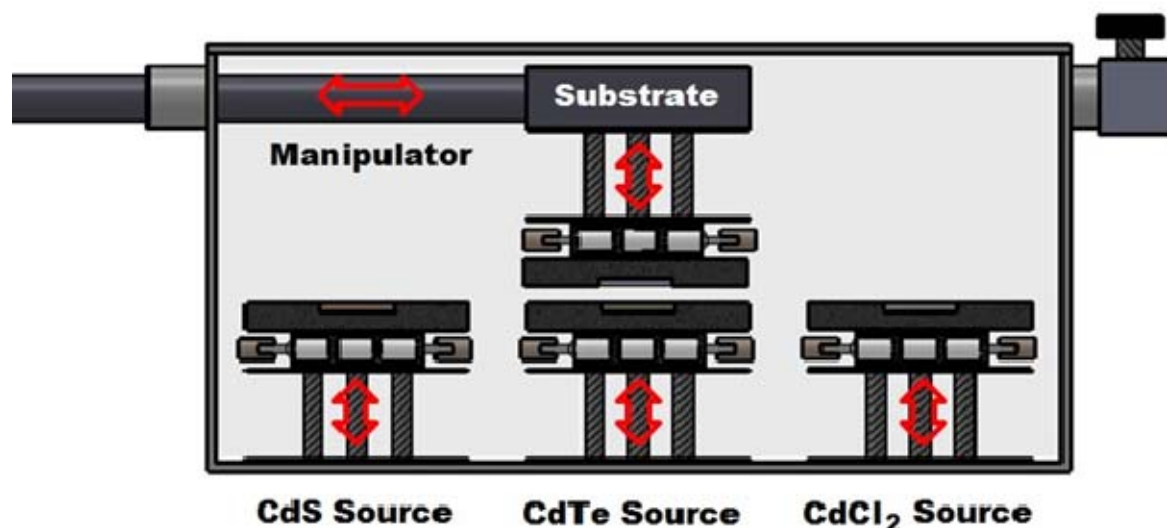
4151 **9.2.1 Concepts and preparation methods**

4152
4153 P-type CdTe possesses an optimum direct bandgap (1.45eV) and high optical
4154 absorption co-efficient ($5 \times 10^5/\text{cm}$) in the visible spectral range. A 0.5 μm thick CdTe is able
4155 to absorb a large percentage (99%) of the solar spectrum [625,652,655]. To form
4156 heterojunction, n-type CdS between 10 and 50 nm layer is required to minimize the photon
4157 absorption losses, without reducing the V_{oc} [652]. Currently work is being carried out in
4158 order to improve the window layer.

4159 For CdS/CdTe solar cells, superstrate configuration is the most commonly used with
4160 the structure illustrated in Fig. 74 [625,656]. Substrate configuration with low-cost flexible
4161 metal substrate is also used [657]. In these configurations, most of the efforts are
4162 concentrated on improving the quality of both window and absorber layers. This is along with
4163 reducing losses through the other components and interfaces due to light absorption in layers
4164 other than the CdTe. Developing a successful solar cell requires a combination of improving
4165 the quality of all components including the electrodes, enhancement of charge transport, and
4166 hence cell efficiency [30].

4167 For the preparation of CdS layer by CBD method, a mixture of KOH, ammonium
4168 nitrate, CdCl_2 , and thiourea are generally used at a working pH value of 8-9 in the
4169 temperature range of 75-90°C. A magnetic stirrer in the solution is used to maintain a
4170 homogenous solution and to control the thickness of the CdS film. In order to obtain the
4171 required thickness, the most important parameters in the growth process are pH, temperature,
4172 stirring rate, and time [658, 659].

4173 CSS method is a physical deposition technique where the source and the substrate are
4174 very close to each other, thus allowing the sublimation of the source and creating epitaxial
4175 thin films without using ultra high vacuum. Using this technique both the window and the
4176 absorber layers are prepared [625, 651, 655, 660-662]; the most sophisticated CSS system are
4177 located in the Technical University of Darmstadt (with *in situ* characterization tools for a
4178 complete study of the solar cell) [656, 662], and CTF Solar GmbH [663]. Figure 76 shows
4179 the schematic diagram of a CSS system for the deposition and processing of CdS and CdTe
4180 layers. A general approach for the CSS method [649, 656, 662, 663] uses commercial
4181 halogen lamps for heating the source and substrate. As an alternative to halogen lamp,
4182 resistance heaters (SiC) have been recently proposed as an approach to reduce the duration of
4183 the process and improving the grain size and homogeneity [664]. Several deposition
4184 parameters must be taken into account, such as controlled high-vacuum or inert atmosphere,
4185 source temperature in the range of 500-650°C, substrate temperature in the range of 300-
4186 500°C, distance between source and substrate of 2-5mm, and deposition time of 5-20 min. A
4187 fast (1 min) or slow (15 min) cooling process after the CdTe layer preparation in the 300-
4188 500°C range has been considered as an important step with great influence in the absorber
4189 layer preparation, with fast cooling yielding slightly thicker Cd layer. This thick Cd-layer
4190 could influence the CdCl₂ diffusion [649] and affect efficiency.



4191

4192 Fig. 76 Schematic diagram of close space sublimation system for the preparation of CdS and CdTe films [665].
 4193 Distance between the source and substrate is 2-5mm and the deposition time is around 5-20min. In order to
 4194 reduce the contamination between three sources, a precise shutter is located over each source, and a vacuum
 4195 process is done before CdS layer deposition. Source temperature and substrate temperature is in the range of
 4196 500-650°C, and 300-500°C respectively. The top substrate is located in a moveable piece over fixed sources
 4197 with the capability for depositing several consecutive different layers of CdS, and CdTe. At the same time,
 4198 cadmium chloride (CdCl₂) treatment could be carried out in the same system. After each layer deposition, CdCl₂
 4199 treatment is required to improve electronic properties.

4200

4201 For CdS/CdTe cell fabrication, there is a general agreement that after the deposition
 4202 of each layer (CdS and CdTe), CdCl₂ treatment is necessary to improve electronic properties,
 4203 recrystallization, grain growth [666] and hence cell efficiency. Prior to CdCl₂ treatment,
 4204 Major et al. [649] showed the importance of creating (tens of nanometers thick) Cd-rich
 4205 surface using nitric-phosphoric acid etching to increase the chlorine and oxygen in-diffusion
 4206 associated with an improvement in the efficiency from <3% to 12%. The absence of this
 4207 etching process will, however, produce a blocking layer of Cd₃O₂Cl₂.

4208

4209 For CdS layers, CdCl₂ treatment is used because of the resulting benefits of the
 4209 window layer causing a recrystallization and increasing the grain size with improvement of
 4210 the structural and optoelectronic properties [625,661, 662-665, 667].

4211

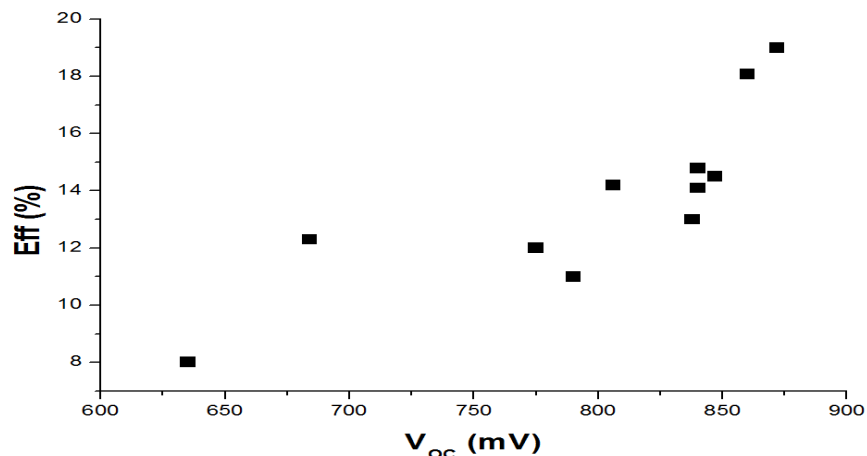
4212 For CdTe layers, post treatment with a CdCl₂ treatment is generally used as a process
 4212 to promote the interdiffusion of CdS/CdTe layer and recrystallization. The result is the
 4213 improvement of the texture and grain size, and reduction of porosity, with reduction of the

4214 point defects [625, 657, 662]. However, CdTe surface roughness increases after CdCl₂
 4215 treatment [666]. At the same time, the introduction of chlorine can compensate native defects
 4216 in the CdTe structure [668]. In the end, this post treatment affects the interdiffusion at the
 4217 CdTe/CdS interface with the consequence of reducing the negative factor of the large
 4218 mismatch between both materials [651,652,655].

4219 Other important layers to be considered are the front and back contact, where some
 4220 novelties have been reported. For the front contact, the ZnO:Al is increasingly used, although
 4221 their lower thermal stability has many advantages compared to other (ITO, FTO) front
 4222 contact materials [642, 662]. For the back contact, a 4-5nm Cu, followed by a 40-100nm gold
 4223 (Au) layer, is the most used. The Au layer is replaced by antimony telluride to avoid the Cu
 4224 diffusion towards the interface [650, 662, 663, 669]. In a complementary way, the use of
 4225 selective acidic etching for a formation of tellurium or a p⁺-layer prior to the contact
 4226 formation is an interesting process, which will improve the back contact [647,662].

4227 9.2.2 CdTe solar cell parameters and properties

4228 Table 6 shows CdTe solar cell parameters. It can be seen that the device with
 4229 maximum efficiency of 19% has the best V_{oc} and J_{sc} values [670]. Figure 77 shows the
 4230 efficiency versus V_{oc} values, where a clear dependence among both values is demonstrated.



4242 Fig. 77 Relationship between V_{oc} and efficiency. The data corresponds to the values shown in Table 6. As can
 4243 be seen, there is a direct relationship between V_{oc} and efficiency. Efficiency >14% has been obtained when V_{oc}
 4244 is greater than 750mV. To obtain high V_{oc} and J_{sc} , CdTe thickness of 2-5 μ m is required.

4245

4246 Table 6 CdS/CdTe solar cell output parameters.

4247

Institution	V_{oc} (mV)	J_{sc} (mA/cm ²)	Fill factor (%)	Eff. (%)	Ref.
University of Liverpool	635	20.2	47.1	8	[671]
Darmstadt University of Technology	775	23.9	64.9	12	[662]
University of Chicago	684	25.8	71	12.3	[641]
CTF Solar GmbH	838	21.8	71.1	13	[663]
University of Oregon	790-840	23.0-24.4	62-72	11-14	[668]
University of Toledo	806	25.2	69.8	14.2	[669]
University of Toledo	847	24.4	69.8	14.5	[672]
University of Durham	840	24	73.41	14.8	[649]
Ferdowsi University of Mashhad	860	25.7	81.8	18.1	[639]
First Solar, Inc	872	28	78	19	[670]
First Solar, Inc	875	30.2	79.4	21	[484]

4248

4249

4250 The dependence of V_{oc} and J_{sc} on CdTe layer has been studied extensively [626, 646
 4251 654]. For CdTe, absorption in the solar spectrum is ~93% for 1 μ m thickness, while 99%
 4252 absorption requires ~20 μ m thickness. For 1 μ m thickness, J_{sc} decreases more than 20% with
 4253 strong interdiffusion effects on the CdS/CdTe layer, while it decreases only ~5% for 2-3 μ m
 4254 [654]. For this reason, in order to obtain an optimum value of V_{oc} and J_{sc} , a critical thickness
 4255 of 2-5 μ m may be required [652, 654, 657, 663].

4256 9.2.3 Defects in CdTe solar cells

4257 Defects such as dislocations, traps, and grain boundaries are important factors that
 4258 affect efficiency in planar CdTe solar cells. For this reason, defects have been investigated
 4259 experimentally, as well as theoretically in order to study the influence of these on the
 4260 optoelectronic properties and consequently on the solar cell efficiency. The quality

4261 improvement for each component, viz. front contact, window layer, absorber layer and back
4262 contact is essential to increase cell performance. The following improve device performance:

4263 (i) A good texture of TCO layer will enhance orientation of CdS film.

4264 (ii) Pin hole free CdS window layer is essential to reduce losses that are associated with
4265 recombination at interfaces. CdS layer thickness below 80 nm could produce pinholes and
4266 increase shunting effects [627,656].

4267 (iii) The presence of grain boundaries affect preferential interdiffusion of sulfur (S) from CdS
4268 to CdTe as a consequence of assisted diffusion mechanism leading to the formation of the
4269 CdTe_{1-x}S_x phase. Grain boundaries induce dislocations, trap minority carriers, and influence
4270 V_{oc} [653] which reduces cell efficiency. At the same time the internal electric field that exists
4271 between the grain boundary core and the bulk material will deteriorate the electrical
4272 conductivity of the material [653, 673].

4273 (iv) CdTe layer requires a thickness of 3-5 μ m to avoid pinholes and shunting
4274 phenomena. Therefore, a double CdTe layer structure formation has been prepared with two
4275 consecutive temperature steps [650].

4276 (v) All interfaces must be carefully controlled. In fact, distorted bonds at the interfaces
4277 introduce extra electronic states, hole traps, and accumulation of positive charges [653].

4278

4279 **9.2.4 Novelties and improvements**

4280

4281 For the development of planar CdS/CdTe solar cells some general novelties have been
4282 proposed:

4283 (i) With spin coating process, tens of sequentially controlled thickness layers can be produced
4284 [641].

4285 (ii) The use of nanoparticles as source material in CSS method will reduce the time for
4286 obtaining a pre-determined thickness of the CdTe layers. As one example, for a given 5 μ m
4287 thickness, a reduced time of 35% is obtained [641].

4288 (iii) In CSS high vacuum process, a double layer structure formation with two consecutive
4289 temperature steps for both window and absorber layer is suggested in Ref. [650].

4290 The new features and improvements that have been introduced recently in the
4291 development of CdS and CdTe layers as well as developments in the characterization
4292 techniques are described below:

4293 (i) An extra oxide layer between the TCO and the window layer to minimize shunting effects
4294 has been introduced. However, it also comes with the disadvantage of increasing production
4295 cost [627]. In fact a ZnO buffer layer before the CdS window layer has been proposed as a
4296 factor for reducing pinholes and voids on the window layer [657].

4297 (ii) CdS window layer prepared with low oxygen content in the order of 2% O₂/Ar gives a
4298 good adhesion layer after CdCl₂ treatment, while without O₂ treatment, the interface is
4299 delaminate [674]. At the same time, the O₂ partial pressure will enhance the transmission
4300 below 500nm with slightly increase in efficiency of 1% [674].

4301 (iii) Widening CdS layer bandgap to allow more region of the solar spectrum to reach the
4302 absorber layer with improving photocurrent. For example Cd_{1-x}Zn_xS composition enhances
4303 the blue-region of solar spectrum with increasing Zn concentration being the bandgap energy
4304 values 2.4-3.5 eV for Cd_{1-x}Zn_xS (0<x<0.9) [627]; Also, smoother and denser CdS layers have
4305 been proposed as a measure to reduce the light absorption in the high energy UV range [627,
4306 656].

4307 (iv) The doping of p-type CdTe layer has been proposed as a way to modify carrier
4308 recombination and increase the shallow acceptors in p-type CdTe to improve bulk minority-
4309 carrier lifetime [625]. It is also a way to increase the work function with dopants such as
4310 arsenic, although arsenic segregation at the grain boundaries will increase the acceptor
4311 concentration in these regions [647]. Furthermore, a step doping profile of the absorber layer
4312 has been done with a structure of p/p⁺ with thickness ratio of 2.24/1.26μm as a way to create

4313 an electric field that improves carrier collection [639], resulting in an improvement in V_{oc} ,
4314 improved fill factor, efficiency, and reduction of the series resistance [639].

4315 (v) Large difference in the valence band offset at the interface will form a barrier for holes,
4316 with an increase in the contact resistance. To obtain negligible valence band offset for
4317 efficiency enhancement, wide bandgap materials such as $Cd_{1-x}Zn_xTe$ ($E_g \sim 1.5-2.4eV$), Cd_{1-}
4318 $_xMn_xTe$ ($E_g \sim 1.5-3.2eV$) and $Cd_{1-x}Mg_xTe$ ($E_g \sim 1.5-3.6eV$) are used with appropriate
4319 composition ratios of Zn, manganese (Mn) and magnesium (Mg), all of them having high
4320 solubility in CdTe [625,626].

4321 (vi) For absorption of low energy photons, an intermediate narrow metallic bandgap material
4322 is used between the n/p type semiconductors [30].

4323 (vii) In the absorber/contact interface, the use of electron reflector barriers such as CdXTe
4324 (X:Mn, Zn, Mg) are useful for reducing back surface recombination, which allows increased
4325 values of 0.2V for V_{oc} and 3% for the efficiency. This is a strategy used for CIGS and Si-
4326 based solar cells, although here the quality of the interface between absorber/electron barrier
4327 must be improved [626]. The other way of increasing efficiency is the use of highly doped
4328 ($10^{18}/cm^3$) buffer layer at the interface between absorber/contact in the substrate
4329 configuration [657].

4330 Apart from classical techniques such as XRD, scanning electron microscope (SEM),
4331 EDX etc. it is of special interest to know new tools that have been successfully used in the
4332 past few years for better understanding the properties of CdTe solar cell. These include
4333 scanning Kelvin probe microscopy for the Fermi level shift determination and CdTe work
4334 function [647], laser beam induced current for photoelectronic properties [653], electron
4335 beam induced current [664] and electron back-scatter diffraction to demonstrate that the grain
4336 structure and the grain boundaries dominate the electrical activity [673], x-ray photoelectron
4337 spectrometer for *in situ* measurements in the CSS chamber [656], thermo photocurrent

4338 measurements to investigate the compensating levels introduced by CdCl₂ treatment [668]
4339 etc.

4340 **9.3 CdTe nanostructured solar cells**

4341
4342 Extensive research has been carried out in the field of 3G solar cells over the past
4343 several years [623,628, 635, 657, 667, 675-684]. The basic structure of these nanostructured
4344 solar cells follows the general configuration of the planar solar cells, where the front and back
4345 contacts, window layers, and absorber layers must be present. In this general configuration of
4346 the solar cell, nanostructures can be incorporated through top-down and bottom-up processes.
4347 Top-down processes such as the lithography, low energy ion sputtering [675], and laser
4348 irradiation [684] can change the solar cell properties, producing an improvement in
4349 luminescence and the crystallinity.

4350 Due to a large number of possibilities, this section will focus on the bottom-up
4351 structures where the nanostructures are created as an intermediate step in the fabrication of
4352 solar cell, and on the superstrate configuration.

4353 Excellent reviews have been published [671, 685] about the new perspectives of the
4354 enhancement of the solar cells efficiencies with the use of 1D nanostructures, nanopatterning
4355 and their applications, in particular dye/quantum dots sensitized solar cells, and single/double
4356 wall carbon nanotubes as strategies for new nanostructured architecture of inorganic and
4357 organic solar cells. This new technology is being used in CdS/CdTe solar cells.

4358 **9.3.1 Concepts and advantages**

4359 The concept of nanostructure on CdTe solar cell, requires a general configuration of a
4360 superstrate structure (glass/TCO/CdS/CdTe/back contact), with the presence of
4361 nanostructures in some of the layers. These nanostructures play an important role with
4362 promising properties in metals, oxides, semiconductors, etc. having an extraordinary

4363 importance in PV energy production due to the decoupling of light absorption and carrier
4364 separation into orthogonal special directions [676].

4365 The concept and structure of nanostructures embedded in bulk film indicates that the
4366 longitudinal direction is long, allowing for optimal and enhanced light absorption due to more
4367 internal reflections and longer path length compared with thin-films, while the orthogonal
4368 direction is thin allowing for an effective minority-carrier collection [676]. The size and
4369 spacing are in the order of the light wavelength, resulting in positive anti-reflective and light
4370 trapping properties, with a reduction of the reflectance of two orders of magnitude compared
4371 to the equivalent planar structures. This allows for a high performance without a reduction of
4372 the J_{sc} [657, 676].

4373 In the nanostructured solar cell, apart from lower defect trapping, the diffusion length
4374 of minority-carriers in the lateral direction is shorter than that of a thin-film solar cell [686].
4375 Nanojunctions generate an electric field in the lateral direction that gives the option to the
4376 minority-carrier to move between the core and the shell, resulting in relatively short carrier
4377 transit length, and consequently the recombination loss is reduced [657,687]. Broadening of
4378 the optical bandgap with the use of nanostructure could maximize the S-Q efficiency limit
4379 which is an attractive electronic property.

4380

4381 **9.3.2 Types of nanostructures and mechanisms of formation**

4382 There are different types of nanostructures that follow the general scheme of a core
4383 structure of ZnO or CdS embedded by the shell structure of CdS or CdTe respectively, named
4384 as ZnO/CdS [681, 683] or CdS/CdTe core/shell structure [677, 685], although there are some
4385 exceptions to this rule. As mentioned in Sec. 7.6.1, the nanostructures can be classified
4386 according to their structure as follows: nanowires [677, 681, 683, 685], nanocones [676, 684,
4387 686], nanopillars [685] and whiskers or needles [677].

4388 There are several methods for core formation. The most general processes use Au and
4389 Ni as catalyst for nanowire core formation through the VLS process [16, 657, 677, 680, 687].
4390 Nevertheless, there are other methods used for core formation: porous anodic alumina
4391 substrates embedded in polycrystalline thin-films for p-type CdTe formation [685], patterned
4392 nanoelectrodes defined on the TCO substrate through e-beam lithography with hole size of
4393 0.4-1 nm [688], and magnetron sputtering deposition using Ar [678].

4394 For core/shell formation, the core begins from a seed material where nanowire
4395 crystallizes or grows, as it happens with Au catalyst. Other methods are: a μm layer of CdTe
4396 as a seed for the growth of CdTe nanowire in substrate configuration [657]; a nm thick
4397 ZnO:Al buffer layer on ITO substrate and using CVD process to develop nanocones shaped
4398 ZnO [686]; TiO₂ nanoparticles deposited by dip-coating on FTO substrate for the preparation
4399 of ZnO nanowire by chemical solution, followed by the growth of nanotubes of CdS in a
4400 chemical galvanostatic process [679]; another alternative for the ZnO nanowire is the
4401 previous creation of ZnO seed layer, with the added advantage that this layer could avoid
4402 shunting paths [681, 683, 686].

4403 The other alternatives that may be of high interest for CdTe nanostructured solar cell
4404 are: the use of nanoink solution processes containing organic ligands and applied in ambient
4405 conditions as a way for nanolayer formation [623]; the use of graphene monolayer with
4406 conductive polymer interlayers, and a spin coating of zinc layer as a mean for ZnO nanowire
4407 preparation in aqueous solutions at a relatively low-temperature [682].

4408 The growth mechanism of CdTe nanowire solar cell has been rarely studied.
4409 Nevertheless, Ref. [678] demonstrates that the CdTe nanowire formation follows the
4410 Stranski-Krastanov model determined by the free energy of the substrate surface (σ_s),
4411 interface free energy (σ_i) and heteroepitaxial surface free energy (σ_f). In consequence, the
4412 seed crystal is nucleated in the 2D layer when σ_s is larger than the addition of the other two,

4413 and 3D islands are formed when σ_s is smaller than the addition of the other two. The growth
4414 process is controlled by the concentration of the nanowire and depends on the temperature
4415 and the type of substrate used.

4416 Growth process indicates that growth rates up to $1\mu\text{m}$ could be obtained due to solid
4417 and vapor phase growth mechanism [657]. A preferential orientation of $\langle 111 \rangle$ in CdTe film
4418 over the ZnO nanowires, with the appearance of side wall facets has been reported [657,
4419 686]. An interesting sulfidation process has been proposed using the following route: ZnO
4420 nanowire produced through a chemical solution is followed by sulfidation (with
4421 thioacetamine) of the ZnO nanowire for the production of ZnO/ZnS core/shell structure, and
4422 completed by the ion exchange Zn-Cd with the result of ZnO/CdS core/shell nanowire
4423 structure. This is due to the fact that the solubility product of CdS is 10^4 times lower than ZnS
4424 [683]. Also, nanowire heterostructures on III-V Wurtzite/zinc-blende cubic compounds [680]
4425 with similar crystallography structures of CdS/CdTe have been studied, and a growth
4426 mechanism is explained through the competition between the Gibbs-Thomson effect and the
4427 different diffusion mechanisms.

4428 The post growth process that follows the nanostructure formation is similar to that of
4429 planar solar cell. To improve efficiency, CdCl₂ treatment in one or several steps is essential
4430 for recrystallization controlling the interdiffusion at the CdS/CdTe interfaces and passivation
4431 of the grain boundary interfaces [657, 667, 686, 689].

4432 **9.3.3 Characteristics of nanostructures and CdTe nanostructured solar** 4433 **cells**

4434 Table 7 shows the most important characteristics of the nanostructures used in CdTe
4435 solar cells, with indication of the preparation methods and nanowire characteristics such as
4436 diameter, height, density, and spacing between the nanowires. There are different methods
4437 from chemical solution to vapor, which produce nanowire geometries with clear difference

4438 between them. Considering the three nanowires geometric properties of diameter, height and
 4439 density, if one considers that the ratio between height and diameter is critical for efficiency, a
 4440 general conclusion to draw is that the VLS method is the most adequate for nanowire
 4441 formation. In the spacing data, there are differences between the reported values that appear
 4442 to be related to preparation method.

4443
 4444 Table 7 Characteristics of the CdTe Nanostructures.
 4445

Nanowire Structure	Method	Diameter (nm)	Height (μm)	Density (/cm ²)	Spacing (nm)	Ref.
ZnO	CBD	140	5		0.3	[681]
ZnO	CVD	80-300	1	10 ⁹	20-200	[686]
ZnO	Dip-coating	80	1	10 ¹⁰	20-40	[679]
CdS	PLD	40-100	0.4-1	2·10 ⁹		[677]
CdS	Electro-deposition	60	100	1.14x10 ¹⁰	106	[628]
CdTe	VLS	50-200	10-100	10 ⁷ -10 ⁸		[657]
CdTe	Sputtering	100-150	3	~10 ⁹	20-50	[678]
CdTe	Electro-deposition	400-1000	1	~5x10 ⁹	2000	[688]

4446
 4447
 4448 The output characteristics of the CdTe nanostructured solar cells are indicated in
 4449 Table 11.8, where the relatively low efficiency can be observed if one compares these data
 4450 with planar solar cell, although the improvement has been steadily increasing over the years.
 4451 An example of this increment is a new efficiency record for this type of devices of 12% using
 4452 CdS nanowires embedded in CdTe [628], with a high value of J_{sc} (26mA/cm²).

4453
 4454 Table 11.8 Output characteristics of nanostructured CdTe solar cells under AM 1.5 conditions
 4455

Institution	V _{oc} (mV)	J _{sc} (mA/cm ²)	Fill factor (%)	Eff. (%)	Ref.
Oak Ridge National Laboratory	630	8.3	38	2	[686]
University of Liverpool	520	13.9	34.3	2.49	[657]
Oak Ridge National Laboratory	610	13.8	38	3.10	[686]
University of Kentucky	770	26	60	12	[628]

4456

4457 **9.4 Future direction**

4458 More work and investment must be done considering the predicted maximum
4459 theoretical efficiency of 29%. Here are some research paths that could be followed to
4460 improve the efficiency: (i) improvements in front contacts by replacing TCO by graphene,
4461 pure and doped, together with buffer layers allowing for Ohmic contacts [682, 690], (ii) well
4462 aligned CdTe nanowires with optimum value of the diameter/thickness ratio, (iii) strategic
4463 alloys and compounds to increase the bandgap of the buffer layer for improving efficiency,
4464 and (iv) adequate buffer layers for lattice mismatch reduction in order to improve the
4465 crystallographic quality.

4466 **10.0 SiNW solar cells**

4467 With the beginning of this millennium it was rapidly realized that nanostructures such
4468 as SiNWs offer a flexible platform for novel 3D solar cell concepts [691-693]. Nanowires
4469 show several advantages over planar solar cell geometries such as the potential for increased
4470 device density, and device development on flexible substrates. Direct bandgaps in smaller
4471 diameter SiNWs also offer the potential for increased efficiency. Since Si is well understood
4472 in terms of its properties, SiNWs come with a solid platform for extending current fabrication
4473 technology in their use as active solar cell materials.

4474 This section will give a short overview about SiNW based solar cells, present the
4475 competing concepts and show the most promising candidates for highly efficient and cost-
4476 effective solar cells.

4477 The term nanowire is often substituted by related terms like nano-rods, whiskers, pillars,
4478 columns or cones. A recent review by Kuang et al. therefore formed the description
4479 “elongated nanostructures” to combine all these different terms with a similar meaning [694].

4480 **10.1 SiNW formation**

4481 SiNWs can be prepared by several different techniques and every method has its own
4482 advantages and drawbacks. The large increase in surface area enables an efficient light
4483 trapping due to multiple scattering events and optical path increase inside the SiNW. In
4484 general, the nanowire synthesis methods are arranged in bottom-up growth and top-down
4485 etching techniques.

4486 In the case of bottom-up synthesis, the VLS growth, which was developed by Wagner
4487 & Ellis in 1964, is the most popular approach of preparation [695]. As mentioned in
4488 Sec.7.6.1, in a VLS process, a metal catalyst which forms a eutectic with Si (Au, Al, Cu and
4489 Ag etc.) is heated in vacuum and is exposed to a gaseous Si source like SiH₄,
4490 tetrachlorosilane (SiCl₄), sputtered or laser ablated Si [696-699]. Most research groups used
4491 SiH₄ precursors for SiNW growth since it can produce well controlled wire dimensions and is
4492 relatively easy to handle once the toxicity is kept under control. A VLS process requires a
4493 high or ultrahigh vacuum chamber in which a substrate covered with the catalyst metal, in the
4494 form of particles or a thin-film, is heated above the eutectic temperature. The SiH₄ molecules
4495 are decomposed on the metal surface and the Si is introduced into the metal droplet, forming
4496 the eutectic. By further insertion of Si, the droplet gets oversaturated and excess Si is
4497 displaced to the contact surface of the droplet to the substrate. In this way a wire arises below
4498 the droplet. By controlling the catalyst geometry, chemistry and process parameters, it is
4499 possible to create nanowires with precise lengths, diameter, direction, doping and pitch. The
4500 advantage of high control has to be weighed by the disadvantages of high costs for vacuum
4501 equipment, highly poisonous gases and catalyst metal contamination inside the wires, which
4502 is the major drawback especially for Au catalyzed SiNWs [700].

4503 Nevertheless, there are many groups that successfully created solar cells out of VLS-
4504 grown SiNWs. Hochbaum et al. showed the advantages of using SiCl₄ as a precursor [701].
4505 During the decomposition of the precursor molecules HCl vapor is formed which etches and

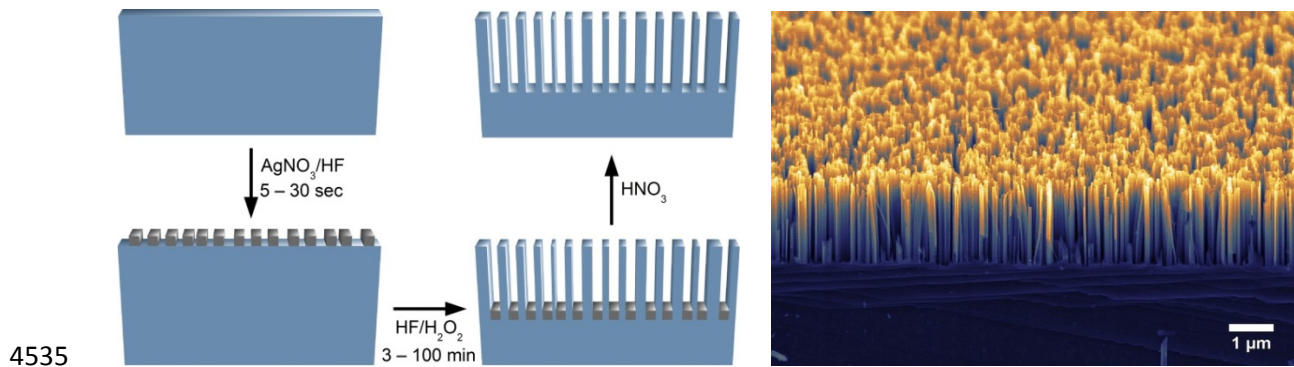
4506 thus cleans both the SiNW sidewalls as well as the substrate surface. In this way it became
4507 possible to grow highly ordered epitaxial SiNWs, which was not possible with SiH₄. The
4508 electrical modification of SiNWs is achieved by adding doping precursors like B₂H₆ or PH₃
4509 into the chamber during growth which leads to p- or n-type doping [692,702] respectively. In
4510 2006, Wang et al. described the growth of SiNWs by using Al catalyst to avoid the deep-level
4511 electronic states that are caused inside the Si when using a gold catalyst [698]. On the other
4512 hand Al comes with another drawback: it needs an extremely clean environment at UHV
4513 conditions to avoid oxidation of the Al which drives the production costs to a
4514 disproportionate level.

4515 Garnett & Yang [532] and Stelzner et al. [703] developed the first solar cell devices
4516 based on carpets of SiNWs grown by VLS method. Their efficiencies were quite low, but
4517 they established a basis for a complete new field of nanostructured solar cells.

4518 In contrast to the bottom-up growth methods, the top-down synthesis of SiNWs uses
4519 existing layer of Si like single- or multicrystalline wafers or deposited layers on supporting
4520 substrates to create wires inside these layers. The most prominent processes are the metal-
4521 catalyzed electroless etching, which was developed by Peng et al. [693] in 2002, and the RIE
4522 [704,705]. Both processes can form randomly distributed or ordered SiNWs.

4523 In a metal-catalyzed electroless etching (MCEE) preparation, a metal catalyzed
4524 anisotropic etching of Si forms the desired SiNWs. The most prominent recipe was developed
4525 by Peng et al. [693,706]. Ag nanoparticles are deposited on Si in a mixture of HF/silver
4526 nitrate and are subsequently used for the anisotropic etching in a HF/H₂O₂ mixture. The Si is
4527 catalytically oxidized at the Si/metal interface and immediately etched by the HF. In this way,
4528 the metal particles move into the Si layer, forming a carpet of SiNWs. Since the anisotropic
4529 etching at room temperature only occurs in the Si<100> direction [707], perpendicular
4530 SiNWs are formed on a Si(100) wafer (Fig. 78), while the use of a Si <111> wafer leads to

4531 zig-zag shaped wires [708]. In multicrystalline layers, each grain is independently etched into
 4532 the $\langle 100 \rangle$ direction [709]. MCEE processes are easily scalable and relatively cheap in
 4533 contrast to bottom-up growth which is why it is an attractive way of generating highly
 4534 absorbing structures for photovoltaics.

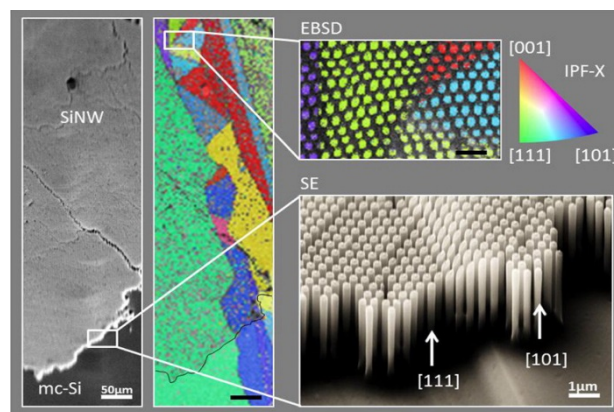


4536
 4537 Fig. 78 Left side: Schematic model of the preparation of wet-chemically etched SiNWs. Ag nanoparticles are
 4538 deposited by rinsing a wafer in a silver nitrate/HF mixture. These particles act as catalysts in the subsequent
 4539 etching of Si in HF/hydrogen peroxide which is highly dependent on the crystal orientation of the wafer. In the
 4540 final step Ag is removed by nitric acid. Right side: A tilted (55°), colored SEM micrograph of an etched
 4541 Si $\langle 100 \rangle$ wafer with SiNW length of $2\mu\text{m}$. Such a structure acts as a nearly perfect light absorber with an
 4542 absorption of over 90% in a wavelength range from 400 – 1000nm. SEM image originally published in [710],
 4543 Björn Hoffmann, Vladimir Sivakov, Sebastian W. Schmitt, Muhammad Y. Bashouti, Michael Latzel, Jiří
 4544 Dluhoš, Jaroslav Jiruse and Silke Christiansen, "Wet-Chemically Etched Silicon Nanowire Solar Cells :
 4545 Fabrication and Advanced Characterization in Nanowires"- Recent Advances., InTech; 2012. Edited by Xihong
 4546 Peng. pp-211-230. Reproduced here under CC BY 3.0 license. Copyright © 2012 InTech.

4547

4548 In addition to wet-chemical processes there is much effort put into the development of
 4549 dry-etching of Si in a deep RIE (DRIE) approach. The process works without metal catalysts
 4550 and can be applied either in a self-organized or a mask-supported process. Two particular
 4551 approaches will be mentioned here: the formation of so-called black Si and the preparation of
 4552 highly regular SiNWs by the use of nanosphere lithography. The term black Si is used for
 4553 many variations of etched Si and refers to the dark appearance of such a layer. In the most
 4554 popular results, a fluorine-based etching [711-713 827-829] creates random pyramidal or
 4555 needle-like structures that can be compared to MCEE results. The advantage is that no
 4556 lithography step for catalysts or masks is needed. Halbwax et al. used a femtosecond laser to
 4557 form Si nanostructures that also carry the name black Si [714].

4558 By combining a RIE process with a prior decoration with a monolayer of silica
 4559 spheres in a Langmuir-Blodgett deposition, Hsu et al. gained a high control over the
 4560 dimensions of the resulting nanostructured Si [705]. Since the RIE approach produces SiNWs
 4561 with a high dimensional reproducibility, which offers a precise tailoring of optical properties,
 4562 it is one of the most promising fabrication mechanisms at the moment. Garnett & Yang have
 4563 investigated the light trapping properties of RIE-prepared SiNWs in c-Si wafers and found an
 4564 increase in path length of incident light inside the SiNW layer by a factor of 73 [715]. In
 4565 2012, Schmitt et al. have shown that such a combination of nanosphere lithography and RIE
 4566 also produces regular vertical SiNWs in multicrystalline Si layers on glass and that the SiNW
 4567 orientation is not influenced by the original grain orientations [716]. Figure 79 shows SEM
 4568 micrographs and electron backscatter diffraction investigations of such prepared SiNWs.
 4569 Since this process is more complicated and expensive, it is mostly used for fundamental
 4570 research of optical properties or comparisons with theoretical models. Nevertheless,
 4571 impressive results have been obtained with RIE prepared SiNWs and the current progress is
 4572 very promising.



4573

4574 Fig.79 SEM and electron backscatter diffraction mappings of multicrystalline thin-film Si that was patterned
 4575 with regular SiNWs. This figure shows that the reactive ion etching doesn't interfere with the crystal orientation
 4576 of the substrate. All wires are perpendicular to the surface. Furthermore, even wires with a grain boundary
 4577 inside them remain in a regular shape. Reprinted with permission from [716], Sebastian W. Schmitt, Florian
 4578 Schechtel, Daniel Amkreutz, Muhammad Bashouti, Sanjay K. Srivastava, Björn Hoffmann, Christel Dieker,
 4579 Erdmann Spiecker, Bernd Rech, and Silke H. Christiansen, Nanowire Arrays in Multicrystalline Si Thin Films
 4580 on Glass: A Promising Material for Research and Applications in Nanotechnology, Nano Lett., 12 (2012) 4050.
 4581 Copyright © 2012 American Chemical Society. Permission granted.

4582

4583 **10.2 Nanowire solar cell concepts**

4584 SiNWs open up new prospects in fundamental research and applications. Lieber and
4585 co-workers created the first reported single nanowire solar cells in axial [717] and radial
4586 [718] geometry and reached efficiencies of 3.4% in the case of radial/coaxial cells and 0.5%
4587 in case of the axial geometry. These fundamental studies showed the potential and limitations
4588 of nanowire-based solar cells and influenced the whole research community since then.

4589 In this review we focus more on realistic applications and industry relevant
4590 realizations of nanowire solar cells. Therefore we will present several different concepts of
4591 radial or axial geometries, bulk or thin-film based SiNWs and random or organized SiNW-
4592 based solar cells. In general, nearly all concepts that are realized in planar geometries, which
4593 were already presented in this article, can be transferred to nanowire-based solar cells.

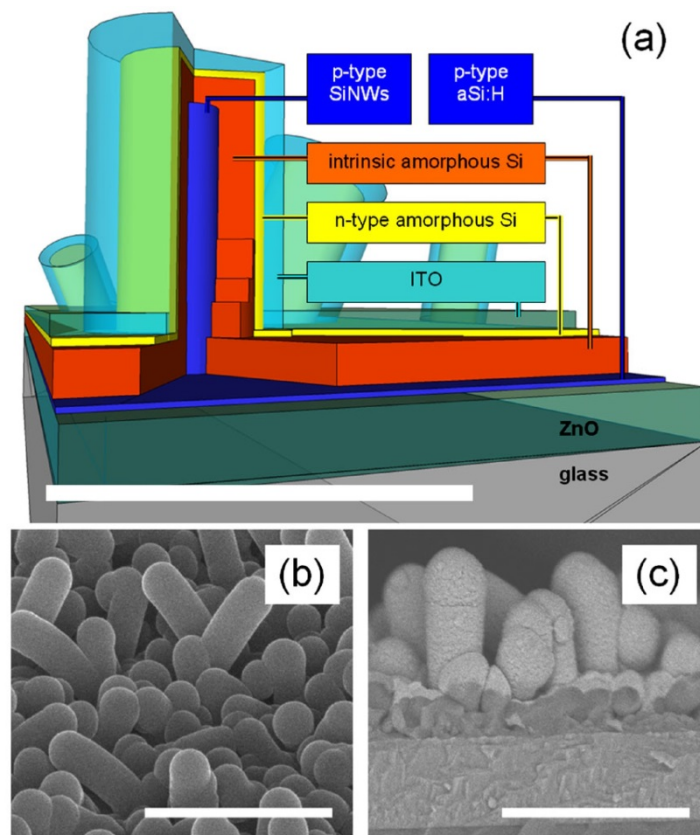
4594 **10.2.1 Axial and radial junctions**

4595 Nearly all SiNW solar cell concepts with a reasonable efficiency or a promising
4596 geometry are based on radial junctions instead of axial junctions, since one of the major
4597 advantages in a radial concept is the decoupling of absorption path and charge carrier
4598 separation path. Nevertheless, there are several realizations of axial solar cells reported. In
4599 2004 Peng et al. fabricated p-n junctions along SiNW carpets by using MCEE on planar p-n
4600 junction wafers [719]. Even though the realized junctions were not suitable for solar cells,
4601 Sivakov et al. were able to use a similar preparation on multicrystalline Si thin-films on glass
4602 to form axial p⁺-n-n⁺ junctions which showed a conversion efficiency of 4.4% [709].

4603 A radial junction geometry is more and more preferred for SiNW-based solar cells in
4604 the last years. In 2005, Kayes, Atwater and Lewis published a theoretical modelling of radial
4605 p-n junctions in Si nanorods and the model showed that a large increase in efficiency is
4606 possible compared to planar p-n junctions [720]. The calculations also showed the crucial
4607 points that had to be concerned: low minority-carrier diffusion lengths compared to the

4608 optical thickness and low depletion region recombination. This concept shows the potential
 4609 of utilization of lower quality Si materials and cost reduction towards a possible mass
 4610 production.

4611 In the early days (2007-2008) of radial SiNW solar cell development mostly VLS
 4612 grown SiNWs were used [535,703], but the efficiency only reached very low values of 0.1%.
 4613 Nevertheless, these initial studies found the crucial points which have to be optimized, like
 4614 the contamination with catalyst atoms or the junction quality. Recently, VLS grown SiNWs
 4615 undergo a renaissance, as Cho et al. prepared SiNWs with Sn as a catalyst and reached nearly
 4616 5% efficiency [721]. Their concept uses a crystalline p-type Si core with intrinsic and n-type
 4617 a-Si:H shells grown on ZnO:Al covered glass, as shown in Fig. 80. One year later in 2013,
 4618 the same group improved their cell concept to an excellent efficiency of 8.14% by optimizing
 4619 the nanowire density [722].

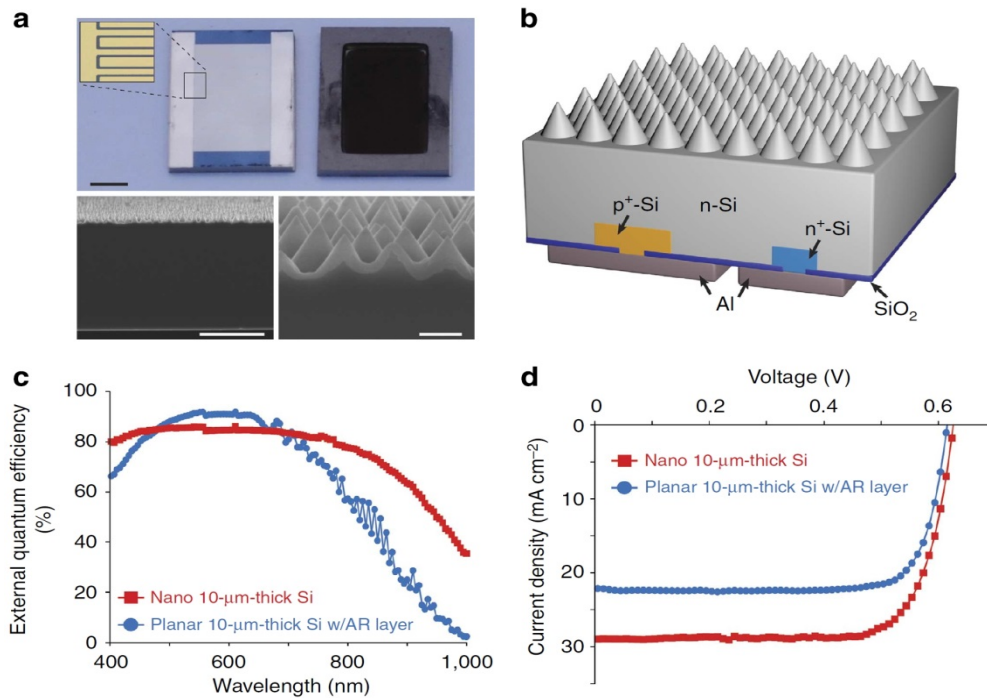


4620

4621 Fig. 80 (a) Schematic of a p-c-Si/i-a-Si:H/n-a-Si:H junction geometry on glass substrate. The SiNWs are grown
 4622 on ZnO covered glass and both SiNWs and substrate are subsequently covered by an intrinsic and an n-type a-Si

4623 layer. A conformal coating with ITO forms the contact. (b) tilted, and (c) cross-section SEM micrograph
4624 showing the conformal coating wrapping the CVD grown SiNWs. Reprinted with permission from [721],
4625 Jinyoun Cho, Benedict O'Donnell, Linwei Yu, Ka-Hyun Kim, Irène Ngo and Pere Roca i Cabarrocas, Sn-
4626 catalyzed silicon nanowire solar cells with 4.9% efficiency grown on glass, Prog. Photovolt: Res. Appl., 21
4627 (2013) 77. Copyright © 2012 John Wiley & Sons, Ltd. License number 3493530552428.
4628

4629 In terms of scalability, and thus industry relevance, top-down prepared SiNWs play a
4630 more important role. In 2010, Garnett and Yang presented radial p-n junction SiNW solar
4631 cells that were prepared by assembly of monolayers of silica beads and subsequent DRIE,
4632 followed by boron diffusion, and reached an efficiency of 5.3% [715]. In 2012 Oh et al.
4633 managed to reduce both Auger and surface recombination in MCEE prepared black Si by
4634 using a special chemical treatment to reduce the surface area of the SiNWs by smoothening
4635 the nanoscale roughness of the sidewalls and thus reached an excellent efficiency of 18.2%
4636 [723]. The authors also suggest that efficiencies above 20% can be reached by optimizing the
4637 nanostructure and by improving the passivation of the back while using point contacts.
4638 Another promising concept was published by the group of Yi Cui from Stanford University in
4639 2013 and describes the formation of Si nanocones on top of ultrathin Si layers [724]. The RIE
4640 fabricated nanocones (Fig. 81) have the advantage of strong light scattering and absorption
4641 while the surface area is much smaller in comparison to long wires. Furthermore they used an
4642 all-back-contact scheme to reduce Auger recombination losses and reached an overall
4643 efficiency of 13.7%.
4644



4645

4646 Fig. 81 (a) Photographs of the metallized back side (top, left side) and the nanostructured front side (top, right
 4647 side) as well as SEM cross section micrographs of the complete thin-film device (bottom, left side) and the Si
 4648 nanocones (bottom right side). (b) schematic diagram of the device showing the highly doped, all back-contact
 4649 design. (c) external quantum efficiency of a nanostructured 10 μm thin Si solar cell and a planar control device
 4650 with the same thickness. (d) J-V measurements of nanostructured and planar solar cells, showing that the
 4651 nanostructuring leads to a massive increase in current density. Reprinted with permission from [724], Sangmuo
 4652 Jeong, Michael D. McGehee & Yi Cui, All-back-contact ultra-thin Si nanocone solar cells with 13.7% power
 4653 conversion efficiency, Nature communications, 4 (2013) 2950. Copyright © 2013 Nature Publishing group.
 4654 License number 3493530933967.

4655

4656 10.2.2 Substrate variations and random versus organized SiNWs

4657 During the development of nanowire based solar cells, mostly c-Si wafers were used
 4658 as substrate for growth or etching of wires. Over the last years new processes have been
 4659 developed to grow SiNWs on cheap substrates like glass [709] or metal foils or to etch
 4660 SiNWs into multicrystalline deposited Si thin-films on cheap substrates [716]. In order to
 4661 reach cost competitiveness with industrial scale production, SiNWs need to be realized on
 4662 substrates that are suitable for existing PV equipment.

4663 The distinction between bottom-up growth and top-down etching are the random
 4664 distribution and organized distribution of SiNWs respectively. The NW axis direction as well
 4665 as the diameter can either be controlled or remain random. Depending on the process this
 4666 control can easily be achieved or needs a very complex treatment. NW orientation and

4667 diameter distribution play an important role for the optical properties of the NW carpet, while
4668 the electrical properties are mostly influenced by the diameter.

4669 The diameter of bottom-up VLS grown SiNWs can be narrowed down easily by the
4670 size of the initial metal catalyst particles. The orientation of VLS grown NWs on the other
4671 hand, can only elaborately be controlled by a very clean environment and the usage of
4672 problematic precursors like SiCl₄ [701]. On the contrary, mats from randomly oriented
4673 SiNWs can also show superior optical properties and they can even be explained by statistical
4674 models as Brönstrup et al. have shown [725].

4675 Recently, top-down etched SiNWs are showing a higher relevance for nanostructured
4676 solar cells. Both wet-chemical etching as well as reactive ion etching yields highly absorbing
4677 randomly shaped SiNWs without using any pre-structuring or lithography steps. The
4678 advantage of high absorption is counteracted by the poor electrical quality, since a random
4679 etching leads to a large distribution of diameters and severe surface roughness. If the wires
4680 are too thin, they can be fully depleted or absorb only a little amount of light, while too thick
4681 wires could show a decreased charge carrier separation due to long needed diffusion lengths
4682 to the contact. Therefore many groups try to gain control over the SiNW diameter to gain
4683 defined electrical properties, without losing the advantage of high optical absorption.

4684 **10.3 Current Status, challenges**

4685 There are many challenges when it comes to a possible commercialization of SiNW
4686 solar cells. One of the main problems of SiNW solar cells is the high surface recombination.
4687 Currently, two different approaches try to minimize these effects: The first method is to
4688 minimize the surface area by tuning the geometry of the SiNWs, especially the aspect ratio.
4689 Here, a combination of electro-optical modeling and experimental investigations is
4690 promising. The second approach is the optimization of surface passivation to reduce the
4691 recombination. For high aspect ratio structures the atomic layer deposition is the most

4692 valuable technique that is also compatible with PV industrial mass production. For instance,
4693 the passivation with ultrathin Al₂O₃ layers is investigated very intensively in the last years
4694 and shows promising results.

4695 **10.3.1 Challenges for mass production**

4696 On the way to an integration of SiNWs into commercial mass production many
4697 challenges have to be overcome. The large-scale synthesis is still a large problem for both
4698 bottom-up and top-down processes. The drawbacks of VLS growth are the needed high-
4699 temperature reactors, the typically used catalyst material and the general reactor design,
4700 which is limited to substrates with sizes of a few cm² at the moment. Furthermore, an
4701 integration into existing PV production lines is a challenge. On the other hand, RIE is a
4702 promising technique that can be scaled to large substrates, but here the masking layer of
4703 typically used micro- or nanospheres is the problem. A solution to this obstacle could be
4704 nanoimprint lithography which could replace the nanosphere mask and offers the possibility
4705 of large-scale and fast patterning.

4706 Even if SiNW solar cells reach high-efficiencies while remaining cheaper than typical
4707 Si thin-film solar cells, they have to be integrated into a complete PV line including module
4708 formation and packaging. Here, a drop-in replacement of typical wafers without the need of
4709 new processes and equipment would be the best solution. However, this is mainly ignored in
4710 the research community by now. So far, the competition against planar devices, which are
4711 extremely advanced because they have been improved with immense investment over the
4712 past several decades, remains tough. A large-scale industrial involvement in the development
4713 of SiNW solar cells would boost their competitiveness. However, in times of hard
4714 competition in the PV market at the moment, the industry mainly concentrates on the further
4715 improvement of their running products instead of investing in novel structures. Therefore,
4716 academic research needs to show the superior properties of SiNWs in large-scale solar cells.

4717 **10.4 Future outlook on promising concepts**

4718 Since the field of SiNW solar cell research is still in the early stages of development,
4719 there exist several competing PV cell architecture concepts. From the viewpoint of
4720 fundamental research, SiNWs are still under intense investigation.

4721 Parallel to the improvement of existing concepts, there is still a large community for
4722 innovative and new ideas, such as hybrid inorganic-organic solar cells [726-728], or
4723 graphene for Schottky junction solar cells [729] or novel contact materials [730].

4724 SiNW solar cells are still a very complex topic with a multitude of subfields. So far, no
4725 concept was able to show its superiority and thus many of them are under investigation
4726 concurrently. Here, many challenges remain for both research and industry.

4727 To gain a more detailed overview about the field, we suggest some of the recent reviews
4728 by Peng & Lee [731], Kuang et al. [694], Garnett et al. [732], and Ramanujam & Verma
4729 [16].

4730 **11. GaAs and its related NWs for solar cells**

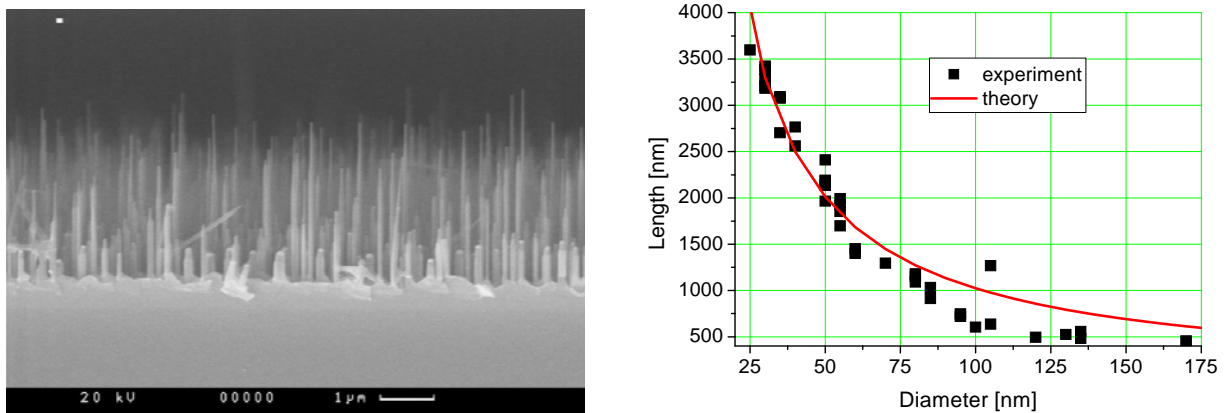
4731 III-V compound semiconductors are very promising materials for NW based PV
4732 devices due to their high absorption co-efficient (e.g. $10^6/\text{cm}$ at $0.3 \mu\text{m}$ for GaAs) and
4733 availability of direct bandgaps within the solar spectrum. Aligned NW arrays are very
4734 promising building blocks for various nanoelectronic devices, such as nanolasers [733,734],
4735 field-effect transistors [735], light-emitting diodes [736, 737] and field emitters [738,739].
4736 Compared to polycrystalline films, vertically oriented NW arrays are particularly
4737 advantageous for PV applications, because the oriented geometry provides direct conduction
4738 paths for photogenerated carriers to transport from the junction to the external electrode,
4739 thereby resulting in high carrier collection efficiency [740, 741]. Moreover, NW arrays have

4740 significantly smaller optical reflectance and enhanced light absorption in comparison to thin-
4741 films due to the foresting effect [742,743]. It is important to note that due to the strain
4742 accommodation at the NW sidewalls, NWs are less restricted by lattice mismatch, which
4743 provides greater freedom for bandgap engineering and the substrate selection [744]. Thus, a
4744 much wider range of material bandgaps may be used in multi-junction NW cells to optimize
4745 solar cell efficiency without the restriction of lattice matching in comparison to the planar
4746 geometry.

4747 **11.1 Basics of GaAs NWs growth**

4748 As for GaAs based arrays, in most cases, NWs can be formed via the so-called VLS
4749 growth mechanism [695] using different epitaxial techniques, such as MOCVD [745-747],
4750 magnetron sputtering [748] or MBE [749-756]. The main stages of the NW growth are
4751 following: (i) the formation of a liquid droplet on the substrate surface (for instance, Au or
4752 another metal), (ii) the deposition of the desired material onto the surface. The droplet on the
4753 surface acts as catalyst, the growth of the NWs is dictated by the diameter and the appropriate
4754 place of the droplet. The catalyst in the liquid state should not wet the semiconductor surface,
4755 which is necessary for formation of three-dimensional seeding droplets and nucleation of
4756 NWs. Additionally, a solution of the catalyst and the semiconductor should have a reasonable
4757 melting point (lower than typical growth temperatures). Since NWs feature the predominant
4758 direction of growth along the [111] axis, the wafers with orientation $\langle 111 \rangle$ (for example, Si
4759 $\langle 111 \rangle$ or GaAs $\langle 111 \rangle$ B) are used in order to obtain the crystals oriented perpendicularly to
4760 the surface. In most cases, at least for MOCVD, magnetron sputtering or MBE, the growth is
4761 conducted via so called diffusion driven mechanism, where the NW length exceeds several
4762 times the effective thickness of deposited material. In the majority of cases, the dependence
4763 of the length (L) of NW on their radius (R) is power law, $L \sim 1/R$ and $L \sim 1/R^2$ [757,758].

4764 Figure 82 shows the typical SEM image and corresponding L(R) dependency for GaAs.
 4765 Similar behavior was observed for (Al, Ga)As NWs.



4766

4767 Fig. 82 SEM image and dependence of the length on diameter of GaAs nanowires grown by molecular beam
 4768 epitaxy (MBE) on GaAs<111>B wafer. The growth temperature was set at 585°C. GaAs layer effective
 4769 thickness was 500nm. The deposition rate of GaAs was 1.0 monolayer/s. MBE technique is mainly used for
 4770 GaAs nanowire growth due to precise control over the shape, height, surface density and doping of the
 4771 nanowires. Nanowire growth is conducted via diffusion driven mechanism, where the nanowire length exceeds
 4772 several times the effective thickness of deposited material. Data from [757], Diffusion-induced growth of GaAs
 4773 nanowhiskers during molecular beam epitaxy: Theory and experiment, V. G. Dubrovskii, G. E. Cirlin, I. P.
 4774 Soshnikov, A. A. Tonkikh, N. V. Sibirev, Yu. B. Samsonenko, and V. M. Ustinov, Phys. Rev. B 71 (2005)
 4775 205325. Permission granted. License number 3582351478488.
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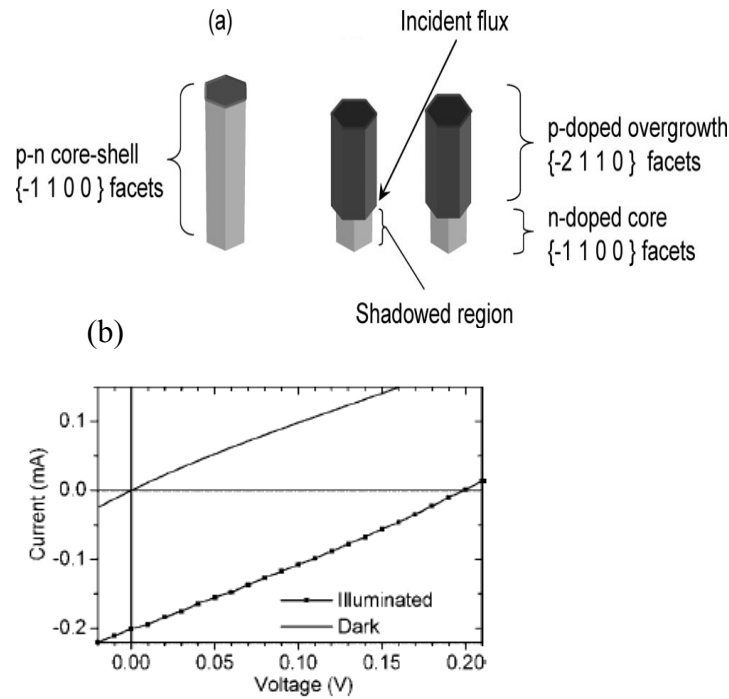
4777 One of the most important features of MBE growth is the ability to precisely control
 4778 the shape, height, diameter and surface density of the NWs by an appropriate choice of
 4779 technological parameters by exploring the diffusion induced growth mode, as well as to
 4780 monitor the formation and time evolution of NWs *in situ* by the reflection high-energy
 4781 electron diffraction (RHEED) technique [759]. These peculiarities (i.e. control over growth
 4782 parameters, doping possibility, growth processes monitoring) allow one to fabricate first PV
 4783 prototypes based on GaAs NWs [760-762] grown by MBE.

4784 11.2 GaAs NW based PV structures

4785 A coaxial GaAs NWs structure in which a doped NW core is surrounded by a shell of
 4786 opposite doping type, forming a core-shell p-n junction grown on GaAs<111>B wafer was
 4787 proposed and successfully realized [760]. Schematic diagram of the MBE grown GaAs
 4788 nanowire and I-V characteristics are presented in Fig. 83 (a) and (b) respectively.

4789 **11.2.1 PV devices based on GaAs NW arrays**

4790 It is well known that Si is commonly used n-type doping impurity during
4791 conventional MBE. In VLS growth, in contrast, Si incorporation may be amphoteric and both
4792 n- and p-type conductivity may appear, depending on Ga or As site substitution [760]. To
4793 avoid this, group VI element tellurium was used. In this study, core-shell p-n structures were
4794 fabricated by switching from n- to p-type doping during the growth. Tellurium from a GaTe
4795 loaded effusion cell was used for n-type doping, and beryllium from an effusion cell was used
4796 for p-type doping. PV devices were fabricated in five steps [760]. First, a ~ 200 nm layer of
4797 SiO_x was deposited over the NWs by PECVD. Next, the sample was covered with Shipley
4798 S1808 photoresist by spin coating. After the photoresist application, the sample was placed in
4799 an oxygen plasma reactive ion etch chamber to remove the photoresist from the tip of the
4800 oxide-covered nanowires. Next, using the photoresist as an etch mask, the oxide was removed
4801 from the tip of the NWs using buffered HF etch followed by acetone rinse to remove the
4802 photoresist. This process isolates the contact to the tips of the NWs and prevents direct
4803 contact to the thin-film that grows simultaneously between the NWs. Either opaque contacts
4804 or transparent contacts were deposited on top of the NWs for top contact. The procedure was
4805 finalized by the contact deposition on the back of the wafer. As a result, several PV
4806 prototypes were synthesized with a maximum conversion efficiency of 0.83%. Corresponding
4807 I-V data taken in the dark and under illumination is presented in Fig.83 (b).



4808

4809

4810 Fig. 83 (a) Schematic diagram of the MBE grown p-n core-shell type GaAs nanowire grown by switching
 4811 doping type during the growth, (b) I-V curves of optimized sample in dark and illuminated conditions. The
 4812 GaAs nanowire samples are grown by MBE on GaAs<111>B wafer. Si is used as n-type dopant. In VLS
 4813 growth, Si incorporation may be n-type or p-type depending upon Ga or As site substitution. Therefore, group
 4814 VI element tellurium (Te) from a GaTe loaded effusion cell is used for n-type doping, and beryllium from an
 4815 effusion cell is used for p-type doping. A maximum efficiency of 0.83% has been obtained. Figure 83 from
 4816 [760], Josef A. Czaban, David A. Thompson and Ray R. LaPierre, GaAs Core-Shell Nanowires for
 4817 Photovoltaic Applications, Nano Lett., 9 (2009) 148. Copyright © 2008 American Chemical Society.
 4818 Permission granted.

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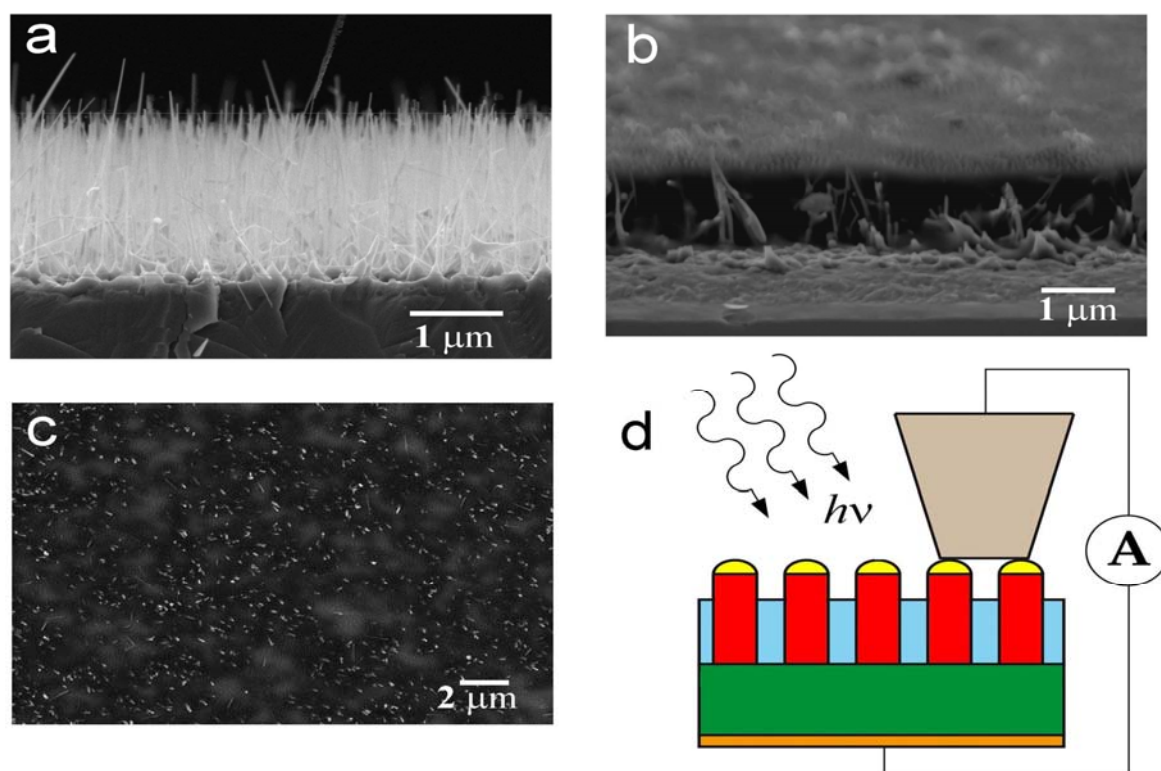
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Another PV prototype concept was proposed in Ref. [756]. Here, GaAs p-type NW
 arrays are grown on the n-type GaAs<111>B wafer at different wafer temperatures.
 Additionally, to prepare the p-n junction, the spaces between the NWs are filled with
 insulating photoresist (Poly (methyl methacrylate) or PMMA) via spin coating. In this
 particular case, PMMA was used for electrical insulation and contact mechanical support.
 After photoresist deposition, the sample surface is treated in oxygen plasma until the tips of
 GaAs NWs are exposed. Conventional ohmic contacts for the backside of n-type wafer are
 fabricated by electron-beam evaporating of AuGe (30nm) and Ni/Au (10/150nm)
 combination having resulting contact resistance $\sim 1 \times 10^{-6} \text{ Ohm/cm}^2$. After each stage, the
 samples are studied by applying the SEM technique as shown in Fig.84 (a-c), together with
 schematics of the device structure. I-V characteristics are measured using a Keithley 238

4831 source meter (Fig.84d). The samples are placed on a Cu base from backside of the wafer; a
 4832 metallic sharp tip ($D \sim 0.5\text{mm}$) is used as top contact to the NWs/PMMA array. The efficiency
 4833 is determined by illuminating the structures with one sun illumination. For the given
 4834 geometry, the highest conversion efficiency 1.65%, with J_{sc} of $27.4\text{mA}/\text{cm}^2$ and the V_{oc} of
 4835 245 mV and fill factor of 25% is achieved when the substrate growth temperature was set at
 4836 550°C .



4837

4838 Fig.84. SEM images taken at different stages of device structure preparation, (a) as-grown GaAs NWs array, (b)
 4839 after insulating photoresist (PMMA) deposition for electrical isolation and mechanical support, (c) top view of the
 4840 resulting structure (after oxygen plasma treatment), and (d) schematic view of the device testing structure.
 4841 The MBE growth of beryllium-doped GaAs NWs on n-type GaAs<111>B wafer is carried out at wafer
 4842 temperature 550°C with GaAs growth rate at 1 monolayer/s. An efficiency of 1.65% has been obtained due to a
 4843 low fill factor of 0.25. From [761], G.E. Cirlin, A.D. Bouravleuv, I.P. Soshnikov, Yu.B. Samsonenko, V.G.
 4844 Dubrovskii, E.M. Arakcheeva, E.M. Tanklevskaya, and P. Werner, Photovoltaic Properties of p-type GaAs
 4845 Nanowire Arrays Grown on n-Type GaAs(111)B wafer, *Nanoscale Res Lett.*, 5(2010)360. Permission granted.
 4846

4847 Different approach was utilized in Ref. [762,763] to combine GaAs and polymer
 4848 films. These hybrid solar cells were fabricated by spin-coating poly (3-hexylthiophene)
 4849 (P3HT) polymer onto vertically aligned n-type GaAs NW arrays synthesized by MBE [762]
 4850 and MOCVD [763]. In both approaches, GaAs<111>B wafer was used. In the last case,

4851 patterned GaAs nanopillars were used as a PV prototype base. According to the scheme
4852 [762], the highest occupied molecular orbital (HOMO_{P3HT}) and lowest unoccupied molecular
4853 orbital, (LUMO_{P3HT}) for P₃HT is -4.76 eV and -2.74 eV, respectively. The electron affinity
4854 of GaAs is $\chi_{\text{GaAs}} \sim 4.07$ eV. Therefore, GaAs NWs are suitable as electron acceptor, and P₃HT
4855 as the electron donor. For this concept, 1.04% and 1.44% conversion efficiencies were
4856 achieved, respectively, showing alternative and less expensive approach to fabricate NWs
4857 based solar cells.

4858 Another way to increase the solar cells efficiency was demonstrated in [764] where p–
4859 n junction GaAs NW solar cell devices of two types consisting of ITO contact dots or opaque
4860 Au finger electrodes, were investigated. Lateral carrier transport from the NWs to the contact
4861 fingers was achieved via a p-type GaAs surface conduction layer. NWs between the opaque
4862 contact fingers had sidewall surfaces exposed for passivation by sulphur. Using this
4863 approach, the relative cell efficiency was increased by 19% upon passivation. Before and
4864 after passivation, efficiency was 1.8% and 2.04% respectively.

4865 It is known that Au-assisted VLS growth can lead to an unintentional Au
4866 contamination [765]. To overcome this disadvantage, it is desirable to utilize the same
4867 material serving the NWs growth catalyst. One of the major steps towards the new PV
4868 prototypes was an introduction of self catalyzed NWs growth where the metal droplet
4869 (catalyst) is a seed particle that is a constituent of the NW itself, e.g. Ga for GaAs NWs
4870 growth [766-771]. A key point is the formation of liquid Ga nanoparticles at the initial stage
4871 in the openings of SiO_x grown on the GaAs<111>B wafer [766], or in a native oxide layer on
4872 the Si<111> wafer [767].

4873 In case of GaAs/Si self catalyzed NWs, the growth procedure is as follows: before
4874 introduction into the growth chamber, the wafers are chemically treated in HF (10% in DI
4875 water) for 1 min, and then rinsed in de-ionized water. Before the growth of NWs, the wafer

4876 temperature is increased to the desired value within the range 560°C-630°C, and is kept
4877 constant during the whole growth process. In this temperature window, a native oxide layer
4878 on Si<111> wafer loses continuity, and openings (i.e. the holes penetrating through the oxide
4879 towards the wafer surface) are formed. The surface density of those openings depends on the
4880 temperature. Above 630°C, the oxide layer is completely desorbed, as detected by the
4881 corresponding transformation of RHEED pattern. After the formation of openings, the Ga
4882 flux is supplied to the surface for several seconds, while the arsenic shutter is closed. This
4883 initiates the formation of Ga droplets in the openings. When the arsenic flux is switched on,
4884 the NW growth is started after an incubation time. The latter is clearly detected by the
4885 transformation of the RHEED pattern and typically amounts to 2-10s, depending on the
4886 temperature. During the NW growth, the RHEED pattern features pronounced 3D spots of
4887 cubic zinc blende phase regardless of the temperature. The spot structure does not change
4888 during the whole growth process excluding the very final stage after the Ga shutter is closed.

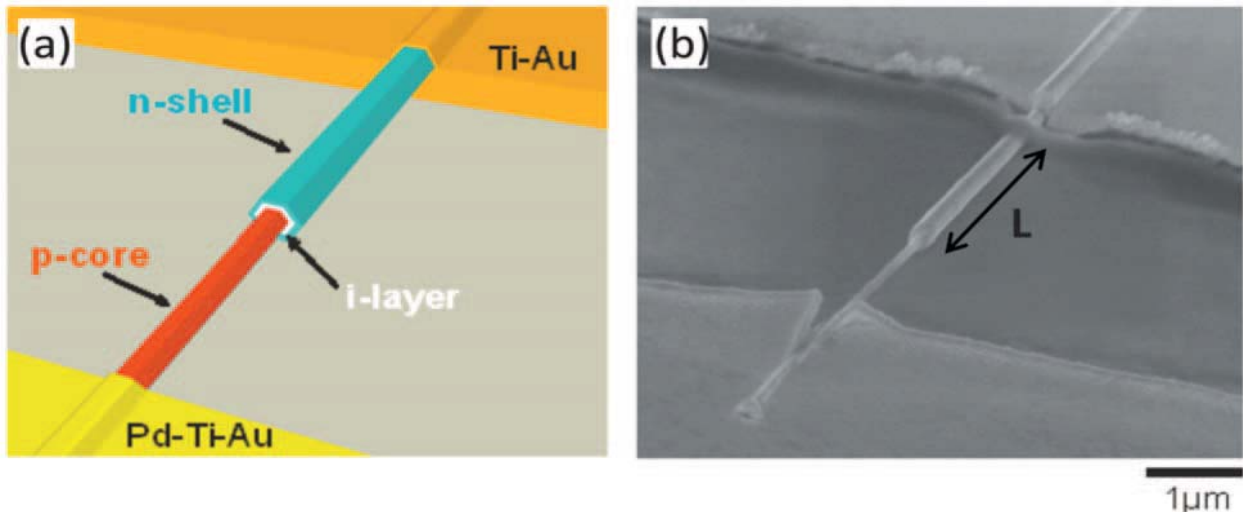
4889 The ability to position regularly the group III droplets in the holes patterned in the
4890 oxide film (by using, e.g. e-beam lithography or focused ion beam techniques) is very
4891 attractive to tune the spacing between the NWs, and hence to maximize light absorption.
4892 Additionally, the self-assisted process is compatible with III-V integration on Si platform,
4893 which will lead to lower cost PV devices. Possible device structures based on self-catalyzed
4894 GaAs NWs are presented in the next section.

4895 **11.2.2 PV devices based on single GaAs NW**

4896 One of the first demonstrations of the self-catalyzed p-i-n radial GaAs NWs applied to
4897 the PV devices was presented in [771], where the fabrication procedure was as follows: GaAs
4898 <111>B wafers coated with a sputtered 10nm thick SiO₂ were used as substrates. The NWs
4899 growth was carried out at a nominal GaAs growth rate of 0.25Å/s, arsenic partial pressure of
4900 2×10^{-6} mbar (Ga rich conditions), a temperature of 630°C. The core of the p-i-n NW junction

4901 was p-type. This was achieved by adding a Si flux during the NWs growth. As it was
4902 mentioned above, Si is an amphoteric impurity in GaAs, and its incorporation can lead to n-
4903 or p-type doping, depending on whether it is incorporated in As or Ga sites, i.e. incorporation
4904 of Si in As (Ga) site results in p-GaAs NW (n-GaAs NW). In the case of Ga-assisted GaAs
4905 NWs growth, incorporation of Si mostly results in a p-type doping [771]. To overcome this
4906 problem, the growth was stopped and the conditions were changed toward planar MBE
4907 growth. Arsenic partial pressure was increased, which resulted in the crystallization of the Ga
4908 droplet. The fabrication of the p-i-n junction continued by the growth of an intrinsic (i) and
4909 an n-type layer on the facets of the nanowires. For this purpose, the temperature was lowered
4910 to 465°C. These conditions had previously been shown to be ideal for growth on {110}
4911 nanofacets [772]. For this growth conditions, due to the lower temperature and higher As₄
4912 beam flux, the incorporation of Si leads to n-type layer [773]. After the growth, the p-i-n
4913 GaAs NW structures were transferred on an oxidized c-Si wafer. The p-type core of the NW
4914 was contacted by first etching a section of the n-type and intrinsic layers of the NW. The
4915 etching was performed with a citric acid solution. Next, a Pd/Ti/Au (70/10/120 nm) layer was
4916 evaporated to form an Ohmic contact with the p-type core. A second lithographic step was
4917 realized with the purpose of contacting the n-type shell. For this, a Ti/Au (10/240 nm) layer
4918 was used. A sketch of the contacted p-i-n nanowire structure is presented in Fig. 85(a). There
4919 the three coaxial layers can be observed, as well as the contacting between the inner and
4920 exterior layers. SEM of a real structure is shown in Fig. 85(b).

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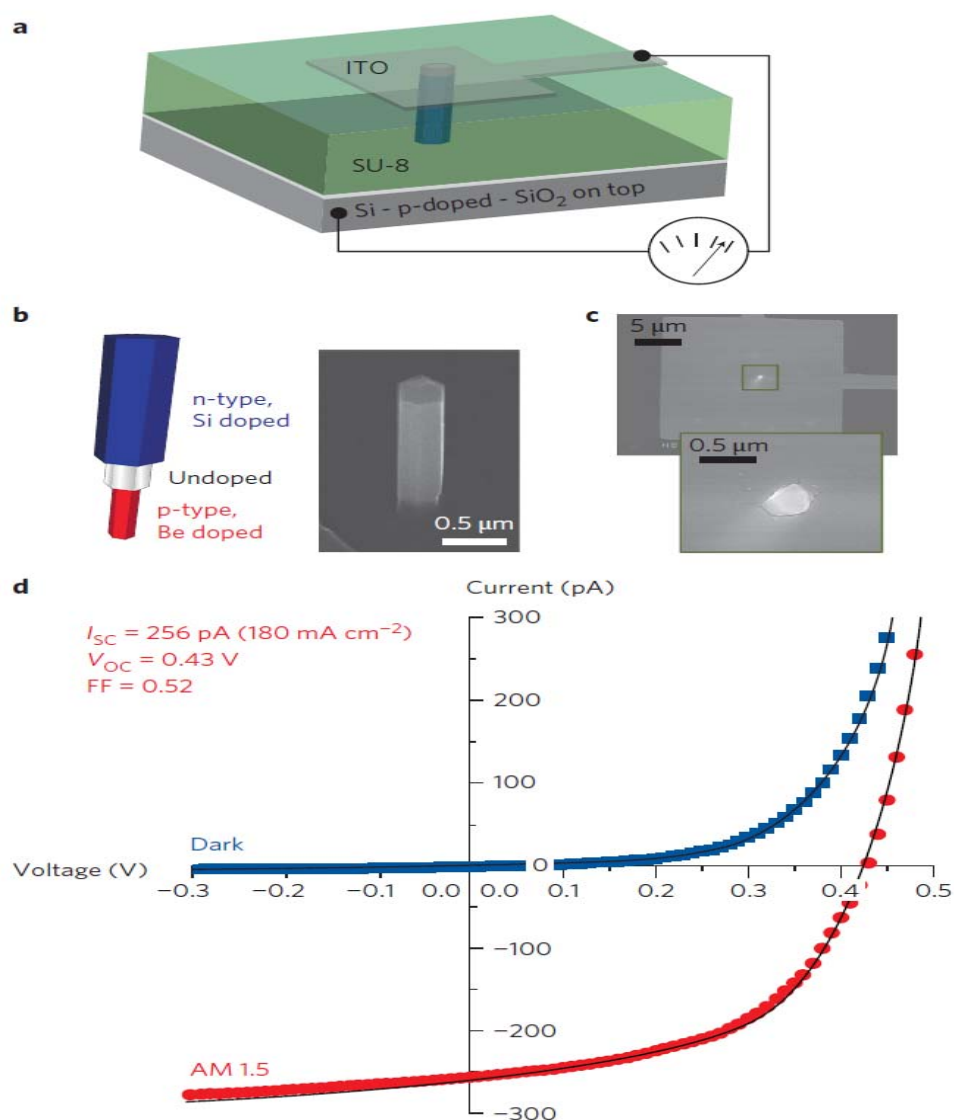


4922 Fig. 85 (a) Sketch of the coaxial p-i-n GaAs nanowire structure showing the contacts to the p-type inner core
 4923 and n-type outer shell, and (b) SEM of a typical PV device. After fabrication, p-i-n GaAs nanowire structure is
 4924 transferred on an oxidized c-Si wafer. The p-type core of the NW is contacted by first etching a section of the n-
 4925 type layer and then intrinsic layer of the NW. Citric acid solution is used as an etchant. For p-type core ohmic
 4926 contact, evaporated palladium-titanium-gold is used. For n-type shell contact, titanium-gold is used. From [771],
 4927 C. Colombo, M. Hei, M. Grätzel and A. Fontcuberta i Morral, Gallium arsenide p-i-n radial structures for
 4928 photovoltaic applications, *Appl. Phys. Lett.* 94(2009)173108. Copyright © 2009 American Institute of Physics.
 4929 License Number 3486980323906.
 4930

4931
 4932 To further characterize the p-i-n junction, the light emitted by the NW in forward bias
 4933 was measured (which corresponds to the regime in which the junction works as a light
 4934 emitting diode) at room temperature. The emission peak at 1.42 eV is in good agreement with
 4935 bandgap of GaAs. The existence of electroluminescence at room temperature constitutes a
 4936 further proof of the quality of the p-i-n junction in the NW, crystallinity and optical quality.
 4937 The efficiency of the NW device was measured under 1.5 AM illumination conditions. The
 4938 total efficiency was calculated by dividing the maximum generated power density by the total
 4939 incident energy density at 1.5 AM. The total area considered was the projected area of the p-
 4940 i-n junction. For the best sample, a value of 4.5% was obtained with fill factor equal to 0.65.

4941 Very impressive result was obtained recently based on the GaAs single NW solar
 4942 cells, grown on a c-Si wafer, where the p-type is contacted through a highly doped wafer and
 4943 the n-type through a transparent top contact [774]. Here, the NWs were grown on oxidized
 4944 Si<111> with 100nm apertures using a self-catalyzed method. The p-doping of the core was
 4945 achieved by adding a flux of beryllium during axial growth. The shell was obtained at lower

4946 wafer temperature, the procedure used before in Ref. [771], and the n-type doping was
 4947 obtained by adding Si at this growth stage. Next, SU-8 was spun onto the wafer. An oxygen
 4948 plasma etching was then performed to expose the NW tip. The top contact was defined by
 4949 electron-beam lithography followed by evaporation of ITO, and the bottom contact was
 4950 obtained by gluing Ag to the back side of the structure. In Fig. 86 (a-d) a sketch of the device
 4951 structure, corresponding microscope images, and I-V characteristics are presented.



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 4955

4956 Fig. 86. (a) Schematic diagram of the vertical p-i-n type single nanowire device connected to a p-type c-Si wafer
 4957 by epitaxial growth, (b) Left side: doping structure of the GaAs nanowire. The p-type core is in contact with the
 4958 doped c-Si wafer and the n-type shell is in contact with the ITO. Right side: SEM image of a GaAs nanowire

4959 solar cell before adding the top contact, (c) SEM images of the device seen from the top electrode, (d) I-V
4960 characteristics of the device in the dark and light under AM 1.5G illumination. From [774], Peter Krogstrup,
4961 Henrik Ingerslev Jørgensen, Martin Heiss, Olivier Demichel, Jeppe V. Holm, Martin Aagesen, Jesper Nygard,
4962 Anna Fontcuberta i Morral, Nature Photonics 7(2013)306. Nature publishing group, copyright © 2013
4963 Macmillan Publishers Limited, Permission granted.

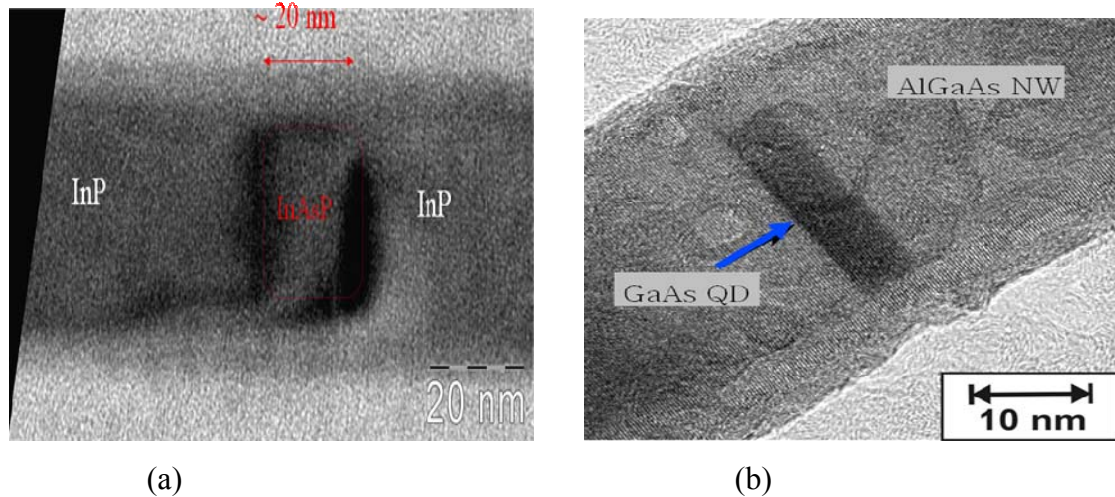
4964
4965 The authors observed a remarkable boost in absorption in single NW solar cells and
4966 explained this observation as due to a vertical configuration of the NW, and by a resonant
4967 increase in the absorption cross-section. For the best case, the PV device exhibits a J_{sc} of
4968 $180\text{mA}/\text{cm}^2$ when normalized to the projected area. This leads to an apparent efficiency of
4969 40%, which is beyond the S-Q limit [22], and opens a new route to third generation solar
4970 cells.

4971 **11.3 PV devices based on other III-V material NW arrays**

4972 As concern to another III-V materials used for the NW based solar cells prototypes,
4973 one should mention InP/Si<111> NWs double-junction structure grown by MOVPE [775],
4974 InGaAs/Si<111> NWs using MOVPE [776], MOCVD grown InGaP/GaAs<111>B NWs
4975 [777], GaAsP/Si<100> MOCVD grown NWs [778], GaAsP/Si<111> NWs using MBE [779]
4976 etc. More detailed information can be found here [780]. But one of the results has to be
4977 outlined separately. The record efficiency for a Au-assisted InP axial p-i-n nanowire array on
4978 an InP<111>B substrate, which was achieved recently an efficiency of 13.8% [781]. This
4979 high value is attributed to the use of the patterned array, more optimal geometry, and lower
4980 SRV in indium phosphide material.

4981 An important aspect, aiming to increase the absorption of the light in the NW based
4982 PV structure, is the use of a combination of several materials inside a NW. Among the
4983 different geometries (e.g. core/shell homo- and heterostructures, or double-junction
4984 structures), a structure consisting of the nanostructures with combined dimensionality,
4985 namely QD inside a nanowire, has additional advantages, such as spreading of the absorption
4986 spectrum and, due to the small sizes, facilitating of the strain relaxation. Recently, a

4987 remarkable progress was achieved in this field. In Fig. 87 (a) and (b), typical transmission
 4988 electron microscopy for the InAsP/InP/InAsP [782] and AlGaAs/GaAs/AlGaAs [783] QD
 4989 inside a NW combined structures are presented. These nano insertions have typically ~5-20
 4990 nm size and exhibit zero-dimensional behavior. Moreover, these structures are optically
 4991 bright up to the room temperature, demonstrating outstanding potential for PV applications.



4992

4993

4994 Fig.87 Transmission electron microscope images for the quantum dot inside a nanowire structure: (a)
 4995 InAsP/InP/InAsP [from 782], and (b) AlGaAs/GaAs/AlGaAs [from 783]. The details of the grown structures are
 4996 presented in the corresponding references. Figure 87 (a) from [782], Maria Tchernycheva, George E. Cirlin,
 4997 Gilles Patriarche, Laurent Travers, Valery Zwiller, Umberto Perinetti, and Jean-Christophe Harmand, Growth
 4998 and Characterization of InP Nanowires with InAsP Insertions, Nano Lett., 7(2007)1500. Copyright © 2007
 4999 American Chemical Society. Permission granted. Figure 87 (b) from [783], V. N. Kats, V. P. Kochereshko, A.
 5000 V. Platonov, T. V. Chizhova, G. E. Cirlin, A.D. Bouravleuv, Yu B Samsonenko, I. P. Soshnikov, E. V.
 5001 Ubyivovk J. Bleuse, H. Mariette, Optical Study of GaAs quantum dots embedded into AlGaAs nanowires,
 5002 Semicond. Sci. Technol., 7 (2012) 015009. Copyright ©2012 IOP Publishing Ltd. Permission granted.

5003

5004 11.4 Future outlook

5005 There is a strong interest in the fabrication of novel PV devices based on III-V
 5006 material NWs, in particular, GaAs NWs. These structures may provide a lower cost, higher
 5007 efficiency devices in PV market. Additionally, different materials combination within a
 5008 single, defect-free NW, may lead to higher absorption efficiency. Nevertheless, further
 5009 investigations are required to make NWs based PV large-scale solar cell commercial devices.
 5010 For better understanding of the processes involved in PV conversion, intensive numerical
 5011 simulation and theoretical approaches with an emphasis on optimizing the NW design has

5012 been performed [784, 785]. Important factors, such as surface charge density, SRV, doping
5013 concentration, and NW geometry were investigated in detail.

5014 The particular interests in this area are: (i) the variation in V_{oc} with NW diameter and
5015 change in J_{sc} with tip length indicates the importance of a monodisperse distribution in NW
5016 dimensions, (ii) the minimum NW diameter should be greater than the bulk and surface
5017 depletion widths, which are determined by the doping concentrations [784] and (iii)
5018 importance of a core-shell geometry of NW solar cells [785]. Based on the analysis of
5019 numerous experimental and theoretical data in this area, the following attributes should be
5020 considered for the use of these NWs for PV applications [780]:

5021 (i) Controlled NW morphology

5022 (ii) Stacking-fault-free crystalline structure

5023 (iii) Orthogonal NWs with optimum diameter, and length to maximize optical absorption

5024 (iv) Patterned arrays using cost-effective processes (perhaps nanoimprint lithography)

5025 (v) Dimensions below the critical thickness or critical diameter to avoid misfit dislocations,
5026 which is very important, in particular, when III-V material NWs are grown on c-Si wafers
5027 [786]

5028 (vi) Removal of catalyst droplets to avoid reflection loss and/or Schottky barrier contacts at
5029 the tip of NWs, and possible elimination of Au as a catalyst due to deep level defects

5030 (vii) Controlled doping for p-i-n junctions

5031 (viii) Surface passivation

5032 **12. Conclusions**

5033 We have reviewed the development and current state of inorganic materials based PV,
5034 with a focus on planar devices and recent developments involving a range of nano-materials.
5035 c-Si based traditional solar cells have dominated the solar cell market for decades, and are
5036 expected to continue playing a dominant role, in particular with recent developments towards
5037 low-cost fabrication. At the same time, other technologies have emerged to address the
5038 limitations and progress the state-of-the-art. For example, a method to overcome optical

5039 shadowing losses completely is to use a back junction design. These cells have shown
5040 efficiencies as high as 24.2%. An important concept is a c-Si based BHJ solar cell. Very
5041 high-efficiency of 25.6% has been reported [246] for BHJ solar cells, and recent simulation
5042 study shows an efficiency of >26%.

5043 Another area of intensive focus is the integration of III-V or metal halide perovskite
5044 based materials on c-Si. This may provide a cost breakthrough for PV technology, unifying
5045 the low-cost of c-Si and the efficiency potential of III-V/c-Si or perovskite/Si multi-junction
5046 solar cells. However, despite the promising potential of these structures, the integration of III-
5047 V on c-Si has been challenging due to mismatches in lattice constants and thermal parameters
5048 of III-V compounds and c-Si, whereas for perovskite/Si cells, the stability of the perovskite
5049 top cell currently appears to be the greatest challenge.

5050 An important challenge for the larger PV community has been to cross the S-Q limit
5051 of solar cell efficiency (29% in case of c-Si). One possible way to achieve this, besides the
5052 use of multi-junction devices based on well-established single-junction cells as mentioned
5053 above, is to use quantum dots. This may include the use of a quantum dot Si absorber layer,
5054 where charge-carriers are collected before they are able to thermalize (hot carrier effect).
5055 Another potential method is to develop solar cells using nano-crystalline Si solar cells. The
5056 use of up-conversion and plasmonics has also garnered immense interest. However, much
5057 further research work needs to be done here to approach the theoretically predicted potential.

5058 Among non-Si based inorganic solar cells, one technology that has been adopted by
5059 the industry has been CIGS solar cells. At the same time, CZTSSe PV technology has
5060 experienced rapid growth both in conversion efficiency and materials understanding, and
5061 future breakthroughs in fabrication methodologies are expected to make this technology a
5062 serious commercial contender. At the same time, the work carried out over the last few years

5063 in perovskite and CdTe solar cells has been significant for both planar and nanostructured
5064 solar cells.

5065 In terms of very nascent technologies, the field of SiNW solar cell research is still in
5066 the early stages of development, and there exist several competing PV cell architecture
5067 concepts. SiNWs are still under intense investigation, and many challenges remain for both
5068 research and industry. Similarly there is a strong interest in the fabrication of novel PV
5069 devices based on III-V material NWs, in particular, GaAs NWs. These structures may
5070 provide lower cost, higher efficiency devices for the PV market. Additionally, different
5071 materials combinations within a single, defect-free NW, may lead to higher absorption
5072 efficiency. Nevertheless, further investigations are required to make NWs based PV large-
5073 scale solar cell commercial devices.

5074

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