

Bulk Nanostructuring Intermetallic Composite Material

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Abstract. The article states the results of a study of the impact rendered by the plastic strain occurring in a high-temperature synthesis product during the thermal explosion of a nickel-aluminum powder mixture on the grain structure, strength and ductility of the Ni₃Al synthesized intermetallic compound.

Keywords: intermetallic compound Ni₃Al, high-temperature synthesis, plastic deformation, ultimate strength and deformation-to-fracture

INTRODUCTION

As structural alloys for high-temperature applications, Ni₃Al intermetallic compound-based refractory nickel alloys hold leading positions in terms of their production volume and use in chemical industry, power industry, aircraft building, space technology, etc. The Ni₃Al intermetallic compound (γ' phase, ordered solid solution) is the main strengthening phase, and its behavior under load largely determines the heat-resistant alloy's lifetime in general. Therefore, the Ni₃Al intermetallic compound is a subject of systematic studies [1]. The use of complex doping is a classical approach to increasing the strength and ductility of the intermetallic compound, including high-temperature conditions, but the doping's potential has been virtually exhausted by now. The use of strength and ductility improving methods in metals and alloys by atomizing the grain structure under severe plastic strain seems to be impossible either, as the Ni₃Al intermetallic compound is characterized by a high susceptibility to brittle intercrystalline fracture. A unique opportunity to obtain the plastic strain of the Ni₃Al intermetallic compound is to expose it to loading it from the melt state in the narrow time interval of intermetallic compound crystallization under the conditions of high-temperature synthesis (SHS) through the thermal explosion of the nickel-aluminum powder mixture of stoichiometric composition (Fig. 1(a)) [2].

The purpose of this study is to investigate the grain formation morphology in terms of its dependence on the degree of the plastic strain of the high-temperature synthesis product as well as its effect on the strength and ductility of the Ni₃Al intermetallic compound.

EXPERIMENTAL PROCEDURES

The effect of severe plastic deformation of a high-temperature synthesis product on the grain structure of the Ni₃Al intermetallic compound synthesized under pressure was observed on intermetallic compound ingots synthesized under pressure in the thermal explosion mode in a nickel (~2.0 μm) – aluminum (~1.0 μm) powder mixture of a stoichiometric composition in a conical open-type mold (Fig. 1(b)).

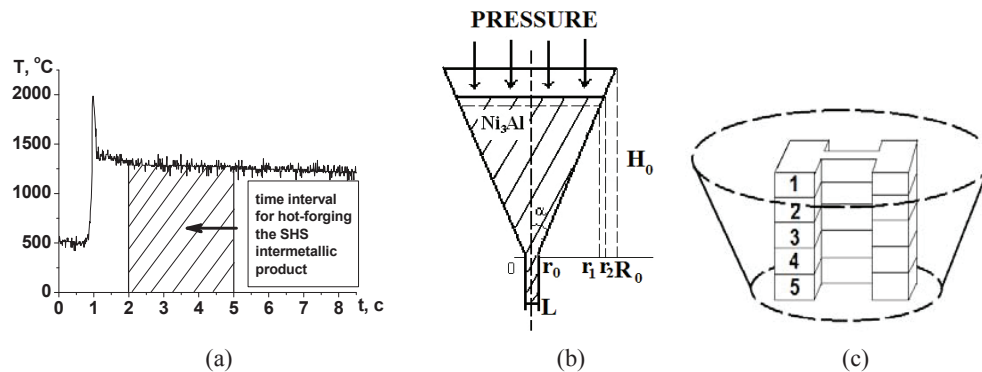


FIGURE 1. Thermogram of the 3Ni +Al powder mixture’s thermal explosion demonstrating the SHS intermetallic product strain time interval (a); the SHS process flow chart for an intermetallic ingot with severe plastic deformation of the SHS product in a conical open-type mold (b); the and method of obtaining samples for the intermetallic compound Ni₃Al tensile tests with various degrees of the SHS product’s plastic strain (c)

The mold diameter was 58.0 mm at the upper part and 7.0 mm at the bottom, the mold was 50 mm high, and the bottom aperture diameter was 7.0 mm. A sample of the rectangular cross section was cut out of the conical intermetallic compact and cut into 30×10×1.5 mm tensile test pieces with a 10 · 4 mm gage length (Fig. 1(c)).

The plastic strain of the Ni₃Al intermetallic compound during its high-pressure synthesis under pressure in a conical mold with subsequent high-temperature synthesis product extrusion was calculated for five equally thick transverse layers of synthesized conical intermetallic compact (Table 1).

The resultant phases in different samples of the intermetallic compound were characterized by the X-ray diffraction (XRD) with a Cu K α radiation at 40 kV and 40 mA. The microstructure of intermetallic alloys was examined using optical metallography (Neophot 32), scanning electron microscopy (SEM-515 scanning electron microscope by Philips with EDAX ECON IV energy-dispersive analyzer of element composition), and transmission diffraction electron microscopy (JEM-2100). The intermetallic compound test specimens were prepared for transmission diffraction electron microscopy by surface ion etching. The samples were tested for tensile strength on the INSTRON machine at a 0.2 mm/min elongation rate.

RESULTS AND DISCUSSION

Microstructure Characteristic

The main phase of all the examined samples of the synthesized alloy is the Ni₃Al intermetallic compound, which is confirmed by the presence of superstructure reflections suggesting an ordered state of the material in appropriate micro diffraction patterns (Fig. 2).

The examination of the grain structure of the Ni₃Al intermetallic compound samples synthesized under pressure under plastic strain in a conical mold showed that the plastic strain of the synthesis product results in the formation of a bimodal grain structure represented by micron size (10 mm or more) grains and “multigrains” consisting of submicron (0.1–0.5 μ m) grains in the intermetallic compound (Fig. 3).

An examination of the fine structure of the synthesized intermetallic compound by transmission diffraction electron microscopy showed that the upper layer of the conical intermetallic ingot is a multiphase material. At the initial degrees of high-temperature synthesis product strain, the bimodal grain structure of the synthesized intermetallic compound consists of γ' phase grains and the areas of submicron structure containing 10–50 nm particles of subsequent phases (Al₂O₃ and an insignificant amount of Ni₂Al₃ and NiAl) located at γ' phase grain joints and at γ' phase grain boundaries.

TABLE 1

Layer number in the intermetallic compact starting from the upper part of the cone	1	2	3	4	5
Degree of plastic strain of the intermetallic synthesis product in the layer, %	4.2	5.6	7.4	10.6	15.2

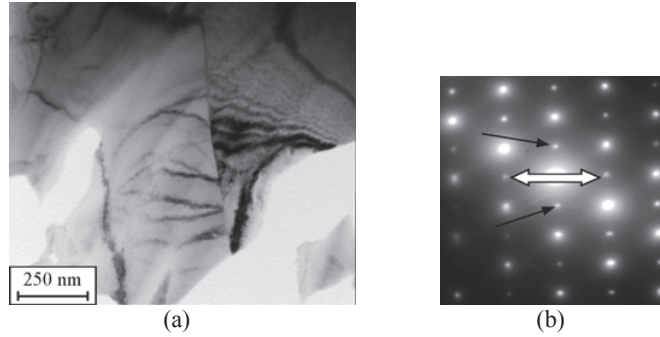


FIGURE 2. Electron microscope image of the structure of the Ni_3Al intermetallic compound (a); electron diffraction pattern obtained from the left grain (b). Arrows indicate superstructure reflections in the electron diffraction pattern: dark arrows— $\{001\}$; light arrows— $\{110\}$

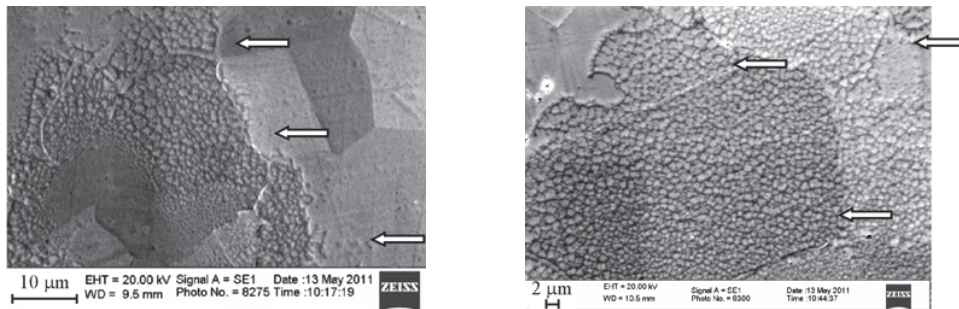


FIGURE 3. Bimodal polycrystalline structure of the Ni_3Al intermetallic compound synthesized in a conical mold under plastic strain of the synthesis product (layer 3 of the conical intermetallic ingot). Arrows indicate submicron grains

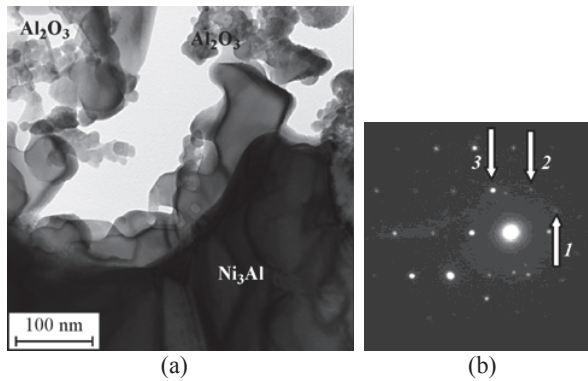


FIGURE 4. Electron microscopic image of the bimodal grain structure formed during the synthesis of the Ni_3Al intermetallic compound (layer 5 of the conical intermetallic ingot) under pressure with plastic strain of the synthesis product; (a) is a bright-field image; (b) is micro electron diffraction pattern obtained from nanoscale grains; arrows on (b) show aluminum oxide reflections $\gamma\text{-Al}_2\text{O}_3$ (lattice parameters: $a = 0.310 \text{ nm}$, $c = 0.499 \text{ nm}$):
 1 — $[100]$, 2 — $[01\bar{2}]$, 3 — $[\bar{1}1\bar{2}]$

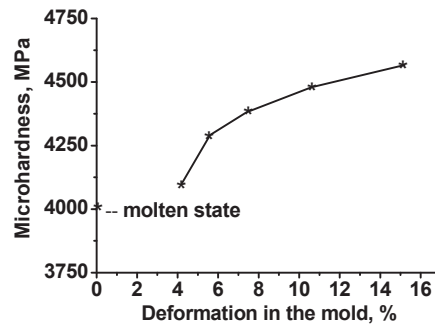


FIGURE 5. Influence of the high-temperature synthesis technology on the microhardness value of the Ni_3Al intermetallic compound

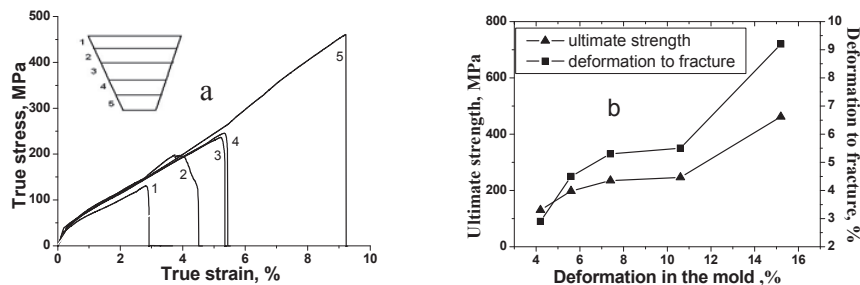


FIGURE 6. Stress-strain curves of the Ni₃Al intermetallic compound test pieces obtained from the transverse layers of the intermetallic compact synthesized under pressure via the plastic strain of the high-temperature synthesis product in a conical mold (a); the ultimate strength and deformation-to-fracture of the synthesized intermetallic compound as the functions of the degree of plastic deformation of the high-temperature synthesis product in a conical mold (b)

During the formation of a bimodal grain structure in the synthesized Ni₃Al intermetallic compound, interlayers consisting of the nanoscale Al₂O₃, Ni₂Al₃ and NiAl crystallites are formed at the interfaces between individual micrograins of the Ni₃Al intermetallic compound, as a result of the plastic deformation of the high-temperature synthesis product (Fig. 4).

Mechanical Properties

The investigation of the relationship between the microhardness of synthesized intermetallic compound and the degree of the high-temperature synthesis product's plastic strain showed that microhardness increases as the degree of plastic strain of the high-temperature synthesis product gets higher (Fig. 5).

Ni₃Al intermetallic compound's yield strength, ultimate tensile strength and strain-to-fracture values get significantly higher as the degree of the plastic strain of the high-temperature synthesis product goes up. The tensile strength and strain-to-fracture of the synthesized Ni₃Al intermetallic compound grow in multiples of their initial values as the degree of strain of the high-temperature synthesis product goes up (Fig. 6).

CONCLUSIONS

Plastic deformation of the Ni₃Al intermetallic compound during its high-temperature synthesis in a nickel-aluminum powder mixture of stoichiometric composition forms, a bimodal grain structure consisting of micron size grains, multigrains consisting of submicron size grains, and intergranular interlayers consisting of nanoscale Al₂O₃, Ni₂Al₃ and NiAl crystallites in the synthesized intermetallic compound.

Formation of a bimodal grain structure in the Ni₃Al intermetallic compound has direct impact on the mechanical characteristics of the intermetallic compound, i.e. the intermetallic compound's microhardness significantly increases and its ultimate strength and deformation-to-fracture grow in multiples of their initial values.

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REFERENCES

1. N. S. Stoloff, C. T. Liu, and S. C. Deevi, *Intermetallics* **8**, 1313 (2000).
2. J. P. Lebrat and A. Varma, *Combust. Sci. Technol.* **88**, 211 (1992).
3. A. G. Merzhanov, *Ceram. Int.* **21**, 371 (1995).
4. J. J. Moore and H. J. Feng, *Prog. Mater. Sci.* **39**, 243 (1995).
5. A. Hibino, S. Matsuoka, and M. Kiuchi, *J. Mater. Process Technol.* **112**, 127 (2001).
6. L. Y. Sheng, W. Zhang, J. T. Guo, Z. S. Wang, V. E. Ovcharenko, L. Z. Zhou, and H. Q. Ye, *Intermetallics* **17**, 572 (2009).