

An evaluation of the historical issues associated with achieving non-helicopter V/STOL capability and the search for the flying car

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ABSTRACT

Combined Vertical and short take-off and landing, or 'V/STOL' capability has been of great demand and interest in the field of aeronautics since the creation of the aircraft. V/STOL capability is a targeted capability for many projected or prototype future aircraft. Past V/STOL aircraft are reviewed and analysed with regard to their performance parameters. This research has found two embedded categories in this class of aircraft based on their propulsion systems, i.e. jet and non-jet propulsion, and highlights the significant performance differences between them. In light of historical experience the performance of a relatively new class of aircraft, the flying cars, has been evaluated.

NOMENCLATURE

a	acceleration m/s^2
C_D	drag coefficient
CG	centre of gravity
C_L	lift coefficient
C_{Lmax}	maximum lift coefficient
$CTOL$	conventional take-off and landing
d	fan diameter (m)
g	gravitational acceleration m/s^2
k_s	suckdown factor
L	lift (N)
L_{OGE}	lift generated by out of ground effect
L_f	jet fountain lift

k_s	suckdown lift
\dot{m}	mass flow rate $\rho AU(kg/s)$
NTSB	National Transportation Safety Board
P	engine power (watts)
S	wing surface area (m^2)
S_d	propeller disk area (m^2)
S_0	take-off ground roll (m)
STOL	short take-off and landing
T	total thrust (N)
T_{dp}	thrust generated by a ducted propeller
T_{reg}	thrust required for VTOL
T_R	reversed engine thrust
UAV	unmanned aerial vehicle
V/STOL	vertical/short take-off and landing
V	cruise velocity (ms^{-1})
V_{max}	maximum cruise velocity
V_{ref}	approach speed
v_c	rate of climb or climb velocity
VTO	vertical take-off
VTOL	vertical take-off and landing
W	gross weight (kN)
ρ	air density at sea level ($1.225Kg/m^3$)
ϕ	area ratio between fan and duct exhaust
μ	dry friction coefficient
η_p	propulsive efficiency

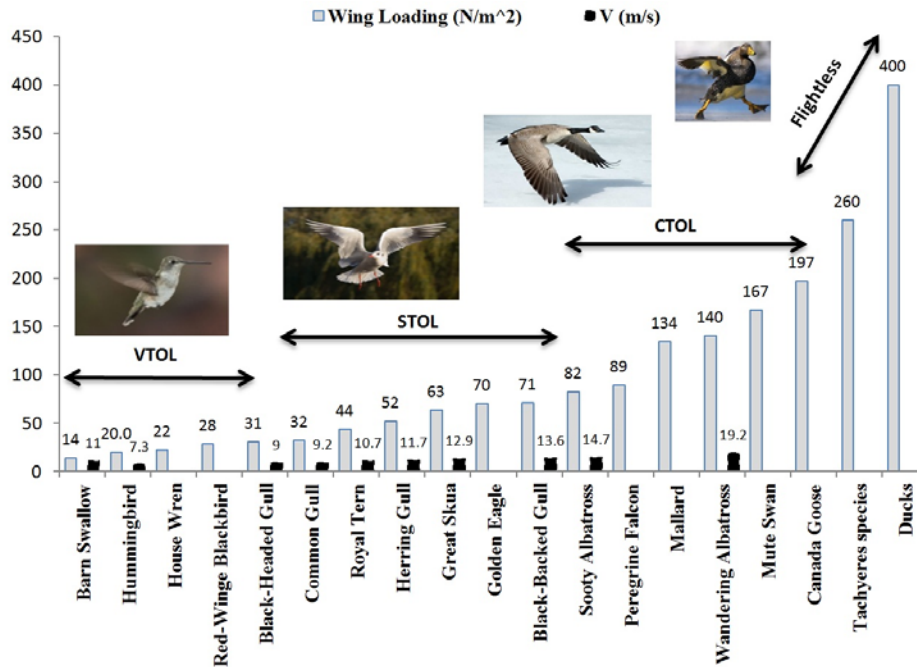


Figure 1. Take-off and landing characteristics of birds (data adapted from Refs 1-5).

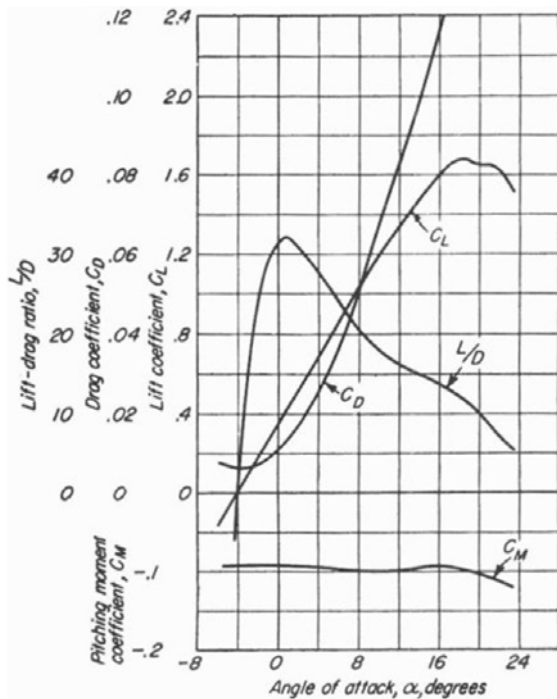


Figure 2. Typical NACA wing-section characteristics (taken from Ref. 6).

1.0 INTRODUCTION

V/STOL refers to vertical or short take-off and landing capability, an aircraft that can perform either vertical or short take-off or landing is said to inherit V/STOL capability e.g. BAe Harrier. The term V/STOL is composed of two other VTOL, vertical take-off and landing, and STOL, short take-off and landing. An aircraft with insufficient vertical thrust may attempt a short take-off and vertical landing upon reducing weight from fuel consumption, this class of aircraft is specifically designated by STOVL.V/STOL capability

cuts the need for long runways and reduces the time to achieve horizontal flight: conventional jet aircraft land and take-off with speeds of, around, 80 to 120ms⁻¹ and may require runways up to 3,500m in length in some cases – this is an expensive infrastructure problem that V/STOL has potential to solve.

Interest in V/STOL flight probably arose when early attempts at powered flight tried emulate the behaviour of birds; however, no early man made machine, based heavily on birds ever achieved controlled flight. It was not then recognised that the short and vertical take-off capability of birds is in large measure made possible by their low wing-loading, which is a natural result of their small size. Figure 1 depicts a chart of wing loading and flight speed for a variety of birds and it can be seen that the birds with relatively low wing-loading and forward velocity are actually VTOL capable, such as the hummingbird, blackbird and barn swallow, other birds being either V/STOL or conventional take-off and landing (CTOL) capable. Sir George Cayley, who was the first to recognise the importance of distinguishing lift from thrust and in particular to recognise the fact that for level flight, the required thrust is one or two orders of magnitude less than the required lift⁽¹⁾.

In order to understand this phenomenon further, consider lift and drag curves for a typical wing section as shown in Fig. 2. The lift is always larger in magnitude than the drag at typical flight conditions, which typically correspond to 10 < C_L/C_D < 15, and hence the thrust required to overcome the drag is less than the lift generated. Early vertical flight – in helicopters – was achieved by an aerodynamic, or rotary wing, solution, rather than a pure propulsive solution. The following equation best describes the relationship between the forces acting on an aircraft in level flight.

$$\Rightarrow \text{Thrust} = \text{Drag} \ll \text{Lift} = \text{Weight}$$

Jet propulsion achieves Vertical Take Off, or VTO by working against an aircraft’s weight due to gravity directly, whereas the rotary wing solution does work initially against drag (profile and induced) and hence benefits from the phenomenon of lift being much larger than drag.

Regardless of mechanism, the development of V/STOL capability has also inevitably been reliant upon the availability of suitable power plants. In particular, the gas turbine engine, with its high

thrust : weight ratio, made possible the eventual development of aircraft with static thrust to gross weight ratios greater than one – a prerequisite for VTOL capability. As the speeds of aircraft continue to increase, the power plant requirements for V/STOL operation and forward flight performance become compatible. Furthermore, at the same time, above Mach 1 the thrust required is nearly equal to or exceeds the gross weight of the aircraft at level flight – coinciding some aspects of the design solutions for V/STOL and supersonic aeroplanes.

The most prolific V/STOL capable aircraft, so far, is clearly the helicopter; however, in level flight the helicopter is inefficient compared to a typical fixed-wing aeroplane, with speed and range only between a half or one third (approximately) that of the aeroplane. Also, due at-least in part to their greater complexity, helicopters demonstrate poorer safety than conventional aeroplanes⁽⁷⁾: with for example light conventional aeroplanes suffering a fatal accident rate of 11.7/million flying hours, versus 33.5/million flying hours for small helicopter. The same complexity also contributes to a greater cost: for example at time of writing the typical hire cost of a Robinson R44 helicopter in the UK is £400/hr or to purchase the aircraft would cost £100,000-£200,000, whilst a Cessna C172 aeroplane, which has similar payload and cruise performance capability, can be rented for about £150/hr or purchased for about £30,000-£100,000 – costs around 30-40% of the cost of the helicopter.

The search for V/STOL capability has provoked research into embedding VTOL capability of a helicopter into a conventional fixed-wing aeroplane. However, this has rarely been achieved. The authors have identified 45 fixed-wing aircraft which have attempted to combine V/STOL capability of the helicopter with high forward flight speed of a conventional aircraft. Of these 45, only four: the BAe Harrier, Yak-38, Bell-Boeing V-22 and Lockheed Martin X-35 Joint Strike Fighter have ventured much beyond the prototype stage. Table 1(left) presents these 45 aircraft arranged according to their propulsion systems.

This table is dominated by aircraft whose designs attempt to use the same power system for both VTOL- lift and propulsion: including the BAe Harrier and the Bell Boeing V-22. The Yak-38 and JSF X-35, which have both, also successfully, entered service, utilised combined power plant for hover and augmented power plant for hover respectively. This paper will attempt to compare these aircraft through performance parameters, specifically: maximum velocity, range, thrust to weight ratio and power.

2.0 DISTINCT AERODYNAMIC FEATURES OF V/STOL AIRCRAFT

The main distinctive feature of V/STOL capability is the high thrust to weight ratio which requires expanding the propulsion performance envelope and makes the powerplant the most significant component of a V/STOL aircraft in terms of weight and body volume. Most jet fighter aeroplanes developed since about 1960 have (at-least in lightweight configurations), the potential to generate a thrust to weight ratio T/W exceeding one. However, conventionally the engine exhaust is located at the rear of aircraft and diverting the exhaust downward will not be the solution – this is useful for horizontal flight, but not hovering flight where a balance problem exists. To solve this, either the thrust must be co-incident with the centre of gravity, or an additional and controllable thrust device must be located away from the main thrustline, creating a balance – such as in the case of the BAe Harrier (see Fig. 3 left). Both of these approaches will tend to prise the aircraft away from the traditional and usually optimal layout.

For cruise-dominated VTOL aircraft – such as may be designed for transport purposes, a more severe problem involves thrust matching. If the thrust required for vertical flight is provided by the same engines used for cruise, the engines will be far too large for

Table 1
V/STOL aircraft arranged according to their propulsion systems

VTO Propulsion Strategy		Aircraft Model	
Same Propulsion System for Hover and Forward Flight	Tilt Shaft/Rotor	Transcendental Model 1G	1
		Bell XV-3	2
	Tilt Prop	Curtiss-Wright X-100	3
		Curtiss-Wright X-19	4
	Tilt Duct	Doak 16 VZ-4	5
		Bell-X22A	6
		Nord 500 Cadet	7
	Tilt Wing	Vertol 76 VZ-2	8
		Hiller X-18	9
		LTV-Hiller Ryan XC-142	10
		Canadair CL-84 Dynavert	11
	Tilt Rotor	Bell XV-15	12
		Bell Boeing V-22 Osprey	13
	Tilt Jet	Bell 65	14
	Deflected Slipstream	Robertson VTOL	15
		Ryan 92 VZ-3 Vertiplane	16
		Fairchild 224 VZ-5	17
	Vectored Thrust	Bell X-14	18
		Hawker P.1127 Kestrel	19
		Yakovlev Yak-36	20
		BAe Harrier	21
		Boeing X-32	22
		Lockheed XFV-1	23
	Tail Sitters	Convair XFV-1 Pogo	24
		Ryan X-13 Vertijet	25
		SNECMA C450	26
Short SC.1		27	
Separate Power Plant for Hover	Lift + Cruise	Dassault Balzac V	28
		Dassault Mirage III-V	29
		EWR VJ101C	30
Combined Power Plant for Hover	Lift + Lift/Cruise	Dornier Do 31	31
		Lockheed XV-4B	32
		VFW VAK 191B	33
		Yakovlev Yak-38	34
		Yakovlev Yak-141	35
	McDonnell XV-1	36	
	Tip Jets	Fairey Rotodyne	37
		Lockheed XV-4A	38
Augmented Power Plant for Hover	Ejector	Rockwell XFV-12A	39
		Vanguard Omniplane	40
	Fan	GE-Ryan XV-5A	41
		Lockheed Martin X-35	42
		Kamov Ka-22	43
	Rotor	Piasecki 16H-1	44
		Lockheed AH-56	45



Figure 3. Hawker Siddeley/Bae Harrier GR Mk 3.

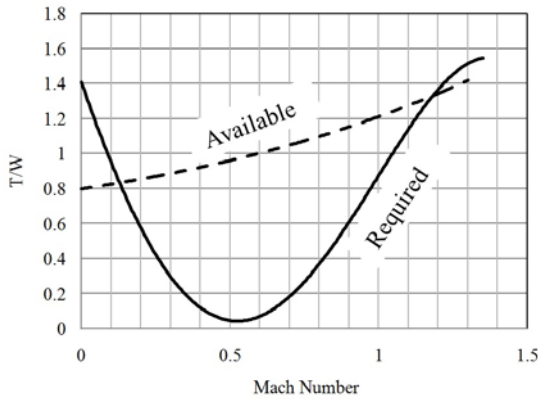


Figure 4. Thrust mismatch for jet V/STOL aircraft at sea level (derived from Ref. 8).

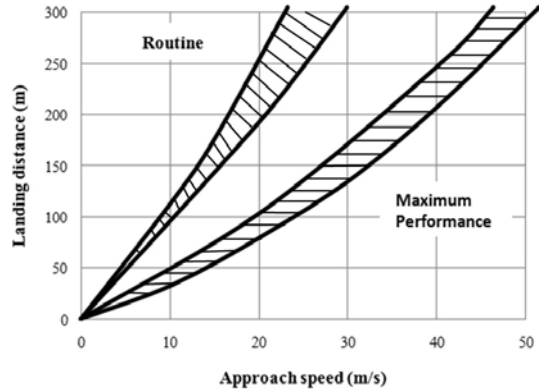


Figure 5. STOL landing performance (derived from Refs 9,10).

efficient cruise. The thrust mismatch will produce great fuel consumption and range penalty for a cruise dominated design that uses only the vectored thrust of its cruise engines for vertical flight. For this reason many conceptual VTOL transport designs have incorporated separate ‘lift engines’ used during vertical flight. Figure 4 highlights the mismatch between thrust required for vertical flight and thrust for horizontal flight for a typical jet V/STOL aircraft. Also, the thrust mismatch may further increase with altitude as the thrust required to maintain a steady flight at higher altitudes, (~15,000m), decreases significantly. These are known to be the fundamental problems which must be overcome in a VTOL aircraft.

In a V/STOL aircraft it becomes necessary to also consider the factors influencing the performance for the CTOL and level flight cases. The factors can be evaluated by simplified analysis of the ground-roll distance of a landing aircraft and the relationship between them is defined by⁽⁹⁾

$$S_0 = \frac{(W/S)V_{ref}^2}{\rho g C_{L_{max}}(T_R/W + \mu)} \dots (1)$$

$$\Rightarrow \begin{cases} S_0 \propto W/S \\ S_0 \propto V_{ref}^2 \\ S_0 \propto 1/C_{L_{max}} \\ S_0 \propto 1/(T_R/W) \end{cases} \dots (2)$$

where S_0 is the ground-roll distance, V_{ref} the approach speed and the other symbols are designated to their usual meanings. The relationship clearly indicates that the thrust to weight ratio is the most significant parameter to achieve minimum ground roll distance and it could be further minimised by maximising $C_{L_{max}}$ and lowering the wing loading W/S . Figure 5 presents the landing performance of typical STOL aircraft unsurprisingly shows that the approach speed should be reduced to minimise the landing distance. To do so, $C_{L_{max}}$ and T_R (which is a function of forward thrust to weight ratio) need to be increased.

Of course, aircraft configuration is also very relevant to achieving STOL performance. In particular at the design stage, the inlet and exhaust of the lift-generator system should be considered. Proper exhaust location, such as that achieved on the Harrier, can enhance even conventionally augmented wing lift considerably⁽¹¹⁾ during a conventional runway take-off.

Figure 6 also shows that wing loading must be reduced to achieve a better weight to power performance. Helicopters possess the highest weight to power ratio and the rest, tilt rotor, lifting propellers and lifting jet, are significantly less efficient. However, this paper is concerned with fixed-wing V/STOL aircraft only and this makes tilt rotor the most efficient aircraft within this class of aircraft.

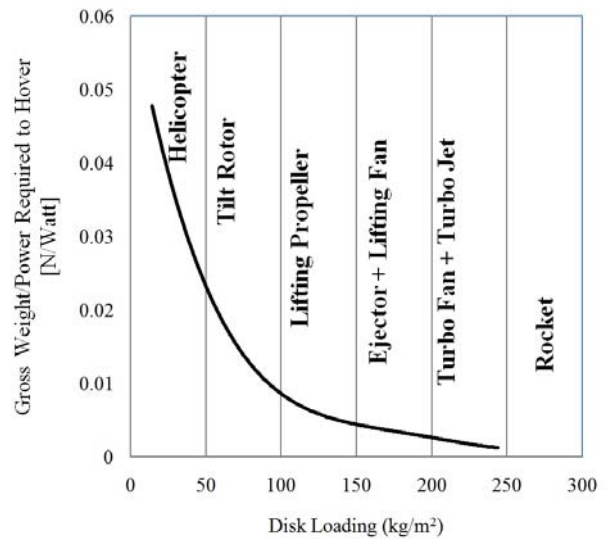


Figure 6. Weight to power ratio versus disk or wing loading for V/STOL aircraft with different propulsion systems (derived from Ref. 12).

3.0 PRIMARY CAUSES OF AERODYNAMIC LOSSES

It is useful to review the main design penalties introduced into the well understood conventional aeroplane by the addition of a VTOL capability. During hovering or vertical flight the aircraft experiences several aerodynamic losses including suckdown, recirculation, hot-gas ingestion, thrust vectoring and reaction control system.

3.1 Suckdown and fountain lift

The downwash that keeps the aircraft in a steady state also accelerates the air flow around it which pushes downward on the aircraft with a vertical drag depending on the whole surface area of the aircraft facing the flow. The critical factors influencing the vertical drag are the relative location of the propeller or jet exhaust and the fixed wing. If the propeller is directly above the main wing, such as in the Lockheed AH-56, or the exhaust nozzles are directly under the wing, such as in the Bell 65 ATV, then a much larger downward force is exerted by the entrained airflow. For a jet aircraft suckdown

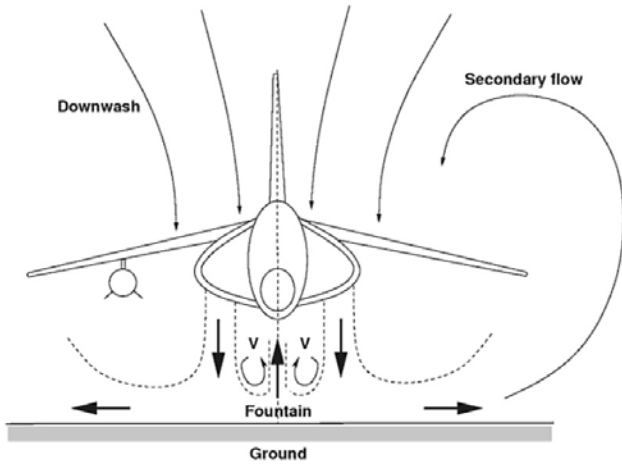


Figure 7. Twin jet V/STOL hover aircraft in ground effect showing potential flow field, suckdown and fountain lift (from Ref. 13).

3.3 Hot-gas ingestion

Hot-gas ingestion is only applicable to jet VTOL aircraft where hot exhaust gases are injected back into the engine which increases the inlet temperature and causes a significant reduction in thrust. The hot-gas ingestion is very configuration dependent, the nozzle arrangement, inlet position, and wing location being important variables. Relative head winds could also have a large effect on the magnitude of the inlet-air temperatures.

3.4 Thrust vectoring

Thrust-vectoring is generally achieved by nozzle-vectoring and the nozzle arrangement has a significant effect on the thrust loss. Rectangular nozzle arrangements and the side-inlet single nozzle have the highest inlet-air temperature rises (up to 111°C)⁽¹⁴⁾.

3.5 Reaction Control System (RCS) losses

In hovering flight, an RCS is necessary to aircraft control; this may for example be achieved through use of compressed air bleed at the wing tips, nose or tail (e.g. the Harrier and Yak-38). Such a system is both heavy in itself, and makes significant power demands upon the aircraft. (For a rotary-wing aircraft balanced VTOL is achieved by a combination of pendular stability, for high wing configuration, and dynamic control via disc angle.)The net T/W for VTO must obviously exceed one in the normal axis, however thrust losses must be considered in light of the above.

is a rather severe aerodynamic loss. The jet lift is a product of mass flow rate m and jet speed U_j , $T = mU_j$. Significantly large amounts of air need to be drawn in from the surroundings which subsequently causes a complex flow field around the aircraft as shown in Fig. 7.

This complex flow field causes variation in total lift arising mainly from suckdown caused by low pressure at lower surface of the aircraft. This loss is often balanced by deploying vertical fins to divert the engine exhaust inwards and generate favourable fountain effect. The variation in lift may be summed up as

$$\frac{\Delta L}{T} = \frac{\Delta L_{OGE}}{T} + \frac{\Delta L_f}{T} + \frac{\Delta L_s}{T} \dots (3)$$

where L_{OGE} is the loss of lift due to profile drag acting at the plan-form surface of the aircraft depending on the climb rate.

Heave Control	$T/W = 0.05$	from Ref. 15.
Suckdown	$T/W = 0.03$	
RCS	$T/W = 0.1$	
HDI	$T/W = 0.08$	
Landing Weight	$T/W = 1.0$	

Thus, to achieve hover for a jet aircraft, normally $1.3 \leq T/W \leq 1.5$

3.2 Recirculation

A V/STOL aircraft near the ground experiences a potential flow field around it that injects its own downwash/exhaust gases into the inlet which results in a significant loss of lift/thrust. This recirculation also often injects dirt and erosion particles that can damage the engine.

4.0 V/STOL PERFORMANCE ANALYSIS

Conventionally, an aircraft's performance, as a whole, is specified by power and thrust loading, W/P and W/T . The shorter the take-off distance, the higher the altitude and hotter the climate, the bigger the engine to provide enough power, or thrust. Specifically, for a V/STOL aircraft the most emphasised parameters, from conceptual design to performance analysis, are static thrust-to-weight ratio and

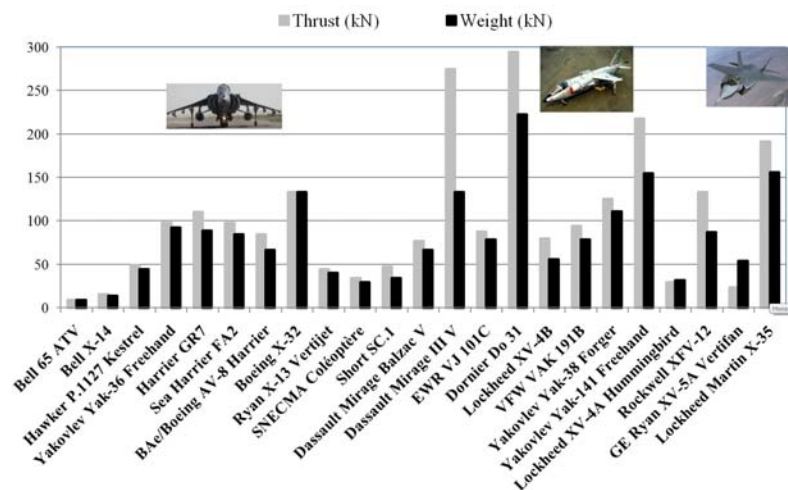


Figure 8. Available jet-thrust and weight chart for jet V/STOL aircraft.

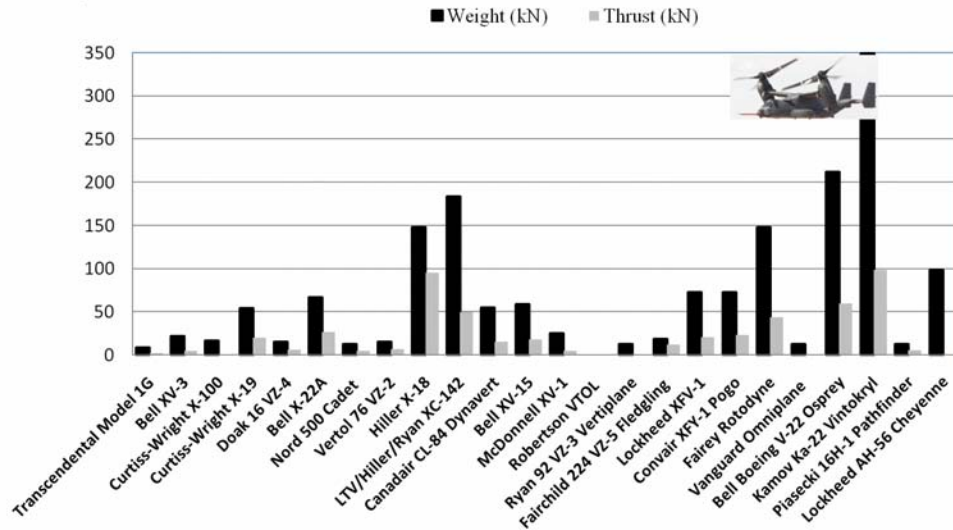


Figure 9. Thrust and weight chart for non-jet V/STOL aircraft.

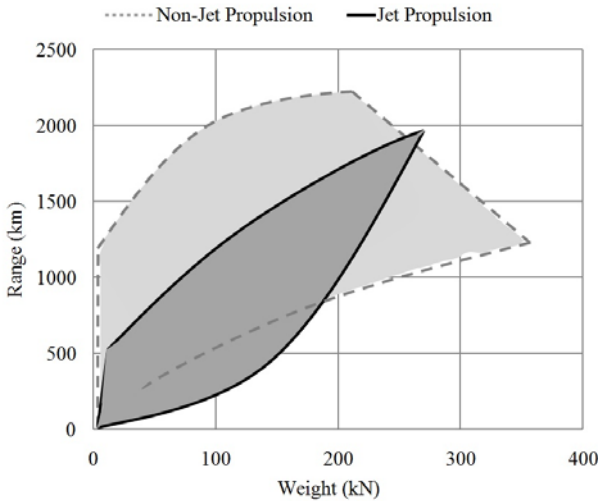


Figure 10. Range comparison for jet and non-jet propulsion driven V/STOL aircraft.

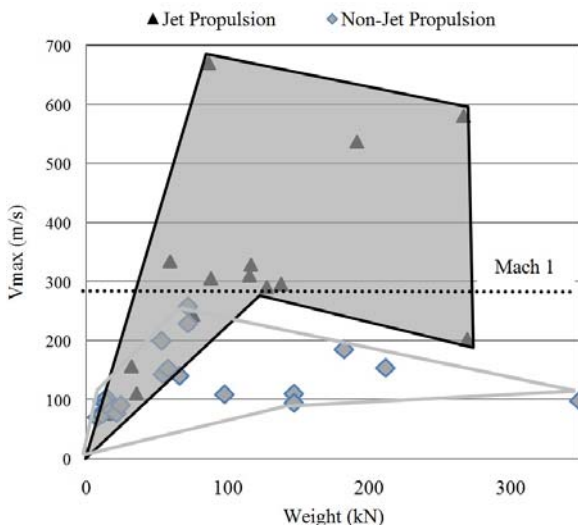


Figure 11. V_{max} -weight envelope comparison for jet and non-jet propulsion driven aircraft.

wing loading⁽¹⁶⁾. For a CTOL aircraft the general performance equation⁽¹⁷⁾ defining the relationship between power, thrust and weight is given by

$$\eta_p P = DV_i + Wv_c + (W/g)a\eta_p \quad \dots (4)$$

where η_p is the propulsive efficiency, V_i the forward target velocity, V_c the rate of climb and a the acceleration of aircraft. This equation, in general, will hold for V/STOL aircraft as well by incorporating the different flight modes. Thus the analysis below will be based on the parameters given in the equation above.

Design and performance data has been collected for the aircraft, presented in Table 1, and tabulated in Table 2 and Table 3, categorised by propulsive class.

Figures 8 and 9 present thrust and VTO weight chart for the jet and the non-jet V/STOL aircraft respectively in order to highlight the scale of each aircraft. Using the available technology, jet aircraft tend to be heaviest with weights on average of 80kN compared to 30kN for other classes. The aircraft are arranged with time scale and there seems to be no strong evidence of improvement in terms of thrust to weight ratios through the history of V/STOL – presumably because most aircraft are designed to a weight which makes full use of the power available.

Once V/STOL capability is achieved, for many aircraft, the most significant performance parameter would then be the range. Figure 10 shows that the non-jet driven aircraft acquire much longer range for a given weight compared to the jet driven aircraft. The lighter non-jet aircraft, up to 50kN weight, give around double the range available to a jet propelled equivalent aircraft.

Another important parameter for some aircraft, particularly those with military applications, is maximum operating altitude (often called the aircraft ceiling). In contrast to range, jet propelled aircraft attain much higher maximum cruise velocities compared to the non-jet, see Fig. 11.

The average cruising speed of heavier jet aircraft is around 300ms^{-1} , which is in the transonic region, and around 100ms^{-1} for the non-jet aircraft. However, for the smaller/lighter class of aircraft, up to 50kN, the difference is insignificant. Rotary winged aircraft are excluded from the high speed flight regime by well-known limiting factors, particularly tip compressibility and retreating blade stall. The high profile drag met at transonic speeds, inevitably, leads to a requirement for a higher T/W for higher speed (normally jet) aircraft, as may be seen in Fig. 12. The average T/W for the jet aircraft is around 1.2 which is a function of Mach number as shown in Fig. 4 above. The average T/W value for the non-jet is 0.35 which again

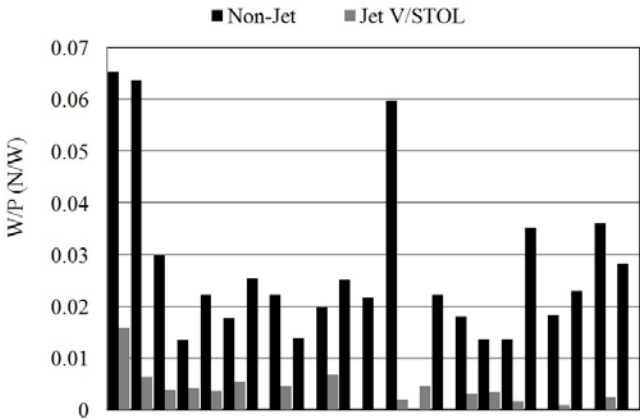


Figure 12. T/W comparison for jet and non-jet propulsion aircraft.

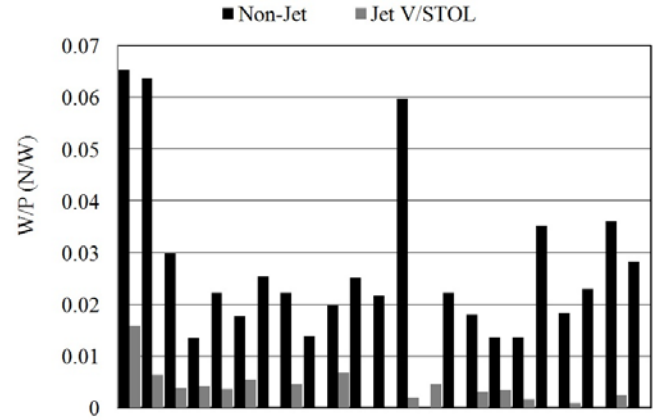


Figure 13. Power loading comparison for jet and non-jet V/STOL aircraft.

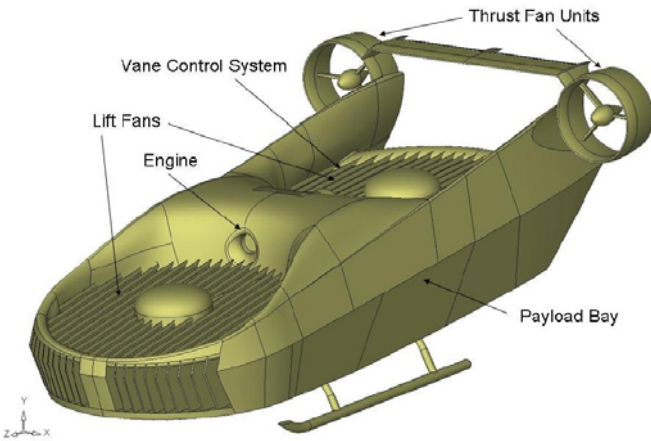


Figure 14. Mule UAV by Urban Aeronautics (photo courtesy of Urban Aeronautics Ref. 21).

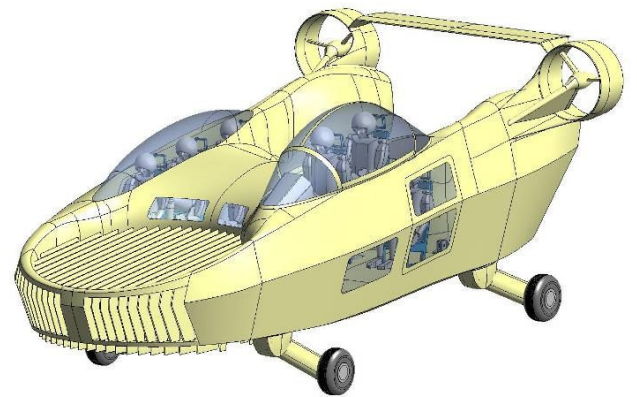


Figure 15. X-Hawk by Urban Aeronautics (photo courtesy of Urban Aeronautics Ref. 22).

highlights the fact that rotary wing benefits from aerodynamic fact that lift generated is much larger than the drag. The rotary wing and jet propulsion efficiencies are given below respectively

$$\eta_p = \frac{1}{1+a} \dots (5)$$

$$\eta_j = \frac{2}{1+a} \dots (6)$$

where *a* is the ratio of vehicle velocity to the exhaust (for jet) or the induced (for propeller) velocity.

For jet engines the propulsive efficiency is the highest when the engine emits an exhaust jet at a speed that is nearly the same as the vehicle velocity. While for the rotary wing the smaller the induced velocity the more efficient the system.

The relationship between performance parameters even for the successful aircraft such as X-35 is nonlinear – this aircraft weighing approximately twice the weights of the Harrier and Yak-38 but displaying triple the range and double the top speed. However, given the small sample and that the X-35 is a much more recent aircraft, this is probably due to improved strength to volume ratio of composite materials used on the X-35 which has direct impact on lift to drag ratio.

Figure 13 highlights the difference in power required to hover for the jet and non-jet aircraft and the non-jet proves to be way more efficient in this regard, it consumes around 4 times less power, in average, to lift a corresponding weight.

5.0 FLYING CARS: THE FUTURE V/STOL VEHICLES?

The flying car is a category of aircraft which has been projected for many years, but is only now approaching possible utility. These are low speed, light weight and short-range vehicles for non-traditional roles such as close area surveillance or personal transport^(18,19,20). There are several projects currently receiving publicity, but which have so far failed to demonstrate commercial success – or in some cases, the ability to sustain flight. Herein, particularly V/STOL capable cars that might be in service in the near future are described and their specifications are given in Table 4.

5.1 Mule UAV

The flying car displayed in Fig. 14 is a UAV developed by Urban Aeronautics, an Israeli company, for a proposed market with the emergency services. It is also related to a projected manned aircraft, the X-Hawk, see Fig. 15. The distinct feature of the vehicle is the vane control system: actuating guided vanes are installed around the main lift fan. Forward flight is achieved by ducted fans powered by the main powerplant. A scale prototype of the vehicle is reported to have been tested in August 2008 in hover and low-speed forward flight, and flight of the first Mule prototype is projected for mid-2009. The vehicle is predicted to be capable of obtaining 51ms⁻¹ of maximum forward velocity, two to four hours of flight endurance and can lift a payload of up to 2.5kN with 480kW of power.



Figure 16. Moller Skycar M400 (photo courtesy of Moller International Ref. 23).



Figure 17. Skyrider (photo courtesy of Macro Industries Ref. 24).



Figure 18. Skyrider Scout (photo courtesy of Macro Industries Ref. 24).

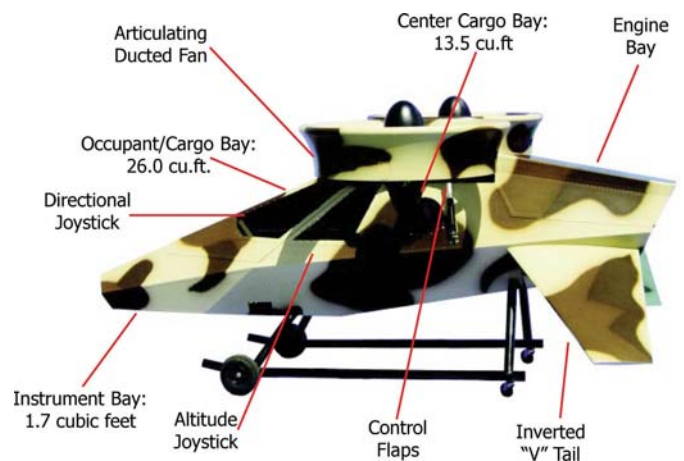


Figure 19. Dragonfly (photo courtesy of Trek Aerospace Ref. 25).

5.2 Moller skycar

The Moller M400, displayed in Fig. 16, claims a better performance compared to the Mule, claiming to be capable of 161ms^{-1} top speed, carriage of up to 3.9kN of payload, $1,200\text{km}$ range, despite a stated maximum weight of 1.7kN (identical to that of the Mule). The vehicle hopes to achieve stable cruise flight but has shown poor stability in hover during the test carried out by the design team⁽²³⁾. Nevertheless, the vehicle seems to be the most advanced in course to a certified operational V/STOL flying car.

5.3 Skyrider

Skyrider, depicted in Fig. 17, is also based on the ducted fan technology and achieves control by the same means. It is similar to the Moller M400 to a great extent, however, promises better performance with 172ms^{-1} top speed, $1,482\text{km}$ range and power consumption of 522kW . The stability is of great concern as the vehicle significantly lacks static-wing area. However, the design is also implemented as a UAV, the Skyrider Scout, which comprises of a much slimmer fuselage, see Fig. 18, and tends to generate lift. Nevertheless, the design is at its prototyping stage and may well be modified to tackle its weaknesses⁽²⁴⁾.

5.4 Dragonfly

The Dragonfly UAV, displayed in Fig. 19, is designed to serve communication purposes in the battlefield. Based around articulated ducted fan technology to achieve VTOL and also has sufficient tail area to enhance stability. Dragonfly's unique feature is the ability to quickly change its flight options from remote, to unmanned or manned result in a well-rounded vehicle with unlimited potential.

5.5 Flying cars performance analysis

It is visible in the vehicles described above that the most common feature in them is the ducted/shrouded fan/propeller. The concept of ducted propellers as a suitable propulsive device for many V/STOL applications has been explored for more than half a century; the Doak 16 VZ-4 and Bell X-22A are good examples of successful application. Ducted fans, or shrouded propellers, hold promise as devices for high static thrust propulsion systems. When compared to an isolated propeller of the same diameter and power loading, ducted propellers typically produce significantly greater static thrust⁽²⁶⁾. However, a better efficiency compared to an un-ducted propeller is only achieved at relatively lower airspeeds. Ducted fans also offer lower noise, uniform loading along the blade span and elimination of the propeller induced tip vortices subsequently eliminating induced

drag. In addition, the ducted fan system offers a supplementary safety feature attributed to enclosing the rotating fan in the duct, therefore making it an attractive option for various advanced unmanned air vehicle configurations or for small/personal air vehicles as described above.

The flying cars claim to be V/STOL capable and recalling that V/STOL is composed of two separate characteristics: VTOL and STOL. Thus the feasibility study may begin by investigating whether these vehicles comply the main condition of VTOL capability that is $T/W > 1$. The thrust required for this flight mode may be evaluated by assuming that the aircraft behaves like a flat plate perpendicular to the flow as shown in Fig. 20. Applying Newton's second law of motion and assuming sum of the forces act through the geometrical centre of the plate/aircraft the following relationship is derived

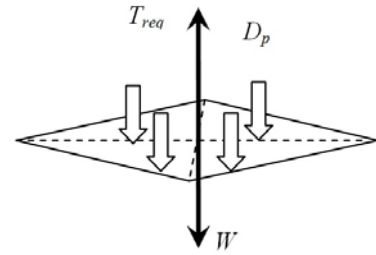


Figure 20. Flat plate theory to estimate VTOL performance.

$$\sum F = ma \quad \dots (7)$$

$$T_{req} - D_p - W = \frac{W}{g} a \quad \dots (8)$$

It is known that for a VTOL aircraft the minimum vertical acceleration requirement is $0.1g^{(13)}$ so the thrust required for vertical take-off is given by

$$\Rightarrow T_{req} = 1.1W + k_s \frac{1}{2} \rho v_c^2 S_p C_{Dp} \quad \dots (9)$$

where k_s is a factor to incorporate loss in lift from suck down (as described above) and C_{Dp} is the profile drag coefficient for a flat plate, a typical value taken to be $1.28^{(27)}$. Also, the typical range of distance from ground to out of ground effect is $5m < H_{OGE} < 10m^{(28,29)}$. Taking $H_{OGE} = 8m$ as mean OGE height; the climb rate v_c may be evaluated by using the equation of uniformly accelerated motion (strictly for point mass object) as

$$v_c^2 = u_i^2 + 2aH_{OGE} \quad \dots (10)$$

and taking the initial velocity u_i near the ground to be zero.

$$\Rightarrow v_c = \sqrt{2aH_{OGE}} \quad \dots (11)$$

Hence $v_c \geq 4ms^{-1}$.

The thrust available for a given engine power, applying the simple momentum theory, for a ducted propeller is defined⁽³⁰⁾ as

$$\Rightarrow T_{ava} = \sqrt{2aH_{OGE}} \quad \dots (12)$$

where ϕ is the area ratio between the fan and the exhaust and $P_{0.8}$ is 80% of the engine power transmitted to the fan since ducted propellers are typically 80% efficient⁽¹⁷⁾. Assuming the climb rate of the range $4 \leq v_c \leq 10$ has negligible effect the relationship for thrust available may be further simplified as

$$\Rightarrow T_{ava} = \left[\frac{\rho \pi}{\phi} \right]^{\frac{1}{3}} [P_{0.8} d]^{\frac{2}{3}} \quad \dots (13)$$

From the equation above it can clearly be seen that the thrust available from a ducted propeller depends on the overall size of the fan and the ratio between the fan disc area and the duct exhaust area. Figure 21 compares the thrust available to the thrust required to achieve VTOL for the flying cars. From the figure it is visible that the Moller M400 and the Mule are just capable of providing enough thrust for VTOL. The Dragonfly and the Skyrider lack sufficient thrust to overcome the weight and the vertical drag. However, Moller and Mule projects are comparably much advanced in

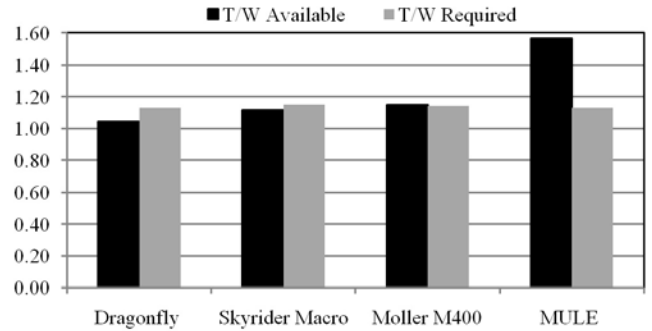


Figure 21. Chart comparing thrust available to thrust required for flying cars.

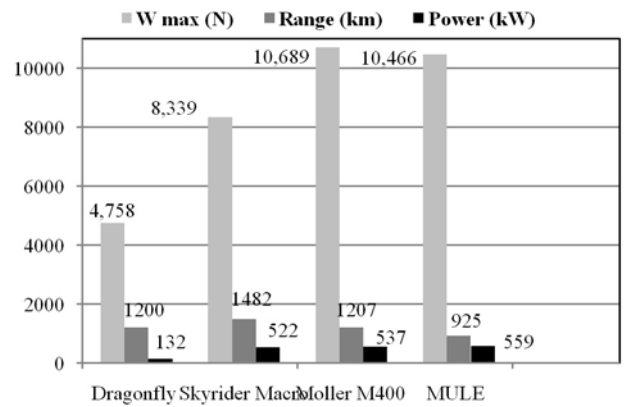


Figure 22. Flying cars' specifications.

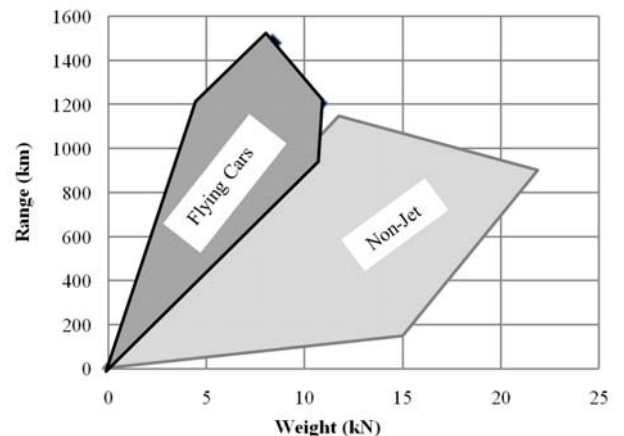


Figure 23. Range-weight envelope of future flying cars and non-jet V/STOL aircraft.

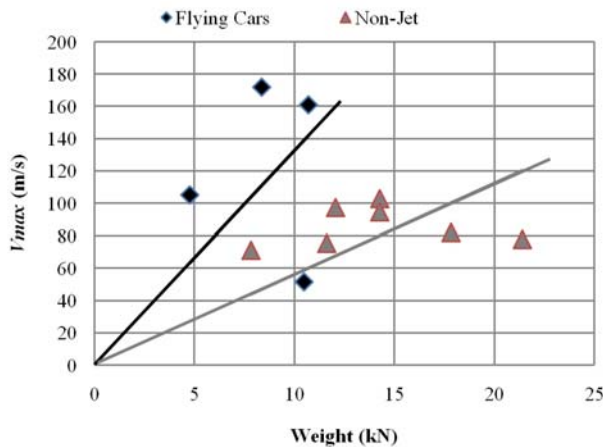


Figure 24. Maximum cruise velocity comparison of future flying cars and non-jet V/STOL aircraft.

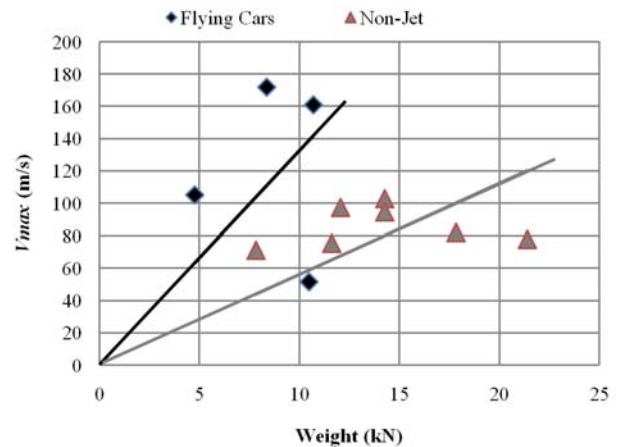


Figure 25. Power consumption comparison of flying cars and non-jet V/STOL aircraft.

reaching their prospective goals. Also, nevertheless, the publishers/designers have clearly mentioned that the performance estimates are preliminary and subject to change. So the analysis above suggests that a higher degree of precision is required for better estimation.

The specifications and flight performance data for the flying cars depicted above are presented in Table 4 and plotted in Figs 22 to 25. These figures compare the flying cars performance to the past, relatively, lighter/smaller non-jet V/STOL aircraft. Clearly, the flying cars are claiming significantly better range envelopes and speeds compared to corresponding past non-jet V/STOL aircraft. It is perhaps curious that, despite a lack of any real track record for any of these projects, they consistently propose significantly better performance: as defined by speed, range and payload, per power and weight, than previous aircraft. It will be interesting, should any of these projects reach fruition, so see the extent to which this claimed performance is ever achieved – the authors venture that they may not, although certainly the extensive use of ducted fan technology may carry some benefits⁽³¹⁾.

6.0 CONCLUSIONS

The analytical review of the past V/STOL aircraft based on their performance parameters has resulted in useful findings.

- V/STOL optimisation is best achieved with light-weight vehicles, with low wing loading.
- the V/STOL aircraft may usefully be divided into two categories, i.e. jet and non-jet, as there exists a significant performance difference between the two.
- non-jet driven V/STOL aircraft acquire better range and consume significantly less power.
- several different propulsive arrangements have been tried on past V/STOL aircraft; however, for jet propelled aircraft a clear best solution has yet to emerge.
- an attempt has been made to define relationship between several parameters by plotting the data presented in the database and most of it depicted a nonlinear relationship.
- performance is not linearly related to aircraft weight.
- aerodynamic based propulsion systems best serve low speed V/STOL aircraft – most of the future V/STOL aircraft are being developed based on this fact. The dominant branch of V/STOL ‘the helicopter’ works with aerodynamic solution i.e. Rotary wing.

- the thrust to weight requirements of a modern fighter aircraft tend towards also satisfying the same requirement for V/STOL.
- whilst proposed future V/STOL vehicles validate the findings above by adopting non-jet propulsion system and keeping the overall size to the minimum, most current projects claim performance unlikely to be met by comparison with historical data.

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APPENDIX

Table 2
Jet V/STOL aircraft data (source Refs 32-35)

Aircraft	VTOW (kN)	Length (m)	b (m)	Vmax (m/s)	Range (km)	Thrust (kN)	Power Plant	T/W
Bell 65 ATV	-	-	-	-	-	9	(2) Fairchild J-44 (1,000 lb)	0.98
Bell X-14	19	8	10	77	483	16	(2) AS V8 Viper (1,750 lb)	1.13
Hawker P.1127 Kestrel	76	13	7	244	563	49	BS Pegasus (11,000 lb)	1.10
Yakovlev Yak-36	116	17	7	311	409	98	(2) Soyuz R-27 (11,000 lb)	1.06
Harrier GR7	138	14	9	296	483	110	Pegasus 11 Mk.103	1.24
Sea Harrier FA2	117	14	8	328	370	98	Pegasus 11-21 Mk.106	1.16
BAe/Boeing AV-8 Harrier	138	15	9	296	483	85	GR.1: RR Pegasus 6 (19,000 lb)	1.27
Boeing X-32	-	-	-	536	1573	133	PW F119-SE614 (approx 30,000 lb vertical)	1.00
Ryan X-13 Vertijet	32	7	6	156	309	44	RR Avon (10,000 lb)	1.11
SNECMA Coléoptère	-	-	-	313	700	34	SNECMA Atar 101E (7,700 lb)	1.16
Short SC.1	36	8	7	110	241	47	(5) RB.108 (2,130 lb)	1.38
Dassault Mirage Balzac V	-	-	-	-	-	77	(8) RB.108 (2,160 lb) + BS Orpheus (5,000 lb)	1.15
Dassault Mirage III V	-	16	9	626	463	275	(8) RB.162-31 (5,400 lb) + PW TF30 (18,520 lb)	1.50
EWR VJ 101C	60	16	7	335	-	88	(2) RB.145 (2750 lb) + (4) RB.145R (3560 lb a/b)	1.12
Dornier Do 31	269	21	18	202	1802	295	(2) BS Pegasus 5-2 (15,500 lb) + (8) RR RB.162-4D (4,400 lb)	1.32
Lockheed XV-4B	-	10	8	150	-	80	(6) J85-GE-19 (3,000 lb)	1.43
VFW VAK 191B	88	16	6	306	396	94	RB.193 (10,000lb) + (2) RR/MTU RB.162-81 (5,600 lb)	1.20
Yakovlev Yak-38 Forger	128	15	7	291	1299	126	Soyuz R-27V-300 (14,770 lb) + (2) Rybinsk RD-35-36FVR (6,725 lb)	1.13
Yakovlev Yak-141	191	18	14	536	1400	218	Soyuz R-79V-300 (30,864 a/b) + (2) Rybinsk RD-41 (9,040 lb)	1.41
Lockheed XV-4A	-	-	-	-	-	29	(2) PW JT12A-PW-3 (3,300 lb)	0.92
Rockwell XFV-12	87	13	9	671	-	133	P&W F401-PW-400 (30,000 lb a/b)	1.54
GE Ryan XV-5A	-	13	9	179	-	24	(2) GE J85-GE-5 (2,650 lb)	0.43
Lockheed Martin X-35	267	15	11	581	1931	191	P&W F119-SE611 (approx 20,000 lb vertical)	1.23

Table 3
Non-jet V/STOL aircraft data (adapted from Refs 15-18)

Aircraft	VTOW (kN)	Length (m)	b (m)	V _{max} (m/s)	Range (km)	Thrust (kN)	Power Plant	T/W
Transcendental Model 1G	8	7.93	11.58	71	384	2	Lycoming O-290-A (160 hp)	0.22
Bell XV-3	21	14.00	9.15	78	890	4	P&W R-985 radial (450 hp)	0.20
Curtiss-Wright X-100	16	7.90	8.64	0	-	-	Lycoming T53-L-1 (1,000 shp)	
Curtiss-Wright X-19	53	12.83	6.55	200	536	20	(2) Lycoming T55-L-7 (2,650 shp)	0.37
Doak 16 VZ-4	14	9.75	7.77	103	370	6	Lycoming YT53 (860 bhp)	0.44
Bell X-22A	66	12.07	11.96	141	716	26	(4) GE YT58-GE-8D (1,250 shp)	0.40
Nord 500 Cadet	12	6.69	6.08	97	-	5	(2) Allison T63-A-5A (317 shp)	0.40
Vertol 76 VZ-2	14	-	-	94	210	7	Lycoming YT53-L-1 (860 hp)	0.48
Hiller X-18	147	19.20	14.60	111	736	95	(2) Allison T40-A-14 (7,100 eshp) + West J34 (3,400 lb)	0.65
LTV/Hiller/Ryan XC-142	183	17.70	20.60	185	756	50	(4) GE T64-GE-1 (3,080 shp)	0.27
Canadair CL-84 Dynavert	54	16.34	10.16	144	547	15	(2) Lycoming T53-LTC K-4A (1,450 shp)	0.28
Bell XV-15	58	12.83	17.42	153	800	18	(2) Avco Lycoming LTC1K-4K (1,800 shp)	0.30
Bell Boeing V-22 Osprey	212	17.50	14.00	154	2200	60	(2) Allison T406-AAD-400 (6,150 shp)	0.28
Robertson VTOL	-	-	-	-	-	-	Lycoming GSO-480 (340 hp)	
Ryan 92 VZ-3 Vertiplane	12	-	-	-	-	-	Lycoming T53-L-1 (1,000 shp)	
Fairchild 224 VZ-5 Fledgling	18	10.26	9.98	82	-	12	GE YT58-GE-2 (1,024 shp)	0.67
Lockheed XFV-1	72	11.23	8.36	258	-	21	Allison YT-40-A-14 (7,100 eshp)	0.28
Convair XFY-1 Pogo	72	10.66	8.43	229	-	23	Allison YT-40-A-14 (7,100 eshp)	0.32
McDonnell XV-1	24	15.37	7.92	91	400	5	Continental R-975-19 radial (550 hp)	0.18
Fairey Rotodyne	147	17.90	27.40	95	830	44	(2) Napier Eland 7 (2,800 shp)	0.30
Vanguard Omniplane	12	-	-	-	-	-	Lycoming O-540-A1A (850 hp)	
Kamov Ka-22 Vintokryl	349	27.00	22.50	99	1200	98	(2) Soloviev D-25VK (6,500 shp)	0.28
Piasecki 16H-1 Pathfinder	12	-	-	76	1152	5	P&W Canada PT6B-2 (550 shp)	0.47
Lockheed AH-56 Cheyenne	98	16.66	15.62	109	1971	-	GE T64-GE-16 (3,435 lb)	

Table 4
Flying cars specifications and performance data

Flying Car	V _{max} (m/s)	Range (km)	Length (m)	W _{max} (kg)	Payload (kg)	Power (kW)	T/W available	T/W required
Dragonfly	105	1200	4.0	485	204	132	1.04	1.13
Skyrider Macro	172	1482	4.3	850	318	522	1.12	1.15
Moller M400	161	1207	5.9	1090	340	537	1.15	1.14
MULE	51	925	5.3	1067	227	559	1.56	1.13