

# Experimental study on combined defrosting performance of heat pump air conditioning system for pure electric vehicle in low temperature

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**Abstract:** The development of defrosting technology is a crucial technical barrier to the application of ~~the~~ heat pump air conditioning system for ~~the~~ pure electric vehicle. The frosting on the air conditioning system significantly affects systematic performance and reliable operation especially in low temperature and high humidity climate condition. Therefore, in this paper, an experimental study of ~~low-low~~-temperature heat pump air conditioning system with the combined defrost technology of increasing enthalpy and temperature is carried out ~~in order~~ to find proper thermal management solutions. Based on the reverse-cycle methods, the combined defrost technology makes full use of the compressor air-supplying enthalpy-adding, air-cooled heat exchanger inside the vehicle preheating, temperature-raising, enthalpy-adding and the external heat exchanger condensation temperature-increasing technologies. The fast defrosting process can be realized by means of releasing the condensation heat and volume significantly while the ~~external-outer~~ heat exchanger ~~is~~ conducting a defrosting operation. Meanwhile, the ~~cold~~ cabin ~~cold~~-sensitivity can be reduced ~~correspondingly~~ while defrosting process taking place ~~correspondingly~~. Experimental results shows that under the operating condition of -20°C outside environment temperature and 80% relative humidity, ~~rapid-instant~~ defrosting time at fully defrosted ~~air-cooled heat exchanger outside the vehicle~~ can be controlled within 100 seconds.

**Keywords:** Heat pump, Pure electric vehicle, Air conditioning, Defrosting, Thermal management

## 1. Introduction

With the intensifying energy crisis and the increasing environmental problems, it is imperative to take actions for energy saving and environmental protections on automotive industries. Pure electric vehicle (PEV) as disruptive technology provide an alternative way to replace traditional automotive industry ~~in order~~ to achieve sustainable development ~~in near future~~ ~~shortly~~. To maintain the PEV working at proper temperature and humidity condition, vehicular air conditioning system becomes an indispensable sub-system that it not only provides the thermal comfort in the cabin but also contributes to the safeties of traction batteries and power ~~electronics~~ ~~electronics~~ [1, 2]. The wide-ranging features of ~~the~~ ~~constantly changing~~ ~~evolving~~ environment outside the car has also raised the requests on the air conditioning system performance in the PEV. And ~~the~~ heat pump air conditioning system has such advantages as high efficiency, energy saving, environmental protection that it is becoming the priority of vehicular air conditioning in the PEV[3-6]. There are, in spite of

42 ~~mentioned~~ merits mentioned above, still some issues of itself especially in low  
43 temperature and high humidity ambient. The exterior heat exchanger of the heat pump prone  
44 to frost while the system is in heating mode. It not only causes both blockages of air channels  
45 and increase of ventilation resistance, but also the overall thermal resistance of exterior heat  
46 exchanger. Consequently, the frost will be accumulated and thickened resulting in ~~serious~~  
47 severe deterioration of working performance and reliability of vehicular conditioning  
48 ~~system~~system [7-9]. Therefore, it is important to find out the main factors of influencing  
49 defrost in the exterior heat exchanger ~~in order~~ to reduce defrosting time through reasonable  
50 and effective control strategies.

51 An eEvaporator is a unit where it is easy to frost, so to analyze operating characteristics of  
52 the evaporator in the case of defrosting is the key to studying the defrosting of the heat pump  
53 system. In the 1970s, Sanders, a Dutch[10] began the study on defrosting of air-conditioning  
54 evaporators, who created a model of evaporator defrosting of the air-conditioning system in  
55 his doctoral thesis, and recorded the whole course of defrosting through experiments and  
56 analyzed the distribution of energy consumption in the system during the defrosting. In the  
57 1980s, E.N.АНДРАЧНИКОВ, a scholar of the former Soviet Union[11] proposed an  
58 ~~effective~~efficient way of automatic evaporator defrosting, and the system was designed with  
59 main and secondary evaporators, and a 2\_PM time relay was used for control over the two  
60 evaporators defrosting alternately. D. L O'Neal and Payne[12] studied the effect of the air  
61 volume of the evaporator fan on the defrosting performance. Based on the basic air volume of  
62 72m<sup>3</sup>/min, experiments were conducted at a low air volume of 40m<sup>3</sup>/min and a high air  
63 volume of 88m<sup>3</sup>/min respectively. The results showed that compared with the basic air  
64 volume, the defrosting time and water accumulation after defrosting were greatly  
65 significantly reduced ~~under~~in the low air volume, yet it lowered the evaporating temperature  
66 of the system and increased the frosting rate of heat exchanger; under the high air volume, the  
67 heat exchange of the system was increased, meanwhile, the defrosting time was prolonged,  
68 yet it increased the evaporating temperature of the system which lowered the frosting rate of  
69 the heat exchanger. Padhmanabhan[13] compared the performance difference between finned  
70 evaporator and micro-channel evaporator during defrosting, and found that the defrosting  
71 time of the finned evaporator was about twice of that of micro-channel evaporator, but the  
72 frosting rate of the micro-channel was ~~obviously~~apparently higher than that of the finned  
73 evaporator.

74 In recent years, computers are used to simulate and analyze the defrosting performance of  
75 the heat pump system, which ~~has~~ve made rapid progress. Liu[14], based on the energy  
76 conservation equation, created a hot air defrosting dynamic cycle ~~dynamic~~ model, aiming to  
77 simulate the performances of evaporator and condenser at reverse cycle defrosting, ~~besides,~~  
78 ~~€~~Through experiments, the model proved that it could not only simulate characteristics of  
79 defrosting of the system, but also ~~simulate~~affect the whole defrosting course. Dopazo[15]  
80 created a heat pump evaporator defrosting model on the basis of hot air, the model divided  
81 the defrosting process into six stages: preheating, defrosting outside tubes, defrosting of fins,  
82 induced air, water film formed on fins surfaces, drying and heating, the control volume in  
83 each stage was represented by a node in the system model. A finite difference method is used  
84 to solve the equation, and the results included time needed for defrosting, energy distribution

85 during defrosting, characteristics of instantaneous refrigerant and temperature distribution of  
86 finned tubes. Qu[16, 17] firstly studied ~~characteristics~~ features of the multi-tube heat  
87 exchanger in defrosting, and the results showed that the defrosting time of upper layers of  
88 tubes was faster than that of the lower ones, the defrosting efficiency was estimated to be  
89 34.5%. In order to quantitatively analyze the effect of ~~different~~ various layers of tubes on  
90 defrosting, he created a semi-empirical mathematical model and the defrosting time trend  
91 calculated for different layers from top to bottom was the same as the conclusion of the  
92 experiment, and pointed out that the frosting time of lower layers of tubes reduced the  
93 defrosting efficiency of the system.

94 At present, it is still at the preliminary stage that there are few researches on defrosting of  
95 heat pump PEV air conditioning system. Zhong Hua and others make defrosting control ~~in~~  
96 ~~terms of~~ regarding traditional vehicle design in combination with the electronic expansion  
97 valve, and enhance air volume of the evaporator while increasing the electronic expansion  
98 valve ~~opening~~ opening [18]. Wu et al. find out through experiment that while the heat pump  
99 air conditioning system for PEV is supplying heat ~~at~~ in low temperature, the outdoor micro  
100 channel heat exchanger was frosted severely, which influences the heating capacity of the  
101 system and the coefficient of performance, but the defrosting solution is not proposed[19].  
102 Therefore, the ~~experimental~~ temporary tables of ~~low~~ low-temperature heat pump air  
103 conditioning system for PEV is designed[9], and the condensation temperature and defrosting  
104 speed under different working conditions are tested. In addition, the variants are analysed  
105 such as system cooling capacity, exhaust temperature, outlet air temperature and the import  
106 and export temperature of exterior heat exchanger along with the changes of system defrost  
107 operating time. The influence on exterior heat exchanger defrosting performance by different  
108 factors ~~is~~ are also studied in order to determine the fast and reliable defrosting method, ~~and~~  
109 provide an experimental basis for further improvement of the performance of PEV air  
110 conditioning system.

## 112 2. Heat pump type air conditioning system for PEV

113 The test rig of a low-temperature heat pump air conditioning system for PEV is designed  
114 and established using the quasi-two-stages compression principle. It combines with both the  
115 characteristics of low-temperature heat pump technology and automotive air conditioning  
116 conditions as shown in Fig.1. This test rig consists of a compressor, four-way valve, air-  
117 cooled heat exchanger outside the vehicle, one-way valve, liquid storage drier, main  
118 expansion valve, air-cooled heat exchanger inside the vehicle, air-supplying expansion valve,  
119 and intermediate heat exchanger as well as other auxiliary parts.

120 The system can achieve multiple basic working modes of electric vehicle cooling, battery  
121 electric heating, and air-cooled heat exchanger outside the vehicle defrosting under different  
122 working conditions. In cooling mode, the four-way valve switches into the cooling channel  
123 which is the same as ~~ordinary~~ conventional car air conditioning cooling processes. The  
124 circulating refrigerant is discharged through compressor with high pressure and subsequently  
125 flow into air-cooled heat exchanger outside the vehicle for condensation process. ~~Thereafter~~  
126 After that, it flows into liquid storage drier through the one-way valve. Then the refrigerant

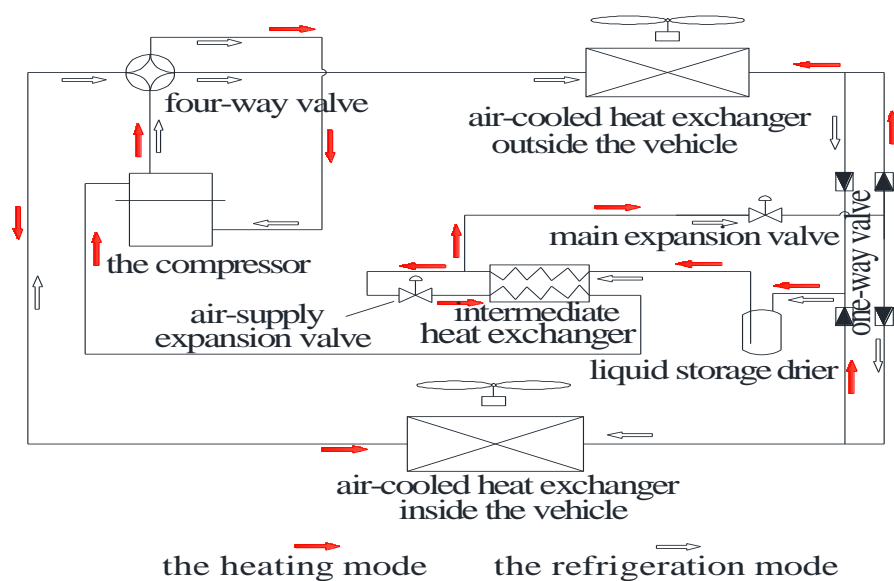
127 flows into the main expansion valve after going through the intermediate heat exchanger, and  
128 then low pressure and low-temperature flow enters into an air-cooled heat exchanger inside  
129 the vehicle for evaporation through the one-way valve. Eventually, it is absorbed by the  
130 compressor after going through the four-way valve.

131 In heating mode, the four-way valve switches into the heating channel, the circulating  
132 refrigerant is discharged ~~through~~from the compressor at high pressure and high-temperature  
133 state. Then the flow enters into an air-cooled heat exchanger inside the vehicle for  
134 condensation purpose, later on, it flows into the liquid storage drier through the one-way  
135 valve and directly flows into the main circulating pipeline of the intermediate heat exchanger.  
136 Different from the cooling mode, the circulating refrigerant ~~is~~are separated into two streams  
137 after flowing out of the intermediate heat exchanger in order to achieve both mass flow and  
138 temperature reduction by the air-supplying expansion valve. The auxiliary circulating  
139 pipeline ~~is~~are formed ~~in order~~ to exchange heat in the intermediate heat exchanger with  
140 circulating refrigerant in the main circulating pipeline. ~~This-It~~ will help increase the degree of  
141 the pipeline. On the other hand, the circulating refrigerant in ~~main~~primary circulating  
142 pipeline flows into the air-cooled heat exchanger outside the vehicle for evaporation purpose  
143 through the one-way valve after mass flow and temperature reduction in the air-supplying  
144 expansion valve and main expansion valve. Finally, the main flow ~~is~~are absorbed by the  
145 compressor through the four-way valve, and it is also blended with the circulating refrigerant  
146 from an auxiliary pipeline in the compression chamber in which the flow are from air-  
147 supplying opening through the one-way valve.

148 When the air-cooled heat exchanger outside the vehicle is in defrosting mode, the reverse  
149 cycle rapid defrost technology of enthalpy and temperature rise can be applied. The four-way  
150 valve switches into cooling mode, the circulating refrigerant are discharged by the  
151 compressor and then flow into the air-cooled heat exchanger outside the vehicle through the  
152 four-way valve for condensation and defrosting purposes. Afterwards, the refrigerants flows  
153 into the liquid storage drier through the one-way valve, and high-pressure refrigerants flow  
154 into the main expansion valve through the intermediate heat exchanger. Eventually, the flow  
155 with low pressure and low-temperature enters into an air-cooled heat exchanger inside the  
156 vehicle for evaporation process and the full cycle will be finished by the compressor through  
157 the same four-way valve.

158 The theoretical cycle of the electric vehicle-based low-temperature heat pump air-  
159 conditioning system, designed by this article, is shown in Fig.2, the working medium in air  
160 recirculation pipelines enters the compressor suction cavity of compressor through the intake  
161 port on the compressor end of cover, which is an insulating and throttling process[20]: After  
162 the working medium in the recirculation pipeline travels through the intake port, a middle  
163 pressure is reduced to be the suction pressure of compressor, there are a few circulating  
164 medium mixed with the suction of the compressor in the recirculation pipelines. During the  
165 course, the superheat of circulating medium was reduced in the compression cavity of the  
166 compressor, after compression, the discharge temperature was reduced, or there are still a few  
167 liquid of circulating medium, according to the insensitiveness of scroll compressor to wet  
168 compression, the circulating medium will continuously evaporate and absorb the heat

169 generated due to vapour compression and friction of kinetic and stationary scroll plates of  
 170 compressor during the compression, which greatly reduced the air discharge temperature of  
 171 the compressor, as shown in Fig. 2, the process from 9' to 2'. The mixture of working medium  
 172 in the recirculation pipelines and that of compressor suction cycle reduce the superheat of  
 173 working medium in the compression cavity from the compressor or some carry a little liquid,  
 174 which both increase the quality and flow of working medium for compression in the  
 175 compressor. Thus it ~~increased~~ improved the quality and flow of the working medium in the  
 176 condensing process and increased the heating capacity of the heat pump system [21]. The  
 177 working medium in the recirculating pipelines will evaporate and absorb heat in the  
 178 ~~middle~~intermediate heat exchanger, which is a latent heat ~~of~~in vaporization, yet the liquid  
 179 working medium in the condensing heat pump in another pipeline of the ~~middle~~intermediate  
 180 heat exchanger released heat, which is a sensible heat. The liquid medium work of the heat  
 181 pump before entering the main expansion valve has a great super-cooling effect, which  
 182 increases the cooling capacity of the heat pump working medium in the evaporator. While,  
 183 the super-cooling is limited by the mixed air pressure, that is, the working medium of the  
 184 lowest main loop heat pump is super-cooling which exceeds the saturated temperature  
 185 corresponding to the air supply pressure. After working medium in the air recirculation  
 186 pipelines is mixed with that of the air intake heat pump of the compressor, it will increase the  
 187 quality and flow of working medium of the heat pump in the compression cavity of the  
 188 compressor, so the compressor power is increased a little. Meanwhile, the ~~middle~~intermediate  
 189 heat exchanger increases the super-cooling of heat pump working medium in the main  
 190 expansion valve, the refrigerating capacity of the heat pump system is increased in the  
 191 evaporator. The expansion valve of recirculation controls the air pressure and the quality and  
 192 flow of working medium in the pipelines, if losing the air expansion valve, the air  
 193 recirculation pressure and the quality and flow of working medium will rise; vice versa it will  
 194 drop, which has higher influence to the performance of air circulation-based heat pump air  
 195 conditioning system.



**Fig.1.** Diagram of the heat pump air conditioning system of the pure electric vehicle.

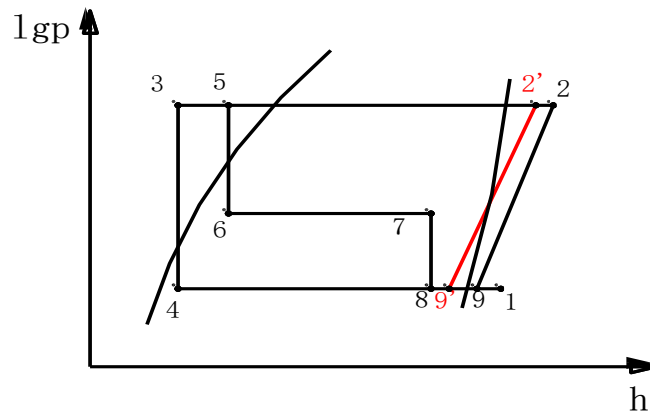


Fig.2. Log p-h diagram of the heat pump cycle with middle heat exchanger

196 **3. The Modelling of Concentric Cylindrical Thermoelectric Generator**

197 The experiment is to study the characteristics of the defrosting mode in heat pump air  
 198 conditioning system of PEV. ~~therefore~~ ~~Therefore~~ heating is supplied within the cabin, and  
 199 the air conditioning system is working at low temperature and high humidity condition which  
 200 leads to heat exchanger frosting outside the vehicle. The frosting conditions of this  
 201 experiment are described in Table1.

202

**Table 1** The working condition of frosting for the experiment.

Working condition	Parameters
Ambient temperature outside the vehicle /°C	-20
Ambient temperature inside the vehicle /°C	15、 20、 25
Relative air humidity outside the vehicle/%	80
Revolving speed of compressor/rpm	5000
Air output of fan inside the vehicle/(m <sup>3</sup> /h)	540
Fan speed outside the vehicle/(m/s)	4.5
Air supplement rate /%	30

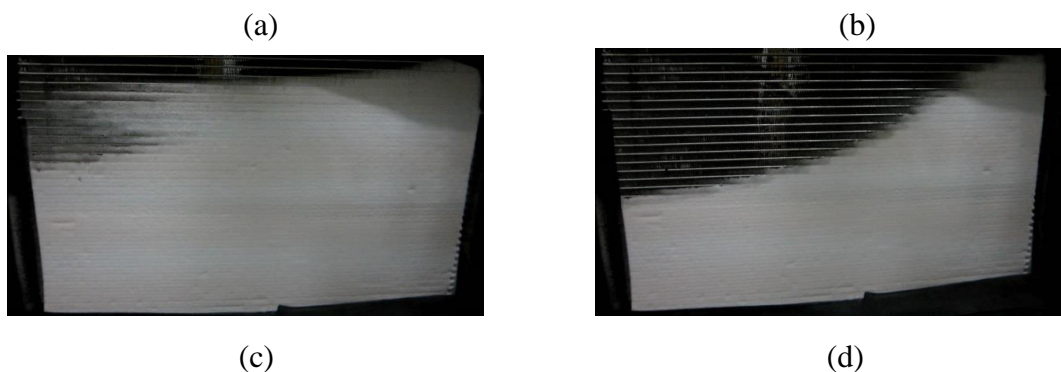
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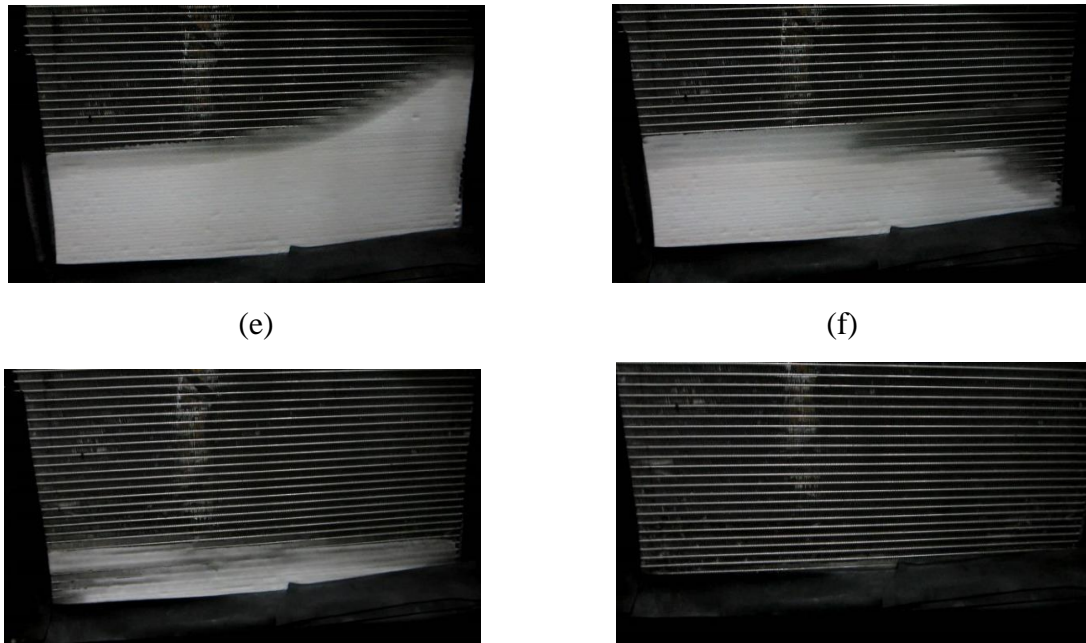
204 If the wind speed at air-cooled heat exchanger outside the vehicle is lower than 0.2 m/s, it  
 205 is noted that the frosting of **air-cooled heat exchanger outside the vehicle** completes  
 206 thoroughly. The frosting scenario is shown inas Fig. 3.



Fig. 3. Complete frosting of heat exchanger outside the vehicle.

207 In the present study, the composite defrosting technology is adopted based on the  
208 defrosting of reversed cycle, integrally uses the technology of increasing enthalpy by air-  
209 supplying of compressor, technology of preheating and raising temperature and increasing  
210 enthalpy of heat exchanger inside the vehicle, technology of increasing condensing  
211 temperature of heat exchanger outside the vehicle, to make heat release of condensation and  
212 heat transfer temperature difference of condensation increase obviously, which realize  
213 defrosting rapidly and reduce draft of cold air supply inside the vehicle when defrosting. Fig.  
214 4 shows the defrosting of heat exchanger outside the vehicle, which is taken after the  
215 defrosting begins with an interval of 20 seconds. Fig. 4(a) is taken when defrosting begins.  
216 Fig. 4(b) is after defrosting operates 20 seconds. At that time, the air exhaust of compressor  
217 passes upside of heat exchanger outside the vehicle to melt the frost here firstly. Fig. 4(c) is  
218 after defrosting operates 40 seconds. At that moment, the defrosting area of heat exchanger  
219 outside the vehicle is enlarged. After defrosting operates 60 seconds (Fig. 4(d)), the area  
220 of defrosting of heat exchanger outside the vehicle is further enlarged extended; after the  
221 defrosting operates 80 seconds (Fig. 4(e)), the frost layer on the surface of heat exchanger  
222 outside the vehicle is basically melted completely. Only the frost layer on the surface of the  
223 flat tube that is close to the bottom doesn't melt; after the defrosting operates 100 seconds  
224 (Fig. 4(f)), the defrosting of heat exchanger outside the vehicle complete.





**Fig. 4.** Defrosting of heat exchanger outside the vehicle: (a) defrosting begins. (b) defrosting operates for 20 seconds. (c) defrosting operates for 40 seconds. (d) defrosting operates for 60 seconds. (e) defrosting operates for 80 seconds. (f) defrosting operates for 100 seconds.

#### 4. ~~Analysis on experiment~~ Experiment results

##### 4.1 Influence of environment temperature inside the vehicle on defrosting characteristics

When the ambient temperature outside the vehicle is 0°C and the temperatures inside the vehicle are 15°C, 20°C and 25°C respectively, under frosting conditions, defrost after the frosting completes on the surface of heat exchanger outside the vehicle. When defrosting begins, other parameters shall stay the same with those under frosting conditions. In the defrosting process, the situation that the average condensation temperature and defrosting time change with the temperature inside the vehicle ~~is~~ are shown in Fig. 4.

It is shown in Fig. 5 that the higher the environment temperature inside the vehicle, the higher the average condensation temperature in the defrosting process be and the shorter the defrosting time will be. ~~This-It~~ is because when the system is in defrosting mode, the heat exchanger inside the vehicle changes from the condenser to evaporator. The environment inside the vehicle changes from the side of the cold source to the side of the heat source. The higher the environment temperature inside the vehicle, the higher the evaporating temperature will be. The performance of the system will be better. The speed of defrosting accelerates.



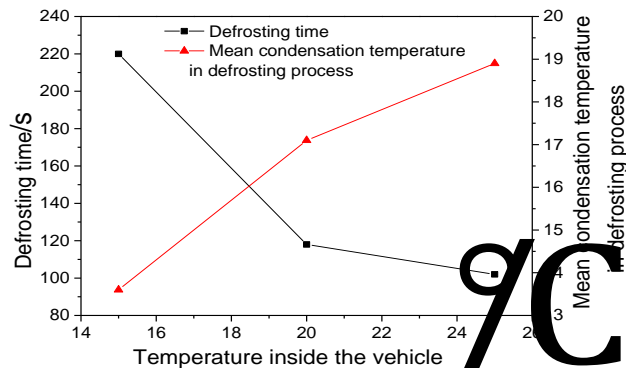


Fig. 5. Influence of temperature inside the vehicle on average condensation temperature and defrosting time during the defrosting process.

#### 241 4.2 Influence of revolving speed of compressor on defrosting characteristics

242 When the ambient temperature outside the vehicle is 0 °C, and the temperature inside the  
 243 vehicle is 25 °C, under frosting conditions, defrost after the frosting completes on the surface  
 244 of heat exchanger outside the vehicle. When defrosting begins, change the revolving speeds  
 245 of the compressor into 5000 rpm, 6000 rpm and 7000 rpm respectively and keep other  
 246 parameters stay the same with those under frosting conditions. The situation that average  
 247 condensation temperature and defrosting time change with the revolving speed of compressor  
 248 during the defrosting process is-are shown in Fig. 6.

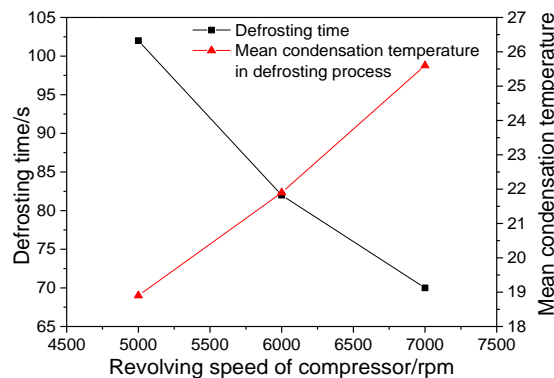


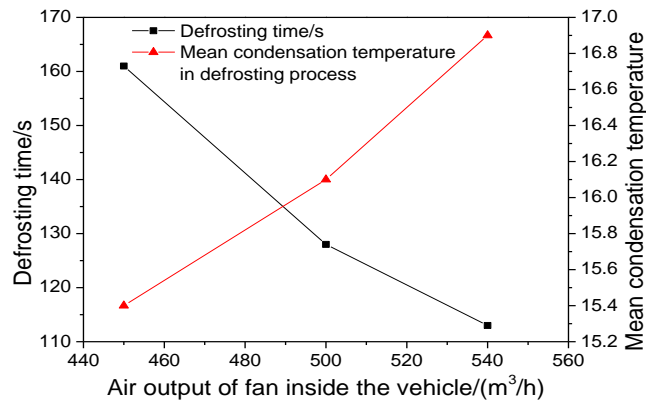
Fig. 6. Influence of revolving speed of compressor on average condensation temperature and defrosting time during defrosting process.

249 It can be seen from Fig. 6 that the higher the revolving speeds of the compressor, the  
 250 higher the mean condensation temperature in defrosting process will be and the shorter the  
 251 defrosting time will be. The revolving speed of compressor increases. The mass flow rate of  
 252 refrigerating fluid that enters condenser increases. The heat release of condenser  
 253 increases. The speed-rate of defrosting accelerates [22].

#### 254 4.3 Influence of air output of fan inside the vehicle on defrosting characteristics

255 When the ambient temperature outside the vehicle is 0 °C, and the temperature inside the  
 256 vehicle is 20 °C, under frosting conditions, defrost after the frosting completes on the surface  
 257 of heat exchanger outside the vehicle. When defrosting begins, change air output of fan inside  
 258 the vehicle into 450 m<sup>3</sup>/h, 500 m<sup>3</sup>/h and 540 m<sup>3</sup>/h respectively and let other parameters stay  
 259 the same with those under frosting conditions. The situation that average condensation

260 temperature and defrosting time change with air output of fan during the defrosting process is  
 261 are shown in Fig. 7.  
 262

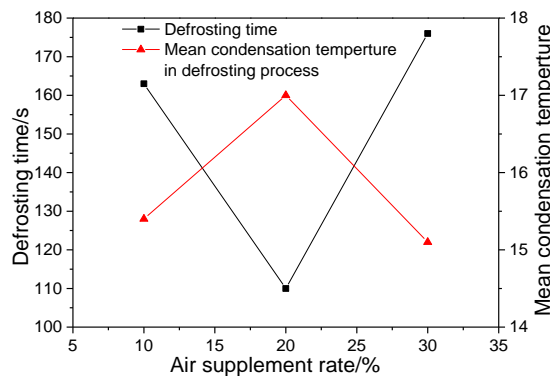


**Fig.7.** Influence of air output of fan inside the vehicle on average condensation temperature and defrosting time during the defrosting process.

263 **Fig. 7 shows** that the greater the air output of fan inside the vehicle, the higher the average  
 264 condensation temperature in the defrosting process will be and the shorter the defrosting time  
 265 will be. ~~This~~ It is because when the system is in defrosting mode, the heat exchanger inside  
 266 the vehicle changes from the condenser to evaporator. With the increase of air output of fan  
 267 inside the vehicle, the heat exchange amount of evaporator increases. The heat release of  
 268 condenser also increases. ~~The~~ speed-rate of defrosting of heat exchanger outside the vehicle  
 269 accelerates.

270 **4.4 Influence of air supplement rate (air recirculation percentage in the air discharge**  
 271 **of compressor) on defrosting characteristics**

272 When the ambient temperature outside the vehicle is 0\_°C, and the temperature inside the  
 273 vehicle is 20\_°C, under frosting conditions, defrost after the frosting completes on the surface  
 274 of heat exchanger outside the vehicle. When defrosting begins, it is necessary to control the  
 275 air supplement rate at 10%, 20% and 30% and keep other parameters stay the same with  
 276 those under frosting conditions. The situation that the average condensation temperature and  
 277 defrosting time during defrosting process change with air supplement rate is shown in Fig. 8.



**Fig. 8.** Influence of air supplement rate on average condensation temperature and defrosting time during defrosting process

278 Fig. 8 shows that when the air supplement rate is 20%, the average condensation  
279 temperature in the defrosting process is the highest and the defrosting time is the shortest.  
280 Compared with the situation that the air supplement rate is 20%, when the air supplement rate  
281 is 10%, the mass flow rate of refrigerating fluid in circulation line of air supplement reduces.  
282 The heat exchange amount in intermediate heat exchanger between it and working medium of  
283 the main line is small. It causes that the condensate depression before the main expansion  
284 valve is small and leads to the fact that the proportion of working medium of gas state in  
285 evaporator increases. The resistance increases. Evaporating temperature and evaporating  
286 pressure reduce. It goes against the absorption of the evaporator, thus reduces the heat release  
287 of the condenser and prolongs the defrosting time. When the air supplement rate is 30%,  
288 although the condensate depression before the ~~main-primary~~ expansion valve increases and  
289 the resistance of working medium in evaporator reduces, the mass flow rate of working  
290 medium that enters evaporator is small. The ~~influence-impact of it on~~ the reduction of heat  
291 absorption capacity of the evaporator is bigger than the influence of reduction of working  
292 medium resistance in evaporator on increase of heat absorption capacity of the evaporator. It  
293 causes the reduction of total heat absorption capacity of evaporator and heat release of the  
294 condenser. Compared with the moment when the air supplement rate is 20%, defrosting time  
295 increases.

296

#### 297 **4.5 Influence of fan delivery outside the vehicle on defrosting characteristics**

298 The change of fan delivery outside the vehicle is realized through changing the frequency of  
299 fan outside the vehicle. When the ambient temperature outside the vehicle is 0°C and the  
300 temperature inside the vehicle is 20°C, under frosting conditions, defrost when the frosting  
301 completes on the surface of heat exchanger outside the vehicle. When defrosting begins,  
302 change the frequencies of fan outside the vehicle into 0Hz, 5Hz and 10Hz, keep the revolving  
303 speed of compressor at 6,000 rpm and keep other parameters stay the same with those under  
304 frosting conditions. Figs 9, 10 and 11 show the situations when refrigerating capacity of the  
305 system, exhaust gas temperature, outlet air temperature, temperatures at inlet and outlet of  
306 heat exchanger outside the vehicle change with time of defrosting operation of the system.  
307 With the operation of defrosting, the refrigerating capacity of the system reduces gradually.  
308 The exhaust gas temperature reduces firstly and then increases. The outlet air temperature  
309 reduces gradually. The temperatures at inlet and outlet of heat exchanger outside the vehicle  
310 increases gradually. When the frequency outside the vehicle change with the time of  
311 defrosting operation of the system of a fan outside the vehicle is 0Hz, the refrigerating  
312 capacity of the system reduces 26.6 %. The outlet air temperature reduces 3.2°C. When the  
313 frequency is 5Hz, the refrigerating capacity reduces 36.2 %. The outlet air temperature  
314 reduces 4.9°C. Although the outlet air temperature reduces, the lowest temperature is above  
315 24°C. So it will not let people inside the vehicle have the feeling of cold air.

316 Fig.12 shows the curve that average condensation temperature and defrosting time change  
317 with frequency of fan outside the vehicle in defrosting process. The greater the frequency of  
318 fan outside the vehicle, the greater the air output of fan outside the vehicle will be. The  
319 average condensation temperature in the defrosting process will be lower. The defrosting  
320 time will be longer. ~~This-It~~ is because the system is in defrosting mode. The heat exchanger  
321 outside the vehicle serves as the condenser. The air output of fan outside the vehicle increases.

322 The condensing temperature of heat exchanger outside the vehicle reduces. The speed of  
 323 defrosting of heat exchanger outside the vehicle slows down.  
 324

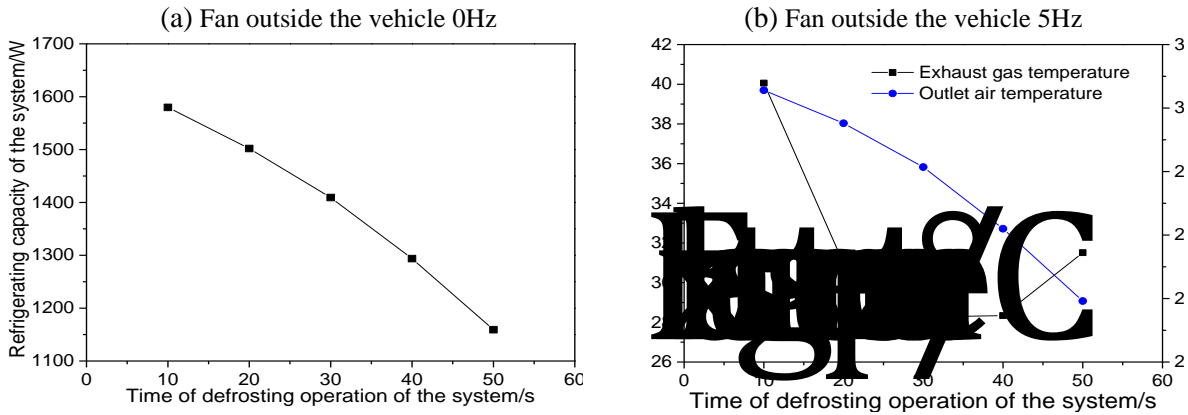


Fig. 9. Curve that refrigerating capacity changes with time of defrosting operation of the system.

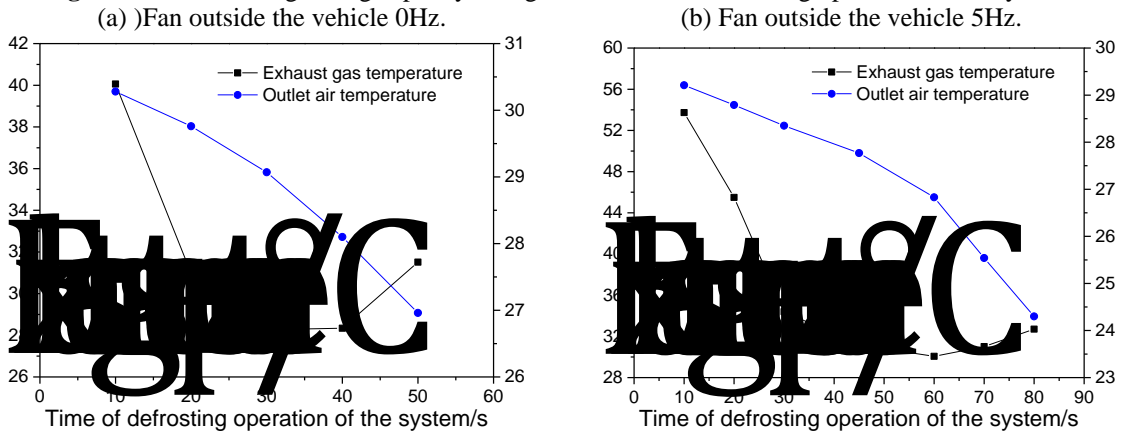


Fig.10. Curve that exhaust gas temperature and outlet air temperature change with time of defrosting operation of the system.

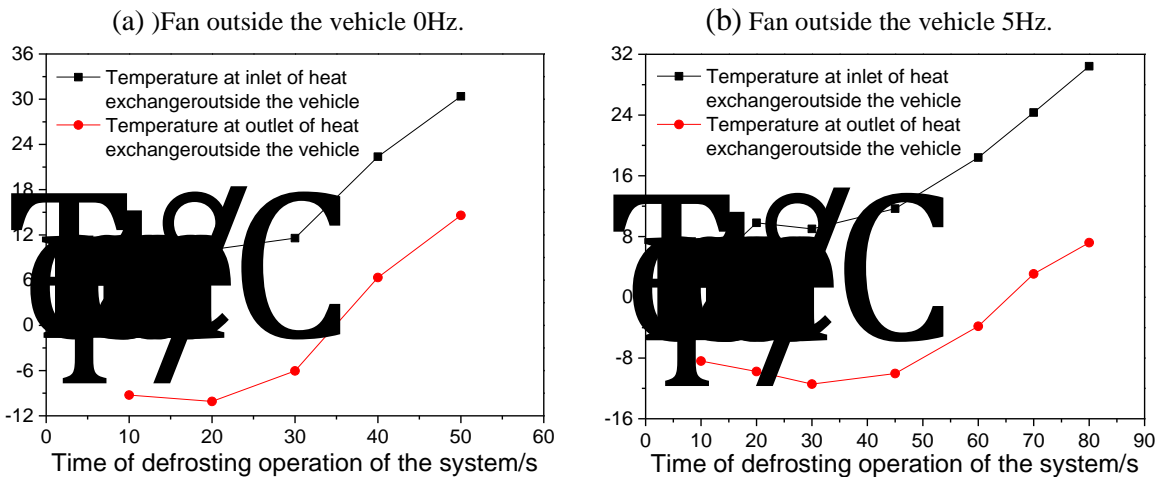
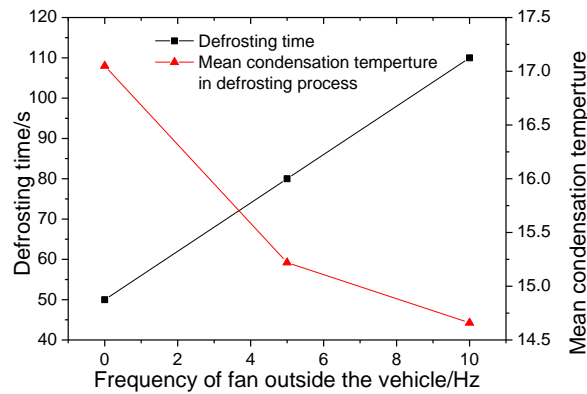


Fig.11. The curve that the temperatures of inlet and outlet of the heat exchanger.



**Fig.12.** Influence of fan delivery outside the vehicle on average condensation temperature during the defrosting process and defrosting time

## 326 5. Conclusion

327 Aiming at the problem that the heat exchanger outside the vehicle is easy to frost when the  
 328 heat pump type air conditioning system for PEVs operates under the environment of low  
 329 temperature and high humidity, **the article proposes a technical method of fast defrosting**  
 330 **relying on increasing temperature and enhancing gas injection in reverse circulation.**  
 331 **Following the basic principle of defrosting via reverse circulation, the method well integrates**  
 332 **the air speed control outside, air and effect increase of compressor, air intake preheating**  
 333 **inside and so on, so that during the defrosting operation of heat exchanger outside, the**  
 334 **condensing temperature and heat release in condensing are both increased obviously so as to**  
 335 **achieve rapid defrosting.** Experimental research shows that it can obviously shorten the  
 336 defrosting time through raising the in-car temperature, the revolving speed of compressor, air  
 337 output of draught fan inside the car and reducing fan delivery outside the vehicle and  
 338 controlling proper air supplement rate, and then ~~adequately~~properly improve the performance  
 339 of air conditioning system to ensure the stable operation of air conditioning system of PEVs.

340

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