

1	Wetting Transition Energy Curves for a Droplet on a Square-Post
2	Patterned Surface
3	
4	Wei Gong ¹ , Yingqing Zu ² , Sheng Chen ¹ , Yuying Yan ^{1*}
5	
6	¹ Fluids & Thermal Engineering Research Group, Faculty of Engineering, University
7	of Nottingham, University Park, Nottingham, NG7 2RD, UK
8	² Department of Aeronautics and Astronautics, Fudan University, Shanghai, 200433, P.R.
9	China
10	
11	
12	Abstract: Due to the property of water repellence, biomimetic superhydrophobic surfaces
13	have been widely applied to green technologies, in turn inducing wider and deeper
14	investigations on superhydrophobic surfaces. Theoretical, experimental and numerical studies
15	on wetting transitions have been carried out by researchers, but the mechanism of wetting
16	transitions between Cassie-Baxter state and Wenzel state, which is crucial to develop a stable
17	superhydrophobic surface, is still not fully understood. In this paper, the free energy curves
18	based on the transition processes are presented and discussed in detail. The existence of energy
19	barriers with or without consideration of the gravity effect, and the irreversibility of wetting
20	transition are discussed based on the presented energy curves. The energy curves show that
21	different routes of the Cassie-to-Wenzel transition and the reverse transition are the main reason
22	for the irreversibility. Numerical simulations are implemented via a phase field lattice
23	Boltzmann method of large density ratio, and the simulation results show good consistency
24	with the theoretical analysis.
25	
26	Keywords: wetting transition, energy curves, lattice Boltzmann method
27	

28 1 Introduction

Surface roughness, which can be found in the form of micro or hierarchical structures in nature, 29 30 has been widely investigated for its enhancement to hydrophobicity [1-4]. Through mimicking 31 natural superhydrophobic surfaces including plant leaves and animals such as lotus leaves, rice 32 leaves and water strider legs, manmade superhydrophobic surfaces via various of 33 methodologies have been presented and applied in industrial applications, for instance, coating, 34 self-cleaning surfaces, microfluidic devices with surface-tension-induced drop motion and so 35 forth [5, 6]. Among all the natural water-repellence examples, lotus leaves are the most 36 impressive for their superhydrophobic characteristic which is also known as "lotus effect". Due 37 to the micrometre order length scales of the micro posts on the surfaces, the apparent contact angle (APCA) of lotus leaves is approximately 160° while the hysteresis angle is just about 4° 38 39 [7].

40

As the wetting phenomena have been investigated over the past decades, significant progress
on theoretical models has also been achieved with considerable attention. The starting point of
wetting on an ideal rigid, flat and homogeneous surface is characterized by the well-known
Young's Equation [8]:

$$45 \qquad \cos\theta_Y = \frac{\sigma_{SG} - \sigma_{SL}}{\sigma_{LG}} \tag{1}$$

46 where σ is the surface tension which represents the energy per unit area of the interface 47 between solid/gas, solid/liquid or liquid/gas, and θ_Y is the Young's contact angle. Young's 48 Equation reveals the relationship between surface tensions and contact angle in the ideal 49 situation, however, it cannot be applied to most real surface conditions due to the existence of 50 surface roughness. For the surface roughness, a new correlation where the apparent contact 51 angle is related to surface roughness was presented by Wenzel [9]:

52
$$\cos\theta_w = r \frac{\sigma_{SG} - \sigma_{SL}}{\sigma_{LG}}$$
 (2)

53 which is also normally written as the following reformed equation:

54
$$\cos\theta_w$$

$$55 = r \cos \theta_{\rm Y} \tag{3}$$

where r, the roughness parameter corresponding to the "roughness factor", which is also referred to as roughness area ratio, denotes as the ratio of the actual surface area with respect to the projected structure surface, and θ_w is the Wenzel's angle. The Wenzel equation is associated with the homogeneous wetting states, where the grooves caused by the surface roughness are penetrated with water. Apart from the homogeneous wetting state, there is another stable state, the heterogeneous wetting state, and the corresponding equation to the heterogeneous wetting regime was proposed by Cassie and Baxter [10]:

$$63 \qquad \cos\theta_{CB} = f\cos\theta_Y + f - 1 \tag{4}$$

64 If the roughness ratio, r_f , the ratio of the actual wetted area over the projected area is 65 considered, equation (4) can be modified to the following form [11]:

$$\cos\theta_{CB} = r_f f \cos\theta_Y + f - 1 \tag{5}$$

where f is the area fraction on the horizontal projected plane of the liquid-solid contact area over the total area of solid-liquid and liquid-gas contact. Equation (5) would become the same form with Wenzel's equation when f = 1 and $r_f = r$. By equating equation (3) and equation (5), the critical contact angle theoretically used to separate the two wetting states can be calculated as [12]:

$$72 \qquad \cos\theta_C = \frac{1-f}{r_f f - r} \tag{6}$$

It should be noted that when $\theta_C > 90^\circ$, both two wetting states exist. Then the homogeneous wetting state is preferable only if $\theta_Y < \theta_C$, otherwise the droplet stays at a heterogeneous wetting state, theoretically [13]. However, it has been observed that, even the Young's angle is smaller than the critical angle, the Cassie-Baxter wetting state can exist, which means that Wenzel and Cassie Baxter states may stay on the same specific surface at the same time [14-18].

79

66

Bormashenko E. reviewed the main experimental and theoretical approaches to wetting transitions in 2010 and 2015 respectively [19, 20]. Experiments to study the wetting transitions were implemented by giving external factors such as pressure [21], initial velocity [22], evaporation of droplets [23], vibration [24], and electric field [25, 26]. And the role of gravity in wetting transitions was also discussed [11]. Neelesh A. Patankar [11] and Zu Y. et al [27] 85 theoretically analyzed the wetting transition from Cassie-Baxter state to Wenzel state from the 86 free energy point of view, and the energy barrier was discussed both in their work. Whyman G. 87 et al. [28] theoretically investigated the interfacial free energy and discussed the irreversibility 88 of Cassie-to-Wenzel transition. Ren W [29] computed the transition states, the energy barriers 89 and the minimum energy paths for Cassie-to-Wenzel transition using the string method. G. 90 Pashos et al. [30, 31] developed a numerical method to investigate the minimum energy paths 91 and the free energy changes were presented in their works. S. Prakash et al. [32] studied the 92 spontaneous recovery of superhydrophobicity on nanotextured surfaces using molecular 93 simulations. Bico J. et al. [33] and Aurbach D. et al. [34] studied the Cassie impregnating state 94 apart from the Cassie-Baxter state and Wenzel state, and Gibbs free energy curves of the three 95 wetting states were presented. In their work the impregnating state was observed via vibration 96 so that the liquid can impregnate the grooves outside of the droplet/solid interface. In this paper, 97 we focus on the transition between the more regular Cassie-Baxter and Wenzel wetting states.

98

99 Wenzel's equation and Cassie and Baxter's equation can describe the stable wetting states on 100 real rough surfaces to a great extent when the droplet size is much larger than the typical 101 roughness scale. Nevertheless, there are still points of the theory of wetting states which are not 102 fully understood. For instance, when a droplet stays in a stable wetting state, and how the 103 transition between the two wetting states occurs [13]. It is crucial to understand the mechanism 104 of wetting transition process for the design and manufacturing of devices with highly stable 105 superhydrophobic surfaces. This paper focuses on the wetting transition process as well as the 106 different wetting states on the simplest model, the square-post patterned surface from the free 107 energy point of view.

108

109 **2** Theoretical analysis

In the present study, the substrate patterned by square posts as the roughness surface is considered as shown in Figure 1, where a, b and h are the post width, post spacing, and post height respectively. It should be pointed out that the droplet size scale is much larger than the size scale of micro posts in the theoretical analysis. Under this assumption, the theoretical analysis can be conducted based on a single unit of patterned substrate with periodical pattern and the Wenzel and Cassie-Baxter equations can be used for the calculation of the apparent contact angles. In the presented pattern, r_f equals to 1.



1	1	7

118 Figure 1 Structure of the micro roughness surface

119

120 2.1 The model of net free energy

All the parameters needed for the following theoretical analysis are presented in Figure 2 in three typical wetting state cases. Firstly, considering a droplet staying steady on a flat ideal surface as shown in Figure 2(a), the equilibrium free energy can be calculated as [13]:

124
$$E_Y = S(\sigma_{SL} - \sigma_{SG}) + S'\sigma_{LG}$$
(7)

where S and S' represent the solid/liquid interface area and the liquid/gas interface area respectively. Similarly, the equilibrium free energy equations for Cassie-Baxter and Wenzel states are:

128

129
$$E_{CB} = S_{CB}(\sigma'_{SL} - \sigma_{SG}) + S'_{CB}\sigma_{LG}$$
(8)

130
$$E_W = S_W(\sigma'_{SL} - \sigma_{SG}) + S'_W \sigma_{LG}$$
(9)

131 where σ'_{SL} is the equivalent free energy per unit area of the solid/liquid interfaces for both of 132 the two states, while S_{CB} and S_W both represent the projected horizontal areas. Considering 133 the equivalent surface tension, Young's equation can be applied into the heterogeneous and 134 homogeneous wetting states:

 $\cos\theta_{CB}$

 $\cos\theta_W$

$$136 \qquad = \frac{\sigma_{SG} - \sigma'_{SL}}{\sigma_{LG}} \tag{10}$$

137

135

$$138 \qquad = \frac{\sigma_{SG} - \sigma'_{SL}}{\sigma_{LG}} \tag{11}$$

By combining the above equations, the free energy equations for Cassie-Baxter and Wenzelstates can be expressed as:

141
$$E_{CB} = S_{CB}[f(\sigma_{SL} - \sigma_{SG}) + (1 - f)\sigma_{LG}] + S'_{CB}\sigma_{LG}$$
(12)

142
$$E_W = S_W r(\sigma_{SL} - \sigma_{SG}) + S'_W \sigma_{LG}$$
(13)

143

144



145 146

147 Figure 2 Parameters of the droplet in (a) flat surface (b) Cassie-Baxter state and (c) Wenzel
148 state

149

150 2.2 Cassie-to-Wenzel wetting transition

151 2.2.1 Without gravity effects

Usually, the transition process from Cassie-Baxter state to Wenzel state can be easily observed, however, the reverse process is hard to be achieved. Thus it is generally agreed that the wetting transition from Cassie-Baxter state to Wenzel state is irreversible [20]. Figure 3 shows the two main processes of wetting transition: (a) water starting to penetrate the posts intervals without touching the bottom surface; (b) water immersing the bottom surface. The position of the air pocket in Figure 3(b) can be neglected because the immersing-bottom process just lowers the free energy and does not hinder the transition regarding the following analysis. \tilde{E}_{CB} and \tilde{E}_{W} are used to represent the intermediate free energy of the droplet. According to equation (7), there are:

161
$$\tilde{E}_{CB} = \tilde{S}_{CB} \left\{ \left[f + (r-1)\frac{h'}{h} \right] (\sigma_{SL} - \sigma_{SG}) + (1-f)\sigma_{LG} \right\} + \tilde{S}_{CB}' \sigma_{LG}$$
(14)

162
$$\tilde{E}_W = \tilde{S}_W \left[r - (1 - f) \frac{d'}{d} \right] (\sigma_{SL} - \sigma_{SG}) + \left[\tilde{S}'_W + \tilde{S}_W (1 - f) \frac{d'}{d} \right] \sigma_{LG}$$
 (15)

163 When h' and d' are on their extreme values h and d, the critical free energy states can be 164 achieved:

165
$$\hat{E}_{CB} = \hat{S}_{CB} \{ [f + (r-1)](\sigma_{SL} - \sigma_{SG}) + (1-f)\sigma_{LG} \} + \hat{S}'_{CB}\sigma_{LG}$$
(16)

$$\hat{E}_W = \hat{S}_W [r - (1 - f)] (\sigma_{SL} - \sigma_{SG}) + [\hat{S}'_W + \hat{S}_W (1 - f)] \sigma_{LG}$$
(17)



167 168

169

Figure 3 Intermediate states for transition (a) water starting to penetrate the posts

- 170 intervals without touching the bottom surface (b) water immersing the bottom surface
- 171

172 It has been proved that the differences of the liquid/gas area and the droplet bottom projected 173 area when transition happens are negligible owing to the much larger size scale compared to 174 that of the surface roughness, which means $\hat{S}_{CB} \approx S_{CB}$, $\hat{S}_W \approx S_W$, $\hat{S}'_{CB} \approx S'_{CB}$ and $\hat{S}'_W \approx S'_W$ 175 [11, 35]. Hence there is $\hat{E}_{CB} = \hat{E}_W = E_{Cr}$ for the same droplet in different states. And the 176 energy barriers for the two transitions process can be calculated as:

177
$$E_{bar}^{CB-Cr} = \hat{E}_{CB} - E_{CB} = S_{CB}(r-1)(\sigma_{SL} - \sigma_{SG})$$
(18)

178
$$E_{bar}^{Cr-W} = E_W - \hat{E}_W = S_W (f-1)(\sigma_{LG} - \sigma_{SL} + \sigma_{SG})$$
(19)

179

180 For hydrophobic surfaces, i.e. $\theta_Y > 90^\circ$, according to the Young's equilibrium equation, there

181 are
$$\sigma_{SL} - \sigma_{SG} > 0$$
 and $\sigma_{LG} - \sigma_{SL} + \sigma_{SG} > 0$, therefore

182			
183		E_{bar}^{CB-Cr}	
184	> 0	(20)	
185		$E_{bar}^{\mathrm{Cr}-W}$	
186	< 0	(21)	
187	Correspondingly, for hydrophilic water, i.e. $\theta_Y < 90^\circ$, there are $\sigma_{SL} - \sigma_{SA} < 0^\circ$	and σ_{LA} –	
188	$\sigma_{SL} + \sigma_{SA} > 0$, therefore		
189		E_{bar}^{CB-Cr}	
190	< 0	(22)	
191		$E_{bar}^{\mathrm{Cr}-W}$	
192	< 0	(23)	
193	Whether the transition can occur depends on the sign of the differential of free energy at the		
194	beginning of the process. For transitions from Cassie-Baxter state to Wenzel state and the		
195	reverse, the free energy differentials can be given as:		
	ST(B-Cr)		

196
$$\left. \frac{\delta E^{CB-Cr}}{\delta h'} \right|_{h'=0} = \frac{S_{CB}(r-1)(\sigma_{SL}-\sigma_{SG})}{h}$$
(24)

197

198 Consequently, without considering the gravity effect or other external forces, the free energy curves can be drawn in Figure 4. Figure 4(a) and Figure 4(b) show the case of $\theta_Y > 90^\circ$, when 199 two main roughness surface features exist: (a) $90^{\circ} < \theta_Y < \theta_C$, $E_{CB} > E_W$, according to the 200 201 assumption that the equilibrium state occurs when the free energy is minimized [11], both of 202 the two states exist, however, the Wenzel state is stable while Cassie-Baxter state is not; (b) 203 $\theta_Y > \theta_C, E_W > E_{CB}$, the droplet would stay in the Cassie-Baxter state, but may not in the 204 Wenzel state and the analysis relating to this is in the next section. This means the energy barrier always exists for the Cassie-to Wenzel transition for $\theta_Y > 90^\circ$. In addition, $\frac{\delta E^{CB-W}}{\delta h'}\Big|_{h'=0} > 0$ 205 206 denotes that the transition processes cannot happen spontaneously without any external stimuli triggering event. Figure 4(c) indicates that Cassie-Baxter state cannot be achieved if $\theta_Y < 90^\circ$, 207 when $E_{CB} > E_W$ and $\frac{\delta E^{CB-W}}{\delta h'}\Big|_{h'=0} < 0$ thus the droplet can only stays at the Wenzel state. It 208

should be noted that all the free energy curves presented in this paper are qualitatively constructed because there exist uncertainties for the wetting transitions, for example, the bottom droplet surface moving down along the posts is not definitely horizontal and when and which part of the droplet touches the bottom solid surface first is indeterminate.

213



drop radius is much smaller than $(\sigma_{LA}/\rho g)^{1/2}$. However, its influence on transition may be nonnegligible [11]. When a droplet transits from the Cassie-Baxter state to the Wenzel state, the potential energy of gravity E_G declines as well. Since the potential energy change occurs along with the transition process between Cassie-Baxter state and the critical state when the droplet is about to immerse the air pockets completely but have not yet reached the bottom surface, the energy curves can be modified by adding the potential energy change of which the

sign is negative. When $\theta_Y < 90^\circ$, the energy curve is similar to Figure 4(c), where the energy

change is monotonous. However, for $\theta_Y > 90^\circ$, one more case appears as shown in figure 5:





Figure 5 Energy curves with gravity effect for $\theta_Y > 90^\circ$

234

Figure 5 shows the extra curve of case 3 when considering the gravity effect with a monotonous energy change, which denotes that the transition can occur spontaneously. In this case, the source of potential energy change ΔE_G can overcome the energy barrier E_{bar}^{CB-Cr} , and the conclusion is the same with that from Patankar, N. A. [11] which is achieved via comparing the theoretical analysis with experimental data from Yoshimitsu et al [26].

240

241 2.3 Discussion about the irreversibility of wetting transition

As mentioned above, it is generally thought that the transition from Cassie-Baxter state to Wenzel state is irreversible. From figure 5 it can be seen that the gravity potential energy can decrease the energy barrier E_{bar}^{CB-W} or even overcome it. Besides, other external stimuli such as initial velocity, pressure and vibration can also be also used to overcome the energy barrier. Therefore, in most cases the Cassie-to-Wenzel transition is easier to be achieved, and more attention is paid on this transition due to its importance to superhydrophobic surfaces development.

249

Without considering the gravity effect, the reverse Wenzel-to-Cassie transition would take a different route. It is reasonable to assume the transition happens on the bottom from the vicinity 252 of the gas-liquid-solid triple line, since air cannot be generated from the void, as shown in 253 Figure 6. Therefore, the triple lines may move simultaneously in the horizontal and vertical 254 directions. The energy decreased as solid-liquid contact area decreases may overcome the 255 energy increased as liquid-gas contact area and solid-gas contact area increase, and if not, the 256 reversible transition cannot occur spontaneously. Figure 6 presents the different routes of 257 wetting transitions. It should be noticed that the reverse energy change may not be monotonous 258 in Figure 7(a) in the case that the droplet is separated from the bottom but the vertical process 259 has not finished yet, and in Figure 7(b) the critical Young's angle for the Wenzel-to-Cassie transition may not be the same with the critical angle in Equation (6). 260







Figure 7 Free energy curves without gravity effect for (a) $90^{\circ} < \theta_Y < \theta_C$ (b) $\theta_Y > \theta_C$ Gravity potential can be considered as a part of the energy barrier needed to overcome. It is much more difficult to trigger the reverse transition than the Cassie-to-Wenzel transition due to the different transition routes, which can explain the irreversibility of wetting transition. Experiments to achieve the reverse transition were carried out by heating the substrate [36] or transmitting a short pulse of electrical current [26], and

both of the two experiments appeared to be conducted by the evaporation of the droplet in the vicinity of their gas-liquid-solid triple line, changing liquid phase to vapor phase to break the reverse energy barrier and complete the reverse transition. Thus a metastable Cassie-Baxter wetting state can be achieved as shown in Figure 7(a).

276

The energy curves shown in Figure 7 can be very helpful to understand the wetting 277 transition mechanism and develop superhydrophobic surfaces. Some surfaces with 278 279 topographic features involving specialized geometries such as inverse trapezoidal [37], T-shape [38] and serif-T [39] are the typical examples to impede Cassie-to-Wenzel 280 281 wetting transition by increasing the energy barrier during Cassie-to-critical process, namely raising the critical state energy in Figure 7. However, few papers were found to 282 283 focus on the critical-to-Wenzel process, which could also be a crucial factor to affect wetting transition because no matter how high the critical state energy is the Cassie-to-284 Wenzel transition can be finished when the energy barrier is overcame by external 285 286 forces. Such work relating to the bottom surface as well as the critical-to-Wenzel 287 process will be investigated in the future.

288

289 **3 Numerical simulation**

290 In this section, the simulation with a phase field lattice Boltzmann method with large density 291 ratio developed by Y. Q. Zu [40] is implemented to study the wetting states. As shown in Figure 292 8, a spherical water droplet with the initial radius $30\mu m$ is placed on the patterned surfaces in 293 different wetting states and different Young's contact angles. In the simulation, a = d = h = $5\mu m$, and the critical Young's angle $\theta_C = 115.4^\circ$ calculated via equation (6). Young's angles 294 θ_{Y} of 105° and 130° are set for a Wenzel preferable and a Cassie-Baxter preferable states. 295 The water/gas properties are set naturally as: $\rho_L = 1000 kg/m^3$, $\rho_G = 1.204 kg/m^3$, $\mu_L =$ 296 $1 \times 10^{-3} kg/(m \cdot s)$, $\mu_G = 1.9 \times 10^{-5} kg/(m \cdot s)$ for the density and dynamic viscosity, 297 298 respectively. Gravity is not considered in the simulation because it can be seen as an external 299 force to trigger the transition.

After evolving for 2,000,000 δ_t (20*ms*), where δ_t is the time step of LBM, all the droplets go stable and the shapes of the droplets do not change anymore. Eventually, for $\theta_Y = 105^\circ$, both Wenzel state and Cassie-Baxter state can be achieved with the apparent contact angles 119° and 137°, while for $\theta_Y = 130^\circ$, there is just the Cassie-Baxter state left, with $\theta_{CB} =$ 158°. The apparent contact angles calculated by equation (3) and equation (5) are 121.2°, 144.6° and 155.6° respectively, which are close to the present simulation data.



309 Figure 8 Wetting states for different Young's angles, $\theta_C = 115.4^\circ$, $t = 2,000,000\delta_t$ (a) 310 $\theta_Y = 105^\circ$, Wenzel state (b) $\theta_Y = 105^\circ$, Cassie-Baxter state (c) $\theta_Y = 130^\circ$, Cassie-Baxter 311 state

312 The dynamic wetting transition on an intrinsically hydrophilic surface with $\theta_Y = 75^\circ$ is 313 simulated, as shown in Figure 9. The stable Cassie-Baxter state cannot be observed as the 314 transition occurs spontaneously without any external forces.









320 of 130° being initially placed on the patterned surface in a Wenzel state. It can be clearly seen 321 that the transition occurs on the patterned surface from the vicinity of the three phase line.



328 The simulations are in good agreement with the proposed energy curves. The droplet in Cassie-329 Baxter state in Figure 8(b) has a higher free energy compared to the droplet in Wenzel state, but 330 it can keep steady, which means there is an energy barrier existing between the two wetting 331 states. In addition, the simulation excludes the influence from the roughness of much smaller 332 order of sizes which might be a factor to determine the two wetting state in experimental studies. 333 When the intrinsic contact angle is 75°, smaller than 90°, there is no stable Cassie-Baxter state 334 observed. The transition occurs spontaneously without any external forces, which means there 335 is no energy barrier between the two wetting states. For a higher inherent contact angle $\theta_Y =$ 336 130° the Wenzel state in the simulation is unstable and the Wenzel-to-Cassie occurs 337 spontaneously, confirming the reverse transition route in Figure 7(b). However, when testing some cases in which the Young's angles are between 130° and the critical angle, the reverse 338 339 transition cannot be observed. This means the critical contact angle for Wenzel-to-Cassie transition is not the same as the one determining the same energies of Cassie-Baxter state andWenzel state.

342

343

344 **4** Conclusions

345 In this paper, the wetting transitions for a droplet on a square-post patterned surface are theoretically analyzed. Numerical simulations with a phase field lattice Boltzmann method 346 347 were carried out, and the results show good agreement with the theoretical analysis. The main 348 finding of this work is that the energy curves during wetting transitions are proposed for Cassie-349 to-Wenzel transition together with the reverse transition via the theoretical analysis of the free 350 energy changes during the transitions processes. The energy curves give a clear description of 351 the conditions in which the transitions occur and the energy barriers exist for both transition processes. Gravity effect for wetting transition is considered, and the energy curves illustrate 352 353 that the gravity can be a driving force to trigger the transition. The irreversibility is discussed 354 based on the energy curves presented. The Wenzel-to-Cassie transition can occur spontaneously 355 only if the inherent contact angle is large enough. It can also be concluded from the curves that different routes of the Cassie-to-Wenzel transition and the reverse transition are the main reason 356 for the irreversibility of wetting transitions. The work is based on the regular square-post 357 358 patterned surface, which is also the basis of most complicated rough surfaces. Therefore the presented energy curves can be very helpful to understand the mechanism of complex wetting 359 360 phenomena.

- 361
- 362

363 Acknowledgement

The authors would like to acknowledge the financial support of this work by the doctoral degree
scholarship of China Scholarship Council and the University of Nottingham, UK.

366

368 **References**

369

370 1. Li L, Liu X, Dai X J, et al. (2013) Surface wetting processing on BNNT films by selective plasma 371 modes. Chin Sci Bull 58:3403-3408 372 Yao J, Wang J, Yu Y, et al. (2012) Biomimetic fabrication and characterization of an artificial rice 2. 373 leaf surface with anisotropic wetting. Chin Sci Bull 57:2631-2634 374 3. Yao Z, Hao P, Zhang X, et al. (2012) Static and dynamic characterization of droplets on 375 hydrophobic surfaces. Chin Sci Bull 57:1095-1101 376 Yan Y (2009) Physical and numerical modelling of biomimetic approaches of natural 4. 377 hydrophobic surfaces. Chin Sci Bull 54:541-548 378 5. Gao N, Yan Y, Chen X, et al. (2012) Nanoparticle-induced morphology and hydrophilicity of 379 structured surfaces. Langmuir 28:12256-65 380 Huang Y, Hu Y, Zhu C, et al. (2016) Long-Lived Multifunctional Superhydrophobic 6. 381 Heterostructure Via Molecular Self-Supply. Adv Mater Interfaces 3:1500727 382 7. Koch K, Bhushan B, and Barthlott W (2009) Multifunctional surface structures of plants: an 383 inspiration for biomimetics. Prog Mater Sci 54:137-178 384 8. Young T (1805) An essay on the cohesion of fluids. Philos Trans R Soc London 95:65-87 385 9. Wenzel R N (1949) Surface Roughness and Contact Angle. J Phys Chem 53:1466-1467 386 10. Cassie A and Baxter S (1944) Wettability of porous surfaces. Trans Faraday Society 40:546-551 387 11. Patankar N A (2004) Transition between superhydrophobic states on rough surfaces. Langmuir 388 20:7097-7102 389 12. Gao N and Yan Y (2009) Modeling Superhydrophobic Contact Angles and Wetting Transition. J 390 Bionic Eng 6:335-340 391 13. Yan Y, Gao N, and Barthlott W (2011) Mimicking natural superhydrophobic surfaces and 392 grasping the wetting process: A review on recent progress in preparing superhydrophobic 393 surfaces. Adv Colloid Interface Sci 169:80-105 394 14. Marmur A and Bittoun E (2009) When Wenzel and Cassie are right: reconciling local and global 395 considerations. Langmuir 25:1277-1281 396 15. Marmur A (2008) From hygrophilic to superhygrophobic: theoretical conditions for making 397 high-contact-angle surfaces from low-contact-angle materials. Langmuir 24:7573-7579 398 16. Ran C, Ding G, Liu W, et al. (2008) Wetting on nanoporous alumina surface: transition between 399 Wenzel and Cassie states controlled by surface structure. Langmuir 24:9952-9955 400 17. Jung Y C and Bhushan B (2007) Wetting transition of water droplets on superhydrophobic 401 patterned surfaces. Scripta Mater 57:1057-1060 402 18. Koishi T, Yasuoka K, Fujikawa S, et al. (2009) Coexistence and transition between Cassie and 403 Wenzel state on pillared hydrophobic surface. Proc Natl Acad Sci U S A 106:8435-40 404 19. Bormashenko E (2010) Wetting transitions on biomimetic surfaces. Philos Trans A Math Phys 405 Eng Sci 368:4695-711 406 20. Bormashenko E (2015) Progress in understanding wetting transitions on rough surfaces. Adv 407 Colloid Interface Sci 222:92-103 408 21. Lafuma A and Quéré D (2003) Superhydrophobic states. Nat Mater 2:457-460 409 22. Jung Y C and Bhushan B (2009) Dynamic effects induced transition of droplets on biomimetic

410		superhydrophobic surfaces. Langmuir 25:9208-9218
411	23.	McHale G, Aqil S, Shirtcliffe N, et al. (2005) Analysis of droplet evaporation on a
412		superhydrophobic surface. Langmuir 21:11053-11060
413	24.	Bormashenko E, Pogreb R, Whyman G, et al. (2007) Resonance Cassie-Wenzel wetting
414		transition for horizontally vibrated drops deposited on a rough surface. Langmuir 23:12217-
415		12221
416	25.	Bahadur V and Garimella S V (2008) Electrowetting-based control of droplet transition and
417		morphology on artificially microstructured surfaces. Langmuir 24:8338-8345
418	26.	Krupenkin T N, Taylor J A, Wang E N, et al. (2007) Reversible wetting-dewetting transitions on
419		electrically tunable superhydrophobic nanostructured surfaces. Langmuir 23:9128-9133
420	27.	Zu Y and Yan Y (2016) Single Droplet on Micro Square-Post Patterned Surfaces-Theoretical
421		Model and Numerical Simulation. Sci Rep 6:
422	28.	Whyman G and Bormashenko E (2012) Wetting transitions on rough substrates: General
423		considerations. J Adhes Sci Technol 26:207-220
424	29.	Ren W (2014) Wetting transition on patterned surfaces: transition states and energy barriers.
425		Langmuir 30:2879-85
426	30.	Pashos G, Kokkoris G, and Boudouvis A G (2015) Minimum energy paths of wetting transitions
427		on grooved surfaces. Langmuir 31:3059-68
428	31.	Pashos G, Kokkoris G, Papathanasiou A G, et al. (2016) Wetting transitions on patterned
429		surfaces with diffuse interaction potentials embedded in a Young-Laplace formulation. J Chem
430		Phys 144:034105
431	32.	Prakash S, Xi E, and Patel A J (2016) Spontaneous recovery of superhydrophobicity on
432		nanotextured surfaces. Proc Natl Acad Sci 201521753
433	33.	Bico J, Thiele U, and Quéré D (2002) Wetting of textured surfaces. Colloids Surf Physicochem
434		Eng Aspects 206:41-46
435	34.	Bormashenko E, Pogreb R, Stein T, et al. (2008) Characterization of rough surfaces with vibrated
436		drops. Phys Chem Chem Phys 10:4056-4061
437	35.	Zu Y, Yan Y, Li J, et al. (2010) Wetting behaviours of a single droplet on biomimetic micro
438		structured surfaces. J Bionic Eng 7:191-198
439	36.	Liu G, Fu L, Rode A V, et al. (2011) Water droplet motion control on superhydrophobic surfaces:
440		exploiting the Wenzel-to-Cassie transition. Langmuir 27:2595-2600
441	37.	Im M, Im H, Lee J-H, et al. (2010) A robust superhydrophobic and superoleophobic surface with
442		inverse-trapezoidal microstructures on a large transparent flexible substrate. Soft Matter
443		6:1401-1404
444	38.	Cai T-m, Jia Z-h, Yang H-n, et al. (2016) Investigation of Cassie-Wenzel Wetting transitions on
445		microstructured surfaces. Colloid Polym Sci 294:833-840
446	39.	Liu T L and Kim C J (2014) Repellent surfaces. Turning a surface superrepellent even to
447		completely wetting liquids. Science 346:1096-100
448	40.	Zu Y Q and Yan Y Y (2011) Lattice Boltzmann method for modelling droplets on chemically
449		heterogeneous and microstructured surfaces with large liquid-gas density ratio. IMA J Appl
450		Math 76:743-760